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(54) **POWER CONVERTER WITH DEMAND
PULSE ISOLATION**

(58) **Field of Classification Search**

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See application file for complete search history.

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(63) Continuation of application No. 15/090,929, filed on Apr. 5, 2016, now Pat. No. Re. 47,031, which is an application for the reissue of Pat. No. 9,071,152.

(60) Provisional application No. 61/667,473, filed on Jul. 3, 2012, provisional application No. 61/727,795, filed on Nov. 19, 2012.

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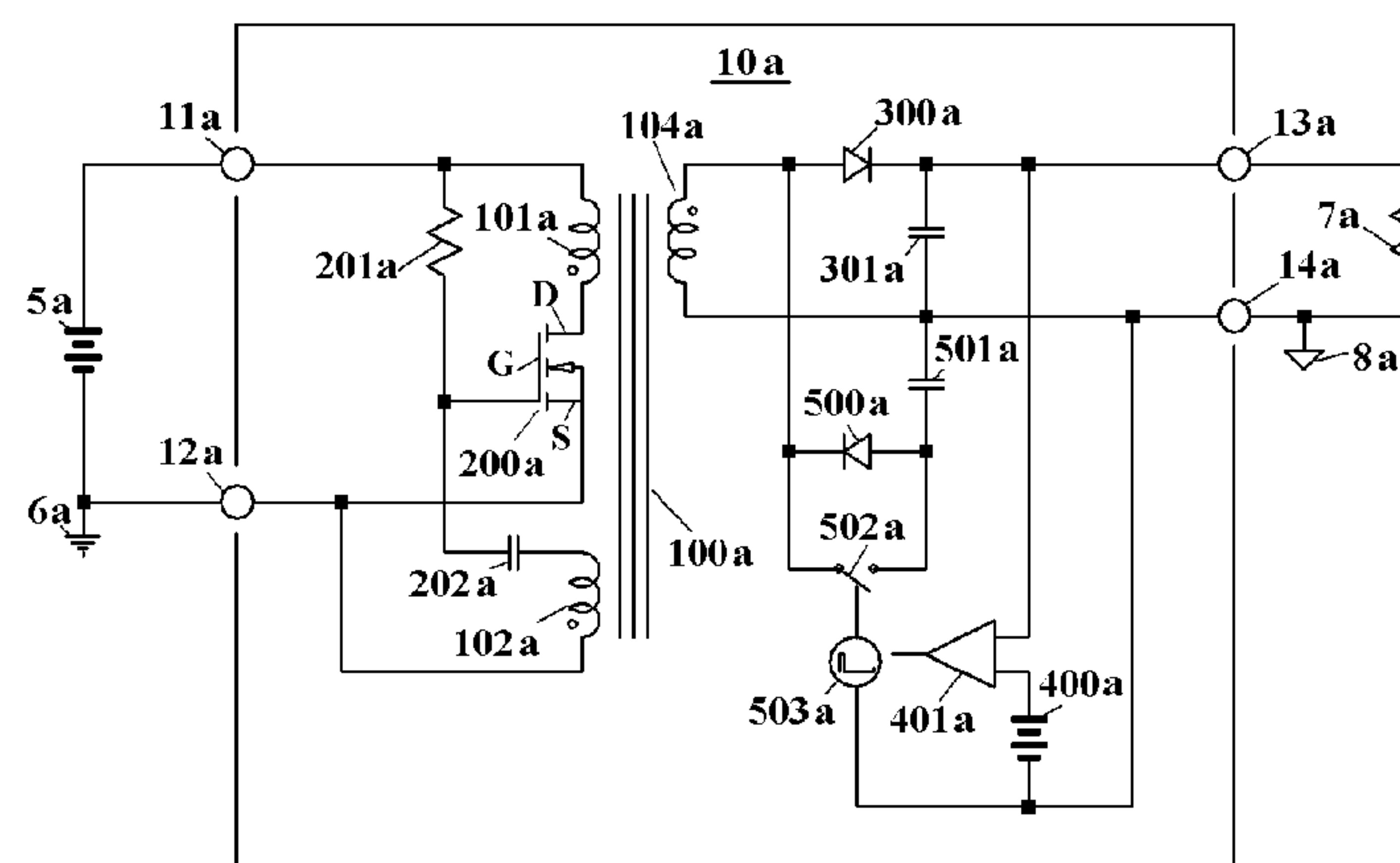
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(57) **ABSTRACT**

The present invention provides a switched-mode power converter with regulation demand pulses sent across a galvanic isolation barrier.

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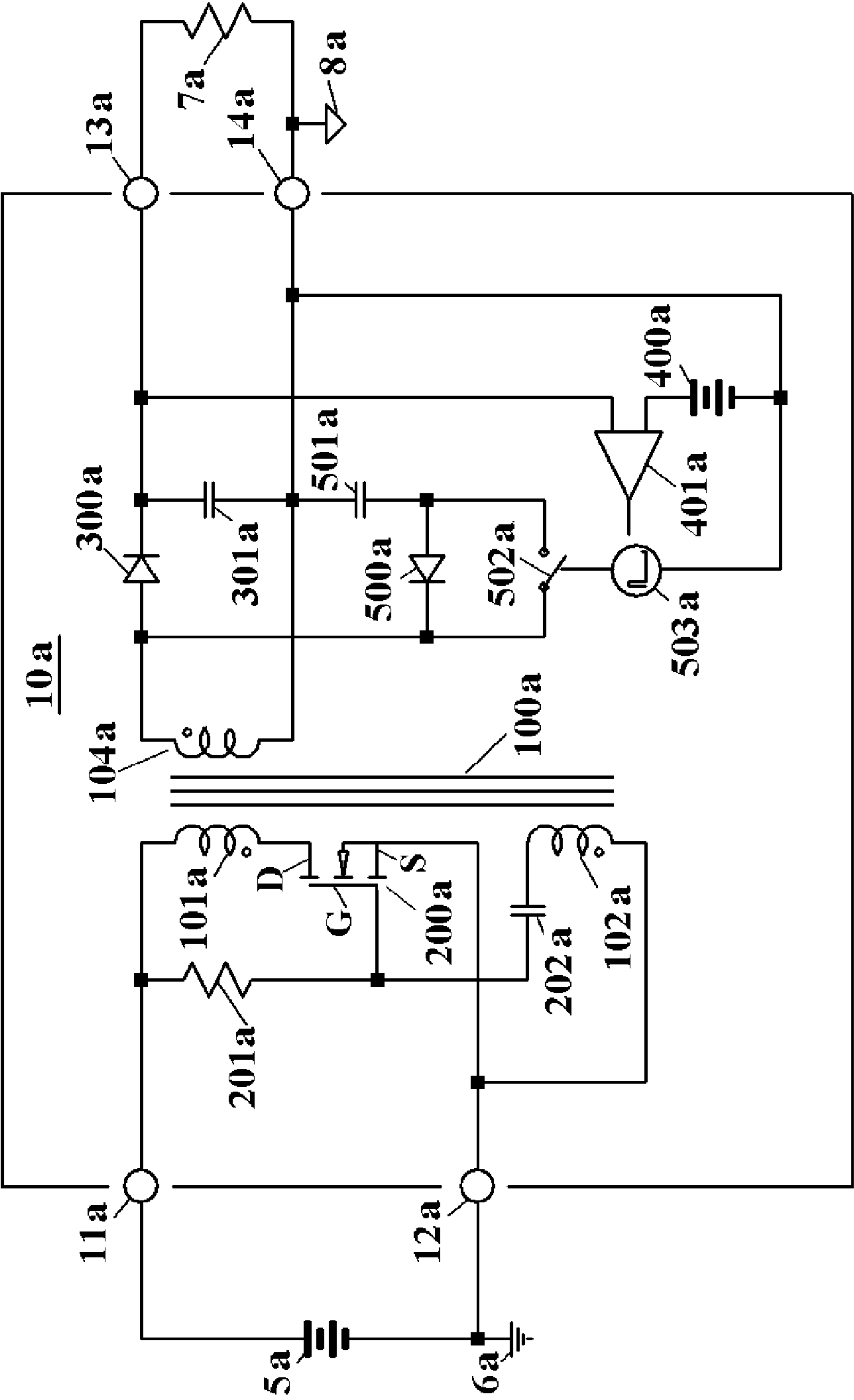


