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(54) **IMAGE PICKUP LENS FOR SOLID-STATE
IMAGE PICKUP ELEMENT**

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(*) Notice: This patent is subject to a terminal dis-
claimer.

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(2013.01)

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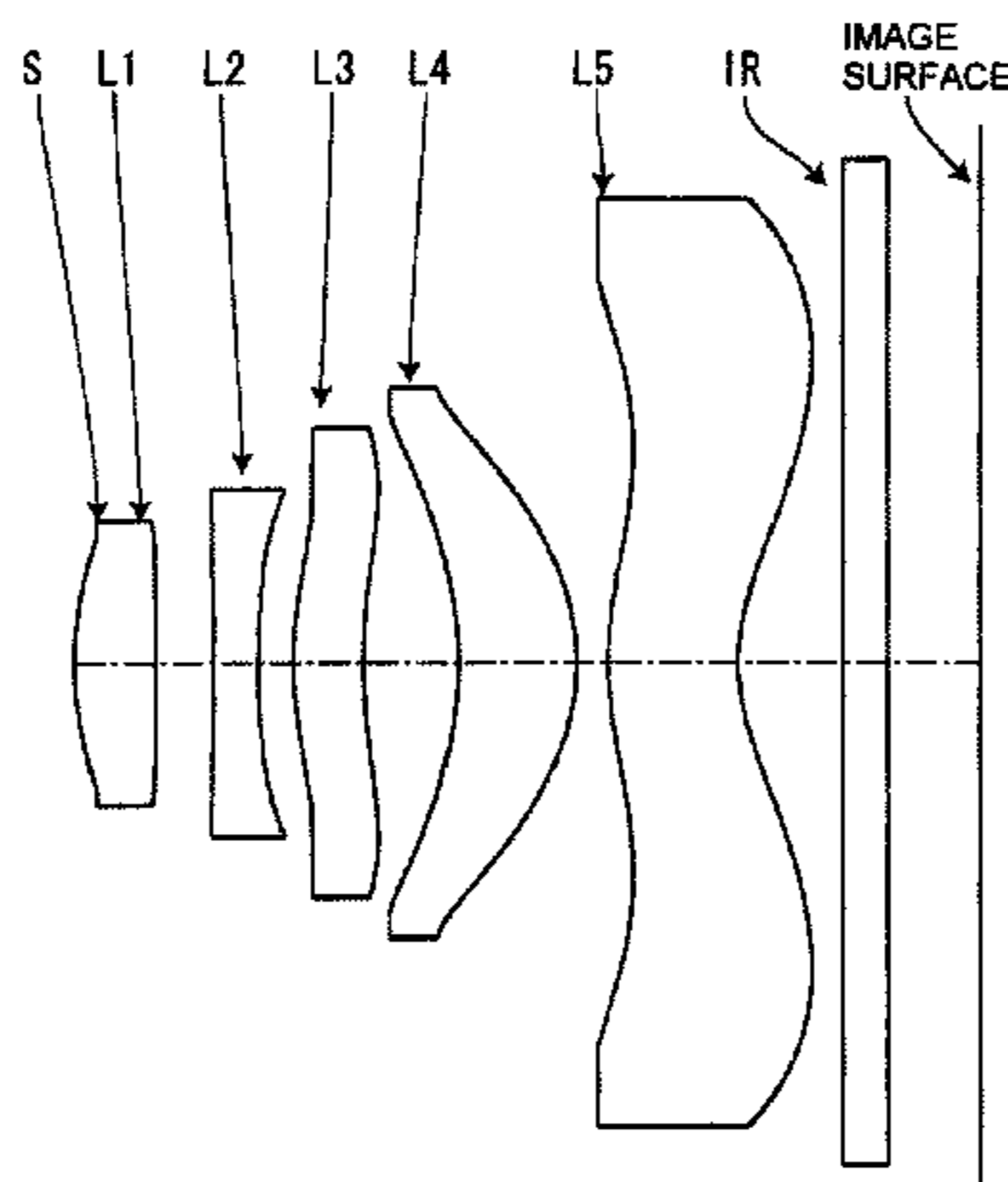
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(57) **ABSTRACT**

Disclosed is a low-cost, compact image pickup lens for a
solid-state image pickup element. The image pickup lens
includes, in the order from an object side, a first lens L1,
which has a convex surface facing the object side on an
optical axis and has a positive refractive power; a second
lens L2, which has a concave surface facing an image side
on the optical axis and has a negative refractive power; a
third lens L3, which has a convex surface facing the object
side on the optical axis and has a meniscus shape; a fourth
lens L4, which has a convex surface facing the image side
on the optical axis, has a positive refractive power, and has
a meniscus shape; and a fifth lens L5, which has a concave
surface facing the image side on the optical axis, has a
negative refractive power, and has a meniscus shape.

19 Claims, 12 Drawing Sheets



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(58) **Field of Classification Search**

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See application file for complete search history.

