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(54) **CIRCULAR DICHROISM DETECTION SYSTEM**

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**G01J 4/00** (2006.01)

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(58) **Field of Classification Search** ..... None  
See application file for complete search history.

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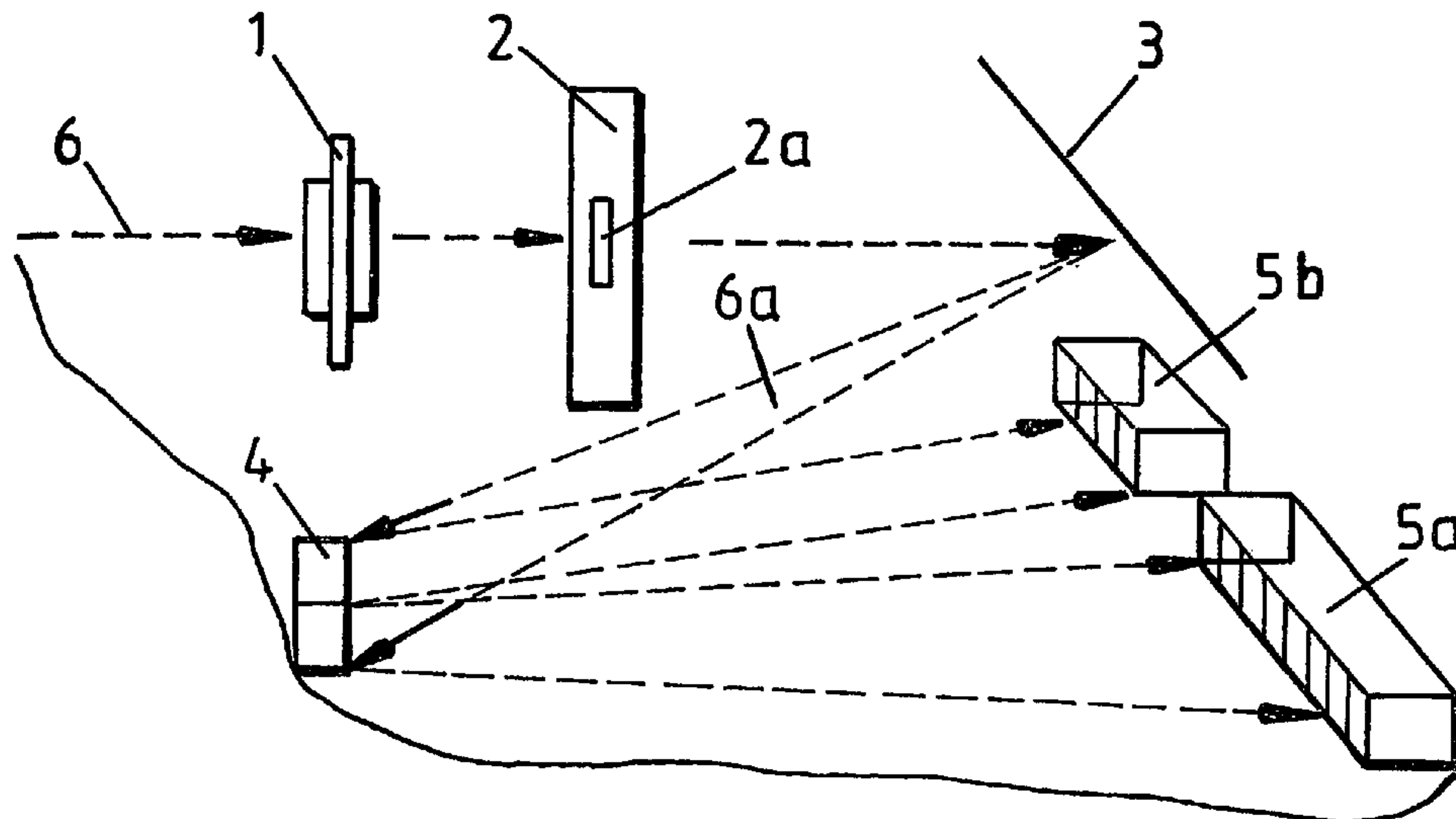
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(57) **ABSTRACT**

A detection system includes a modulator to apply a circular polarization modulation to an incident beam of radiation, a sample holder through which the modulated beam is pass, a grating to diffract the beam of radiation, an array of solid state detectors arranged to receive different wavelengths of the beam, and a process arranged to synchronise detected signals with the modulation applied by the modulator, in order to measure the spectral circular dichroism of the sample.