Fig. 1

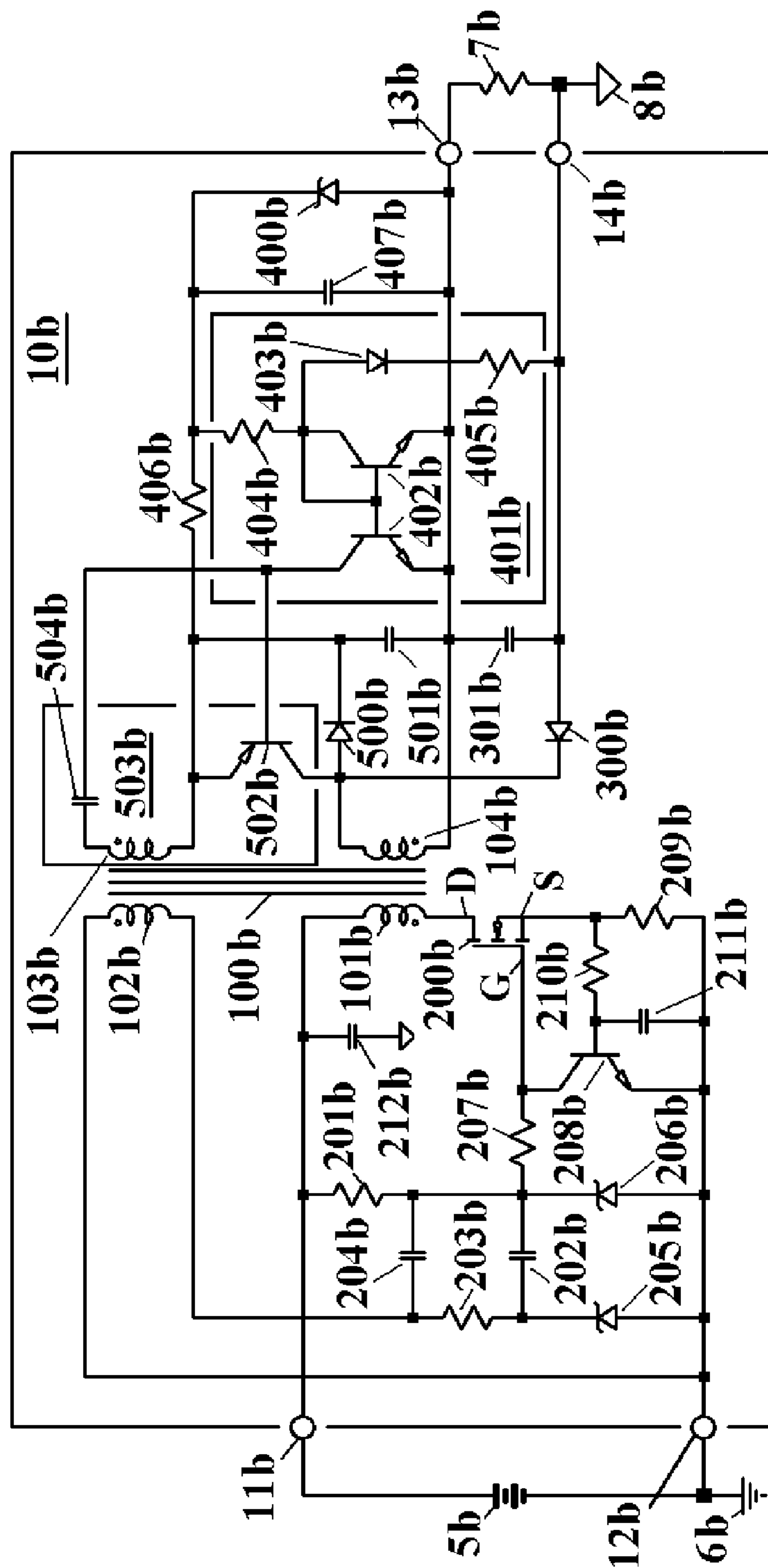


Fig. 2

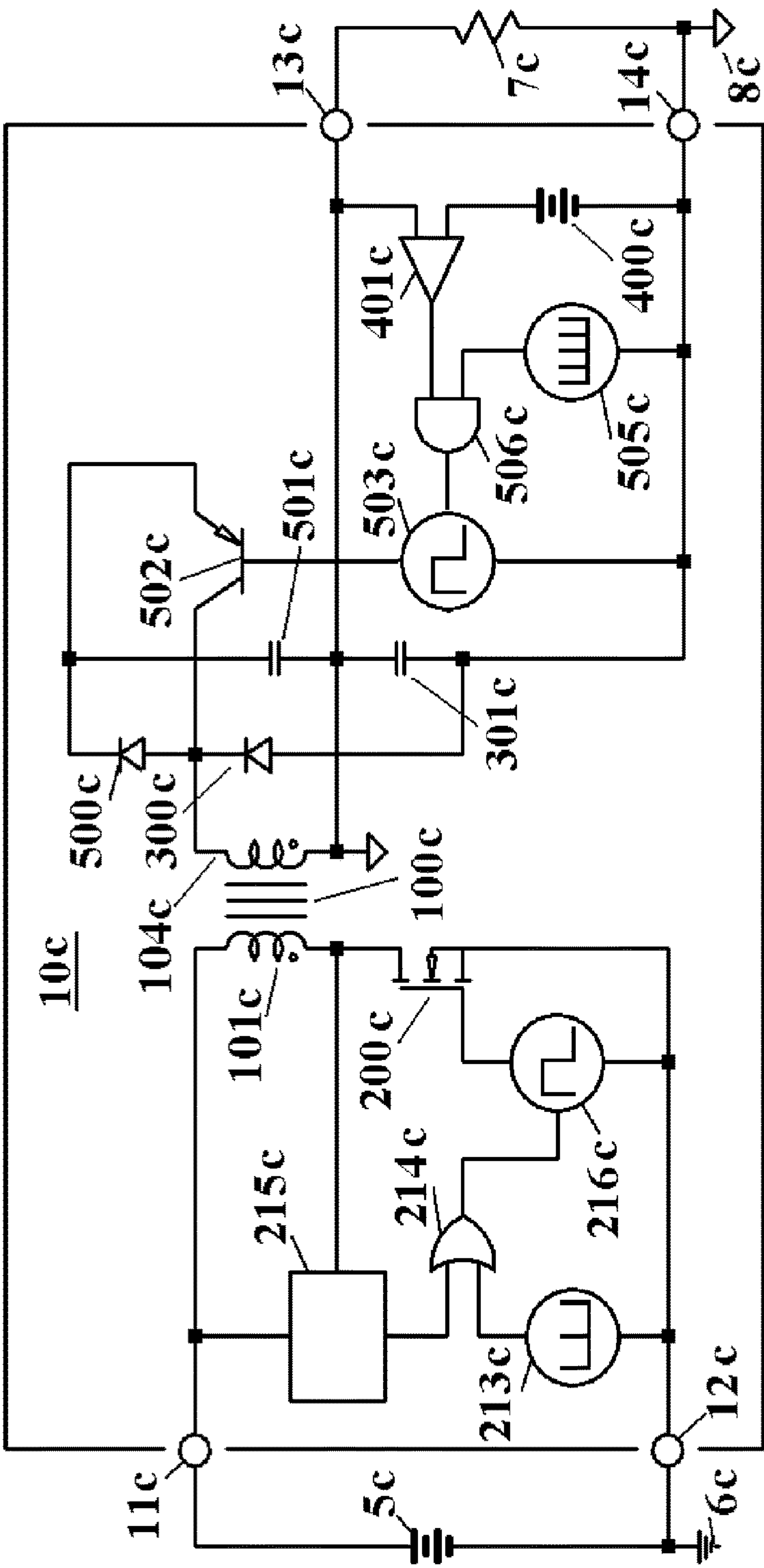


Fig. 3

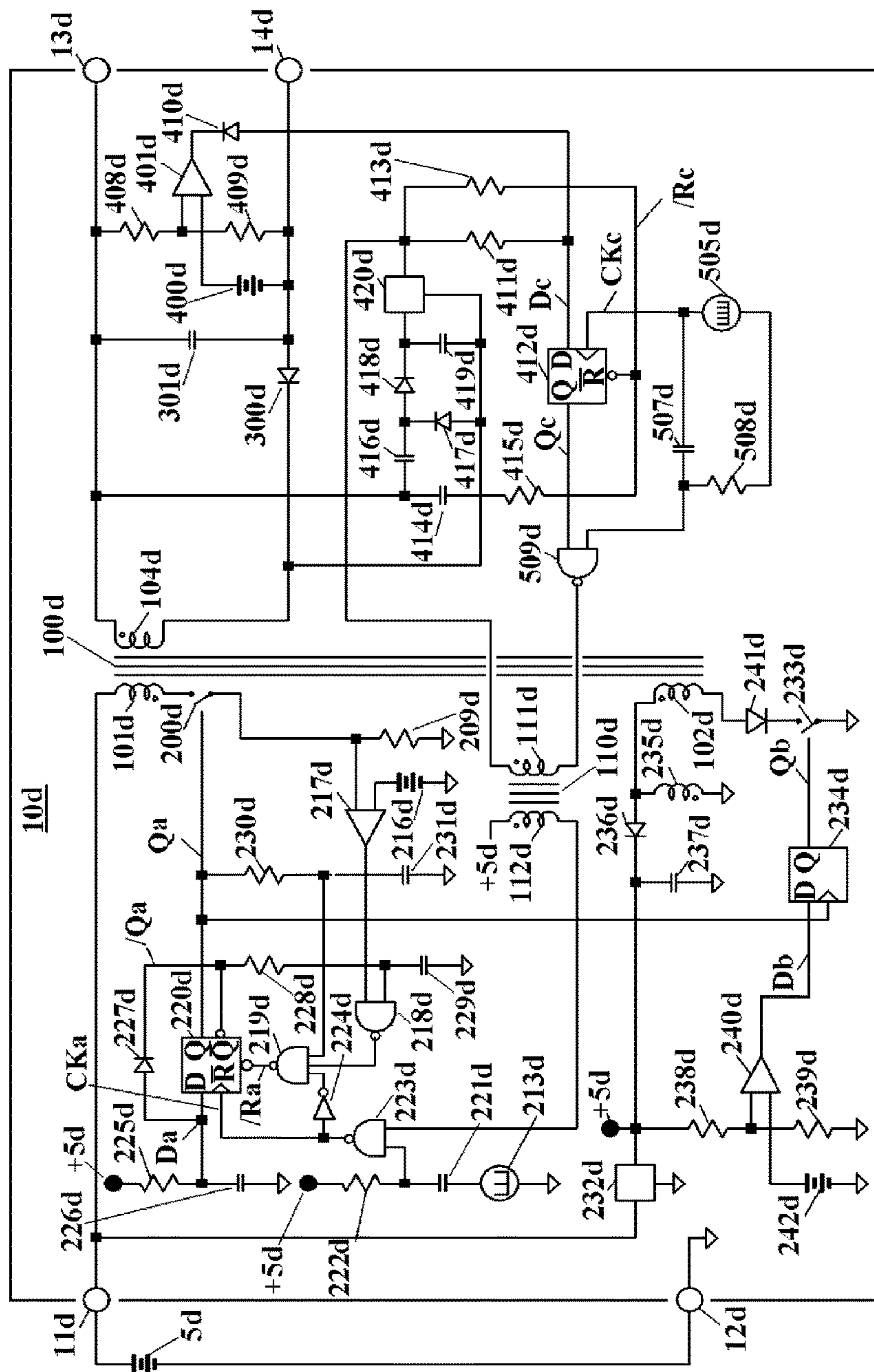


Fig. 4

POWER CONVERTER WITH DEMAND PULSE ISOLATION

Matter enclosed in heavy brackets [] appears in the original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue; a claim printed with strikethrough indicates that the claim was canceled, disclaimed, or held invalid by a prior post-patent action or proceeding.

