



US00RE48347E

(19) **United States**
(12) **Reissued Patent**
Mugler, III et al.

(10) **Patent Number:** **US RE48,347 E**
(45) **Date of Reissued Patent:** ***Dec. 8, 2020**

(54) **METHOD AND APPARATUS FOR SPIN-ECHO-TRAIN MR IMAGING USING PRESCRIBED SIGNAL EVOLUTIONS**

(52) **U.S. Cl.**
CPC **G01R 33/5615** (2013.01); **G01R 33/50** (2013.01); **G01R 33/5617** (2013.01); **G01R 33/586** (2013.01)

(71) Applicant: **University of Virginia Patent Foundation**, Charlottesville, VA (US)

(58) **Field of Classification Search**
CPC **G01R 33/5615**; **G01R 33/50**; **G01R 33/5617**; **G01R 33/586**

(72) Inventors: **John P. Mugler, III**, Charlottesville, VA (US); **James R. Brookeman**, Charlottesville, VA (US)

(Continued)

(73) Assignee: **University of Virginia Patent Foundation**, Charlottesville, VA (US)

(56) **References Cited**

U.S. PATENT DOCUMENTS

(*) Notice: This patent is subject to a terminal disclaimer.

4,520,315 A 5/1985 Loeffler et al.
4,684,892 A 8/1987 Graumann

(Continued)

(21) Appl. No.: **16/195,079**

OTHER PUBLICATIONS

(22) Filed: **Nov. 19, 2018**

Schaffter, T., "PSF Improvements in Single Shot GRASE Imaging", Proceedings of the Society of Magnetic /K.W/ Resonance, 1994. Second Meeting, San Francisco. p. 27.

(Continued)

Related U.S. Patent Documents

Reissue of:

(64) Patent No.: **7,164,268**
Issued: **Jan. 16, 2007**
Appl. No.: **10/451,124**
PCT Filed: **Dec. 21, 2001**
PCT No.: **PCT/US01/50551**
§ 371 (c)(1),
(2) Date: **Jun. 19, 2003**
PCT Pub. No.: **WO02/50574**
PCT Pub. Date: **Jun. 27, 2002**

Primary Examiner — Kenneth Whittington
(74) *Attorney, Agent, or Firm* — Panitch Schwarze Belisario & Nadel LLP

U.S. Applications:

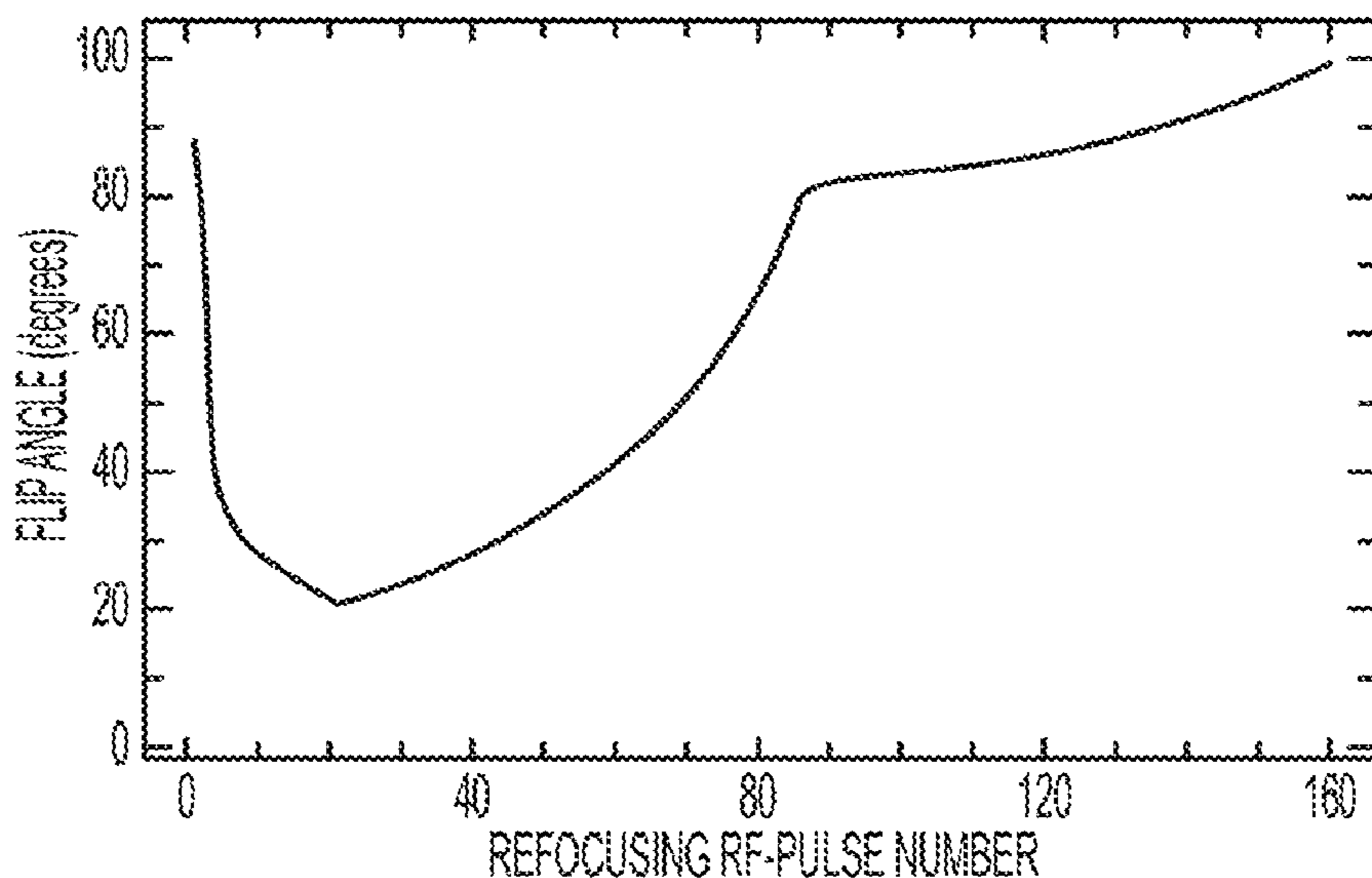
(63) Continuation of application No. 14/708,875, filed on May 11, 2015, now Pat. No. Re. 47,178, which is a
(Continued)

(57) **ABSTRACT**

A magnetic resonance imaging "MRI" method and apparatus for lengthening the usable echo-train duration and reducing the power deposition for imaging is provided. The method explicitly considers the t1 and t2 relaxation times for the tissues of interest, and permits the desired image contrast to be incorporated into the tissue signal evolutions corresponding to the long echo train. The method provides a means to shorten image acquisition times and/or increase spatial resolution for widely-used spin-echo train magnetic resonance techniques, and enables high-field imaging within the safety guidelines established by the Food and Drug Administration for power deposition in human MRI.

(51) **Int. Cl.**
G01R 33/561 (2006.01)
G01R 33/50 (2006.01)
G01R 33/58 (2006.01)

15 Claims, 8 Drawing Sheets



Related U.S. Application Data

continuation of application No. 14/053,190, filed on Oct. 14, 2013, now Pat. No. Re. 45,725, which is a continuation of application No. 12/354,471, filed on Jan. 15, 2009, now Pat. No. Re. 44,644, which is an application for the reissue of Pat. No. 7,164,268.

(60) Provisional application No. 60/257,182, filed on Dec. 21, 2000.

(58) **Field of Classification Search**
USPC 324/300–322; 600/410–423
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,695,800	A	9/1987	Kramer et al.	
4,703,271	A	10/1987	Loeffler et al.	
4,733,186	A	3/1988	Oppelt et al.	
4,769,603	A	9/1988	Oppelt et al.	
4,782,839	A	11/1988	Hennig et al.	
4,818,940	A	4/1989	Hennig et al.	
4,901,020	A	2/1990	Ladebeck et al.	
4,940,055	A	7/1990	Brown	
5,001,428	A	3/1991	Maier et al.	
5,189,370	A	2/1993	Kolem et al.	
5,214,382	A *	5/1993	Harms et al.	324/309
5,235,280	A	8/1993	Deimling	
5,245,282	A *	9/1993	Mugler et al.	324/309
5,256,967	A *	10/1993	Foo et al.	324/311
5,270,654	A	12/1993	Feinberg et al.	
5,304,929	A	4/1994	Fang et al.	
5,307,014	A	4/1994	Laub	
5,315,249	A	5/1994	LeRoux et al.	
5,315,250	A	5/1994	Ehnholm et al.	
5,337,000	A	8/1994	Bruder	
5,345,176	A	9/1994	LeRoux et al.	
5,345,178	A	9/1994	Manabe et al.	
5,347,216	A *	9/1994	Foo	324/309
5,391,990	A	2/1995	Schmitt et al.	
5,402,067	A *	3/1995	Pauly et al.	324/307
5,422,576	A	6/1995	Kao et al.	
5,432,448	A	7/1995	Heid et al.	
5,451,877	A	9/1995	Weissenberger	
5,459,401	A	10/1995	Kiefer	
5,541,511	A	7/1996	Hennig	
5,541,514	A	7/1996	Heid et al.	
5,545,992	A *	8/1996	Foo	324/309
5,553,619	A	9/1996	Prince	
5,557,204	A	9/1996	Lenz	
5,565,776	A	10/1996	Kanazawa	
5,583,437	A	12/1996	Smith et al.	
5,612,619	A	3/1997	Feinberg	
5,631,560	A	5/1997	Machida	
5,680,045	A	10/1997	Feinberg	
5,704,357	A *	1/1998	Miyazaki	G01R 33/4835 324/307
5,739,688	A	4/1998	Krieg	
5,746,208	A	5/1998	Prince	
5,749,834	A	5/1998	Hushek	
5,798,643	A	8/1998	Werthner	
6,020,739	A *	2/2000	Meyer et al.	324/309
6,075,362	A	6/2000	Loncar et al.	
6,230,039	B1	5/2001	Stuber et al.	
6,265,872	B1	7/2001	Heid	
6,320,378	B1	11/2001	Maier et al.	
6,404,194	B1 *	6/2002	Irrarrazabal et al.	324/307
6,445,182	B1	9/2002	Dean et al.	
6,456,071	B1	9/2002	Hennig	
6,472,870	B1	10/2002	Bendall et al.	
6,850,063	B2	2/2005	Hennig	
6,956,374	B2	10/2005	Busse	
7,164,268	B2	1/2007	Mugler, III et al.	
7,425,828	B2	9/2008	Garwood et al.	
7,847,551	B2	12/2010	Park	

8,040,135	B1	10/2011	Cukur et al.	
8,067,936	B2	11/2011	Garwood et al.	
8,228,060	B2	7/2012	Busse	
8,258,786	B2	9/2012	Hennel	
RE44,644	E *	12/2013	Mugler, III	324/307
RE45,725	E *	10/2015	Mugler, III	G01R 33/5602
RE47,178	E *	12/2018	Mugler, III	G01R 33/5615
2004/0051527	A1 *	3/2004	Mugler III et al.	324/309
2004/0090230	A1	5/2004	Appel et al.	
2008/0319301	A1	12/2008	Busse	
2010/0013479	A1	1/2010	Park	
2011/0288402	A1	11/2011	Pikkemaat et al.	

OTHER PUBLICATIONS

Slavin et al., “Dual-Echo Interleaved Echo-Planar Imaging of the Brain,” *Magnetic Resonance in Medicine*. vol. 33. nn. 254-270(1995).

Stuber et al., Submillimeter Three-dimensional Coronary MR Angiography with Real-time Navigator Correction: Comparison of Navigator Locations, *Radiology*, vol. 212, Issue No. 2, pp. 579-587.

Tim Luijkx & Matt Skalski, MRI Sequence Parameters, <<http://radiopaedia.org/articles/mri-sequence-parameters>>, Copyright © 2005-2016 Radiopaedia.org.

Tkach, et al., “A Comparison of Fast Spin Echo and Gradient Field Echo Sequences”, *Magnetic Resonance Imaging* 1988, vol. 6, p. 373-389.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. J—Invalidity of the ’644 Patent and 190 Application in view of Mugler, 3D Spin-Echo 1998 and the Mugler 3D Spin-Echo 1998 Disclosure.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. K—Invalidity of the ’644 Patent and 190 Application in view of Hennig 1988.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. L—Invalidity of the ’644 Patent and 190 Application in view of Hennig 1995 and/or the Hennig 1995 Disclosure.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. M.—Invalidity of the ’644 Patent and 190 Application in view Bishop 1994, the Bishop Disclosure, and/or the Bishop 1994 Research.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. N—Invalidity of the ’644 Patent and 190 Application in view of Mugler, Overview 1999.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. O—Invalidity of the ’644 Patent and 190 Application in view of Claim U.S. Pat. No. 5,245,282 to Mugler.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. P—Invalidity of the ’644 Patent and 190 Application in view of Stuber 1999.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. Q—Invalidity of the ’644 Patent and 190 Application in view of Haacke 1999.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. R—Invalidity of the ’644 Patent and 190 Application in view of Mugler 3D TurboSE Imaging 1999 Disclosure.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company*

(56)

References Cited

OTHER PUBLICATIONS

(Case No. 3:14-CV-00051-NKM-JCH), Exh. S—Invalidity of the '644 Patent and 190 Application in view of Mugler, Optimized 3D Spin-Echo Imaging 2000.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. T—Invalidity of the '644 Patent and 190 Application in view of the Mugler Advances in 3D MR Imaging 2000 Disclosure.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. U—Invalidity of the '644 Patent and 190 Application in view of Busse 2001.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. V—Invalidity of the '644 Patent and 190 Application in view of Mugler 1992.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. W—Invalidity of the '644 Patent and 190 Application in view of Mugler, Low-Flip Angle Refocusing RF Pulses 2001 and the Mugler Low-Flip Angle Refocusing RF Pulses 2001 Disclosure.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. X—Invalidity of the '644 Patent and 190 Application in view of Hennig, Hyperechoes Basic Principles 2001.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. Y—Invalidity of the '644 Patent and 190 Application in view of Hennig, Hyperechoes in RARE 2001.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. Z—Invalidity of the '644 Patent and 190 Application in view of Disclosure to Siemens of Draft Mugler, Imaging Using Very Long SE Trains 2000 (UVAPFGE006011-12, marked Confidential (CEO)).

John R. Hesselink, Basic Principles of MR Imaging, <<http://spinwarp.ucsd.edu/neuroweb/text/br-100.htm>>, Download date: Mar. 14, 2016, Earliest known posting date according to Internet Archive Wayback Machine: Oct. 6, 1999.

Jones, K.M., "Fast Spin-Echo MR Imaging of the Brain and Spine: Current Concepts", *AJR* 1992, 158, p. 1313-1320.

Kallmes, et al., "Suppression of Cerebrospinal Fluid and Blood Flow Artifacts in FLAIR MR Imaging with a Single-Slab Three-dimensional Pulse Sequence: Initial Experience", *Radiology* 2001, vol. 221, No. 1, p. 221-255.

Keiper, M.D., The Low Sensitivity of Fluid-Attenuated Inversion-Recovery MR in the Detection of Multiple Sclerosis of the Spinal Cord, *American Journal of Neuroradiology*, 1997, vol. 18, p. 1035-1039.

Leroux, P., "Stabilization of Echo Amplitudes in FSE Sequences", *Magnetic Resonance in Medicine*, 1993, vol. 30, p. 183-190.

Melki et al., Comparing the FAISE Method with Conventional Dual-Echo Sequences, *Journal of Magnetic Resonance Imaging*, vol. 1, pp. 319-326 (1991).

Melki, P.S., "Partial RF Echo Planar Imaging with the FAISE Method. I. Experimental and Theoretical Assessment of Artifact", *Magnetic Resonance in Medicine*, 1992, vol. 26, p. 328-341.

Mugler et al., "Shaping the Signal Response during the Approach to Steady State in Three-Dimensional Magnetization-Prepared Rapid Gradient-Echo Imaging Using Variable Flip Angles," *Magnetic Resonance in Medicine*, vol. 28, pp. 165-185.

Mugler III, et al., "Optimized Single-Slab Three-dimensional Spin-Echo MR Imaging of the Brain", *Radiology* 2000, vol. 216, No. 3, p. 891-899.

Mugler, "Overview of MR Imaging Pulse Sequences," *Physics of MR Imaging*, vol. 7, No. 4, pp. 661-697 (Nov. 1999).

Mugler, III, J.P., "Motion-Artifact-Free T2-Weighted 3D Imaging of the Cervical Spine", *Proceedings of the International Society for Magnetic Resonance in Medicine*, 2000. Eighth Meeting, Denver. p. 402.

Mugler, III, J.P., "Single-Slab Three-Dimensional FLAIR Imaging of the Brain", *Proceedings of the International Society for Magnetic Resonance in Medicine*, 1999. Seventh Meeting, Philadelphia. p. 8.

Mugler, III, J.P., "T1-Weighted and T2-Weighted 3D Spin-Echo-Based Imaging of the Whole Brain: 1 mm³ Resolution in Under 10 Minutes", *Proceedings of the International Society for Magnetic Resonance in Medicine*, 1998. Sixth Meeting, Sydney. p. 1959.

Mugler, III, J.P., "T2-Weighted 3D Spin-Echo Train Imaging of the Brain at 3 Tesla: Reduced Power Deposition Using Low Flip-Angle Refocusing RF Pulses", *Proceedings of the International Society for Magnetic Resonance in Medicine*, 2001. Ninth Meeting, Glasgow. p. 438.

Mugler, III, J.P., "Three-Dimensional Spin-Echo-Train Proton-Density-Weighted Imaging Using Shaped Signal Evolutions", *Proceedings of the International Society for Magnetic Resonance in Medicine*, 1999. Seventh Meeting, Philadelphia. p. 1631.

Mugler, III, J.P., Three-Dimensional T2-Weighted Imaging of the Brain Using Very Long Spin-Echo Trains, *Proceedings of the International Society for Magnetic Resonance in Medicine*, 2000. Eighth Meeting, Denver. p. 687.

Mulkern, R.V., "Contrast Manipulation and Artifact Assessment of 2D and 3D RARE Sequences", *Magnetic Resonance Imaging*, 1990, vol. 8, p. 557-566.

Nat'l. Inst. of Neurological Disorders and Stroke, Appendix II: Imaging parameters for MRI and protocols for MRI and CT.

Ortendahl, D.A., "Analysis of Hybrid Imaging Techniques", *Magnetic Resonance in Medicine*, 1992, vol. 26, p. 155-173.

Oshio, K., "GRASE (Gradient- and Spin-Echo) Imaging: A Novel Fast MRI Technique", *Magnetic Resonance in Medicine*, 1991, vol. 20, p. 344-349.

Patent Owner's Amended Preliminary Response, filed on Jan. 30, 2017 in IPR2017-00109.

Patent Owner's Amended Request for Rehearing, filed on Jul. 21, 2017 in IPR2016-00357.

Patent Owner's Response, filed on Jul. 13, 2017 in IPR2017-00109.

Patent Owner's Sur-reply, filed on Oct. 27, 2017 in IPR2017-00109.

Petition for Inter Partes Review of U.S. Pat. No. Re. 45,725, filed on Oct. 19, 2016.

Petitioner's Reply to Patent Owner's Response to Petition, filed on Nov. 28, 2016 in IPR2016-00357.

Petitioner's Reply to Patent Owner's Response to Petition, filed on Nov. 28, 2016 in IPR2016-00358.

