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(54) **THERMOELECTRIC HEAT EXCHANGER**

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USPC **62/3.7**; 62/3.1; 62/3.2; 62/3.3; 62/259.3; 165/86; 310/58; 310/60 R; 310/61; 310/64

(58) **Field of Classification Search**
USPC 62/3.1-3.7, 259.3; 165/86; 310/58, 310/306, 60 R, 61-64
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,362,259 A 11/1944 Findley
2,363,168 A 11/1944 Findley

(Continued)

FOREIGN PATENT DOCUMENTS

DE 19503291 8/1996
DE 299 11 519 U1 11/2000

(Continued)

OTHER PUBLICATIONS

Search Report for PCT/US 99/10333, mailed Aug. 27, 1999.

(Continued)

Primary Examiner — Judy Swann

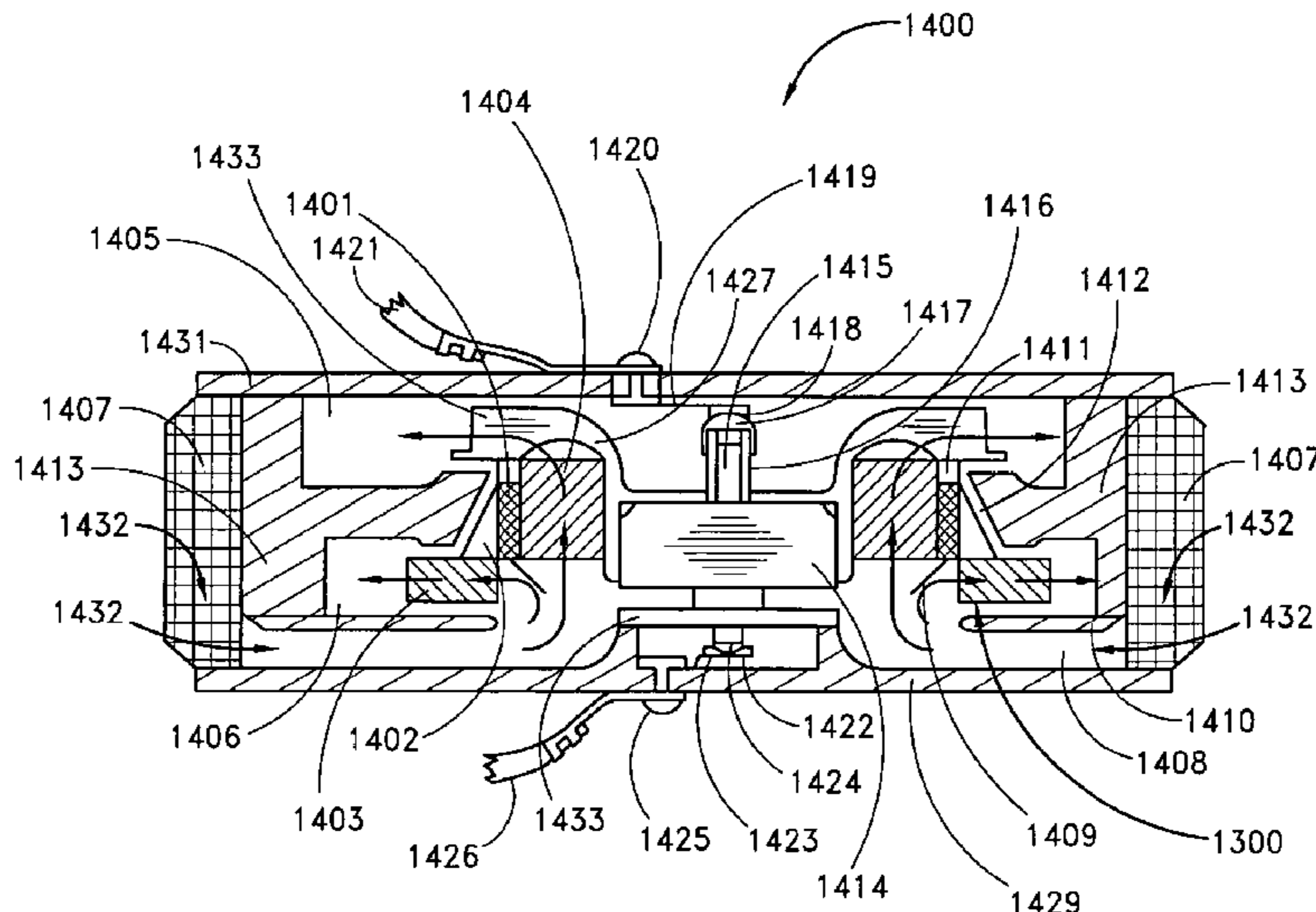
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(57) **ABSTRACT**

Disclosed is a system for thermally conditioning and pumping a fluid. The system includes a thermoelectric heat exchanger having a thermoelectric device configured to pump heat. Heat exchangers are provided for transferring heat to and from the thermoelectric device and for generating a fluid flow across the thermoelectric device. The conditioned fluid may be placed in thermal communication with a variety of objects, such as a vehicle seat, or anywhere localized heating and cooling are desired. Thermal isolation may also be provided in the direction of flow to enhance efficiency.

25 Claims, 19 Drawing Sheets



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U.S. PATENT DOCUMENTS							
2,519,241	A	8/1950	Findley	6,855,880	B2	2/2005	Feher
2,984,077	A	5/1961	Gaskill	6,857,697	B2	2/2005	Brennan et al.
3,019,609	A *	2/1962	Pietsch 62/3.3	6,893,086	B2	5/2005	Bajic et al.
3,085,405	A *	4/1963	Frantti 62/3.5	6,907,739	B2	6/2005	Bell
3,136,577	A	6/1964	Richard	6,954,944	B2	10/2005	Feher
3,137,142	A	6/1964	Venema	6,976,734	B2	12/2005	Stoewe
3,137,523	A	6/1964	Karner	7,040,710	B2	5/2006	White et al.
3,197,342	A	7/1965	Neild	7,070,232	B2	7/2006	Minegishi et al.
3,212,275	A	10/1965	Tillman	7,108,319	B2	9/2006	Hartwich et al.
3,392,535	A *	7/1968	De Coye De Castelet 62/3.61	7,114,771	B2	10/2006	Lofy et al.
3,599,437	A	8/1971	Panas	7,124,593	B2	10/2006	Feher
3,839,876	A *	10/1974	Privas 62/3.62	7,131,689	B2	11/2006	Brennan et al.
4,413,857	A	11/1983	Hayashi	7,147,279	B2	12/2006	Bevan et al.
4,491,173	A *	1/1985	Demand 165/11.1	7,168,758	B2	1/2007	Bevan et al.
4,665,707	A	5/1987	Hamilton	7,178,344	B2	2/2007	Bell
4,671,567	A	6/1987	Frobosc	7,201,441	B2	4/2007	Stoewe et al.
4,685,727	A	8/1987	Cremer et al.	7,272,936	B2	9/2007	Feher
4,823,544	A	4/1989	Igel	7,425,034	B2	9/2008	Bajic et al.
4,823,554	A	4/1989	Trachtenberg	7,426,835	B2	9/2008	Bell et al.
4,923,248	A	5/1990	Feher	7,462,028	B2	12/2008	Cherala et al.
4,988,847	A	1/1991	Argos et al.	7,475,464	B2	1/2009	Lofy et al.
5,002,336	A	3/1991	Feher	7,480,950	B2	1/2009	Feher
5,077,709	A	12/1991	Feher	7,506,938	B2	3/2009	Brennan et al.
5,088,790	A	2/1992	Wainwright et al.	7,587,901	B2	9/2009	Petrovski
5,106,161	A	4/1992	Meiller	7,591,507	B2	9/2009	Giffin et al.
5,111,664	A	5/1992	Yang	7,640,754	B2	1/2010	Wolas
5,117,638	A	6/1992	Feher	7,665,803	B2	2/2010	Wolas
5,385,382	A	1/1995	Single, II et al.	7,708,338	B2	5/2010	Wolas
5,419,780	A	5/1995	Suski	RE41,765	E	9/2010	Gregory et al.
5,448,891	A	9/1995	Nakagiri et al.	7,827,620	B2	11/2010	Feher
5,505,520	A	4/1996	Frusti et al.	7,827,805	B2	11/2010	Comiskey et al.
5,524,439	A *	6/1996	Gallup et al. 62/3.5	7,862,113	B2	1/2011	Knoll
5,544,487	A	8/1996	Attey et al.	7,866,017	B2	1/2011	Knoll
5,561,981	A	10/1996	Quisenberry et al.	7,877,827	B2	2/2011	Marquette et al.
5,597,200	A	1/1997	Gregory et al.	7,937,789	B2	5/2011	Feher
5,623,828	A	4/1997	Harrington	7,963,594	B2	6/2011	Wolas
5,626,021	A	5/1997	Karunasiri et al.	7,966,835	B2	6/2011	Petrovski
5,798,583	A *	8/1998	Morita 310/216.111	7,996,936	B2	8/2011	Marquette et al.
5,822,993	A	10/1998	Attey	8,065,763	B2	11/2011	Brykalski et al.
5,850,741	A	12/1998	Feher	8,104,295	B2	1/2012	Lofy
5,887,304	A	3/1999	Von der Heyde	8,143,554	B2	3/2012	Lofy
5,921,314	A	7/1999	Schuller et al.	8,181,290	B2	5/2012	Brykalski et al.
5,924,766	A	7/1999	Esaki et al.	8,191,187	B2	6/2012	Brykalski et al.
5,927,817	A	7/1999	Ekman et al.	8,222,511	B2	7/2012	Lofy
5,934,748	A	8/1999	Faust et al.	8,256,236	B2	9/2012	Lofy
6,003,950	A	12/1999	Larsson	8,332,975	B2	12/2012	Brykalski et al.
6,019,420	A	2/2000	Faust et al.	2001/0028185	A1	10/2001	Stowe et al.
6,048,024	A	4/2000	Wallman	2003/0145380	A1	8/2003	Schmid
6,059,018	A	5/2000	Yoshinori et al.	2004/0090093	A1	5/2004	Kamiya et al.
6,062,641	A	5/2000	Suzuki et al.	2004/0164594	A1	8/2004	Stoewe et al.
6,079,485	A	6/2000	Esaki et al.	2004/0195870	A1	10/2004	Bohlender
6,085,369	A	7/2000	Feher	2004/0255364	A1	12/2004	Feher
6,119,463	A *	9/2000	Bell 62/3.7	2005/0285438	A1	12/2005	Ishima et al.
6,145,925	A	11/2000	Eksin et al.	2006/0053529	A1	3/2006	Feher
6,186,592	B1	2/2001	Orizaris et al.	2006/0087160	A1	4/2006	Dong et al.
6,189,966	B1	2/2001	Faust et al.	2006/0137099	A1	6/2006	Feher
6,196,627	B1	3/2001	Faust et al.	2006/0137358	A1	6/2006	Feher
6,206,465	B1	3/2001	Faust et al.	2006/0214480	A1	9/2006	Terech
6,213,198	B1	4/2001	Shikata et al.	2006/0273646	A1	12/2006	Comiskey et al.
6,223,539	B1 *	5/2001	Bell 62/3.7	2007/0086757	A1	4/2007	Feher
6,263,530	B1	7/2001	Feher	2007/0200398	A1	8/2007	Wolas et al.
6,509,704	B1	1/2003	Brown	2007/0204629	A1	9/2007	Lofy
RE38,128	E	6/2003	Gallup et al.	2007/0251016	A1	11/2007	Feher
6,598,251	B2	7/2003	Habboub et al.	2007/0262621	A1	11/2007	Dong et al.
6,604,785	B2	8/2003	Bargheer et al.	2007/0277313	A1	12/2007	Terech
6,606,866	B2 *	8/2003	Bell 62/3.7	2008/0000025	A1	1/2008	Feher
6,619,736	B2	9/2003	Stowe et al.	2008/0047598	A1	2/2008	Lofy
6,626,488	B2	9/2003	Pfahler	2008/0087316	A1	4/2008	Inaba et al.
6,644,735	B2	11/2003	Bargheer et al.	2008/0148481	A1	6/2008	Brykalski et al.
6,676,207	B2	1/2004	Rauh et al.	2008/0164733	A1	7/2008	Giffin et al.
6,695,402	B2	2/2004	Sloan, Jr.	2008/0166224	A1	7/2008	Giffin et al.
6,700,052	B2	3/2004	Bell	2008/0173022	A1	7/2008	Petrovski
6,761,399	B2	7/2004	Bargheer et al.	2008/0223841	A1	9/2008	Lofy
6,786,541	B2	9/2004	Haupt et al.	2009/0000031	A1	1/2009	Feher
6,786,545	B2	9/2004	Bargheer et al.	2009/0025770	A1	1/2009	Lofy
6,808,230	B2	10/2004	Buss et al.	2009/0026813	A1	1/2009	Lofy
6,828,528	B2	12/2004	Stowe et al.	2009/0033130	A1	2/2009	Marquette et al.
6,841,957	B2	1/2005	Brown	2009/0126110	A1	5/2009	Feher
				2009/0193814	A1	8/2009	Lofy

US RE44,272 E

Page 3

2009/0218855	A1	9/2009	Wolas	WO	WO 94/20801	9/1994
2010/0001558	A1	1/2010	Petrovski	WO	WO 94/20801 A	9/1994
2010/0011502	A1	1/2010	Brykalski et al.	WO	WO 95/14899	6/1995
2010/0193498	A1	8/2010	Walsh	WO	WO 95/14899 A	6/1995
2011/0048033	A1	3/2011	Comiskey et al.	WO	WO 95/31688	11/1995
2011/0115635	A1	5/2011	Petrovski et al.	WO	WO 95/31688 A	11/1995
2011/0253340	A1	10/2011	Petrovski	WO	WO 02/11968	2/2002
2011/0296611	A1	12/2011	Marquette et al.	WO	WO 03/014634	2/2003
2012/0080911	A1	4/2012	Brykalski et al.	WO	WO 03/051666	6/2003
2012/0104000	A1	5/2012	Lofy			
2012/0114512	A1	5/2012	Lofy et al.			
2012/0131748	A1	5/2012	Brykalski et al.			
2012/0227182	A1	9/2012	Brykalski et al.			
2012/0319439	A1	12/2012	Lofy			

FOREIGN PATENT DOCUMENTS

DE	10115242	10/2002
DE	10238552	3/2003
EP	0 834 421 A1	4/1998
EP	0834 421	4/1998
JP	60-80044	5/1985
JP	60085297 A *	5/1985
JP	01 281344	11/1989
JP	60-80044	11/1989
JP	01 281344 A	1/1990
JP	04-165234	6/1992
LU	66619	2/1973
LU	66619 A	2/1973

OTHER PUBLICATIONS

Search Report for EP 04 00 6634, mailed May 13, 2005.

Office Action in corresponding Japanese Patent Application JP 2000-548669, mailed Aug. 2, 2005.

Feher, Steve, Thermoelectric Air Conditioned Variable Temperature Seat (VTS) & Effect Upon Vehicle Occupant Comfort, Vehicle Energy Efficiency, and Vehicle Environment Compatibility, SAE Technical Paper, Apr. 1993, pp. 341-349.

Lofy, J. et al., Thermoelectrics for Environmental Control in Automobiles, Proceeding of Twenty-First International Conference on Thermoelectrics (ICT 2002), published 2002, pp. 471-476.

Photographs and accompanying description of climate control seat assembly system components publicly disclosed as early as Jan. 1998.

