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[54] **PHOTOGRAPHIC ELEMENTS CONTAINING DIRECT-POSITIVE EMULSIONS AND PROCESSES FOR THEIR USE**

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Related U.S. Patent Documents

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[58] Field of Search **430/409, 502, 509, 567, 430/410, 598, 603, 605, 608, 564, 940**

[56] **References Cited**

U.S. PATENT DOCUMENTS

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2,592,250 4/1952 Davey et al. 430/569
3,206,313 9/1965 Porter et al. 430/599
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3,615,573 10/1971 Smith et al. 430/567
3,761,276 9/1973 Evans 430/567

3,846,128 11/1974 Thomas et al. 430/219
3,846,135 11/1974 Helmig et al. 430/496
3,850,637 11/1974 Evans 430/409
3,854,953 12/1974 Shiba et al. 430/505
3,859,093 1/1975 Beckey 430/411
3,923,513 12/1975 Evans 430/598
3,942,986 3/1976 Florens 430/572
4,023,972 5/1977 Vanassche et al. 430/567
4,035,185 7/1977 Atwell et al. 430/569
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Zelikman and Levi, *Making and Coating Photographic Emulsions*, Focal Press, 1964, pp. 234-238.

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[57] **ABSTRACT**

Photographic elements particularly adapted for forming direct-positive images are disclosed in which a radiation-sensitive core-shell emulsion layer and a silver halide emulsion layer incapable of forming a surface latent image within the direct-positive exposure latitude of the first emulsion layer and containing a grain population capable of internally forming a latent image by internally trapping photolytically generated electrons are both present. The photographic elements are capable of exhibiting increased covering power, greater maximum density, and increased speed.

22 Claims, No Drawings

**PHOTOGRAPHIC ELEMENTS CONTAINING
DIRECT-POSITIVE EMULSIONS AND
PROCESSES FOR THEIR USE**

Matter enclosed in heavy brackets [] appears in the original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue.

This application is a reissue application for U.S. Pat. No. 4,444,874, based on U.S. Ser. No. 418,313, filed Sept. 15, 1982, by Robert A. Silverman and Harry A. Hoyer.

This invention relates to improved photographic elements incorporating direct-positive core-shell emulsions. The invention further relates to processes of obtaining direct-positive images from imagewise exposed photographic elements.

BACKGROUND OF THE INVENTION

Photographic elements which produce images having an optical density directly related to the radiation received on exposure are said to be negative-working. A positive photographic image can be formed by producing a negative photographic image and then forming a second photographic image which is a negative of the first negative—that is, a positive image. A direct-positive image is understood in photography to be a positive image that is formed without first forming a negative image. Direct-positive photography is advantageous in providing a more straight-forward approach to obtaining positive photographic images.

A conventional approach to forming direct-positive images is to use photographic elements employing internal latent image-forming silver halide grains. After imagewise exposure, the silver halide grains are developed with a surface developer—that is, one which will leave the latent image sites within the silver halide grains substantially unrevealed. Simultaneously, either by uniform light exposure or by the use of a nucleating agent, the silver halide grains are subjected to development conditions that would cause fogging of a surface latent image forming photographic element. The internal latent image-forming silver halide grains which received actinic radiation during imagewise exposure develop under these conditions at a slow rate as compared to the internal latent image-forming silver halide grains not imagewise exposed. The result is a direct-positive silver image. In color photography, the oxidized developer that is produced during silver development is used to produce a corresponding positive, direct-positive dye image. Multicolor direct-positive photographic images have been extensively investigated in connection with image transfer photography.

Direct-positive internal latent image-forming emulsions can take the form of halide-conversion type emulsions. Such emulsions are illustrated by Knott et al U.S. Pat. No. 2,456,953 and Davey et al U.S. Pat. No. 2,592,250.

More recently the art has found it advantageous to employ core-shell emulsions as direct positive internal latent image-forming emulsions. An early teaching of core-shell emulsions is provided by Porter et al U.S. Pat. No. 3,206,313, wherein a coarse grain monodispersed chemically sensitized emulsion is blended with a finer grain emulsion. The blended finer grains are Ostwald ripened onto the chemically sensitized larger grains. A shell is thereby formed around the coarse

grains. The chemical sensitization of the coarse grains is "buried" by the shell within the resulting core-shell grains. Upon imagewise exposure latent image sites are formed at internal sensitization sites and are therefore also internally located. The primary function of the shell structure is to prevent access of the surface developer to the internal latent image sites, thereby permitting low minimum densities.