**51 Claims, 4 Drawing Sheets**



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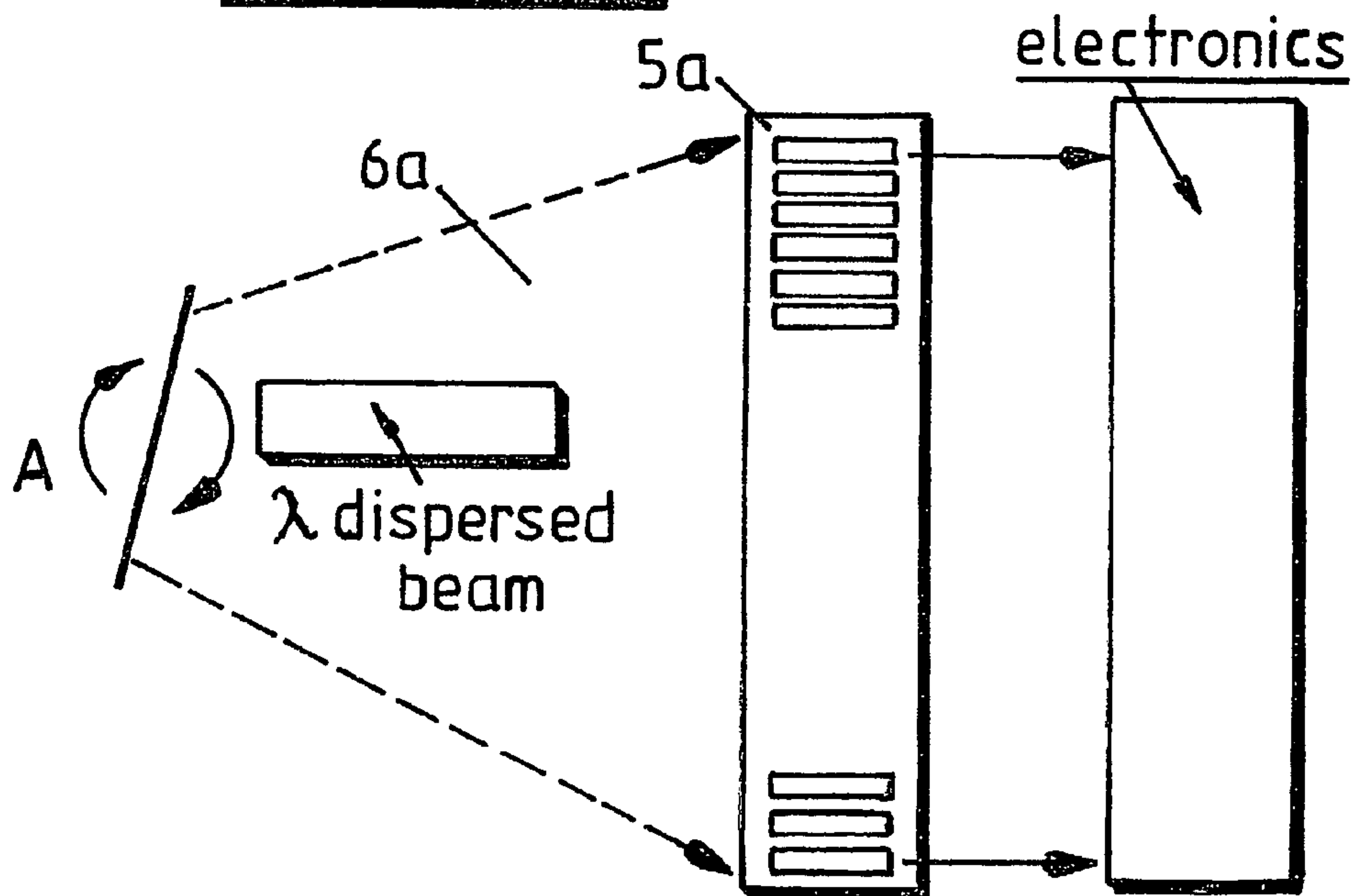
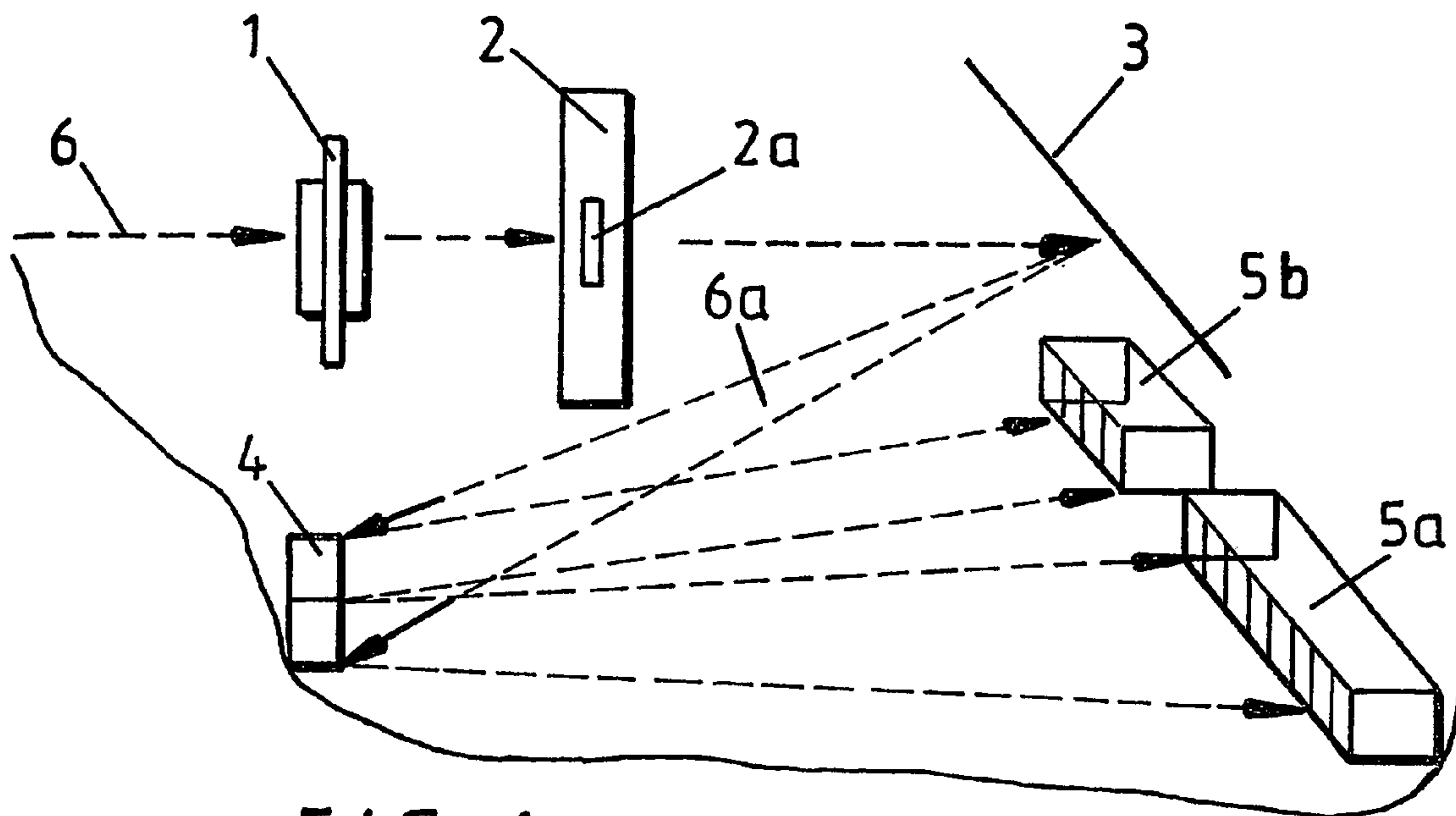
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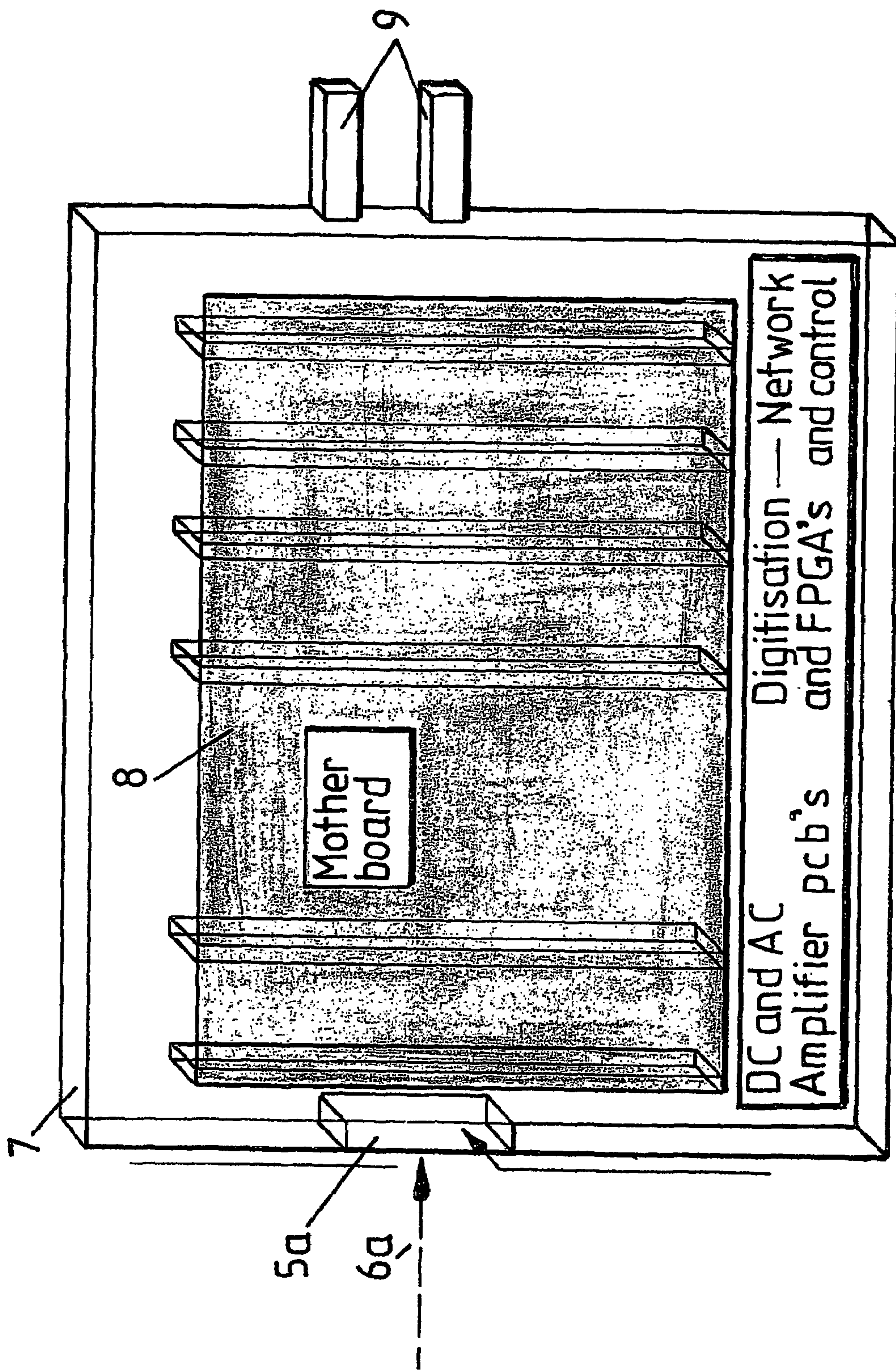