* cited by examiner

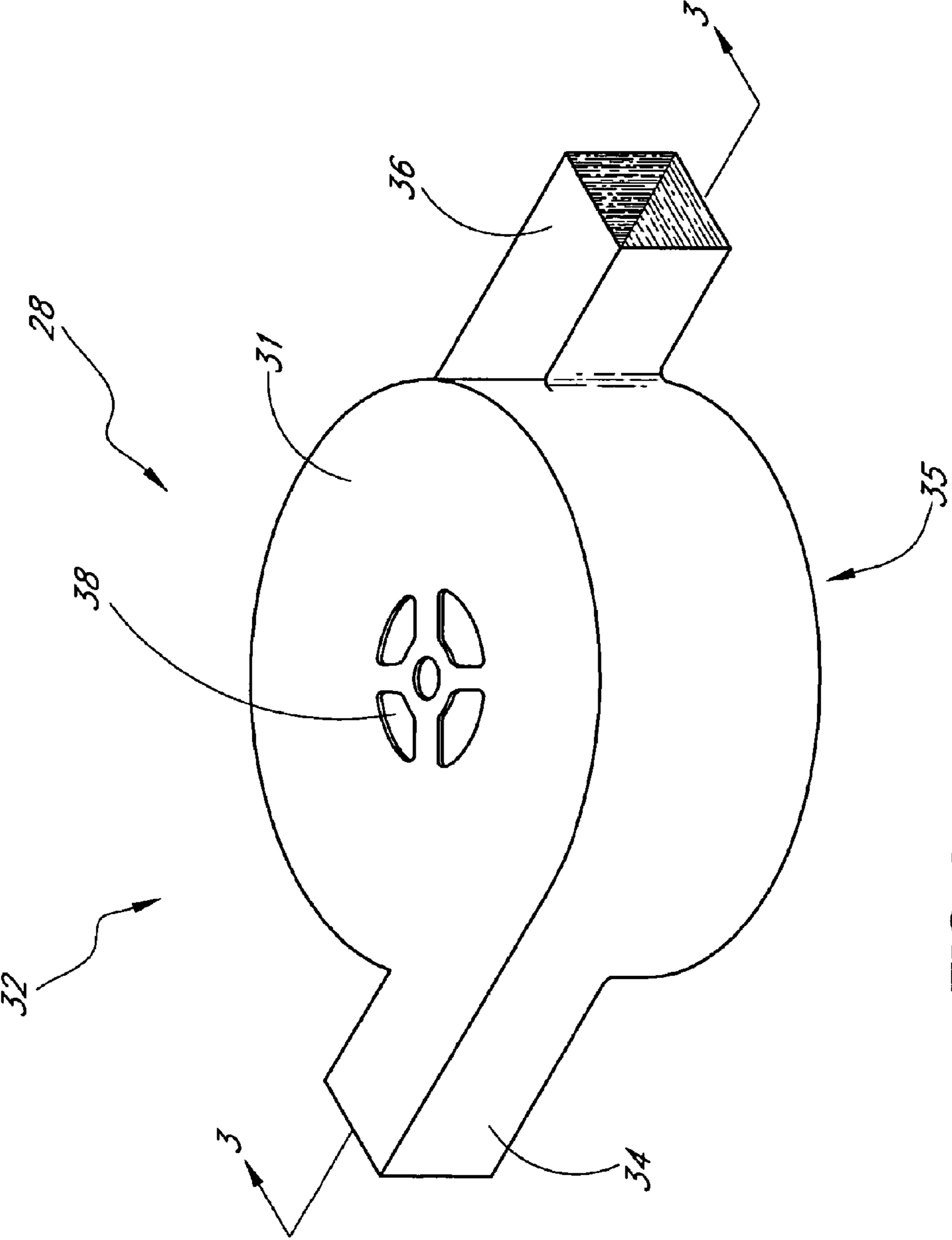


FIG. 1

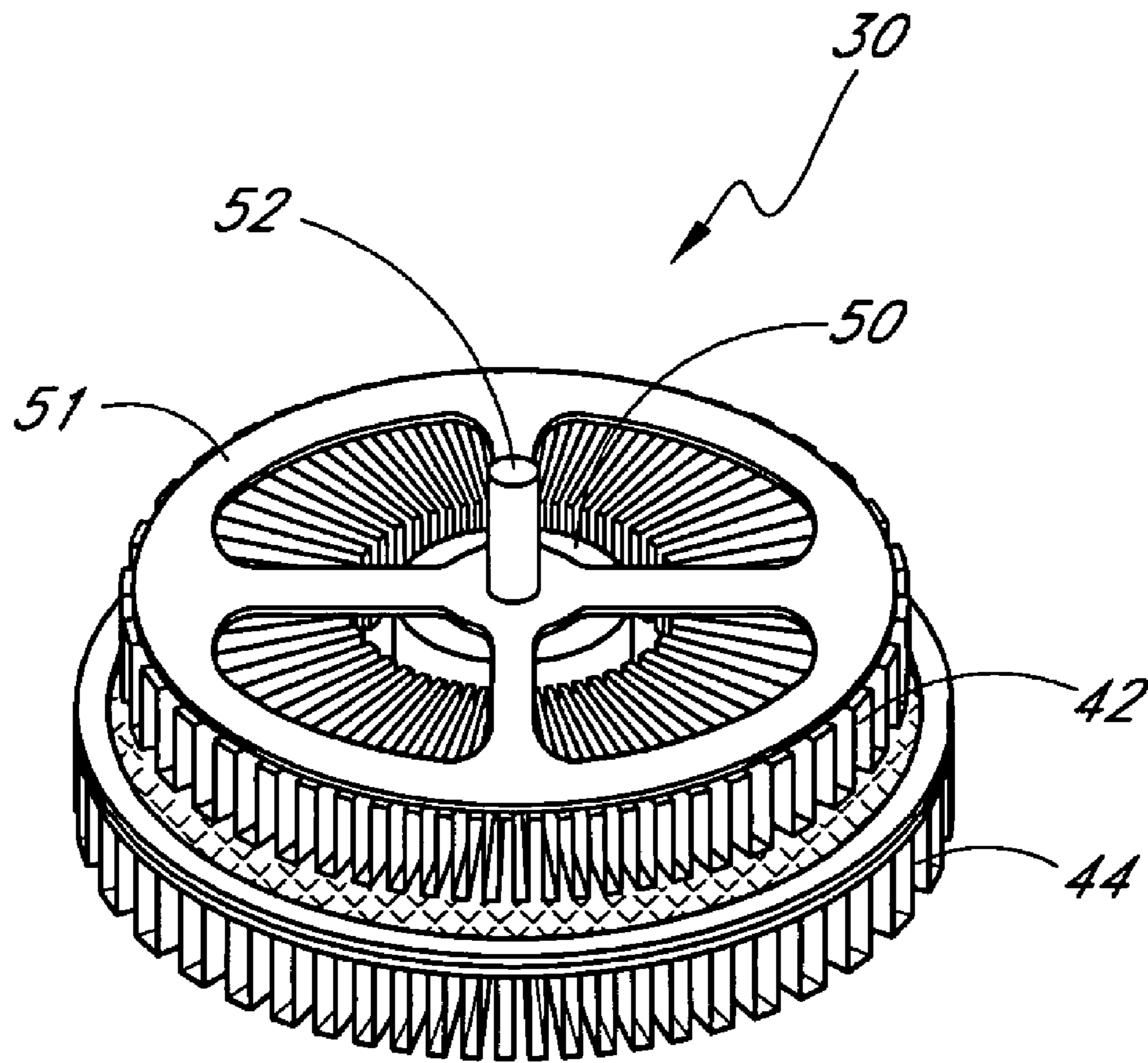


FIG. 2

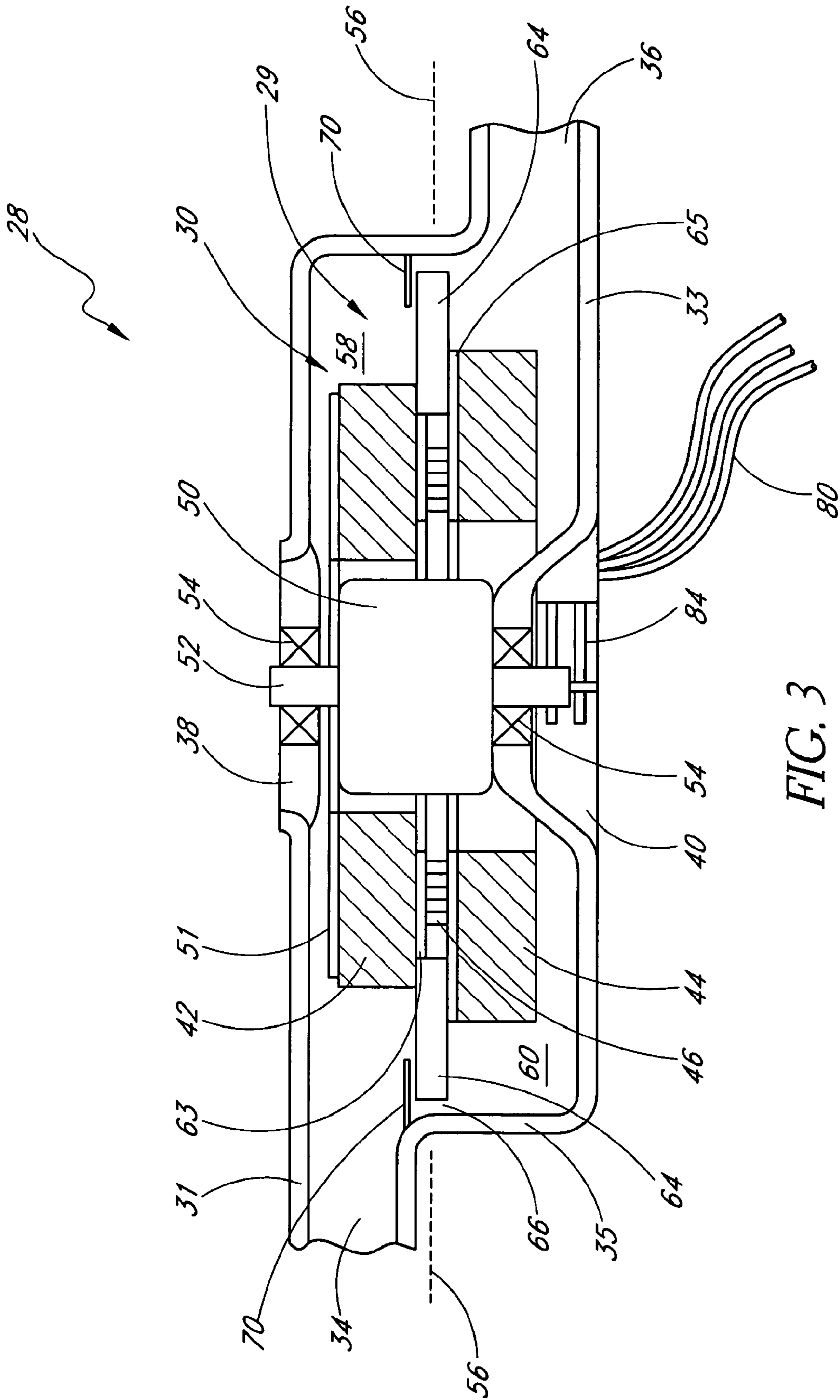


FIG. 3

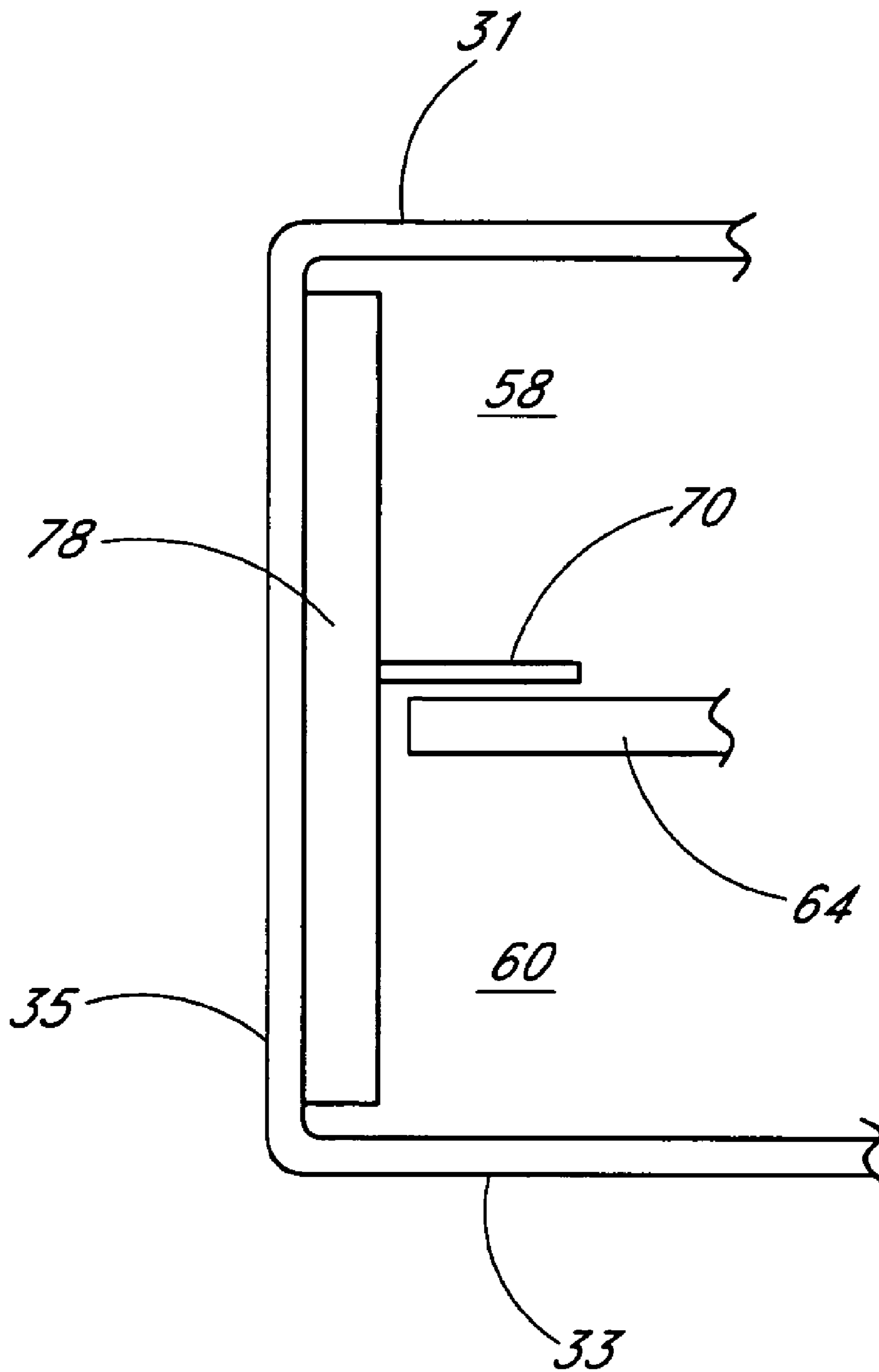


FIG. 4

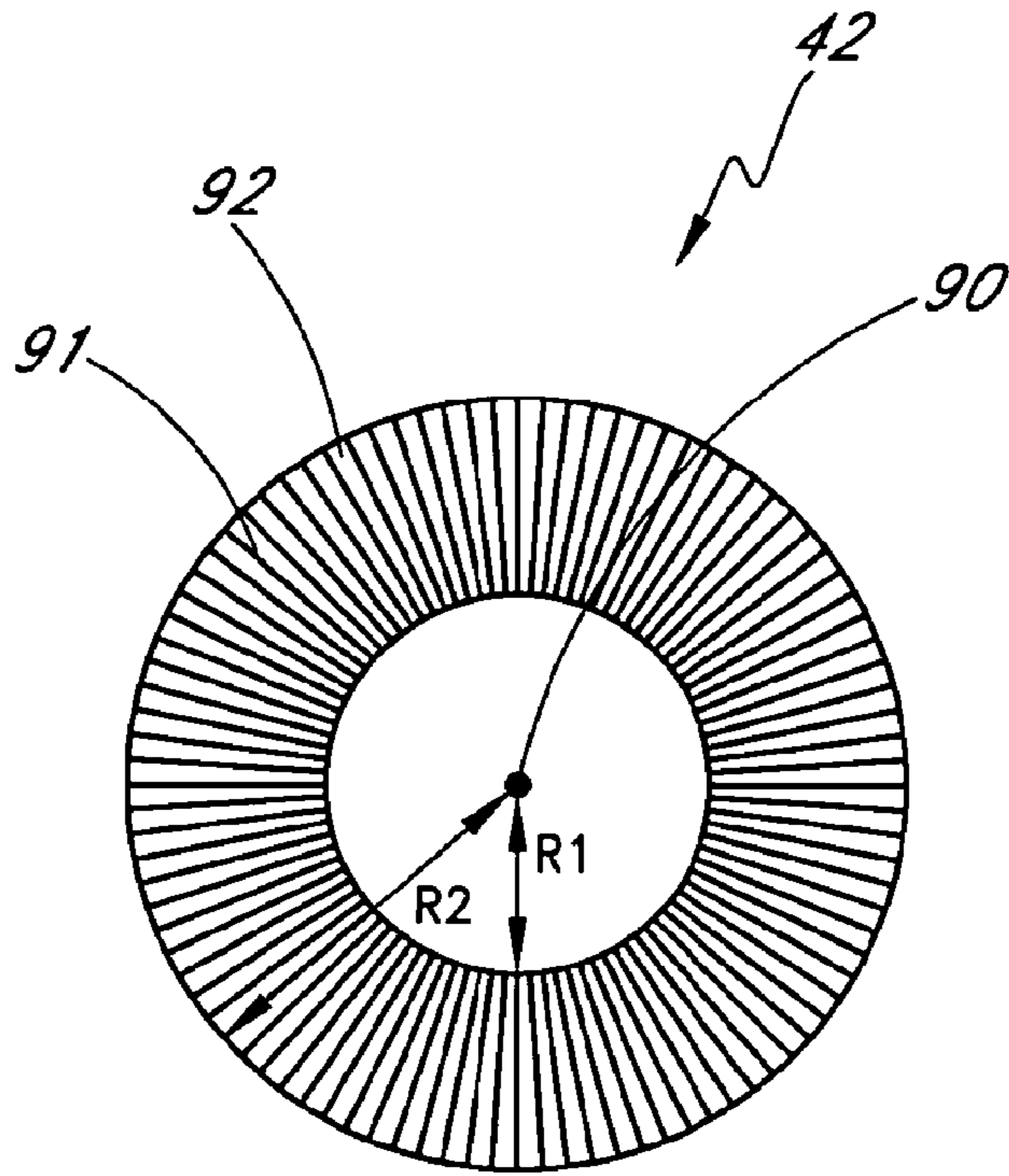