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FIG. 1

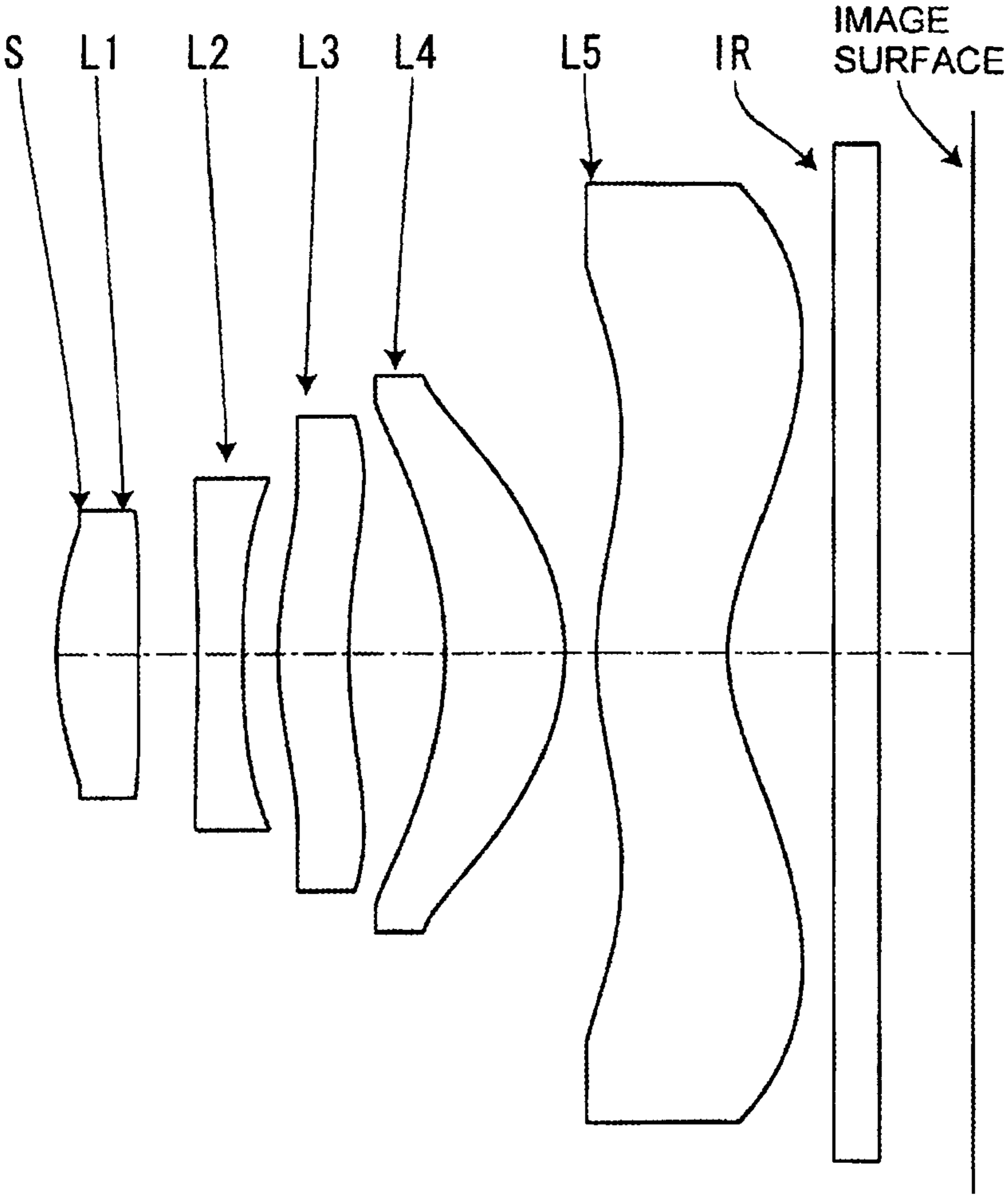


FIG. 2

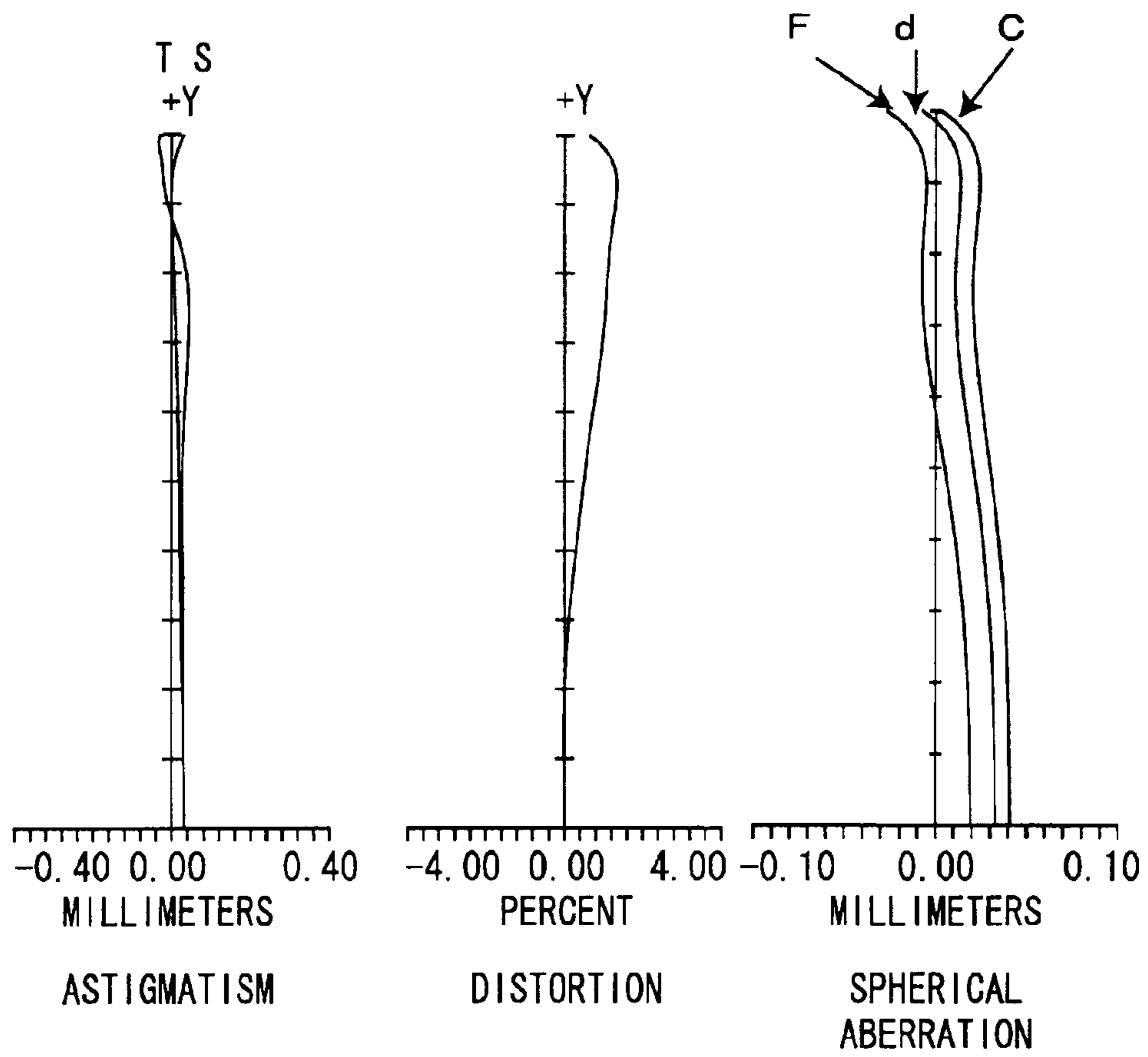


FIG. 3

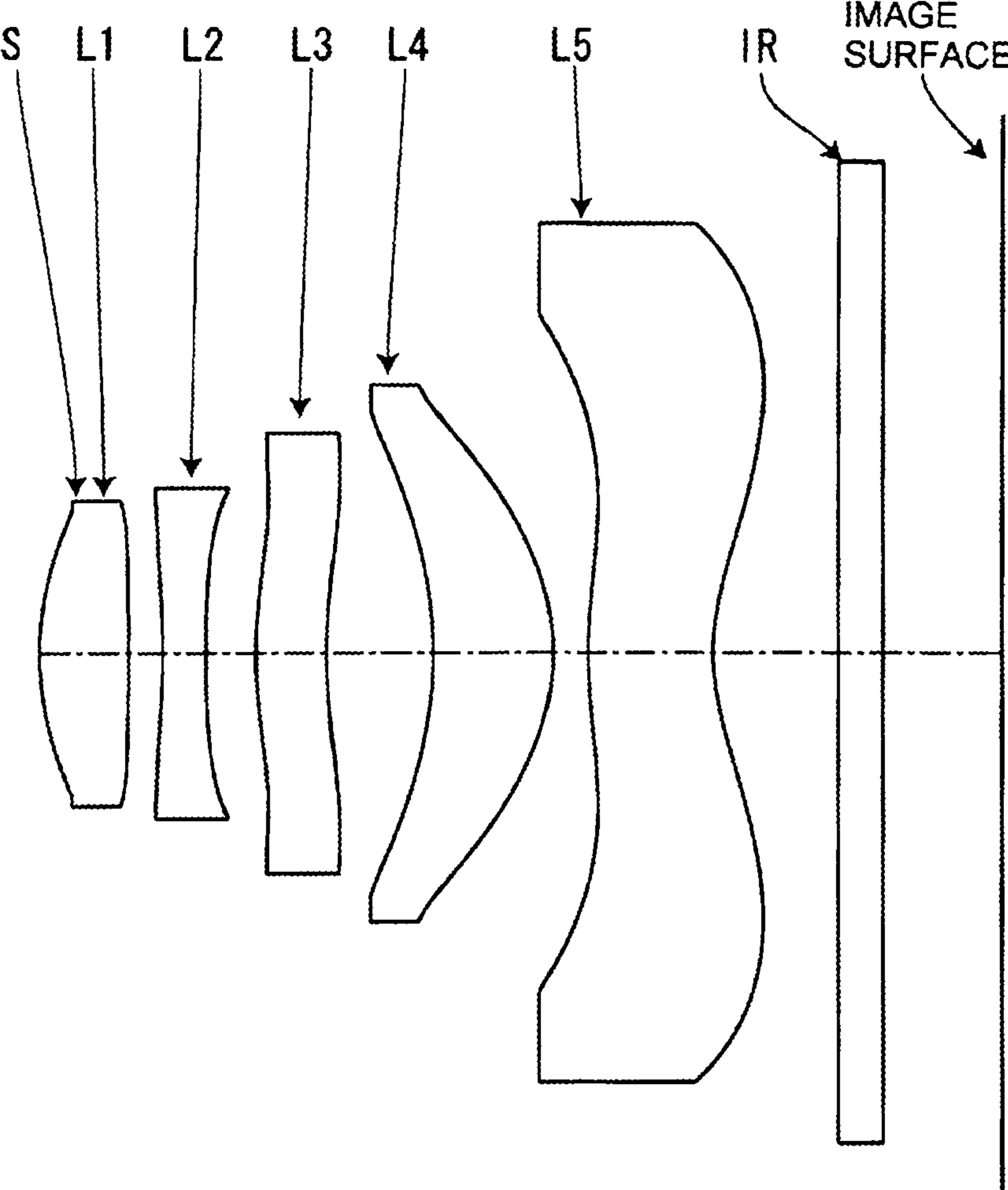


FIG. 4

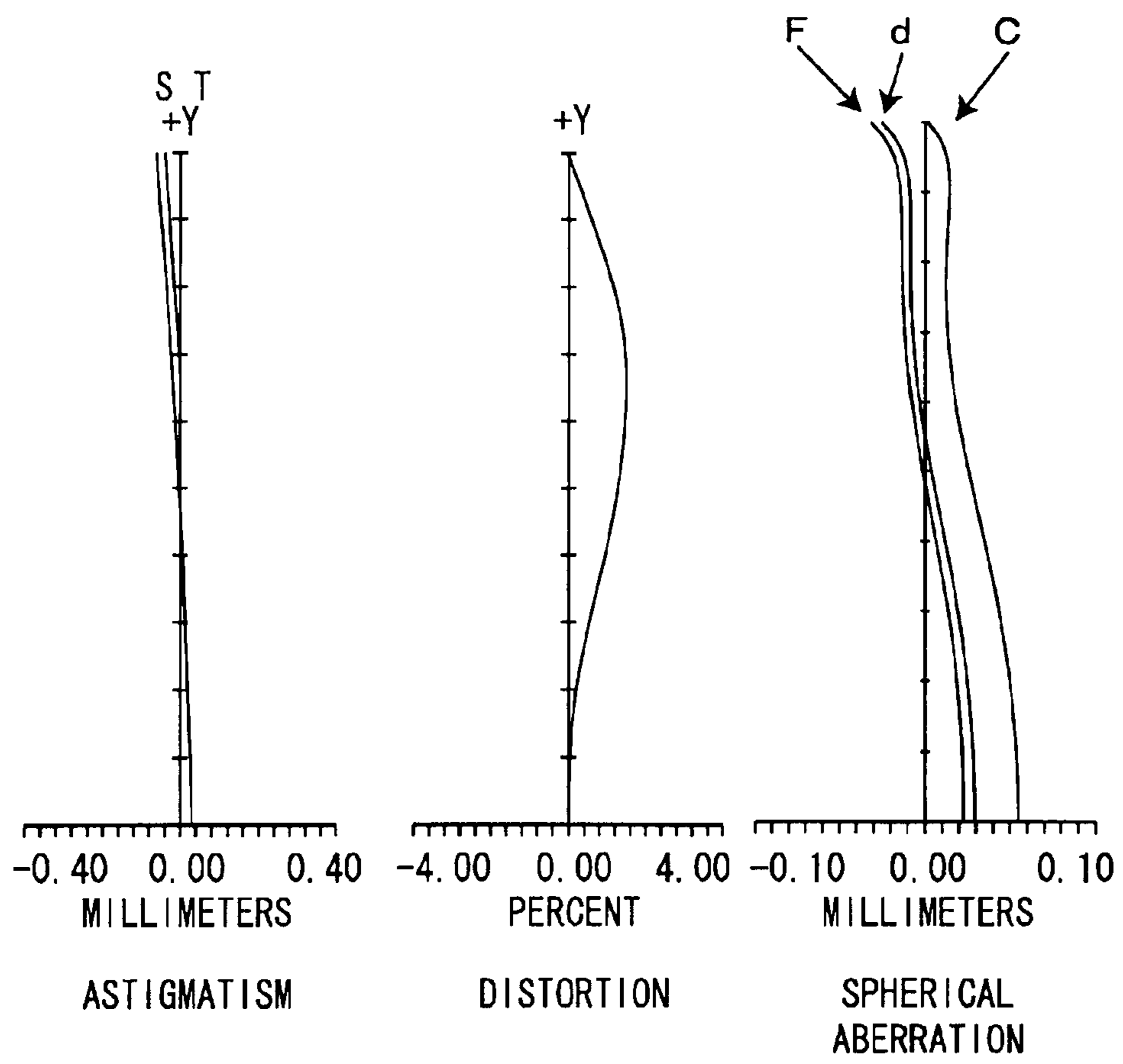


FIG. 5

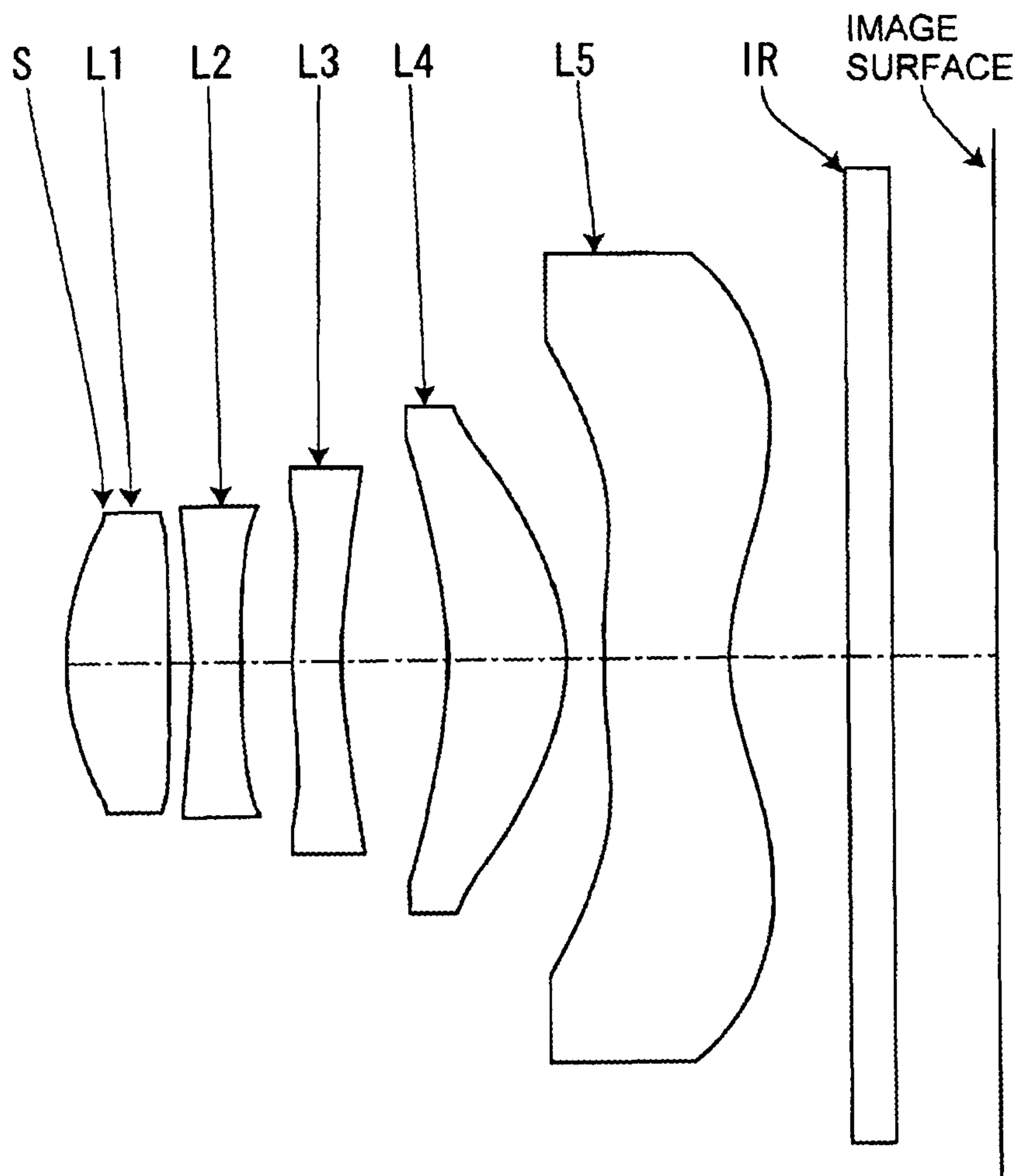


FIG. 6

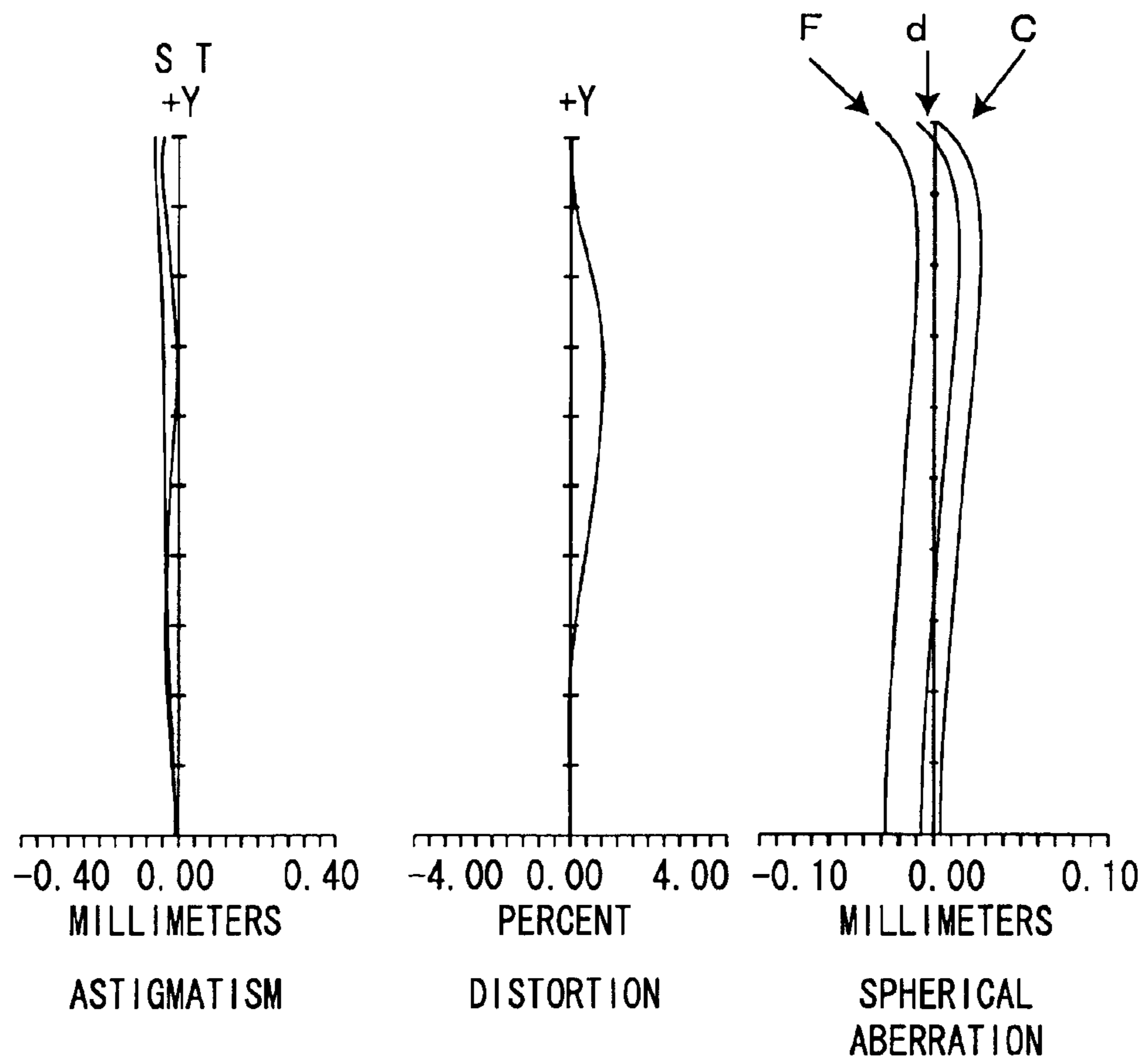


FIG. 7

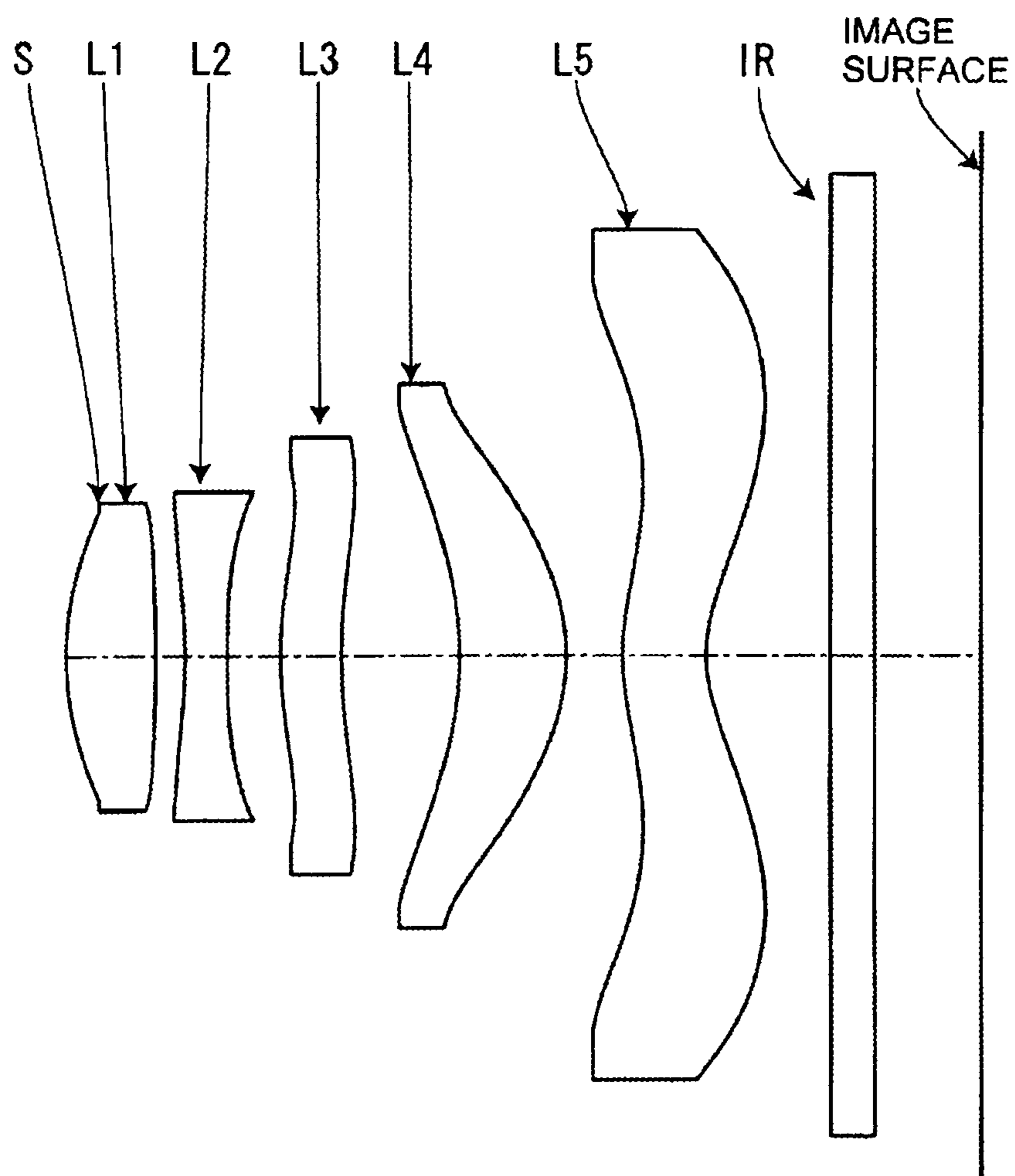


FIG. 8

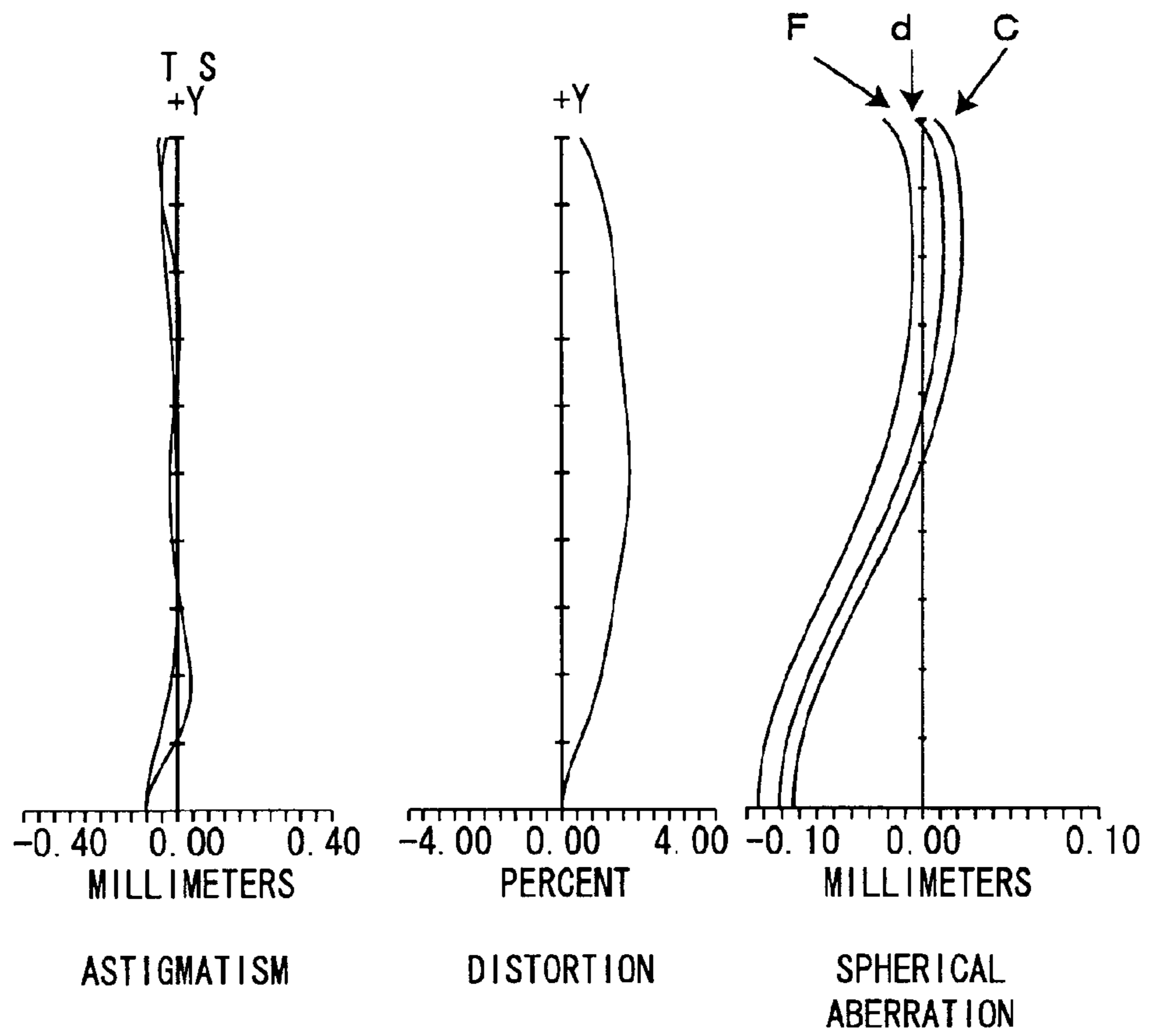


FIG. 9

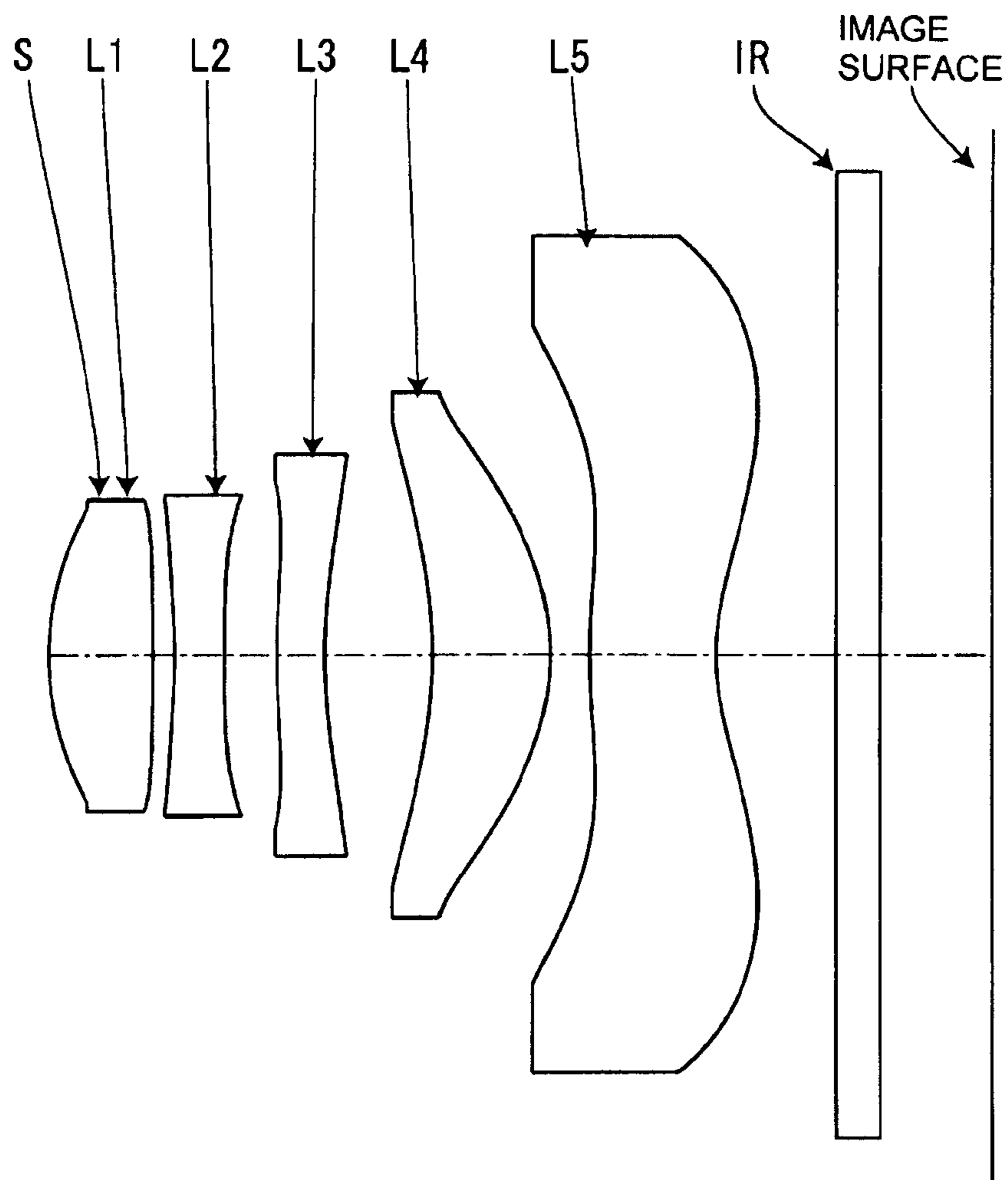


FIG. 10

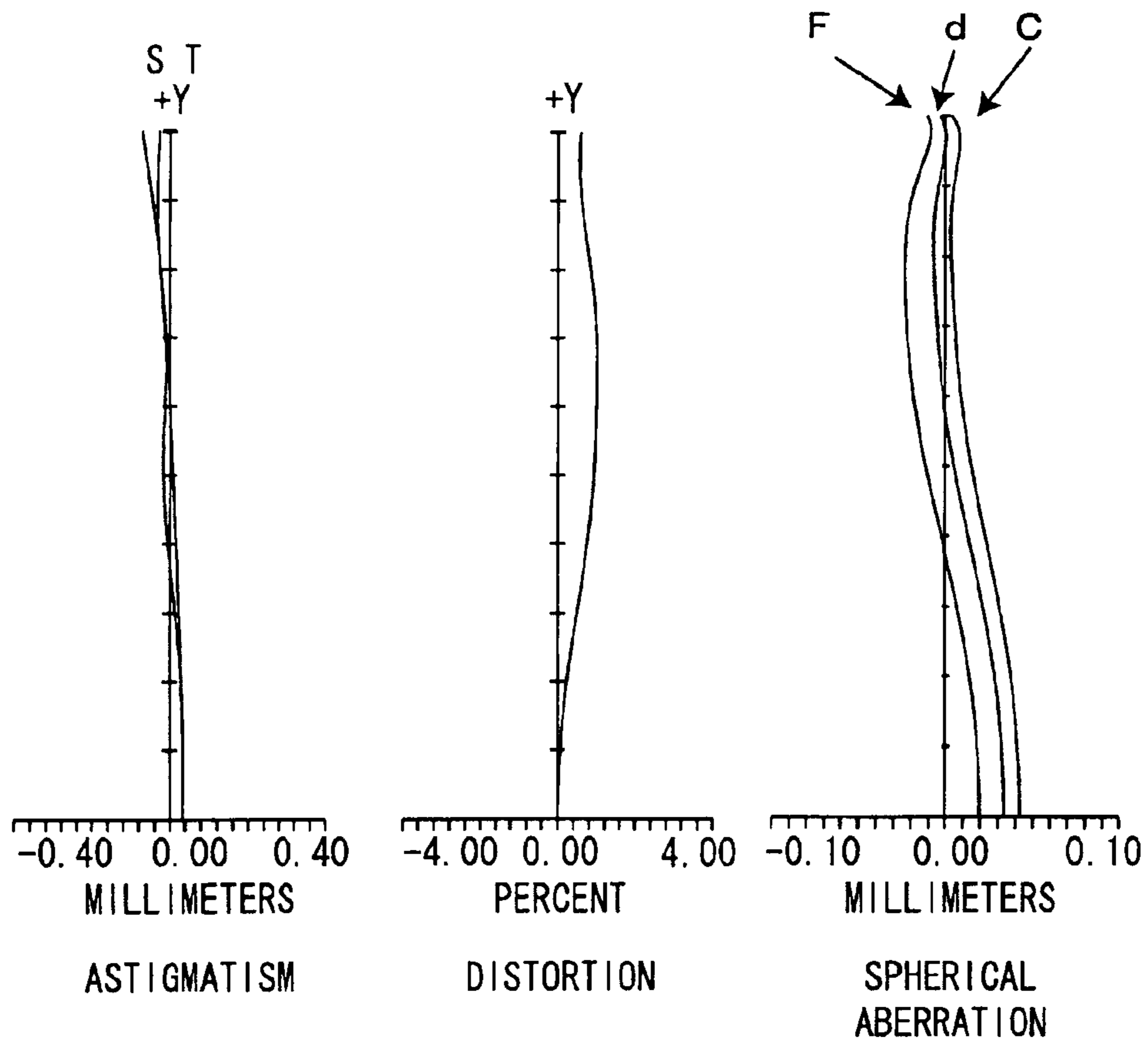


FIG. 11

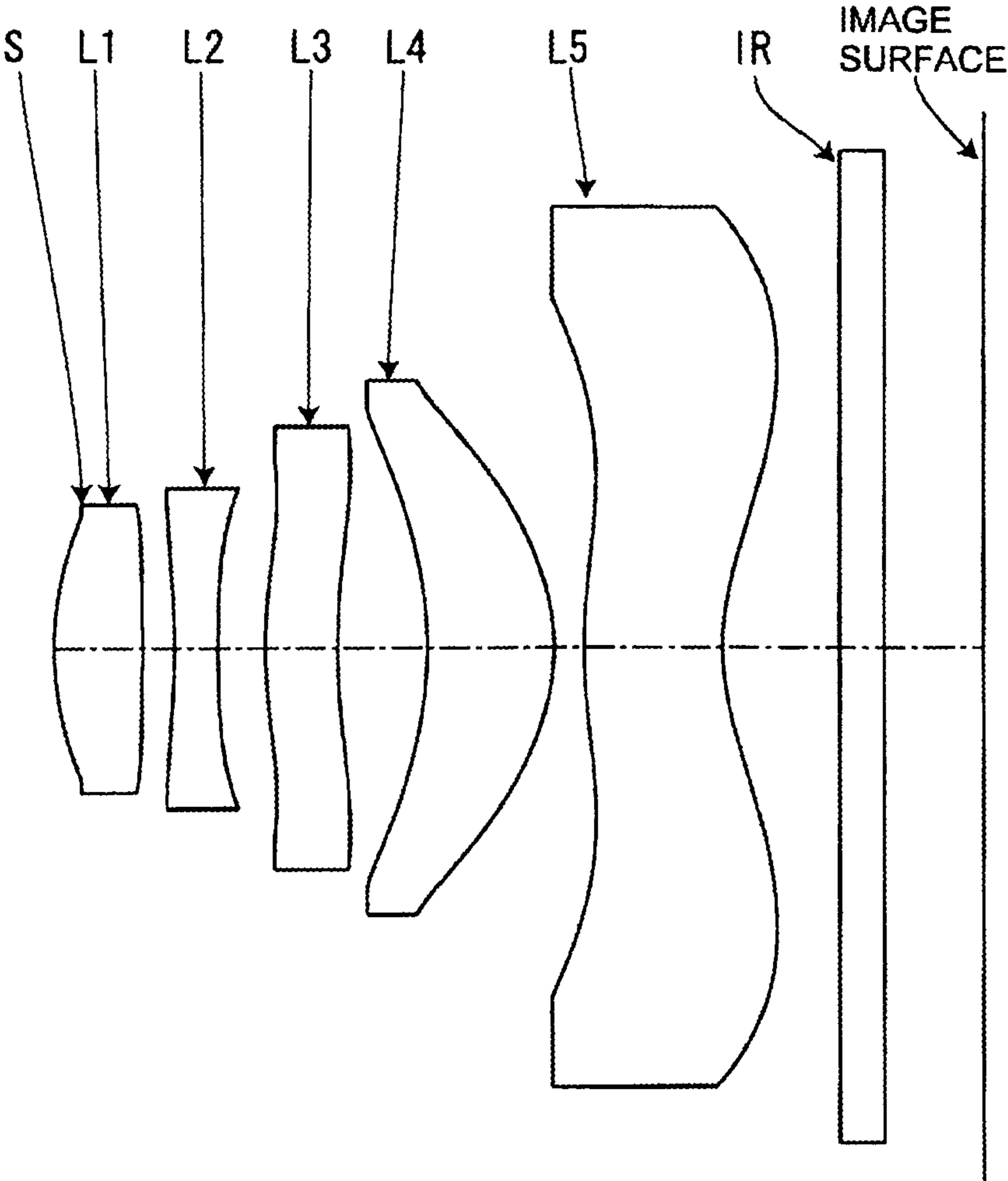
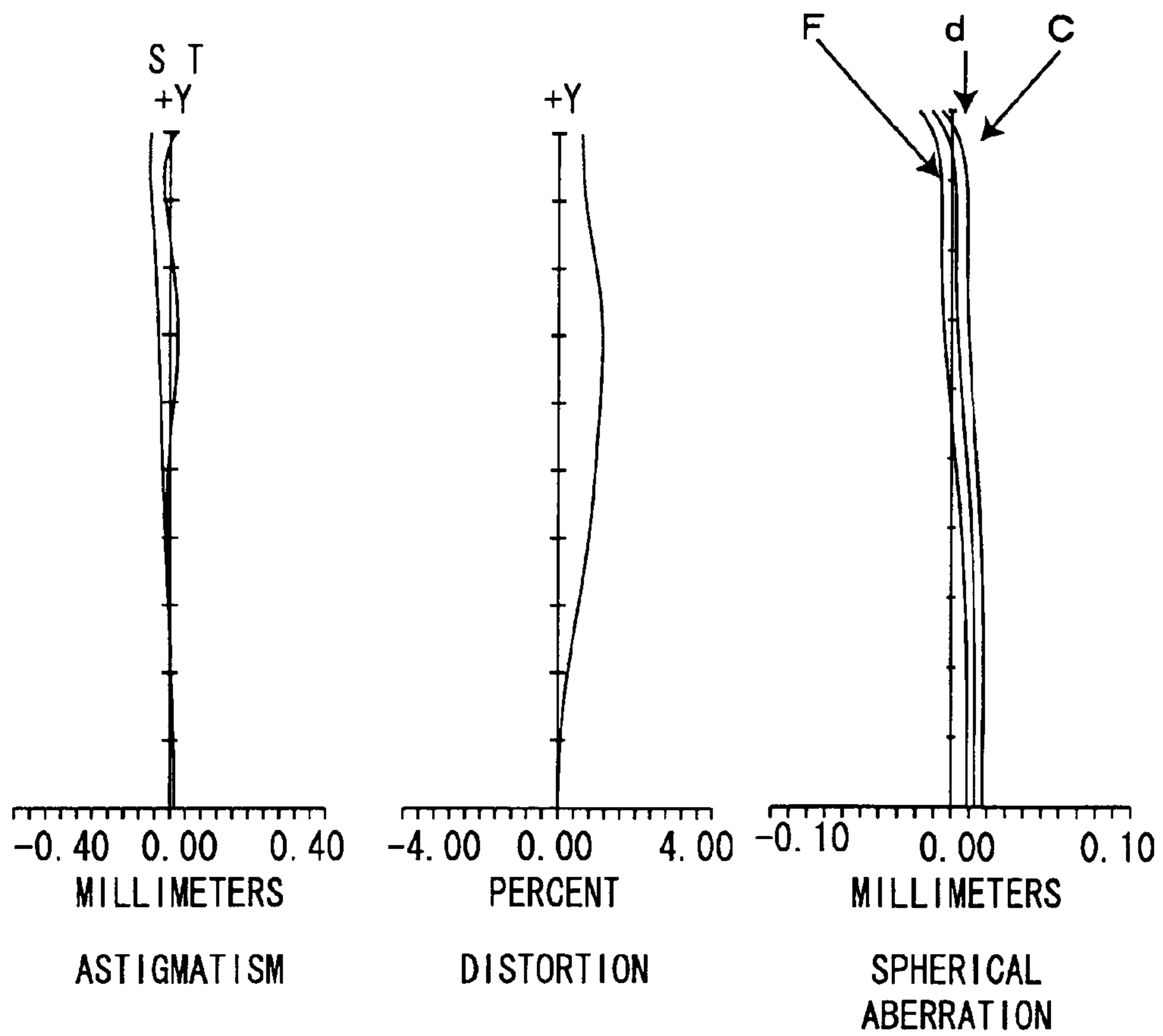


FIG. 12



**IMAGE PICKUP LENS FOR SOLID-STATE
IMAGE PICKUP ELEMENT**

Matter enclosed in heavy brackets [] appears in the original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue; a claim printed with strikethrough indicates that the claim was canceled, disclaimed, or held invalid by a prior post-patent action or proceeding.

This application is a reissue continuation of application Ser. No. 14/684,878, which is an application for reissue of U.S. Pat. No. 8,422,145; more than one reissue of U.S. Pat. No. 8,422,145 has been filed, including application Ser. No. 14/993,878, filed Jan. 12, 2016, which is a reissue continuation of application Ser. No. 14/684,878.

TECHNICAL FIELD

The present invention relates to an image pickup lens for a solid-state image pickup element that is used in a small-size image pickup device for mobile terminals, PDA (Personal Digital Assistance) devices, and other small-size, thin electronic devices.

BACKGROUND ART

In recent years, the market for mobile terminals having an image pickup device has grown. Consequently, the image pickup device has begun to incorporate a small-size, high-pixel-number, solid-state image pickup element.

As an increasing number of small-size, high-pixel-number, image pickup elements are used, it is demanded that image pickup lenses be improved in terms of resolution and image quality. It is also demanded that such high-resolution, high-quality image pickup lenses become widespread and available at low cost.