FIG. 3

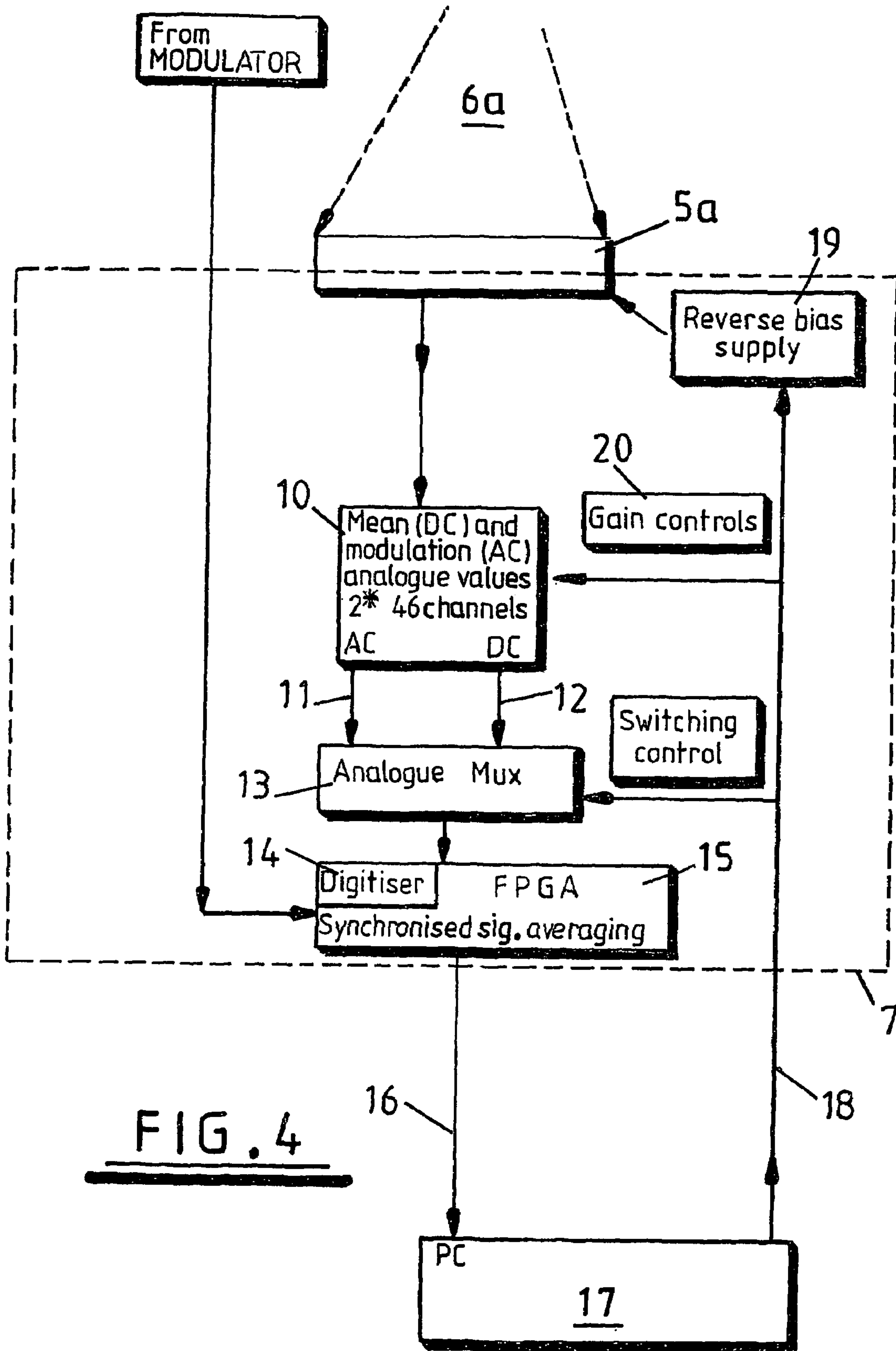


FIG. 4

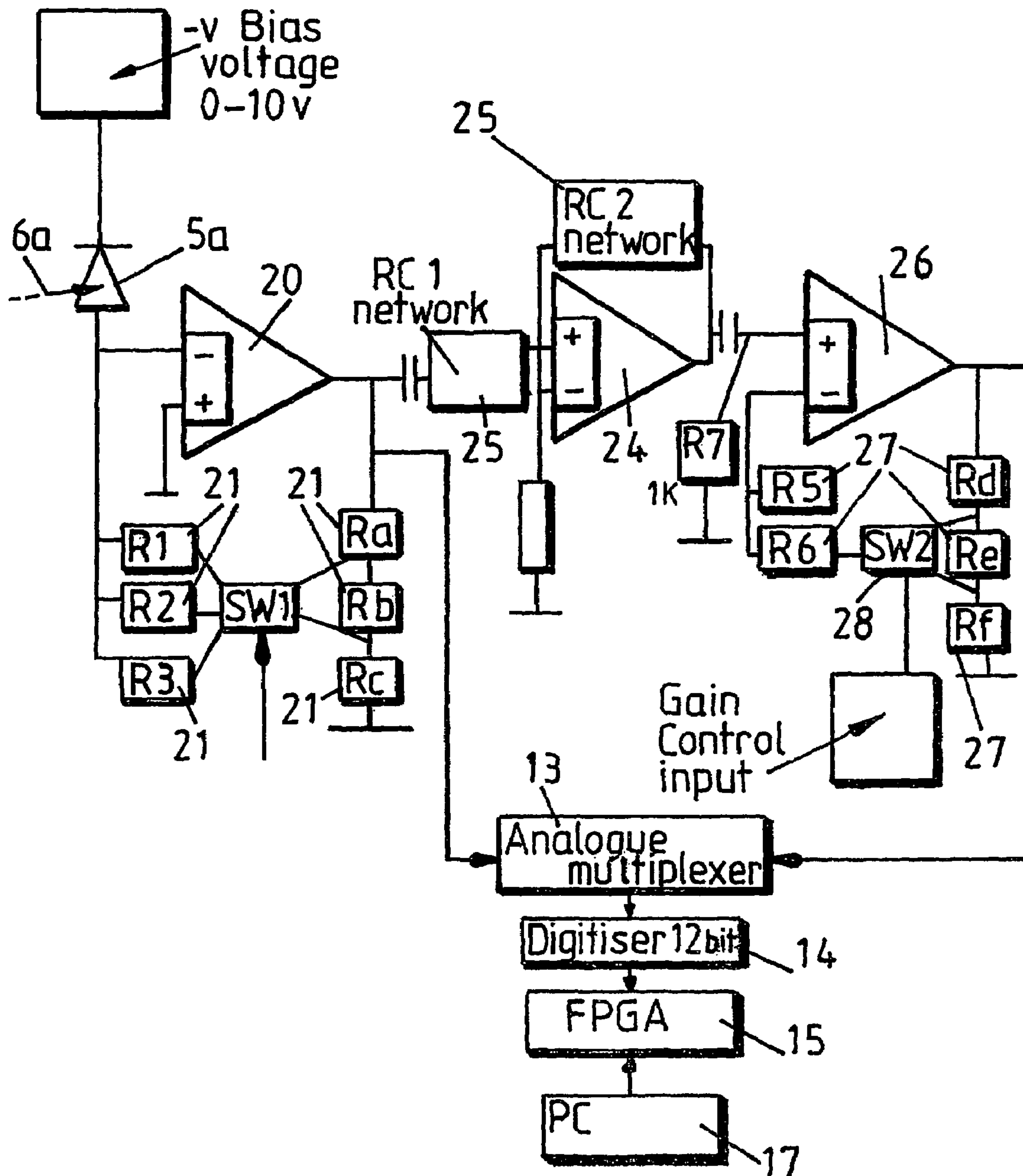


FIG. 5



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**CIRCULAR DICHROISM DETECTION SYSTEM**

This application is the U.S. national phase under 35 U.S.C. § 371 of PCT International Application No. PCT/GB2004/000365, which has an International filing date of Jan. 30<sup>th</sup>, 2004, designating the United States of America, and claims the benefit of British Patent Application No. 0302378.5, which was filed Feb. 1, 2003.

**BACKGROUND AND SUMMARY OF THE INVENTION**

The present invention relates to a detection system, and particularly though not exclusively to a detection system suitable for detecting circular dichroism.

Circular dichroism is the differential absorption between left and right circularly polarised light on passage through a sample. When light passes through a sample, linear absorbance of the light occurs with the result that the amount of light that passes from the sample is less than the amount of light that passed into the sample. Measuring this difference provides a measurement of the linear absorbance of the sample. When the light is circularly polarised a secondary absorbance component arises from circular dichroism. The secondary absorbance component is measured by switching between left and right circularly polarised light, and measuring the resulting difference in absorbance.

Measurement of circular dichroism gives detailed structural and enantiomeric (handedness) information on proteins, carbohydrates, nucleic acids, pharmaceuticals, liquid crystals, etc. With circular dichroism one can follow e.g. the conversion of simple peptides into the destructive fibrils of CJD, Alzheimer's, cystic fibrosis etc. Handedness was at the heart of the thalidomide disaster.

Since circular dichroism is a secondary component of the measurement of absorbance, it is a difficult property to measure. Typically the absorbance due to circular dichroism is around one part in  $10^5$  of the mean intensity of light transmitted by a sample. Measurement is further complicated by the fact that absorbance measurements are often performed at ultraviolet and deep ultraviolet wavelengths (i.e. <200 nm).

It is conventional to detect circular dichroism by modulating the polarisation of light incident on a sample using a polarising modulator, and then detecting the modulation of light transmitted by the sample using phase-locked detection. The polarising modulator is for example configured to switch the polarisation of the incident light beam between left hand polarisation and right hand polarisation at a frequency of 50 kHz, and the phase-locked detector measures at 50 kHz light incident upon the detector. This allows detection of circular dichroism which effectively comprises a small AC signal on a very large DC background.

Conventionally, a single element detection system is used to detect circular dichroism. The system comprises a photo multiplier tube with a high dynamic range (typically  $10^9$ ), coupled to a phase-locked signal extraction amplifier that is able to distinguish the circular dichroism signal from the background signal. The detection system uses a servo system to adjust the high tension on the photo multiplier to produce a constant DC current output, independent of the intensity of DC light incident upon the photo multiplier tube. This is done to compensate for changes of beam intensity and of linear absorbance as the wavelength of the incident light is scanned (the beam intensity and linear absorbance may change by four orders of magnitude). The constant DC current output is

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advantageous because it provides a constant DC level from which the AC circular dichroism signal may be easily phase-locked extracted.

The wavelength range of interest is scanned wavelength by wavelength (with about 1 nm resolution). The scanning process takes many minutes when the circular dichroism signal is strong, but many hours when the circular dichroism signal is weaker (as is the case for most useful circular dichroism work).

It is an object of the present invention to provide a detection system which overcomes or mitigates at least one of the above disadvantages.