FIG. 5

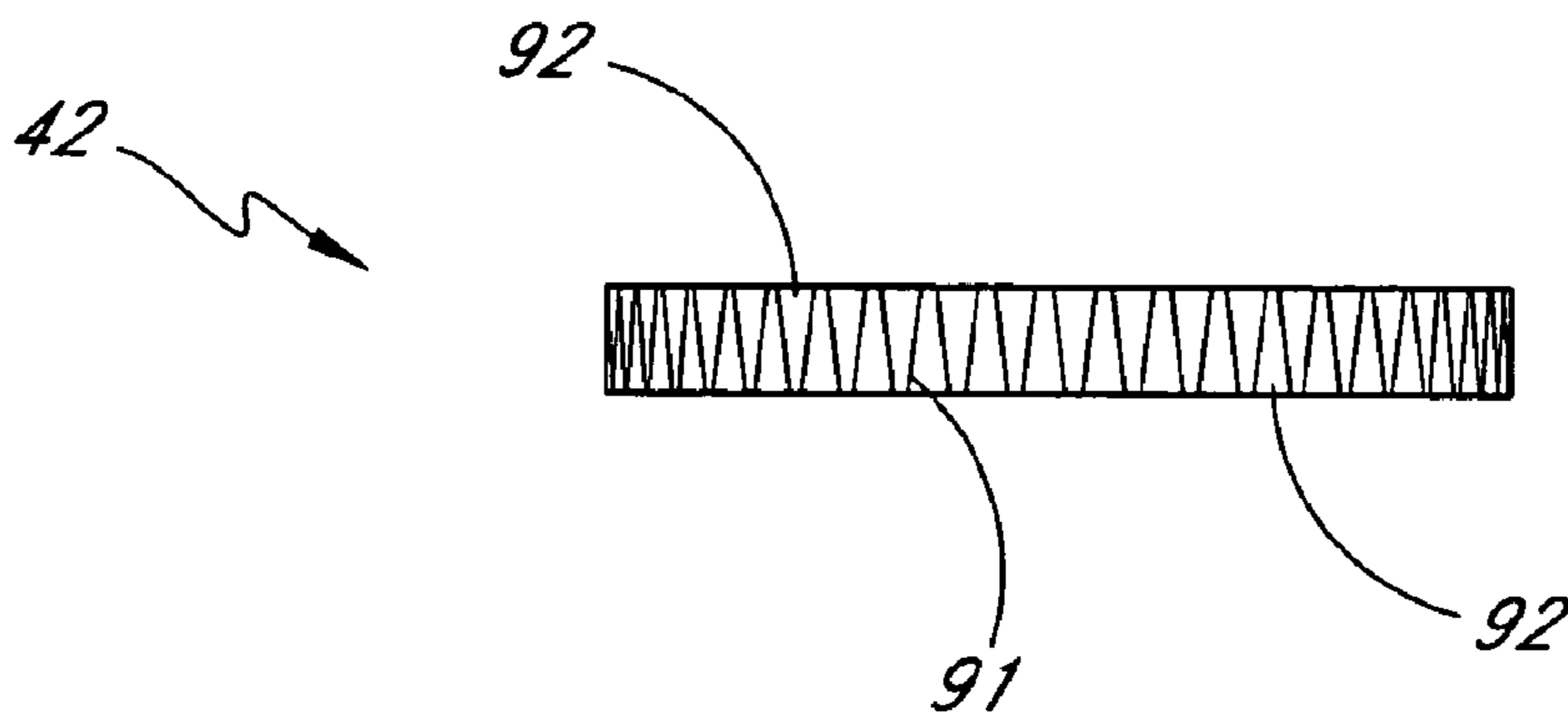


FIG. 6

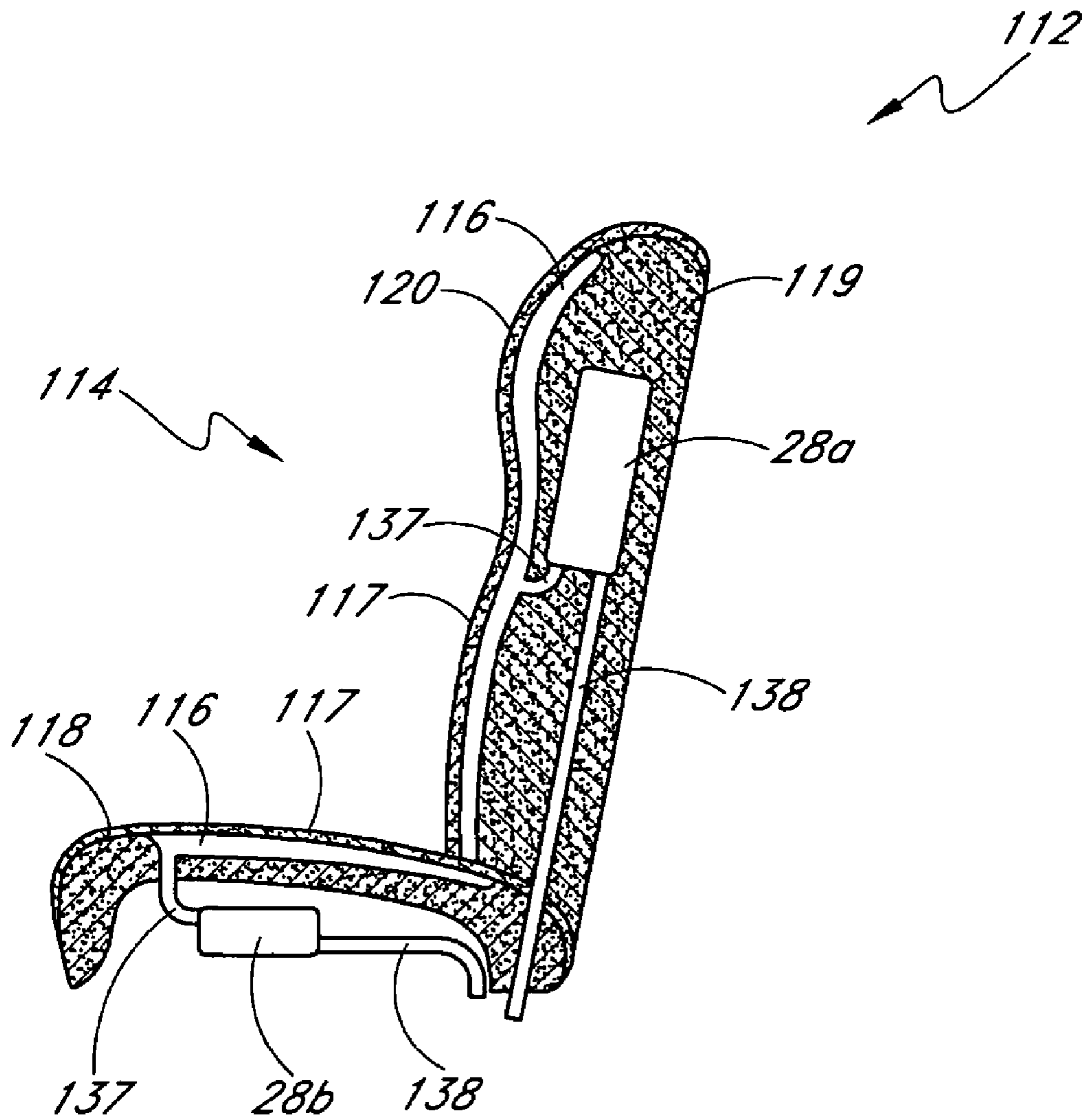


FIG. 7

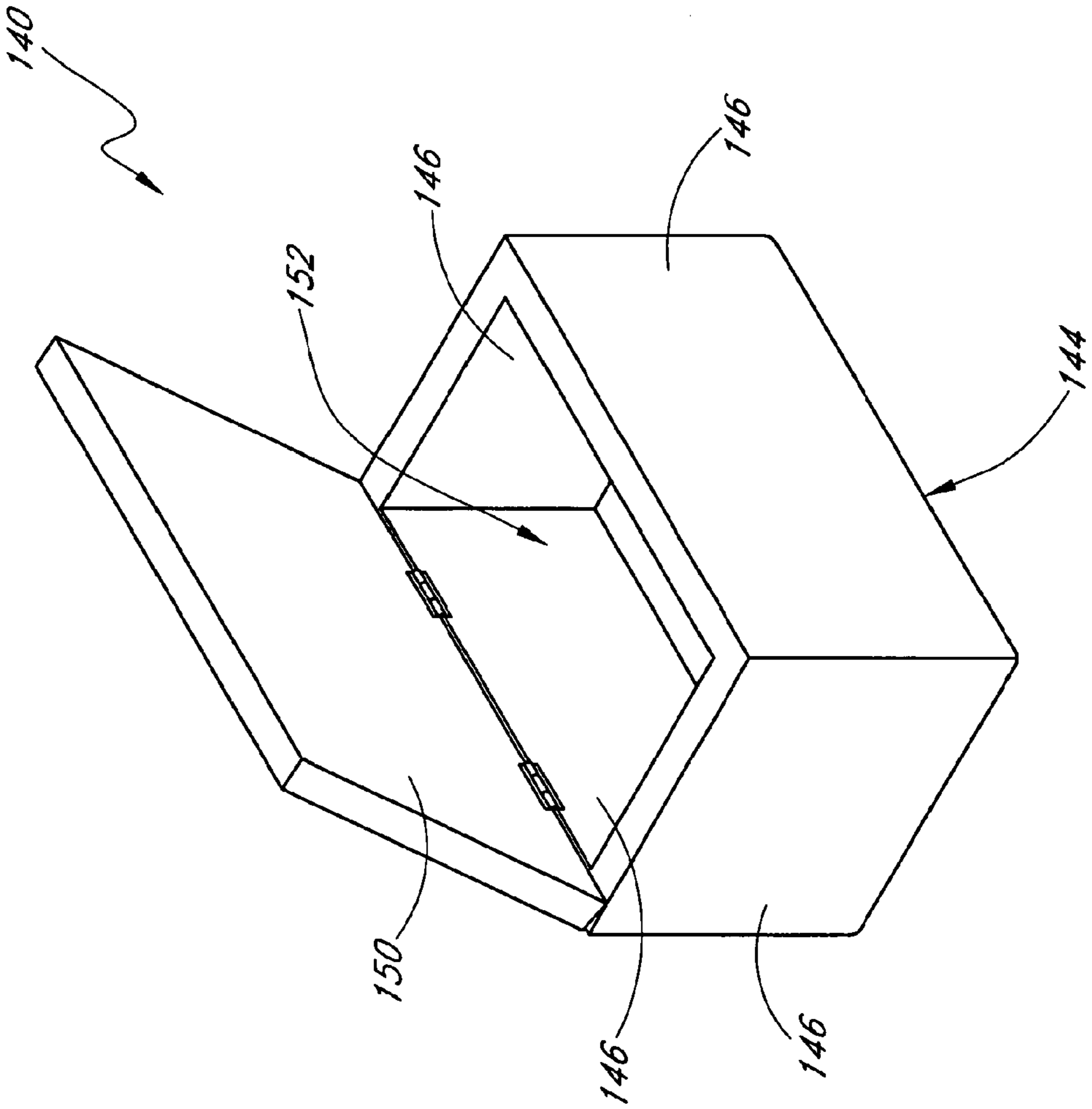


FIG. 8

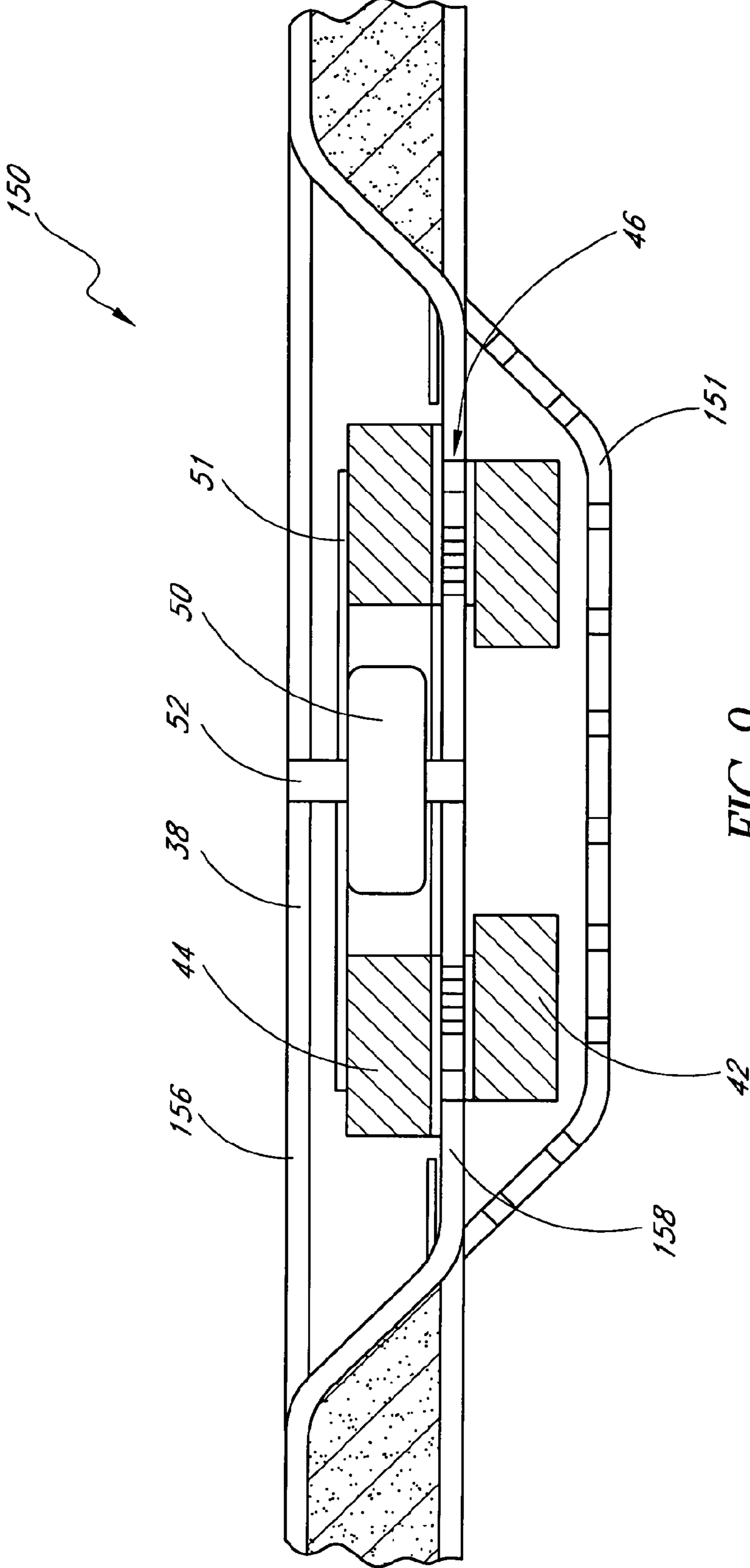
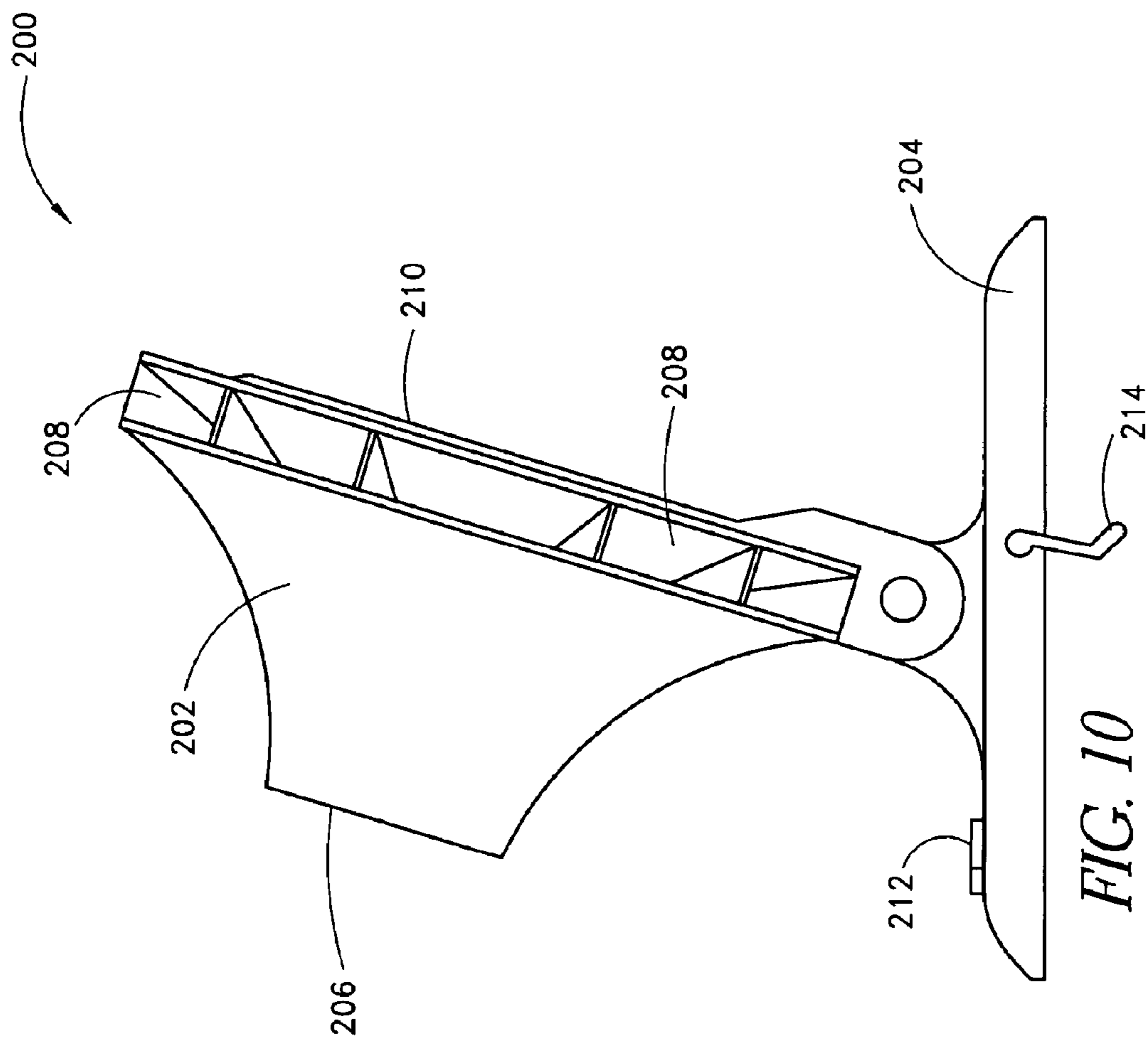