CROSS-REFERENCE TO RELATED APPLICATIONS

[This application] *Notice: The following multiple reissue applications have been filed for the reissue of U.S. Pat. No. 9,071,152: (1) reissue application Ser. No. 15/090,929, filed on Apr. 5, 2016 and reissued as U.S. Reissue Pat. No. RE47,031; (2) reissue application Ser. No. 15/168,998, filed on May 31, 2016, which is a reissue continuation of Ser. No. 15/090,929; (3) reissue application Ser. No. 15/202,746 (the present application), filed on Jul. 6, 2016, which is a reissue continuation of Ser. No. 15/090,929; (4) reissue application Ser. No. 16/547,850, filed on Aug. 22, 2019, which is a reissue continuation of Ser. No. 15/202,746; and (5) reissue application Ser. No. 16/548,897, filed on Aug. 23, 2019, which is a reissue continuation of Ser. No. 15/202,746. U.S. Pat. No. 9,071,152 claims the benefit of the filing dates of U.S. provisional application Nos. 61/667,473, filed on Jul. 03, 2012, and 61/727,795, filed on Nov. 19, 2012, the teachings of both of which are incorporated herein by reference in their entirety.*

BACKGROUND

1. Field of the Invention

The present invention relates to electronics and, more specifically but not exclusively, to switched-mode power converters.

2. Description of the Related Art

This section introduces aspects that may help facilitate a better understanding of the invention. Accordingly, the statements of this section are to be read in this light and are not to be understood as admissions about what is prior art or what is not prior art.

Switched-mode DC-DC power converters, often powered by rectified DC from AC mains, are ubiquitous as plug-in adapters used to power a plethora of electronic devices.

A typical such converter is copiously documented in the Power Integrations Design example report DER-227. Such converters are also taught in U.S. Pat. No. 4,459,651 and U.S. Patent Application Publication Nos. 2011/0026277 A1 and 2011/0018590 A1. Such converters typically generate commutation pulses on the mains side of galvanic isolation circuitry.

Some known converters use forms of absorption modulation to convey feedback information through the power transformer. In U.S. Pat. No. 8,000,115, a temporary decrease in the loading of a transformer secondary winding during a flyback pulse generates a corresponding voltage disruption of the same pulse, which disruption is detected on another transformer winding to effect primary-winding-side converter control. In U.S. Pat. No. 5,973,945, a similar method is taught, but instead of unloading a flyback pulse, temporary loading of a forward power pulse is taught. The circuitry for extracting the resulting information-bearing

current disruption in the transformer primary circuit is quite involved. A similar absorption modulator is taught in U.S. Pat. No. 4,996,638.

Converters are also known wherein an analog voltage reflection of the converter output voltage seen on a primary-side winding is processed to generate a primary-side analog feedback signal which is used to control the commutating signals applied to the commutating switch to regulate converter output on its secondary side. Such feedback methods are taught in U.S. Pat. Nos. 4,597,036 and 3,889,173. Such methods are becoming less common due to the difficulty of reliably processing the analog information reflected into a primary-side winding to obtain an accurate feedback signal.

U.S. Pat. No. 4,937,727 teaches a mains-side pulse generator that is pulse-width controlled by a voltage-responsive clamp on the output side of a galvanic isolation barrier.

BRIEF DESCRIPTION OF THE DRAWINGS

Other embodiments of the invention will become more fully apparent from the following detailed description, the appended claims, and the accompanying drawings in which like reference numerals identify similar or identical elements.

FIG. 1 shows a schematic diagram of a power converter according to an embodiment of the present invention using a blocking oscillator.

FIG. 2 shows a schematic diagram of a power converter according to another embodiment of the present invention using a blocking oscillator.

FIG. 3 shows a schematic diagram of a power converter according to an embodiment of the present invention using a simple transformer.

FIG. 4 shows a schematic diagram of a power converter according to an embodiment of the present invention using a separate pulse transformer.

DETAILED DESCRIPTION

FIG. 1 shows a schematic diagram of a power converter 10a. A DC voltage source 5a, external to this converter, which may be derived from AC mains, may be connected to an earth ground 6a. Terminals 11a and 12a constitute a power input port that places source 5a in circuit with a primary winding 101a of a transformer 100a and with a commutating switch 200a, which is usually a MOSFET but may be a BJT or any other suitable electronic switch. For the diagrammed embodiment, switch 200a is a MOSFET having a source S, a gate G, and a drain D. Transformer 100a also comprises a regeneration winding 102a which is referenced to source S of MOSFET 200a, is connected through a capacitor 202a to gate G of MOSFET 200a, and is poled to provide regenerative feedback to gate G of MOSFET 200a. Connected between terminal 11a and gate G of MOSFET 200a is a resistor 201a which charges capacitor 202a to enhance MOSFET 200a at a slow pulse rate. Thus, MOSFET 200a, transformer 100a, capacitor 202a, and resistor 201a form an input-side blocking oscillator which acts as a driver circuit toggling ON and OFF MOSFET 200a.

Transformer 100a also comprises a secondary winding 104a which may be connected to a floating common terminal 14a. A diode 300a and a capacitor 301a form a rectifier circuit to rectify and filter voltage pulses from winding 104a to supply power through a power output port comprising terminals 13a and 14a to an external load represented by resistor 7a connected in circuit therewith, one end of which may be referred to a floating common 8a. The power input

port 11a/12a and the power output port 13a/14a may be galvanically isolated from each other.

Flyback pulses of transformer 100a occur when MOSFET 200a ceases conduction, i.e., turns OFF. Winding 104a is poled to cause diode 300a to rectify only these flyback pulses.

Forward pulses, of opposite polarity to the flyback pulses, occur while MOSFET 200a is ON. Another diode 500a, poled to rectify forward pulses, and another capacitor 501a form an auxiliary rectifier circuit to rectify and filter forward pulses from winding 104a, and to store energy for triggering the input-side blocking oscillator formed by MOSFET 200a, transformer 100a, capacitor 202a, and resistor 201a. Resistor 201a is made sufficiently large to set a low free-running frequency of the blocking oscillator, perhaps 1 KHz or less, to minimize power consumption. Nevertheless, the miniscule power thus provided suffices to charge capacitor 501a to a voltage related, through the turns ratio of transformer 100a, to the voltage at the power input port, even with the power output port short-circuited.

This magnetically-coupled blocking oscillator may be triggered through any transformer winding magnetically coupled thereto. Therefore, just as MOSFET 200a may be turned ON through winding 102a, it may as easily be triggered through winding 104a. To trigger thusly, diode 500a is briefly short-circuited by a switch 502a which is driven by a demand pulse generator 503a to source a pulse of energy from capacitor 501a into transformer 100a. When this is done, the voltage at the cathode of diode 500a falls rapidly to the voltage on its anode, also being the voltage across capacitor 501a. Since winding 104a is coupled to winding 101a, the voltage on drain D of MOSFET 200a also rapidly falls from near the voltage on terminal 11a to near the voltage on terminal 12a. Since winding 102a is also magnetically coupled, the voltage at its node shared with capacitor 202a abruptly rises, turning ON MOSFET 200a. This triggering action occurs in a few tens of nanoseconds. Until regeneration is established in MOSFET 200a through winding 102a, triggering energy is supplied by capacitor 501a of the auxiliary rectifier circuit. However, once regeneration is established in MOSFET 200a, capacitor 501a is charged for the duration of the ON time of MOSFET 200a, fully replacing any energy lost during triggering. The demand pulse generator 503a may be used to adjust the commutation frequency of the converter 10a to cause its output to attain a desired value, as will be described below.

It is important to understand certain important advantages of this embodiment. Firstly, this embodiment allows minimal, simple, and robust circuitry to be galvanically associated with the power input port where high voltages and mains transients may be expected. According to this embodiment, more complex and vulnerable regulation circuitry may be galvanically associated with the power output port where voltages are often lower and protection is more easily implemented. Secondly, the control of a flyback converter that may cross from the discontinuous conduction mode (DCM), through the critical conduction mode, to the continuous conduction mode (CCM), is well known to be problematic. This embodiment simply avoids that problem. In the embodiment shown in FIG. 1, transformer 100a is used during the conduction of MOSFET 200a as a forward converter supplying the auxiliary rectifier circuit, and during the flyback of transformer 100a as a flyback converter supplying power to the power output port. During these cycle portions, it is difficult and impractical to re-trigger the blocking oscillator through transformer 100a to generate another energy-bearing cycle. Once the flyback pulse has

reset the inductance of transformer 100a, i.e., has depleted energy from its magnetic field, transformer 100a is free, until the next ON time of MOSFET 200a, to be used as a magnetically coupled isolator to convey trigger information between its windings. In FIG. 1, the information thus conveyed is a pulse from pulse generator 503a which, responsive to the output of comparator 401a, indicates the need for another energy-bearing cycle, and moreover re-triggers the blocking oscillator to provide that energy-bearing cycle. Since it is difficult or impractical to re-trigger until transformer 100a energy has been depleted, this converter will, if driven as hard as possible, approach critical conduction, but refuse to enter the critical conduction mode.

This converter may be fitted with a reference voltage 400a and a comparison circuit 401a. When the voltage at terminal 13a falls below the comparison voltage, comparison circuit 401a causes pulse generator circuit 503a to pulse, turning ON switch 502a, triggering an energy-bearing ON cycle of the blocking oscillator, and charging capacitor 301a. As load 7a drains capacitor 301a, terminal 13a voltage repeatedly falls to the voltage of reference 400a, causing comparison circuit 401a to initiate energy-bearing ON cycles. An interesting property of this embodiment is that the bottom of its output ripple corresponds to the voltage of reference 400a, and the amplitude of its ripple decreases with increased current in load 7a.