The chemical sensitization of the core emulsion can take a variety of forms. One technique is to sensitize the core emulsion chemically at its surface with conventional sensitizers, such as sulfur and gold. Atwell et al U.S. Pat. No. 4,035,185 teaches that controlling the ratio of middle chalcogen to noble metal sensitizers employed for core sensitization can control the contrast produced by the core-shell emulsion. Another technique that can be employed is to incorporate a metal dopant, such as iridium, bismuth, or lead, in the core grains as they are formed.

The shell of the core-shell grains need not be formed by Ostwald ripening, as taught by Porter et al, but can be formed alternatively by direct precipitation onto the sensitized core grains. Evans U.S. Pat. Nos. 3,761,276, 3,850,637, and 3,923,513 teach that further increases in photographic speed can be realized if, after the core-shell grains are formed, they are surface chemically sensitized. Surface chemical sensitization is, however, limited to maintain a balance of surface and internal sensitivity favoring the formation of internal latent image sites.

It is generally well known in the photographic art to employ mixtures of negative-working emulsions to control the shape and position of the characteristic curve of a photographic element. Such practices are discussed by Zelikman and Levi, *Making and Coating Photographic Emulsions*, Focal Press, 1964, pp. 234 to 238. Blending of surface fogged direct-positive emulsions is also well known in the art, as illustrated by Smith and Illingsworth U.S. Pat. No. 3,615,573.

Whereas conventional negative-working emulsions and surface fogged direct-positive emulsions have been commonly prepared as either monodisperse or heterodisperse emulsions and blending of these emulsions has been undertaken, the characteristics of core-shell emulsions has dictated their preparation as monodisperse emulsions. For example, the Ostwald ripening process of Porter et al, cited above, requires that both the core and shell emulsions be monodisperse. Further, even when precipitation directly onto the core emulsion is undertaken, as described by Evans, cited above, monodisperse core emulsions permit control and uniformity of shell formation.

Blending of core-shell emulsions has been taught prior to this invention only when core-shell grains of similar average grain size have been blended. For example, Atwell et al, cited above, successfully blends monodisperse core-shell emulsions differing in the ratio of sulfur to gold internal sensitization. More recently monodisperse core-shell emulsions of the same average grain size, but with differing levels of surface chemical sensitization have been successfully blended.

Silverman and Hoyer U.S. Ser. No. 320,903, filed Nov. 12, 1981, now abandoned, and refiled as U.S. Ser. No. 418,314 concurrently with this patent application is directed to blended grain emulsions adapted to forming a direct-positive image. The emulsion is comprised of a dispersing medium containing a first, core-shell silver halide grain population having a coefficient of variation

of less than 20% and second silver halide grain population capable of internally trapping photolytically generated electrons and substantially incapable of forming a surface latent image within the direct-positive exposure latitude of the first grain population. The second grain population has an average diameter less than 70% that of the first grain population, and the first and second silver halide grain populations are present in a weight ratio of from 5:1 to 1:5.

Hoyen U.S. Ser. No. No. 320,902, filed Nov. 12, 1981, commonly assigned, titled DIRECT-POSITIVE CORE-SHELL EMULSIONS AND PHOTOGRAPHIC ELEMENTS AND PROCESSES FOR THEIR USE, now U.S. Pat. No. 4,395,478, discloses the use of polyvalent metal ion dopants in the shell of core-shell emulsions to reduce rereversal.

Evans et al U.S. Ser. No. 320,891, filed Nov. 12, 1981, commonly assigned, titled DIRECT REVERSAL EMULSIONS AND PHOTOGRAPHIC ELEMENTS USEFUL IN IMAGE TRANSFER FILM UNITS now abandoned in favor of continuation-in-part U.S. Ser. No. 431,912, filed Sept. 30, 1982, now abandoned in favor of U.S. Ser. No. 564,976, filed Dec. 23, 1983, issued as U.S. Pat. No. 4,504,570, discloses image transfer film units containing tabular grain core-shell silver halide emulsions.