Petitioner's Reply to Patent Owner's Response to Petition, filed on Nov. 28, 2016 in IPR2016-00359.

Petitioner's Reply to Patent Owner's Response to Petition, filed on Sep. 29, 2017 in IPR2017-00109.

Petitioner's Response to Patent Owner's Sur-reply, filed on Nov. 7, 2017 in IPR2017-00109.

Proceedings of the International Society for Magnetic Resonance in Medicine, Eighth Meeting, Denver, Apr. 1-7, 2000.

Proceedings of the International Society for Magnetic Resonance in Medicine, Seventh Meeting, Philadelphia, May 22-28, 1999.

Rydberg et al., "Comparison of dual-echo breathhold fast spin echo and dual-echo conventional T2-weighted spin echo imaging of liver lesions," *Proceedings of the International Society for Magnetic Resonance in Medicine*, Fifth Meeting, at 921 (1997).

"Patent Owner's Preliminary Response Under 37 CFR § 42.107" for *General Electric Co.(Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00357 for U.S. Pat. No. Re. 44,644.

"Patent Owner's Preliminary Response Under 37 CFR § 42.107" for *General Electric Co.(Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00358 for U.S. Pat. No. Re. 44,644.

"Patent Owner's Preliminary Response Under 37 CFR § 42.107" for *General Electric Co.(Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00359 for U.S. Pat. No. Re. 44,644.

(56)

References Cited

OTHER PUBLICATIONS

“Patent Owner’s Response for U.S. Pat. No. Re. 44,644”, *General Electric Co. (Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00357 dated Sep. 6, 2016.

“Patent Owner’s Response for U.S. Pat. No. Re. 44,644”, *General Electric Co. (Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00358 dated Sep. 6, 2016.

“Patent Owner’s Response for U.S. Pat. No. Re. 44,644”, *General Electric Co. (Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00359 dated Sep. 6, 2016.

“Petition for Inter Partes Review of U.S. Pat. No. Re. 44,644 Under 37 CFR § 42.104”, *General Electric Co. (Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00357.

“Petition for Inter Partes Review of U.S. Pat. No. Re. 44,644 Under 37 CFR § 42.104”, *General Electric Co. (Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00358.

“Petition for Inter Partes Review of U.S. Pat. No. Re. 44,644 Under 37 CFR § 42.104”, *General Electric Co. (Petitioner) v. University of Virginia Patent Foundation* (Patent Owner), IPR2016-00359.

Alsop, D.C., The Sensitivity of Low Flip Angle RARE Imaging, *Magnetic Resonance in Medicine*, 1997, vol. 37, p. 176-184.

Beatrice De Coene et al., MR of the Brain Using Fluid-Attenuated Inversion Recovery (FLAIR) Pulse Sequences, *AJNR* 13:1555-1564, Nov./Dec. 1992.

Bottomley et al., “A review of normal tissue hydrogen NMR relaxation times and relaxation mechanisms from 1-100 MHz: Dependence on tissue type, NMR frequency, temperature, species, excision, and age,” *Medical Physics*, vol. 11, pp. 425-448 (1984).

Busse, R.F., “Reducing SAR in Real-Time SSFSE Imaging with Variable-Flip Hard Refocusing RF Pulses”, *Proceedings of the International Society for Magnetic Resonance in Medicine*, 2001. Ninth Meeting, Glasgow. p. 1790.

Constable, R.T., “The Loss of Small Objects in Variable TE Imaging: Implications for FSE, RARE, and EPI”, *Magnetic Resonance in Medicine*, 1992, vol. 28, pp. 9-24.

Decision on Institution, filed on Apr. 26, 2017 in IPR2017-00109.

Decision on Institution, filed on Jun. 22, 2016 in IPR2016-00357.

Decision on Institution, filed on Jun. 23, 2016 in IPR2016-00358.

Decision on Institution, filed on Jun. 24, 2016 in IPR2016-00359.

Decision on Request for Rehearing, filed on Sep. 19, 2017 in IPR2016-00357.

Elster, et al., “Questions and Answers in Magnetic Resonance Imaging”, 2001, 2 ed., pp. 102-103.

Excerpt from Evan S. Siegelman, *Body MRI 3* (Elsevier Saunders 2014), <<http://www.slideshare.net/nyxdianagutierrez/body-mri>>.

Excerpt from Haacke, E., et al., *Magnetic Resonance Imaging: Physical Principles and Sequence Design* (John Wiley & Sons 1999).

Feinberg, D.A., “GRASE (Gradient- and Spin-Echo) MR Imaging: A New Fast Clinical Imaging Technique”, *Radiology*, 1991, vol. 181, No. 2, p. 597-602.

Final Written Decision, filed on Jun. 21, 2017 in IPR2016-00357.

Final Written Decision, filed on Jun. 21, 2017 in IPR2016-00358.

Final Written Decision, filed on Jun. 21, 2017 in IPR2016-00359.

Forsythe, G. E., “Computer Methods for Mathematical Computations”, Prentice-Hall, Englewood Cliffs, N.J., 1977, p. 156-177.

Glover, G. H., “Reduction of Non-Equilibrium Effects in RARE Sequences”, *Works in Progress Book of Abstracts, Tenth Annual Scientific Meeting and Exhibition, Society of Magnetic Resonance in Medicine*, 1991, San Francisco. p. 1242.

Haacke, E.M., “Magnetic Resonance Imaging: Physical Principles and Sequence Design”, John Wiley & Sons, New York, 1999, p. 51-64.

Hajnal, J.V., “Use of Fluid Attenuated Inversion Recovery (FLAIR) Pulse Sequences in MRI of the Brain”, *Journal of Computer Assisted Tomography*, 1992, vol. 16, No. 6, p. 841-844.

Hennig et al., “Single Shot 3D RARE: A Fast Method for Volumetric Acquisition,” *Proceedings of the Society of Magnetic Resonance and the European Society for Magnetic Resonance in Medicine and Biology; Twelfth Meeting, Nice, France*, p. 635.

Hennig, J., “Easy Improvement of Signal-to-Noise in RARE Sequences with Low Refocusing Flip Angles”, *Magnetic Resonance in Medicine*, 2000, vol. 44, p. 983-985.

Hennig, J., “Hyperechoes in RARE(TSE, FSE)-Sequences”, *Proceedings of the International Society for Magnetic Resonance in Medicine*, 2001. Ninth Meeting, Glasgow. p. 1769.

Hennig, J., “Hyperechoes”, *Magnetic Resonance in Medicine*, 2001, vol. 46, p. 6-12.

Hennig, J., “Hyperechoes—Basic Principles and Applications”, *Proceedings of the International Society for Magnetic Resonance in Medicine*, 2001. Ninth Meeting, Glasgow. p. 437.

Hennig, J., “Multiecho Imaging Sequences with Low Refocusing Flip Angles”, *Journal of Magnetic Resonance*, 1988, vol. 78, p. 397-407.

Hennig, J., “Multiecho Imaging Sequences with Variable Refocusing Flip Angles: Optimization of Signal Behavior Using Smooth Transitions Between Pseudo Steady States (TRAPS)”, *Magnetic Resonance in Medicine*, 2003, vol. 49, p. 527-535.

Hennig, J., “RARE Imaging: A Fast Imaging Method for Clinical MR”, *Magnetic Resonance in Medicine*, 1986, vol. 3, p. 823-833.

Hennig, Jürgen, Echoes—How to Generate, Recognize, Use or Avoid Them in MR-Imaging Sequences, Part I: Fundamental and Not So Fundamental Properties of Spin Echoes, *Concepts in Magnetic Resonance*, 1991, 3, 125-143.

Hittmair, K., “Spinal Cord Lesions in Patients with Multiple Sclerosis: Comparison of MR Pulse Sequences”, *American Journal of Neuroradiology*, 1996, vol. 17, p. 1555-1565.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Defendant’s Preliminary Invalidity Contentions Pursuant to Patent Local Rules 3-3 and 3-4, Aug. 25, 2015.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. A—Invalidity of the ’644 Patent and 190 Application in view of Mugler, *Imaging Using Very Long Spin-Echo Trains 2000* and/or the *Mugler Imaging Using Very Long Spin-Echo Trains 2000 Disclosure*.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. B—Invalidity of the ’644 Patent and 190 Application in view of Mugler, *3D Spin-Echo-Train Imaging 1999* and/or the *Mugler 3D Spin-Echo-Train Imaging 1999 Disclosure*.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. C—Invalidity of the ’644 Patent and 190 Application in view of Mugler, *Motion-Artifact-Free Imaging 2000* and the *Mugler Motion-Artifact-Free Imaging 2000 Disclosure*.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. D—Invalidity of the ’644 Patent and 190 Application in view of Schäffter 1994, the *Schäffter 1994 Disclosure*, and/or the *Schäffter 1994 Research*.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. E—Invalidity of the ’644 Patent and 190 Application in view of Schäffter 1994 Thesis Reference.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. F—Invalidity of the ’644 Patent and 190 Application in view of Alsop, *Low Flip Angle RARE Imaging 1997*.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. G—Invalidity of the ’644 Patent and 190 Application in view of Le Roux 1993.

Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. H—Invalidity of the

(56)

References Cited

OTHER PUBLICATIONS

'644 Patent and 190 Application in view of U.S. Pat. No. 5,345,176 to Le Roux et al./ U.S. Pat. No. 5,315,249 to Le Roux et al.
Invalidity Contention Documents served by Defendant in *University of Virginia Patent Foundation v. General Electric Company* (Case No. 3:14-CV-00051-NKM-JCH), Exh. I—Invalidity of the '644 Patent and '190 Application in view of Mugler 3D FLAIR Imaging 1999 and/or the Mugler 3D FLAIR Imaging 1999 Disclosure.

* cited by examiner

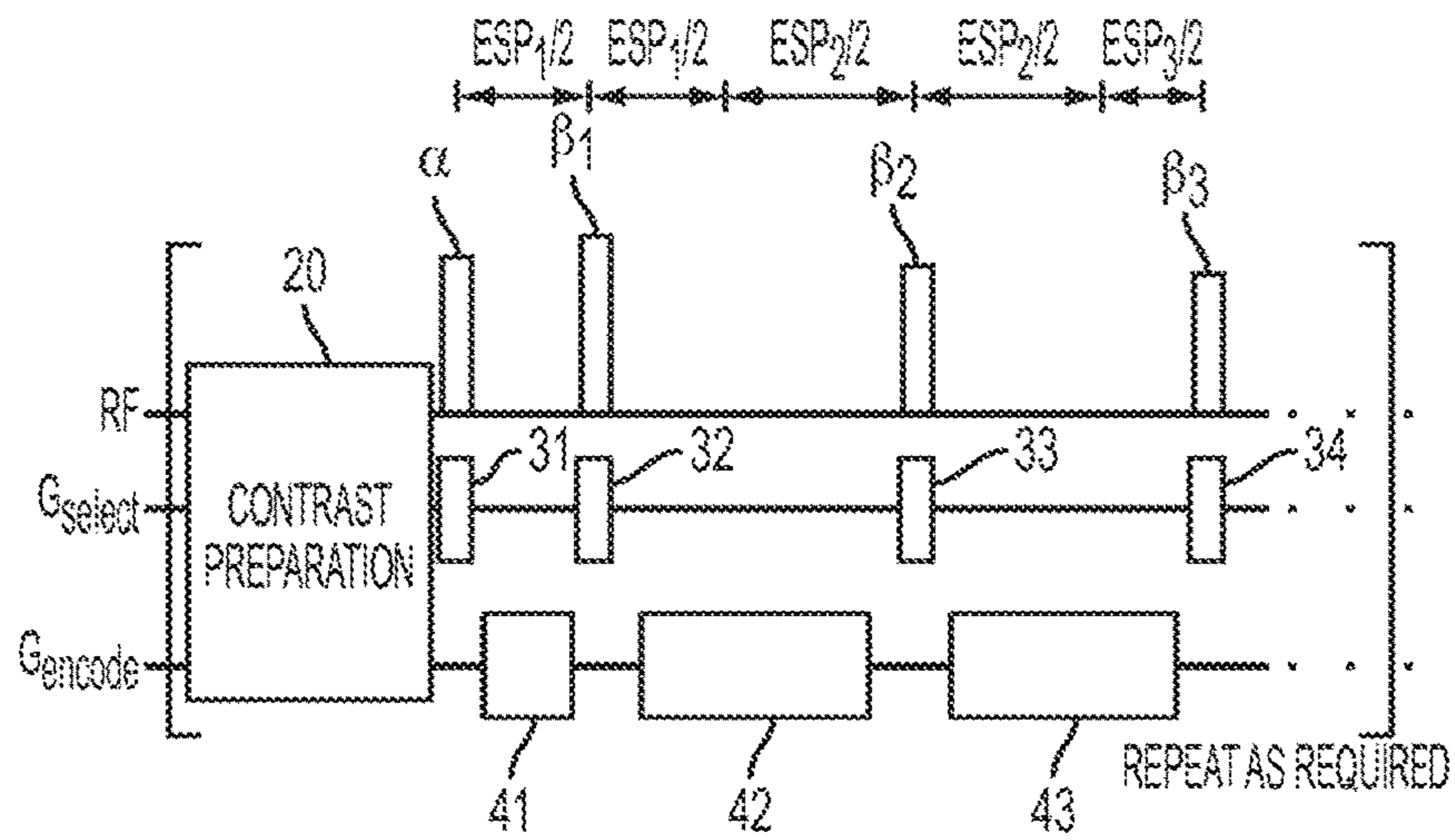
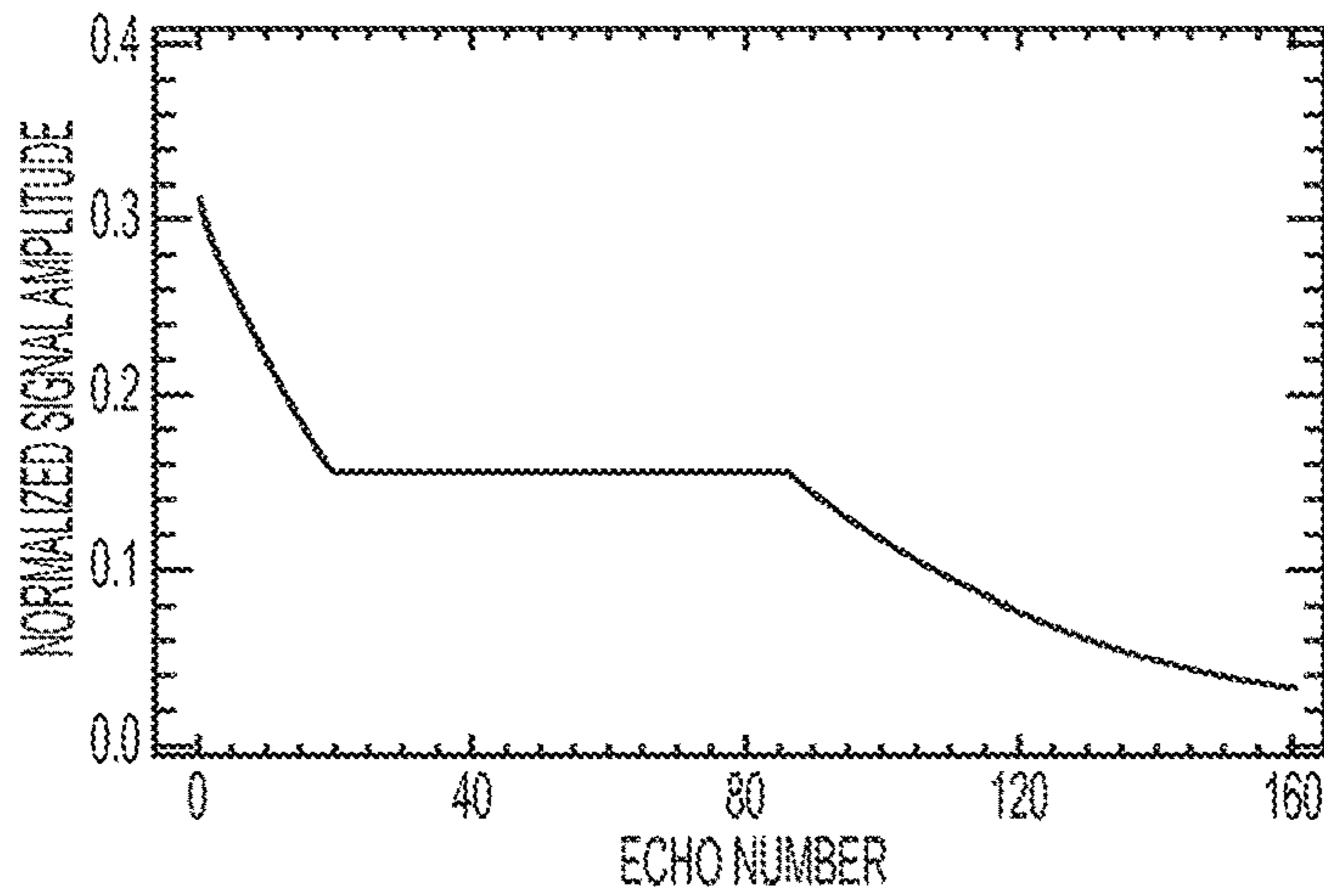


FIG. 1



(TOTAL NUMBER OF ECHOES FOR SIGNAL EVOLUTION = 160)
(ECHO SPACING = 4.1 MILLISECONDS. TIME FROM EXCITATION RF PULSE
TO A GIVEN ECHO NUMBER = ECHO NUMBER x 4.1 MILLISECONDS.)