An image pickup lens having plural lenses is made commonly available to meet the demand for high performance. An image pickup lens having five lenses, which exhibit higher performance than a lens having two to four lenses, is also proposed.

An image pickup lens disclosed, for instance, in Patent Document 1 exhibits high performance by including, in the order from an object side, a first lens, a second lens, a third lens, a fourth lens, and a fifth lens. The first lens has a convex surface on the object side and has a positive refractive power. The second lens has a concave surface facing an image side, has a negative refractive power, and has a meniscus shape. The third lens has a convex surface facing the image side, has a positive refractive power, and has a meniscus shape. The fourth lens has an aspherical surface on both sides, has a concave surface on the image side on an optical axis, and has a negative refractive power. The fifth lens has an aspherical surface on both sides and has a positive or negative refractive power.

An image pickup lens disclosed, for instance, in Patent Document 2 exhibits high performance by including, in the order from an object side, a first lens, a second lens, a third lens, a fourth lens, and a fifth lens. The first lens has an aperture stop and has a positive refractive power. The second lens is joined to the first lens and has a negative refractive power. The third lens has a concave surface facing the object side and has a meniscus shape. The fourth lens has a concave surface facing the object side and has a meniscus shape. The

fifth lens has at least one aspherical surface, has a convex surface facing the object side, and has a meniscus shape.

CITATION LIST

Patent Documents

Patent Document 1: JP-A No. 2007-264180

Patent Document 2: JP-A No. 2007-298572

SUMMARY OF INVENTION

Problems to be Solved by the Invention

The image pickup lenses described in Patent Documents 1 and 2 each include five lenses to exhibit high performance. From the viewpoint of their optical length, however, they are not adequately designed to reduce their size and thickness.