FIG. 2 shows a schematic diagram of a power converter 10b. As in converter 10a of FIG. 1 above, converter 10b is powered, through terminals 11b and 12b, from an external source 5b, that may be referred to earth ground 6b. Power from converter 10b flows through terminals 13b and 14b through a load 7b, which may be referred to a floating common 8b. A MOSFET 200b, preferably ON Semiconductor type NDD02N60, forms an input-side blocking oscillator with a (preferably 1 nF) capacitor 202b, a (preferably 66 megohm) resistor 201b, and a transformer 100b. Transformer 100b comprises a winding 101b, preferably about 250 uH, and windings 102b and 104b, preferably about 3.09 uH each, and a winding 103b, preferably about 193 nH, which may be a single turn. A capacitor 212b provides a short local circuit for high frequency currents and preferably comprises a 4.7 uF capacitor and a 100 nF capacitor (neither explicitly shown) in parallel. A resistor 210b, preferably about 180 ohms, and a capacitor 211b, preferably about 10 pF, filter out capacitive spikes generated by fast transitions of MOSFET 200b. When MOSFET 200b is turned on, the current therein rises, but is limited by a transistor 208b, the base of which is driven by a voltage across a resistor 209b, which voltage is responsive to current through MOSFET 200b. When MOSFET 200b current reaches about 250 mA, transistor 208b shunts current at gate G of MOSFET 200b to ground, limiting gate G voltage to prevent further current rise. With current rise prevented, the voltages across the windings of transformer 100b collapse. Thus, a regenerative turn-OFF of MOSFET 200b begins, and the voltage at its drain D flies positive past the voltage on terminal 11b until the energy in its magnetic field finds a current path through one of its windings. A corresponding negative voltage occurs at the shared node of winding 102b and a capacitor 204b, preferably about 100 pF, which immediately couples through a resistor 207b, preferably about 47 ohms, vigorously turning off MOSFET 200b. Within a few nanoseconds, the same transition couples through a resistor 203b, preferably about 1K, and a capacitor 202b, preferably about 1 nF, to join the signal passing through capacitor 204b, to reinforce the OFF transition at gate G of MOSFET 200b. Both the OFF and ON transitions at gate G of MOSFET 200b are

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regenerative and follow the path just described. To prevent damage to MOSFET **200b**, its gate voltage should be limited. Resistor **203b** and a diode **205b**, preferably an 8.2 volt zener, form an L-network to limit that voltage. Since the voltage at the cathode of diode **205b** is capacitively coupled to resistor **207b**, and resistor **201b** is pulling up on resistor **207b**, the gate G voltage of MOSFET **200b** would be free to rise, turn ON MOSFET **200b** continually, and perhaps damage its gate, if means for limiting gate voltage were not provided. Another zener diode **206b**, preferably the zenered base-emitter junction of an NXP type PMBT 3904, is used to limit the gate voltage rise. This device is used because, at high temperature, excess leakage of diode **205b** would shunt to ground the current of resistor **201b**, preventing the blocking oscillator from starting. Most of the current from winding **102b**, being too great for diode **206b** to conduct without damage, flows in diode **205b**.

As in FIG. 1, when the voltage at the node of winding **104b** and a diode **300b**, preferably type 1N4148, flies back, the energy in transformer **100b** is dumped into a capacitor **301b**, preferably 4.7 uF, ultimately to be consumed by load **7b**. As in FIG. 1, a diode **500b**, preferably type 1N4148, and a capacitor **501b**, preferably 220 nF, form a forward converter to supply an auxiliary voltage.

Please note that, in this embodiment, the poling of winding **104b**, diode **300b**, and diode **500b** are reversed, and the output polarity is reversed, with respect to FIG. 1. This reversal illustrates that this embodiment will function with either poling, and that polarity is of little practical concern in an isolated supply. The rectifiers and windings are so poled that the auxiliary supply forms a forward converter, and the output forms a flyback converter with the remaining circuitry. A switch **502b** is, in this embodiment, a PNP transistor, preferably type MMBT 3906. This switch also coacts with another winding **103b** of transformer **100b**, which may be a single turn, and a capacitor **504b**, to form an output-side triggering blocking oscillator **503b** corresponding to pulse generator **503a** of FIG. 1, which triggering blocking oscillator is magnetically coupled through transformer **100b** to the above-described input-side, power-blocking oscillator comprising MOSFET **200b**. Thus, an input-side, master blocking oscillator comprising MOSFET **200b** and an output-side, slave blocking oscillator comprising switch **502b** are magnetically coupled to each other through transformer **100b**. The auxiliary voltage of capacitor **501b** flows through a resistor **406b**, preferably 27K, to feed another zener diode **400b**, preferably another zenered PMBT3904, corresponding to reference **400a** of FIG. 1. A capacitor **407b**, preferably 100 nF, bypasses diode **400b** at high frequencies. A dual transistor **402b**, preferably NXP type BS846, is connected as a current mirror, and mirrors the current in a resistor **404b**, the latter current being set by the reference voltage of diode **400b**. This current sets the free running oscillation frequency of blocking oscillator/pulse generator **503b**. Since the transformer **100b** current flowing in MOSFET **200b** is set by transistor **208b**, the per-cycle energy in transformer **100b** is quantized. Setting the current in resistor **404b**, preferably 100K, therefore sets a maximum frequency of blocking oscillator/demand-pulse generator **503b**, thereby setting the maximum frequency for these energy-quantized cycles, thus limiting maximum converter power, even in the event of an output short-circuit. A diode **403b**, preferably type 1N4148, compensates the base-emitter voltage of dual-transistor **402b**. Dual transistor **402b**, resistor **404b**, diode **403b**, and a resistor **405b** form a current comparator corresponding to comparator **401a** of FIG. 1. Resistor **405b**, preferably about 82K for a 5V output, pro-

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vides feedback by robbing resistor **404b** current from the current mirror of dual-transistor **402b** as output voltage increases, thus setting operating frequency roughly in proportion to the demand of load **7b**.

FIG. 3 shows a schematic diagram of a power converter **10c** arranged to use a simple, two-winding transformer. The function of converter **10c** closely parallels that of converters **10a** and **10b** of FIGS. 1 and 2, save that components have been added to replace the functions of regenerative (tickler) windings needed by blocking oscillators. As in the previous figures, a source **5c** may be referenced to an earth ground **6c**, and load **7c** may be referenced to a floating common **8c**. As in FIG. 1, a transformer **100c** primary winding **101c** is in circuit with a switch **200c** and terminals **11c** and **12c**. As in FIG. 1, flyback pulses on a secondary winding **104c** of transformer **100c** charge a capacitor **301c** through a diode **300c** to supply energy to the load **7c** through terminals **13c** and **14c**. As in FIG. 1, forward pulses on the secondary winding of transformer **100c** charge a capacitor **501c** through a diode **500c**. As in FIG. 1, a comparison circuit **401c** compares the voltage on the output terminal **13c** with a reference **400c**. As in FIG. 1, a switch **502c** is driven by a demand pulse generator **503c**.

We now depart from the FIGS. 1 and 2 function. A fast oscillator **505c**, preferably about 100 KHz, drives an AND gate **506c** which is also driven by comparison circuit **401c**. If the voltage between terminals **13c** and **14c** is smaller than that of reference **400c**, gate **506c** passes oscillator **505c** pulses to trigger pulse generator **503c**, which initiates, through transformer **100c** additional energy-bearing pulses by eventually driving switch **200c**, as described below. If, however, the output voltage is adequate, then gate **506c** does not pass oscillator **505c** pulses.

The pulses of energy from capacitor **501c** sourced to transformer **100c**, [though] through a switch **502c**, during the pulse of generator **503c**, under the command of gate **506c**, appear as voltage pulses across the primary winding of transformer **100c**. These pulses are detected and processed to logic levels by a demand pulse detector **215c** and passed through an OR gate **214c** to a pulse generator that turns ON switch **200c** to energize transformer **100c** to begin an energy-bearing cycle. When switch **200c** turns OFF, the subsequent flyback pulse charges capacitor **301c** through diode **300c**, as previously described. Since capacitor **501c** is charged from the converter forward pulse, its voltage persists even in the presence of a short-circuit load, allowing the converter to recover once the short-circuit is removed.

Had no energy-bearing cycle ever occurred, there might be insufficient, or no, charge in capacitor **501c** to be used to initiate energy-bearing cycles as described above. Therefore, a slow pulse oscillator **213c**, preferably about 1 KHz, is also connected to gate **214c**, through which it initiates energy-bearing cycles by triggering a pulse generator **216c**, thus turning on switch **200c**. These infrequent pulses cause energy-bearing cycles that are sufficient to charge capacitor **501c**, which also may supply power to generator **503c**, gate **506c**, oscillator **505c**, reference **400c**, and comparison circuit **401c**. Of course, slow oscillator **213c** must somehow be powered along with gate **214c** and pulse generator **216c**. A bias supply (not shown but well known in the art) powered from terminals **11c** and **12c**, may be used to power these components of the circuit.

FIG. 4 shows a schematic diagram of a power converter **10d**, comprising a separate transformer **110d** to transmit demand pulses across a galvanic isolation barrier. As in FIG. 1 above, converter **10d** is powered, through terminals **11d**

and 12d, from an external source 5d, and power output from converter 10d flows through terminals 13d and 14d.

Input voltage from terminals 11d and 12d powers a slow oscillator 213d, preferably of less than 1 KHz frequency, and a start-up regulator 232d which, through a supply node +5d, 5 initially powers, with a voltage preferably about 4V, logic and drive circuitry described below. Each label "+5d" in FIG. 4 refers to a supply node that is initially about 4 volts when the input-side logic is starting to function and about 5 volts when in regulation. A capacitor 221d and a resistor 222d differentiate transitions of a slow pulse oscillator 213d to provide pulses of about 200 nS duration. These pulses pass [though] through a NAND gate 223d to clock a D-type flip-flop 220d through a node CKa. 10

Responsive to its clock pulse, flip-flop 220d turns ON a switch 200d, preferably a MOSFET, ON Semiconductor type NDD02N60, which is in circuit with a primary winding 101d of a transformer 100d, with a sense resistor 209d, and with terminals 11d and 12d. Current then flows in this circuit, and the voltage of source 5d is impressed upon 20 primary winding 101d. According to the turns-ratio between primary winding 101d and a secondary winding 104d of transformer 100d, a voltage appears across winding 104d. This latter voltage charges a capacitor 416d through a diode 417d.

As current in resistor 209d rises, a voltage is applied to an input of a comparator 217d, which voltage is compared with a reference 216d, also connected to an input of comparator 217d. When current in resistor 209d exceeds a value set by reference 216d, comparator 217d issues a reset signal which propagates through NAND gates 218d and 219d to a node /Ra where the reset signal resets flip-flop 220d, turning OFF switch 200d. 30

When switch 200d is turned ON, unavoidable gate-to-source capacitance of MOSFET switch 200d causes a current spike in resistor 209d. To prevent comparator 217d from prematurely resetting flip-flop 220d responsive to this spike, the rise of node Qa charges a capacitor 231d through a resistor 230d to reach the threshold of a gate 219d in about 75 nS, prior to which the low voltage of capacitor 231d 40 inhibits gate 219d from resetting flip-flop 220d.