According to a first aspect of the invention there is provided a detection system comprising modulation means for applying a modulation to an incident beam of radiation, sample holding means through which the modulated beam of radiation is passed, beam expansion means to expand the beam of radiation, an array of solid state detectors arranged to receive different parts of the expanded beam of radiation, and processing means arranged to synchronise detected signals with the modulation applied by the modulation means.

The detection system is advantageous because the use of an array of solid state detectors, rather than the single detector used by the prior art, allows more information to be determined from the detected signals.

Preferably, the processing means further comprises amplification means to amplify signals detected by the array of solid state detectors.

The detectors are preferably solid state detectors although other forms of detector, such as for instance multi-channel photo-multipliers could be used.

Preferably, the processing means further comprises digitisation means to digitise detected signals.

Preferably, the processing means is arranged to digitise detected signals before they are synchronised with the modulation applied by the modulation means. This is advantageous as compared to the conventional approach of synchronising before digitisation, since it provides faster and more sensitive measurement.

The beam expansion means may comprise wavelength separation means arranged to convert the beam of radiation into a diverging fan of wavelengths.

Preferably, the wavelength separation means comprises a reflective grating.

Preferably, the system further comprises a steering mirror, the orientation of the steering mirror being adjustable to allow selection of the wavelengths of the fan that are incident upon the array of solid state detectors.

The beam expansion means may comprise means for expanding the beam of radiation whilst retaining spatial properties of the beam in at least one direction perpendicular to the direction of propagation of the beam of radiation.

Preferably, the array of solid state detectors is a two dimensional array.

Wavelength separation may be provided in a first direction perpendicular to the direction of propagation of the beam of radiation, and beam expansion whilst retaining spatial properties may be provided in a second direction perpendicular to the direction of propagation of the beam of radiation, the two dimensional array being used to detect wavelength dependent properties and spatial properties of the expanded beam.

Preferably, the array of solid state detectors comprises a first array of photodiodes arranged to detect near ultraviolet wavelengths, and a second array of photodiodes arranged to detect deep ultraviolet wavelengths.

Preferably, the first array of photodiodes comprises silicon.



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Preferably, the second array of photodiodes comprises AlGaIn.

Preferably, the modulation means is configured to apply a modulated circular polarisation to the beam of radiation. It will be appreciated that other forms of modulation may be applied to the beam of radiation.

Preferably, the modulation means is configured to apply a modulation at a frequency greater than 1 kHz.

Preferably, the sample holding means is provided with an adjustable aperture, which allows adjustment of the width of beam incident upon a sample.

Preferably, each detector of the array of solid state detectors is provided with a transconductance amplifier arranged to convert photocurrent output by the detector into a voltage.

Preferably, the transconductance amplifier is provided with a plurality of resistors which may be connected to the transconductance amplifier in different combinations using a switch, to modify the gain of the transconductance amplifier.

Preferably, the switch is controlled by a microprocessor.

Preferably, each detector of the array of solid state detectors is provided with an AC amplifier arranged to amplify AC components of a signal detected by the solid state detector.

Preferably, the AC amplifier is provided with a plurality of resistors which may be connected to the transconductance amplifier in different combinations using a switch, to modify the gain of the AC amplifier.

Preferably, the switch is controlled by a microprocessor.

Preferably, the system is provided with a band pass filter tuned to the frequency of operation of the modulation means.