The present invention has been made in view of the above circumstances and has an object to provide a small-size, low-cost, high-performance image pickup lens for a solid-state image pickup element.

Means for Solving the Problems

The above-mentioned problem can be addressed when the image pickup lens for a solid-state image pickup element is configured as described below.

The image pickup lens described in aspect 1 of the invention includes, in the order from an object side, a first lens, a second lens, a third lens, a fourth lens, and a fifth lens. The first lens has a convex surface facing the object side on an optical axis and has a positive refractive power. The second lens has a concave surface facing an image side on the optical axis and has a negative refractive power. The third lens has a convex surface facing the object side on the optical axis and has a meniscus shape. The fourth lens has a convex surface facing the image side on the optical axis, has a positive refractive power, and has a meniscus shape. The fifth lens has a concave surface facing the image side on the optical axis, has a negative refractive power, and has a meniscus shape.

The image pickup lens described in aspect 2 of the invention satisfies conditional expressions (1) and (2) below, which concern the Abbe number of a material used for the first lens and the second lens:

$$45 < v_1 < 90 \quad (1)$$

$$22 < v_2 < 35 \quad (2)$$

where v_1 is the Abbe number for d-line of the first lens, and v_2 is the Abbe number for d-line of the second lens.

Conditional expression (1) above defines the Abbe number of the first lens. If the lower limit indicated by conditional expression (1) is exceeded, the variance value difference from the second lens is decreased so that chromatic aberration correction is insufficient. If, on the contrary, the upper limit is exceeded, the balance between axial chromatic aberration and chromatic aberration of magnification is impaired so that performance deterioration occurs at the periphery of an image area.