Black-and-white photography has relied traditionally upon developed silver to produce a viewable image. The silver that is not incorporated in the final image is frequently recovered, although in many applications, such as silver image transfer, for instance, silver is rarely recovered. Silver which forms the image is sometimes recovered, particularly from radiographic elements, but even in this instance the silver which remains in the element for imaging may be unavailable for reclamation for many years. Because of the cost of silver, it is highly desirable to make efficient use of it in photographic elements. One measure of the efficiency of silver use is covering power. Covering power is herein quantitatively defined as 100 times the ratio of maximum density to developed silver, expressed in grams per square decimeter. High covering power is recognized to be an advantageous characteristic of black-and-white photographic elements. Covering power and conditions which effect it are discussed by James, Theory of the Photographic Process, 4th Ed., Macmillan, 1977, pp. 404, 489, and 490, and by Farnell and Solomon, "The Covering Power of Photographic Silver Deposits I. Chemical Development", The Journal of Photographic Science, Vol. 18, 1970, pp. 94-101.

Both color and black-and-white photographic elements containing multiple silver halide emulsion layers are well known. In producing color images three color forming layer units are present in the photographic element each containing at least one silver halide emulsion layer. As illustrated by Zelikman and Levi, cited above, adjustment of the characteristic curve in both color and black-and-white photography by using multilayer coatings is known in the art. Hellmig et al U.S. Pat. No. 3,846,135 teaches that unexpected speed increases can be obtained by coating a faster negative-working silver halide emulsion over a slower negative-working silver halide emulsion. Florens U.S. Pat. No. 3,942,986 teaches reducing contrast and improving detail in highlight areas by coating a monodisperse fogged direct positive emulsion and a heterodisperse fogged direct positive emulsion in separate layers. Shiba et al U.S. Pat. No. 3,854,953 teaches the use of multilayers of

fogged direct positive emulsions to increase information recording capacity. None of the above teachings, however, relate to photographic elements intended to form a direct-positive image incorporating a core-shell silver halide emulsion.

SUMMARY OF THE INVENTION

In one aspect, this invention is directed to a photographic element particularly adapted to forming a direct-positive image comprised of a support and, located on said support, a first, radiation-sensitive emulsion layer containing a core-shell silver halide grain population having a coefficient of variation of less than 20%, and, adjacent said first emulsion layer, a second emulsion layer substantially incapable of forming a surface latent image within the direct-positive exposure latitude of the first grain population and containing a second silver halide grain population capable of *internally forming a latent image* by internally trapping photolytically generated electrons. The second grain population has an average diameter less than 70% that of the first grain population, and the first and second silver halide grain populations are present in said adjacent emulsion layers in a weight ratio of from 5:1 to 1:5.

In still another aspect, this invention is directed to processing in a surface developer an imagewise exposed photographic element as described above (1) in the presence of a nucleating agent or (2) with light-flashing of the exposed photographic element during processing.

It is an advantage of the present invention that increased silver covering power can be realized with the photographic elements of this invention. This is totally unexpected from the prior uses of core-shell emulsions. In certain preferred forms more specifically described below increased photographic speed for photographic elements according to the present invention can be realized, even when silver coverage is reduced.

As taught by Hoyen, cited above, when the first, core-shell emulsions of the photographic elements of the present invention incorporate a polyvalent metal ion as a shell dopant, rereversal of the emulsions is reduced. Rereversal can also be reduced by forming the shell portion of the core-shell grains with increasing concentrations of iodide, as taught by Evans et al, cited above. As further taught by Hoyen, in embodiments in which the shell portion of the grains contain chloride, reduction of low intensity reciprocity failure and more rapid processing can also be realized. Still other advantages of this invention will become apparent from consideration of the following detailed description of the invention.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The photographic elements of the present invention are particularly adapted to forming direct-positive photographic images. The photographic elements incorporate at least two adjacent silver halide emulsion layers. A first emulsion layer is radiation-sensitive while a second emulsion layer is substantially incapable of forming a surface latent image within the direct-positive exposure latitude of the first emulsion layer. The emulsion layers are each comprised of a dispersing medium and at least one silver halide grain population. The first, radiation-sensitive emulsion layer contains a first grain population consisting of core-shell silver halide grains which are monodisperse. That is, the core-shell silver halide grains have a coefficient of variation of less than 20%. For applications requiring high contrast (at least 5 and

more typically at least 8) it is preferred that the core-shell silver halide grains have a coefficient of variation of less than 10%. (As employed herein the coefficient of variation is defined as 100 times the standard deviation of the grain diameters divided by the average grain diameter.) The second silver halide emulsion layer contains a second silver halide grain population capable of internally forming a latent image by internally trapping photolytically generated electrons. The second grain population has an average diameter less than 70% that of the first grain population, preferably less than 50% and optimally less than 40% that of the first grain population. The first and second grain populations are present in the emulsion in a weight ratio of from 5:1 to 1:5, preferably 2:1 to 1:3, respectively.