Preferably, the system further comprises a multiplexor arranged to multiplex, for each detector of the array of solid state detectors, a DC signal and an AC signal after amplification.

Preferably, synchronisation is performed by a field programmable array. The skilled person will appreciate that a field programmable array (FPGA) is a known form of commercially available programmable electronic circuit which may be integrated on a single chip with very fast operation and small size. A single chip may contain very large numbers (in excess of 20,000) semi conductor gates that can be configured to form discrete electronic function circuits, such as adders and the like. The circuit can then be programmed to perform arithmetic operations, such as addition, subtraction and division, very rapidly. The ability to re-configure such arrays is an advantage over existing ASIC technology.

Preferably, the system further comprises a personal computer arranged to receive data, and to control operation of components of the system.

Preferably, the array of solid state detectors is translatable and pivotable to allow it to be aligned with the beam.

According to a second aspect of the invention there is provided a detection system comprising modulation means for applying a modulation to an incident beam of radiation, sample holding means through which the modulated beam is passed, at least one solid state detector, and processing means arranged to amplify and digitise signals detected by the at least one detector, and then to subsequently synchronise the amplified and digitised signal with the modulation applied by the modulation means.

The second aspect of the invention is advantageous because it provides detection which is faster and more sensitive than conventional circular dichroism measurement systems, where the signal is synchronised with the polarising modulator before it is digitised.

The second aspect of the invention may further comprise any of the preferred features of the first aspect of the invention.

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According to a third aspect of the invention there is provided a detection method comprising applying a modulation to an incident beam of radiation, passing the modulated beam of radiation through a sample held in a sample holding means, expanding the beam of radiation, detecting different part of the expanded beam of radiation using an array of solid state detectors, synchronising detected signals with the applied modulation.

Preferably, the detected signals are amplified.

Preferably, the detected signals are digitised.

Preferably, the detected signals are digitised before they are synchronised with the applied modulation.

According to a fourth aspect of the invention there is provided a detection method comprising applying a modulation to an incident beam of radiation, passing the modulated beam of radiation through a sample, detecting the beam of radiation using at least one solid state detector, amplifying and digitising the signals detected by the at least one detector, and then subsequently synchronising the amplified and digitised signals with the applied modulation.

The fourth aspect of the invention may further comprise any of the preferred features of the second aspect of the invention.

## BRIEF DESCRIPTION OF THE DRAWINGS

A specific embodiment of the invention will now be described by way of example only, with reference to the accompanying figures, in which:

FIG. 1 is a schematic perspective view of optical components of an embodiment of the invention;

FIG. 2 is a schematic view from above of part of FIG. 1;

FIG. 3 is a schematic view of the physical configuration of electronic component of the embodiment of the invention;

FIG. 4 is a schematic diagram showing the electronic components of the embodiment of the invention; and

FIG. 5 is a schematic circuit diagram showing part of the circuit in more detail.

## DETAILED DESCRIPTION OF THE INVENTION

Referring to FIG. 1, optical components of a detection system comprise a polarising modulator 1, a sample cell 2, a reflective grating 3, a mirror 4, and detector arrays 5a, 5b. A beam 6 of synchrotron radiation, which comprises electromagnetic radiation at an ultraviolet wavelength, is directed through the polarising modulator 1. The polarising modulator 1, which is electrostatic, is switched at a frequency of 50 kHz and polarises the ultraviolet beam of radiation to have a left or right handed circular polarisation (the handedness of the polarisation switches at 50 kHz).

The polarised beam 6 passes through the sample cell 2, which contains a protein sample. The sample cell 2 is provided with an aperture 2a which is adjustable in size, the aperture 2a typically being arranged to allow a beam of approximately 4 mm diameter into the sample cell 2. The polarised beam 6 is absorbed by the protein sample, linear absorption occurring together with absorption due to circular dichroism. Upon exiting the sample cell, the attenuated beam 6 comprises a DC component and a low intensity 50 kHz AC component (the AC component arising from the dichroic absorption of the polarisation modulated light).

The beam 6 passes to the reflective grating 3, which has a 1 nm per mm dispersion characteristic. The grating separates the beam 6 into a fan 6a of different wavelengths, as shown schematically in FIG. 1. The fan 6a is incident upon the mirror 4 which, in addition to steering the fan 6a to the



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detector arrays **5a**, **5b** is used to provide wavelength band selection. The detector arrays **5a**, **5b** comprise a first silicon array **5a** which is capable of detecting near ultraviolet, and a second AlGaIn array **5b** which is capable of detecting deep ultraviolet.

FIG. 2 shows the steering mirror **4** and the near UV detector array **5a** from above. The detector array **5a** comprises a linear array of silicon photodiodes, which are manufactured by Hamamatsu Photonics KK of Japan (product number 4114-46Q-SP). The array comprises 46 photodiodes each 4.6 by 0.9 mm. It will be appreciated that, since the fan **6a** provides wavelength separation, each photodiode will detect a different wavelength of light. The wavelength detected by each photodiode may be adjusted by rotating the steering mirror **4**. Rotation of the steering mirror **4** in the clockwise direction, as shown by the arrows A in FIG. 2, will move shorter wavelengths onto the detector array **5a**, and move longer wavelengths off the detector array **5a**. Rotation of the steering mirror **4** in the anticlockwise direction will move longer wavelengths onto the detector array **5a**, and move shorter wavelengths off the detector array **5a**. The wavelength band detected by each photodiode may be broadened or narrowed by increasing or decreasing respectively the path length between the reflective grating **3** and the array **5a**. Alternatively, a reflective grating **3** with a different dispersion characteristic may be used. Output signals from the array **5a** are passed to electronics which are described in detail further below.

The optical components of the detection system, as shown in FIGS. 1 and 2, are advantageous because they allow simultaneous parallel detection of light at different wavelengths, instead of requiring serial wavelength measurements as is the case with the prior art. This allows circular dichroism (circular dichroism) measurements to be made quickly, in the order of seconds or faster, rather than over several hours.

Referring to FIG. 3, the detector array **5a** is located at a left hand end of a box **7**. The box contains a mother board **8** onto which electronics used to process signals output by the sensor array **5a** are located. Buses **9** carry data from the electronics to a personal computer (PC). The box **7** is mounted upon a translatable mounting which allows the box **7** to be translated accurately in any required direction. The mounting also includes pivot controls which allow the box **7** to be angled in any direction. This combination of translation and pivoting is advantageous because it allows the sensor array **5a** to be located in a preferred region of the dispersed ultraviolet beam and at a preferred angle.

FIG. 4 shows schematically the electronics held within the box **7**. The sensor array **5a** is located at an exterior wall of the box **7** as shown. Photocurrents output from each photodiode of the sensor array **5a** are passed to AC and DC gain controlled amplifiers **10**. The photocurrents are shown as passing via a single connection **10a** for ease of illustration (a separate connection is provided for each photodiode of the sensor array **5a**).

The DC gain controlled amplifier is a transconductance amplifier, and is used to convert the photodiode photocurrent into an output voltage. The AC gain controlled amplifier amplifies the AC component of the photocurrent, and provides an AC voltage output **11**. The DC gain controlled amplifier amplifies the DC component of the photocurrent, and provides a DC voltage output **12**. Separate amplifiers **10** and outputs **11**, **12** are provided for each photodiode of the sensor array **5a**, although only one is shown in FIG. 4 for ease of illustration.