Conditional expression (2) above defines the Abbe number of the second lens. If the lower limit indicated by conditional expression (2) is exceeded, the balance between axial chromatic aberration and off-axis chromatic aberration is impaired so that performance deterioration occurs at the periphery of the image area. If, on the contrary, the upper

limit is exceeded, the variance value difference from the first lens is decreased so that chromatic aberration correction is insufficient.

The image pickup lens described in aspect 3 of the invention is configured so that the second lens, the third lens, the fourth lens, and the fifth lens are so-called plastic lenses that have at least one aspherical surface and are made of a resin material.

Cost reduction can be achieved when at least the second lens, the third lens, the fourth lens, and the fifth lens are made of an inexpensive resin material exhibiting high production efficiency.

The image pickup lens described in aspect 4 of the invention is configured so that an aperture stop is positioned on the object side of the first lens.

As the aperture stop is positioned on the object side of the first lens, it is easy to reduce a CRA (Chief Ray Angle) and obtain sufficient light intensity at the periphery of an image surface at which light intensity decreases.

The image pickup lens described in aspect 5 of the invention is configured so that the object-side surface and image-side surface of the fifth lens have an aspherical shape, which contains at least one inflection point between the center and the periphery of the lens.

As the object-side surface and image-side surface of the fifth lens have an aspherical shape that contains at least one inflection point between the center and the periphery of the lens, it is possible to obtain adequate off-axis performance and CRA.

The image pickup lens described in aspect 6 of the invention is configured so that the first lens and the second lens satisfy conditional expressions (3) and (4) below:

$$0.50 < f1/f < 1.00 \quad (3)$$

$$-1.50 < f2/f < -0.65 \quad (4)$$

where f is the composite focal length of lenses included in the entire image pickup lens, $f1$ is the focal length of the first lens, and $f2$ is the focal length of the second lens.

Conditional expression (3) above defines the range of the focal length of the first lens with respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (3) is exceeded, the focal length of the first lens is too small. This makes it difficult to correct spherical aberration and coma aberration. If, on the contrary, the upper limit is exceeded, the optical length is too great so that the thickness of the image pickup lens cannot be sufficiently reduced.

Conditional expression (4) above defines the range of the focal length of the second lens with respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (4) is exceeded, the power of the second lens is insufficient so that chromatic aberration cannot be adequately corrected. If, on the contrary, the upper limit is exceeded, the focal length of the second lens is too small. This not only makes it difficult to correct spherical aberration and coma aberration, but also decreases manufacturing error sensitivity.

The image pickup lens described in aspect 7 of the invention is configured so that the fourth lens and the fifth lens satisfy conditional expressions (5) and (6) below:

$$0.9 < f4/f < 1.50 \quad (5)$$

$$-1.70 < f5/f < -0.85 \quad (6)$$

where f is the composite focal length of lenses included in the entire image pickup lens, $f4$ is the focal length of the fourth lens, and $f5$ is the focal length of the fifth lens.

Conditional expression (5) above defines the range of the focal length of the fourth lens with respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (5) is exceeded, the focal length of the fourth lens is too small. This makes it difficult to correct astigmatism and coma aberration, and decreases the manufacturing error sensitivity. If, on the contrary, the upper limit is exceeded, chromatic aberration of magnification and astigmatism are not adequately corrected so that expected performance is not obtained.

Conditional expression (6) above defines the range of the focal length of the fifth lens with respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (6) is exceeded, the power of the fifth lens is insufficient. This makes it difficult to decrease the optical length. If, on the contrary, the upper limit is exceeded, it is difficult to decrease the CRA, thereby decreasing the manufacturing error sensitivity at low image height.

The image pickup lens described in aspect 8 of the invention is configured so that the first lens and the third lens satisfy conditional expression (7) below:

$$-0.15 < f1/f3 < 0.37 \quad (7)$$

where $f1$ is the focal length of the first lens, and $f3$ is the focal length of the third lens.

Conditional expression (7) above defines the ratio between the focal length of the first lens and the focal length of the third lens. If the lower limit indicated by conditional expression (7) is exceeded, the focal length of the third lens is negative and too small. This makes it difficult to provide aberration correction. If, on the contrary, the upper limit is exceeded, the focal length of the third lens is positive and too small. This impairs the balance between astigmatism and coma aberration and decreases the manufacturing error sensitivity.

The image pickup lens described in aspect 9 of the invention is configured so that the second lens, the third lens, and the fourth lens satisfy conditional expression (8) below:

$$0.0 < f2 \cdot 3 \cdot 4 \quad (8)$$

where $f2 \cdot 3 \cdot 4$ is the composite focal length of the second, third, and fourth lenses.

Conditional expression (8) above defines the composite focal length of the second, third, and fourth lens. If the lower limit indicated by conditional expression (8) is exceeded, the negative power of the second lens is too strong so that the manufacturing error sensitivity is excessively low, or the positive power of the fourth lens is too weak so that it is difficult to correct astigmatism and distortion.

The image pickup lens described in aspect 10 of the invention is configured so that the first lens, the second lens, the third lens, the fourth lens, and the fifth lens satisfy conditional expressions (9), (10), and (11) below:

$$f1 < |f2| < |f3| \quad (9)$$

$$f1 < f4 < |f3| \quad (10)$$

$$f1 < |f5| < |f3| \quad (11)$$

where $f1$ is the focal length of the first lens, $f2$ is the focal length of the second lens, $f3$ is the focal length of the third lens, $f4$ is the focal length of the fourth lens, and $f5$ is the focal length of the fifth lens.

Conditional expression (9) above defines the power relationship, that is, the focal length relationship, between the first lens, the second lens, and the third lens. If the lower limit indicated by conditional expression (9) is exceeded, the

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negative power of the second lens is too strong. This increases the optical length and decreases the manufacturing error sensitivity. If, on the contrary, the upper limit is exceeded, the power of the third lens is too strong so that it is difficult to obtain adequate off-axis performance.

Conditional expression (10) above defines the power relationship, that is, the focal length relationship, between the first lens, the third lens, and the fourth lens. If the lower limit indicated by conditional expression (10) is exceeded, the power of the fourth lens is too strong. This increases the optical length and makes it difficult to correct astigmatism and distortion. If, on the contrary, the upper limit is exceeded, the power of the third lens is too strong so that it is difficult to obtain adequate off-axis performance.

Conditional expression (11) above defines the power relationship, that is, the focal length relationship, between the first lens, the third lens, and the fifth lens. If the lower limit indicated by conditional expression (11) is exceeded, the negative power of the fifth lens is too strong. This makes it difficult to correct coma aberration and astigmatism. If, on the contrary, the upper limit is exceeded, the power of the third lens is too strong so that it is difficult to obtain adequate off-axis performance.

The third lens has a weaker power than the other lenses. However, its front and rear aspherical surfaces effectively work to reduce an aberration caused within the second lens. Particularly, its fourth-order aspherical coefficient effectively works and plays an important role to exhibit performance characteristics specific to a combination of five lenses.

The image pickup lens described in aspect 11 of the invention is configured so that the curvature radius of the first lens satisfies conditional expression (12) below:

$$-0.40 < r1/r2 < 0.10 \quad (12)$$

where $r1$ is the curvature radius of the object-side surface of the first lens, and $r2$ is the curvature radius of the image-side surface of the first lens.

Conditional expression (12) above defines the lens shape of the first lens. If the lower limit indicated by conditional expression (12) is exceeded, the optical length cannot be readily reduced. In addition, the error sensitivity prevailing during the manufacture of the first lens becomes low. If, on the contrary, the upper limit is exceeded, it is difficult to maintain a proper aberration balance so that expected performance is not obtained.

The image pickup lens described in aspect 12 of the invention is configured so that the curvature radius of the fourth lens satisfies conditional expression (13) below:

$$1.4 < r7/r8 < 3.0 \quad (13)$$

where $r7$ is the curvature radius of the object-side surface of the fourth lens, and $r8$ is the curvature radius of the image-side surface of the fourth lens.

Conditional expression (13) above defines the lens shape of the fourth lens. If the lower limit indicated by conditional expression (13) is exceeded, the power of the fourth lens is too weak. Consequently, performance deterioration occurs because it is difficult to correct various aberrations. If, on the contrary, the upper limit is exceeded, the fourth lens has an excessively strong power or has a small degree of meniscus curvature. In this instance, too, it is difficult to maintain a proper aberration balance so that expected performance is not obtained.

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The image pickup lens described in aspect 13 of the invention is configured so that its image pickup optical system's optical length and focal length satisfy conditional expression (14) below:

$$1.05 < L/f < 1.30 \quad (14)$$

where L is the distance between the front surface of the first lens and the image surface, and f is the composite focal length of lenses included in the entire image pickup lens.

Conditional expression (14) above defines the optical length with respect to the focal length. If the lower limit indicated by conditional expression (14) is exceeded, it is difficult to correct various aberrations due to an excessively decreased optical length. In addition, the manufacturing error sensitivity becomes excessively low. If, on the contrary, the upper limit is exceeded, it is difficult to reduce the thickness of the image pickup lens due to an excessively increased optical length.

The image pickup lens described in claim 14 of the invention is configured so that the diameter of the aperture stop satisfies conditional expression (15) below:

$$0.30 < CA1/f < 0.50 \quad (15)$$

where $CA1$ is the diameter of the aperture stop, and f is the composite focal length of lenses included in the entire image pickup lens.

Conditional expression (15) above defines the F-number (Fno), which is an indication of lens brightness. If the lower limit indicated by conditional expression (15) is exceeded, the F-number is excessively great so that requested brightness is not achieved in most cases. If, on the contrary, the upper limit is exceeded, the F-number is excessively small or the distance between an aperture stop (F-number light flux restriction plate) and the front surface of the first lens is excessively great. In either of these cases, expected optical performance is not obtained.

Effects of the Invention

The image pickup lens according to the present invention includes five lenses (the first to fifth lenses). Further, the third lens plays a role that is not found in a conventional four-lens configuration. Therefore, the present invention makes it possible to provide a high-performance, low-cost, compact lens in which various aberrations are properly corrected to support large-size, high-resolution image pickup elements having highly minute pixels.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross-sectional view of an image pickup lens according to a first embodiment of the present invention.

FIG. 2 shows various aberrations of the image pickup lens according to the first embodiment of the present invention.

FIG. 3 is a cross-sectional view of the image pickup lens according to a second embodiment of the present invention.

FIG. 4 shows various aberrations of the image pickup lens according to the second embodiment of the present invention.

FIG. 5 is a cross-sectional view of the image pickup lens according to a third embodiment of the present invention.

FIG. 6 shows various aberrations of the image pickup lens according to the third embodiment of the present invention.

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FIG. 7 is a cross-sectional view of the image pickup lens according to a fourth embodiment of the present invention.

FIG. 8 shows various aberrations of the image pickup lens according to the fourth embodiment of the present invention.

FIG. 9 is a cross-sectional view of the image pickup lens according to a fifth embodiment of the present invention.

FIG. 10 shows various aberrations of the image pickup lens according to the fifth embodiment of the present invention.

FIG. 11 is a cross-sectional view of the image pickup lens according to a sixth embodiment of the present invention.

FIG. 12 shows various aberrations of the image pickup lens according to the sixth embodiment of the present invention.

BEST MODE FOR CARRYING OUT THE INVENTION

Embodiments of the present invention will now be described by using concrete numerical values. In the first to sixth embodiments, the image pickup lens for a solid-state image pickup element includes, in the order from the object side, an aperture stop S, a first lens L1, a second lens L2, a third lens L3, a fourth lens L4, a fifth lens L5, a plane-parallel glass plate IR, and an image surface.

In the first to sixth embodiments, the second lens L2, the third lens L3, the fourth lens L4, and the fifth lens L5 are

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vertex of a plane is regarded as the origin, the Z-axis is oriented in the direction of an optical axis, and the height measured perpendicularly to the optical axis is h:

$$Z=(h^2/r)/[1+\{1-(1+K)(h^2/r^2)\}^{1/2}]+A_4h^4+A_6h^6+A_8h^8+\dots$$

It should be noted that the following symbols are used in the above aspherical surface formula and in the description of each embodiment:

A_i: ith-order aspherical coefficient

r: Curvature radius

K: Conical constant

f: Focal length of the entire image pickup lens

F: F-number

d: On-axis surface spacing

nd: Refractive index of a lens material relative to d-line

v: Abbe number of a lens material

In the subsequent description, the exponent of 10 (e.g., 4.5×10⁻⁰⁴) is expressed by using the letter E (e.g., 4.5E-04), and surface numbers for lens data are sequentially assigned so that, for example, the object-side surface of the first lens L1 is surface 1.

First Embodiment

Table 1 shows numerical data about the image pickup lens according to the first embodiment. FIG. 1 is a cross-sectional view of the image pickup lens. FIG. 2 shows various aberrations.

TABLE 1

Surface Number	r	d	nd	v	K
1 (S)	2.297	0.550	1.5247	56.26	0.175
2	8384.615	0.411			0
3	-6.170	0.299	1.6142	25.58	2.471
4	8.586	0.242			0
5	2.383	0.481	1.5247	56.26	-7.218
6	3.460	0.658			-1.443
7	-2.320	0.815	1.5094	56.00	-0.455
8	-1.502	0.217			-0.645
9	2.288	0.897	1.5094	56.00	-3.909
10	1.274	0.714			-3.515
11	∞	0.300	1.5168	64.20	
12	∞	0.635			

Surface Number	A4	A6	A8	A10	A12	A14	A16
1 (S)	-5.423E-3	-2.923E-3	-1.511E-2	2.424E-3	-1.233E-2	3.275E-3	4.002E-3
2	8.525E-3	-2.136E-2	-1.410E-2	-1.071E-2	3.924E-3	0	0
3	1.427E-1	-1.124E-1	5.307E-2	-1.649E-2	-1.541E-2	1.183E-2	0
4	9.163E-2	-4.267E-2	9.557E-3	1.336E-2	-1.497E-2	5.154E-3	0
5	-4.203E-2	-4.711E-3	-2.518E-3	2.523E-3	0	0	0
6	-4.458E-2	-3.915E-3	-4.687E-4	4.421E-4	0	0	0
7	5.934E-2	-4.778E-2	2.552E-2	-7.375E-3	9.592E-4	0	0
8	2.946E-2	-6.592E-3	-1.052E-3	1.407E-3	-1.257E-4	0	0
9	-6.925E-2	1.547E-2	-1.984E-3	4.124E-5	2.050E-5	-1.537E-6	-5.993E-9
10	-4.400E-2	1.076E-2	-2.049E-3	2.486E-4	-1.983E-5	1.014E-6	-2.577E-8

f = 4.815 F = 2.8

so-called plastic lenses that have at least one aspherical surface and are made of a resin material. It should also be noted that the aperture stop S is positioned on the object side of the first lens L1.