Prior to its rise, node Qa has been low, and a complementary node/Qa has been high. When node Qa rises, node/Qa falls, discharging a capacitor 229d through a resistor 228d to the threshold of NAND gate 218d in about 2 uS, and [though] through NAND gate 219d resetting flip-flop 220d, thus limiting the maximum ON time of switch 200d, should comparator 217d fail to reset flip-flop 220d. 45

In addition to limiting ON times of switch 200d, it is desirable to limit maximum frequency of these ON times. To this end, the voltage across a capacitor 226d is charged to a logic high through a resistor 225d and applied to a node Da, the D-input of flip-flop 220d. When node/Qa falls, capacitor 226d is discharged through a diode 227d, slowly to be recharged through resistor 225d. Until the capacitor 226d 55 voltage is recharged to the D-input threshold voltage, flip-flop 220d is inhibited from turning ON switch 200d.

When switch 200d is turned OFF, the energy in the magnetic field of transformer 100d generates flyback voltage across its windings. Flyback voltage of winding 104d is rectified by a diode 300d and begins to charge a filter capacitor 301d to begin to supply output voltage to terminals 13d and 14d. This flyback voltage also raises the voltage on capacitor 416d, causing diode 417d to turn OFF and a diode 418d to turn ON, charging a capacitor 419d. Voltage across 60 capacitor 419d supplies an auxiliary regulator 420d, which in turn powers a fast oscillator 505d, preferably of about 60

KHz frequency. Regulator 420d also powers logic and drive circuitry on the winding 104d side of the power converter.

The ON pulses of switch 200d responsive to oscillator 213d are sufficiently frequent to start the converter of this embodiment, but insufficiently frequent to drive it to full output. To initiate more frequent pulses, an oscillator 505d drives a capacitor 507d and a resistor 508d to supply differentiated pulses of about 100 nS width to a NAND gate 509d, which in turn drives a primary winding 111d of demand pulse transformer 110d, thus producing demand pulses across a secondary winding 112d thereof. These winding 112d pulses are conveyed through a NAND gate 223d to clock flip-flop 220d at up to the frequency of oscillator 505d.

If all of the pulses of oscillator 505d were allowed to clock flip-flop 220d, under some conditions, the converter of this embodiment would produce excess output. To regulate this output, a flip-flop 412d is used to gate the pulses passed by NAND gate 509d. At a node CKc, oscillator 505d clocks 20 a flip-flop 412d, which generates a logic high at a node Qc only when a logic high is present at a node Dc at the rising edge of its clock. Thus, pulses driving transformer 110d are permitted responsive to a logic high only at node Dc.

It would be wasteful of power to drive winding 111d for the full duration of the differentiated pulse at resistor 508d. Therefore, when switch 200d turns ON causing a negative transition at the dotted end of winding 101d, a corresponding negative transition appears at the dotted end of winding 104d. This transition is coupled through a small capacitor 414d, preferably about 10 pF, through a current-limiting resistor 415d to a node/Rc, the reset input of flip-flop 412d, which is normally held high by a resistor 413d. Thus, once the turning ON of switch 200d has propagated through transformer 100d, flip-flop 412d is reset, usually in less than 35 20 nS.

Node Dc is usually held at a logic high by a resistor 411d, thus enabling pulses gated by flip-flop 412d. However, between terminals 13d and 14d is disposed a voltage divider comprising resistors 408d and 409d, the voltage at the junction of which is applied to an input of a comparator 401d. Should the voltage at that junction exceed the voltage of a reference 400d, also applied to a comparator 401d input, an output of comparator 401d will drop to a logic low, drawing current through a diode 410d, thus presenting a logic low at node Dc and, after clocking, responsively at node Qc, inhibiting pulses through gate 509d that would otherwise turn ON switch 200d. Thus, the voltage between terminals 13d and 14d is regulated responsive to the voltage of reference 400d. 45

Since the voltage between terminals 11d and 12d may be high, perhaps 375V, and the desired regulated voltage at node +5d is typically 5V, it might be inefficient to obtain the power to supply the logic and drive circuitry associated with winding 101d from regulator 232d. Therefore, transformer 100d is fitted with an auxiliary winding 102d, which is connected in circuit with an inductor 235d, a diode 241d, and a switch 233d, preferably a MOSFET. While switch 200d is ON, current flows in this circuit. When switch 200d turns OFF, diode 241d also turns OFF and energy in inductor 235d generates a positive flyback voltage, causing current through a diode 236d to charge a filter capacitor 237d, raising the voltage of node +5d. As node +5d approaches 5V, regulator 232d ceases to supply energy to node +5d, but continues to power a voltage reference 242d, which drives 60 an input of a comparator 240d. Should the voltage of node +5d exceed 5V, the voltage at the junction of resistors 238d and 239d, connected to another input of comparator 240d,

will exceed that of reference **242d**, causing the output of comparator **240d** at node **Db** to drop to a logic low.

A flip-flop **234d** drives node **Qb** to turn ON switch **233d** responsive to clock pulses on node **Qa**, and to a logic high being present at node **Db**. When node **Db** drops to a logic low, node **Qb** follows it upon the next clock, and switch **233d** turns OFF. In this state, inductor **235d** no longer receives energy and no longer charges capacitor **237d** through diode **236d**. Thus, node **+5d** is regulated to approximately 5V, and the energy supplying node **+5d** is provided efficiently through transformer **100d**.

In one embodiment, the invention is a switched-mode power-converter comprising a power input port, a transformer comprising windings, a commutating switch connected in circuit with the input port and a winding of the transformer, a driver circuit for toggling the commutating switch, a power output port, a rectifier circuit for supplying power to the power output port, a reference voltage or current source, a comparison circuit for comparing the voltage or current at the power output port with the reference voltage or current, and a demand pulse source circuit coupled to the transformer for transmitting galvanically isolated trigger information through the transformer to the driver circuit responsive to the comparison circuit.

The converter may comprise as its driver circuit a blocking oscillator comprising the converter transformer. The converter may further comprise an input-side, master blocking oscillator for power conversion and an output-side, slave blocking oscillator for generating demand pulses. Both blocking oscillators may be mutually coupled through the converter power transformer or may drive separate transformers.

The converter may comprise inductive, capacitive, opto-coupled, or piezoelectric galvanic isolation circuitry to transmit demand pulses across the galvanic isolation barrier.

The converter may have one or more output rectifier circuits poled to rectify flyback pulses of its transformer.

The converter may comprise one or more auxiliary rectifier circuits which may be poled as forward converters.

The converter may be powered by a rectifier circuit to provide an AC/DC converter.

It should be understood that replicas of pulses generated and applied to one winding of the power transformer appear, suitably modified by turns-ratio, across all other windings of the power transformer.

Though blocking oscillators usually require tickler windings, single output embodiments of this invention may comprise a power transformer with as few as two, and in excess of five windings, with multiple output embodiments possibly comprising yet more windings.

Startup pulse generation circuitry resides on the powered side of the isolation barrier, though its pulses appear on both sides of the isolation barrier. This circuitry may comprise a blocking oscillator, another form of oscillator with drive circuitry to turn ON the commutating switch, or this circuitry may comprise an external source of pulses.

Demand pulse generator circuitry resides with the output port to be regulated, though its pulses appear on both sides of the isolation barrier. This circuitry may comprise a slave blocking oscillator, another form of oscillator with drive circuitry to turn ON the demand pulse generator switch, or may be externally applied.

Demand pulses may be generated to regulate the power converter to provide either a desired output voltage or a desired output current responsive to the voltage across or a current through an output port.

Between the commencement of start-up and the attainment of regulation, a pulse generator sources pulses to turn ON the commutating switch. This pulse generator may be the same generator that sources regulation pulses, or may be a separate pulse generator.

Each internal pulse generator is powered. The startup pulse generator is powered from the input port. The demand pulse generator is only indirectly powered from the input port by DC-DC power conversion through the power transformer and one or more rectifiers and filters powering the power output port with which the generator is associated.

Power for pulse generation circuitry may be rectified from either forward pulses, from flyback pulses, or both, appearing across one or more power transformer windings. Rectification of forward pulses helps to assure startup.

Windings, switches, and diodes may be poled to provide either polarity of input, and either polarity of output.

In each of the embodiments of FIGS. 1-4, galvanic isolation circuitry transfers (i) power from the input-port side to the output-port side of the power converter and (ii) demand pulses from the output-port side to the input-port side. In particular, in FIG. 1, the galvanic isolation circuitry consists of transformer **100a**, which transfers (i) power from winding **101a** to winding **104a** and (ii) demand pulses from winding **104a** to winding **102a**. In FIG. 2, the galvanic isolation circuitry consists of transformer **100b**, which transfers (i) power from winding **101b** to winding **104b** and (ii) demand pulses from winding **104b** to winding **102b**. In FIG. 3, the galvanic isolation circuitry consists of transformer **100c**, which transfers (i) power from winding **101c** to winding **104c** and (ii) demand pulses from winding **104c** to winding **101c**. In FIG. 4, the galvanic isolation circuitry consists of (i) transformer **100d**, which transfers power from winding **101d** to winding **104d** and (ii) transformer **110d**, which transfers demand pulses from winding **111d** to winding **112d**. Winding **102d** generates the bias supply for powering the **+5d** node.

In each of the embodiments of FIGS. 1-4, a demand pulse generator on the output-port side of the converter generates the demand pulses that are conveyed to the input-port side of the converter via the galvanic isolation circuitry. In FIGS. 1, 2, and 3, the demand pulse generator comprises elements **503a**, **503b**, and **503c**, respectively. In FIG. 4, the demand pulse generator comprises NAND Gate **509d** and flip-flop **412d**.

In each of the embodiments of FIGS. 1-4, slow-pulse source circuitry generates pulses on the input side of the power converter. In FIGS. 1 and 2, the slow-pulse source circuitry is the corresponding input-side blocking oscillator. In FIGS. 3 and 4, the slow-pulse source circuitry is slow oscillator **213c** and slow oscillator **213d**, respectively. Note that, depending on the particular implementation, the slow-pulse source circuitry may be implemented internal to or external to the switched-mode power converter. Similarly, depending on the particular implementation, fast oscillator **505c** and fast oscillator **505d** of FIGS. 3 and 4, respectively, may be implemented internal to or external to the switched-mode power converter.

Embodiments of the invention may be implemented as (analog, digital, or a hybrid of both analog and digital) circuit-based processes, including possible implementation as one or more integrated circuits (such as an ASIC or an FPGA), a multichip module, a single card, or a multichip circuit pack.