THE FIRST AND SECOND EMULSION LAYERS

The first emulsion layer consists of a conventional radiation-sensitive core-shell emulsion. The dispersing medium and first grain population can be provided by a conventional core-shell emulsion, such as any one of those described by Porter et al U.S. Pat. No. 3,206,313, Evans U.S. Pat. Nos. 3,761,276, 3,850,637, and 3,923,513, and Atwell et al U.S. Pat. No. 4,035,185, here incorporated by reference to provide a disclosure of such features. Accordingly, the following discussion is confined to certain core-shell emulsion features which are particularly preferred and to those features which differ from the teachings of the Porter et al, Evans, and Atwell et al patents.

Useful core-shell emulsions can be prepared by first forming a sensitized core emulsion. The core emulsion can be comprised of silver bromide, silver chloride, silver chlorobromide, silver chloroiodide, silver bromoiodide, or silver chlorobromoiodide grains. The grains can be coarse, medium, or fine and can be bounded by {100}, {111}, or {110} crystal planes. The core grains can be high aspect ratio tabular grains, as taught by Evans et al. The coefficient of variation of the core grains should be no higher than the desired coefficient of variation of the completed core-shell grains.

Perhaps the simplest manipulative approach to forming sensitized core grains is to incorporate a metal dopant within the core grains as they are being formed. The metal dopant can be placed in the reaction vessel in which core grain formation occurs prior to the introduction of silver salt. Alternately the metal dopant can be introduced during silver halide grain growth at any stage of precipitation, with or without interrupting silver and/or halide salt introduction.

Iridium is specifically contemplated as a metal dopant. It is preferably incorporated within the silver halide grains in concentrations of from about 10^{-8} to 10^{-4} mole per mole of silver. The iridium can be conveniently incorporated into the reaction vessel as a water soluble salt, such as an alkali metal salt of a halogen-iridium coordination complex, such as sodium or potassium hexachloroiridate or hexabromoiodate. Specific examples of incorporating an iridium dopant are provided by Berriman U.S. Pat. No. 3,367,778.

Lead is also a specifically contemplated metal dopant for core grain sensitization. Lead is a common dopant in direct print and printout emulsions and can be employed in the practice of this invention in similar concentration ranges. It is generally preferred that the lead dopant be present in a concentration of at least 10^{-4} mole per mole of silver. Concentrations up to about 5×10^{-2} , preferably 2×10^{-2} , mole per mole of silver

are contemplated. Lead dopants can be introduced similarly as iridium dopants in the form of water soluble salts, such as lead acetate, lead nitrate, and lead cyanide. Lead dopants are particularly illustrated by McBride U.S. Pat. No. 3,287,136 and Bacon U.S. Pat. No. 3,531,291.

Another technique for sensitizing the core grains is to stop silver halide grain precipitation after the core grain has been produced and to sensitize chemically the surface of the core. Thereafter additional precipitation of silver halide produces a shell surrounding the core. Particularly advantageous chemical sensitizers for this purpose are middle chalcogen sensitizers—i.e., sulfur, selenium, and/or tellurium sensitizers. Middle chalcogen sensitizers are preferably employed in concentrations in the range of from about 0.05 to 15 mg per silver mole. Preferred concentrations are from about 0.1 to 10 mg per silver mole. Further advantages can be realized by employing a gold sensitizer in combination. Gold sensitizers are preferably employed in concentrations ranging from 0.5 to 5 times that of the middle chalcogen sensitizers. Preferred concentrations of gold sensitizers typically range from about 0.01 to 40 mg per mole of silver, most preferably from about 0.1 to 20 mg per mole of silver. Controlling contrast by controlling the ratio of middle chalcogen to gold sensitizer is particularly taught by Atwell et al U.S. Pat. No. 4,035,185, cited above and here incorporated by reference specifically for this teaching. Evans, cited above, provides specific examples of middle chalcogen core grain sensitizations.