The object-side surface and image-side surface of the fifth lens L5 have an aspherical shape that contains at least one inflection point between the center and the periphery of the lens. The aspherical shape in each embodiment is expressed by the following aspherical surface formula in which the

Second Embodiment

Table 2 shows numerical data about the image pickup lens according to the second embodiment. FIG. 3 is a cross-sectional view of the image pickup lens. FIG. 4 shows various aberrations.

TABLE 2

Surface Number	r	d	n d	v	K
1 (S)	2.035	0.605	1.497	81.60	0.145
2	-19.788	0.233			0
3	-4.221	0.295	1.6142	25.58	-1.602
4	13.376	0.341			0
5	3.098	0.486	1.5247	56.26	-11.308
6	4.140	0.731			0.271
7	-2.446	0.818	1.5247	56.26	-0.334
8	-1.493	0.239			-0.653
9	3.310	0.855	1.5247	56.26	-12.446
10	1.488	0.849			-4.788
11	∞	0.300	1.5168	64.20	
12	∞	0.803			

Surface Number	A4	A6	A8	A10	A12	A14	A16
1 (S)	-7.452E-3	-1.617E-4	-1.335E-2	4.383E-3	-9.221E-3	4.483E-3	-3.834E-3
2	1.998E-2	-2.240E-2	-1.467E-2	-1.152E-2	3.209E-3	0	0
3	1.470E-1	-1.118E-1	5.112E-2	-1.648E-2	-1.373E-2	1.325E-2	0
4	9.526E-2	-4.060E-2	1.128E-2	1.414E-2	-1.462E-2	5.794E-3	0
5	-4.356E-2	-4.909E-3	-2.662E-3	2.513E-3	0	0	0
6	-4.106E-2	-3.596E-3	3.640E-7	6.811E-4	0	0	0
7	5.620E-2	-4.763E-2	2.579E-2	-7.309E-3	9.426E-4	0	0
8	3.109E-2	-6.202E-3	-9.889E-4	1.388E-3	-1.345E-4	0	0
9	-7.078E-2	1.540E-2	-1.993E-3	4.351E-5	2.090E-5	1.538E-6	-1.030E-8
10	-4.561E-2	1.071E-2	-2.036E-3	2.488E-4	-1.998E-5	9.963E-7	-2.502E-8

f = 5.372 F = 2.8

Third Embodiment

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Fourth Embodiment

Table 3 shows numerical data about the image pickup lens according to the third embodiment. FIG. 5 is a cross-sectional view of the image pickup lens. FIG. 6 shows various aberrations.

Table 4 shows numerical data about the image pickup lens according to the fourth embodiment. FIG. 7 is a cross-sectional view of the image pickup lens. FIG. 8 shows various aberrations.

TABLE 3

Surface Number	r	d	n d	v	K
1 (S)	2.093	0.608	1.5441	56.00	0.123
2	-25.611	0.211			0
3	-4.074	0.307	1.5850	30.00	-1.357
4	11.977	0.336			0
5	3.166	0.478	1.5441	56.00	-11.659
6	4.064	0.731			0.351
7	-2.478	0.790	1.5247	56.26	-0.290
8	-1.540	0.274			-0.648
9	3.353	0.859	1.5247	56.26	-12.746
10	1.488	0.794			-4.901
11	∞	0.300	1.5168	64.20	
12	∞	0.713			

Surface Number	A4	A6	A8	A10	A12	A14	A16
1 (S)	-8.004E-3	4.932E-5	-1.335E-2	4.345E-3	-9.202E-3	4.586E-3	-3.708E-3
2	1.747E-2	-2.375E-2	-1.468E-2	-1.094E-2	3.436E-3	0	0
3	1.466E-1	-1.114E-1	5.110E-2	-1.663E-2	-1.384E-2	1.328E-2	0
4	9.639E-2	-4.030E-2	1.113E-2	1.390E-2	-1.439E-2	5.879E-3	0
5	-4.371E-2	-5.274E-3	-3.020E-3	2.317E-3	0	0	0
6	-4.084E-2	-3.546E-3	-2.715E-5	7.200E-4	0	0	0
7	5.558E-2	-4.774E-2	2.575E-2	-7.317E-3	9.431E-4	0	0
8	3.087E-2	-6.449E-3	-1.021E-3	1.386E-3	-1.344E-4	0	0
9	-7.043E-2	1.531E-2	-2.006E-3	4.195E-5	2.091E-5	-1.493E-6	8.400E-10
10	-4.574E-2	1.069E-2	-2.047E-3	2.484E-4	-1.994E-5	1.002E-6	-2.527E-8

f = 5.269 F = 2.8

TABLE 4

Surface Number	r	d	n d	v	K
1 (S)	2.119	0.626	1.5441	56.00	0.177
2	-11.544	0.208			0
3	-3.147	0.298	1.5850	30.00	-5.094
4	9.796	0.373			0
5	2.701	0.428	1.5441	56.00	-11.168
6	3.842	0.837			0.129
7	-2.253	0.750	1.5247	56.26	-0.654
8	-1.467	0.401			-0.694
9	1.656	0.587	1.5247	56.26	-10.501
10	0.981	0.874			-4.578
11	∞	0.300	1.5168	64.20	
12	∞	0.742			

Surface Number	A4	A6	A8	A10	A12	A14	A16
1 (S)	-7.510E-3	1.743E-3	-1.246E-2	5.493E-3	-8.377E-3	4.978E-3	-3.500E-3
2	2.507E-2	-1.481E-2	-1.129E-2	-1.181E-2	3.172E-3	0	0
3	1.526E-1	-1.113E-1	5.074E-2	-1.533E-2	-1.395E-2	1.133E-2	0
4	9.710E-2	-4.050E-2	1.124E-2	1.365E-2	-1.474E-2	5.407E-3	0
5	-3.599E-2	-8.738E-3	-4.179E-3	2.048E-3	0	0	0
6	-4.051E-2	-4.801E-3	-6.520E-4	5.650E-4	0	0	0
7	6.564E-2	-4.702E-2	2.607E-2	-7.359E-3	8.648E-4	0	0
8	3.490E-2	-3.356E-3	-1.098E-3	1.296E-3	-1.421E-4	0	0
9	-7.077E-2	1.589E-2	-1.963E-3	4.145E-5	2.045E-5	-1.557E-6	-2.866E-9
10	-5.003E-2	1.088E-2	-1.968E-3	2.477E-4	-2.068E-5	9.622E-7	-1.548E-8

f = 5.187 F = 2.7

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Fifth Embodiment

Table 5 shows numerical data about the image pickup lens according to the fifth embodiment. FIG. 9 is a cross-sectional view of the image pickup lens. FIG. 10 shows various aberrations.

Sixth Embodiment

Table 6 shows numerical data about the image pickup lens according to the sixth embodiment. FIG. 11 is a cross-sectional view of the image pickup lens. FIG. 12 shows various aberrations.

TABLE 5

Surface Number	r	d	n d	v	K
1 (S)	1.974	0.720	1.5311	5600	0.260
2	-14.375	0.150			0
3	-4.100	0.350	1.6142	25.58	1.248
4	55.800	0.360			0
5	5.600	0.340	1.5311	56.00	-20.645
6	3.868	0.750			1.356
7	-3.010	0.820	1.5311	56.00	-0.508
8	-1.634	0.270			-0.656
9	4.156	0.880	1.5311	56.00	-29.637
10	1.582	0.830			-5.617
11	∞	0.300	1.5168	64.20	
12	∞	0.770			

Surface Number	A4	A6	A8	A10	A12	A14	A16
1 (S)	-6.011E-3	4.555E-3	-1.140E-2	5.896E-3	-7.660E-3	5.633E-3	-3.706E-3
2	3.346E-2	-2.148E-2	-1.342E-2	-1.061E-2	3.525E-3	0	0
3	1.407E-1	-1.057E-1	4.976E-2	-1.790E-2	-1.431E-2	1.182E-2	0
4	1.000E-1	-4.704E-2	1.326E-2	1.542E-2	-1.468E-2	5.766E-3	0
5	-5.387E-2	-6.340E-3	-1.971E-3	2.628E-3	0	0	0
6	-4.023E-2	2.476E-4	1.005E-3	6.170E-4	0	0	0
7	5.679E-2	-4.556E-2	2.594E-2	-7.443E-3	8.944E-4	0	0
8	3.073E-2	-5.791E-3	-8.590E-4	1.367E-3	-1.517E-4	0	0
9	-6.996E-2	1.530E-2	-1.966E-3	5.619E-5	2.207E-5	-1.613E-6	-4.417E-8
10	-4.594E-2	1.064E-2	-2.039E-3	2.506E-4	-2.003E-5	9.526E-7	-2.202E-8

f = 5.700 F = 2.8

TABLE 6

Surface Number	r	d	n d	v	K
1 (S)	2.084	0.604	1.5311	56.00	0.168
2	-21.296	0.222			0
3	-3.958	0.300	1.6142	25.58	-1.423
4	13.768	0.323			0
5	3.075	0.497	1.5311	56.00	-11.809
6	4.139	0.624			0.275
7	-2.412	0.870	1.5247	56.26	-0.378
8	-1.484	0.208			-0.649
9	3.407	0.955	1.5247	56.26	-5.620
10	1.561	0.802			-4.276
11	∞	0.300	1.5168	64.20	
12	∞	0.674			

Surface Number	A4	A6	A8	A10	A12	A14	A16
1 (S)	-6.789E-3	2.618E-4	-1.386E-2	3.682E-3	-9.711E-3	4.535E-3	-2.955E-3
2	1.842E-2	-2.358E-2	-1.510E-2	-1.166E-2	3.030E-3	0	0
3	1.465E-1	-1.117E-1	5.082E-2	-1.681E-2	-1.391E-2	1.334E-2	0
4	9.611E-2	-4.021E-2	1.153E-2	1.421E-2	-1.461E-2	5.550E-3	0
5	-4.518E-2	-5.504E-3	-2.914E-3	2.385E-3	0	0	0
6	-4.104E-2	-3.503E-3	-5.896E-5	6.932E-4	0	0	0
7	5.684E-2	-4.751E-2	2.584E-2	-7.290E-3	9.508E-4	0	0
8	3.092E-2	-6.249E-3	-1.018E-3	1.379E-3	-1.373E-4	0	0
9	-6.971E-2	1.550E-2	-1.986E-3	4.363E-5	2.079E-5	-1.571E-6	-1.765E-8
10	-4.447E-2	1.070E-2	-2.036E-3	2.489E-4	-1.996E-5	1.000E-6	-2.448E-8

f = 4.986 F = 2.8

Table 7 below relates to the first to sixth embodiments and shows values for conditional expressions (1) to (17) below.

Conditional expression (1) concerns the Abbe number of a material used for the first lens L1. Conditional expression (2) concerns the Abbe number of a material used for the second lens L2.

$$45 < v_1 < 90 \quad \text{Conditional expression (1)}$$

$$22 < v_2 < 35 \quad \text{Conditional expression (2)}$$

where v_1 is the Abbe number for d-line of the first lens, and v_2 is the Abbe number for d-line of the second lens.

Conditional expression (3) defines the range of the focal length of the first lens L1 with respect to the focal length of the entire image pickup lens. Conditional expression (4) defines the range of the focal length of the second lens L2 with respect to the focal length of the entire image pickup lens.

$$0.5 < f_1/f < 1.00 \quad \text{Conditional expression (3)}$$

$$-1.50 < f_2/f < -0.65 \quad \text{Conditional expression (4)}$$

where f is the composite focal length of lenses included in the entire image pickup lens, f_1 is the focal length of the first lens, and f_2 is the focal length of the second lens.

Conditional expression (5) defines the range of the focal length of the fourth lens L4 with respect to the focal length of the entire image pickup lens. Conditional expression (6) defines the range of the focal length of the fifth lens L5 with respect to the focal length of the entire image pickup lens.

$$0.9 < f_4/f < 1.50 \quad \text{Conditional expression (5)}$$

$$-1.70 < f_5/f < -0.85 \quad \text{Conditional expression (6)}$$

where f is the composite focal length of lenses included in the entire image pickup lens, f_4 is the focal length of the fourth lens, and f_5 is the focal length of the fifth lens.

Conditional expression (7) defines the ratio between the focal length of the first lens L1 and the focal length of the third lens L3.

$$-0.15 < f_1/f_3 < 0.37 \quad \text{Conditional expression (7)}$$

where f_1 is the focal length of the first lens, and f_3 is the focal length of the third lens.

Conditional expression (8) defines the composite focal length of the second lens L2, the third lens L3, and the fourth lens L4.

$$0.0 < f_2 \cdot 3 < 4 \quad \text{Conditional expression (8)}$$

Conditional expression (9) defines the power relationship, that is, the focal length relationship, between the first lens L1, the second lens L2, and the third lens L3. Conditional expression (10) defines the power relationship, that is, the focal length relationship, between the first lens L1, the third lens L3, and the fourth lens L4. Conditional expression (11) defines the power relationship, that is, the focal length relationship, between the first lens L1, the third lens L3, and the fifth lens L5.

$$f_1 < |f_2| < |f_3| \quad \text{Conditional expression (9)}$$

$$f_1 < f_4 < |f_3| \quad \text{Conditional expression (10)}$$

$$f_1 < |f_5| < |f_3| \quad \text{Conditional expression (11)}$$

Conditional expression (12) defines the lens shape of the first lens L1.

$$-0.40 < r_1/r_2 < 0.10 \quad \text{Conditional expression (12)}$$

where r_1 is the curvature radius of the object-side surface of the first lens, and r_2 is the curvature radius of the image-side surface of the first lens.