Also for purposes of this description, the terms "couple," "coupling," "coupled," "connect," "connecting," or "connected" refer to any manner known in the art or later

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developed in which energy or signals are allowed to be transferred between two or more elements, and the interposition of one or more additional elements is contemplated, although not required. Conversely, the terms “directly coupled,” “directly connected,” etc., imply the absence of such additional elements.

Also, for purposes of this disclosure, it is understood that all gates are powered from a fixed voltage power domain (or domains) and ground unless shown otherwise. Accordingly, all digital signals generally have voltages that range from approximately ground potential to that of one of the power domains and transition (slew) quickly. However and unless stated otherwise, ground may be considered a power source having a voltage of approximately zero volts, and a power source having any desired voltage may be substituted for ground. Therefore, all gates may be powered by at least two power sources, with the attendant digital signals therefrom having voltages that range between the approximate voltages of the power sources.

Signals and corresponding nodes or ports may be referred to by the same name and are interchangeable for purposes here.

Transistors are typically shown as single devices for illustrative purposes. However, it is understood by those with skill in the art that transistors will have various sizes (e.g., gate width and length) and characteristics (e.g., threshold voltage, gain, etc.) and may consist of multiple transistors coupled in parallel to get desired electrical characteristics from the combination. Further, the illustrated transistors may be composite transistors.

The terms “source,” “drain,” and “gate” should be understood to refer either to the source, drain, and gate of a MOSFET or to the emitter, collector, and base of a bipolar device when an embodiment of the invention is implemented using bi-polar transistor technology. Unless explicitly stated otherwise, each numerical value and range should be interpreted as being approximate as if the word “about” or “approximately” preceded the value of the value or range.

It will be further understood that various changes in the details, materials, and arrangements of the parts which have been described and illustrated in order to explain embodiments of this invention may be made by those skilled in the art without departing from embodiments of the invention encompassed by the following claims.

The use of figure numbers and/or figure reference labels in the claims is intended to identify one or more possible embodiments of the claimed subject matter in order to facilitate the interpretation of the claims. Such use is not to be construed as necessarily limiting the scope of those claims to the embodiments shown in the corresponding figures.

It should be understood that the steps of the exemplary methods set forth herein are not necessarily required to be performed in the order described, and the order of the steps of such methods should be understood to be merely exemplary. Likewise, additional steps may be included in such methods, and certain steps may be omitted or combined, in methods consistent with various embodiments of the invention.

Although the elements in the following method claims, if any, are recited in a particular sequence with corresponding labeling, unless the claim recitations otherwise imply a particular sequence for implementing some or all of those elements, those elements are not necessarily intended to be limited to being implemented in that particular sequence.

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Reference herein to “one embodiment” or “an embodiment” means that a particular feature, structure, or characteristic described in connection with the embodiment can be included in at least one embodiment of the invention. The appearances of the phrase “in one embodiment” in various places in the specification are not necessarily all referring to the same embodiment, nor are separate or alternative embodiments necessarily mutually exclusive of other embodiments. The same applies to the term “implementation.”

The embodiments covered by the claims in this application are limited to embodiments that (1) are enabled by this specification and (2) correspond to statutory subject matter. Non-enabled embodiments and embodiments that correspond to nonstatutory subject matter are explicitly disclaimed even if they fall within the scope of the claims.

What is claimed is:

[1. Apparatus configured to provide switched-mode power conversion, the apparatus comprising:

- an input port configured to receive input power;
- a switch configured to commutate the input power;
- galvanic isolation circuitry configured to provide galvanic isolation between the input port and an output port, wherein the galvanic isolation circuitry comprises a transformer comprising (i) a primary winding arranged in circuit with the input port and the switch and (ii) a secondary winding arranged in circuit with a rectifier and the output port, wherein the transformer is configured to transfer power from the input port to supply voltage or current to a load connected to the output port; and
- a demand pulse generator galvanically connected to the secondary winding and configured to generate demand pulses applied via the galvanic isolation circuitry to the switch to adjust a frequency of the commutation of the input power to supply a desired amount of voltage or current to the load.]

[2. The apparatus of claim 1, further comprising:

- a source configured to provide a reference signal; and
- comparison circuitry configured to compare the output port voltage or current to the reference signal wherein frequency of the demand pulses is responsive to the comparison between the output port voltage or current and the reference signal.]

[3. The apparatus of claim 1, further comprising input-side blocking oscillator circuitry configured to drive the switch.]

[4. The apparatus of claim 3, wherein the demand pulse generator comprises output-side blocking oscillator circuitry configured to generate the demand pulses.]

[5. The apparatus of claim 1, further comprising:

- a fast oscillator configured to initiate the generation of the demand pulses; and
- logic circuitry configured to provide gating of the demand pulses applied to the galvanic isolation circuitry.]

[6. The apparatus of claim 1, wherein the galvanic isolation circuitry further comprises dedicated circuitry configured to convey the demand pulses across the galvanic isolation.]

[7. The apparatus of claim 1, wherein the demand pulses are conveyed from the demand pulse generator to the switch via the transformer.]

[8. The apparatus of claim 1, wherein:

- the galvanic isolation circuitry divides the apparatus into (i) an input side corresponding to the primary winding of the transformer and (ii) an output side corresponding to the secondary winding of the transformer; and

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the demand pulse generator is located on the output side of the apparatus.]

[9. The apparatus of claim 1, further comprising a capacitor and a diode both galvanically connected to the secondary winding, wherein:

the diode is different from the rectifier and is poled to charge the capacitor during forward pulses of the apparatus; and

the demand pulse generator is powered by energy stored in the capacitor to generate the demand pulses.]

[10. Apparatus configured to provide galvanically isolated switched-mode power conversion, the apparatus comprising:

an input port configured to receive input power;

a switch configured to commutate the input power;

a transformer comprising (i) a primary winding arranged in circuit with the input port and the switch and (ii) a secondary winding arranged in circuit with a rectifier and an output port, wherein the transformer is configured to supply power from the input port to a load connected to the output port; and

a first pulse source circuitry located on an input side of the apparatus and configured to generate pulses to control the switch to start the power conversion; and

a second pulse source circuitry located on an output side of the apparatus and configured to generate pulses to control the switch to continue the power conversion after being started by the first pulse source circuitry.]

[11. The apparatus of claim 10, wherein the frequency of pulses generated by the second pulse source circuitry is different from the frequency of pulses generated by the first pulse source circuitry.]

[12. The apparatus of claim 11, wherein the frequency of pulses generated by the second pulse source circuitry is greater than the frequency of pulses generated by the first pulse source circuitry.]

[13. The apparatus of claim 10, wherein the frequency of pulses generated by the first pulse source circuitry is about 1 KHz or smaller.]

[14. The apparatus of claim 13, wherein the frequency of pulses generated by the second pulse source circuitry is about 60 KHz or greater.]

[15. The apparatus of claim 10, further comprising a capacitor and a diode both galvanically connected to the secondary winding, wherein:

the diode is different from the rectifier and is poled to charge the capacitor during forward pulses of the apparatus; and

the second pulse source circuitry is powered by energy stored in the capacitor to generate the pulses.]

[16. In an isolated switched-mode power converter having an input port and an output port, a method of regulation comprising:

(a) comparing a voltage or current at the output port with a reference that is galvanically associated therewith;

(b) generating or gating demand pulses responsive to that comparison;

(c) applying the demand pulses to an output-port side of galvanic isolation circuitry;

(d) receiving replicas of the demand pulses from an input-port side of the galvanic isolation circuitry; and

(e) adjusting commutation frequency of the converter responsive to the demand pulses to cause the voltage or current at the output port to attain a desired value.]

[17. The method of claim 16, wherein step (b) comprises: (b1) using a diode to charge a capacitor during forward pulses of the power converter, wherein the diode and

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the capacitor are galvanically connected within the output-port side of the galvanic isolation circuitry; and (b2) generating or gating the demand pulses using energy stored in the capacitor.]

18. Circuitry for controlling a flyback converter, the flyback converter comprising:

a converter primary side comprising an input port;

a converter secondary side comprising an output port, wherein the converter secondary side is galvanically isolated from the converter primary side; and

a power transformer configured to transfer input power received at the input port to provide output power at the output port, wherein:

the converter primary side further comprises a primary-side switch configured to selectively transfer the input power at the input port via the power transformer to the output power at the output port; the circuitry comprises primary-side circuitry and secondary-side circuitry, wherein, when the circuitry is configured to control the flyback converter, (i) the primary-side circuitry is on the converter primary side and (ii) the secondary-side circuitry is on the converter secondary side;

the secondary-side circuitry (i) determines when to turn on the primary-side switch based on output port voltage or current at the output port and (ii) generates corresponding demand pulses;

the converter secondary side is configured to transmit the demand pulses to the converter primary side;

the primary-side circuitry is configured to turn on the primary-side switch in response to the demand pulses conveyed from the converter secondary side to the converter primary side, wherein the primary-side circuitry, and not the secondary-side circuitry, originates the determination of when to turn off the primary-side switch;

frequency with which the primary-side switch is turned on is adjusted by the demand pulses conveyed from the converter secondary side to the converter primary side to regulate the output port voltage or current; and

the converter secondary side further comprises:

a first capacitor; and

a first rectifier poled to charge the first capacitor during forward power converter pulses of the flyback converter, wherein the demand pulses are generated using energy stored in the first capacitor.

19. The circuitry of claim 18, wherein the converter secondary side further comprises a second capacitor, different from the first capacitor, and a second rectifier, different from the first rectifier, wherein flyback voltage of the power transformer is rectified by the second rectifier and charges the second capacitor to supply the output port voltage or current.

20. The circuitry of claim 18, wherein the first rectifier is part of the secondary-side circuitry.

21. The circuitry of claim 18, wherein the flyback converter is configured to charge the first capacitor during flyback power converter pulses of the flyback converter.

22. The circuitry of claim 18, wherein the flyback converter is configured to charge the first capacitor during forward power converter pulses of the flyback converter even if the output port is short-circuited.