Although preferred, it is not essential that the core grains be sensitized prior to shelling to form the completed core-shell grains. It is merely necessary that the core-shell grains as formed be capable of forming internal latent image sites. Internal sensitization sites formed by shelling of sensitized core grains—that is, occlusion of foreign (i.e., other than silver and halogen) materials within the core-shell grains—are hereinafter referred to as internal chemical sensitization sites to distinguish them from internal physical sensitization sites. It is possible to incorporate internal physical sensitization sites by providing irregularities in the core-shell grain crystal lattice. Such internal irregularities can be created by discontinuities in silver halide precipitation or by abrupt changes in the halide content of the core-shell grains. For example, it has been observed that the precipitation of a silver bromide core followed by shelling with silver bromoiodide of greater than 5 mole percent iodide requires no internal chemical sensitization to produce a direct-positive image.

Although the sensitized core emulsions can be shelled by the Ostwald ripening technique of Porter et al, cited above, it is preferred that the silver halide forming the shell portion of the grains be precipitated directly onto the sensitized core grains by the double-jet addition technique. Double-jet precipitation is well known in the art, as illustrated by Research Disclosure, Vol. 176, December 1978, Item 17643, Section I, here incorporated by reference. Research Disclosure and its predecessor, Product Licensing Index, are publications of Industrial Opportunities Ltd., Homewell, Havant, Hampshire, P09 1EF, United Kingdom. The halide content of the shell portion of the grains can take any of the forms described above with reference to the core emulsion. To improve developability it is preferred that the shell portion of the grains contain at least 80 mole percent chloride, the remaining halide being bromide or bromide and up to 10 mole percent iodide. (Except as oth-

erwise indicated, all references to halide percentages are based on silver present in the corresponding emulsion, grain, or grain region being discussed.) Improvements in low intensity reciprocity failure are also realized when the shell portion of the core-shell grains is comprised of at least 80 mole percent chloride, as described above. For each of these advantages silver chloride is specifically preferred. On the other hand, the highest realized photographic speeds are generally recognized to occur with predominantly bromide grains, as taught by Evans, cited above. Thus, the specific choice of a preferred halide for the shell portion of the core-shell grains will depend upon the specific photographic application. When the same halides are chosen for forming both the core and shell portions of the core-shell grain structure, it is specifically contemplated to employ double-jet precipitation for producing both the core and shell portions of the grains without interrupting the introduction of silver and halide salts in the transition from core to shell formation.

The silver halide forming the shell portion of the core-shell grains must be sufficient to restrict developer access to the sensitized core portion of the grains. This will vary as a function of the ability of the developer to dissolve the shell portion of the grains during development. Although shell thicknesses as low as a few crystal lattice planes for developers having very low silver halide solvency are taught in the art, it is preferred that the shell portion of the core-shell grains be present in a molar ratio with the core portion of the grains of about 1:4 to 8:1, as taught by Porter et al and Atwell et al, cited above.

The amount of overexposure which can be tolerated by the emulsions of this invention without encountering rereversal can be increased by incorporating into the core-shell grains metal dopants for this purpose. As employed herein the term "rereversal" refers to the negative-working characteristic exhibited by an overexposed direct-positive emulsion. (Rereversal is the converse of solarization, a positive-working characteristic exhibited by an overexposed negative-working emulsion.) Hoyen, cited above and here incorporated by reference, discloses the use of polyvalent metal ions as dopants in the shell of core-shell emulsions to reduce rereversal. Preferred metal dopants for this purpose are divalent and trivalent cationic metal dopants, such as cadmium, zinc, lead, and erbium. These dopants are generally effective at concentration levels below about 5×10^{-4} , preferably below 5×10^{-5} , mole per mole of silver. Dopant concentrations of at least 10^{-6} , preferably at least 5×10^{-6} , mole per silver mole, should be present in the reaction vessel during silver halide precipitation. The rereversal modifying dopant is effective if introduced at any stage of silver halide precipitation. The rereversal modifying dopant can be incorporated in either or both of the core and shell. It is preferred that the dopant be introduced during the latter stages of precipitation (e.g., confined to the shell) when the core-shell grains are high aspect ratio tabular grains. The metal dopants can be introduced into the reaction vessel as water soluble metal salts, such as divalent and trivalent metal halide salts. Zinc, lead, and cadmium dopants for silver halide in similar concentrations, but to achieve other modifying effects, are disclosed by McBride U.S. Pat. No. 3,287,136, Mueller et al U.S. Pat. No. 2,950,972, Iwaosa et al U.S. Pat. No. 3,901,711, and Atwell U.S. Pat. No. 4,269,927. Other techniques for improving rereversal characteristics discussed below

can be employed independently or in combination with the metal dopants described.