Conditional expression (13) defines the lens shape of the fourth lens L4.

$$1.4 < r_7/r_8 < 3.0 \quad \text{Conditional expression (13)}$$

where r_7 is the curvature radius of the object-side surface of the fourth lens, and r_8 is the curvature radius of the image-side surface of the fourth lens.

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Conditional expression (14) defines the optical length with respect to the focal length.

$$1.05 < L/f < 1.30 \quad \text{Conditional expression (14)}$$

where L is the distance between the front surface of the first lens and the image surface, and f is the composite focal length of lenses included in the entire image pickup lens.

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Conditional expression (17) defines the lens shape of the fourth lens L4 and relates to a case where conditions more stringent than those defined by conditional expression (13) are satisfied.

$$1.45 < r7/r8 < 2.0 \quad \text{Conditional expression (17)}$$

where r7 is the curvature radius of the object-side surface of the fourth lens, and r8 is the curvature radius of the image-side surface of the fourth lens.

TABLE 7

	First Embodiment	Second Embodiment	Third Embodiment	Fourth Embodiment	Fifth Embodiment	Sixth Embodiment
Conditional Expression (1)	56.26	81.60	56.00	56.00	56.00	56.00
Conditional Expression (2)	25.58	25.58	30.00	30.00	25.58	25.58
Conditional Expression (3)	0.909	0.698	0.680	0.645	0.582	0.723
Conditional Expression (4)	-1.205	-0.966	-0.979	-0.778	-1.089	-0.997
Conditional Expression (5)	1.300	1.050	1.141	1.163	0.978	1.115
Conditional Expression (6)	-1.671	-1.144	-1.150	-1.262	-0.957	-1.340
Conditional Expression (7)	0.346	0.185	0.162	0.226	-0.131	0.186
Conditional Expression (8)	10.266	10.597	13.323	15.698	18.816	10.806
Conditional Expression (9)						
f 1	4.379	3.747	3.584	3.344	3.319	3.606
f 2	5.800	5.191	5.160	4.037	6.205	4.973
f 3	12.647	20.214	22.174	14.764	25.268	19.382
Conditional Expression (10)						
f 1	4.379	3.747	3.584	3.344	3.319	3.606
f 4	6.258	5.638	6.011	6.033	5.577	5.558
f 3	12.647	20.214	22.174	14.764	25.268	19.382
Conditional Expression (11)						
f 1	4.379	3.747	3.584	3.344	3.319	3.606
f 5	8.045	6.144	6.059	6.546	5.457	6.680
f 3	12.647	20.214	22.174	14.764	25.268	19.382
Conditional Expression (12)	0.000	-0.103	-0.082	-0.184	-0.137	-0.098
Conditional Expression (13)	1.545	1.638	1.609	1.536	1.842	1.625
Conditional Expression (14)	1.292	1.220	1.215	1.238	1.147	1.279
Conditional Expression (15)	0.357	0.355	0.357	0.385	0.355	0.355

Conditional expression (15) defines the F-number (Fno), which is an indication of lens brightness.

$$0.30 < CA1/f < 0.50 \quad \text{Conditional expression (15)}$$

where CA1 is the diameter of the aperture stop, and f is the composite focal length of lenses included in the entire image pickup lens.

Conditional expression (16) defines the range of the focal length of the second lens L2 with respect to the focal length of the entire image pickup lens, and relates to a case where conditions more stringent than those defined by conditional expression (4) are satisfied.

$$-1.30 < f2/f < -0.75 \quad \text{Conditional expression (16)}$$

where f is the composite focal length of lenses included in the entire image pickup lens, and f2 is the focal length of the second lens.

As shown in Table 7, the first to sixth embodiments of the present invention satisfy all of conditional expressions (1) to (17). Conditional expressions (1) and (2) define the Abbe number of the first lens L1 or the second lens L2. If the lower limit indicated by conditional expression (1) or (2) is exceeded, the variance value difference from the second lens L2 is decreased so that chromatic aberration correction is insufficient. If, on the contrary, the upper limit is exceeded, the balance between axial chromatic aberration and chromatic aberration of magnification is impaired so that performance deterioration occurs at the periphery of the image area. However, when conditional expressions (1) and (2) are satisfied, a proper balance is maintained between axial chromatic aberration and chromatic aberration of magnification. This makes it possible to prevent performance deterioration at the periphery of the image area and provide excellent chromatic aberration correction.

Conditional expressions (3) and (4) define the range of the focal length of the first lens L1 or the second lens L2 with

respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (3) is exceeded, the focal length of the first lens L1 is too small. This makes it difficult to correct spherical aberration and coma aberration. If, on the contrary, the upper limit is exceeded, the optical length is too great so that the thickness of the image pickup lens cannot be sufficiently reduced. If the lower limit indicated by conditional expression (4) is exceeded, the power of the second lens L2 is insufficient so that chromatic aberration cannot be adequately corrected. If, on the contrary, the upper limit is exceeded, the focal length of the second lens L2 is too small. This makes it difficult to correct spherical aberration and coma aberration, and decreases manufacturing error sensitivity. However, when conditional expressions (3) and (4) are satisfied, it is possible to properly correct spherical aberration and coma aberration. Further, the power of the second lens L2 becomes sufficient, making it possible to properly correct chromatic aberration, spherical aberration, and coma aberration.

Conditional expression (5) defines the range of the focal length of the fourth lens L4 with respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (5) is exceeded, the focal length of the fourth lens L4 is too small. This makes it difficult to correct astigmatism and coma aberration, and decreases the manufacturing error sensitivity. If, on the contrary, the upper limit is exceeded, chromatic aberration of magnification and astigmatism are not adequately corrected so that expected performance is not obtained. However, when conditional expression (5) is satisfied, it is easy to correct astigmatism, coma aberration, and chromatic aberration of magnification. This makes it possible to obtain expected performance.

Conditional expression (6) defines the range of the focal length of the fifth lens L5 with respect to the focal length of the entire image pickup lens. If the lower limit indicated by conditional expression (6) is exceeded, the power of the fifth lens L5 is insufficient. This makes it difficult to decrease the optical length. If, on the contrary, the upper limit is exceeded, it is difficult to decrease the CRA, thereby decreasing the manufacturing error sensitivity at low image height. However, when conditional expression (6) is satisfied, the fifth lens L5 has a sufficient power, making it possible to reduce the optical length. This makes it easy to decrease the CRA so that the manufacturing error sensitivity at low image height increases.

Conditional expression (7) defines the ratio between the focal length of the first lens L1 and the focal length of the third lens L3. If the lower limit indicated by conditional expression (7) is exceeded, the focal length of the third lens L3 is negative and too small. This makes it difficult to provide aberration correction. If, on the contrary, the upper limit is exceeded, the focal length of the third lens L3 is positive and too small. This impairs the balance between astigmatism and coma aberration and decreases the manufacturing error sensitivity. However, when conditional expression (7) is satisfied, it is easy to provide aberration correction. Further, it is possible not only to prevent the focal length of the third lens L3 from being positive and too small, but also to maintain an excellent balance between astigmatism and coma aberration.

Conditional expression (8) defines the composite focal length of the second lens L2, the third lens L3, and the fourth lens L4. If the lower limit indicated by conditional expression (8) is exceeded, the negative power of the second lens L2 is too strong so that the manufacturing error sensitivity is excessively low, or the positive power of the fourth lens L4 is too weak so that it is difficult to correct astigmatism

and distortion. However, when conditional expression (8) is satisfied, it is easy to correct astigmatism and distortion.

Conditional expression (9) defines the power relationship, that is, the focal length relationship, between the first lens L1, the second lens L2, and the third lens L3. If the lower limit indicated by conditional expression (9) is exceeded, the negative power of the second lens L2 is too strong. This increases the optical length and decreases the manufacturing error sensitivity. If, on the contrary, the upper limit is exceeded, the power of the third lens is too strong so that it is difficult to obtain adequate off-axis performance. However, when conditional expression (9) is satisfied, it is possible to decrease the optical length and easily obtain adequate off-axis performance.

Conditional expression (10) defines the power relationship, that is, the focal length relationship, between the first lens L1, the third lens L3, and the fourth lens L4. If the lower limit indicated by conditional expression (10) is exceeded, the power of the fourth lens L4 is too strong. This increases the optical length and makes it difficult to correct astigmatism and distortion. If, on the contrary, the upper limit is exceeded, the power of the third lens L3 is too strong so that it is difficult to obtain adequate off-axis performance. However, when conditional expression (10) is satisfied, it is easy to correct astigmatism and distortion and obtain adequate off-axis performance.

Conditional expression (11) defines the power relationship, that is, the focal length relationship, between the first lens L1, the third lens L3, and the fifth lens L5. If the lower limit indicated by conditional expression (11) is exceeded, the negative power of the fifth lens L5 is too strong. This makes it difficult to correct coma aberration and astigmatism. If, on the contrary, the upper limit is exceeded, the power of the third lens L3 is too strong so that it is difficult to obtain adequate off-axis performance. However, when conditional expression (11) is satisfied, it is easy to correct coma aberration and astigmatism and obtain adequate off-axis performance.

Conditional expression (12) defines the lens shape of the first lens L1. If the lower limit indicated by conditional expression (12) is exceeded, the optical length cannot be readily reduced. In addition, the error sensitivity prevailing during the manufacture of the first lens L1 becomes low. If, on the contrary, the upper limit is exceeded, it is difficult to maintain a proper aberration balance so that expected performance is not obtained. However, when conditional expression (12) is satisfied, the optical length can be readily reduced. In addition, it is possible to maintain a proper aberration balance and obtain expected performance.

Conditional expression (13) defines the lens shape of the fourth lens L4. If the lower limit indicated by conditional expression (13) is exceeded, the power of the fourth lens L4 is too weak. Consequently, performance deterioration occurs because it is difficult to correct various aberrations. If, on the contrary, the upper limit is exceeded, the fourth lens L4 has an excessively strong power or has a small degree of meniscus curvature. In this instance, too, it is difficult to maintain a proper aberration balance so that expected performance is not obtained. However, when conditional expression (13) is satisfied, it is easy to correct various aberrations and maintain a proper aberration balance. As a result, expected performance is obtained.

Conditional expression (14) defines the optical length with respect to the focal length. If the lower limit indicated by conditional expression (14) is exceeded, it is difficult to correct various aberrations due to an excessively decreased optical length. In addition, the manufacturing error sensi-

tivity becomes excessively low. If, on the contrary, the upper limit is exceeded, it is difficult to reduce the thickness of the image pickup lens due to an excessively increased optical length. However, when conditional expression (14) is satisfied, it is easy to correct various aberrations. In addition, the thickness of the image pickup lens can be readily reduced because the optical length is not excessively small.

Conditional expression (15) defines the F-number (Fno), which is an indication of lens brightness. If the lower limit indicated by conditional expression (15) is exceeded, the F-number is excessively great so that requested brightness is not achieved in most cases. If, on the contrary, the upper limit is exceeded, the F-number is excessively small or the distance between the aperture stop (F-number light flux restriction plate) and the front surface of the first lens is excessively great. In either of these cases, expected optical performance is not obtained. However, when conditional expression (15) is satisfied, the expected optical performance can be obtained with ease.

Further, the second lens L2, the third lens L3, the fourth lens L4, and the fifth lens L5 are so-called plastic lenses that have at least one aspherical surface and are made of a resin material. Cost reduction can be achieved when at least the second lens L2, the third lens L3, the fourth lens L4, and the fifth lens L5 are made of an inexpensive resin material exhibiting high production efficiency.

Furthermore, as the aperture stop S is positioned on the object side of the first lens L1 to decrease the CRA (Chief Ray Angle), it is easy to reduce the CRA (Chief Ray Angle) and obtain sufficient light intensity at the periphery of the image surface at which light intensity decreases.

Moreover, as the object side surface and image side surface of the fifth lens L5 have an aspherical shape that contains at least one inflection point between the center and the periphery of the lens, it is possible to obtain adequate off axis performance and CRA.

While the present invention has been described in terms of exemplary embodiments, it should be understood that the invention is not limited to those exemplary embodiments. Those skilled in the art will understand that various changes and modifications can be made within the scope and spirit of the invention.

EXPLANATION OF REFERENCE NUMERALS AND SYMBOLS

L1	First lens
L2	Second lens
L3	Third lens
L4	Fourth lens
L5	Fifth lens
S	Aperture stop

The invention claimed is:

[1. An image pickup lens for a solid-state image pickup element, comprising, in the order from an object side:

a first lens, which has a convex surface facing the object side on an optical axis and has a positive refractive power;

a second lens, which has a concave surface facing an image side on the optical axis and has a negative refractive power;

a third lens, which has a convex surface facing the object side on the optical axis and has a meniscus shape;

a fourth lens, which has a convex surface facing the image side on the optical axis, has a positive refractive power, and has a meniscus shape; and

a fifth lens, which has a concave surface facing the image side on the optical axis, has a negative refractive power, and has a meniscus shape.]

[2. The image pickup lens according to claim 1, wherein the Abbe number of a material used for the first lens and the second lens satisfies conditional expressions (1) and (2) below:

$$45 < v_1 < 90 \quad (1)$$

$$22 < v_2 < 35 \quad (2)$$

where v_1 is the Abbe number for d-line of the first lens, and v_2 is the Abbe number for d-line of the second lens.]