FIG. 2

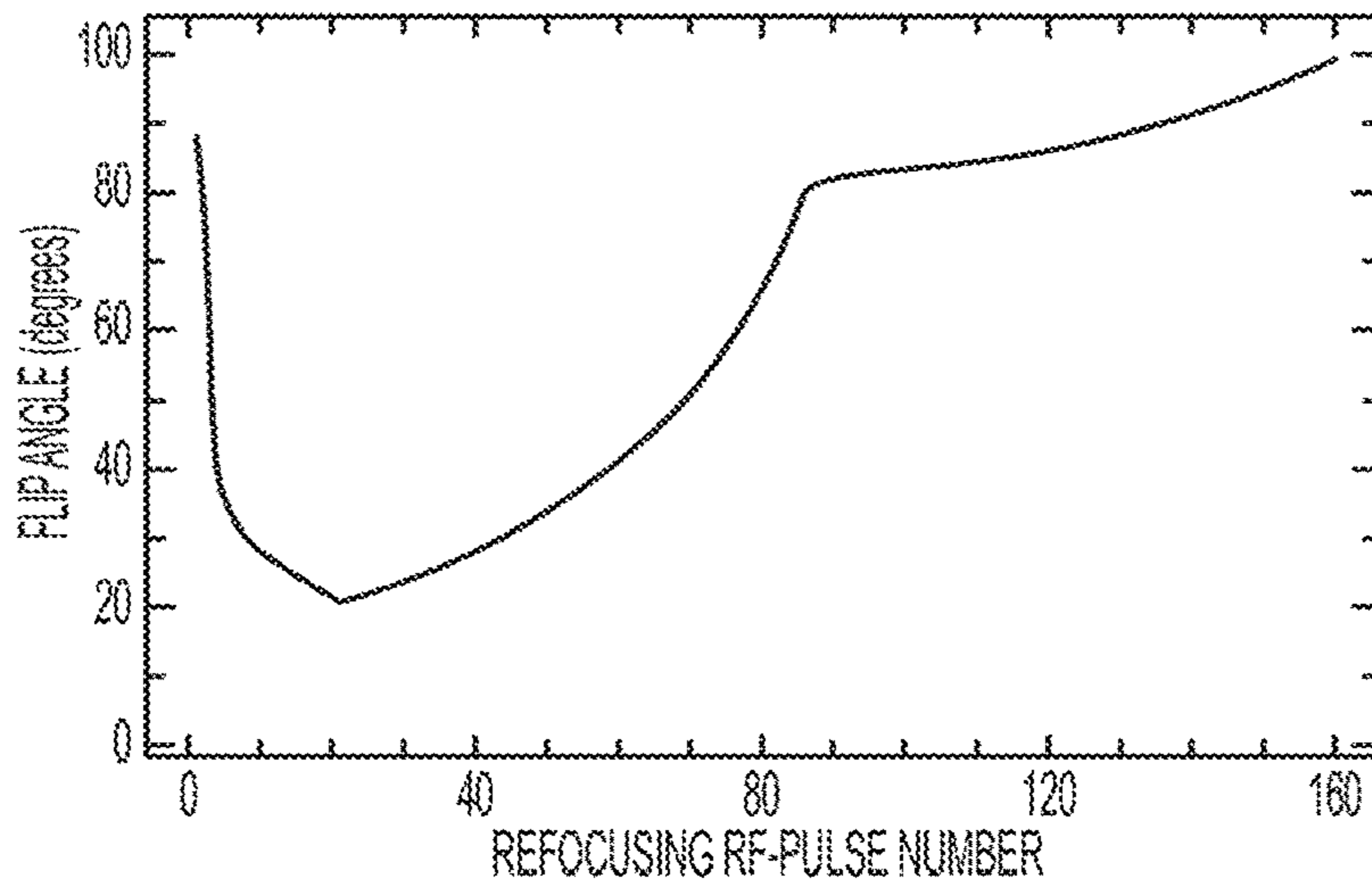


FIG. 3



FIG. 4A

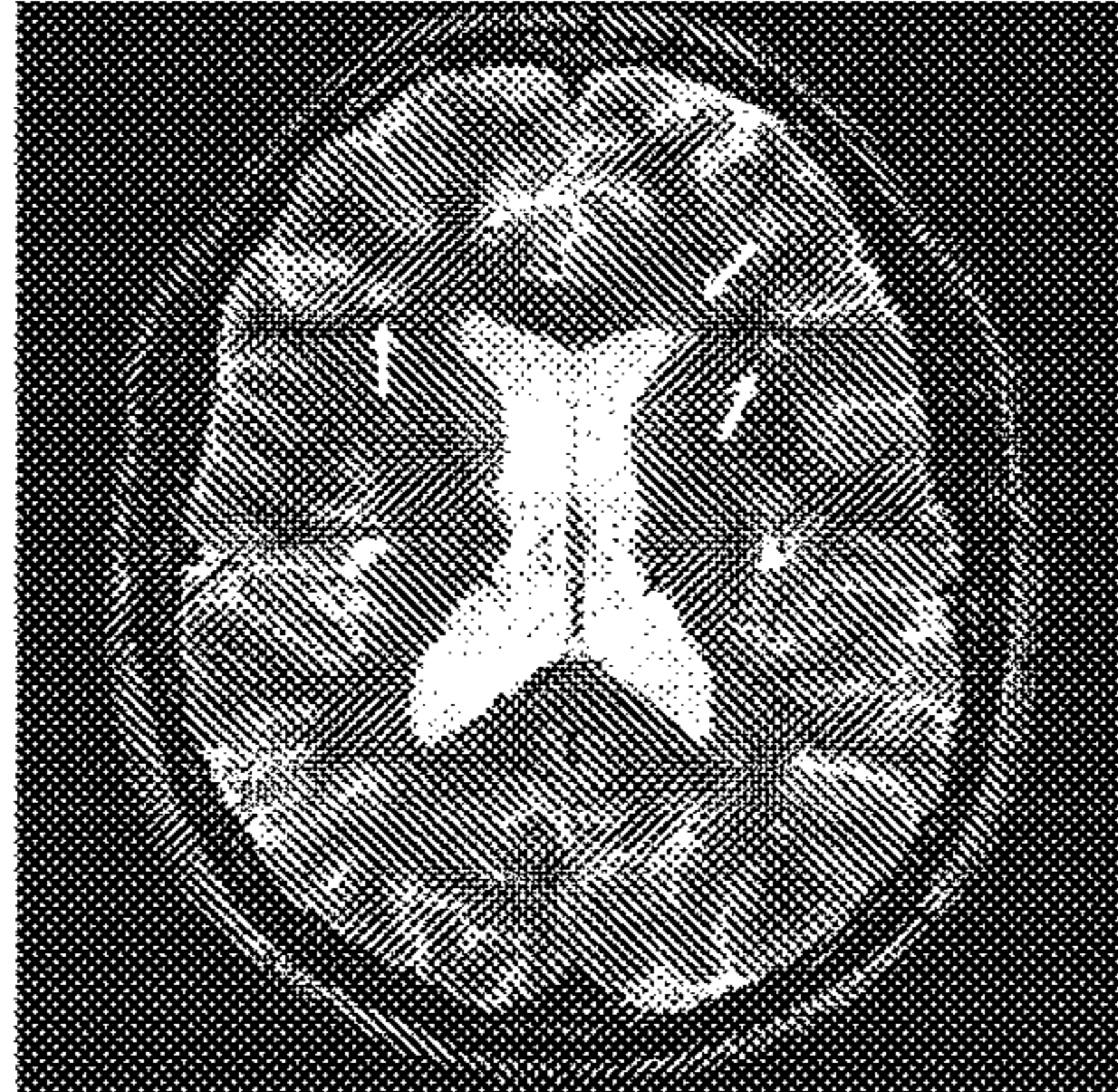


FIG. 4B

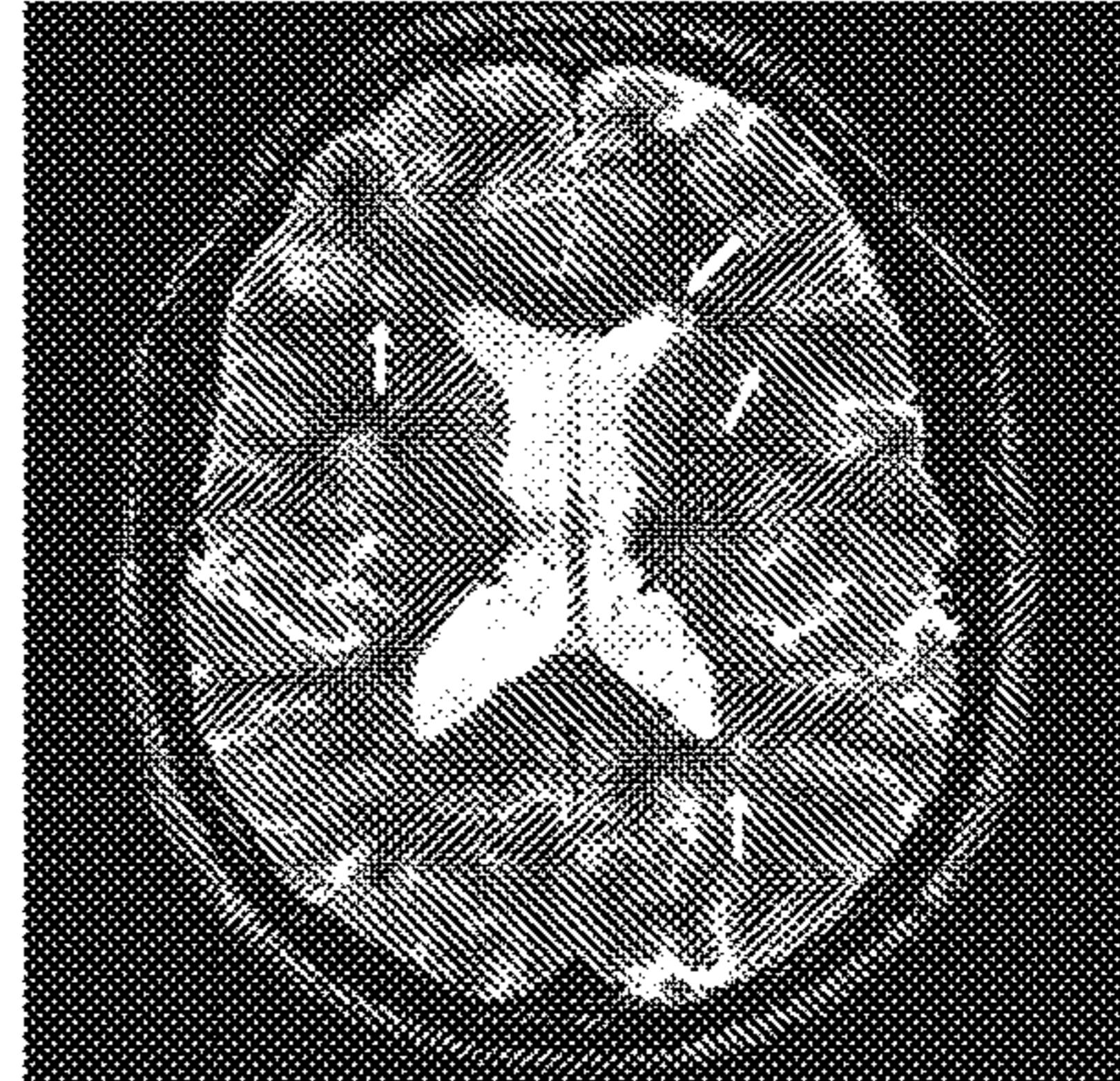


FIG. 4C

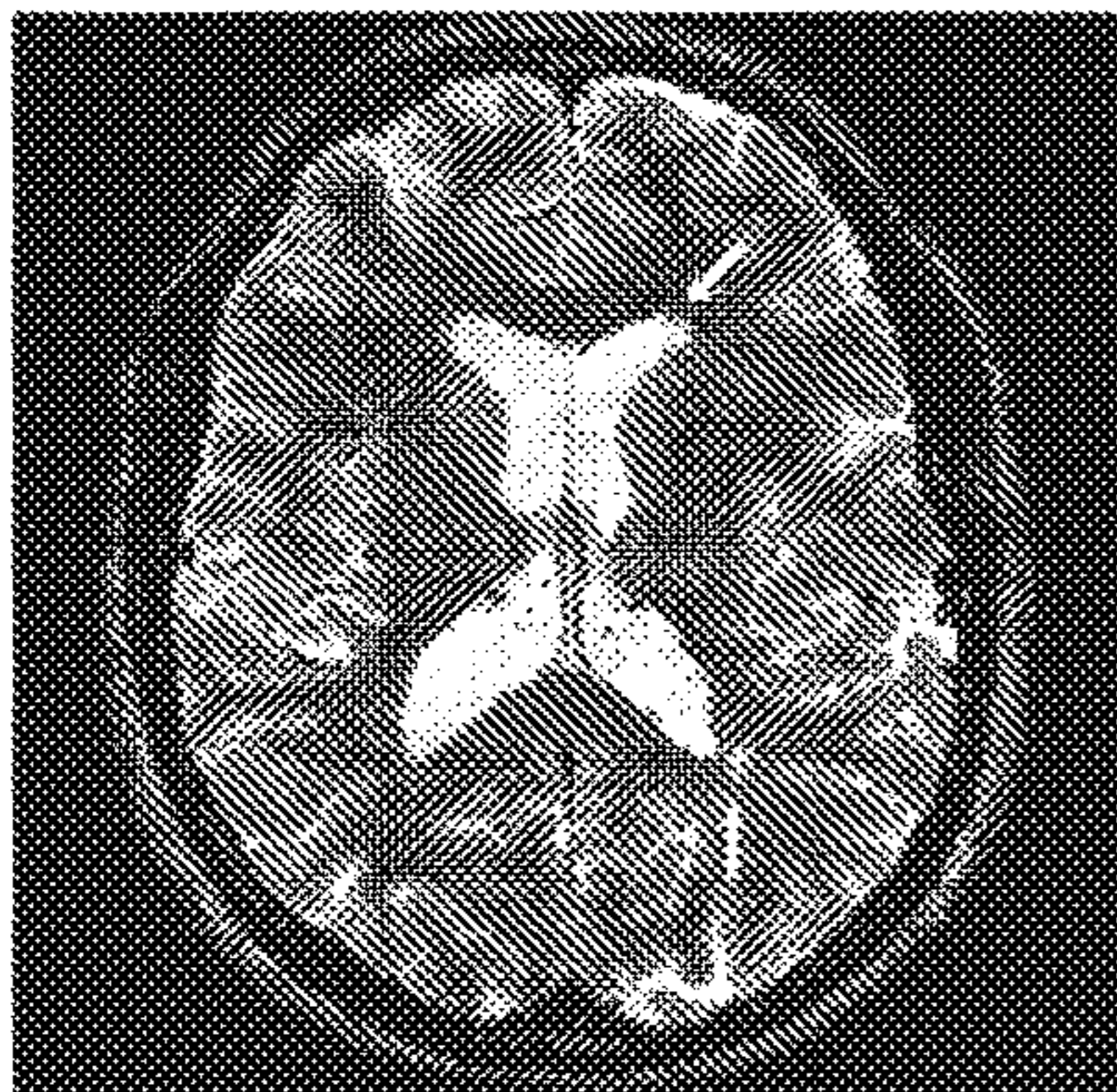


FIG. 4D



FIG. 4E

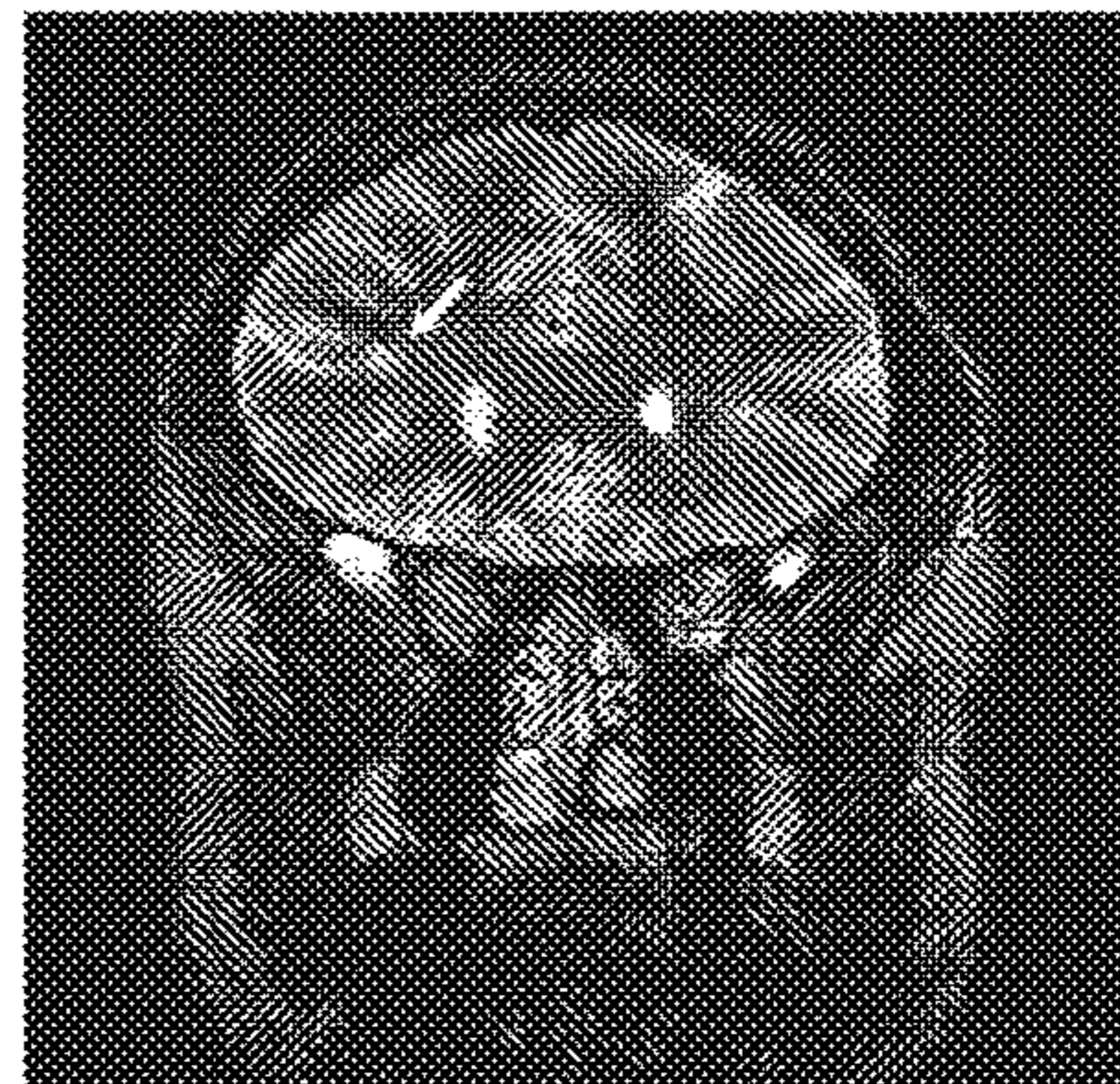


FIG. 4F

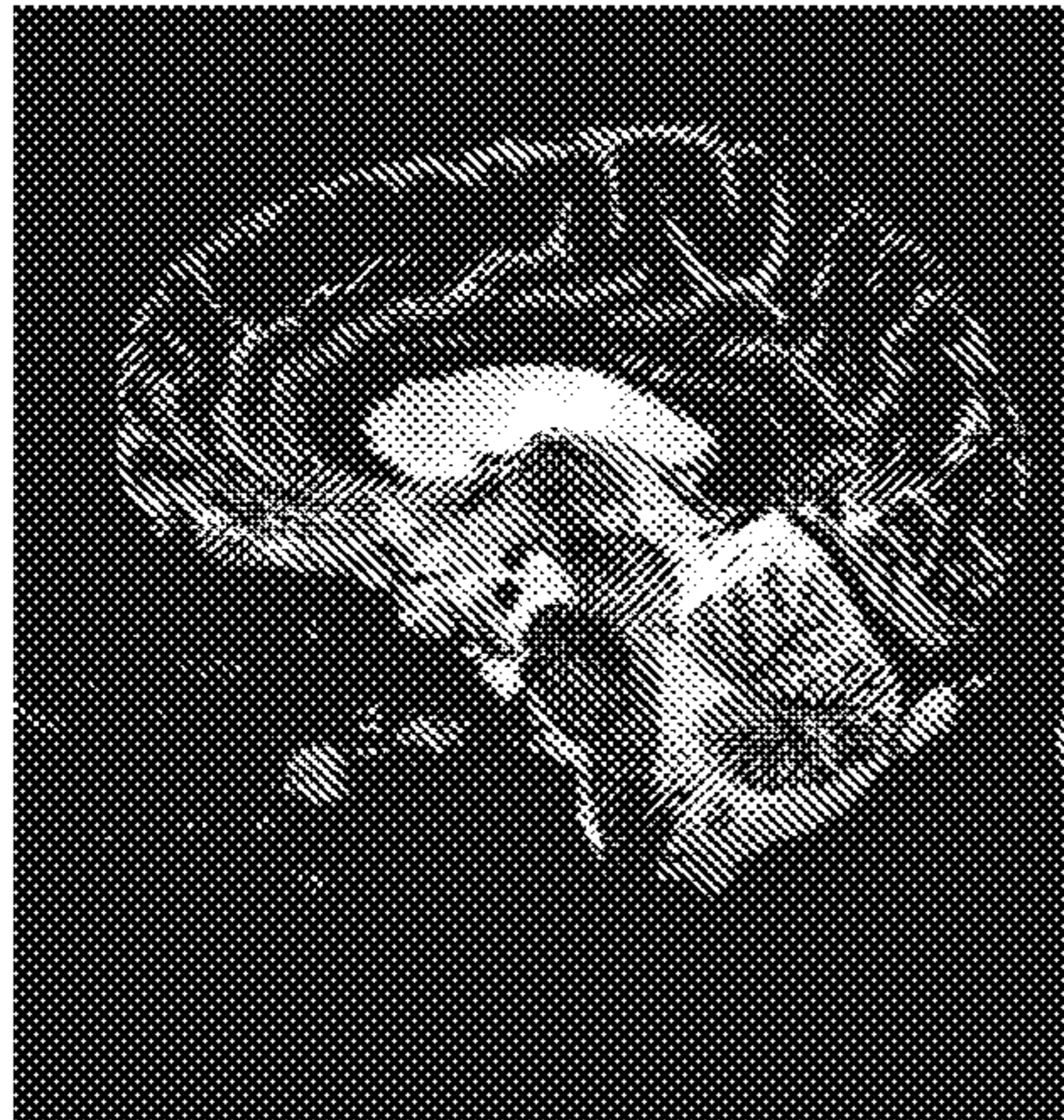


FIG. 5A

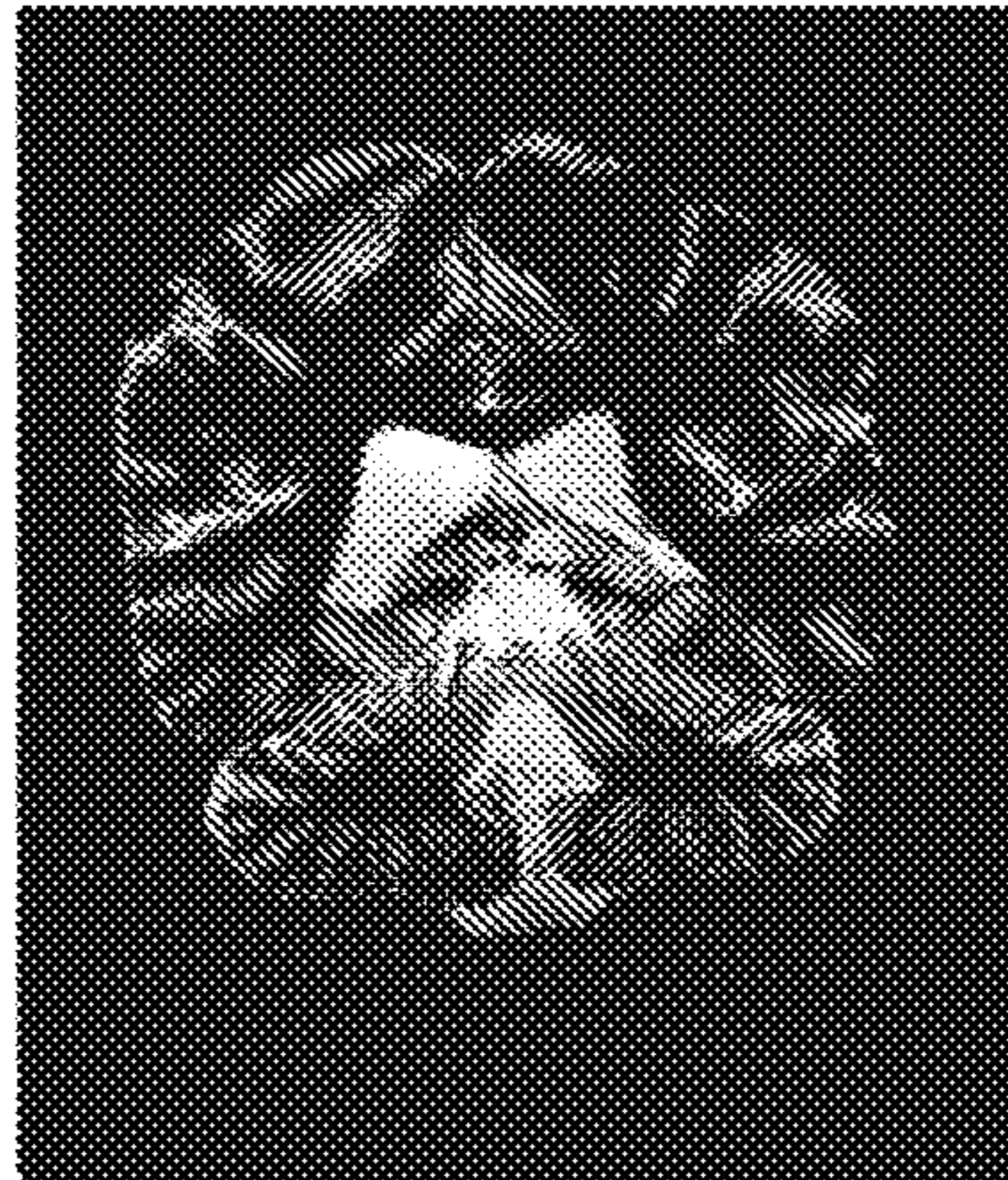


FIG. 5B

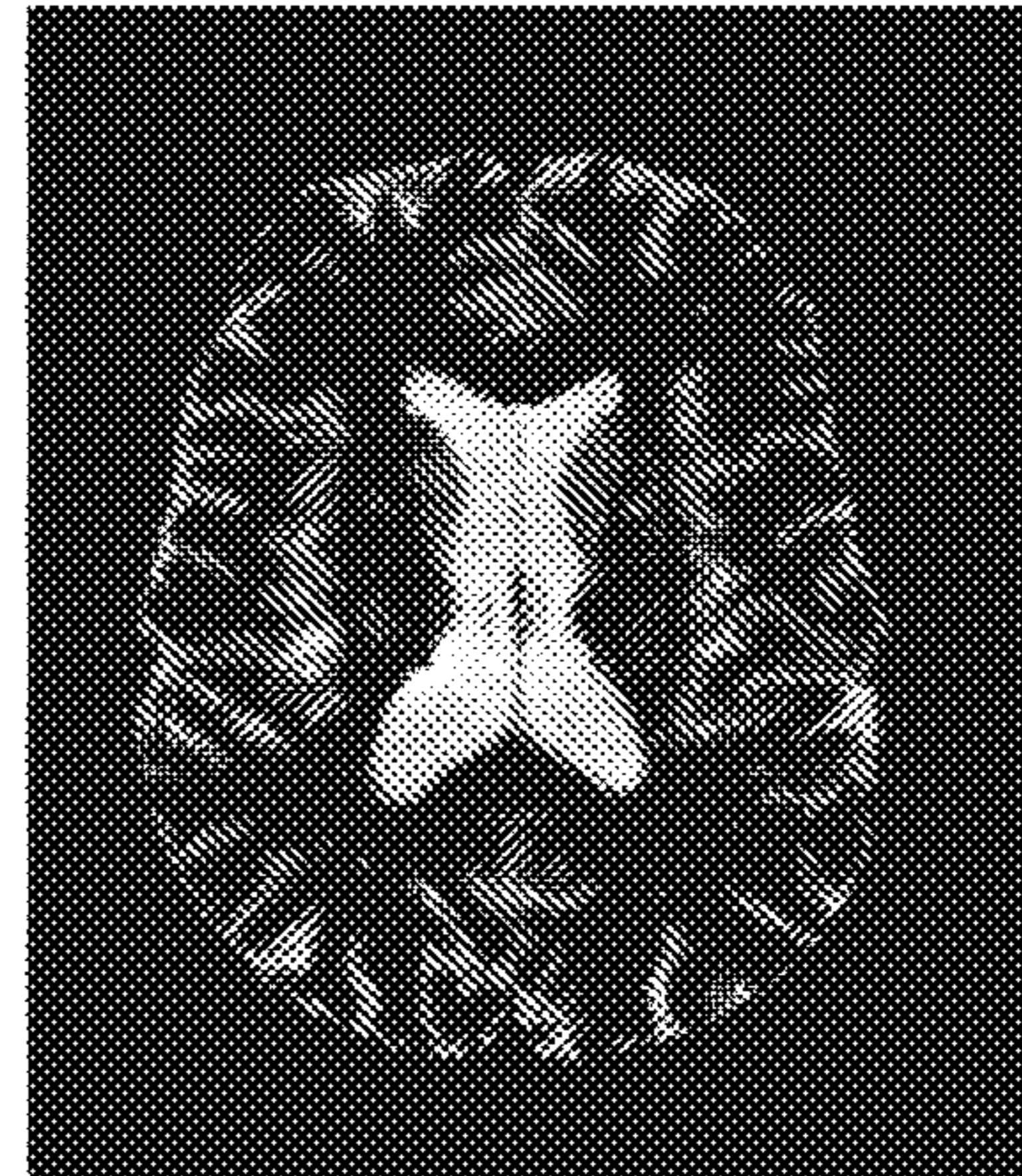


FIG. 5C



FIG. 6

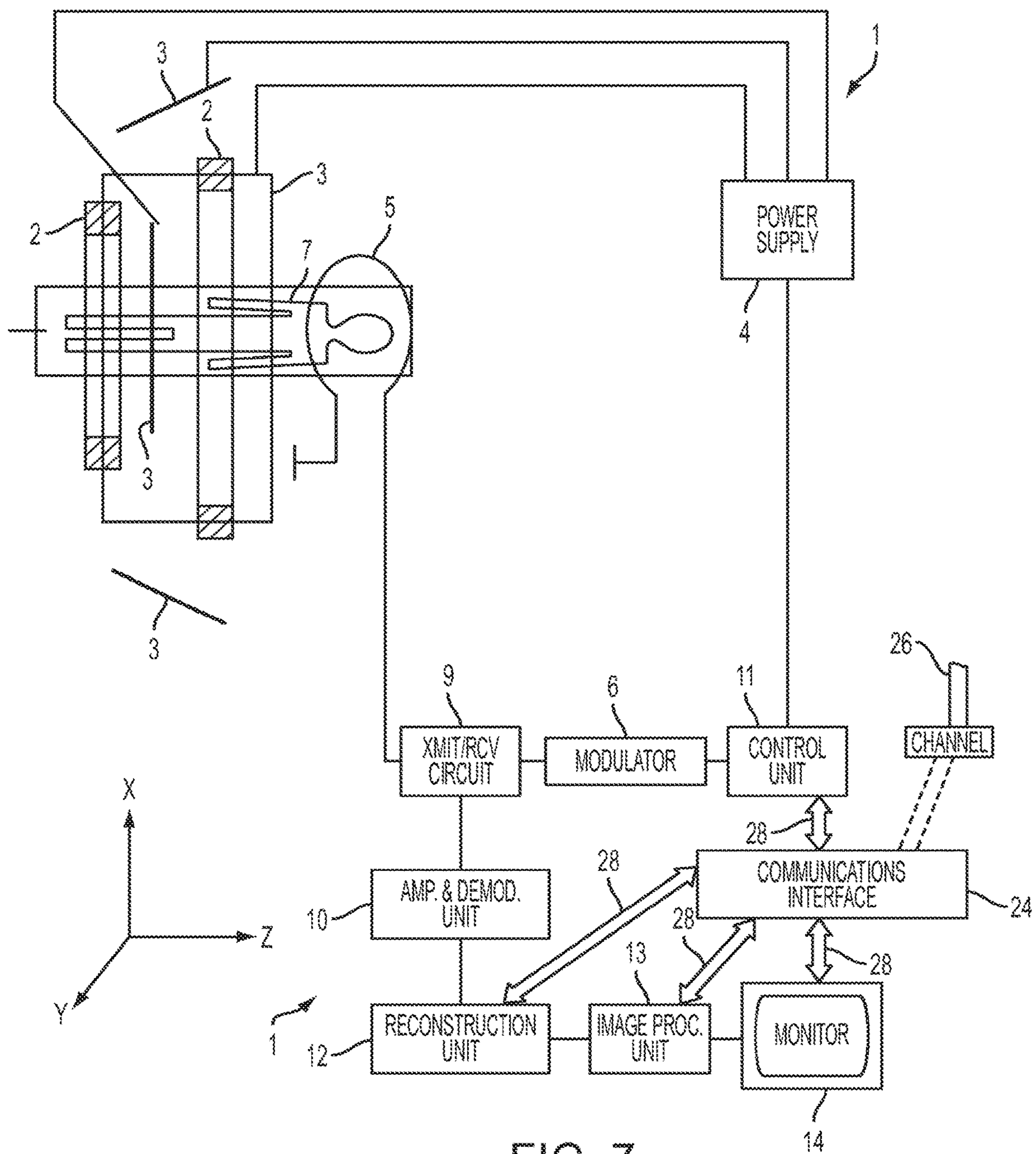


FIG. 7

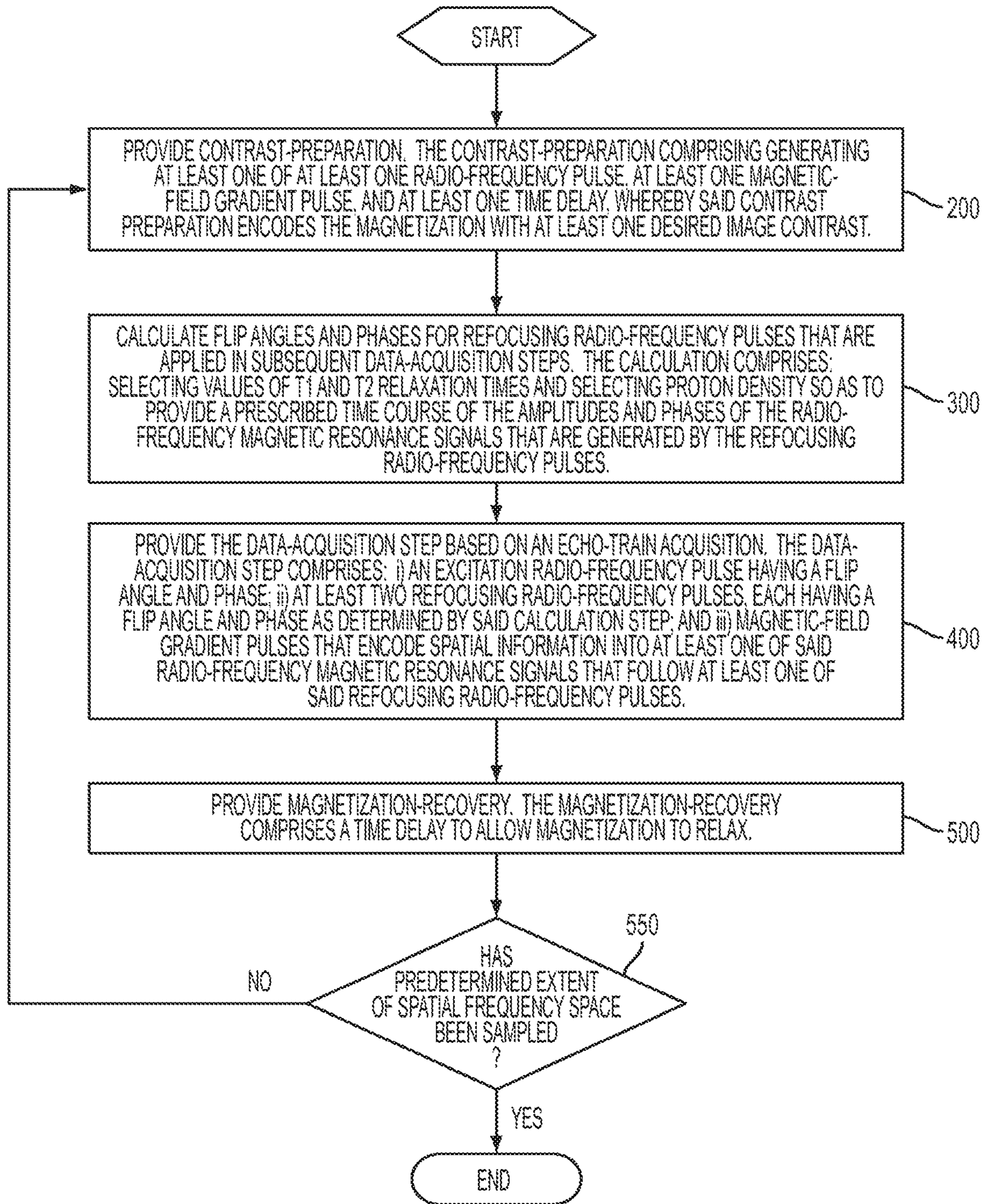


FIG. 8

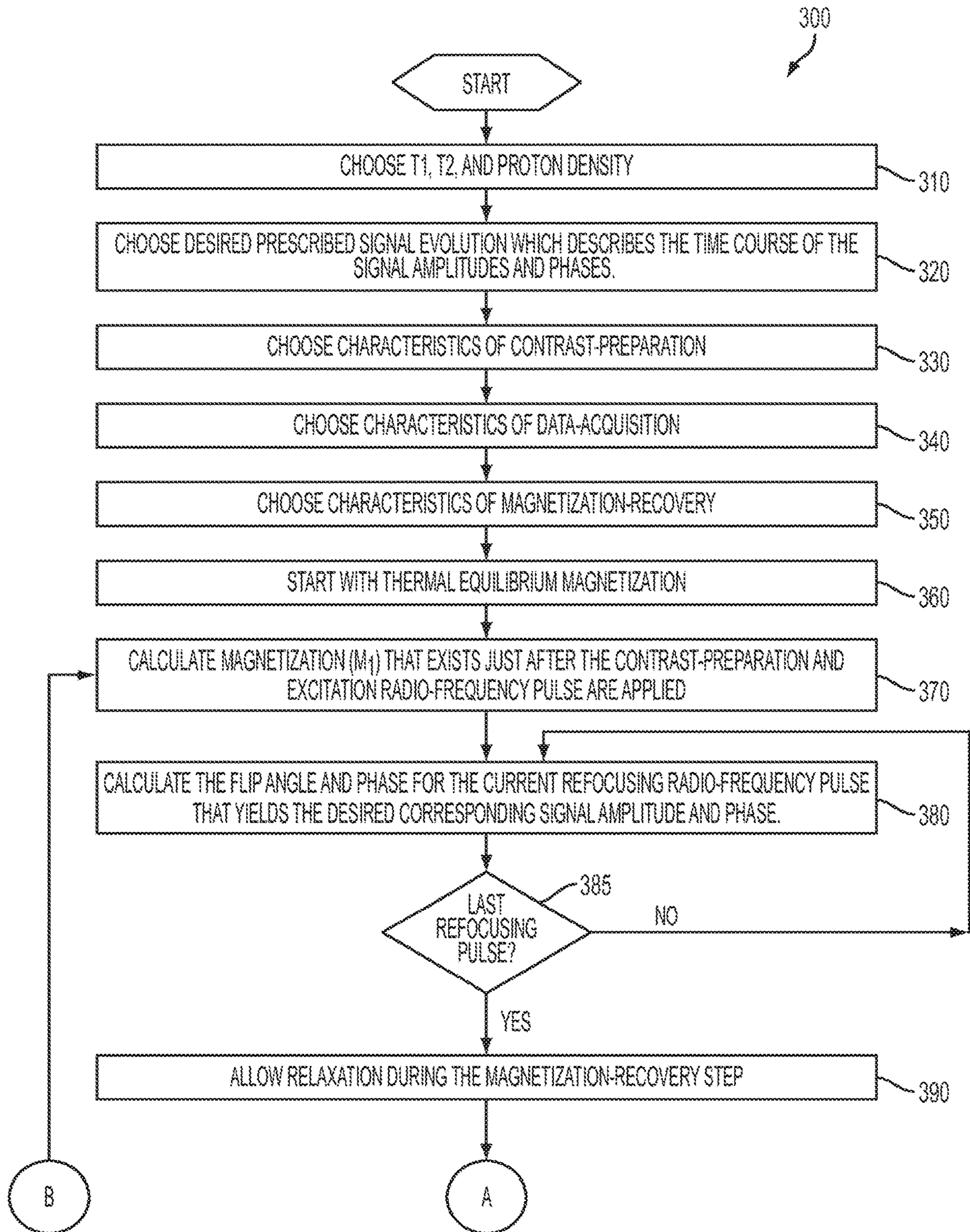


FIG. 9A

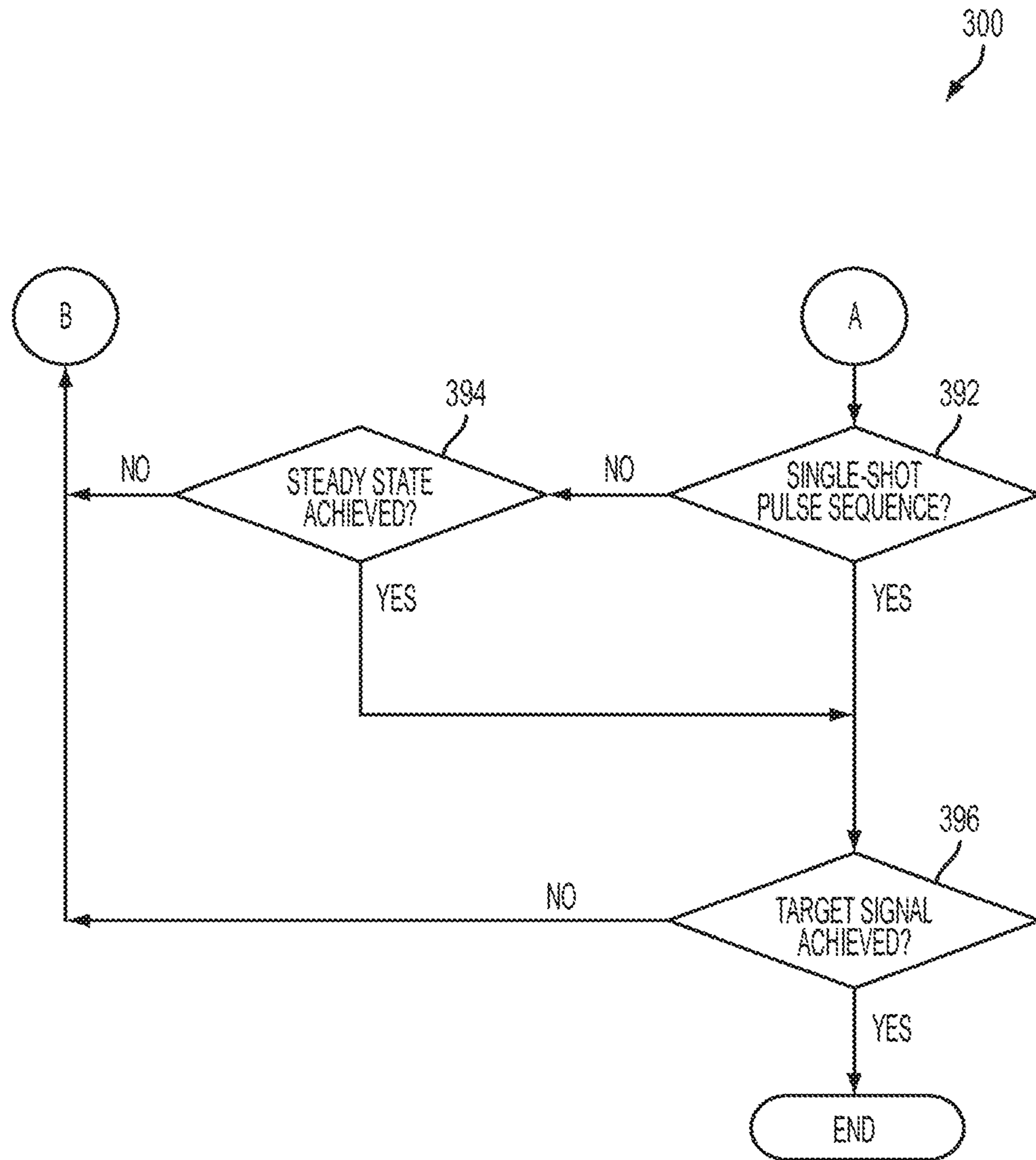


FIG. 9B

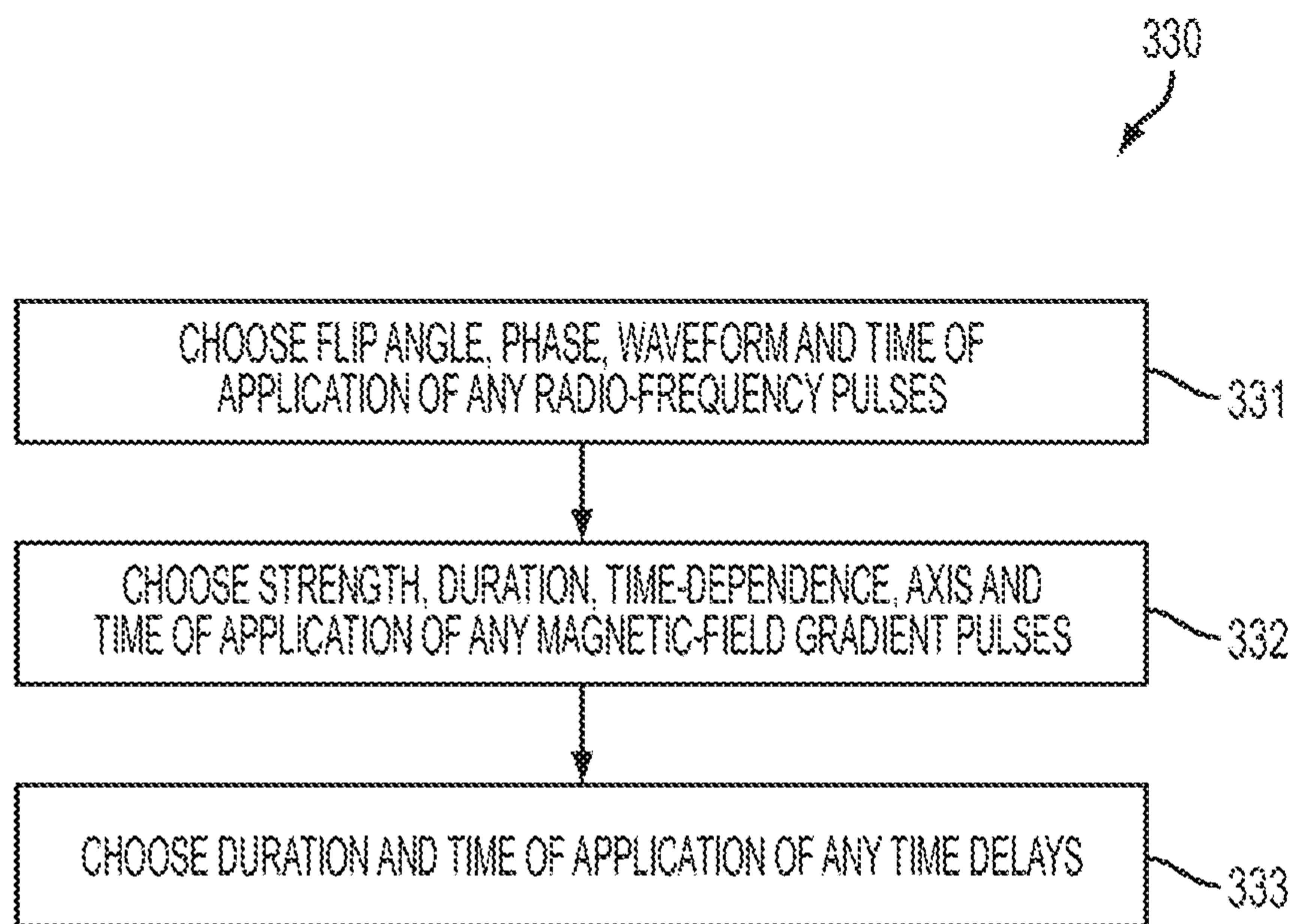


FIG. 10

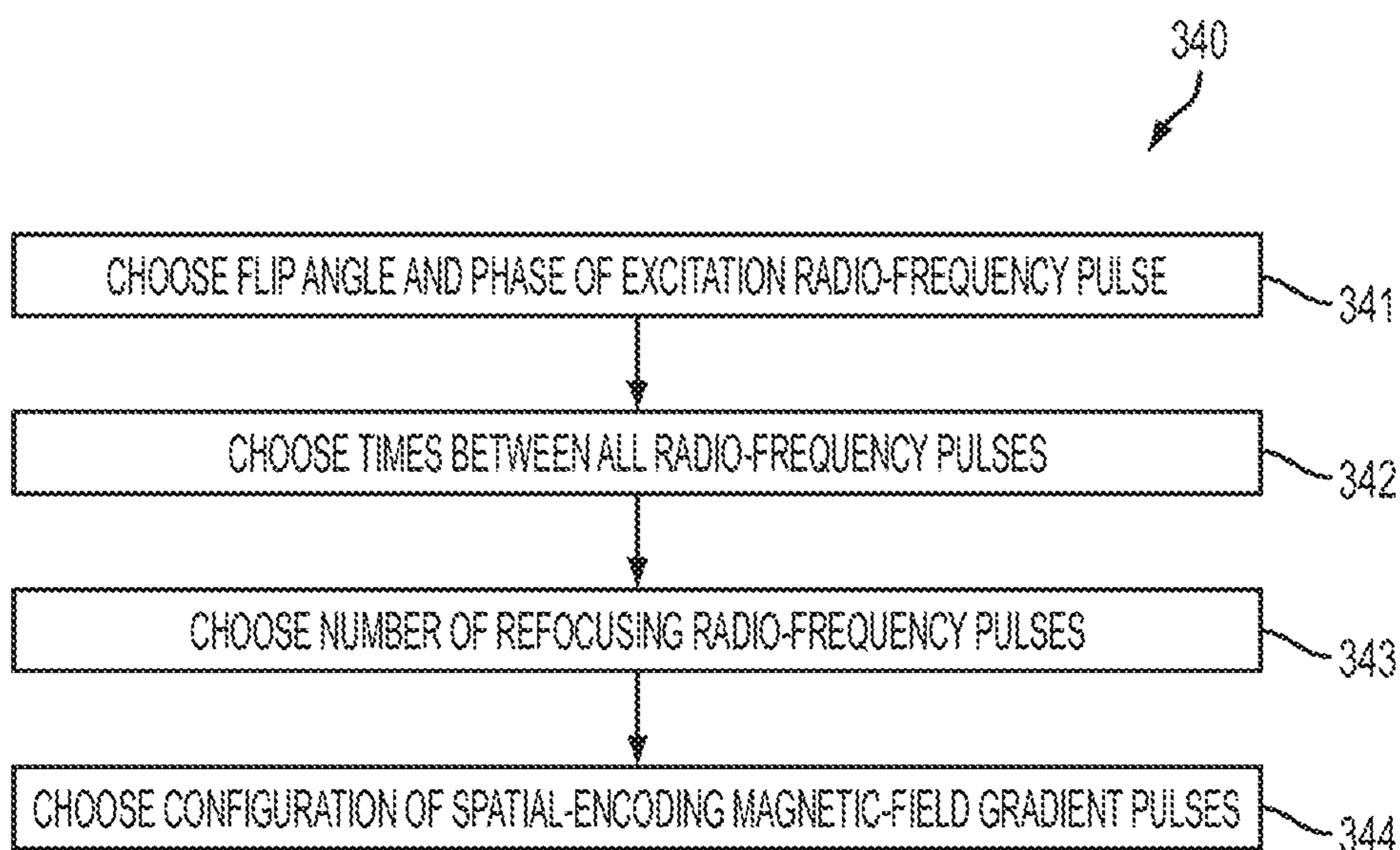


FIG. 11

**METHOD AND APPARATUS FOR
SPIN-ECHO-TRAIN MR IMAGING USING
PRESCRIBED SIGNAL EVOLUTIONS**

Matter enclosed in heavy brackets [] appears in the original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue; a claim printed with strikethrough indicates that the claim was canceled, disclaimed, or held invalid by a prior post-patent action or proceeding.

Notice: More than one reissue application has been filed for the reissue of U.S. Pat. No. 7,164,268. The reissue applications are Ser. No. 16/195,079 (the present application), application Ser. No. 14/708,875 (now U.S. Pat. No. RE47,178), filed May 11, 2015, application Ser. No. 14/053,190 (now U.S. Pat. No. RE45,725), filed Oct. 14, 2013, and application Ser. No. 12/354,471 (now U.S. Pat. No. RE44,644), filed Jan. 15, 2009. The present application is a reissue continuation of application Ser. No. 14/708,875.

RELATED APPLICATIONS

This application is a [national stage] reissue continuation of U.S. patent application Ser. No. 14/708,875, filed on May 11, 2015, which is a reissue continuation of U.S. patent application Ser. No. 14/053,190, filed on Oct. 14, 2013 (now, U.S. Pat. No. RE45,725), which was a reissue continuation of U.S. patent application Ser. No. 12/354,472, filed on Jan. 15, 2009 (now, U.S. Pat. No. RE44,644), which was a reissue of U.S. Pat. No. 7,164,268, which issued from U.S. patent application Ser. No. 10/451,124, filed on Jun. 19, 2003 as a U.S. National Stage filing of International Application No. PCT/US01/50551, filed 21 Dec. 2001, which claims [benefit] priority under 35 U.S.C. Section 119(e) from U.S. Provisional Patent Application [Ser.] No. 60/257,182, filed on Dec. 21, 2000, entitled "Spin-Echo-Train MR Imaging Using Prescribed Signal Evolutions," the entire [disclosure] disclosures of which [is hereby] are incorporated by reference herein. The present application is related to U.S. Pat. No. 5,245,282, filed on Jun. 28, 1991, entitled "Three-dimensional Magnetic Resonance Imaging," the entire disclosure of which is hereby incorporated by reference herein.

GOVERNMENT SUPPORT

Work described herein was supported by Federal Grant Number NS-35142, awarded by the National Institutes of Health. The United States Government possesses certain rights in and to this invention.