A multiplexor **13** is used to multiplex the AC and DC signals such that an AC signal relating to a given photodiode

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channel is multiplexed with a DC signal for that channel. In FIG. 4 only one output signal is shown for ease of illustration, whereas the multiplexor **13** has 46 outputs. The use of the multiplexor is advantageous because it reduces the number of data carrying channels from 92 (separate AC and DC channels for each photodiode) to 46 (a single channel carrying multiplexed AC and DC for each photodiode). The multiplexor outputs the multiplexed photodiode signals to a digitiser **14**. The digitiser **14** digitises analogue voltages to 12 bits, 4096 levels, at 33 MHz.

Following digitisation, the AC signals are synchronised to the modulation of the polarising modulator (**1** in FIG. 1) by a field programmable array **15**. The fast programmable array (FPGA) comprises three 16 channel FPGA's. These are programmed in firmware to perform the synchronisation. All output signals are treated in parallel by the FPGA, thereby synchronising all of the signals with respect to the modulation of the polarising modulator. The FPGA's are programmed to, integrate the signal average over a selected number of synchronisation periods. The synchronisation period depends on the frequency of modulation of the polarising modulator, and will typically be of the order of 20 micro seconds for a full period (comprising two half periods of 10 micro seconds which determine the left and right handed intervals of polarisation). In application other than CD detection, faster modulation could be used with synchronisation periods down to the digitalisation time (typically 50 nano seconds) or better. Each period of left and right-handed polarisation is detected and integrated separately. Integration is performed to average the required signal by adding the digital values of the selected sample within each synchronisation period and then add together a selected number of synchronisation periods for each polarisation and divide by the total number of samples.

The digital signal output by the FPGA's is passed via a 32 bit digital bus **16** to a PC **17** for processing. The PC **17** determines the integration period for signal measurement, subtracts background signals from measured signals, determines the ratio of modulated signal to mean signal (AC to DC) levels, stores data, and displays instantaneous and integrated data. In addition, the PC **17** controls via a control output **18** operation of components located within the box **7**. The PC **17** controls the reverse bias which is supplied to the sensor array **5a** by a reverse bias supply **19**, thereby controlling the sensitivity of the sensor array **5a**. The PC **17** also controls the gain of the AC and DC amplifiers via gain controls **20**. In addition, the PC **17** controls operation of the analogue multiplexor **13**.

The AC and DC amplifier **10** will now be described in more detail, with reference to FIG. 5. A single photodiode **5c** of the photodiode array **5a** is shown in FIG. 5. Similarly, a single AC and DC amplifier arrangement is shown rather than the 46 amplifier arrangements that are used to amplify signals generated by each photodiode **5c** of the photodiode array **5a**. The photocurrent output from the photodiode **5c** passes to an inverting input of a transimpedance amplifier **20**. The transimpedance amplifier **20** amplifies the DC component and the AC component of the signal (i.e. the entire signal is amplified), and provides an output voltage. The gain provided by the transimpedance amplifier **20** is determined by feedback resistors **21**. The gain is adjusted by selecting combinations of resistors **21** using a switch **22** which is controlled by the PC **17** (see FIG. 4). An output from the transimpedance amplifier **20** is split to provide two signals. The capacitor **23** allows the majority of the AC component of the signal output by the transimpedance amplifier **20** to pass to a band pass amplifier **24**, whereas a substantially DC signal is passed to the multiplexor **13**.



Gain control steps of factors of 10 in the DC stage are required to compensate for the variation of DC beam absorption with respect to wavelength. The DC beam absorption will vary by a factor of 100 between 190 nm and 200 nm. In prior art photo-multiplier tubes the gain must be continually adjusted as the wavelength of the light changes. In contrast to this, when the invention is used the wavelength of light detected by each photodiode does not change over time. This means that the gain may be set separately for each photodiode (each photodiode detects a different wavelength) and may then remain fixed. This is a substantial advantage over the prior art. In addition, the fact that detection for all wavelengths takes place during a time period of a few seconds means that gain does not need to be adjusted to take account of time dependent variation of beam intensity (the time scale for such variations is around 1 hour).

The combination of resistors which is used provide gain adjustment is set out on the following table:

R1	200K	Ra	50K * 1
R2	2 M	Rb	25K * 2
R3	10 M	Rc	25K * 4

Different combinations of these resistors are connected together using the switch 22.

The capacitor 23 allows the AC components of the signal output by the transimpedance amplifier 20 to pass to a 50 kHz band pass amplifier 24. A RC network 25 is used to tune the amplifier 24 to 50 kHz. A separate amplifier 26 provides controlled gain for the 50 kHz signal, the gain being selected by selecting a combination of resistors 27 using a switch 28. The gain is controlled by the PC 17 (see FIG. 4). The output signal is passed to the analogue multiplexor 13. Subsequent components of the system are as described in relation to FIG. 4.

The magnitude of the AC circular dichroism signal will vary, for example due to protein to protein variation. The variation is likely to be by roughly factors of 2. These are compensated for using the resistors 27, values of which are given in the following table:

		Rd	17K * 1.0
R5	200K * 200	Re	16K * 1.2
R6	400K * 400	Rf	66k * 1.5

The switches 22, 28 are controlled by the PC 17, which specifies the switch settings for each photodiode 5c. The switch 22 at the DC amplifier may provide nine different gain options, and these may be specified using a 4-bit code. The switch 28 at the AC amplifier may provide six different gain options, and these may be specified using a 3-bit code. Hence, the PC 17 is able to specify a given photodiode 5c, and specify DC and AC gain for that photodiode using a 16-bit word (the switches 22, 28 are controlled digitally). The configuration of the switches may be changed between measurements to provide desired DC and AC gains.

Two amplifiers 20, 26 are used to provide independently adjustable gain for the DC signal and the AC signal, in order to obtain a circular dichroic signal with an optimum signal to noise ratio. The peak photodiode current is around 4.8  $\mu$ A per photodiode of the array 5a. This means that the transimpedance amplifier 20 has a transimpedance of 200 k $\Omega$ , to obtain an output of 1V. The AC gain control amplifier 26 provides a

voltage gain of 500, to provide an AC signal output with a peak-to-peak value of approximately 1V (this is based upon the AC signal being  $1/500$  of the DC signal).

Communication between the PC 17 and the FPGA 15 and other components of the detection system electronics is provided by an Ethernet link. The Ethernet link carries control signals to the detection system electronics, for example the gain control signal described above. Other control signals carried by the Ethernet link include signal averaging and integration commands, and control signals for the multiplexor 13. The integration period may vary between 10 microseconds (1 sync pulse period) and 10 seconds.

The Ethernet link carries raw spectrum data from the detection system electronics after collection (the spectrum data comprises both DC and AC data). The data is stored in the FPGA's during collection.

A display unit (not shown) is connected to the PC, and is used to display DC and AC<sub>p-p</sub> (peak to peak) spectra. The display also shows the circular dichroism spectra as calculated by the PC (circular dichroism=AC<sub>p-p</sub>/DC).

Photodiodes are available which may be used as an alternative to the silicon photodiodes described above. For instance, photodiodes manufactured by United Detector Technology may be used to detect deep ultraviolet signals (i.e. <200 nm) or calibrated to operate in the near ultraviolet wavelength region.

Although FIGS. 2, 3 and 4 have been described with reference to the near UV detector array 5a, it will be appreciated that the deep UV detector array 5b of Al<sub>x</sub>Ga<sub>1-x</sub>N photodiodes may be connected, used, and the signals generated from those photodiodes processed, in an essentially identical fashion.