FIG. 9



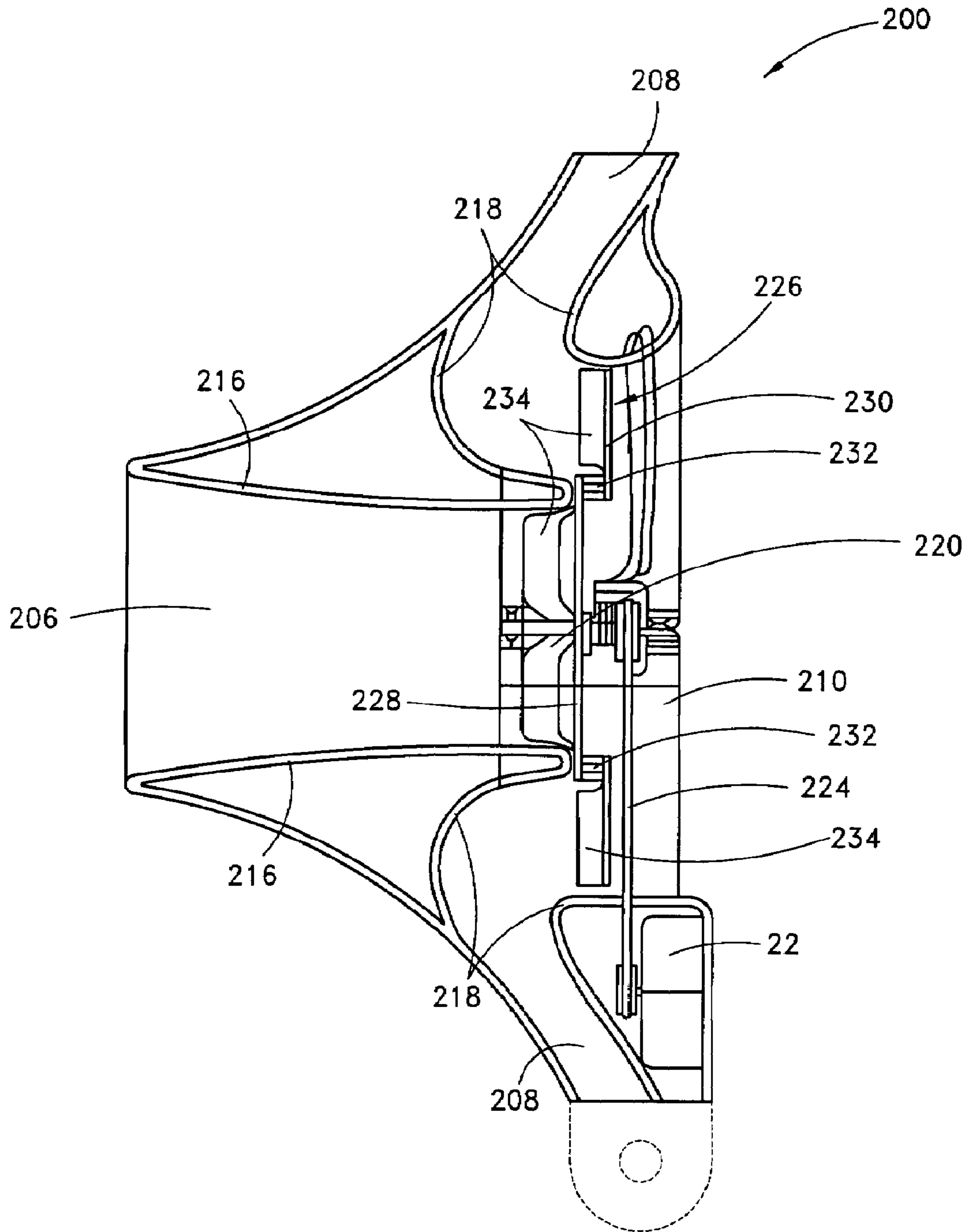


FIG. 11

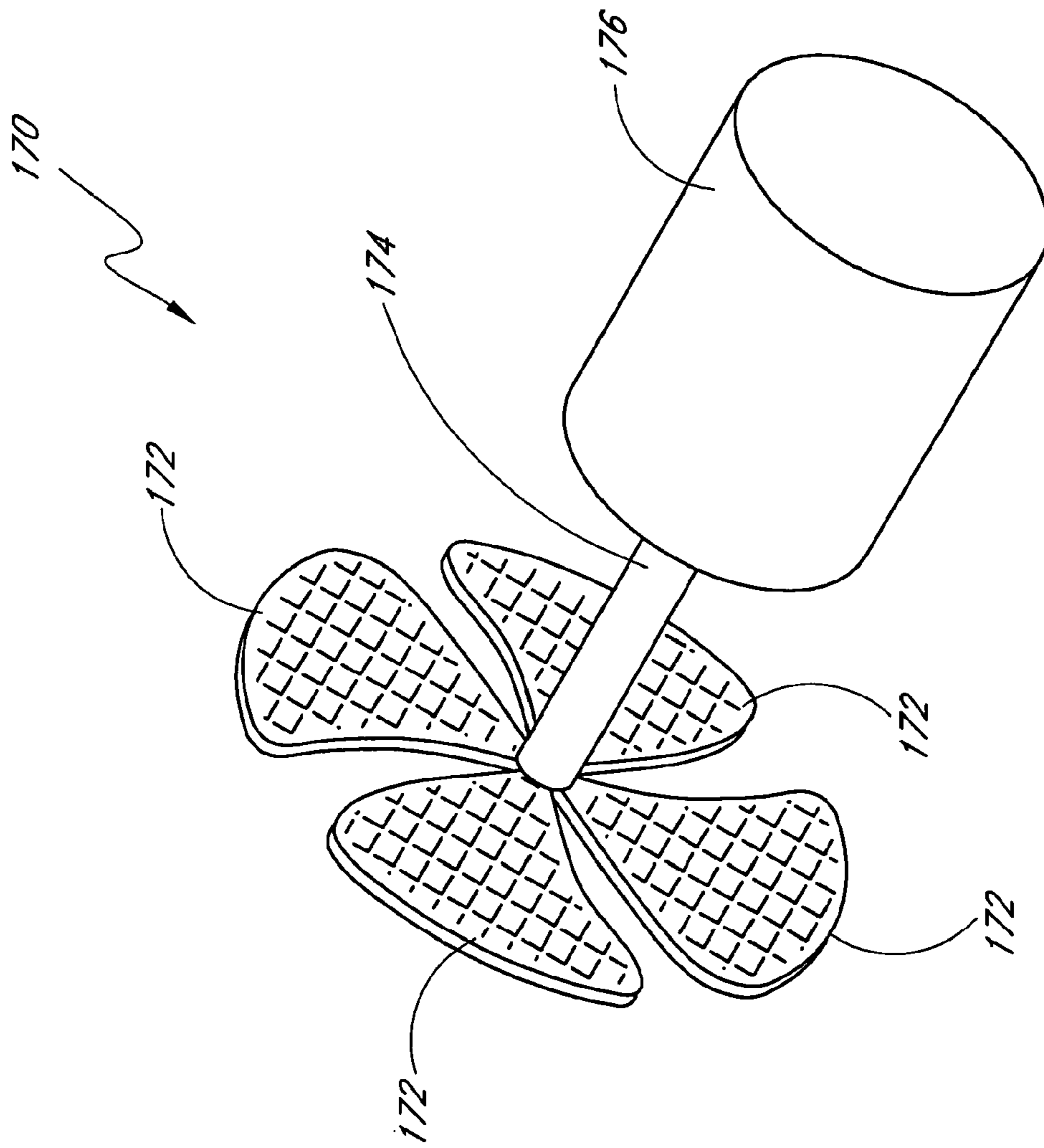


FIG. 12

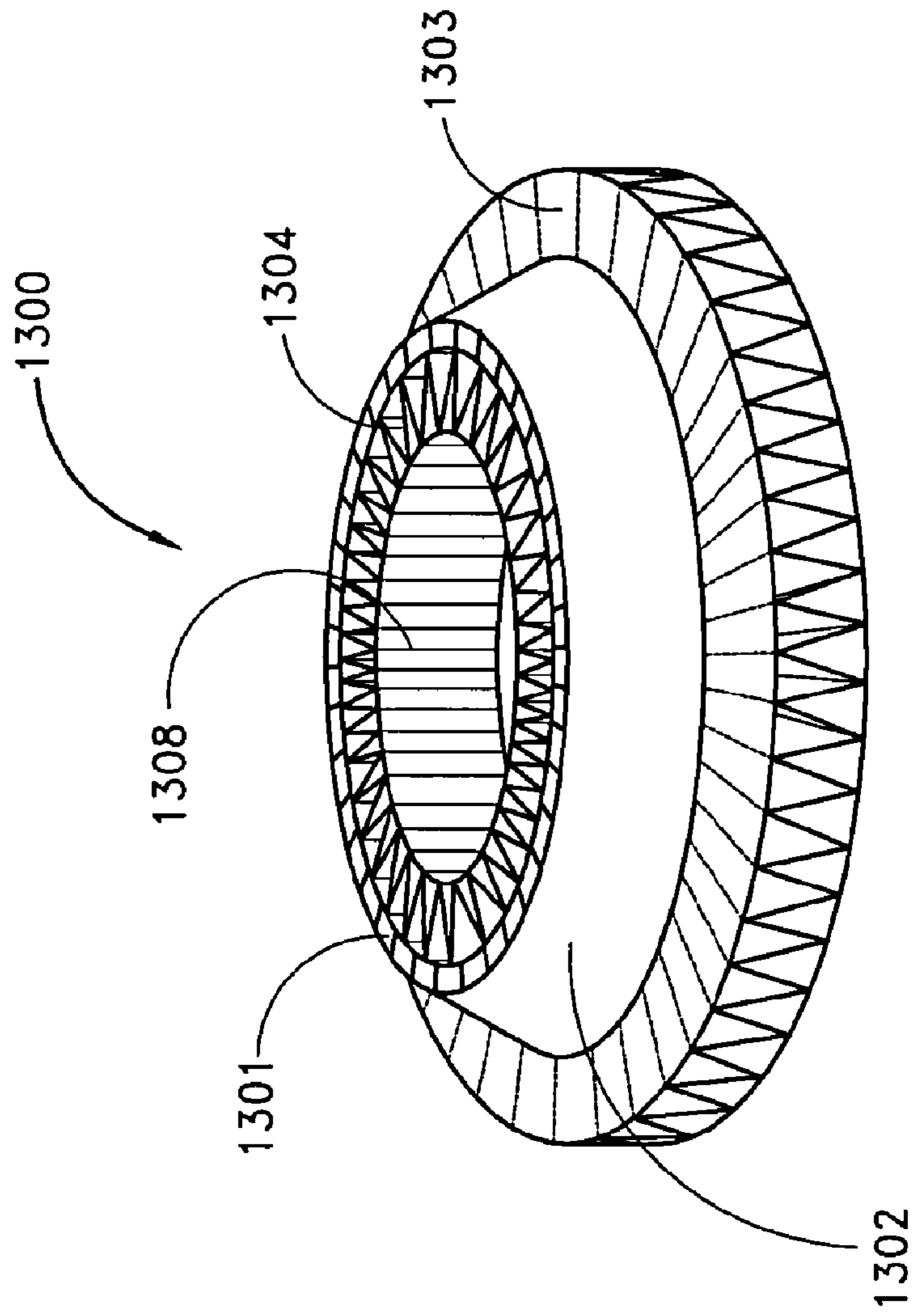


FIG. 13A

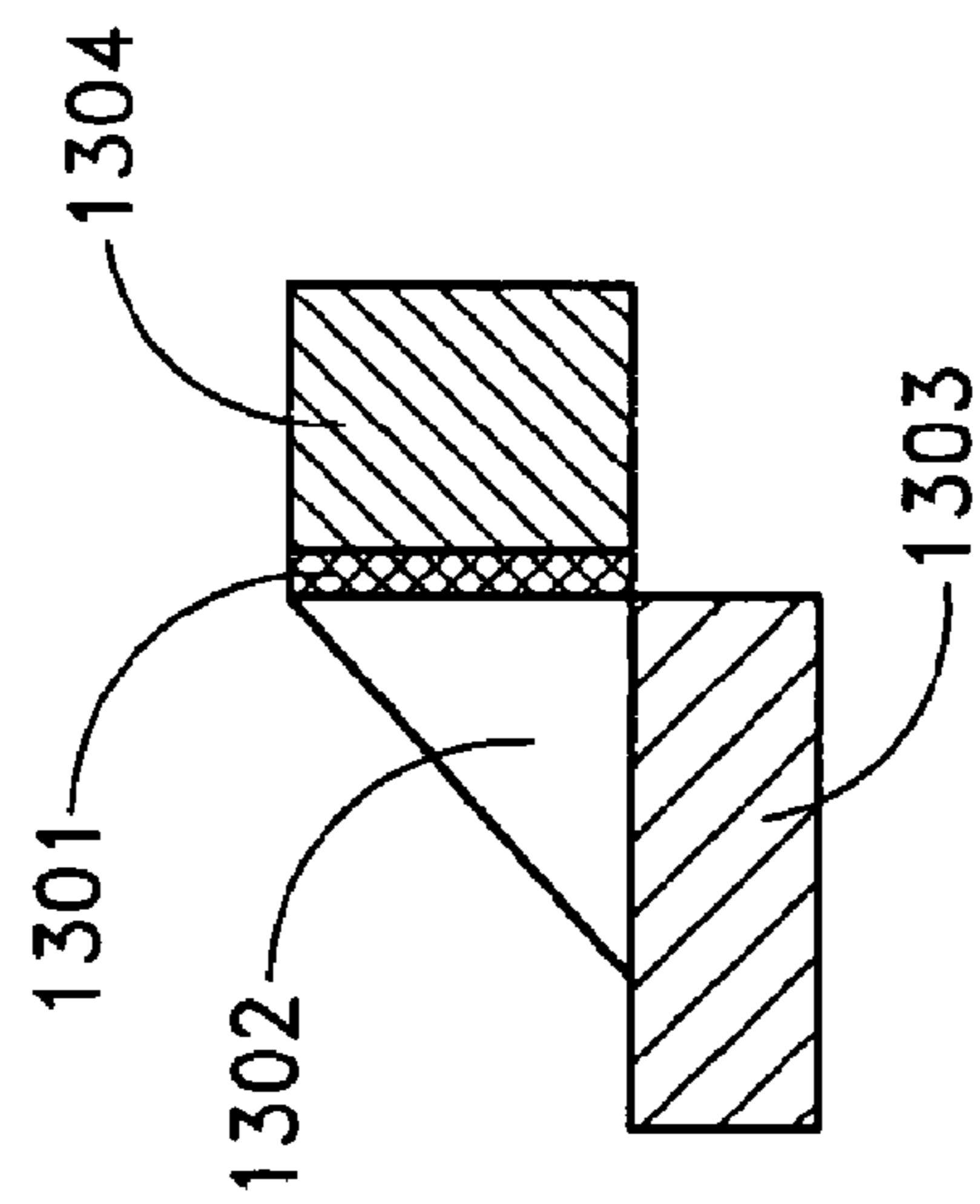


FIG. 13B

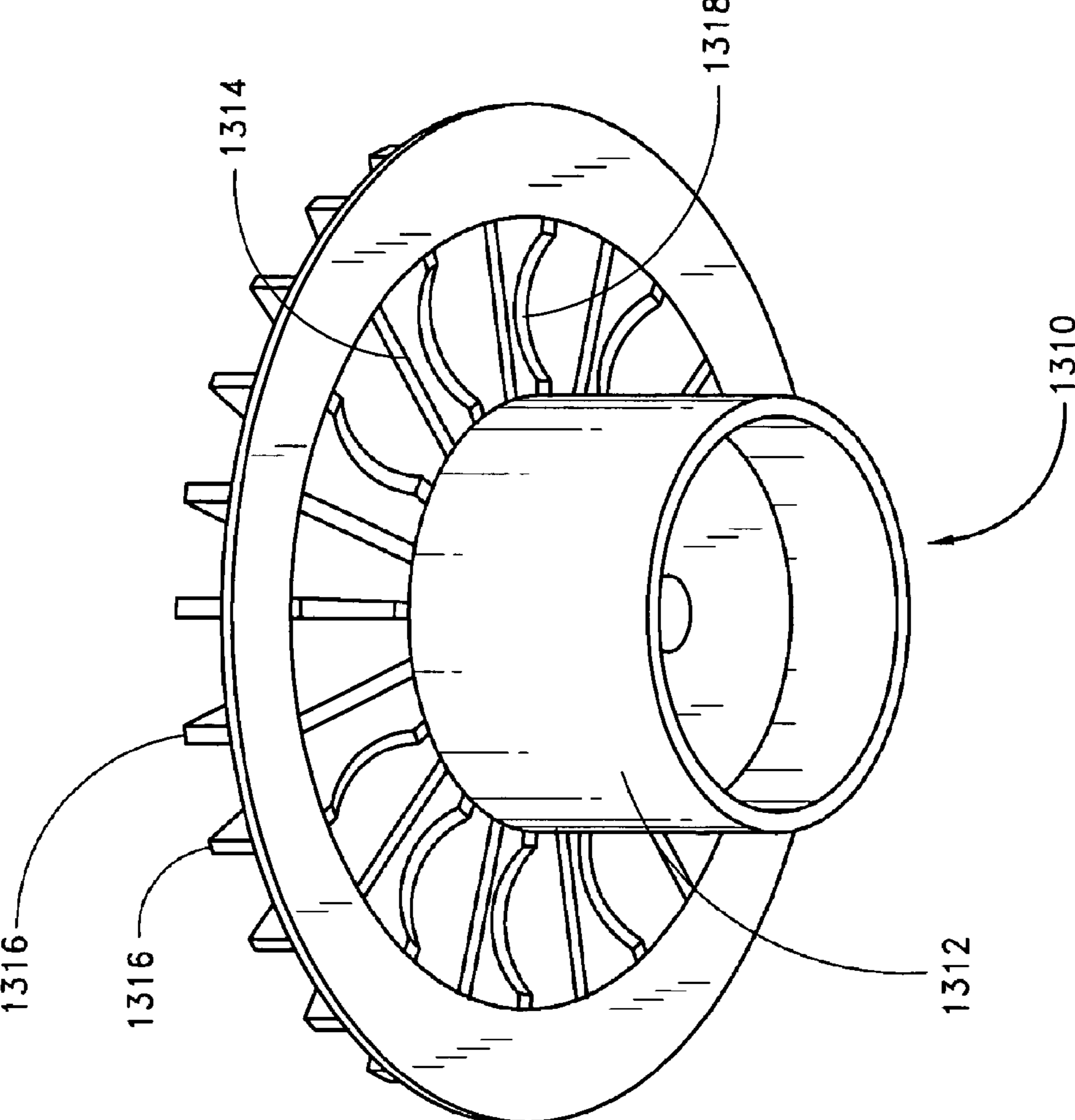


FIG. 13C

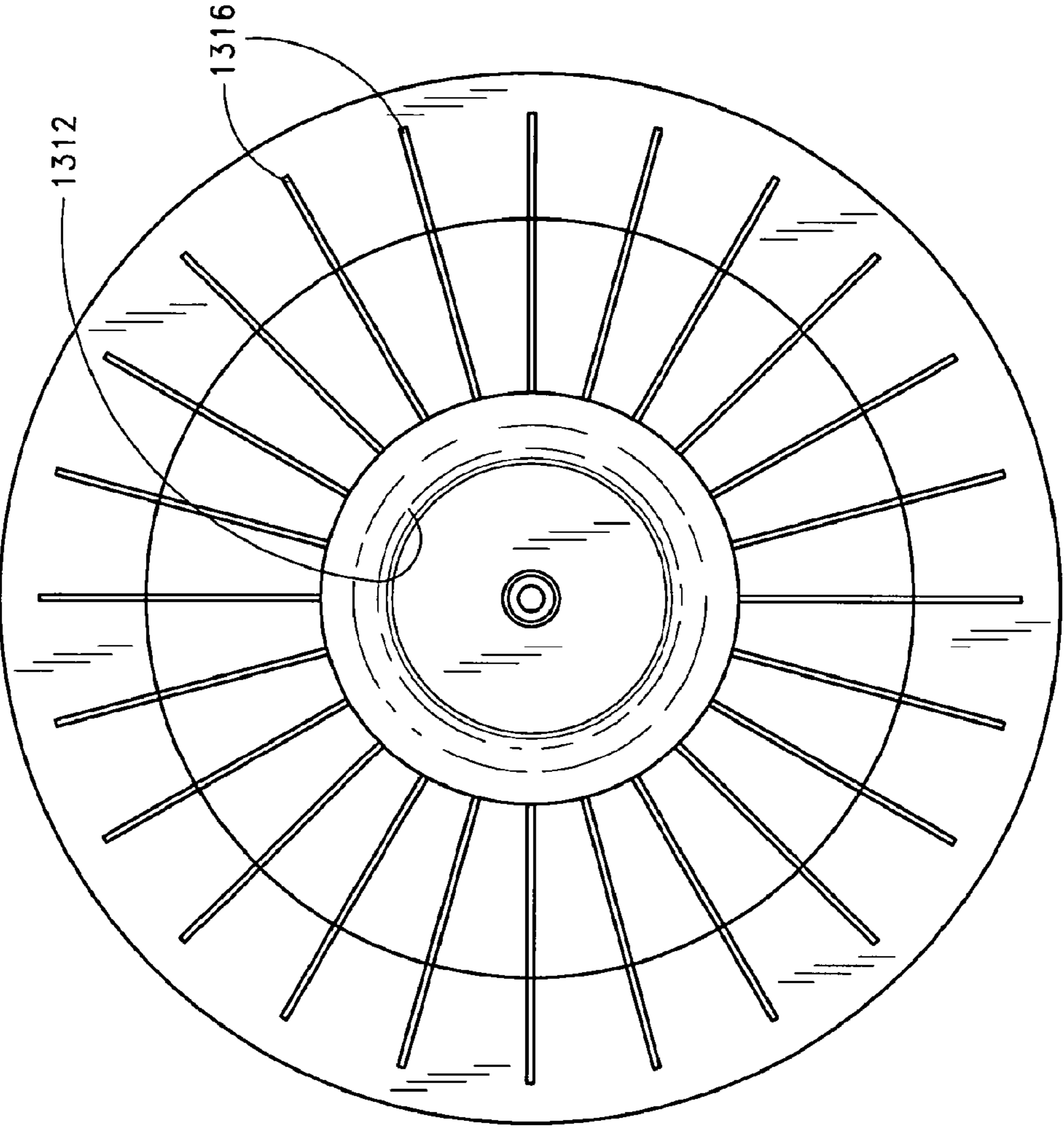


FIG. 13D

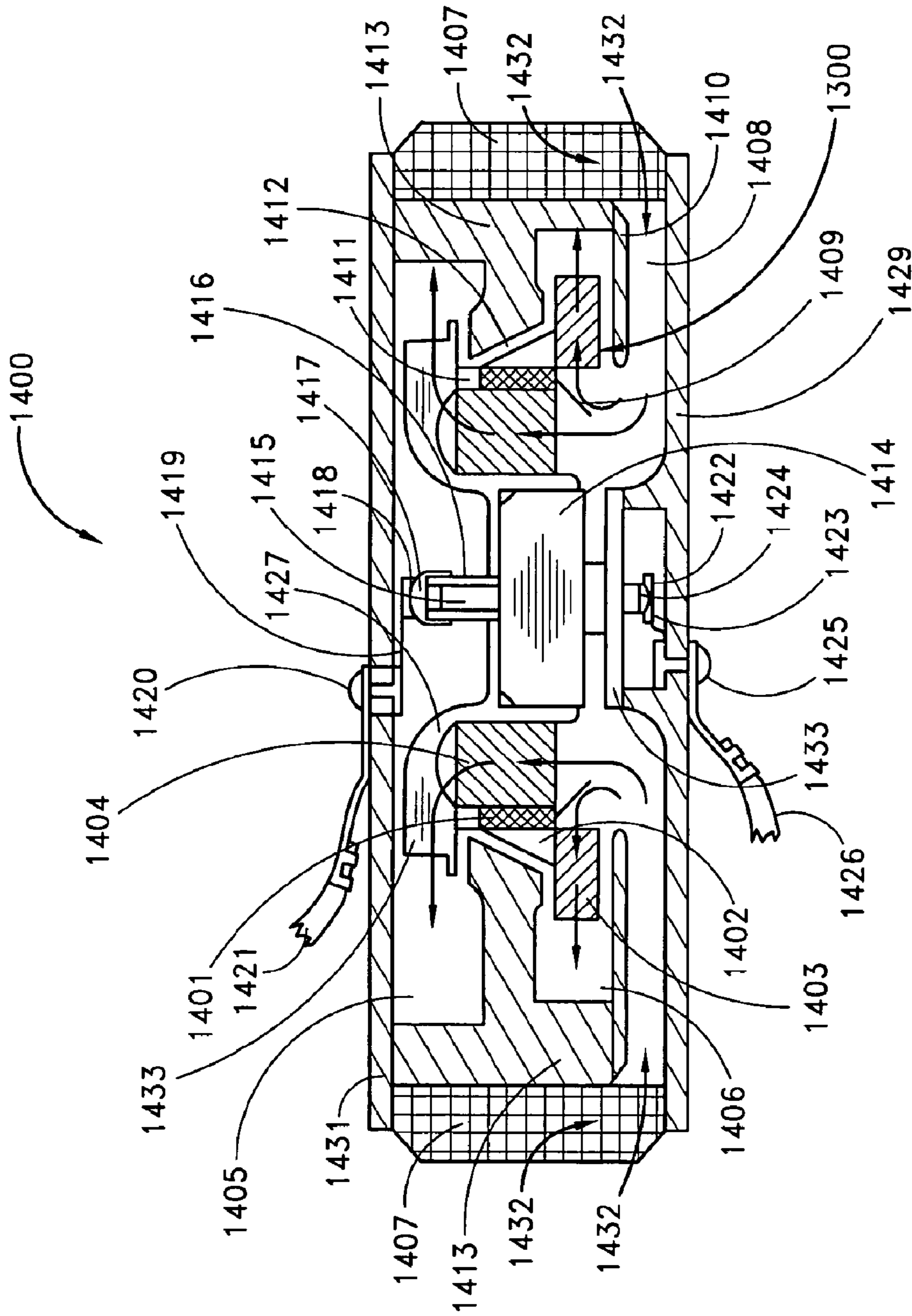


FIG. 14

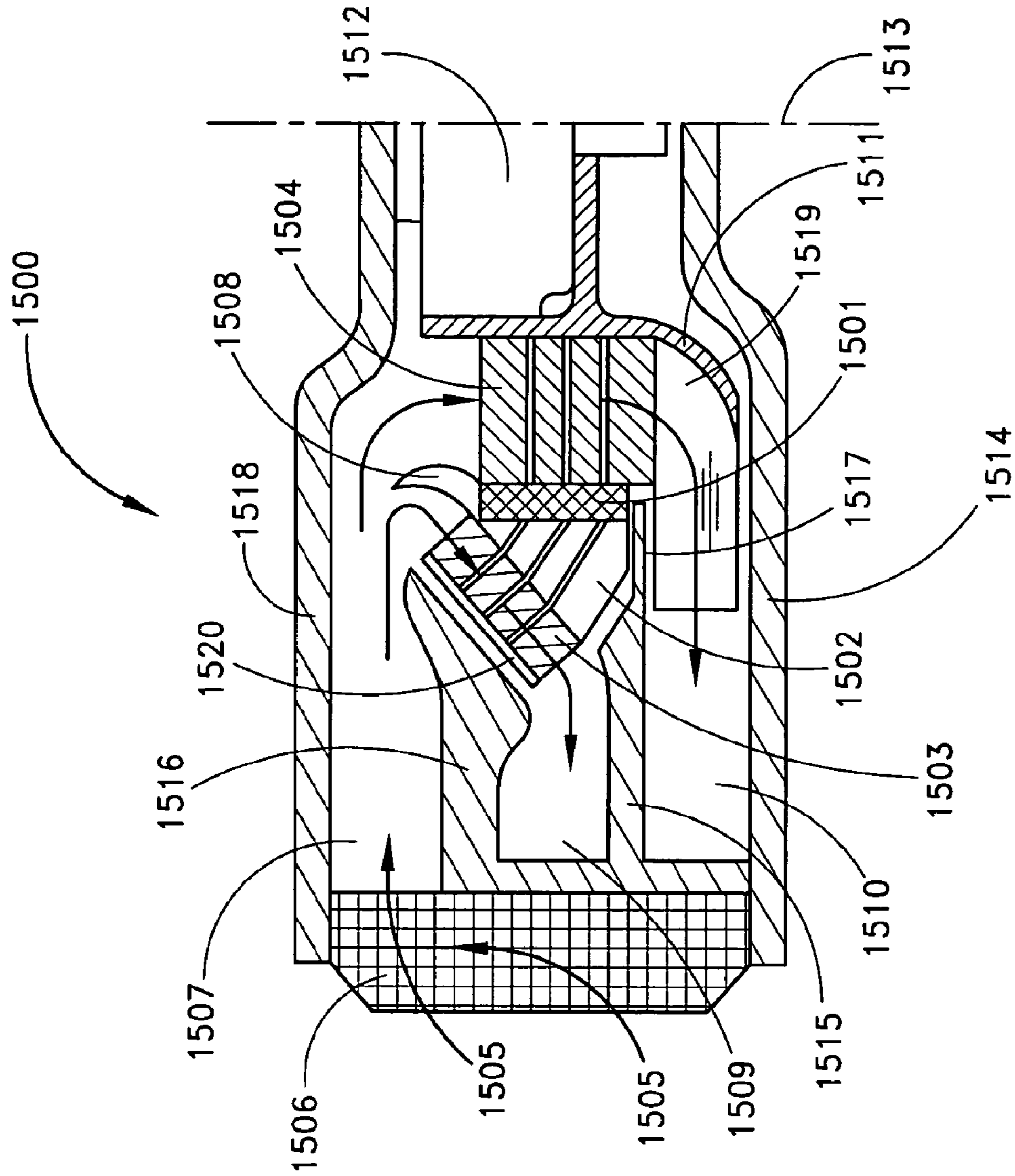


FIG. 15

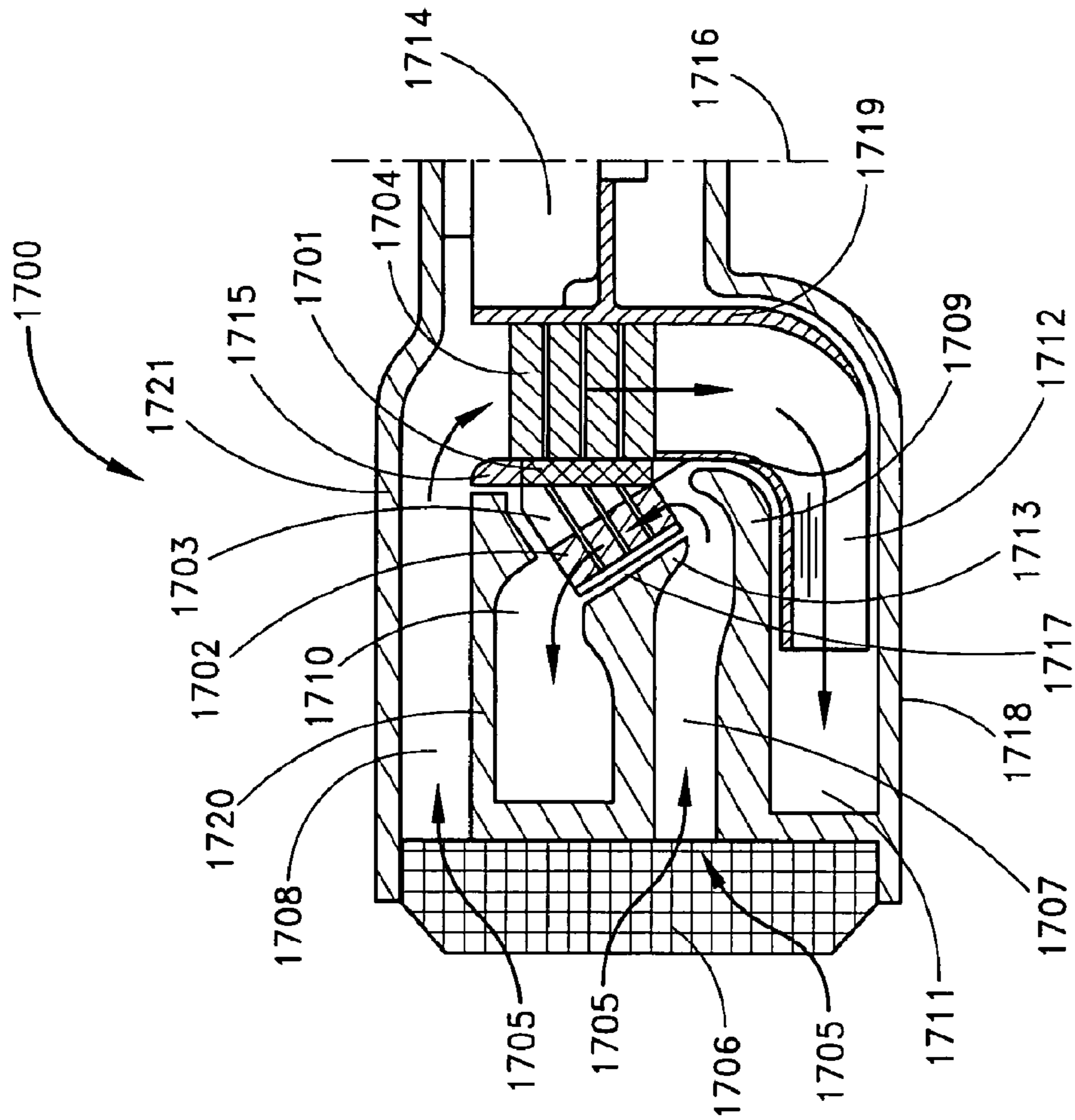


FIG. 17

THERMOELECTRIC HEAT EXCHANGER

Matter enclosed in heavy brackets [] appears in the original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue.

PRIOR APPLICATION DATA

This application is a continuation of U.S. patent application Ser. No. 10/608,807 filed Jun. 27, 2003, now U.S. Pat. No. 6,907,739, which is a continuation of U.S. patent application Ser. No. 09/971,539, filed Oct. 2, 2001, now U.S. Pat. No. 6,606,866, which is a continuation-in-part of U.S. patent application Ser. No. 09/847,856 filed May 1, 2001, abandoned, which is a continuation of U.S. application Ser. No. 09/428,018, filed Oct. 27, 1999, now U.S. Pat. No. 6,223,539, which is a continuation of U.S. application Ser. No. 09/076,518, filed May 12, 1998, now U.S. Pat. No. 6,119,463.

BACKGROUND OF THE INVENTION

The present invention relates to temperature control devices. More particularly, the present invention relates to a thermoelectric heat exchanger that is particularly useful for converting electricity to a flow of conditioned air. The air may be heated or cooled.

Modern automobile seats may be equipped with temperature control systems that allow the occupant to vary the temperature of the seat by flowing temperature-controlled air through the seat covering. One type of system comprises a seat having a heat transfer system mounted therein, such as a thermoelectric element configured to heat or cool air that is moved over the element using a separate fan unit that is also mounted within the seat. The conditioned air is distributed to the occupant by passing the air through the seat surface via a series of air ducts within the seat.

The amount of space available within, below and around the seat for such temperature control systems is severely limited. In some cars, to save weight or increase passenger room, the seats are a few inches thick and abut the adjacent structure of the car, such as the floorboard or the back of the car. Further, automobile manufacturers are increasingly mounting various devices, such as electronic components or variable lumbar supports, within, below and around the seat. Additionally, the size of the seat, particularly the seat back, needs to be as small as possible to reduce the amount of cabin space consumed by the seat.

Present temperature control systems are often too large to be mounted within, below or around vehicle seats. Conventional systems may have a squirrel cage fan five or six inches in diameter generating an air flow that passes through a duct to reach a heat exchanger that adjusts the temperature of the air. The heat exchanger is several inches wide and long, and at least an inch or so thick. From the heat exchanger the air is transported through ducts to the bottom of the seat cushion and to the back of the seat cushion. Such systems are bulky and difficult to fit underneath or inside car seats. Using thermoelectric devices to heat and cool the heat exchanger helps reduce the size of unit, but still requires a large volume for the combined heating and cooling system.

The ducting used with these systems is also bulky and difficult to use if the duct must go from a seat bottom to a seat back that is allowed to pivot or rotate. These ducts not only use additional space within the seat, but also resist air flow and thus require a larger fan to provide the air flow, and the

larger fan requires additional space or else runs at greater speeds and generates more noise. Noise is undesirable inside motor vehicles. Further, the ducting affects the temperature of the passing air and either heats cool air, or cools heated air, with the result of often requiring larger fans or heat exchangers. In light of these drawbacks, there is a need for a more compact and energy efficient heating and cooling system for automobile seats, and preferably a quieter system. In addition, a more compact and energy-efficient heating and cooling system useful in seats also has uses in other localized conditioned air settings.

SUMMARY OF THE INVENTION

The present devices use air flow generators, such as fan blades, that act as both a heat exchanger to transfer a thermal differential from a thermoelectric device and thereby condition air passing over the heat exchanger, and that act as an air pump. The heat exchanger rotates and provides aerodynamic and centrifugal force to the air passing through the heat exchanger to generate pressurized air for distribution, such as to the seat of a motor vehicle.

An improved thermoelectric heat exchanger system is disclosed. The heat exchanger system has a first heat exchanger formed about an axis and configured such that fluid flows along the first heat exchanger at least partially in a first direction, and a second heat exchanger formed about the axis and configured such that fluid flows along the second heat exchanger at least partially in a direction other than the first direction. A thermoelectric device having opposing surfaces exhibits a temperature gradient between one surface and an opposing surface in response to electrical current flowing through the thermoelectric device. The one surface is in thermal communication with the first heat exchanger and the opposing surface is in thermal communication with the second heat exchanger.

Several different combinations of fluid flow directions are disclosed. For example: the first direction is at least partially outward from the axis; the first direction is at least partially perpendicular to the axis; the second direction is at least partially along the axis, while the first direction is generally outward or away from the axis; the first direction is at least partially at an angle from the axis, and the second direction is at least partially at an angle from the axis; the first direction is at least partially along the axis, and the second direction is at least partially at an angle from the axis.

In one embodiment, a heat transfer member is in thermal communication with the one or the opposing surface of the thermoelectric device and in thermal communication with the first or second heat exchanger. Another heat transfer member may also be provided in thermal communication with the other surface and with the other heat exchanger.

At least one of the first and second heat exchangers may be formed in segments to provide thermal isolation in the direction of flow. The heat transfer members may also be formed in segments to provide thermal isolation in the direction of flow, where one or more heat transfer members are used. Where the heat exchanger is made from a plurality of blades, thermal isolation may be provided by spaces in the blades in the direction of flow.

A housing containing at least one of the first and the second heat exchangers may be used to form an outlet through which air exits after passing through the at least one of the first or second heat exchangers. An auxiliary fan may also be used in conjunction with the heat exchangers. In certain configurations, the heat exchangers themselves generate fluid flow.

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These configurations may also use the auxiliary fan to augment the flow. The auxiliary fan may also be used as the primary or only fluid flow generator.

A thermoelectric heat exchanger system is also disclosed that has a thermoelectric device configured to generate a thermal gradient between a first temperature side and a second temperature side in response to an electrical current with at least one first heat exchanger in thermal communication with the first or the second temperature side of the thermoelectric device, wherein the heat exchanger is rotatable about a rotational axis. In this embodiment, an auxiliary fan is configured to rotate about the rotational axis and to generate fluid flow along the heat exchanger. In one embodiment, the first heat exchanger may be oriented such that fluid flow from the auxiliary fan flows through the heat exchanger along the rotational axis.

A second heat exchanger may also be provided configured to generate a fluid flow in a first direction away from the rotational axis with rotation about the rotational axis. In such case, the first heat exchanger is preferably oriented such that fluid flow generated by the auxiliary fan flows through the first heat exchanger in a second direction other than the first direction. Advantageously, the heat exchanger is constructed to provide thermal isolation in the direction of flow, such as with segments in blades or the like.

Another heat exchanger system is disclosed wherein a thermoelectric device formed about an axis and has opposing surfaces that generate a temperature gradient between one surface and an opposing surface in response to electrical current flowing through the thermoelectric device. In this heat exchanger system, first and second heat exchangers are formed about the axis and configured such that fluid flows along the first heat exchanger and along the second heat exchanger generally away from the axis. The first heat exchanger is in thermal communication with the one surface, and the second heat exchanger is in thermal communication with the opposing surface. At least one of the first and second heat exchangers is formed to provide thermal isolation in the direction of fluid flow between a plurality of portions of the at least one heat exchanger.

This configuration can be constructed such that the heat exchangers and thermoelectric device rotate about the axis during operation, at least one of the heat exchangers operating to induce fluid flow through the heat exchangers. Alternatively, the heat exchangers and thermoelectric device are stationary, but an auxiliary fan rotates about the axis and causes fluid to flow along at least one of the first and second heat exchangers. In one preferred embodiment of this system, at least one of the first and second heat exchangers is formed in segments to provide the thermal isolation.

Yet another thermoelectric heat exchanger system is disclosed with a thermoelectric device formed about an axis and having opposing surfaces that generate a temperature gradient between one surface and an opposing surface in response to electrical current flowing through the thermoelectric device. First and second heat exchangers are about the axis and configured such that fluid flows along the first heat exchanger and along the second heat exchanger generally away from the axis. The first heat exchanger is in thermal communication with the one surface, and the second heat exchanger is in thermal communication with the opposing surface. An auxiliary fan rotates about the axis and generates fluid flow along at least one of the first and second heat exchangers. Preferably, at least one of the first and second heat exchangers is formed to provide the thermal isolation in the direction of flow, such as through construction in a plurality of substantially thermally isolated segments.

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A method of conditioning a fluid flow is also contemplated which involves the steps of flowing current through a thermoelectric device having opposing surfaces to generate a temperature gradient between a first surface and a second surface of the thermoelectric device, flowing a fluid along a first heat exchanger formed about an axis at least partially in a first direction, the first heat exchanger in thermal communication with the first surface, and flowing a fluid along a second heat exchanger formed about the axis at least partially in a direction other than the first direction, the second heat exchanger in thermal communication with the second surface.