FIELD OF INVENTION

The present invention relates to a pulse sequence for use in operating a magnetic resonance imaging apparatus, and in particular for lengthening the usable echo-train duration and reducing the power deposition for spin-echo-train magnetic resonance imaging.

BACKGROUND OF INVENTION

Over the past twenty years, nuclear magnetic resonance imaging (MRI) has developed into an important modality for both clinical and basic-science imaging applications. A large portion of MRI techniques are based on spin-echo (SE)

acquisitions because they provide a wide range of useful image contrast properties that highlight pathological changes and are resistant to image artifacts from a variety of sources such as radio-frequency or static-field inhomogeneities.

Spin-echo-based methods can be subdivided into two categories, including those that generate one spin echo for each desired image contrast following each excitation radio-frequency (RF) pulse, and those that generate more than one spin echo for each desired image contrast following each excitation RF pulse. The first category includes, but is not limited thereto, the techniques commonly referred to as "conventional SE" imaging. The second category includes, but is not limited thereto, a method called "RARE" (See Hennig J., Nauert A., Friedburg H., "RARE Imaging: A Fast Imaging Method for Clinical MR", *Magn. Reson. Med.* 1986, 3:823-833; and Mulkern R. V., Wong S. T. S., Winalski C., Jolesz F. A., "Contrast Manipulation and Artifact Assessment of 2D and 3D RARE Sequences", *Magn. Reson. Imaging* 1990, 8:557-566, of which are hereby incorporated by reference in their entirety) and its derivatives, commonly referred to as "turbo-SE" or "fast-SE" imaging (See Melki P. S., Jolesz F. A., Mulkern R. V., "Partial RF Echo Planar Imaging with the FALSE Method. I Experimental and Theoretical Assessment of Artifact", *Magn. Reson. Med.* 1992, 26:328-341 and Jones K. M., Mulkern R. V., Schwartz R. B., Oshio K., Barnes P. D., Jolesz F. A., "Fast Spin-Echo MR Imaging of the Brain and Spine: Current Concepts", *AJR* 1992, 158:1313-1320, of which are hereby incorporated by reference in their entirety). For the purposes of this disclosure, we are primarily interested in the generalized form of techniques in the second category; however the present invention is applicable to the first category as well. The term "generalized" refers to the form of the spatial-encoding gradients that are applied following any given refocusing RF pulse. For example, RARE imaging encodes one line of spatial-frequency space (k-space) data following each refocusing RF pulse using a constant, frequency-encoding magnetic field gradient. In contrast, "GRASE" imaging (See Feinberg D. A., Oshio K. "GRASE (Gradient-And Spin-Echo) MR Imaging: A New Fast Clinical Imaging Technique", *Radiology* 1991, 181: 597-602; and Oshio K., Feinberg D. A. "GRASE (Gradient- And Spin-Echo) Imaging: A Novel Fast MRI Technique", *Magn. Reson. Med.