The use of Al<sub>x</sub>Ga<sub>1-x</sub>N to detect deep UV is well known. A typical deep UV detector array 5b may comprise a ternary Al<sub>x</sub>Ga<sub>1-x</sub>N (Aluminium Gallium Nitride) compound semiconductor as its active, or UV detecting material. Al<sub>x</sub>Ga<sub>1-x</sub>N is a direct bandgap semiconductor, therefore having greater absorption efficiency than indirect bandgap semiconductors. In this particular compound, a subscript 'x' denotes the percentage (or 'atomic ratio') of Al in a specific compound and hence the ratio of Al:Ga in the ternary compound semiconductor. For example, for a 40% Al content, the ternary compound Al<sub>x</sub>Ga<sub>1-x</sub>N would read Al<sub>40</sub>Ga<sub>60</sub>N.

UV detectors made from Al<sub>x</sub>Ga<sub>1-x</sub>N have a tuneable cutoff wavelength between 365 nm and 200 nm, a specific wavelength being defined by selecting and implementing an appropriate value for the atomic ratio 'x'. Above this cutoff wavelength, little or no radiation is detected. Thus the deep UV detector array 5b can be tuned to have an upper cutoff wavelength that slightly overlaps the detectable range of the near UV detector 5a, whilst having a greater detection efficiency in the deep UV thus complimenting the near UV detector array 5b. By having a near UV detector array 5a and a deep UV detector array, each array 5a, 5b can be optimised for, or tuned to, a particular part of a (UV) spectrum. The upper cutoff wavelength may also be defined by an experimental region of interest. For example, in CD measurement, the upper cutoff may conveniently be 260 nm. To achieve this value, the atomic ratio 'x' is substantially 40%. The atomic ratio may be greater than 40%, thus increasing the range of detectable wavelengths by increasing the value of the upper cutoff wavelength.

Undoped AlGa<sub>n</sub> layers may be grown on a sapphire substrate using epitaxial methods, such as Metal Organic Chemical Vapour Deposition (MOCVD) or Molecular Beam Epitaxy (MBE). The AlGa<sub>n</sub> layer and sapphire substrate each have a lattice constant. If the lattice constants are not substantially equivalent (mismatched), crystal defects, such as



cracks, may form in the AlGa<sub>N</sub> layers. To prevent this from occurring, the mismatch in lattice constants must be reduced. Thus any strain on the AlGa<sub>N</sub> layers due to the mismatch is reduced, and the probability of any resultant defects occurring reduced accordingly. This is achieved by growing a layer 5 between the AlGa<sub>N</sub> layer and the sapphire substrate with a lattice constant of a value that is between that of the AlGa<sub>N</sub> layer and sapphire substrate. Such a layer may be a Ga<sub>N</sub> layer. Furthermore, to optimise growth of the layers and to prevent the propagation of any cracks that may, nevertheless, develop, 10 the AlGa<sub>N</sub> layers may be graded or be interspersed with thin AlN (Aluminium Nitride) layers.

Interdigitated photo-detecting structures are formed on the Al<sub>x</sub>Ga<sub>1-x</sub>N material using metal-semiconductor-metal configurations with alternate Schottky-Ohmic contacts. The size of the photo-detecting structures and any gaps between them may be varied according to the application. For example, the structures and their dimensions may be optimised with respect to response time and/or signal strength.

It will be appreciated that in timing the cutoff wavelength of the Al<sub>x</sub>Ga<sub>1-x</sub>N, the range of wavelengths which the deep UV detector array 5*b* can detect is also tuneable. Thus, if detection of wavelengths above a certain value is undesirable, the upper limit of this range can be defined to exclude these wavelengths. It will be appreciated that by excluding undesirable wavelengths, this may improve the signal to noise ratio of any measurements made by reducing background noise.

The active, or UV detecting material may be another material with a high absorption efficiency with regard to deep UV radiation. Such a material may be SiC (Silicon Carbide) or Diamond. It will also be appreciated that a substrate of a material other than sapphire may be used. The substrate must have a good crystal quality, chemical inertness and thermal matching. In the case of light detectors, the layer must be transparent. For example, Si (111) may be used as the substrate material.

Although the composition of the deep UV detector array 5*b* may vary, it will be appreciated that regardless of this fact, the detection system itself operates in an identical manner.

The detection system described above may be operated for capture times of 50 ns or lower. This means that fast changes of circular dichroism with respect to time may be measured using the detection system, the measurements being wavelength resolved.

The invention may be used to provide spatial image measurements of circular dichroism. This is done by replacing the reflective grating 3 with reflective optics which expand the beam 1 such that different spatial zones of the beam are incident upon different photodiodes 5*c* of the array 5*a* (or 5*b*). The photodiode array 5*a* (or 5*b*) may be replaced with a two-dimensional array to allow two-dimensional spatial imaging.

A mixture of wavelength resolved and spatial imaging measurements may be obtained using the invention. This may be done for example by using a combination of the reflective grating 3 to obtain wavelength resolution in the horizontal direction, and beam expansion optics arranged to spatially expand the beam in the vertical direction (a two-dimensional array is required when this is done).

The detection system works in a manner which is completely opposite to the conventional measurement of circular dichroism. The detection system amplifies and digitises detected signals, and then subsequently synchronises the signals with the polarising modulator. This is faster and more sensitive than conventional circular dichroism measurement

systems, where the signal is synchronised with the polarising modulator before it is digitised.

The amplification and detection, together with the digitisation and synchronisation is performed by the detection using firmware. This allows the detection system to operate at high speeds (50 ns capture times or lower), allowing time resolved measurements to be performed.

Although the described embodiment of the invention relates to the measurement of circular dichroism, it will be appreciated that the invention may be used for other applications requiring the extraction of a small modulated signal from a high background signal. Examples include laser pulsed fluorescence and synchronisation to a synchrotron radiation.

The invention claimed is:

1. A circular dichroism detection system comprising a modulator to apply a modulation to an incident beam of radiation, a sample cell through which the modulated beam of radiation is passed, a beam expander to expand the beam of radiation, an array of detectors arranged to receive different parts of the expanded beam of radiation, and a processor arranged to synchronise detected signals with the modulation applied by the modulator, wherein the modulator is configured to apply a modulated circular polarisation to the beam and is configured to apply a modulation at a frequency greater than 1 kHz, the processor further comprising a digitiser arranged to digitise detected signals before they are synchronised with the modulation applied by the modulator.

2. The circular dichroism detection system according to claim 1, wherein the detectors are solid state detectors.

3. The circular dichroism detection system according to claim 2, wherein the processing means further comprises an amplifier to amplify signals detected by the array of solid state detectors.

4. The circular dichroism detection system according to claim 1, wherein the beam expander comprises a wavelength separator arranged to convert the beam into a diverging fan of wavelengths.

5. The circular dichroism A detection system according to claim 4, wherein the wavelength separator comprises a reflective grating.

6. The circular dichroism detection system according to claim 4, wherein the system further comprises a steering mirror, the orientation of the steering mirror being adjustable to allow selection of the wavelengths of the fan that are incident upon the array of detectors.

7. The circular dichroism detection system according to claim 1, wherein the beam expander comprises optics to expand the beam of radiation whilst retaining spatial properties of the beam of radiation in at least one direction perpendicular to the direction of propagation of the beam of radiation.

8. The circular dichroism detection system according to claim 2, wherein the array of solid state detectors is a two dimensional array.

9. The circular dichroism detection system according to claim 4, wherein wavelength separation is provided in a first direction perpendicular to the direction of propagation of the beam of radiation, and beam expansion whilst retaining spatial properties is provided in a second direction perpendicular to the direction of propagation of the beam of radiation, the two dimensional array being used to detect wavelength dependent properties and spatial properties of the expanded beam.

10. The circular dichroism detection system according to claim 2, wherein the array of solid state detectors comprises a first array of photodiodes arranged to detect near ultraviolet



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wavelengths, and a second array of photodiodes arranged to detect deep ultraviolet wavelengths.