After precipitation of a shell portion onto the sensitized core grains to complete formation of the core-shell grains, the emulsions can be washed, if desired, to remove soluble salts. Conventional washing techniques can be employed, such as those disclosed by Research Disclosure, Item 17643, cited above, Section II, here incorporated by reference.

Since the core-shell emulsions are intended to form internal latent images, intentional sensitization of the surfaces of the core-shell grains is not essential. However, to achieve the highest attainable reversal speeds, it is preferred that the core-shell grains be surface chemically sensitized, as taught by Evans and Atwell et al, cited above. Any type of surface chemical sensitization known to be useful with corresponding surface latent image-forming silver halide emulsions can be employed, such as disclosed by Research Disclosure, Item 17643, cited above, Section III. Middle chalcogen and/or noble metal sensitizations, as described by Atwell et al, cited above, are preferred. Sulfur, selenium and gold are specifically preferred surface sensitizers.

The degree of surface chemical sensitization is limited to that which will increase the reversal speed of the internal latent image-forming emulsion, but which will not compete with the internal sensitization sites to the extent of causing the location of latent image centers formed on exposure to shift from the interior to the surface of the tabular grains. Thus, a balance between internal and surface sensitization is preferably maintained for maximum speed, but with the internal sensitization predominating. Tolerable levels of surface chemical sensitization can be readily determined by the following test: A sample of the high aspect ratio tabular grain internal latent image-forming silver halide emulsion of the present invention is coated on a transparent film support at a silver coverage of 4 grams per square meter. The coated sample is then exposed to a 500 watt tungsten lamp for times ranging from 0.01 to 1 second at a distance of 0.6 meter. The exposed coated sample is then developed for 5 minutes at 20° C. in Developer Y below (an "internal type" developer, note the incorporation of iodide to provide access to the interior of the grain), fixed, washed, and dried. The procedure described above is repeated with a second sample identically coated and exposed. Processing is also identical, except that Developer X below (a "surface type" developer) is substituted for Developer Y. To satisfy the requirements of the present invention as being a useful internal latent image-forming emulsion the sample developed in the internal type developer, Developer Y, must exhibit a maximum density at least 5 times greater than the sample developed in the surface type developer, Developer X. This difference in density is a positive indication that the latent image centers of the silver halide grains are forming predominantly in the interior of the grains and are for the most part inaccessible to the surface type developer.

Developer X	Grams
N—methyl-p-aminophenol sulfate	2.5
Ascorbic acid	10.0
Potassium metaborate	35.0
Potassium bromide	1.0
Water to 1 liter.	

Developer Y	Grams
N—methyl-p-aminophenol sulfate	2.0
Sodium sulfite, desiccated	90.0
Hydroquinone	8.0
Sodium carbonate, monohydrate	52.5
Potassium bromide	5.0
Potassium iodide	0.5
Water to 1 liter.	

In one specifically preferred form the core-shell emulsions employed in the practice of this invention are high aspect ratio tabular grain core-shell emulsions, as disclosed by Evans et al, cited above and here incorporated by reference. As applied to the emulsions the term "high aspect ratio" is herein defined as requiring that the core-shell grains having a thickness of less than 0.5 micron (preferably 0.3 micron) and a diameter of at least 0.6 micron have an average aspect ratio of greater than 8:1 and account for at least 50 percent of the total projected surface area of the core-shell silver halide grains.