* 1991, 20:344-349, of which are hereby incorporated by reference in their entirety) encodes three or more lines of k-space data following each refocusing RF pulse using an oscillating, frequency-encoding gradient waveform. This oscillating gradient waveform collects one line of k-space data that includes the spin echo, and one or more additional lines of k-space data before the spin echo and after the spin echo. One skilled in the art would appreciate that there exist an infinite number of possibilities for spatially encoding the MR signal following each refocusing RF pulse. For the purpose of this disclosure, we define the term "spin-echo-train" imaging to encompass all of these possibilities, including, but not limited thereto, RARE, turbo-SE, fast-SE and GRASE imaging, because the present invention deals with, among other things, the RF-pulse history during the echo train, not the details of the spatial encoding.

In general, one of the major goals of technique development for MRI has been to increase the amount of k-space data sampled per unit time, under the constraints of obtaining the desired image contrast and maintaining image artifacts at a tolerable level. Increases in the data rate are typically traded for a decrease in the image acquisition time and/or an increase in the spatial resolution. In this respect,

spin-echo-train methods have played an important role; fast-SE imaging is routinely and widely used in clinical MRI.

For instance, the echo trains used in clinical fast-SE imaging generally employ high flip angles ($>100^\circ$) for the refocusing RF pulses, and their durations are typically less than the T2 relaxation times of interest for short effective echo times (e.g., T1 or proton-density weighting) or less than two to three times these T2 values for long effective echo times (e.g., T2 weighting or "FLAIR"; see Hajnal J. V., Bryant D. J., Kasuboski L., Pattany P. M., De Coene B., Lewis P. D., Pennock J. M., Oatridge A., Young I. R., Bydder G. M., "Use of Fluid Attenuated Inversion Recovery (FLAIR) Pulse Sequences in MRI of the Brain", *J. Comput. Assist. Tomogr.* 1992, 16:841-844, of which is hereby incorporated by reference in its entirety). For example, considering brain imaging at 1.5 Tesla, these limits translate to echo-train durations of <100 ms and <300 ms for short and long effective echo times, respectively. When high flip angles are used for the refocusing RF pulses, echo-train durations that are longer than these limits can substantially degrade image contrast and introduce artifacts such as blurring (See Mulkern et al.; Melki et al.; Constable R. T., Gore J. C., "The Loss of Small Objects in Variable TE Imaging: Implications for FSE, RARE and EPI", *Magn. Reson. Med.* 1992, 28:9-24; and Ortendahl D. A., Kaufman L., Kramer D. M., "Analysis of Hybrid Imaging Techniques", *Magn. Reson. Med.* 1992, 26:155-173, of which are hereby incorporated by reference in their entirety).