The direction may be in any reasonable configuration, such as, but not limited to: the first direction is at least partially outward from the axis; the first direction is at least partially perpendicular to the axis; the second direction is at least partially along the axis; the first direction is at least partially at an angle from the axis, and the second direction is at least partially at an angle from the axis and; the first direction is at least partially along the axis, and the second direction is at least partially at an angle from the axis.

Advantageously, the method further involves forming at least one of the first and second heat exchangers to provide thermal isolation in the direction of flow, such as forming the heat exchangers in segments. The flowing of fluid may be provided by an auxiliary fan that rotates about the axis. In addition, or alternatively, the flowing of fluid may be provided by the first or second heat exchanger rotating about the axis.

Yet another method is disclosed, involving the steps of flowing current through a thermoelectric device having opposing surfaces to generate a temperature gradient between a first surface and a second surface of the thermoelectric device, flowing a fluid along a first heat exchanger formed and rotational about an axis, the first heat exchanger in thermal communication with the first surface. The flowing is at least partially provided via an auxiliary fan configured to rotate about the axis and to generate fluid flow along the first heat exchanger.

In one embodiment, the first heat exchanger is oriented such that fluid from the auxiliary fan flows through the heat exchanger along the rotational axis. Generating fluid flow along a second heat exchanger in a direction away from the rotational axis with rotation about the rotational axis may also be provided. The second heat exchanger may at least partially generate the fluid flow along the second heat exchanger. The method may also involve thermally isolating portions or segments of the heat exchanger in the direction of fluid flow.

Another method of conditioning flowing fluid involves the steps of generating a temperature gradient in a thermoelectric device between one surface and an opposing surface and flowing fluid along first and second heat exchangers formed about an axis and configured such that the fluid flows along the first heat exchanger and along the second heat exchanger generally away from the axis, the first heat exchanger in thermal communication with the one surface, and the second heat exchanger in thermal communication with the opposing surface. At least one of the first and second heat exchangers is formed to provide thermal isolation in the direction of fluid flow, such as by using a plurality of segments to form the at least one heat exchanger.

The method may further involve rotating the heat exchangers and thermoelectric device about the axis during operation, the heat exchangers operating to induce fluid flow through the heat exchangers. The heat exchangers and thermoelectric device may also be stationary, wherein fluid flow is generated

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along at least one of the first and second heat exchangers by rotating an auxiliary fan about the axis.

These and other features are disclosed in further detail below.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other features of the inventions will now be described with reference to the drawings of an embodiment in which like number indicate like parts throughout, and which are intended to illustrate and not to limit the inventions, and in which:

FIG. 1 is a perspective view of the heat exchanger of the present invention;

FIG. 2 is a perspective view of a rotary assembly of the heat exchanger of FIG. 1;

FIG. 3 is a cross-sectional view of the heat exchanger along line 3-3 of FIG. 1;

FIG. 4 is an enlarged cross-sectional view of a portion of the heat exchanger;

FIG. 5 is a top view of a rotor used with the heat exchanger;

FIG. 6 is a side view of the rotor of FIG. 4;

FIG. 7 is a schematic view of a seat temperature control system incorporating the heat exchanger of the present invention;

FIG. 8 is a perspective view of a cooler box that incorporates the heat exchanger;

FIG. 9 is a cross-sectional side view of a lid of the cooler box of FIG. 8;

FIG. 10 is a side view of a fan unit incorporating the heat exchanger of the present invention;

FIG. 11 is a side cross-sectional view of the fan unit of FIG. 10;

FIG. 12 is a perspective view of another embodiment of the heat exchanger;

FIG. 13 illustrates an embodiment of a rotary thermoelectric heat exchanger;

FIG. 14 depicts the embodiment of a rotary thermoelectric heat exchanger of FIG. 13 in a housing;

FIG. 15 depicts one portion of the rotary thermoelectric heat exchanger in the housing;

FIG. 16 depicts a cutaway of another embodiment of a rotary thermoelectric heat exchanger;

FIG. 17 depicts a cross-section of a portion of a thermoelectric heat exchanger; and

FIG. 18 depicts a portion of a thermoelectric heat exchanger, in which the heat exchangers are generally pancake-shaped, are stationary and attached to an insulator.

DETAILED DESCRIPTION

A variety of examples described below illustrate various configurations that may be employed to achieve desired improvements. The particular embodiments and examples are only illustrative and not intended in any way to restrict the general inventions presented and the various aspects and features of these inventions. In addition, it should be understood that the terms cooling side, heating side, cold side, hot side, cooler side and hotter side and the like do not indicate any particular temperature, but are relative terms. For examples, the "hot," "heating" or "hotter" side of a thermoelectric element or array may be at ambient temperature, with the "cold," "cooling" or "cooler" side at a cooler temperature than ambient. Conversely, the "cold," "cooling" or "cooler" side may be at ambient with the "hot," "heating" or "hotter" side at a higher temperature than ambient. Thus, the terms are relative to each other to indicate that one side of the thermoelectric is

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at a higher or lower temperature than the counter-designed side. In addition, fluid flow is referenced in the discussion below as having directions. When such references are made, they generally refer to the direction as depicted in the two dimensional figures. For example, fluid flow for the heat exchanger depicted in FIG. 13 may be described as away from or along an axis about which these heat exchangers are formed. However, it will be understood from the discussion that the flow when the device is rotating is not just away from the axis or along the axis but may actually take the form of a spiral or have a circular motion or other turbulent flow patterns. The terminology indicating "away" from the axis or "along" the axis or any other fluid flow direction described in the application is meant to be an illustrative generalization of the direction of flow as considered from the perspective of two dimensional figures.

As shown in FIG. 1, a heat exchanger unit 28 includes an outer housing 32 that defines an interior cavity 29 (FIG. 3) in which a rotor assembly 30 (FIGS. 2 and 3) is rotatably mounted for producing a conditioned airflow into and out of the outer housing 32. While other shapes are suitable, the outer housing 32 is shown as resembling a generally flat disc with a first surface or first wall 31 that corresponds to an upper or top surface if the housing 32 is placed in a seat bottom generally parallel to the ground. As used herein, up or upper will refer to a direction away from the ground. Down, lower or bottom will refer to a direction toward the ground. The relative direction of parts would alter if the entire orientation of housing 32 were changed, as may occur in actual use. A second wall 33, corresponding to a bottom surface, is opposite the first wall 31. The generally circular peripheries of walls 31, 33 are joined by side wall 35 to form an enclosure.

A first outlet 34 extends outwardly from the side wall 35 adjacent the first or upper wall 31 of the outer housing 32. A second outlet 36 extends outwardly from the side wall 35 adjacent the second, or lower wall 33. Advantageously the outlets 34, 36 extend generally tangential from the periphery of the housing 32. The outlets 34, 36 are shown extending in generally opposite directions, about 180° relative to each other. But depending on the particular direction the air needs to flow, the outlets 34, 36 could be located at other angles relative to each other, with 60°, 90° on either side of the housing 32, being the most likely relative positions. The outlets 34, 36 could exit in the same direction if desired, but then it would be advantageous to have insulation between the outlets to help maintain the temperature differential between the outlets.

A set of apertures 38 are centrally formed in the first or top wall 31 of the outer housing 32 to form a first inlet 38 that communicates with the interior cavity 29 formed and enclosed by the outer housing 32. Although not necessary, a second inlet 40 (FIG. 3) may also be located on the second or bottom wall 33 of the outer housing 32 opposite the first inlet 38.

As illustrated in FIGS. 2 and 3, the rotor assembly 30 generally comprises a plurality of components including an annular first rotor 42, an annular second rotor 44 disposed below the first rotor 42, and at least one annular thermoelectric device 46 interposed between, and in thermal communication with, the first rotor 42 and the second rotor 44. The thermoelectric device depicted is preferably a Peltier device which comprises at least one pair of dissimilar materials connected electrically in series and thermally in parallel, and typically comprises a series of n-type and p-type semiconductor elements connected electrically in series and thermally in parallel. Depending on the direction of current passing through the thermoelectric device 46, one surface will be heated and the opposing surface will be cooled. The thermoelectric device 46 generates a temperature differential that

causes heat to transfer by conduction through the rotors **42**, **44**. The greater the temperature differential, the greater the rate of heat transfer. The temperature differentials and efficiencies are expected to increase as the technology improves.

The rotors **42**, **44** comprise annular heat exchangers in direct thermal communication with the thermoelectric device **46** to conduct heat throughout the rotors **42**, **44**, primarily by thermal conduction to thereby form a short thermal path length between the rotors **42**, **44** and the thermoelectric device **46**. Depending on the material and construction of the rotors **42**, **44**, the rate of thermal conduction will vary. The rotors **42**, **44** also allow air to pass outward, such as in a radial direction, through the heat exchanger, and further comprise blades of fans that cause the air to pass outward through the rotors **42**, **44**. The heat exchanger thus forms the fan that causes the air to flow through the heat exchanger. Alternatively phrased, the fan that generates the air flow also forms the heat exchanger. In one embodiment, the fins of the heat exchanger comprise the blades or airfoils of the fan generating the air flow. Alternately, the heat exchanger could comprise a series of heat exchange surfaces that are configured to generate an airflow when the surfaces are rotated.