As employed herein the term "aspect ratio" refers to the ratio of the diameter of the grain to its thickness. The "diameter" of the grain is in turn defined as the diameter of a circle having an area equal to the projected area of the grain as viewed in a photomicrograph of an emulsion sample. The core-shell tabular grains of Evans et al have an average aspect ratio of greater than 8:1 and preferably have an average aspect ratio of greater than 10:1. Under optimum conditions of preparation aspect ratios of 50:1 or even 100:1 are contemplated. As will be apparent, the thinner the grains, the higher their aspect ratio for a given diameter. Typically grains of desirable aspect ratios are those having an average thickness of less than 0.5 micron, preferably less than 0.3 micron, and optimally less than 0.2 micron. Typically the tabular grains have an average thickness of at least 0.05 micron, although even thinner tabular grains can in principle be employed. In a preferred form of the invention the tabular grains account for at least 70 percent and optimally at least 90 percent of the total projected surface area of the core-shell silver halide grains. Tabular grain average diameters are in all instances less than 30 microns, preferably less than 15 microns, and optimally less than 10 microns.

A second emulsion layer is coated adjacent the first emulsion layer to produce a photographic element according to the present invention. The purpose of the second emulsion layer is to provide a second silver halide grain population closely associated with the low coefficient of variation first, core-shell grain population. In selecting the second emulsion for use with the core-shell emulsion consideration must be given (1) to the relative proportion of the first and second grain populations, (2) the relative grain size of the first and second grain populations, and (3) the specific characteristics of the silver halide grains making up the second grain population.

The relative proportions of the first and second grain populations, (1) above, can be varied. As noted above, a weight ratio of the first and second grain populations in the range of from 5:1 to 1:5 is generally contemplated, with weight ratio of from 2:1 to 1:3 being preferred for most applications. If the second grain population falls below the minimum proportions indicated above, the advantages of the present invention will not be fully realized. Similarly, if the second grain population is increased to higher than indicated proportions, im-

provements in silver coverage will not be fully realized. Nevertheless, since photographic elements frequently constitute a balance of competing demands to satisfy the needs of a specific end use wider than indicated variations in the weight ratios of the first and second grain populations can not be ruled out.

The relationship of the average grain sizes of the first and second grain populations, (2) above, are such that the second grain population has an average diameter less than 70%, preferably less than 50%, and optimally less than 40% that of the first, core-shell grain population. The second grain population can be either heterodisperse or monodisperse. It is generally preferred that the coefficient of variation of the second grain population be less than about 30%, although higher coefficients of variation can be readily tolerated at smaller average grain sizes. The first, core-shell grain population can have any convenient conventional average grain size. The specific choice will depend upon the specific photographic application and will include a variety of factors, such as desired photographic speed (which generally increases with increasing grain size), covering power (which generally decreases with increasing grain size), and granularity (which generally increases with increasing grain size). Average grain diameters for tabular grain core-shell emulsions are provided above. For nontabular core-shell grains average diameters of less than about 3.0 microns, preferably less than about 2.0 microns, are normally contemplated. It is generally advantageous for the second grain population to have the smallest average grain diameter that can be conveniently prepared. This will vary as a function of the composition and structure of the second grain population. Generally average grain diameters of less than 1.0 micron and preferably less than 0.5 micron are contemplated for the second grain population.

The further specific characteristics of the silver halide grains making up the second grain population, (3) above, are (a) that the second population grains be capable of internally trapping photolytically generated electrons and (b) that the second grain population be substantially incapable of forming a surface latent image within the direct-positive exposure latitude of the first grain population.

When a photon is captured by a silver halide grain on exposure, an electron and a hole pair are generated within the crystal structure of the grain. Internal latent image forming silver halide grains capture photolytically generated electrons internally. Thus, the second grain population can be chosen from among silver halide grains capable of forming an internal latent image. [The second grain population is not, however, limited to internal latent image forming grains. Photolytically generated electrons can be efficiently captured internally by internally fogged grains, which are incapable of forming latent images on exposure. It is in general preferred to employ conventional internal latent image forming silver halide grains or grains of this type which have been internally fogged by light exposure to form the second grain population.]

The further consideration (b) of the second grain population is that it be substantially incapable of forming a surface latent image within the direct-positive exposure latitude of the first grain population. Stated somewhat more quantitatively, when a photographic element containing first and second grain populations according to the invention is imagewise exposed and processed in a surface developer to produce a direct-

positive image, the second grain population is, by its presence, incapable of increasing the minimum density to more than 20% of the maximum image density. Preferably the minimum density should be less than 10% of the maximum density and, optimally, less than 5%. (Acceptable minimum densities vary considerably with the specific photographic application, with projection films, for example, being capable of tolerating much higher minimum densities than reflection prints.) With the first grain population omitted, the second grain population preferably produces a difference in density between exposed and unexposed areas (image discrimination) of less than 0.2, optimally less than 0.5. The fact that the second grain population can be made to produce higher minimum densities or larger density differences at varied exposure levels or processing conditions is immaterial, so long as less than the indicated values are realized under the conditions of exposure and processing contemplated for producing a direct-positive image in the photographic element containing the second grain population. For example, it is specifically contemplated to employ as a second grain population a core-shell emulsion requiring an extended period of development, as compared to the photographic element in which it is incorporated, to produce substantial image discrimination.