Nonetheless, if it were possible to substantially lengthen echo-train durations beyond these limits, while achieving the desired image contrast and limiting artifacts, it would represent a useful and widely applicable advance.

Preliminary studies with the goal of lengthening the echo-train duration in spin-echo-train-based acquisitions have been performed by other researchers. Over a decade ago, Hennig (See Hennig J., "Multiecho Imaging Sequences with Low Refocusing Flip Angles", *J. Magn. Reson.* 1988, 78:397-407, of which is hereby incorporated by reference in its entirety) proposed the use of constant, low-flip-angle refocusing RF pulses to introduce a T1 dependence to the evolution of the echo train and thereby lengthen its usable duration. More recently, this concept was extended by Alsop, who derived variable flip-angle series based on the "pseudosteady-state" condition of a constant signal level when T1 and T2 relaxation are neglected (See Alsop D. C., "The Sensitivity of Low Flip Angle RARE Imaging", *Magn. Reson. Med.* 1997; 37:176-184, of which is hereby incorporated by reference in its entirety). Alsop also found that the echo-train performance was improved by using a signal evolution that decreased for the first few echoes and was then constant, instead of being constant for the complete echo train. Using these evolutions, artifact-free human brain images with T2-weighting were acquired by Alsop. An 80-echo train with a duration of 400 ms and asymptotic flip angles ranging from 17° to 90° were used.

Turning to the present invention, a method and related apparatus is provided for lengthening the usable echo-train duration for spin-echo-train imaging substantially beyond that achievable with the constant, low-flip-angle or pseudosteady-state approaches. The present invention method and apparatus explicitly consider the T1 and T2 relaxation times for the tissues of interest and thereby permit the desired image contrast to be incorporated into the tissue signal evolutions corresponding to the long echo train. Given the considerable role that spin-echo-train methods

already play in MR imaging, the present invention methodology will be of significant importance.

SUMMARY OF THE INVENTION

This present invention comprises the methodology, related apparatus, and computer useable medium (readable media) for using a series of refocusing RF pulses with variable flip angles and, optionally, variable phase angles, in a spin-echo-train MRI pulse sequence wherein the flip-angle series is specifically designed to achieve a prescribed signal evolution during the echo train for selected T1 and T2 relaxation times. By employing such a series of refocusing RF pulses, the usable duration of the echo train can be extended substantially beyond that obtainable with conventional methods. This increase in the echo-train duration can be used to decrease the image acquisition time and/or increase the spatial resolution.

In one aspect, the present invention features a method for generating a pulse sequence for operating a magnetic resonance imaging apparatus for imaging an object, the method comprising:

- a) providing contrast-preparation, the contrast-preparation comprising generating at least one of at least one radio-frequency pulse, at least one magnetic-field gradient pulse, and at least one time delay, whereby the contrast preparation encodes the magnetization with at least one desired image contrast;
- b) calculating flip angles and phases of refocusing radio-frequency pulses that are applied in a data-acquisition step, wherein the calculation provides desired prescribed signal evolution and desired overall signal level, the calculation comprises:
 - i) selecting values of T1 and T2 relaxation times and selecting proton density;
 - ii) selecting a prescribed time course of the amplitudes and phases of the radio-frequency magnetic resonance signals that are generated by the refocusing radio-frequency pulses; and
 - iii) selecting characteristics of the contrast-preparation step, the data-acquisition step and a magnetization-recovery step, with the exception of the flip angles and phases of the refocusing radio-frequency pulses that are to be calculated; and
- c) providing the data acquisition step based on a spin echo train acquisition, the data-acquisition step comprises:
 - i) an excitation radio-frequency pulse having a flip angle and phase;
 - ii) at least two refocusing radio-frequency pulses, each having a flip angle and phase as determined by the calculation step; and
 - iii) magnetic-field gradient pulses that encode spatial information into at least one of the radio-frequency magnetic resonance signals that follow at least one of the refocusing radio-frequency pulses;
- d) providing magnetization-recovery, the magnetization-recovery comprises a time delay to allow magnetization to relax; and
- e) repeating steps (a) through (d) until a predetermined extent of spatial frequency space has been sampled.

In a second aspect, the present invention features a magnetic resonance imaging apparatus for generating a pulse sequence for operating the apparatus for imaging an object, the apparatus comprising a main magnet system for generating a steady magnetic field; a gradient magnet system for generating temporary gradient magnetic fields; a radio-frequency transmitter system for generating radio-frequency

pulses; a radio-frequency receiver system for receiving magnetic resonance signals; a reconstruction unit for reconstructing an image of the object from the received magnetic resonance signals; and a control unit for generating signals controlling the gradient magnet system, the radio-frequency transmitter system, the radio-frequency receiver system, and the reconstruction unit, wherein the control unit generates signals causing:

- a) providing contrast-preparation, the contrast-preparation comprising generating at least one of at least one radio-frequency pulse, at least one magnetic-field gradient pulse, and at least one time delay, whereby the contrast preparation encodes the magnetization with at least one desired image contrast;
- b) calculating flip angles and phases of refocusing radio-frequency pulses that are applied in a data-acquisition step, wherein the calculation provides desired prescribed signal evolution and desired overall signal level, the calculation comprises:
 - i) selecting values of T1 and T2 relaxation times and selecting proton density;
 - ii) selecting a prescribed time course of the amplitudes and phases of the radio-frequency magnetic resonance signals that are generated by the refocusing radio-frequency pulses; and
 - iii) selecting characteristics of the contrast-preparation step, the data-acquisition step and a magnetization-recovery step, with the exception of the flip angles and phases of the refocusing radio-frequency pulses that are to be calculated; and
- c) providing the data acquisition step based on a spin echo train acquisition, the data-acquisition step comprises:
 - i) an excitation radio-frequency pulse having a flip angle and phase,
 - ii) at least two refocusing radio-frequency pulses, each having a flip angle and phase as determined by the calculation step, and
 - iii) magnetic-field gradient pulses that encode spatial information into at least one of the radio-frequency magnetic resonance signals that follow at least one of the refocusing radio-frequency pulses;
- d) providing magnetization-recovery, the magnetization-recovery comprises a time delay to allow magnetization to relax; and
- e) repeating steps (a) through (d) until a predetermined extent of spatial frequency space has been sampled.

In a third aspect, the present invention features a computer readable media carrying encoded program instructions for causing a programmable magnetic resonance imaging apparatus to perform the method discussed above in the first aspect of the invention. Similarly, the invention features a computer program product comprising a computer useable medium having computer program logic for enabling at least one processor in a magnetic resonance imaging apparatus to generate a pulse sequence, the computer program logic comprising the method discussed above in the first aspect of the invention.

Because the flip angles for the refocusing RF pulses that are derived with this method are typically much less than 180° for a substantial portion of the total number of RF pulses, the power deposition is much less than that corresponding to 180° RF pulses, which are commonly used in conventional spin-echo-train pulse sequences. This feature is particularly important for high field MRI (>1.5 Tesla), wherein power deposition is a critical pulse-sequence design factor for human applications. The present invention permits long, closely-spaced echo trains to be used for high-field

imaging that would not otherwise meet the safety guidelines established by the Food and Drug Administration for power deposition in human MRI.

Another potentially useful feature of the present invention is that, for specific forms of the encoding-gradient waveforms, signals from moving or flowing materials are strongly attenuated, even when the velocities are relatively low. A specific example of this behavior is the attenuation of the signal from cerebrospinal fluid (CSF) surrounding the cervical spinal cord due to its oscillatory motion, which can be used to generate CSF-suppressed T2-weighted MR images of the spinal cord without requiring inversion-nulling of the CSF signal. Studies have indicated that the full range of clinically-relevant cord lesions may not be adequately detected using inversion-nulling of the CSF signal (i.e., FLAIR) (See Hittmair K., Mallek R., Prayer D., Schindler E. G., Kollegger H., "Spinal Cord Lesions in Patients with Multiple Sclerosis: Comparison of MR Pulse Sequences", *AJNR* 1996, 17:1555-1565; and Keiper M. D., Grossman R. I., Brunson J. C., Schnall M. D., "The Low Sensitivity of Fluid-Attenuated Inversion-Recovery MR in the Detection of Multiple Sclerosis of the Spinal Cord", *AJNR* 1997, 18:1035-1039, of which are hereby incorporated by reference in their entirety).

These and other objects, along with advantages and features of the invention disclosed herein, will be made more apparent from the description, drawings and claims that follow.

BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing and other objects, features and advantages of the present invention, as well as the invention itself, will be more fully understood from the following description of preferred embodiments, when read together with the accompanying drawings, in which:

FIG. 1 is a schematic representation of a general spin-echo-train MRI pulse sequence. This is an exemplary type of MRI pulse sequence to which the invention applies. The present invention method can be applied to various types of pulse sequences.

FIG. 2 shows an example of a prescribed signal evolution that can be used to generate T2-weighted MR images of the brain or spine.

FIG. 3 shows the variable-flip-angle series corresponding to FIG. 2 that was derived using the present invention methods as described herein.

FIGS. 4-6 show example MR images obtained using the variable-flip-angle series of FIG. 3 in a "turbo-SE" type spin-echo-train pulse sequence; collectively, FIGS. 4-6 provide examples of the potential utility of the present invention. In particular, showing brain images obtained at 1.5 Tesla, FIGS. 4(A) and 4(B)-4(C) compare T2-weighted two-dimensional and three-dimensional SE images, respectively. Further, showing brain images obtained at 3 Tesla, FIGS. 5(A)-5(C) show T2-weighted sagittal, coronal, and axial images, respectively, reconstructed from the same three-dimensional acquisition. Finally, FIG. 6 shows a sagittal image of the cervical spinal cord obtained at 1.5 Tesla.

FIG. 7 illustrates a simplified exemplary embodiment of a MRI apparatus for practicing the present invention. The present invention method can be applied to various commercially available MRI apparatuses.

FIG. 8 is an exemplary flowchart for a simplified preferred implementation of the methods of the present invention.

FIGS. 9A-9B is an exemplary flowchart for a simplified preferred implementation of the calculation methods of the present invention, step 200.

FIG. 10 is an exemplary flowchart for a simplified preferred implementation of the contrast-preparation methods of the present invention.

FIG. 11 is an exemplary flowchart for a simplified preferred implementation of the data-acquisition methods of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

In the following, first presented is an exemplary embodiment of a MR apparatus for practicing the MR methods of the present invention for imaging an object, moving or stationary. Following are descriptions of preferred and alternative embodiments of the methods of the present invention, including their exemplary implementation as computer hardware, firmware, and/or software.

An Exemplary MR-Apparatus of the Present Invention

FIG. 7 illustrates a simplified schematic of a MR apparatus 1 for practicing the present invention. The MR apparatus 1 includes a main magnet system 2 for generating a steady magnetic field in an examination zone(s) of the MR apparatus. The z-direction of the coordinate system illustrated corresponds to the direction of the steady magnetic field generated by the magnet system 2.

The MR apparatus also includes a gradient magnet system 3 for generating temporary magnetic fields G_x , G_y , and G_z directed in the z-direction but having gradients in the x, y or z directions, respectively. With this magnetic gradient system, magnetic-field gradients can also be generated that do not have directions coinciding with the main directions of the above coordinate system, but that can be inclined thereto, as is known in the art. Accordingly, the present invention is not limited to directions fixed with respect to the MR apparatus. In this application, for ease of description, the directions x, y and z (and the gradients along these directions) are used for the read direction, the phase-encode direction and slice-selection direction (or second phase-encode direction for 3D imaging), respectively.

Also, while traditional commercial methods provide linear gradients in the x, y, or z directions it is also possible not to utilize all three of these linear gradients. For example, rather than using a linear z gradient, one skilled in the art can use a z-squared dependence or some other spatial dependence to provide desired results.

The magnet systems 2 and 3 enclose an examination zone(s) which is large enough to accommodate a part of an object 7 to be examined, for example a part of a human patient. A power supply means 4 feed the gradient magnet system 3.

The MR apparatus also includes an RF transmitter system including RF transmitter coil 5, which generates RF pulses in the examination zone and is connected via transmitter/receiver circuit 9 to a RF source and modulator 6. The RF transmitter coil 5 is arranged around the part of body 7 in the examination zone. The MR apparatus also comprises an RF receiver system including an RF receiver coil which is connected via transmitter/receiver circuit 9 to signal amplification and demodulation unit 10. The receiver coil and the RF transmitter coil 5 may be one and the same coil. The MR apparatus also includes an amplification and demodulation unit 10, which, after excitation of nuclear spins in a part of the body placed within the examination space by RF pulses, after encoding by the magnetic-field gradients and after

reception of the resulting MR signals by the receiver coil, derives sampled phases and amplitudes from the received MR signals. An image reconstruction unit 12 processes the received MR imaging signals to, inter alia, reconstruct an image by methods well-known in the art, such as by Fourier transformation. It should be appreciated by one skilled in the art that various reconstruction methods may be employed besides the Fourier Transform (FT) depending on factors such as the type of signal being analyzed, the available processing capability, etc. For example, but not limited thereto, the present invention may employ Short-Time FT (STFT), Discrete Cosine Transforms (DCT), or wavelet transforms (WT). By means of an image processing unit 13, the reconstructed image is displayed, for example, on monitor 14. Further, the image reconstruction unit can optionally process MR navigator signals to determine the displacement of a portion of the patient.

The MR apparatus also includes a control unit 11 that generates signals for controlling the RF transmitter and receiver systems by means of a modulator 6, the gradient magnetic field system by means of the power supply means 4, an image reconstruction unit 12 and an image processing unit 13. In a preferred embodiment, the control unit 11 (and other control elements in the MR apparatus) are implemented with programmable elements, such as one or more programmable signal processors or microprocessors, communicating over busses with supporting RAM, ROM, EPROM, EEPROM, analog signal interfaces, control interfaces, interface to computer-readable media and so forth. These programmable elements are commanded by software or firmware modules loaded into RAM, EPROM, EEPROM or ROM, written according to well-known methods to perform the real-time processing required herein, and loaded from computer-readable media (or computer useable medium), such as magnetic disks or tapes, or optical disks, or network interconnections, removable storage drives, or so forth. The present invention may be implemented using hardware, software or a combination thereof and may be implemented in one or more computer systems or processing systems, such as personal digit assistants (PDAs), for various applications, e.g., remote care and portable care practices.

In a less preferred embodiment, the control unit that directs a MR apparatus for practicing the present invention can be implemented with dedicated electronic components in fixed circuit arrangements. In this case, these dedicated components are arranged to carry out the method described above. For example, the invention is implemented primarily in hardware using, for example, hardware components such as application specific integrated circuits (ASICs). Implementation of the hardware state machine to perform the functions described herein will be apparent to persons skilled in the relevant art(s).

In particular, the control unit commanded by its loaded software causes the generation of MR signals by controlling the application of MR pulse sequences, which comprise RF-pulses, time delays and temporary magnetic-field gradient pulses. These pulse sequences are generated according to the methods of the present invention as subsequently described, and generally include 2D and 3D imaging pulse sequences and optionally navigator pulse sequences for determining the displacement of the patient or material.

Furthermore, according to alternate embodiments of the present invention, the MR apparatus also optionally includes various other units (not illustrated) from which the state of motion of the part of the patient being imaged can be measured. These can include sensors directly indicating the

instantaneous state of motion of the part of the patient being imaged, such as a chest belt for directly indicating chest displacement during respiration, or MR-active micro-coils whose position can be tracked, or optical means, or ultrasound means, or so forth. These units can also include sensors indirectly indicating the instantaneous state of motion of the part of the patient being imaged. For example, electrocardiogram and peripheral pulse sensors measure the temporal progress of the cardiac cycle, and permit inference of the actual state of motion of the heart from knowledge of cardiac displacements associated with each phase of the cardiac cycle. When these sensors are present to measure the state of motion, the control unit need not generate navigator pulse sequences.

Moreover, the control unit **11** may also include a communications interface **24**. The communications interface **24** allows software and data to be transferred between and among, via communication path (i.e. channel) **28**, the control unit **11**, reconstruction unit **12**, image processing unit **13**, and monitor **14** and external devices. Examples of the communications interface **24** may include a modem, a network interface (such as an Ethernet card), a communications port, a PCMCIA slot and card, etc. Software and data transferred via communications interface **24** are in the form of signals which may be electronic, electromagnetic, optical or other signals capable of being received by communications interface **24**. The signals are provided to communications interface **24** via the communications path (i.e., channel) **26**. The channel **26** carries signals and may be implemented using wire or cable, fiber optics, a phone line, a cellular phone link, a RF link, IR link and other communications channels.

The preferred embodiments of the present invention may be implemented as software/firmware/hardware with various MR apparatuses, and methods, as one skilled in the art would appreciate. Other exemplary apparatuses and methods, but not limited thereto, are disclosed in the following U.S. patents, of which are hereby incorporated by reference in their entirety herein: U.S. Pat. No. 6,230,039 B1—Staber et. al.; U.S. Pat. No. 5,749,834—Hushek; and U.S. Pat. No. 5,656,776—Kanazawa.

The Methods of the Present Invention

Turning now to FIG. 1, pertaining to the general methods of this invention, first in a preferred embodiment, the present invention applies to magnetic resonance imaging (MRI) using a “spin-echo-train” MRI pulse sequence, which is a pulse sequence that generates more than one spin echo for each desired image contrast following each excitation RF pulse. Any form of the applied spatial-encoding gradient waveforms, variations in the spacing between refocusing RF pulses, and/or any combination of non-selective, spatially-selective, and spectrally-selective RF pulses are applicable to the present invention methods as long as their effects on the magnetization are appropriately considered in the derivation of the variable-flip-angle series. A contrast preparation phase, such as an inversion RF pulse followed by a time delay, may precede the acquisition phase of the pulse sequence.

Still referring to FIG. 1, there is shown a schematic representation of a general spin-echo-train MRI pulse sequence. This is an exemplary type of MRI pulse sequence to which the invention applies. The representation is of a general spin-echo-train MRI pulse sequence showing the excitation RF pulse (α) and the first three ($\beta_1, \beta_2, \beta_3$) of n refocusing RF pulses, where $n > 1$. The RF pulse waveforms are drawn as rectangular for simplicity, but they may be amplitude and/or phase modulated as appropriate for the

desired application. The echo spacing (ESP) may be fixed or may vary between echoes. The contrast preparation module **20** denotes the optional use of additional RF pulses, gradient pulses and/or time delays (e.g., an inversion pulse followed by a time delay) to permit additional control over the image contrast. The boxes on the G_{select} axis, referenced as **31, 32, 33** and **34**, symbolically denote the optional use of magnetic-field gradient waveforms for spatial and/or spatial-spectral selection. The boxes on the G_{encode} axis, referenced as **41, 42**, and **43**, symbolically denote the magnetic-field gradient waveforms used for spatial encoding. The contrast preparation (if any) and the echo train are repeated as necessary to collect the desired k-space data. The timing parameters and the number of echoes may vary between repetitions.