The rotors **42**, **44** are advantageously formed by taking a length of heat exchanger of aluminum or copper that is formed from a flat strip of metal having corrugated or accordion-like pleats folded so heat sinks and sources can be connected at the ends of the pleats where the metal folds to change direction. The pleats are orientated so air can flow along the corrugations of the heat exchanger. The opposing ends of that length of heat exchanger are curved toward each other, and then overlapped and fastened together either mechanically or by thermal or adhesive bonding. This bending forms the previously straight length into a circle so the air flows radially through what is now a circular heat exchanger. In this annular configuration the heat exchanger can effectively act as the blades of a squirrel cage fan or a circular fan. This method is advantageously, but not necessarily, used to form both the first rotor **42** and the second rotor **44**.

In the illustrated embodiment, the first rotor **42** is located on the supply side of the heat exchanger that supplies conditioned air to a user, and has an outer diameter that is smaller than the diameter of the second rotor **44**. The second rotor **44** is located on the waste side of the system and exhausts conditioned air, advantageously to a location that does not direct air to the supply side or that otherwise directs air to a location that could affect the user. Each of the components are axially aligned to rotate about a central axis aligned with a drive shaft or axle **52** of motor **50**. A disc-shaped connector **51** having a central aperture is disposed on top of the first rotor **42** and the motor **50**. The motor **50** may be directly coupled to the axle **52** or could be indirectly coupled, such as via a gear assembly.

The connector **51** mechanically couples at least one of the shaft **52** or motor **50** to the first rotor **42** so that the motor **50** is configured to rotatably drive the first rotor **42**, the thermoelectric device **46**, and the second rotor **44** about a common axis, as described in more detail below. The interior diameter of rotors **42**, **44** is advantageously large enough to allow motor **50** to be inserted inside the space formed inside the annular rotors **42**, **44**, to minimize the height of the unit along the longitudinal axis about which rotors **42**, **44** rotate.

As shown in FIG. 3, the rotor assembly **30** is mounted within the outer housing **32** on a drive axle **52** that, in the illustrated embodiment, is journaled at opposing ends of the axle on shaft bearings **54** which are advantageously mounted to walls **31**, **33**. The drive axle **52** of the rotor assembly **30** is axially aligned with the first and second inlets **38** and **40** of the

outer housing **32**. The outer housing **32** could also be equipped with only a single inlet or with more than two inlets.

The plane of the thermoelectric device **46** defines a boundary line **56** that divides the interior cavity **29** into an upper portion or supply side **58** and a lower portion or waste side **60**. The first rotor **42** is located within the upper portion or supply side **58** and the second rotor **44** is located within the lower portion or waste side **60**.

As shown in FIG. 3, the rotor assembly **30** further includes a first annular plate **63** that is disposed between a top edge of the thermoelectric device **46** and a bottom edge of the first rotor **42**. A second annular plate **65** is disposed between a bottom edge of the thermoelectric device **46** and the top of the second rotor **44** so that the thermoelectric device **46** is interposed between the first and second plates **63** and **65**. The first and second plates **63** and **65** are preferably manufactured of a material that is thermally conductive but is electrically insulative, such as, for example, alumina. In one embodiment, a heat-resistant, thermally-conductive adhesive, such as silver-filled silicon adhesive, is used to mount the first rotor **42** to the first plate **63** and the second rotor **44** to the second plate **65**. Alternately, plates **63** and **65** may be omitted and the first and second rotors **42** and **44** may be directly attached to the thermoelectric device **46**.

An annular, disc-like insulation member **64** of thermally insulated material extends from between the rotors **42**, **44**, radially outward and ends before it hits the inside of the side walls **35**. Advantageously the member **64** is positioned on top of the second annular plate **65** adjacent the inner and outer periphery of the thermoelectric device **46** and is placed generally in the plane containing boundary line **56**. The insulation member **64** is dimensioned to extend radially inward and outward from the thermoelectric device toward the motor **50** along the boundary line **56**. A gap **66** is defined between the outer periphery of the insulation disc **64** and the interior surface of the outer housing **32**, with the gap **66** forming an air bearing to reduce the passage of air across the gap **66**.

As shown in FIGS. 3 and 4, a thin and flexible annular seal **70** of thermally insulated material is positioned so as to extend radially inward from the interior surface of the outer housing **32** generally along the boundary line **56**. The annular seal **70** is preferably sized so that it overlaps, but does not contact the adjacent surface of the insulation member **64**. The annular seal **70** cooperates with the insulation member **64** to define a labyrinth seal around the outer periphery of the member **64** that thermally insulates the upper portion or supply side **58** of the interior cavity **29** from the lower portion or waste side **60** of the interior cavity **29**. The insulation member **64** and annular seal **70** prevent significant heat convection between the waste and main sides. The annular seal **70** can be in the form of an air bearing that facilitates rotation of the rotor assembly **30**. The insulation member **64** may comprise any of a wide variety of heat resistant, thermally-insulative materials, such as expanded polypropylene.

As illustrated in FIG. 4, at least a portion of the interior surface of the housing **32** advantageously is coated with a wicking material **78** that is adapted to absorb and conduct moisture. The wicking material **78** extends between the upper and lower portions **58**, **60**, and advantageously comprises a woven cotton fabric that has been texture coated to prevent microbe growth. The wicking material **78** absorbs condensed moisture expelled by centrifugal force from whichever rotor **42**, **44** produces the condensation, and conducts the moisture to the other rotor where it is evaporated by the heated air—in order to avoid accumulation in the interior cavity **33** and in passages distributing the cooled air. Advantageously the wicking material **78** absorbs enough moisture to prevent

accumulation in the downstream passages in fluid communication with whichever rotor **42**, **44** is cooled prompting a potential for condensation.

The annular seal **70** must allow the wicking material **78** to pass. Thus, the seal **70** may be connected to an exterior surface of the material **78**, may extend through the material **78** at intermittent locations, or may connect to side walls **35** at locations where the material **78** is absent. The material **70** could also extend outside of the interior cavity **33**.

As seen in FIG. **3**, electrically-conductive wires **80** are electrically coupled to the thermoelectric device **46** to provide an electrical potential thereto in a well known manner through brushes **84** that are in electrical communication with the rotating drive axle **52**. Because electrical current must be provided to the thermoelectric device **46** in a closed circuit, two brushes **84** are in electrical communication with the axle **52** and thermoelectric **46** through brush and slip-ring assemblies known in the art. Other electrical connections, such as, for example, an inductive coupling, can be devised given the present disclosure.

FIGS. **5** and **6** are top and side views, respectively, of the first rotor **42**. The structure of the second rotor **44** may be identical to that of the first rotor **42**, although the respective dimensions may differ. The following more detailed description of the first rotor **42** is therefore equally applicable to that of the second rotor **44**. The first rotor **42** comprises a strip of corrugated metal having two connected ends so that the first rotor **42** is annular in shape. The corrugations or accordion-like pleats in the first rotor **42** form a series of radially-extending fins or blades **91** that define a series of radially-extending chambers or spaces **92** therebetween. As seen in FIG. **4**, the width (i.e., the circumferential distance between adjacent fins **91**) of the chambers **92** gradually increases moving radially outward from a center point **90** of the first rotor **42**. Each rotor **42** and **44** has an inner radius R_1 and an outer radius R_2 . The spacing between adjacent fins **91** is sufficiently wide at the inner radius R_1 to allow air flow radially outward through the rotor **42**.

In the illustrated embodiment, the blades **91** comprise generally flat walls that are connected and extend radially outward from a center point **90** on the rotational axis of the rotor **42**. This design is not believed optimum from the aerodynamic viewpoint of moving the maximum volume of air through the rotor **42** for a given rotational speed or rotor size. The blades **91** may also be more aerodynamically configured to provide various airflow profiles. For example, the blades **91** may be s-shaped, c-shaped, etc. Alternately, the blades **91** may comprise any type of straight or curved surface that produces an airflow when the surfaces are rotated.

The outer radius R_2 preferably ranges from approximately 12-75 mm when incorporated into a temperature control system for a motor vehicle seat. The radial length of the blade **91**, the difference between the inner radius R_1 and outer radius R_2 , is approximately 10-40 mm when the heat exchanger **28** is incorporated into a temperature control system for a motor vehicle seat, as described below with reference to FIG. **7**. The blades **91** may have a height measured along the rotational axis, in the range of approximately 6-15 mm when used with car seats. Adjacent blades **91** are preferably spaced apart a distance of approximately 0.5-2 mm for a temperature control system for a seat. The thickness of the blades **91** when made of copper or aluminum is preferably in the range of approximately 0.05-0.2 mm when incorporated into a car seat.

In an alternative embodiment, the thermoelectric device **46** is replaced by a resistive heating element which converts electrical energy into heat energy. This resistive heating element does not have the cooling capability of the thermoelec-

tric device **46**, but it does provide heated air which may have wider applicability in certain climates.

As illustrated in FIG. **3**, in operation, the motor **50** rotates the axle **52** by activating the power source through a control, such as a manual switch or a thermostatically controlled switch. The motor is in driving communication with the first rotor **42**, the second rotor **44**, and the thermoelectric device **46** so as to rotate those components about the rotational axis of drive axle **52**. The rotation of the first rotor **42** creates a pressure differential that draws air into the supply side **58** of the interior cavity **29** through the first inlet **38**. The air flows into the spaces **92** and radially outward across the blades **91** of the first rotor **42**. The rotation of the rotor **42** imparts centrifugal force to the air that propels the air radially outward from rotor **42** so that the air travels out of the supply side **58** of the interior cavity **29** through the first outlet **34**.

In a similar manner, the second rotor **44** also rotates and draws air into the lower portion or waste side **60** of the interior cavity **29** through the second inlet **40** (or through either inlet **38** or **40** if only one inlet is provided). The air passes through the spaces **92** between the blades **91** of the second rotor **44**, radially outward across blades **91**, and is propelled out of the waste side **60** through the second outlet **36**. The divider **64** keeps the air flows from intermingling, and because it is thermally insulated, maintains a temperature differential between the supply side **58** and waste side **60**.

The electrical wires **80** also supply an electrical current to the thermoelectric device **46**, advantageously through shaft **52**, so that the thermoelectric device **46** heats the rotor **42** and cools rotor **44**, or cools rotor **42** and heats rotor **44**, depending on which direction the electrical current flows through the thermoelectric device **46**. As the air flows across the blades **91** of the first rotor **42** and the second rotor **44**, the air is either heated or cooled. That is, on the hot side of the thermoelectric device **46**, heat is transferred to the air from the heated fins of the rotor as the air flows thereover. On the cooled side of the thermoelectric device, heat is absorbed from the air as the air passes over the cooled rotor to thereby cool the air. The heat exchanger thus produces heated air through one outlet and cooled air through the other outlet. The heated or cooled air is then directed to the appropriate location in the seat for heating or cooling the passenger seat. The air with the undesired temperature is vented to a location where it will not noticeably affect the vehicle passengers. Preferably, the waste air is vented to a location such that the waste air is not drawn back into the outer housing **32**.

The first rotor **42** and the second rotor **44** simultaneously function as fan units for generating an airflow at a predetermined pressure and also as heat exchangers for transferring heat to and from the airflow and maintaining the airflow at the desired temperature. By combining the heat exchanger function into the fan that generates the air flow, several advantages are achieved. By forming the heat exchanger into an annular fan and nesting the motor inside the heat exchanger/fan, space and weight savings are achieved.

Current systems are about 45 mm in height, which is too big for many motor vehicles and other applications requiring a small size. Newly designed systems are about 30 mm in height, but a great number of motor vehicles still have seats too small to accommodate such fans underneath or around the seat, and few can accommodate that size within the seat. Fan and heat exchanger units **28** with a height below about 20-30 mm will accommodate a majority of automotive seats, and the present invention can allow such construction. But systems **28** of the present invention having a height of about 16 mm are believed possible, which is about half the height of the smallest systems currently available, and small enough to allow the

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use of the heating/cooling system inside a significant majority of seat bottoms and seat backs currently used in motor vehicles. The smaller size also benefits any application where size constraints are an issue.

This height reduction represents the distance between walls 31, 33 and associated ducting to carry the air to the location within the seat. The design of rotors 42, 44 can be used to vary the dimensions, with the heat exchanger surface area of blades 91 being a compromise between blade height, blade length, and diameter, and that area must be offset by the change in performance and rotational speed of the fan. Also, shorter rotors 42, 44 can be achieved by increasing the diameter of the rotors or by operating the rotors at higher speeds, which may increase noise.

Further, the design eliminates the interconnecting ducting between the fan and the heat exchanger, saving weight, size and pressure losses in the transmitted air. The small size also allows placement of heating and cooling systems directly in the seat bottoms and backs, further reducing the need for ducting, and especially reducing the need for ducting across the pivoted joints between seat bottoms and backs. The reduced ducting and its associated pressure losses and performance degradation, also allows the use of smaller fans, which use less energy and generate less noise.

Moreover, the consolidation of several parts and functions allows a reduced manufacturing cost and an increase in efficiency of the system. The drag normally caused by passing the air over the heat exchanger is significantly reduced because the heat exchanger forms the fan blades that generate the air flow. Further, adequate heating and cooling of a motor vehicle seat are believed to use about 1000 watts less than the power needed to provide the same comfort level to a passenger using the heating and cooling system of a motor vehicle—which must heat and cool the entire passenger compartment rather than the localized environment of the seat on which the passenger sits.

A further advantage is the reduction of noise because two small fans can be used. The rotors 42 and 44 preferably operate at a rotational speed in the range of approximately 2,000-5,000 revolutions per minute, although speeds of about 1000 rpm may be desirable in some applications, and higher speeds of up to 10,000 revolutions per minute in others. The rate of airflow of the main side of the heat exchanger is in the range of approximately 2-6 cubic feet per minute at a pressure of about 0.2-1 inches of water, with a flow rate of about 3-4 cfm being preferred. The rate of airflow of the waste side of the heat exchanger is in the range of approximately 2-10 cubic feet per minute, at a pressure of about 0.3-0.4 inches of water. The rotors 42, 44 with the blades acting as conductive heat exchanger as well as fan blades to move air, provide these needed air flows. In typical automobile use, 12 volt motors drive the rotors 42, 44. This fan flow rate and pressure are smaller than in prior seat systems where the fan had to generate enough pressure and air flow to provide air to both the bottom and backrest portions of the seat.

To further enhance the above advantages, in a further embodiment the blades 91 may comprise a series of independent walls mounted on an annular plate where the blades 91 are contoured or curved to provide a preselected airflow profile when the first rotor 42 rotates, advantageously a profile that is more efficient than the straight blades 91 described above while still conducting heat well and maintaining a low manufacturing cost. Further, the blades 91 as illustrated and described above are not optimized for minimizing noise, and noise reduction is an important consideration for equipment operating inside the passenger compartment of motor vehicles. A more refined design of the blades 91 could advantageously

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reduce noise. It is believed that the level of noise generated by rotation of the rotors 42 and 44 generally decreases as the number of blades 91 increases. To accommodate the thermal transfer use of the rotor blades 91, more blades are likely to be required than may be desirable for optimum performance if the rotors 42, 44 were designed solely for use as fans to move air—without regard to the heat transfer function and noise of the rotors 42, 44.

The compact design also reduces the weight of the unit. As mentioned, the blades 91 are preferably manufactured of a thermally conductive material, such as pure annealed aluminum, carbon, and copper, which are known to be highly thermally conductive materials. Other material may be used as scientific advances in conductive material are made. While copper is heavier than aluminum, its increased thermal conduction properties offer advantages and design options in configuring the rotor blades 91 to perform both heat transfer and air movement functions. The blades preferably have a thermal conductivity rate of greater than about 12 w/m^o K.

The conditioned air that flows out of the first and second outlets 34 and 36 may be put to any of a wide variety of uses. In one embodiment, the heat exchanger 28 is incorporated into a ventilation system for vehicle seats, such as for automobiles, as described below with reference to FIG. 7. It will be appreciated that the heat exchanger 28 could also be used in other applications as well.

As illustrated in FIG. 7, an automobile seat temperature control system 112 comprises at least one seat 114 and a pair of heat exchangers 28a and 28b (referred to collectively as “heat exchangers 28”) mounted therein. The heat exchangers 28 are of the type described above with reference to FIGS. 1-6. In the illustrated embodiment, the first heat exchanger 28a is mounted within a seat bottom 118 and the second heat exchanger 28b is mounted within a seat back 120. The heat exchangers may also be mounted adjacent any portion of the seat 114, such as below or on the side of the seat 114.

The seat 114 has a series of channels 116 for the passage of air. An outer covering 117 of the seat 114 surrounds a padding layer 119 through which the channels 116 extend. The outer covering 117 is desirably perforated or air-permeable to allow air to flow therethrough from the channels 116. The seat 114 also includes seat bottom 118 and seat back 120 extending upwardly therefrom for supporting a human body in a sitting position. The outer covering 117 may comprise any well known material for covering seats, such as perforated vinyl, cloth, perforated leather, etc. The padding layer of the seat 114 may comprise any well-known material for enhancing user comfort, such as reticulated foam.

As illustrated in FIG. 7, the first outlet 34 (FIG. 1) of the first heat exchanger 28a is attached to channels 116 that extend through the seat back 114. The first outlet 34 of the second heat exchanger 28 is attached to the channels 116 that extend through the seat bottom 118. Each of the heat exchangers 28 is electrically coupled to a power source via a control switch so that a user may selectively power the heat exchangers via the power switch. A control switch is also coupled to the heat exchangers 28 for reversing the polarity of the electrical current applied to the heat exchangers 28 in a well known manner. The control switch is used to switch the heat exchangers 28 between a heating and a cooling mode. In the heating mode, the heat exchangers 28 pump heated air into the seat 114. In the cooling mode, the heat exchangers pump cooled air into the seat 114. The heat exchangers 28 may also be coupled to separate power and temperature controllers for providing independently-controlled conditioned airflow to the seat back 114 and the seat bottom 120.

A feedback control system including a temperature sensor, such as a thermocouple, may also be provided. The system 112 may also be equipped with a control system for varying the speed of the rotors 42 and 44 to vary the flow rate. Those skilled in the art will appreciate that any of a wide variety of control devices may also be provided.

The channels 116 may comprise a series of plastic ducts or pipes that are coupled to at least one of the first and second outlets 34, 36 of the heat exchangers 28 and disposed within the seat 114. Advantageously, the ducts may be formed by heat sealing the plastic foam of which the seat is made, or by coating the duct with a sealant to reduce air loss through the duct. The channels could also comprise air gaps within a permeable material, such as reticulated foam, that allow air to flow therethrough. Additionally, the channels may comprise any type of passage for the flow of air, such as ducts, pipes, small holes, etc.

Preferably, a main duct 137 is connected to the first outlet 34 for routing the cooled or heated air to the seat 114 surface 117 via the channels 116. A waste duct 138 is connected to at least the second outlet 36 for routing the unwanted "waste" air to the outside environment away from the passenger occupying seat 114.

In operation, the power switch is activated to supply an electrical current to the heat exchangers 28. As discussed above, the thermoelectric device 46 and the main and second rotors 42 and 44 combine to generate a flow of heated or cooled air which is routed to the main ducts 137 and throughout the seat 114. The conditioned air flows out of the channels 116 through the permeable outer covering 117 to thereby cool or heat the occupant of the seat 114. Desirably, the waste air is routed away from the seats 114 through the waste ducts 138.

The waste ducts 138 can advantageously vent below the seat bottom 118 because the heating and cooling system in the passenger compartment can produce typically over 20 times the amount of heat or cool air as is exhausted through waste duct 138. As long as the waste ducts 138 do not vent directly on a passenger, toward a passenger, or on the inlets 38, 40 the environmental heating and cooling equipment will amply dissipate the output from waste ducts 138. A waste duct 138 connecting unit 28a located in the back portion 119 can vent below the seat bottom 118 without having a duct extend across the pivoted joint between the bottom portion 118 and backrest 119. Because the airflow of waste duct 138 is downward toward the seat bottom 118, two aligned openings, one at the bottom of back portion 119, and one in the seat bottom 118, are sufficient to convey the air to below the seat bottom 118.

As shown in FIG. 8, in another embodiment, the heat exchanger 28 is incorporated into a cooler, such as an ice chest 140. In the illustrated embodiment, the ice chest 140 comprises a rectangular box that includes a base wall 144 and four side walls 146 extending upwardly therefrom. A lid 150 is pivotably mounted on the four side walls 146 in a well known manner to provide access to a storage space 152 defined by the walls of the ice chest 140. The walls of the ice chest are desirably insulated in a well known manner to maintain the temperature of the storage space 152.