[3. The image pickup lens according to claim 1, wherein the second lens, the third lens, the fourth lens, and the fifth lens are so-called plastic lenses that have at least one aspherical surface and are made of a resin material.]

[4. The image pickup lens according to claim 1, wherein an aperture stop is positioned on the object side of the first lens.]

[5. The image pickup lens according to claim 1, wherein the object-side surface and the image-side surface of the fifth lens have an aspherical shape that contains at least one inflection point between the center and the periphery of the lens.]

[6. The image pickup lens according to claim 1, wherein the first lens and the second lens satisfy conditional expressions (3) and (4) below:

$$0.5 < f_1/f < 1.00 \quad (3)$$

$$-1.50 < f_2/f < -0.65 \quad (4)$$

where f is the composite focal length of lenses included in the entire image pickup lens, f_1 is the focal length of the first lens, and f_2 is the focal length of the second lens.]

[7. The image pickup lens according to claim 1, wherein the fourth lens and the fifth lens satisfy conditional expressions (5) and (6) below:

$$0.9 < f_4/f < 1.50 \quad (5)$$

$$-1.70 < f_5/f < -0.85 \quad (6)$$

where f is the composite focal length of lenses included in the entire image pickup lens, f_4 is the focal length of the fourth lens, and f_5 is the focal length of the fifth lens.]

[8. The image pickup lens according to claim 1, wherein the first lens and the third lens satisfy conditional expression (7) below:

$$-0.15 < f_1/f_3 < 0.37 \quad (7)$$

where f_1 is the focal length of the first lens, and f_3 is the focal length of the third lens.]

[9. The image pickup lens according to claim 1, wherein the second lens, the third lens, and the fourth lens satisfy conditional expression (8) below:

$$0.0 < f_{2\cdot3\cdot4} \quad (8)$$

where $f_{2\cdot3\cdot4}$ is the composite focal length of the second, third, and fourth lenses.]

[10. The image pickup lens according to claim 1, wherein the first lens, the second lens, the third lens, the fourth lens, and the fifth lens satisfy conditional expressions (9), (10), and (11) below:

$$f_1 < |f_2| < |f_3| \quad (9)$$

$$f_1 < f_4 < |f_3| \quad (10)$$

$$f_1 < |f_5| < |f_3| \quad (11)$$

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where f_1 is the focal length of the first lens, f_2 is the focal length of the second lens, f_3 is the focal length of the third lens, f_4 is the focal length of the fourth lens, and f_5 is the focal length of the fifth lens.]

[11. The image pickup lens according to claim 10, wherein the curvature radius of the first lens satisfies conditional expression (12) below:

$$-0.40 < r_1/r_2 < 0.10 \quad (12)$$

where r_1 is the curvature radius of the object-side surface of the first lens, and r_2 is the curvature radius of the image-side surface of the first lens.]

[12. The image pickup lens according claim 10, wherein the curvature radius of the fourth lens satisfies conditional expression (13) below:

$$1.4 < r_7/r_8 < 3.0 \quad (13)$$

where r_7 is the curvature radius of the object-side surface of the fourth lens, and r_8 is the curvature radius of the image-side surface of the fourth lens.]

[13. The image pickup lens according to claim 10, wherein the optical length and focal length of an optical system thereof satisfy conditional expression (14) below:

$$1.05 < L/f < 1.30 \quad (14)$$

where L is the distance between the front surface of the first lens and an image surface, and f is the composite focal length of lenses included in the entire image pickup lens.]

[14. The image pickup lens according to claim 4, wherein the diameter of the aperture stop satisfies conditional expression (15) below:

$$0.30 < CA_1/f < 0.50 \quad (15)$$

where CA_1 is the diameter of the aperture stop, and f is the composite focal length of lenses included in the entire image pickup lens.]

[15. The image pickup lens according to claim 10, wherein the Abbe number of a material used for the first lens and the second lens satisfies conditional expressions (1) and (2) below:

$$45 < v_1 < 90 \quad (1)$$

$$22 < v_2 < 35 \quad (2)$$

where v_1 is the Abbe number for d-line of the first lens, and v_2 is the Abbe number for d-line of the second lens.]

[16. The image pickup lens according to claim 10, wherein the second lens, the third lens, the fourth lens, and the fifth lens are so-called plastic lenses that have at least one aspherical surface and are made of a resin material.]

[17. The image pickup lens according to claim 10, wherein an aperture stop is positioned on the object side of the first lens.]

[18. The image pickup lens according to claim 10, wherein the object-side surface and the image-side surface of the fifth lens have an aspherical shape that contains at least one inflection point between the center and the periphery of the lens.]

19. An image pickup lens for a solid-state image pickup element, comprising, in order from an object side:

a first lens, which has a convex surface facing the object side on an optical axis and has a positive refractive power;

a second lens;

a third lens;

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a fourth lens, which has a convex surface facing an image side on the optical axis; and

a fifth lens, which has a concave surface facing the image side on the optical axis and has a negative refractive power,

wherein the second lens, the third lens, the fourth lens, and the fifth lens are plastic lenses that have at least one aspherical surface and are made of a resin material,

each of the first lens, the second lens, the third lens, the fourth lens, and the fifth lens is positioned without being joined on surfaces facing each other, and

Abbe numbers of materials used for the first lens and the second lens satisfy conditional expressions (1) and (2) below:

$$45 < v_1 < 90 \quad (1)$$

$$22 < v_2 < 35 \quad (2)$$

where v_1 is an Abbe number for d-line of the first lens, and v_2 is an Abbe number for d-line of the second lens.

20. The image pickup lens according to claim 19, wherein the second lens has a concave surface facing the image side on the optical axis and has a negative refractive power.

21. The image pickup lens according to claim 19, wherein the third lens has a convex surface facing the object side on the optical axis and has a meniscus shape.

22. The image pickup lens according to claim 19, wherein the fourth lens has a meniscus shape and a positive refractive power.

23. The image pickup lens according to claim 19, wherein the fifth lens has a meniscus shape.

24. The image pickup lens according to claim 19, wherein an image-side surface of the fifth lens has an aspherical shape that contains at least one inflection point between a center and a periphery of the fifth lens.

25. The image pickup lens according to claim 19, wherein the first lens and the second lens satisfy conditional expressions (3) and (4) below:

$$0.5 < f_1/f < 1.00 \quad (3)$$

$$-1.50 < f_2/f < -0.65 \quad (4)$$

where f is a composite focal length of lenses included in an entirety of the image pickup lens, f_1 is a focal length of the first lens, and f_2 is a focal length of the second lens.

26. The image pickup lens according to claim 19, wherein the fourth lens and the fifth lens satisfy conditional expressions (5) and (6) below:

$$0.9 < f_4/f < 1.50 \quad (5)$$

$$-1.70 < f_5/f < -0.85 \quad (6)$$

where f is a composite focal length of lenses included in an entirety of the image pickup lens, f_4 is a focal length of the fourth lens, and f_5 is a focal length of the fifth lens.

27. The image pickup lens according to claim 19, wherein the first lens and the third lens satisfy a conditional expression (7) below:

$$-0.15 < f_1/f_3 < 0.37 \quad (7)$$

where f_1 is a focal length of the first lens, and f_3 is a focal length of the third lens.

28. The image pickup lens according to claim 19, wherein an optical length and focal length of an optical system thereof satisfy a conditional expression (14) below:

$$1.05 < L/f < 1.30 \quad (14)$$

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where L is a distance between a front surface of the first lens and an image surface, and f is a composite focal length of lenses included in an entirety of the image pickup lens.

29. An image pickup lens for a solid-state image pickup element, comprising, in order from an object side:

a first lens, which has a convex surface facing the object side on an optical axis and has a positive refractive power;

a second lens, which has a concave surface facing an image side on the optical axis and has a negative refractive power;

a third lens;

a fourth lens, which has a convex surface facing the image side on the optical axis; and

a fifth lens, which has a concave surface facing the image side on the optical axis and has a negative refractive power;

wherein the second lens, the third lens, the fourth lens, and the fifth lens are plastic lenses that have at least one aspherical surface and are made of a resin material, and

each of the first lens, the second lens, the third lens, the fourth lens, and the fifth lens is positioned without being joined on surfaces facing each other.

30. The image pickup lens according to claim 29, wherein the third lens has a convex surface facing the object side on the optical axis and has a meniscus shape.

31. The image pickup lens according to claim 29, wherein the fourth lens has a meniscus shape and a positive refractive power.

32. The image pickup lens according to claim 29, wherein the fifth lens has a meniscus shape.

33. The image pickup lens according to claim 29, wherein an image-side surface of the fifth lens has an aspherical shape that contains at least one inflection point between a center and a periphery of the fifth lens.

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34. The image pickup lens according to claim 29, wherein the first lens and the second lens satisfy conditional expressions (3) and (4) below:

$$0.5 < f1/f < 1.00 \quad (3)$$

$$-1.50 < f2/f < -0.65 \quad (4)$$

where f is a composite focal length of lenses included in an entirety of the image pickup lens, $f1$ is a focal length of the first lens, and $f2$ is a focal length of the second lens.

35. The image pickup lens according to claim 29, wherein the fourth lens and the fifth lens satisfy conditional expressions (5) and (6) below:

$$0.9 < f4/f < 1.50 \quad (5)$$

$$-1.70 < f5/f < -0.85 \quad (6)$$

where f is a composite focal length of lenses included in an entirety of the image pickup lens, $f4$ is a focal length of the fourth lens, and $f5$ is a focal length of the fifth lens.

36. The image pickup lens according to claim 29, wherein the first lens and the third lens satisfy a conditional expression (7) below:

$$-0.15 < f1/f3 < 0.37 \quad (7)$$

where $f1$ is a focal length of the first lens, and $f3$ is a focal length of the third lens.

37. The image pickup lens according to claim 29, wherein an optical length and focal length of an optical system thereof satisfy a conditional expression (14) below:

$$1.05 < L/f < 1.30 \quad (14)$$

where L is a distance between a front surface of the first lens and an image surface, and f is a composite focal length of lenses included in an entirety of the image pickup lens.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : RE46,455 E
APPLICATION NO. : 14/993854
DATED : June 27, 2017
INVENTOR(S) : Ise et al.

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

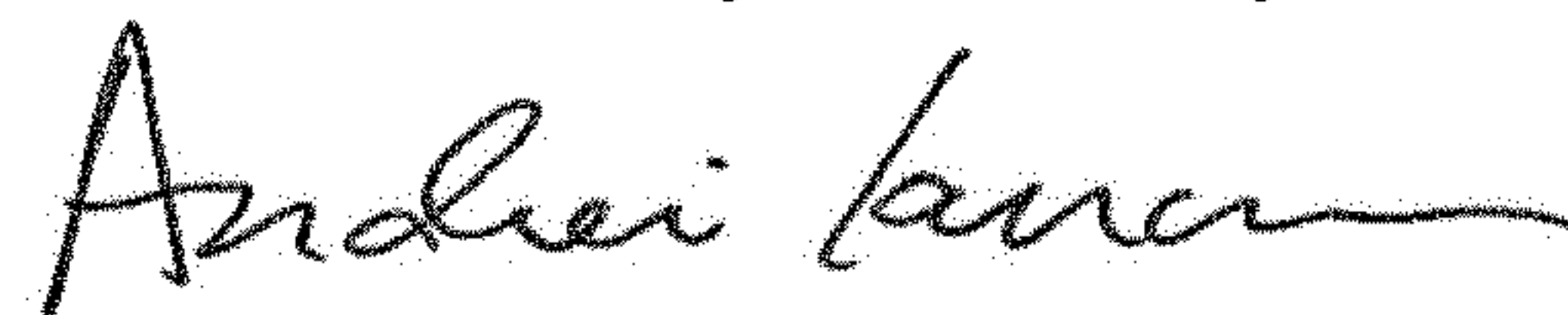
In the Specification

At Column 1, before the heading "TECHNICAL FIELD," please replace the paragraph at Lines 13-18 (approx.), with the following:

--CROSS REFERENCE TO RELATED APPLICATIONS

NOTICE: More than one reissue application has been filed for the reissue of U.S. Patent No. 8,422,145 B2. The reissue applications are U.S. Reissue Patent Application Serial Nos. 16/447,638, 16/447,629, 16/447,615, and 16/447,594, each filed on June 20, 2019, each of which ('638, '629, '615 and '594) is a continuation reissue application of U.S. Reissue Patent Application Serial No. 15/604,863, filed on May 25, 2017, now U.S. Reissue Patent No. RE47,516 E, issued July 16, 2019, which together with U.S. Reissue Patent Application Serial Nos. 15/605,034, 15/604,998, and 15/604,961, each filed on May 25, 2017, now U.S. Reissue Patent Nos. RE47,576 E, RE47,532 E, and RE47,517 E, respectively, issued August 20, 2019, July 23, 2019, and July 16, 2019, respectively, each of which ('863, '034, '998, and '961) is a continuation reissue application of U.S. Reissue Patent Application Serial No. 14/993,854 (the present application), filed on January 12, 2016, now U.S. Reissue Patent No. RE46,455 E, issued June 27, 2017, which together with U.S. Reissue Patent Application Serial No. 14/993,878, filed on January 12, 2016, now U.S. Reissue Patent No. RE46,595 E, issued October 31, 2017, each of which ('854 and '878) is a continuation reissue application of U.S. Reissue Patent Application Serial No. 14/684,878, filed on April 13, 2015, now U.S. Reissue Patent No. RE45,941 E, issued March 22, 2016, which is a reissue application of U.S. Patent Application Serial No. 13/203,159, filed on August 24, 2011, now U.S. Patent No. 8,422,145 B2, issued April 16, 2013, which is a national stage entry of International Patent Application No. PCT/JP2010/055048, filed on March 24, 2010,--

Signed and Sealed this
Nineteenth Day of January, 2021



Andrei Iancu
Director of the United States Patent and Trademark Office