23. The circuitry of claim 18, wherein: the secondary-side circuitry is configured to generate a demand pulse when a feedback signal based on the

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output port voltage or current is lower in magnitude than a magnitude of a reference signal such that the demand pulses regulate the output port by driving the feedback signal to match the reference signal;

the flyback converter regulates the output port to have the feedback signal match the reference signal;

frequency of the demand pulses generated by the secondary-side circuitry is greater than frequency of pulses initiated on the converter primary side that turn on the primary-side switch;

the secondary-side circuitry generates a demand pulse whenever a magnitude of the output port voltage or current is below a magnitude of the output port's regulation voltage or current;

the primary-side switch is turned on for a duration that is independent of duration of the demand pulse that caused the primary-side switch to be turned on;

the secondary-side circuitry is configured to adjust the frequency of turning on the primary-side switch to supply a desired amount of voltage or current to the output port in order to regulate the output port; and

the converter secondary side comprises:

- a reference source configured to provide a reference signal; and
- a secondary-side comparator configured to compare a feedback signal based on the output port voltage or current to the reference signal wherein the frequency of the demand pulses is responsive to a comparison between the feedback signal and the reference signal.

24. The circuitry of claim 23, wherein:

the primary-side circuitry comprises the primary-side switch;

the converter secondary side further comprises a second capacitor, different from the first capacitor, and a second rectifier, different from the first rectifier, wherein flyback voltage of the power transformer is rectified by the second rectifier and charges the second capacitor to supply the output port voltage or current;

the converter secondary side is configured to charge the first capacitor during flyback power converter pulses of the flyback converter;

the converter secondary side is configured to charge the first capacitor during forward power converter pulses of the flyback converter even if the output port is short-circuited;

the first rectifier is part of the secondary-side circuitry;

feedback from the converter secondary side to the converter primary side for regulating the output port voltage or current is provided solely by the demand pulses generated by the secondary-side circuitry;

the secondary-side comparator generates a comparator output;

the secondary-side circuitry comprises:

- an oscillator configured to generate a stream of oscillator pulses independent of the comparator output; and
- logic circuitry configured to (i) receive the comparator output and the stream of oscillator pulses and (ii) process, based on the comparator output, the stream of oscillator pulses to generate the demand pulses by selectively blocking certain oscillator pulses;

regulation of the output port is based solely on the demand pulses generated on the converter secondary side;

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the flyback converter is configured such that the power transformer transfers unipolar input power received at the input port to provide the output power at the output port;

the converter primary side further comprises a primary-side magnetically coupled conductor;

the converter secondary side further comprises a secondary-side magnetically coupled conductor configured to be magnetically coupled to the primary-side magnetically coupled conductor to convey the demand pulses from the converter secondary side to the converter primary side;

the power transformer has a primary-side winding and a secondary-side winding;

the primary-side switch is connected in series with the primary-side winding of the power transformer;

the secondary-side winding of the power transformer is connected to the output port;

the primary-side magnetically coupled conductor is different from the primary-side winding of the power transformer;

the secondary-side magnetically coupled conductor is different from the secondary-side winding of the power transformer;

the primary-side circuitry comprises a primary-side oscillator configured to generate one or more primary-side pulses;

the primary-side switch is configured to be turned on based on (i) the one or more primary-side pulses generated by the primary-side oscillator and (ii) the demand pulses received from the converter secondary side;

the primary-side circuitry is configured to turn on the primary-side switch at power up, in order to transfer input power to the converter secondary side via the power transformer to power the secondary-side circuitry to generate the demand pulses; and

the converter secondary side does not generate pulses instructing the converter primary side to turn off the primary-side switch.

25. The circuitry of claim 18, wherein the secondary-side circuitry is configured to generate a demand pulse when a feedback signal based on the output port voltage or current is lower in magnitude than a magnitude of a reference signal such that the demand pulses regulate the output port by driving the feedback signal to match the reference signal.

26. The circuitry of claim 25, wherein the flyback converter regulates the output port to have the feedback signal match the reference signal.

27. The circuitry of claim 18, wherein feedback from the converter secondary side to the converter primary side for regulating the output port voltage or current is provided solely by the demand pulses generated by the secondary-side circuitry.

28. The circuitry of claim 18, wherein:

- each demand pulse conveyed from the converter secondary side to the converter primary side has a leading edge; and
- when a particular demand pulse results in a particular occurrence of the primary-side switch turning on, the particular occurrence of the primary-side switch turning on is in response to detecting the leading edge of the particular demand pulse independent of any other demand pulses conveyed from the converter secondary side to the converter primary side and independent of any other pulse edges appearing on the converter primary side.

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29. The circuitry of claim 18, wherein the secondary-side circuitry comprises:

an oscillator that generates oscillator pulses, each oscillator pulse representing logic 1; and
logic circuitry that selectively blocks certain oscillator 5 pulses in generating the demand pulses.

30. The circuitry of claim 29, wherein the logic circuitry is not an OR gate.

31. The circuitry of claim 29, wherein the logic circuitry selectively blocks certain oscillator pulses from becoming 10 demand pulses that would otherwise result in the primary-side switch being turned on, while selectively allowing other oscillator pulses to become the demand pulses that do result in the primary-side switch being turned on.

32. The circuitry of claim 18, wherein frequency of the demand pulses generated by the secondary-side circuitry is 15 greater than frequency of pulses initiated on the converter primary side that turn on the primary-side switch.

33. The circuitry of claim 18, wherein the secondary-side circuitry generates a demand pulse whenever a magnitude of 20 the output port voltage or current is below a magnitude of the output port's regulation voltage or current.

34. The circuitry of claim 18, wherein the secondary-side circuitry processes, based on a comparator output, a secondary-side stream of pulses to generate the demand pulses. 25

35. The circuitry of claim 18, wherein the secondary-side circuitry comprises:

a comparator configured to generate a comparator output based on a comparison between (i) a feedback signal 30 based on the output port voltage or current and (ii) a reference signal;

an oscillator configured to generate a stream of pulses independent of the comparator output; and

logic circuitry configured to (i) receive the comparator 35 output and the stream of pulses and (ii) process, based on the comparator output, the stream of pulses to generate the demand pulses.

36. The circuitry of claim 18, wherein regulation of the output port is based solely on the demand pulses generated 40 on the converter secondary side.

37. The circuitry of claim 18, wherein the determination of when to turn off the primary-side switch is always originated on the converter primary side and never on the 45 converter secondary side.

38. The circuitry of claim 18, wherein the flyback converter is configured such that the power transformer transfers unipolar input power received at the input port to provide the output power at the output port.

39. The circuitry of claim 18, wherein, unless the primary-side switch is already on due to a pulse generated on the 50 primary side, the primary-side switch is turned on once for each different demand pulse.

40. The circuitry of claim 18, wherein:

the converter primary side further comprises a primary-side 55 magnetically coupled conductor; and

the converter secondary side further comprises a secondary-side magnetically coupled conductor configured to be magnetically coupled to the primary-side magnetically coupled conductor to convey the demand pulses 60 from the converter secondary side to the converter primary side.

41. The circuitry of claim 40, wherein:

the power transformer has a primary-side winding and a secondary-side winding;

the primary-side switch is connected in series with the primary-side winding of the power transformer;

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the secondary-side winding of the power transformer is connected to the output port;

the primary-side magnetically coupled conductor is different from the primary-side winding of the power transformer; and

the secondary-side magnetically coupled conductor is the secondary-side winding of the power transformer.

42. The circuitry of claim 40, wherein:

the power transformer has a primary-side winding and a secondary-side winding;

the primary-side switch is connected in series with the primary-side winding of the power transformer;

the secondary-side winding of the power transformer is connected to the output port;

the primary-side magnetically coupled conductor is different from the primary-side winding of the power transformer; and

the secondary-side magnetically coupled conductor is different from the secondary-side winding of the power transformer.

43. The circuitry of claim 42, wherein:

the primary-side circuitry comprises the primary-side magnetically coupled conductor; and

the secondary-side circuitry comprises the secondary-side magnetically coupled conductor.

44. The circuitry of claim 40, wherein:

the power transformer has a primary-side winding and a secondary-side winding;

the primary-side switch is connected in series with the primary-side winding of the power transformer;

the secondary-side winding of the power transformer is connected to the output port;

the primary-side magnetically coupled conductor is the primary-side winding of the power transformer; and the secondary-side magnetically coupled conductor is the secondary-side winding of the power transformer.

45. The circuitry of claim 18, wherein:

the primary-side circuitry comprises a primary-side oscillator configured to generate one or more primary-side pulses; and

the primary-side switch is configured to be turned on based on (i) the one or more primary-side pulses generated by the primary-side oscillator and (ii) the demand pulses received from the secondary-side circuitry.

46. The circuitry of claim 18, wherein primary-side circuitry is configured to turn on the primary-side switch for a duration that is independent of duration of the demand pulse that caused the primary-side switch to be turned on.

47. The circuitry of claim 18, wherein the primary-side circuitry is configured to turn on the primary-side switch at power up, in order to transfer input power to the converter secondary side via the power transformer to power the secondary-side circuitry to generate the demand pulses.

48. The circuitry of claim 18, wherein the primary-side circuitry does not receive pulses from the converter secondary side instructing the primary-side circuitry to turn off the primary-side switch.

49. The circuitry of claim 18, wherein the primary-side circuitry is configured to avoid premature turnoff of the primary-side switch due to capacitive charging of the primary-side switch.

50. The circuitry of claim 18, wherein the primary-side circuitry is configured to establish a maximum duration for which the primary-side switch is allowed to stay on.

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51. The circuitry of claim 18, wherein the primary-side circuitry is configured to receive power from a bias winding of the converter primary side.

52. The circuitry of claim 18, wherein the primary-side circuitry is configured to determine when to turn off the primary-side switch based on either (i) current flowing through the primary-side switch or (ii) a maximum duration for which the primary-side switch is allowed to stay on.

53. The circuitry of claim 18, wherein the secondary-side circuitry is configured to adjust the frequency of turning on the primary-side switch to supply a desired amount of voltage or current to the output port in order to regulate the output port.

54. The circuitry of claim 18, wherein the secondary-side circuitry comprises:

a reference source configured to provide a reference signal; and

a secondary-side comparator configured to compare a feedback signal based on the output port voltage or current to the reference signal wherein frequency of the demand pulses is responsive to the comparison between the feedback signal and the reference signal.

55. The circuitry of claim 24, wherein:

each demand pulse conveyed from the converter secondary side to the converter primary side has a leading edge; and

when a particular demand pulse results in a particular occurrence of the primary-side switch turning on, the particular occurrence of the primary-side switch turning on is in response to detecting the leading edge of the particular demand pulse independent of any other demand pulses conveyed from the converter secondary side to the converter primary side and independent of any other pulse edges appearing on the converter primary side.

56. The circuitry of claim 24, wherein the determination of when to turn off the primary-side switch is always originated on the converter primary side and never on the converter secondary side.