FIG. 9 is a cross-sectional side view of the lid 150 of the ice chest 140. At least one heat exchangers 28 of the type described above with reference to FIGS. 1-6 is disposed within the lid 150. The heat exchanger 28 is connected to a power source (not shown), such as a battery of the proper voltage and power, and is configured to operate in a cooling mode such that it outputs a flow of cold air at the first fan 42, as described above. The heat exchanger 28 is rotatably

mounted within the lid 150 such that the waste side of the heat exchanger 28 is positioned between top and bottom walls 156, 158, respectively, with an insulation member positioned to thermally separate the main and waste sides. The main side of the heat exchanger 28 is disposed immediately below the bottom wall 158. A cover unit 159 is positioned over the main side of the heat exchanger 28. The cover unit 159 includes a series of apertures to allow air to flow through the main side of the heat exchanger 28. The main side of the heat exchanger 28 is positioned within the storage space 152 of the ice chest 140 when the lid 150 is closed.

The waste side of the heat exchanger 28 is disposed between the top and bottom walls 156 and 158 of the lid 150. An inlet 38 extends through the top wall 156 to allow air to flow into and out of the heat exchanger 28. The lid 150 is preferably filled within insulative material around heat exchanger 28.

In operation, the heat exchanger 28 is powered in the cooling mode so that the first fan 42 generates a flow of cooled air within the storage space 152 when the lid 150 is closed. In this manner, the storage space 152 is maintained at a relatively cool temperature. The heated waste air is routed to the outside environment such as through an outlet in the top wall 156 of the lid 150. Any of a wide variety of articles, such as food, may be stored within the storage space 152.

With reference to FIG. 10, there is shown a fan unit 200 that is configured to be mounted adjacent or within a standard desk. The fan unit 200 includes a housing 202 that is pivotably mounted to base 204. The housing 202 is substantially cylindrical shaped and includes a conditioned air outlet 206 and one or more waste air outlets 208 around the periphery of the housing 202. An air inlet 210 is located in the housing 200 opposite the conditioned air outlet 206. A control switch 212 and a power cord 214 are coupled to the base 204 for selectively powering the fan unit 200 and/or the thermoelectric element 232 in a well known manner.

FIG. 11 is a cross-sectional view of the fan unit 200. An annular duct 216 is disposed within the housing 202 and defines the conditioned air outlet 206. A second duct 218 defines the waste air outlets 208. A drive axle 220 is rotatably mounted within the housing so as to be axially-aligned with the conditioned air outlet 206. In the illustrated embodiment, a motor 222 is drivingly coupled to the drive axle 220 via a drive belt 224. A rotor assembly 226 is mounted to the drive axle 220 so that the rotor assembly rotates with the drive axle 220.

The rotor assembly 220 comprises a main fan 228 adjacent the conditioned air outlet 206 and an annular waste fan 230 on the side of the main fan 228 opposite the conditioned air outlet 206. A thermoelectric element 232, such as a Peltier heat exchanger, is interposed between the main and waste fans 228 and 230. The main fan 228 has a circumference that is less than or equal to the circumference of the conditioned air outlet 206 so that the main fan is configured to cause air to flow through the conditioned air outlet 206. The waste fan 230 is positioned so to communicate with the waste outlet 208. The main and waste fans 228 and 230 may comprise any type of device that is configured to produce an air flow upon rotation. In one embodiment, the fans comprises flat discs having louvers 234 punched therethrough. The fans are preferably manufactured of a highly thermally conductive material.

In operation, the motor 22 is powered through a power source (not shown) in a well known manner. The thermoelectric device 232 cools the main fan 228 and heats the waste fan 230 (or vice versa) in the manner described above with respect to the previous embodiments. The fans also rotate to

produce a flow of conditioned and waste air through the conditioned air outlet **206** and the waste air outlet **208**, respectively. The air may be routed to cool a desired location, such as beneath a desk. If desired, ducts, hoses and other devices may be connected to the outlets to further direct the flow of air therefrom.

FIG. **12** shows another embodiment of a heat exchanger comprising a fan unit **170** having a plurality of air flow generating members, such as blades **172**, that rotate about an drive axle **174**. A motor **176** is drivingly connected to the axle **174**, either directly or indirectly, such as through a gear mechanism. One or more electrical heat generating devices, such as electrical resistors **180**, are mounted on the blades **172**. The resistors may be embedded within the blades **172** or may be painted thereon, such as with adhesive.

In operation, the resistors **180** are heated by applying an electrical current thereto and the axle **174** is rotated via the motor **176**. The blades **172** generate an airflow, which is heated by the resistors through a convective process. The fan unit **170** is thereby used to generate a heated airflow.

Given the above disclosure, other variations of this invention will be known to those skilled in the art. For example, the rotors **42**, **44** are shown connected to the rotating shaft **52** by plate **51** located adjacent the first or upper wall **31**. In this configuration the interior cavity formed by the inner diameters of rotors **42**, **44** are interconnected. It is believed possible to have the plate **51** contoured to the exterior shape of the top portion of motor **50** and then extend radially outward at about the plane containing the thermoelectric **46**. That would place a physical separation between the air flows entering rotors **42** and **44**. It is also believed possible to form the housing of motor **50** with a radial flange extending radially outward at about the plane containing boundary line **56**, with the motor **50** rotating, and thus provide a physical separation between the air flows entering the rotor **42** and **44**.

Enhanced embodiments of a thermoelectric heat exchanger which could be used in conditioned air seats and many other localized conditioned air applications are shown in FIGS. **13-18**.

A first embodiment of an enhanced thermoelectric heat exchanger **1300** is shown in FIG. **13A**. FIG. **13B** depicts a cross-section of the rotary heat exchanger **1300**. FIG. **13C** depicts an auxiliary fan blade insert **1310** for the heat exchanger **1300**. FIG. **13D** depicts a top view of the thermoelectric heat exchanger **1300** with the auxiliary fan **1310** in place. A thermoelectric device **1301** is attached so as to be in uniform and good thermal contact with a heat transfer member **1302**. A heat transfer fin array forming a first heat exchanger **1303** is in uniform and good thermal contact with the heat transfer member **1302**. The opposite side of the thermoelectric device **1301** is in uniform and good thermal contact with a second heat exchanger **1304**. In an alternative embodiment, a second heat transfer member (not shown) may be provided to conduct heat to the second heat exchanger **1304**. In the depicted embodiment, the thermoelectric device **1301** is arranged in a cylindrical form. Similarly, the heat transfer member **1302**, and heat exchangers **1303**, **1304** are cylindrical in form. All are formed about a central axis. The heat exchanger array **1303** is oriented so that as the assembly spins, fluid (not shown) is ducted in a generally outward direction (or away from the central axis). The heat exchanger **1304** is oriented so that fluid passes along the axis of rotation of the assembly.

The thermal contacts can be made by any means that provide uniform thermal contact with low thermal resistance. Some Examples are braised, soldered, thermally conductive glue or thermally conductive grease joints. Alternately, the

thermoelectric elements and the thermoelectric device may be integral with each other to achieve simplicity of manufacture, lower costs, reduce number of parts, improve thermal heat transfer or to achieve other advantages. For example, the fin array **1303** could be machined from an extension of the heat transfer member **1302** or the thermoelectric elements could be soldered to a suitable circuit pattern formed directly on a high thermal conductivity, electrical insulation layer on the heat transfer member.

FIG. **13C** depicts the auxiliary fan **1310** for the heat exchanger **1300**. The mounting hub **1312** of auxiliary fan **1310** may be inserted into the top of the central cylinder **1308** of the heat exchanger **1300**. In this manner, an annular gap or ring **1314** matches up with the upper exits of the heat exchanger **1304** blades. The auxiliary fan **1310** has fan blades **1316** which are configured to operate in conjunction with the heat exchanger fins **1304**. The fan hub's **1312** outside diameter is sized to be less than the inside diameter of the heat exchanger **1304**. Thus, the auxiliary fan hub **1312** fits within the heat exchanger **1300**. Preferably, the auxiliary fan blades **1316** extend outward above the heat exchanger **1304**, as depicted in the top view of the auxiliary fan **1310** in place with the heat exchanger **1300** of FIG. **13D**. As assembled, when the assembly rotates, the auxiliary fan blades **1316** act to move fluid outward or away from the axis of rotation. This action draws the fluid through the heat exchanger **1304** along the axis of rotation and outward along the auxiliary fan blades **1316**. An assembly view in a housing will be explained in further detail in FIG. **14**. Preferably, some of the auxiliary fan blades **1316** have cut-outs **1318** to facilitate increased airflow from the heat exchanger **1304** through the open ring **1314** and radially outward along the fan blades **1316**.

FIG. **14** depicts a preferred embodiment of the rotary thermoelectric heat exchanger assembly **1400** having a heat exchanger **1300** with auxiliary fan, a motor and a housing. The thermoelectric device **1401**, heat transfer member **1402** and heat exchangers **1403** and **1404** are as described in FIGS. **13A** and **13B**, and form the rotating heat exchanger **1300**. The heat exchanger **1304** is attached to an auxiliary fan **1427** and the motor rotor **1414** of an electric motor. The auxiliary fan **1427** corresponds to the auxiliary fan of FIG. **13C**. The motor rotor **1414**, fan assembly **1427** and rotating heat exchanger **1300** rotate as a unit. A filter **1407** surrounds the assembly fluid chamber **1408** formed by an outer wall **1429** and an inner wall **1410**. A flow directing member **1409** attached to the thermoelectric array **1401** guides fluid flow. Fan blades **1433** are part of the rotating auxiliary fan **1427**. A motor rotor **1414** and the thermoelectric array are attached to the auxiliary fan **1427**. A fluid chamber **1405** is formed by a wall **1431** and an insulator **1413**. A second chamber **1406** is formed by the insulator **1413** and the inner wall **1410**.

A contact **1424** is attached to the shaft **1415** of the motor rotor **1414** and mates with a stationary contact **1422**. An electrical wire and terminal assembly **1426** is attached to a rivet **1425** thence to a contact leaf **1423** and the contact **1422**. A second contact **1417** is insulated from the shaft **1415** by an electrically insulating sleeve **1416**. The contact **1417** mates with a contact **1418** that is attached to a contact leaf **1419** which, in turn, is in contact with a rivet **1420**, and thence, to a terminal assembly **1421**.

The motor rotor **1414** rotates on the motor base **1433** at a suitable velocity to draw fluid **1432** through the filter **1407** and radially inward through the duct **1408**. A first part of the fluid passes around the inner edge of the inner wall **1410** and through the heat exchanger **1403** and into the fluid chamber **1406**. A second portion of the fluid **1432** passes through the second heat exchanger **1404** and thence through the fan

blades **1433** and to the fluid chamber **1405**. The fluids in the chambers **1405** and **1406** have been pressurized by the fan assembly **1427**. Electric current passes from the terminal assembly **1421** through the stationary contact **1418** to a contact **1417** that is electrically isolated from the shaft **1415**. The circuit of the thermoelectric array **1401** is connected to the contact **1417** and to the shaft **1415** so that current from the terminal assembly **1421** passes through the rotating thermoelectric assembly **1401** and to the shaft **1415**. The contact **1424** is electrically connected to the shaft **1415** and mates with the stationary contact **1422**. Current from the shaft **1415** passes through the contacts **1424** and **1422** the contact leaf **1423** the rivet **1425** to the terminal assembly **1426** completing the system circuitry.

The thermoelectric device circuitry is such that current flow in once direction causes the inner side of the thermoelectric device to become hot and the outer side to become cold. When the current is reversed, the inner side becomes cold and the outer side becomes hot. In the first case, the outer side of the thermoelectric device **1401** cools the heat transfer assembly **1402** due to thermal conduction; thence the heat exchanger fin array **1403** and the fluid **1432** being pumped to the fluid chamber **1406** are cooled. Advantageously, the heat exchanger **1403** comprises a fin array or other blade based heat exchanger. The fluid **1432** collected in the fluid chamber **1406** is thus cooled, and pressurized, and exits through an opening (not shown) where it can be used as a cooling medium. Similarly, the second portion of the fluid is heated by passing through the heat exchanger **1404** that has been heated by the hot side of the thermoelectric device **1401**. Advantageously, the heat exchanger **1304** comprises a fin array or similar blade based heat exchanger. The hot fluid **1423** is pumped to high pressure by the rotating fan blades **1433** and collects in the fluid chamber **1405**. The heated fluid **1432** exits through a port (not shown) as a source of heated fluid. Alternatively, it is exhausted as waste heat, if cooling alone is required.

By reversing the direction of current flow, hot fluid will collect in the fluid chamber **1405** and cold fluid will collect in the fluid chamber **1406**. The rotational speed of the heat exchanger assembly and the current can be varied to achieve different pressures, fluid flow rates, and chamber temperatures.

Preferably, the insulator **1413** is designed to form an effective labyrinth seal where it is in proximity to the heat transfer array **1402** at **1412**. Convective heat transfer from the hot side to the cold side of the thermoelectric array preferably is further reduced by the inclusion of a thermally insulative seal **1411**. Preferably, the flow directing member **1409** is designed to keep fluid **1432** prior to entering the heat exchanger arrays, **1403** and **1404**, from stirring and thereby convectively transporting heat content from one array to the other.

The filter **1407** serves to remove particles and other contaminants from the fluid stream. For example, if the fluid is air containing hydrocarbon contaminants, the contaminants can be removed by incorporating activated charcoal or other suitable agent in the filter media. Similarly, the filter can have layers of various porosity to remove particulates of different sizes at several locations within it, so as to increase capacity, lower pressure drop across the filter and achieve high filtration efficiency.

FIG. **15** depicts the left portion of another embodiment of a rotary thermoelectric heat exchanger **1500**. The axis of rotation of this design is about the centerline **1513**. Contacts, electrical connections to the thermoelectric device **1501** and exit ports for fluid **1505** are not shown. The right portion is a mirror image of the left portion, with the exceptions of the

areas of the fluid chambers **1509** and **1510** which are portions of fan scrolls well-known to the art.

The outer surface of the thermoelectric device **1501** is in good, uniform thermal communication with a heat transfer member **1502**. The heat transfer member **1502** is divided into four sections, each relatively thermally isolated from one another compared with the thermal conductivity in the direction from the thermoelectric array **1501** to the rotary heat exchanger array **1503**. The rotary heat exchanger **1503** is similarly divided into four sections each in good, uniform thermal communication with a section of the heat transfer member **1502**. The thermoelectric device **1501** is attached in its inner surface to a rotary heat exchanger **1504**, which is divided into four sections, each preferably thermally isolated from the other. The above thermal isolation is consistent with the teachings of U.S. patent application Ser. No. 09/844,818, filed Apr. 27, 2001, which is incorporated by reference herein.

In general, in any of the embodiments in the description, the heat exchangers may be formed in segments or sections or in other manners to provide thermal isolation from section to section in the direction of fluid flow.

The rotary heat exchanger **1504** is mechanically attached to a rotor **1511** and fan blades **1519**. The rotor **1511** is attached to a motor rotor **1512**. The parts so attached rotate as a unit. A fluid chamber **1510** is formed by an outer wall **1514** and an insulator **1515**. A second chamber **1509** is formed by the insulator **1515** and an inner wall **1516**. A third chamber **1507** is formed by the inner wall **1507** and second outer wall **1518**. A filter **1506** surrounds the rotary thermoelectric heat exchanger **1500**. Fluid **1505** is drawn through the filter **1506**, thence through the fluid chamber **1507** where a first portion goes through the heat exchanger **1503** and a second portion through the heat exchanger **1504**. A flow directing member **1508** splits the fluid **1505** so that convective heat transfer is reduced from fluid stirring at the entrance to the rotary heat exchangers **1503** and **1504**. Current is passed through the thermoelectric as described in FIG. **14**.

If, for example, the outer side of the thermoelectric array **1501** is cooled, the thermal energy is transferred by the rotary heat exchanger **1502** cooling the first portion of the fluid **1506**. The rotational motion generates centrifugal forces on the fluid **1506** so that the cooled fluid **1506** enters the fluid chamber **1510** and is pressurized. The conditioned fluid exits through a port (not shown). In this example, the inner side transfers heat to the rotary heat exchanger **1504** and thence to a second portion of the fluid **1506**. The fan blades **1519** increase the pressure in the heated fluid **1506** and convey the fluid **1506** to the fluid chamber **1510**. The fluid **1506** exits the fluid chamber **1510** through a port (not shown). A seal **1517** prevents significant convective heat transfer between the cold and hot fluid **1506** streams.

This assembly is capable of greater cooling or more efficient operation than the design of FIG. **14** due to the use of thermal isolation. As depicted, the heat transfer member **1502** and rotary heat exchangers **1503** and **1504** are divided into four sections. Other numbers of sections can be used. Performance increases with more sections and with higher material thermal conductivity.

In the preferred embodiment, the heat exchanger array **1503** is not aligned so that the fluid flows radially from the axis of the spin of the fan assembly **1511**. Advantageously, a system incorporates a fan duct **1520** on to the rotary heat exchanger **1503** so as to maintain thermal isolation while-directing fluid flow through all sections.

FIG. **16** depicts another embodiment of a thermoelectric heat exchanger with thermal isolation. A cutaway portion of a rotary thermoelectric heat exchanger system **1600** is shown

with the centerline **1621** to the right as in FIG. **15**. Again, contacts, thermoelectric circuitry, current flow and conditioned fluid exit ports are omitted for clarity. The system consists of a washer-shaped rotary thermoelectric device **1601** with a first rotary heat exchanger **1602** divided into four sections and a second rotary heat exchanger **1603** also divided into four sections, each in good, uniform thermal contact with the rotary thermoelectric array **1601**. These parts are attached to a fan assembly **1620**, which has two sets of fan blades **1608** and **1609**, and in turn is attached to a motor rotor **1619**. All of these parts rotate as a unit driven by the electric motor **1622**.

A filter **1606** surrounds the assembly. A first wall **1610** and an inner insulator or wall **1618** form a fluid chamber **1607**. A second fluid chamber **1613** is formed by the inner wall **1618** and an insulator **1611**. A third chamber **1614** is formed by the insulator **1611** and a second wall **1612**.

As in FIG. **14**, by way of example, when suitable current is passed through the rotary thermoelectric device **1601** the side in thermal contact with the rotary heat exchanger **1602** is cooled, and the opposite side is heated. If the current is reversed, the cold side becomes hot, and the hot side becomes cold.

Fluid **1606** passes through the filter **1605** and flows along the chamber **1607**. A first portion passes through the rotary heat exchanger **1602** where, for example, it is cooled and then goes into the fluid chamber **1613**. A second portion passes through the rotary heat exchanger **1603** where it is heated and then goes into the fluid chamber **1614**. The rotation of the fan assembly **1620** pressurizes the fluid in the fluid chambers **1613** and **1614**. Advantageously, a flow-directing member **1604** serves to prevent stirring of the fluid **1606** as previously discussed in FIG. **14**.

The rotary heat exchangers **1602** and **1603** are formed in sections to increase performance through thermal isolation in the direction of fluid flow as referenced in FIG. **15**.

FIG. **17** depicts a section of a rotary thermoelectric heat exchanger assembly **1700** with a centerline **1716** at the right. A rotary thermoelectric device **1701** is in good, uniform thermal contact with a rotary heat transfer member **1703** that is divided into sections and thence, to a rotary heat exchanger **1702**, which is divided into corresponding sections. The other side of the rotary thermoelectric array **1701** is attached to a rotary heat exchanger **1704** that is divided into sections, and is attached to a fan assembly **1719**. As with the prior figures, the division into sections or segments provides thermal isolation in the direction of fluid flow to increase efficiency of the unit. The fan assembly **1719** contains fan blades **1712**. It is attached to a motor rotor **1714**. Preferably, all parts attached to the fan assembly **1719** rotate in unison.

A chamber **1708** is formed by an upper wall **1721** and first insulator or wall **1720**. A fluid chamber **1710** is formed by the first insulator **1720** and an insulator **1713**. A chamber **1707** is formed by the insulator **1713** and a second insulator or wall **1709**. A fluid chamber **1711** is formed by the insulator **1709** and a lower outer wall **1718**. A filter **1706** surrounds the assembly.

The operation of the rotary thermoelectric heat exchanger **1700**, is similar to that of FIG. **15**, except that the fluid **1705** flows in a generally upward direction through the heat exchanger **1702** and downward through the heat exchanger **1703**. In accordance with the teachings of patent application Ser. No. 09/844,818, this can further improve efficiency in some circumstances over that of the configuration of FIG. **15**.

As in FIG. **15**, if fluid **1706** flows on one side of the rotary thermoelectric array **1701**, it can be heated and the other side cooled.

The system of FIG. **17** incorporates two walls **1709** and **1715** that separate flows by providing suitable barriers to convective heat transport between the hot and cold side fluids. The wall or flow directing member **1715** plays a similar role, and also acts to direct and smooth the flow of fluid **1705** as it enters the rotary heat exchanger **1704**. It also incorporates a duct **1717** for the same purposes described in FIG. **15**.