For a spin-echo-train pulse sequence, an object of the present invention is to derive a series of refocusing RF pulses with variable flip angles, and, optionally, variable phase angles, that yields a specifically prescribed signal evolution during the echo train for selected T1 and T2 relaxation times. To achieve this, a mathematical model of the pulse sequence, incorporating the specific timing, gradient and RF parameters of choice, is used to calculate the signal evolution during the echo train. This model would typically be implemented in the form of a computer program that is based on the established mathematical equations that describe the behavior of the magnetization during a pulse sequence. See Haacke E. M., Brown R. W., Thompson M. R., Venkatesan R., “Magnetic Resonance Imaging: Physical Principles and Sequence Design”, John Wiley & Sons, New York, 1999, of which is hereby incorporated by reference in its entirety. Other exemplary spin-echo-train MR imaging methods are disclosed in the following U.S. patents, of which are hereby incorporated by reference in their entirety herein: U.S. Pat. No. 5,680,045—Feinberg; U.S. Pat. No. 5,612,619—Feinberg; U.S. Pat. No. 5,541,511—Henning; U.S. Pat. No. 5,315,249—Le Roux et al.; U.S. Pat. No. 5,270,654—Feinberg et al.; U.S. Pat. No. 4,901,020—Ladbeck et al. and U.S. Pat. No. 4,818,940—Henning et al.

Given such a computer-based calculation tool, the process for deriving this flip-angle series can be generally summarized in the following four steps (steps I-IV) briefly discussed below. Firstly, STEP I, the pulse sequence timing parameters (e.g., repetition time, echo spacing(s), other time delays), the pulse sequence magnetic-field gradient configuration, the desired shape of the prescribed signal evolution during the echo train, the T1 and T2 relaxation parameters and the proton density for the “target” tissue, and a target signal intensity are chosen. The signal evolution may assume any physically-realizable shape. Some examples, but not limited thereto, include: a constant; a linear decay; an exponential decay; a linear or exponential decay for the initial portion and a constant for the remainder; and a linear or exponential decay for the initial portion, a constant for the second portion and a linear or exponential decay for the remainder. The T1, T2 and proton density for the target tissue may equal those for a specific biological tissue (e.g., brain gray matter) or material, or they may be arbitrarily chosen. The target signal intensity is the desired signal intensity corresponding to a specific echo in the echo train (e.g., the first or the middle echo).

Secondly, STEP II, the flip angle β_i (see FIG. 1) which yields the desired signal intensity for the i^{th} echo interval is determined, where i ranges from 1 to the number of refocusing RF pulses in the echo train. This flip angle can be calculated using any appropriate method such as a “brute-force” search or interval bisection and interpolation. See Forsythe G. E., Malcolm M. A., Moler C. B., “Computer

11

Methods for Mathematical Computations”, Prentice-Hall, Englewood Cliffs, 1977, of which is hereby incorporated by reference in its entirety.

Thirdly, STEP III, the pulse number i is incremented and the second step is repeated until all flip angles for a given echo train are calculated. If, for any value of i , the desired signal intensity for the i^{th} echo interval cannot be achieved, the target signal intensity is reduced and the calculation process is restarted.

Fourthly, STEP IV, if the pulse sequence under consideration requires more than one repetition of the echo train to acquire the desired k-space data, the second and third steps are repeated as necessary until a steady state of the magnetization is reached.

After a given series of variable flip angles are derived, the target signal intensity can be incremented until the maximum value for which the prescribed signal-evolution shape can be realized is reached, thus allowing determination of the maximum signal and/or contrast values that can be obtained for a specific pulse sequence configuration and signal evolution.

Next, exemplary hardware, firmware and software implementations of the methods of the present invention are discussed.

FIG. 8 illustrates a preferred method for practicing the invention as implemented by, for example, software loaded into the control unit of the MR apparatus. Once the process starts and initializes, at step 200, the contrast-preparation is provided by generating at least one of a RF pulse, magnetic-field gradient pulse, and/or time delay. The contrast-preparation encodes the magnetization with at least one desired image contrast.

During step 300, flip angles and phases are calculated for refocusing RF pulses that are applied in subsequent data-acquisition steps so as to yield—for selected values of T1 and T2 relaxation times and proton density—a prescribed time course for the amplitudes and phases of the RF magnetic resonance signals that are generated by the refocusing RF pulses.

During step 400, data-acquisition is achieved based on an echo-train acquisition, comprising the following: i) an excitation RF pulse having a flip angle and phase; ii) at least two refocusing RF pulses, each having a flip angle and phase as determined by the calculation step; and iii) magnetic-field gradient pulses that encode spatial information into at least one of the RF magnetic resonance signals that follow at least one of the at least two refocusing RF pulses.

Also, in step 500, magnetization-recovery is provided whereby the magnetization-recovery comprises a time delay to allow magnetization to relax. Finally, as illustrated by step 550, the aforementioned method is repeated until a predetermined extent of spatial-frequency space has been sampled.

It is important to appreciate that the various steps discussed herein need not be performed in the illustrated order, and in fact it may be preferred to perform the steps, at least in part, simultaneously or omit some of the illustrated steps, at least in part.

Next, turning to FIGS. 9A-9B, an exemplary method for the calculating step 300 is provided. In step 310, T1, T2, and proton density are chosen, and in step 320, a desired prescribed signal evolution which describes the time course of the signal amplitudes and phases, is also chosen. Turning to steps 330 and 340, the characteristics of the contrast-preparation and data-acquisition, respectively, are chosen (additional details shall be discussed with FIGS. 10-11). Provided in step 350, the characteristics of the magnetiza-

12

tion-recovery period are chosen. Accordingly, at step 360, the process of calculating the individual flip angles starts and is initialized with thermal equilibrium magnetization. At step 370, the magnetization, M_1 , is calculated that exists immediately after the contrast-preparation and excitation RF pulse are applied. At step 380, starting with M_1 which is the input magnetization for the first refocusing RF pulse, the flip angle and phase are calculated for the current refocusing RF pulse that yields the desired corresponding signal amplitude and phase, and this process is repeated until the last refocusing RF pulse is achieved, step 385. If the last pulse is achieved, then step 390 permits relaxation during the magnetization-recovery period. In steps 392 and 394, the process checks for a single-shot pulse sequence method and whether steady state has been achieved. This accounts for the effects of multiple applications of the contrast-preparation, data-acquisition and magnetization-recovery steps if required to sample the desired extent of spatial-frequency space. As used herein, the “steady state” of magnetization is a state created by certain fast (with repeat times short compared to relaxation times) imaging pulse sequences during which both the longitudinal and the transverse components of the nuclear magnetization exhibit a steady temporal state. Once steady state is satisfied the process checks whether the target signal has been achieved, step 396, so as to increment across the overall signal level.

Turning to the exemplary contrast-preparation process as shown in FIG. 10, at step 331, the following are chosen: flip angle, phase, waveform and the time of application of any RF pulses. In step 332, the following are chosen: strength, duration, time-dependence, axis and time of application of any magnetic-field gradient pulses. Moreover, in step 333, the following are chosen: duration and time of application of any time delays.

Turning to the exemplary data-acquisition process as shown in FIG. 11, at step 341, the following are chosen: the flip angle and phase of the excitation RF pulse. Also, at steps 342, 343, and 344, the times between all RF pulses; number of refocusing RF pulses; and configuration of spatial-encoding magnetic-field gradient pulses are chosen, respectively.

EXAMPLES

Specific implementations of the present invention methodology are useful to illustrate its nature. These examples are non-limiting and are offered as exemplary only. For this purpose, set forth herein are experimental studies in which the present invention method was used to generate variable-flip-angle series for three-dimensional (3D) T2-weighted MR imaging of the human brain and cervical spine using a “turbo-SE” type (i.e., RARE-as set forth in Henning et al., Magn. Res. Med. 1986, 3:823-833) spin-echo-train pulse sequence, of which is hereby incorporated by reference in its entirety. Brain studies were performed at 1.5 Tesla and 3 Tesla; spine studies were performed at 1.5 Tesla. MR images were obtained using a 1.5-Tesla commercial whole-body imager (MAGNETOM SYMPHONY, Siemens Medical Systems, Iselin, N.J.) or a 3-Tesla commercial whole-body imager (MAGNETOM ALLEGRA, Siemens Medical Systems, Iselin, N.J.). The standard head RF coil supplied with the imager was used. Informed consent was obtained from all subjects prior to imaging.

Turning to FIGS. 2-3, FIG. 2 shows an example of a prescribed signal evolution for gray matter that can be used to generate T2-weighted MR images of the brain. The evolution consists of the following: exponential decay during the first 20 echoes with decay constant of 114 ms,

constant for 66 echoes, and exponential decay during the remaining echoes with decay constant of 189 ms. FIG. 3 shows the corresponding variable-flip-angle series that was derived using the present invention methods as described herein. Using an interactive computer-based (Ultra-60 work-
 5 station; Sun Microsystems, Inc.) theoretical model, and the prescribed signal evolution for brain gray matter, at 1.5 Tesla (see FIG. 2), the four-step process described above was used to derive the corresponding variable-flip-angle series depicted in FIG. 3. The pulse-sequence parameters included an echo train length of 160, an echo spacing of 4.1 ms (fixed), a total echo-train duration of 656 ms, a repetition time of 2750 ms and an effective echo time of 328 ms.

Example No. 1

FIGS. 4B-4F show an example of MR brain images obtained at 1.5 Tesla using the variable-flip-angle series of FIG. 3 in a “turbo-SE” type spin-echo-train pulse sequence; collectively. In particular, the T2-weighted two-dimensional and three-dimensional SE images of FIGS. 4(A) and 4(B)-
 4(C), respectively, were obtained from a 59 year old volunteer for demonstrating age-related non-specific white-matter lesions. As can be observed, arrows mark several of these lesions. The adjacent 1-mm thick 3D images, as shown in
 FIGS. 4B-4D, correspond to the single 3-mm thick 2D image in FIG. 4A. In the 3D images, the phase-encoding direction corresponding to the 160-echo train is left-to-right in FIGS. 4B-4D and 4F. No image artifacts secondary to this very long spin-echo train are apparent. Pulse sequence
 parameters for the 10 minute 3D acquisition included the following: repetition time/effective echo time, 2750/328 ms; matrix, 256×160×216; field of view, 25.6×16.0×21.6 cm; voxel size, 1.0×1.0×1.0 mm; echo spacing, 4.1 ms; echo
 train length, 160; and full-Fourier acquisition. Pulse sequence parameters for the 14.8 minute 2D acquisition included the following: repetition time/first echo time/second
 echo time, 2750/20/80 ms; matrix, 256×160; field of view, 25.6×16.0 cm; section thickness, 3.0 mm; number of sections, 54; full-Fourier acquisition; first-order flow compensation; and reduced bandwidth on second echo.

In summary, using the variable-flip-angle series of FIG. 3, the T2-weighted 3D images were obtained at 1.5 Tesla from the brain of a healthy volunteer, and were compared to images from a 2D conventional-SE pulse sequence (see FIG. 4). The images in FIG. 4 exhibit two important features: (1) the very long spin-echo-train images (FIGS. 4B-4F) display high contrast between the age-related lesions in the brain of this volunteer and surrounding normal appearing white matter, indicating that this echo train shall provide clinically useful contrast characteristics that appear very similar to those for conventional T2-weighted SE images (FIG. 4A); and (2) the thin 1-mm sections provide an improved definition of lesion location and extent; the lesions seen in the 2D image appear, to varying degrees, in three adjacent 1-mm sections. Furthermore, the overall image quality for the very long spin-echo-train and conventional-SE images is similar, despite the much thinner sections of the former.

Finally, referring to FIGS. 4E-4F, such figures depict the largest lesion in sagittal and coronal orientations, respectively, this demonstrates the capability of the 3D acquisition to provide high-quality images in arbitrary orientations.

Example No. 2

Next, referring to FIGS. 5A-5C, using the same pulse-sequence parameters as described above in FIGS. 2-4,

T2-weighted images were also obtained at 3 Tesla from the brain of a healthy volunteer. The three 1-mm thick images were all reconstructed from the same 3D acquisition. These images appeared similar to those obtained at 1.5 Tesla, but
 5 exhibited higher signal-to-noise ratios. Of particular importance, the partial-body and local values for the specific absorption rate (SAR) were 1.29 W/kg and 3.16 W/kg, respectively, compared to the FDA limits for partial-body and local SAR of 3.0 and 8.0 W/kg, respectively. The SAR values at 3 Tesla were much less than the FDA limits,
 10 indicating that there remains substantial latitude in the pulse-sequence design from the perspective of power deposition, including the possibility for even more refocusing RF pulses per excitation. Thus, according to the present invention, although the use of spin-echo-train methods has been
 15 restricted at high fields, such as 3 Tesla, due to power deposition limits, very long spin-echo trains based on prescribed signal evolutions permit high-quality brain images to be acquired at 3 Tesla with power deposition well below the FDA limits.

Example No. 3

Referring to FIG. 6, as the final example, FIG. 6 shows a T2-weighted sagittal image of the cervical spinal cord obtained at 1.5 Tesla from a healthy volunteer, again using a 160-echo train. The quality of cervical-spine images from T2-weighted MRI techniques is often compromised by artifacts arising from the pulsatile motion of the CSF surrounding the cord. One potential solution to this problem is to use FLAIR imaging. See Hajnal et al. While this technique can completely suppress the signal from CSF, there remains some concern about its ability to depict the full range of clinically-relevant lesions. See Hittmair et al. and
 25 Keiper et al. As illustrated in FIG. 6, an alternative is to use a T2-weighted technique with a very long spin-echo train based on a prescribed signal evolution, as provided by the present invention. The signal from CSF is uniformly suppressed without generating motion artifacts. The combination of the long echo train and the relatively low flip angles of the refocusing RF pulses results in suppression of even slowly moving fluid. The “dark-CSF” image in FIG. 6 differs from a FLAIR image, among other things, in an important way. With FLAIR, the CSF is suppressed based on its long T1. Hence, the signals from any other tissues with relatively long T1s will be diminished. This is one potential explanation for the problems in depicting certain lesions with FLAIR—these lesions may have long T1 components. In contrast, turning to the present invention, the CSF suppressed in FIG. 6 is solely due to its motion; long T1 lesions in the cord will be unaffected.

An advantage of the present invention is that it provides a method, apparatus, and computer useable medium (readable media) to extend the usable duration of the echo train in magnetic resonance imaging pulse sequences such as RARE, turbo-spin-echo, fast-spin-echo or GRASE, substantially beyond that obtainable with conventional methods. This increase in the echo-train duration can be used to decrease the image acquisition time and/or increase the spatial resolution. The power deposition achieved with this technique is much less than that for conventional spin-echo-train pulse sequences, and thus the invention shall be especially useful, among other things, for human imaging applications at high magnetic field strengths.

Another advantage of the present invention is that it improves the imaging of various objects and zones, including the brain. The present invention is also applicable to

other regions of the body such as the spinal cord or joints. In particular, the present invention enables high-resolution 3D imaging of the brain with clinically-reasonable acquisition times, which is useful for quantitative imaging of disseminated diseases such as multiple sclerosis. For these diseases, high-resolution 3D imaging provides a valuable tool for monitoring disease progression and response to therapy during treatment or drug trials. The present invention is also useful for non-human applications of magnetic resonance, such as imaging of materials (e.g., plants or food products) or animal models of disease at high field.

Further yet, an advantage of the present invention is that it provides a means to shorten image acquisition times and/or increase spatial resolution for widely-used spin-echo-train magnetic resonance imaging techniques. Such improvements will in turn make it feasible to obtain images with certain valuable combinations of resolution and image contrast which have not been practical heretofore. In addition, the present invention permits spin-echo-train methods to be used for high-field imaging that would not otherwise meet the safety guidelines established by the Food and Drug Administration for power deposition in human MRI.

Finally, another advantage of the present invention method and apparatus is that it explicitly considers the T1 and T2 relaxation times for the tissues of interest and thereby permits the desired image contrast to be incorporated into the tissue signal evolutions corresponding to the long echo train. Given the considerable role that spin-echo-train methods already play in MR imaging, the present invention methodology will be of significant importance.

All US patents and US patent applications cited herein are incorporated herein by reference in their entirety and for all purposes to the same extent as if each individual patent or patent application was specifically and individually indicated to be incorporated by reference in its entirety for all purposes.

The invention may be embodied in other specific forms without departing from the spirit or essential characteristics thereof. The foregoing embodiments are therefore to be considered in all respects illustrative rather than limiting of the invention described herein. Scope of the invention is thus indicated by the appended claims rather than by the foregoing description, and all changes which come within the meaning and range of equivalency of the claims are therefore intended to be embraced herein.

We claim:

[1. A method for generating a spin echo pulse sequence for operating a magnetic resonance imaging apparatus for imaging an object that permits at least one of lengthening usable echo-train duration, reducing power deposition and incorporating desired image contrast into the tissue signal evolutions, said method comprising:

- a) providing contrast-preparation, said contrast-preparation comprising generating at least one of at least one radio-frequency pulse, at least one magnetic-field gradient pulse, and at least one time delay, whereby said contrast preparation encodes the magnetization with at least one desired image contrast;
- b) calculating flip angles and phases of refocusing radio-frequency pulses that are applied in a data-acquisition step, wherein said calculation provides desired prescribed signal evolution and desired overall signal level, said calculation comprises:
 - i) selecting values of T1 and T2 relaxation times and selecting proton density;
 - ii) selecting a prescribed time course of the amplitudes and phases of the radio-frequency magnetic reso-

nance signals that are generated by said refocusing radio-frequency pulses; and

- iii) selecting characteristics of said contrast-preparation step, said data-acquisition step and a magnetization-recovery step, with the exception of the flip angles and phases of the refocusing radio-frequency pulses that are to be calculated; and
- c) providing said-data acquisition step based on a spin echo train acquisition, said data-acquisition step comprises:
 - i) an excitation radio-frequency pulse having a flip angle and phase;
 - ii) at least two refocusing radio-frequency pulses, each having a flip angle and phase as determined by said calculation step; and
 - iii) magnetic-field gradient pulses that encode spatial information into at least one of said radio-frequency magnetic resonance signals that follow at least one of said refocusing radio-frequency pulses;
- d) providing magnetization-recovery, said magnetization-recovery comprises a time delay to allow magnetization to relax; and
- e) repeating steps (a) through (d) until a predetermined extent of spatial frequency space has been sampled.]

[2. The method of claim 1, wherein said calculation of the flip angles and phases is generated using an appropriate analytical or computer-based algorithm.]

[3. The method of claim 1, wherein said calculation of the flip angles and phases is generated to account for, the effects of multiple applications of: said contrast-preparation, said data-acquisition and said magnetization-recovery steps, which are required to sample the desired extent of spatial-frequency space.]

[4. The method of claim 1, wherein a two-dimensional plane of spatial-frequency space is sampled.]

[5. The method of claim 1, wherein a three-dimensional volume of spatial-frequency space is sampled.]

[6. The method of claim 1, wherein at least one of said contrast-preparation and magnetization-recovery steps is omitted.]

[7. The method of claim 1, wherein said calculation step is performed once before one of said first contrast-preparation step and said first data-acquisition step.]

[8. The method of claim 1, wherein at least one of at least one said contrast-preparation step, at least one said data-acquisition step and at least one said magnetization-recovery step is initiated by a trigger signal to synchronizes the pulse sequence with at least one of at least one external temporal event and at least one internal temporal event.]