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57. The circuitry of claim 24, wherein, unless the primary-side switch is already on due to a pulse generated on the converter primary side, the primary-side switch is turned on once for each different demand pulse.

58. The circuitry of claim 24, wherein the primary-side circuitry is configured to avoid premature turnoff of the primary-side switch due to capacitive charging of the primary-side switch.

59. The circuitry of claim 24, wherein the primary-side circuitry is configured to establish a maximum duration for which the primary-side switch is allowed to stay on.

60. The circuitry of claim 24, wherein the primary-side circuitry is configured to receive power from a bias winding of the converter primary side.

61. The circuitry of claim 24, wherein the primary-side circuitry is configured to determine when to turn off the primary-side switch based on either (i) current flowing through the primary-side switch or (ii) a maximum duration for which the primary-side switch is allowed to stay on.

62. The circuitry of claim 18, wherein the demand pulses are transmitted from the secondary-side circuitry to the primary-side circuitry via inductive galvanic isolation circuitry.

63. The circuitry of claim 18, wherein the demand pulses are transmitted from the secondary-side circuitry to the primary-side circuitry via capacitive galvanic isolation circuitry.

64. The circuitry of claim 18, wherein the demand pulses are transmitted from the secondary-side circuitry to the primary-side circuitry via optocoupled galvanic isolation circuitry.

65. The circuitry of claim 18, wherein the demand pulses are transmitted from the secondary-side circuitry to the primary-side circuitry via piezoelectric galvanic isolation circuitry.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : RE47,714 E
APPLICATION NO. : 15/202746
DATED : November 5, 2019
INVENTOR(S) : Morong et al.

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

In the Specification

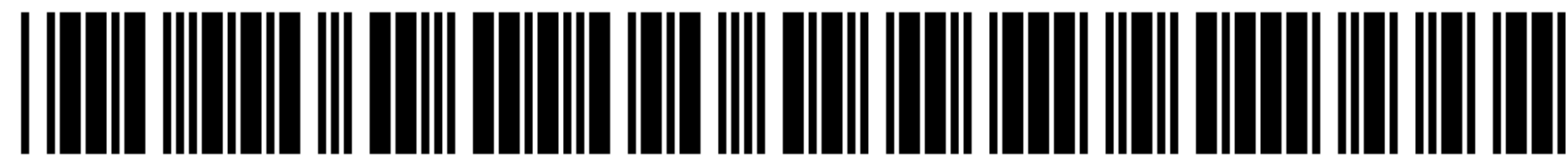
At Column 1, under the heading "CROSS-REFERENCE TO RELATED APPLICATIONS," replace Lines 15-31 (approx.), with the following:

--NOTICE: More than one reissue application has been filed for the reissue of U.S. Patent No. 9,071,152 B2. The reissue applications are U.S. Reissue Patent Application Serial No. 16/987,654, filed on August 7, 2020, which is a continuation reissue of U.S. Reissue Patent Application Serial No. 16/547,850, filed on August 22, 2019, which together with U.S. Reissue Patent Application Serial No. 16/548,897, filed on August 23, 2019, are each ('897 and '850) a continuation reissue application of U.S. Reissue Patent Application Serial No. 15/202,746 (the present application), filed on July 6, 2016, now U.S. Reissue Patent No. RE47,714 E, issued November 5, 2019, which together with U.S. Reissue Patent Application Serial No. 15/168,998, filed on May 31, 2016, now U.S. Reissue Patent No. RE47,713 E, issued November 5, 2019, each of which ('746 and '998) are a continuation reissue application of U.S. Reissue Patent Application Serial No. 15/090,929, filed on April 5, 2016, now U.S. Reissue Patent No. RE47,031 E, issued September 4, 2018, which is a reissue application of U.S. Patent Application Serial No. 13/923,394, filed on June 21, 2013, now U.S. Patent No. 9,071,152 B2, issued June 30, 2015, which claims the benefit of the filing dates of U.S. Provisional Patent Application No. 61/667,473, filed on July 3, 2012, now expired, and U.S. Provisional Patent Application No. 61/727,795, filed on November 19, 2012, now expired, the--

Signed and Sealed this
Second Day of August, 2022



Katherine Kelly Vidal
Director of the United States Patent and Trademark Office



US00RE47714C1

(12) **EX PARTE REEXAMINATION CERTIFICATE** (12942nd)
United States Patent
Morong et al.

(10) **Number:** **USRE47,714C1**(45) **Certificate Issued:** ***Jun. 24, 2025**(54) **POWER CONVERTER WITH DEMAND PULSE ISOLATION**(71) Applicant: **CogniPower, LLC**, Malvern, PA (US)(72) Inventors: **William H. Morong**, Paoli, PA (US);
Thomas E. Lawson, Malvern, PA (US)(73) Assignee: **CogniPower, LLC****Reexamination Request:**

No. 90/019,538, Jun. 13, 2024

Reexamination Certificate for:Patent No.: **RE47,714**
Issued: **Nov. 5, 2019**
Appl. No.: **15/202,746**
Filed: **Jul. 6, 2016**

Certificate of Correction issued Aug. 2, 2022

(*) Notice: This patent is subject to a terminal disclaimer.

Related U.S. Application Data

(63) Continuation of application No. 15/090,929, filed on Apr. 5, 2016, now Pat. No. Re. 47,031, which is an application for the reissue of Pat. No. 9,071,152.

(60) Provisional application No. 61/667,473, filed on Jul. 3, 2012, provisional application No. 61/727,795, filed on Nov. 19, 2012.

(51) **Int. Cl.**
H02M 3/335 (2006.01)(52) **U.S. Cl.**
CPC ... **H02M 3/33523** (2013.01); **H02M 3/33507** (2013.01); **H02M 3/33515** (2013.01)(58) **Field of Classification Search**

None

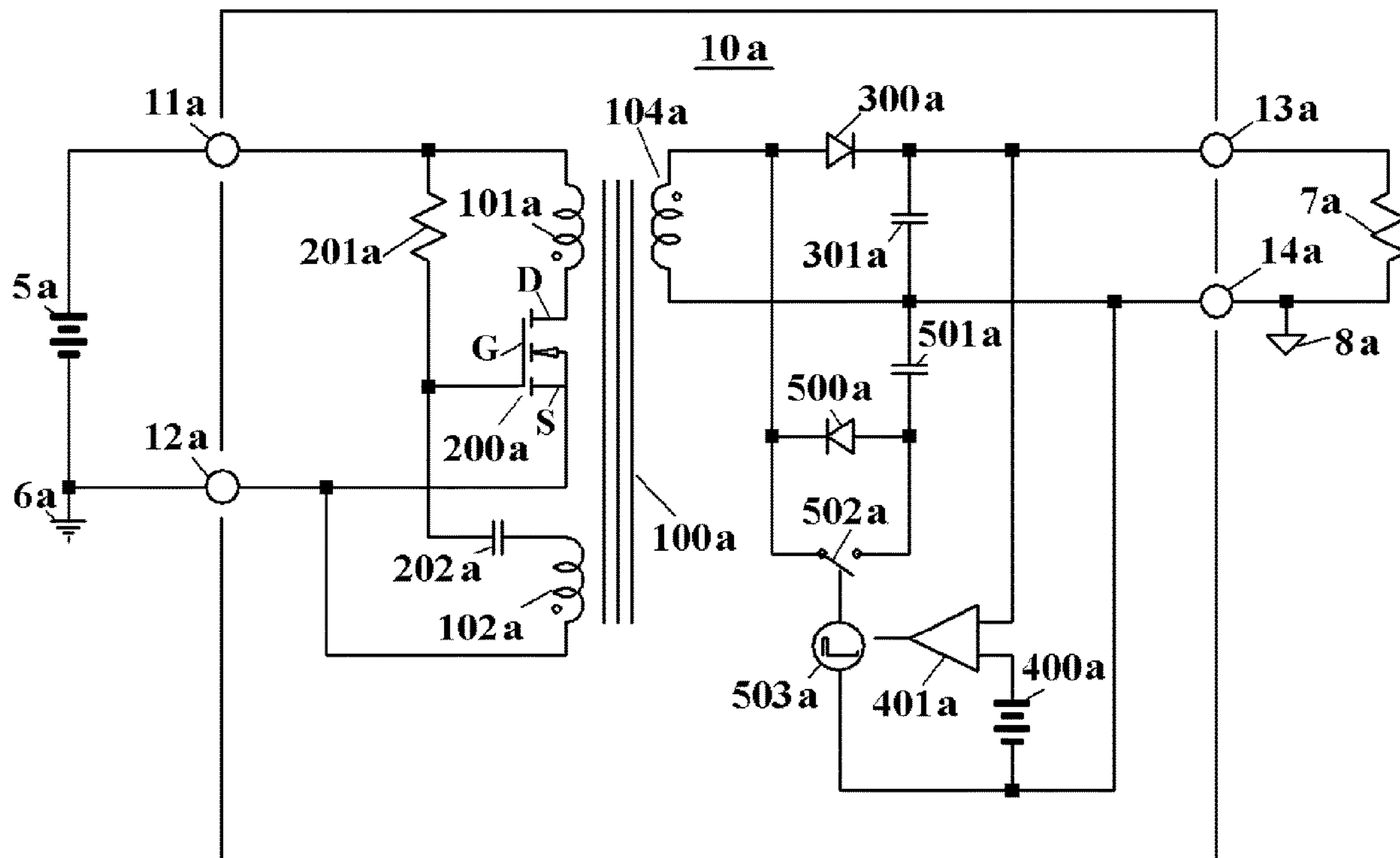
See application file for complete search history.

(56) **References Cited**

To view the complete listing of prior art documents cited during the proceeding for Reexamination Control Number 90/019,538, please refer to the USPTO's Patent Electronic System.

Primary Examiner — Stephen J. Ralis(57) **ABSTRACT**

The present invention provides a switched-mode power converter with regulation demand pulses sent across a galvanic isolation barrier.



**EX PARTE
REEXAMINATION CERTIFICATE**

NO AMENDMENTS HAVE BEEN MADE TO
THE PATENT

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AS A RESULT OF REEXAMINATION, IT HAS BEEN
DETERMINED THAT:

The patentability of claims **18-40** and **42-64** is confirmed. ¹⁰

Claims **1-17** were previously cancelled.

Claims **41** and **65** were not reexamined.

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