FIG. **18** depicts a portion of a thermoelectric heat exchanger system **1800**, in which the heat exchangers **1802** and **1803**, and the thermoelectric device **1801** are generally pancake-shaped, are stationary and are attached to an insulator **1813**. The portion shown is generally rotationally symmetrical about the centerline **1816**. The parts can be of the same general structure as those described in FIG. **16**. Omitted for clarity, are details of electrical circuitry current paths and terminals that power the thermoelectric element array **1801**. However, in this configuration, no contacts are required as the thermoelectric array is stationary.

A fan assembly **1812** with the fan blades **1809** is attached to a motor rotor **1808**. A filter **1805** is attached to the lower part of the assembly, with its upper most surface positioned by grillwork or radial ribs **1806**. The filter **1805**, an insulated flow directing member **1815** and fan assembly **1812** form a chamber **1807**. A first fluid chamber **1810** is formed by a portion of the insulated flow directing member **1815** and the insulator **1813**. A second fluid chamber **1811** is formed by the insulator **1813** and a wall **1814**.

Fluid **1804** passes through the filter **1805** into the chamber **1807**. The fluid **1805** is pressurized as it passes by the fan blades **1809**. A first portion passes through the heat exchanger **1802** where, for example, it is cooled. The cooled fluid **1805** passes into a chamber **1810** from where it exits the assembly through a port (not shown). A second portion of the fluid is heated as it passes through the heat exchanger **1803** and enters the chamber **1811**. It exits the assembly through a port (not shown).

As with the previous embodiments of FIGS. **15**, **16** and **17**, the heat exchangers **1802**, **1803** are formed in sections or segments to provide thermal isolation in the direction of fluid flow. As explained above, this improves efficiency of the thermal electric system.

The method and apparatus of the present invention are applicable to many uses, such as seats and wheelchairs, but it is not limited to use in seats. The method and apparatus is useful anywhere a localized flow of conditioned air is desired.

The present apparatus and method is not limited to the use of air or other gases. Indeed, some gases, such as helium, have greater thermal conductivity than air and are desirable in certain applications, while other gasses such as oxygen, nitrogen or argon may be more desirable in other applications. A variety of gases and gas mixtures can be used as the particular application requires.

Further, liquids can be used with the present invention. By applying appropriate liquid seals and insulators known in the art, the liquid circulating through the heat exchanger can be kept from affecting the performance of electrical contacts, the thermoelectric device, and any other electrical components. Thus, liquids such as water and antifreeze are contemplated for use with the present method and apparatus, as are liquid metals such as liquid sodium. Also contemplated are slurries of fluids and solids. The particular fluid used will depend upon the application. The increased thermal conductivity achieved by passing liquids over the rotating heat exchanger offer the possibility of increased heat conduction over that of less dense and less conductive gases. Whether a liquid or gas is most advantageous will vary with the particular applica-

tion. For ease of reference, the term "fluid" is used to refer to gases, liquids, slurries and combinations thereof.

Because the temperature change available from a thermoelectric system can be significant, the rotating heat exchangers of the present invention have potential applicability to a wide variety of uses. The method and apparatus described herein are generally applicable to any situation where there is a desire to pump a thermally conditioned fluid. Such applications include constant temperature devices, as for example devices using a reference temperature as in a thermocouple assembly. Another exemplary application is in componentry for constant temperature baths for laboratory equipment and experiments. The method and apparatus described herein are particularly useful for applications requiring low flow rates and/or small temperature changes, but the invention is not so limited and may find application in situations requiring large flow rates and/or substantial temperature differences.

By placing a temperature sensor at a predetermined location, whether on the heat exchanger, the rotating fan, upstream or downstream of the heat exchanger, and electronically controlling the thermoelectric and the fan rotation, a controlled stream of thermally conditioned fluid can be provided to maintain the temperature at a predetermined temperature, or to provide predetermined thermal conditions. Thus, the invention provides advantages where localized thermal control is desired, as in vehicle seats, water-beds, aquariums, water coolers, and cooling of beverages such as wine and punch.

Further, this device and method find particular application in situations where a fluid of differing temperature is desired at various times. The device may be operated as a fan capable of heating and cooling. The thermoelectric aspect can be activated when desired to thermally condition the fluid. Thus a heated, cooled, or neutral temperature fluid can be provided by the same device and method.

Although the foregoing description is of several preferred embodiments and has shown, described, and pointed out certain novel features of the inventions, it will be understood that various omissions, substitutions, combinations and changes in the form of the detail of the apparatus as illustrated as well as the uses thereof, may be made by those skilled in the art without departing from the spirit of the present invention. Also, one or more various components of one figure or embodiment may be used in different combinations with components of other figures to produce specific combinations not pictured in any one figure. For example, the fluid flow direction through heat exchanger **1802** of FIG. **18** could be reversed by adding an insulating wall to the end of the thermoelectric device **1801** so as to create an additional fluid chamber. In this example, the fluid would be pulled toward the rotational axis and then could be pumped outward through a second fan blade attached to fan rotor **1812** and exit in a generally radially outward direction through yet an additional fluid chamber with its lower side formed by the insulated flow directing member **1815**. Thus, in this example, FIG. **18** is combined with opposing flow as described in FIG. **17**, has the number of flow passages of FIG. **17**, and the number of fan blades that are not heat exchangers of FIG. **16**. Consequently, the scope of the present invention should not be limited by the foregoing discussion, which is intended to illustrate rather than limit the scope of the invention. The words used in the attached claims are used in their ordinary meaning sense, with no special or restrictive meaning intended by anything stated in the above description.

What is claimed is:

[1. A system for providing a conditioned fluid, comprising: a motor including a stator and a rotor that extends about an axis and that rotates relative to the stator; and a thermoelectric element defining an opening therethrough about the axis, the thermoelectric element coupled to the rotor, wherein the motor extends through the opening in the thermoelectric element.]

[2. The system of claim **1**, further comprising first and second heat exchangers, the first heat exchanger disposed on one side of the thermoelectric element and the second heat exchanger disposed on another side of the thermoelectric element.]

[3. The system of claim **2**, wherein the heat exchangers and the thermoelectric device rotate about an axis of the rotor, the heat exchangers configured to induce a fluid flow along the heat exchangers.]

[4. The system of claim **1**, wherein the thermoelectric element has a generally planar first side adjacent the first heat exchanger and has a generally planar second side adjacent the second heat exchanger.]

[5. The system of claim **1**, wherein the stator is disposed within the rotor.]

[6. The system of claim **1**, wherein the thermoelectric element is a Peltier element.]

[7. A method for conditioning a fluid flow, comprising: providing a current to a rotor to cause the rotor to rotate relative to a stator about an axis of rotation; and

supplying a current to a thermoelectric element coupled to the rotor to provide a temperature differential across the thermoelectric element, the thermoelectric element defining an opening therein about said axis of rotation, wherein the rotor is disposed along the axis of rotation and extends through the opening in the thermoelectric element.]

[8. The method of claim **7**, wherein rotating the rotor includes rotating first and second heat exchangers about an axis of the rotor, the first and second heat exchangers coupled to the thermoelectric element.]

[9. The method of claim **8**, wherein rotation of the first and second heat exchangers induces a fluid flow along the first and second heat exchangers.]

[10. The method of claim **7**, wherein the rotor rotates about the stator.]

[11. A system for providing conditioned fluid to a seat, comprising:

a thermoelectric unit configured to convert electrical energy into thermal energy to generate a temperature change in response to an electrical current applied to the unit, the thermoelectric unit mounted so as to rotate about a rotational axis, the thermoelectric unit defining an opening therein about the rotational axis;

a heat transfer unit having an outlet in fluid communication with a seat, the heat transfer unit comprising:

a flow generator rotatable about the axis, the flow generator configured to induce a fluid flow when rotated, the flow generator in conductive thermal communication with the thermoelectric unit so that the flow generator conducts the temperature change generated by the heat transfer unit to transfer the temperature change to the fluid flowing across the heat transfer unit; and

a housing having an inlet and an outlet on an exterior of the flow generator, the housing and flow generator cooperating to intake fluid along the rotational axis and to expel temperature conditioned fluid from the

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housing in a plane orthogonal to the rotational axis, the flow generator defining a recess into which at least a portion of a motor is positioned, the motor disposed along the axis of rotation and extending through the opening in the thermoelectric element, the motor configured to rotate the flow generator.]

[12. The system of claim 11, wherein at least one of the inlet and outlet of the housing is on a periphery of the flow generator.]

[13. An apparatus for thermally conditioning a fluid, comprising:

a thermoelectric unit configured to convert electrical energy into thermal energy to produce a temperature change in response to an electrical current being applied to the unit, the thermoelectric unit comprising a circular disk having first and second opposing surfaces, the unit mounted so as to rotate about a rotational axis extending through the center of the disk; and

an annular heat transfer unit having an inner diameter and an outer diameter and placed in conductive thermal communication with the thermoelectric device, the heat transfer unit mounted on one of the first and second opposing surfaces and configured to rotate about the axis, the heat transfer device having thermally radiating surfaces arranged to induce a fluid flow across the first and second surfaces outward from the rotational axis when rotated about the axis, the heat transfer device having a height measured along the rotational axis and the diameters being measured along an axis orthogonal to the rotational axis,

wherein the distance between the inner and outer diameters is greater than the height.]

[14. An apparatus for thermally conditioning a fluid, comprising:

a thermoelectric device configured to convert electrical energy into thermal energy to produce a temperature change in response to an electrical current being applied to the device, the thermoelectric device comprising a circular disk having first and second opposing surfaces, the thermoelectric device mounted so as to rotate about a rotational axis extending through the center of the disk; and

an annular heat transfer unit comprising:

a first series of heat transfer surfaces in conductive thermal communication with the first surface of the thermoelectric device, the first series of heat transfer surfaces aligned with a plurality of axes orthogonal to the rotational axis; and

a second series of heat transfer surfaces in conductive thermal communication with the second surface of the thermoelectric unit, the second series of heat transfer surfaces aligned with a plurality of axes orthogonal to the rotational axis,

wherein at least a portion of the first and second series of heat transfer surfaces comprise folds of a thermally conductive material, the first and second series of heat transfer surfaces further configured to induce a fluid flow across the surfaces outward from the rotational axis when rotated about the axis.]

15. A thermal conditioning device comprising:

a housing having a fluid inlet, an interior cavity and at least one fluid outlet;

a fan positioned within the interior cavity, said fan configured to selectively transfer a fluid from the fluid inlet to the at least one fluid outlet;

wherein the fan is configured to selectively rotate about an axis;

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at least one thermoelectric device positioned within the cavity of the housing and generally radially away from the axis of the fan, said at least one thermoelectric device having a first surface and a second surface, said second surface opposite of said first surface,

wherein the at least one thermoelectric device is completely positioned within the cavity of the housing through which fluid is configured to pass;

wherein the at least one thermoelectric device is adapted to generate a temperature gradient between the first surface and the second surface in response to an electrical current flowing through said at least one thermoelectric device;

a first heat exchanger positioned along the first surface of the at least one thermoelectric device, said first heat exchanger being in thermal communication with the first surface of the at least one thermoelectric device; and a second heat exchanger positioned along the second surface of the at least one thermoelectric device, said second heat exchanger being in thermal communication with the second surface of the at least one thermoelectric device;

wherein the first and second heat exchangers are generally positioned between the fluid inlet and the at least one fluid outlet to selectively temperature condition a fluid passing through the cavity of the housing; and

wherein the at least one thermoelectric device and the first and second heat exchangers are stationary within the thermal conditioning device; and

a divider positioned within the interior cavity and extending across at least a portion of the housing associated with the at least one fluid outlet;

wherein the divider generally abuts the at least one thermoelectric device so as to maintain fluid passing through or near the first heat exchanger separate from fluid passing through or near the second heat exchanger;

wherein the divider comprises a continuous physical barrier that divides at least a portion of the cavity of the housing into a first fluid chamber and a second fluid chamber; and

wherein the divider prevents fluid communication between the first fluid chamber and the second fluid chamber, both when the thermal conditioning device is in use and when the thermal conditioning device is not in use.

16. The device of claim 15, wherein the at least one thermoelectric device and the first and second heat exchangers are oriented radially around the fan.

17. The device of claim 15, wherein the at least one thermoelectric device comprises a Peltier element.

18. The device of claim 15, wherein the housing comprises a main fluid outlet and a waste fluid outlet, the said main fluid outlet being configured to receive a thermally-conditioned fluid passing through the first heat exchanger, and said waste fluid outlet being configured to receive a thermally-conditioned fluid passing through the second heat exchanger.

19. The device of claim 18, wherein the main fluid outlet is configured to be in fluid communication with at least one fluid channel formed within a climate controlled seating assembly, the fan being adapted to transfer a fluid from the fluid inlet of the device through the at least one fluid channel of the seating assembly.

20. The device of claim 18, wherein the main fluid outlet and the waste fluid outlet are separated by thermal insulation.

21. The device of claim 15, wherein the at least one thermoelectric device and the first and second heat exchangers are oriented around an outer periphery of the fan.

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22. The device of claim 15, wherein the device comprises at least two separate thermoelectric devices positioned around a periphery of the fan.

23. The device of claim 15, wherein at least one of the first and second heat exchangers is oriented so that a fluid being transferred by the fan enters at least one of the first and second heat exchangers in a direction that is generally perpendicular to the axis of the fan.

24. The device of claim 15, wherein at least one of the first and second heat exchangers is oriented so that a fluid being transferred by the fan enters at least one of the first and second heat exchangers in a direction that is at an angle relative to the axis.

25. The device of claim 15, wherein the at least one of the first and second heat exchangers comprises segments in order to provide thermal isolation in a direction of fluid flow.

26. The device of claim 15, wherein the device is configured for use with a climate controlled seating assembly.

27. A thermoelectric heat exchanger system comprising: at least one thermoelectric device positioned about an axis, said at least one thermoelectric device being configured to generate a temperature gradient between one surface and an opposing surface in response to electrical current flowing through said at least one thermoelectric device;

first and second heat exchangers positioned about the axis and configured such that fluid flows along the first heat exchanger and along the second heat exchanger generally away from the axis, the first heat exchanger being in thermal communication with the one surface of the at least one thermoelectric device, and the second heat exchanger being in thermal communication with the opposing surface of the at least one thermoelectric device; and

an auxiliary fan that is configured to rotate about the axis to selectively generate fluid flow along at least one of the first and second heat exchangers;

wherein the at least one thermoelectric device is positioned within an interior cavity of a housing of the thermoelectric heat exchanger system, wherein the fluid flow generated by the auxiliary fan is configured to pass through said interior cavity;

wherein the housing comprises a fluid inlet and at least one fluid outlet;

wherein the first and second heat exchangers are stationary relative to the auxiliary fan; and

wherein a direction of fluid flow through at least one of the first and second heat exchangers is generally titled relative to the axis; and

a divider positioned within the interior cavity immediately adjacent the at least one thermoelectric device, said divider defining a first outlet passage and a second outlet passage within the at least one fluid outlet;

wherein the divider is configured to keep fluid passing through or near the first heat exchanger from intermingling with fluid passing through or near the second heat exchanger;

wherein the divider comprises a continuous physical barrier so that the first outlet passage is not in fluid communication with the second outlet passage, both when the system is activated and when the systems is inactivated.

28. The system of claim 27, wherein the direction of fluid flow through at least one of the first and second heat exchangers is generally radially away from the axis.

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29. The system of claim 27, wherein the direction of fluid flow through at least one of the first and second heat exchangers is generally perpendicular to the axis.

30. The system of claim 27, wherein the direction of fluid flow through at least one of the first and second heat exchangers is at an angle relative to the axis and a direction perpendicular to the axis.

31. The system of claim 27, wherein the at least one thermoelectric device and the first and second heat exchangers are oriented around an outer periphery of the auxiliary fan.

32. A thermoelectric heat exchanger system comprising: at least one thermoelectric device positioned about an axis, said at least one thermoelectric device being configured to generate a temperature gradient between one surface and an opposing surface in response to electrical current flowing through said at least one thermoelectric device;

first and second heat exchangers positioned about the axis and configured such that fluid flows along the first heat exchanger and along the second heat exchanger generally away from the axis, the first heat exchanger being in thermal communication with the one surface of the at least one thermoelectric device, and the second heat exchanger being in thermal communication with the opposing surface of the at least one thermoelectric device; and

an auxiliary fan that is configured to rotate about the axis to selectively generate fluid flow along at least one of the first and second heat exchangers;

wherein the at least one thermoelectric device is positioned within an interior cavity of a housing of the thermoelectric heat exchanger system, wherein the fluid flow generated by the auxiliary fan is configured to pass through said interior cavity;

wherein fluid flow through at least one of the first and second heat exchangers is in a generally radial direction away from the axis; and

a divider positioned within the interior cavity and extending across at least a portion of the housing associated with the at least one fluid outlet;

wherein the divider generally abuts the at least one thermoelectric device so as to maintain fluid passing through or near the first heat exchanger separate from fluid passing through or near the second heat exchanger;

wherein the divider comprises a continuous physical barrier that prevents all fluid flow across it regardless of whether the system is activated or deactivated.

33. The system of claim 32, wherein the first and second heat exchangers are stationary relative to the auxiliary fan.

34. The system of claim 32, wherein fluid passing through the first heat exchanger is in fluid communication with a first outlet, and fluid passing through the second heat exchanger is in fluid communication with a second outlet, said first outlet being generally thermally isolated from said second outlet.

35. The system of claim 32, wherein the at least one thermoelectric device and the first and second heat exchangers are positioned around an outer periphery of the auxiliary fan.

36. The system of claim 35, wherein the at least one thermoelectric device and the first and second heat exchangers are positioned generally continuously around the outer periphery of the auxiliary fan.

37. The system of claim 35, wherein the system comprises a plurality of thermoelectric devices positioned around the outer periphery of the auxiliary fan.

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38. A heat exchanger system comprising:
 a housing having an inlet, an interior cavity and at least one outlet;
 an auxiliary fan configured to rotate about a rotational axis to selectively generate fluid flow through the housing from the inlet to the at least one outlet;
 at least one thermoelectric device positioned entirely within the cavity of the housing and generally radially away from an outer periphery of the auxiliary fan; and
 at least one first heat exchanger in thermal communication with a first side of the at least one thermoelectric device;
 at least one second heat exchanger in thermal communication with a second side of the at least one thermoelectric device, said first and second heat exchangers being configured to selectively heat or cool a fluid passing therethrough;
 wherein the first side of the at least one thermoelectric device is opposite of the second side of the at least one thermoelectric device;
 wherein the at least one thermoelectric device and the first and second heat exchangers are stationary relative to the auxiliary fan; and
 wherein the first and second heat exchangers are oriented so that a fluid being transferred by the auxiliary fan passes through said first and second heat exchangers at an angle relative to the rotational axis of the auxiliary fan; and
 a divider positioned within the interior cavity of the housing, said divider extending from the at least one thermoelectric device to and through the at least one outlet;
 wherein the divider is configured to keep fluid passing through the at least one first heat exchanger from intermingling with fluid passing through the at least one second heat exchanger;
 wherein the divider comprises a continuous physical barrier that divides at least a portion of the cavity of the housing into a first outlet passage and a second outlet passage; and
 wherein the divider prevents the passage of fluids from the first outlet passage to the second outlet passage, and vice versa, both when the system is operating and when the system is not operating.

39. A climate controlled seat assembly comprising:
 a seat back portion;
 a seat bottom portion;

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at least one channel formed within at least one of the seat back portion and the seat bottom portion, said at least one channel configured to receive a thermally conditioned fluid and deliver said thermally conditioned fluid toward a seated occupant;
 at least one heat exchanger device configured to selectively deliver a fluid through the at least one channel, said at least one heat exchanger device comprising:
 a housing having an inlet, an interior cavity and an outlet;
 a fan configured to rotate about an axis to selectively generate fluid flow from the inlet to the outlet;
 at least one thermoelectric device positioned entirely within the cavity of the housing and generally radially away from an outer periphery of the fan; and
 at least one first heat exchanger in thermal communication with a first side of the at least one thermoelectric device, and at least one second heat exchanger in thermal communication with a second side of the at least one thermoelectric device, said at least one first heat exchanger and said at least one second heat exchanger being configured to selectively heat or cool a fluid passing there-through;
 wherein the at least one thermoelectric device, the at least one first heat exchanger and the at least one second heat exchanger are stationary within the housing; and
 wherein fluid flow through the at least one first heat exchanger and the at least one second heat exchanger is in a generally radial direction away from the axis of the fan; and
 a divider positioned within the interior cavity of the housing and abutting the at least one thermoelectric device, the divider extending from the at least one thermoelectric device to the outlet;
 wherein the divider is configured to maintain fluid passing through or near the at least one first heat exchanger separate from fluid passing through or near the at least one second heat exchanger;
 wherein the outlet of the at least one heat exchanger device is in fluid communication with the at least one channel formed within the seat back portion or the seat bottom portion; and
 wherein the divider is a continuous physical barrier that prevents fluid flow across it both when the fan is activated and when the fan is deactivated.

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