[9. The method of claim 8, wherein said external and internal events comprise at least one of at least one voluntary action, at least one involuntary action, at least one respiratory cycle and at least one cardiac cycle.]

[10. The method of claim 1, wherein at least one of at least one radio-frequency pulse and at least one magnetic-field gradient pulse is applied as part of at least one of at least one said magnetization-preparation step and at least one said data-acquisition step is for the purpose of stabilizing the response of at least one of magnetization related system and said apparatus related hardware system.]

[11. The method of claim 1, wherein time duration varies between repetitions for at least one of at least one said contrast-preparation step, at least one said data-acquisition step and at least one said magnetization-recovery step.]

17

[12. The method of claim 1, wherein the time periods between consecutive refocusing radio-frequency pulses applied during said data-acquisition steps are all of equal duration.]

[13. The method of claim 1, wherein time periods between consecutive refocusing radio-frequency pulses applied during said data-acquisition steps vary in duration amongst pairs of refocusing radio-frequency pulses during at least one said data-acquisition step.]

[14. The method of claim 1 wherein all the radio-frequency pulses are at least one of non-spatially selective and non-chemically selective.]

[15. The method of claim 1, wherein at least one of the radio-frequency pulses is at least one of spatially selective in one of one, two and three dimensions, chemically selective, and adiabatic.]

[16. The method of claim 1, wherein during each said data-acquisition step, the phase difference between the phase for the excitation radio-frequency pulse and the phases for all refocusing radio-frequency pulses is about 90 degrees.]

[17. The method of claim 1, wherein during each data-acquisition step, the phase difference between the phase for any refocusing radio-frequency pulse and the phase for the immediately subsequent refocusing radio-frequency pulses is about 180 degrees, and the phase difference between the phase for the excitation radio-frequency pulse and the phase for the first refocusing pulse is one of about 0 degrees and about 180 degrees.]

[18. The method of claim 17, wherein the flip angle for the excitation radio-frequency pulse is about one-half of the flip angle for the first refocusing radio-frequency pulse.]

[19. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during each said data-acquisition step are configured so as to collect data, following each of at least one of the refocusing radio-frequency pulses, for one line in spatial-frequency space which is parallel to all other lines of data so collected, so as to collect the data using a magnetic resonance imaging technique selected from the group consisting of rapid acquisition with relaxation enhancement (RARE), fast spin echo (FSE), and turbo spin echo (TSE or TurboSE).]

[20. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during each said data-acquisition step are configured so as to collect data, following each of at least one of the refocusing radio-frequency pulses, for two or more lines in spatial-frequency space which are parallel to all other lines of data so collected, so as to collect the data using a magnetic resonance imaging technique selected from the group consisting of gradient and spin echo (GRASE) and turbo gradient spin echo (TGSE or TurboGSE).]

[21. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during each said data-acquisition step are configured so as to collect data, following each of at least one of the refocusing radio-frequency pulses, for one or more lines in spatial-frequency space, each of which pass through one of a single point in spatial-frequency space and a single line in spatial-frequency space, so as to collect the data using a magnetic resonance imaging technique selected from the group consisting of radial sampling or projection-reconstruction sampling.]

[22. The method of claim 21, wherein the single point in spatial-frequency space is about zero spatial frequency.]

[23. The method of claim 21, wherein the single line in spatial-frequency space includes zero spatial frequency.]

18

[24. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during each said data-acquisition step are configured so as to collect data, following each of at least one of the refocusing radio-frequency pulses, along a spiral trajectory in spatial-frequency space, each trajectory of which is contained in one of two dimensions and three dimensions, and each trajectory of which passes through one of a single point in spatial-frequency space and a single line in spatial-frequency space.]

[25. The method of claim 24, wherein the single point in spatial-frequency space is about zero spatial frequency.]

[26. The method of claim 24, wherein the single line in spatial-frequency space includes zero spatial frequency.]

[27. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during at least one of said data-acquisition steps are configured to collect sufficient spatial-frequency data to reconstruct at least two image sets, each of which exhibits contrast properties different from the other image sets.]

[28. The method of claim 27, wherein at least some of the spatial-frequency data collected during at least one of said data-acquisition steps is used in the reconstruction of more than one image set, whereby the data is shared between image sets.]

[29. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during at least one of said data-acquisition steps are configured so that, for the echo following at least one of the refocusing radio-frequency pulses, at least one of the first moment, the second moment and the third moment corresponding to at least one of the spatial-encoding directions is approximately zero.]

[30. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during at least one of said data-acquisition steps are configured so that, following at least one of the refocusing radio-frequency pulses, the zeroth moment measured over the time period between said refocusing radio-frequency pulse and the immediately consecutive refocusing radio-frequency pulse is approximately zero for at least one of the spatial-encoding directions.]

[31. The method of claim 1, wherein during all said data-acquisition steps the duration of all data-sampling periods are equal.]

[32. The method of claim 1, wherein during at least one of said data-acquisition steps at least one of the data-sampling periods has a duration that differs from the duration of at least one other data-sampling period.]

[33. The method of claim 1, wherein the spatial-encoding magnetic-field gradient pulses applied during said data-acquisition steps are configured so that the extent of spatial-frequency space sampled along at least one of the spatial-encoding directions is not symmetric with respect to zero spatial frequency, whereby a larger extent of spatial-frequency space is sampled to one side of zero spatial frequency as compared to the opposite side of zero spatial frequency.]

[34. The method of claim 33 wherein said spatial-frequency data is reconstructed using a partial-Fourier reconstruction algorithm.]

[35. The method of claim 1, wherein during at least one of said data-acquisition steps the temporal order in which spatial-frequency space data is collected for at least one of the spatial-encoding directions is based on achieving at least one of selected contrast properties in the image and selected properties of the corresponding point spread function.]

[36. The method of claim 1, wherein during at least one of said data-acquisition steps the temporal order in which

19

spatial-frequency space data is collected is different from that for at least one other data-acquisition step.]

[37. The method of claim 1, wherein during at least one of said data-acquisition steps the extent of spatial-frequency space data that is collected is different from that for at least one other data-acquisition step.]

[38. The method of claim 1, wherein during at least one of said data-acquisition steps spatial encoding of the radio-frequency magnetic resonance signal that follows at least one of the refocusing radio-frequency pulse is performed using only phase encoding so that said signal is received by the radio-frequency transceiver in the absence of any applied magnetic-field gradient pulses and hence contains chemical-shift information.]

[39. The method of claim 1, wherein at least one navigator radio-frequency pulse is incorporated into the pulse sequence for the purpose of determining the displacement of a portion of the object.]

[40. A magnetic resonance imaging apparatus generating a spin echo pulse sequence in order to operate the apparatus in imaging an object that permits at least one of lengthening usable echo-train duration, reducing power deposition and incorporating desired image contrast into the tissue signal evolutions, the apparatus comprising:

a main magnet system generating a steady magnetic field;

a gradient magnet system generating temporary gradient magnetic fields;

a radio-frequency transmitter system generating radio-frequency pulses;

a radio-frequency receiver system receiving magnetic resonance signals;

a reconstruction unit reconstructing an image of the object from the received magnetic resonance signals; and

a control unit generating signals controlling the gradient magnet system, the radio-frequency transmitter system, the radio-frequency receiver system, and the reconstruction unit, wherein the control unit generates signals causing:

a) providing contrast-preparation, said contrast-preparation comprising generating at least one of at least one radio-frequency pulse, at least one magnetic-field gradient pulse, and at least one time delay, whereby said contrast preparation encodes the magnetization with at least one desired image contrast;

b) calculating flip angles and phases of refocusing radio-frequency pulses that are applied in a data-acquisition step, wherein said calculation provides desired prescribed signal evolution and desired overall signal level, said calculation comprises:

i) selecting values of T1 and T2 relaxation times and selecting proton density;

ii) selecting a prescribed time course of the amplitudes and phases of the radio-frequency magnetic resonance signals that are generated by said refocusing radio-frequency pulses; and

iii) selecting characteristics of said contrast-preparation step, said data-acquisition step and a magnetization-recovery step, with the exception of the flip angles and phases of the refocusing radio-frequency pulses that are to be calculated; and

20

c) providing said-data acquisition step based on a spin echo train acquisition, said data-acquisition step comprises:

i) an excitation radio-frequency pulse having a flip angle and phase,

ii) at least two refocusing radio-frequency pulses, each having a flip angle and phase as determined by said calculation step, and

iii) magnetic-field gradient pulses that encode spatial information into at least one of said radio-frequency magnetic resonance signals that follow at least one of said refocusing radio-frequency pulses;

d) providing magnetization-recovery, said magnetization-recovery comprises a time delay to allow magnetization to relax; and

e) repeating steps (a) through (d) until a predetermined extent of spatial frequency space has been sampled.]

[41. A magnetic resonance imaging apparatus generating a spin echo pulse sequence in order to operate the apparatus in imaging an object that permits at least one of lengthening usable echo-train duration, reducing power deposition and incorporating desired image contrast into the tissue signal evolutions, the apparatus comprising:

main magnet means generating a steady magnetic field;

gradient magnet means generating temporary gradient magnetic fields;

radio-frequency transmitter means generating radio-frequency pulses;

radio-frequency receiver means receiving magnetic resonance signals;

reconstruction means reconstructing an image of the object from the received magnetic resonance signals; and

control means generating signals controlling the gradient magnet means, the radio-frequency transmitter means, the radio-frequency receiver means, and the reconstruction means, wherein the control means generates signals causing:

a) providing contrast-preparation, said contrast-preparation comprising generating at least one of at least one radio-frequency pulse, at least one magnetic-field gradient pulse, and at least one time delay, whereby said contrast preparation encodes the magnetization with at least one desired image contrast;

b) calculating flip angles and phases of refocusing radio-frequency pulses that are applied in a data-acquisition step, wherein said calculation provides desired prescribed signal evolution and desired overall signal level, said calculation comprises:

i) selecting values of T1 and T2 relaxation times and selecting proton density;

ii) selecting a prescribed time course of the amplitudes and phases of the radio-frequency magnetic resonance signals that are generated by said refocusing radio-frequency pulses; and

iii) selecting characteristics of said contrast-preparation step, said data-acquisition step and a magnetization-recovery step, with the exception of the flip angles and phases of the refocusing radio-frequency pulses that are to be calculated;

21

c) providing said-data acquisition step based on a spin echo train acquisition, said data-acquisition step comprises:

- i) an excitation radio-frequency pulse having a flip angle and phase,
- ii) at least two refocusing radio-frequency pulses, each having a flip angle and phase as determined by said calculation step, and
- iii) magnetic-field gradient pulses that encode spatial information into at least one of said radio-frequency magnetic resonance signals that follow at least one of said refocusing radio-frequency pulses;

d) providing magnetization-recovery, said magnetization-recovery comprises a time delay to allow magnetization to relax; and

e) repeating steps (a) through (d) until a predetermined extent of spatial frequency space has been sampled.]

[42. A computer readable media carrying encoded program instructions for causing a programmable magnetic resonance imaging apparatus to perform the method of claim 1.]

[43. A computer program provided on a computer useable readable medium having computer program logic enabling at least one processor in a magnetic resonance imaging apparatus to generate a spin echo pulse sequence that permits at least one of lengthening usable echo-train duration, reducing power deposition and incorporating desired image contrast into the tissue signal evolutions, said computer program logic comprising:

- a) providing contrast-preparation, said contrast-preparation comprising generating at least one of at least one radio-frequency pulse, at least one magnetic-field gradient pulse, and at least one time delay, whereby said contrast preparation encodes the magnetization with at least one desired image contrast;
- b) calculating flip angles and phases of refocusing radio-frequency pulses that are applied in a data-acquisition step, wherein said calculation provides desired prescribed signal evolution and desired overall signal level, said calculation comprises:
 - i) selecting values of T1 and T2 relaxation times and selecting proton density;
 - ii) selecting a prescribed time course of the amplitudes and phases of the radio-frequency magnetic resonance signals that are generated by said refocusing radio-frequency pulses; and
 - iii) selecting characteristics of said contrast-preparation step, said data-acquisition step and a magnetization-recovery step, with the exception of the flip angles and phases of the refocusing radio-frequency pulses that are to be calculated; and

c) providing said-data acquisition step based on a spin echo train acquisition, said data-acquisition step comprises:

- i) an excitation radio-frequency pulse having a flip angle and phase;
- ii) at least two refocusing radio-frequency pulses, each having a flip angle and phase as determined by said calculation step; and
- iii) magnetic-field gradient pulses that encode spatial information into at least one of said radio-frequency magnetic resonance signals that follow at least one of said refocusing radio-frequency pulses;

d) providing magnetization-recovery, said magnetization-recovery comprises a time delay to allow magnetization to relax; and

22

e) repeating steps (a) through (d) until a predetermined extent of spatial frequency space has been sampled.]

[44. The method of claim 40, wherein at least one of said contrast-preparation and magnetization-recovery steps is omitted.]

[45. The method of claim 41, wherein at least one of said contrast-preparation and magnetization-recovery steps is omitted.]

[46. The method of claim 43, wherein at least one of said contrast-preparation and magnetization-recovery steps is omitted.]

47. A method of generating a T2-weighted fast-spin-echo or turbo-spin-echo pulse sequence having refocusing radio-frequency pulses with varying flip angles, said method comprising:

generating, via a control unit, a three-dimensional T2-weighted fast-spin-echo or turbo-spin-echo pulse sequence used in operating a magnetic resonance imaging apparatus that images tissues of a human subject, the generated pulse sequence having varying flip angles that vary among a majority of refocusing radio-frequency pulses of an echo train by decreasing to a minimum value and later increasing, and

wherein the varying flip angles result in a reduced power deposition compared to the power deposition that is obtained using refocusing radio-frequency pulses with constant flip angles of approximately 180 degrees;

applying the pulse sequence to a radio-frequency transmitter coil of the magnetic resonance imaging apparatus to generate radio-frequency pulses in an examination zone that includes tissues of the human subject and receiving resulting magnetic resonance signals from tissues of the human subject, using a radio-frequency receiver coil of the magnetic resonance imaging apparatus; and

reconstructing magnetic resonance images from the resulting magnetic resonance signals from the tissues of the human subject,

wherein the reconstructed magnetic resonance images have a T2-weighted contrast, and

wherein the T2-weighted contrast is substantially the same as contrast in T2-weighted magnetic resonance images generated from a fast-spin-echo or turbo-spin-echo pulse sequence using refocusing radio-frequency pulses with constant flip angles of approximately 180 degrees.

48. The method of claim 47, wherein the pulse sequence has a usable echo-train duration for spin-echo train imaging that is lengthened substantially beyond that achievable with constant, low-flip-angle or pseudosteady-state approaches.

49. The method of claim 47, wherein the varying flip angles are calculated to provide a prescribed signal evolution.

50. The method of claim 49, wherein the prescribed signal evolution is associated with T1 and T2 relaxation times that are arbitrarily chosen.

51. The method of claim 50, wherein the pulse sequence has a usable echo-train duration for spin-echo train imaging that is lengthened substantially beyond that achievable with constant, low-flip-angle or pseudosteady-state approaches.

52. A magnetic resonance imaging (MRI) apparatus that images tissues of a human subject and is configured to generate a T2-weighted fast-spin-echo or turbo-spin-echo pulse sequence having refocusing radio-frequency pulses with varying flip angles, the apparatus comprising:

a main magnet system that generates a steady magnetic field;
 a gradient magnet system that generates temporary gradient magnetic fields;
 a radio-frequency transmitter system that generates radio-frequency pulses;
 a radio-frequency receiver system that receives magnetic resonance signals;
 a reconstruction unit that reconstructs magnetic resonance images of the subject from the received magnetic resonance signals from the tissues of the human subject; and
 a control unit that generates signals controlling the gradient magnet system, the radio-frequency transmitter system, the radio-frequency receiver system, and the reconstruction unit, wherein the control unit further provides signals that generate:
 a three-dimensional T2-weighted fast-spin-echo or turbo-spin-echo pulse sequence used in operating the MRI apparatus, the generated pulse sequence having varying flip angles that vary among a majority of refocusing radio-frequency pulses of an echo train by decreasing to a minimum value and later increasing, and
 wherein the varying flip angles result in a reduced power deposition compared to the power deposition that is obtained using refocusing radio-frequency pulses with constant flip angles of approximately 180 degrees,
 wherein the reconstructed magnetic resonance images have a T2-weighted contrast, and
 wherein the T2-weighted contrast is substantially the same as contrast in T2-weighted magnetic resonance images generated from a fast-spin-echo or turbo-spin-echo pulse sequence using refocusing radio-frequency pulses with constant flip angles of approximately 180 degrees.

53. The apparatus of claim 52, wherein the pulse sequence that is generated has a usable echo-train duration for spin-echo train imaging that is lengthened substantially beyond that achievable with constant, low-flip-angle or pseudosteady-state approaches.

54. The apparatus of claim 52, wherein a control unit executes a software program that performs calculations and is configured to calculate the varying flip angles to provide a prescribed signal evolution.

55. The apparatus of claim 54, wherein the prescribed signal evolution is associated with T1 and T2 relaxation times that are arbitrarily chosen.

56. The apparatus of claim 55, wherein the pulse sequence that is generated has a usable echo-train duration for spin-echo train imaging that is lengthened substantially beyond that achievable with constant, low-flip-angle or pseudosteady-state approaches.

57. A non-transitory computer readable medium having computer program logic that when implemented enables one or more processors in a magnetic resonance imaging apparatus that images tissues of a human subject to generate a T2-weighted fast-spin-echo or turbo-spin-echo pulse sequence having refocusing radio-frequency pulses with varying flip angles, said computer program logic comprising:

logic for generating a three-dimensional T2-weighted fast-spin-echo or turbo-spin-echo pulse sequence used in operating the magnetic resonance imaging apparatus, the generated pulse sequence having varying flip angles that vary among a majority of refocusing radio-frequency pulses of an echo train by decreasing to a minimum value and later increasing, and

wherein the varying flip angles result in a reduced power deposition compared to the power deposition that is obtained using refocusing radio-frequency pulses with constant flip angles of approximately 180 degrees; and
 logic for reconstructing magnetic resonance images from magnetic resonance signals received from tissues of the human subject as a result of applying the generated pulse sequence,

wherein the reconstructed magnetic resonance images have a T2-weighted contrast, and

wherein the T2-weighted contrast is substantially the same as contrast in T2-weighted magnetic resonance images generated from a fast-spin-echo or turbo-spin-echo pulse sequence using refocusing radio-frequency pulses with constant flip angles of approximately 180 degrees.

58. The non-transitory computer readable medium having computer program logic as defined in claim 57, wherein the pulse sequence that is generated has a usable echo-train duration for spin-echo train imaging that is lengthened substantially beyond that achievable with constant, low-flip-angle or pseudosteady-state approaches.

59. The non-transitory computer readable medium having computer program logic as defined in claim 57, wherein the computer program logic also calculates the varying flip angles to provide a prescribed signal evolution.

60. The non-transitory computer readable medium having computer program logic as defined in claim 59, wherein the prescribed signal evolution is associated with T1 and T2 relaxation times that are arbitrarily chosen.

61. The non-transitory computer readable medium having computer program logic as defined in claim 60, wherein the pulse sequence that is generated has a usable echo-train duration for spin-echo train imaging that is lengthened substantially beyond that achievable with constant, low-flip-angle or pseudosteady-state approaches.

* * * * *