11. The circular dichroism detection system according to claim 10, wherein the first array of photodiodes is a silicon photodiode array.

12. The circular dichroism detection system according to claim 10, wherein the second array of photodiodes is an AlGaIn photodiode array.

13. The circular dichroism detection system according to claim 1, wherein the sample cell is provided with an adjustable aperture, which allows adjustment of the width of beam incident upon a sample.

14. The circular dichroism detection system according to claim 2, wherein each detector of the array of solid state detectors is provided with a transconductance amplifier arranged to convert photocurrent output by the detector into a voltage.

15. The circular dichroism detection system according to claim 14, wherein the transconductance amplifier is provided with a plurality of resistors which may be connected to the transconductance amplifier in different combinations using a switch, to modify the gain of the transconductance amplifier.

16. The circular dichroism detection system according to claim 15, wherein the switch is controlled by a microprocessor.

17. The circular dichroism detection system according to claim 2, wherein each detector of the array of solid state detectors is provided with an AC amplifier arranged to amplify AC components of a signal detected by the solid state detector.

18. The circular dichroism detection system according to claim 17, wherein the AC amplifier is provided with a plurality of resistors which may be connected to the transconductance amplifier in different combinations using a switch, to modify the gain of the AC amplifier.

19. The circular dichroism detection system according to claim 18, wherein the switch is controlled by a microprocessor.

20. The circular dichroism detection system according to claim 1, wherein the system is provided with a band pass filter tuned to the frequency of operation of the modulator.

21. The circular dichroism detection system according to claim 2, wherein the system further comprises a multiplexer arranged to multiplex, for each detector of the array of solid state detectors, a DC signal and an AC signal after amplification.

22. The circular dichroism detection system according to claim 1, wherein synchronisation is performed by a fast programmable array.

23. The circular dichroism detection system according to claim 1, wherein the system further comprises a personal computer arranged to receive data, and to control operation of components of the system.

24. The circular dichroism detection system according to claim 2, wherein the array of solid state detectors is translatable and pivotable to allow it to be aligned with the beam.

25. A circular dichroism detection system comprising a modulator to apply a modulation to an incident beam of radiation, a sample cell through which the modulated beam is passed, at least one solid state detector, and processor arranged to amplify and digitise signals detected by the at least one detector, and then to subsequently synchronise the amplified and digitised signal with the modulation applied by the modulator, wherein the modulator is configured to apply a modulated circular polarisation to the beam and is configured to apply a modulation at a frequency greater than 1 kHz, the processor further comprising a digitiser arranged to digitise

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detected signals before they are synchronized with the modulation applied by the modulator.

26. A circular dichroism detection method comprising applying a modulation to an incident beam of radiation, passing the modulated beam of radiation through a sample held in a sample cell, expanding the beam of radiation, detecting different part of the expanded beam of radiation using an array of solid state detectors, synchronising detected signals with the applied modulation, wherein applying the modulation includes applying a modulated circular polarization to the beam and applying the modulation at a frequency of greater than 1 kHz and digitising the detected signals before they are synchronized with the applied modulation.

27. The circular dichroism detection method according to claim 26, wherein the detected signals are amplified.

28. A circular dichroism detection method comprising applying a modulation to an incident beam of radiation, passing the modulated beam of radiation through a sample, detecting the beam of radiation using at least one solid state detector, amplifying and digitising the signals detected by the at least one detector, and then subsequently synchronising the amplified and digitised signals with the applied modulation, wherein applying the modulation includes applying a modulated circular polarization to the beam and applying the modulation at a frequency of greater than 1 kHz and digitising the detected signals before they are synchronized with the applied modulation.

29. The circular dichroism detection system according to claim 3, wherein the processor further comprises a digitiser to digitise detected signals.

30. The circular dichroism detection system according to claim 29, wherein the processor is arranged to digitise detected signals before they are synchronised with the modulation applied by the modulator.

31. The circular dichroism detection system according to claim 1, wherein the beam expander comprises a wavelength separator arranged to convert the beam into a diverging fan of wavelengths.

32. The circular dichroism detection system according to claim 2, wherein the beam expander comprises a wavelength separator arranged to convert the beam into a diverging fan of wavelengths.

33. The circular dichroism detection system according to claim 32, wherein the wavelength separator comprises a reflective grating.

34. The circular dichroism detection system according to claim 5, wherein the system further comprises a steering mirror, the orientation of the steering mirror being adjustable to allow selection of the wavelengths of the fan that are incident upon the array of detectors.

35. The circular dichroism detection system according to claim 2, wherein the system further comprises a steering mirror, the orientation of the steering mirror being adjustable to allow selection of the wavelengths of the fan that are incident upon the array of solid state detectors.

36. The circular dichroism detection system according to claim 34, wherein the beam expander comprises optics to expand the beam of radiation whilst retaining spatial properties of the beam of radiation in at least one direction perpendicular to the direction of propagation of the beam of radiation.

37. The circular dichroism detection system according to claim 35, wherein the array of solid state detectors is a two dimensional array.

38. The circular dichroism detection system according to claim 7, wherein wavelength separation is provided in a first direction perpendicular to the direction of propagation of the



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beam of radiation, and beam expansion whilst retaining spatial properties is provided in a second direction perpendicular to the direction of propagation of the beam of radiation, the two dimensional array being used to detect wavelength dependent properties and spatial properties of the expanded beam.

39. The circular dichroism detection system according to claim 8, wherein wavelength separation is provided in a first direction perpendicular to the direction of propagation of the beam of radiation, and beam expansion whilst retaining spatial properties is provided in a second direction perpendicular to the direction of propagation of the beam of radiation, the two dimensional array being used to detect wavelength dependent properties and spatial properties of the expanded beam.

40. The circular dichroism detection system according to claim 36, wherein wavelength separation is provided in a first direction perpendicular to the direction of propagation of the beam of radiation, and beam expansion whilst retaining spatial properties is provided in a second direction perpendicular to the direction of propagation of the beam of radiation, the two dimensional array being used to detect wavelength dependent properties and spatial properties of the expanded beam.

41. The circular dichroism detection system according to claim 39, wherein the array of solid state detectors comprises a first array of photodiodes arranged to detect near ultraviolet wavelengths, and a second array of photodiodes arranged to detect deep ultraviolet wavelengths.

42. The circular dichroism detection system according to claim 11, wherein the second array of photodiodes is an AlGaIn photodiode array.

43. The circular dichroism detection system according to claim 41, wherein the sample cell is provided with an adjustable aperture, which allows adjustment of the width of beam incident upon a sample.

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44. The circular dichroism detection system according to claim 42, wherein each detector of the array of solid state detectors is provided with a transconductance amplifier arranged to convert photocurrent output by the detector into a voltage.

45. The circular dichroism detection system according to claim 16, wherein each detector of the array of solid state detectors is provided with an AC amplifier arranged to amplify AC components of a signal detected by the solid state detector.

46. The circular dichroism detection system according to claim 19, wherein the system is provided with a band pass filter tuned to the frequency of operation of the modulator means.

47. The circular dichroism detection system according to claim 45, wherein the system further comprises a multiplexor arranged to multiplex, for each detector of the array of solid state detectors, a DC signal and an AC signal after amplification.

48. The circular dichroism detection system according to claim 46, wherein synchronisation is performed by a fast programmable array.

49. The circular dichroism detection system according to claim 47, wherein the system further comprises a personal computer arranged to receive data, and to control operation of components of the system.

50. The circular dichroism detection system according to claim 48, wherein the array of solid state detectors is translatable and pivotable to allow it to be aligned with the beam.

51. The circular dichroism detection method according to claim 27, wherein the detected signals are digitised.

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