Subject to the considerations indicated above, the second emulsion layer can be provided by coating adjacent the first, core-shell emulsion a conventional internal latent image forming emulsion [or such an emulsion that has been internally fogged]. It is specifically contemplated to employ halide-conversion type emulsions to provide the second grain population. Converted halide emulsions are illustrated by Knott et al U.S. Pat. No. 2,456,953 and Davey et al U.S. Pat. No. 2,592,250. As is well understood by those skilled in the art, halide-conversion emulsions can be prepared by bringing a silver chloride emulsion into contact with bromide and, optionally, iodide salts. The bromide and, optionally, iodide salts displace chloride ions in the silver chloride crystal lattice producing internal crystal irregularities which function as internal electron trapping sites. Generally converted halide grains are comprised of at least 50 mole percent bromide, preferably at least 80 mole percent bromide, based on total halide. The balance of the halide present is chloride, optionally in combination with iodide. Iodide is usually present in a concentration of less than about 10 mole percent, based on total halide.

In a specifically preferred form of the invention the grains of the second population are also core-shell grains. They can be identical to the core-shell grains of the first grain population, subject to the considerations noted above. In general, when the second core-shell grain population satisfies the relative size requirements of the two grain populations the other considerations will also be satisfied when the first and second grain populations are of the same silver halide composition and similarly internally sensitized. Maintaining the second grain population substantially free of intentional surface chemical sensitization is also advantageous both in reducing the surface latent image forming capability of the second grain population within the direct-positive exposure latitude of the first emulsion layer and in increasing the reversal speed of the photographic element.

The photographic elements of the present invention can, if desired, be spectrally sensitized. Only the first grain population need have spectral sensitizing dye

absorbed, but where spectral sensitization follows coating, dye can be adsorbed to both grain populations. Any one or combination of red, green, or blue spectral sensitizing dyes can be employed, depending upon the specific photographic application contemplated. For black-and-white imaging applications spectral sensitizing is not required, although orthochromatic or panchromatic sensitization is usually preferred. Generally, any spectral sensitizing dye or dye combination known to be useful with a negative-working silver halide emulsion can be employed with the emulsions of the present invention. Illustrative spectral sensitizing dyes are those disclosed in Research Disclosure, Item 17643, cited above, Section IV. Particularly preferred spectral sensitizing dyes are those disclosed in Research Disclosure, Vol. 151, November 1976, Item 15162, here incorporated by reference. Although the emulsions can be spectrally sensitized with dyes from a variety of classes, preferred spectral sensitizing dyes are polymethine dyes, which include cyanine, merocyanine, complex cyanine and merocyanine (i.e., tri-tetra, and polynuclear cyanine and merocyanine), oxonol, hemioxonol, styryl, merostyryl, and streptocyanine dyes. Cyanine and merocyanine dyes are specifically preferred. Spectral sensitizing dyes which sensitize surface-fogged direct-positive emulsions generally desensitize both negative-working emulsions and the core-shell emulsions of this invention and therefore are not normally contemplated for use in the practice of this invention. Spectral sensitization can be undertaken at any stage of emulsion preparation heretofore known to be useful. Most commonly spectral sensitization is undertaken in the art subsequent to the completion of chemical sensitization. However, it is specifically recognized that spectral sensitization can be undertaken alternatively concurrently with chemical sensitization or can entirely precede surface chemical sensitization. Sensitization can be enhanced by pAg adjustment, including cycling, during chemical and/or spectral sensitization.

NUCLEATING AGENTS

It has been found advantageous to employ nucleating agents in preference to uniform light exposure in processing. The term "nucleating agent" (or "nucleator") is employed herein in its art-recognized usage to mean a fogging agent capable of permitting the selective development of internal latent image-forming silver halide grains which have not been imagewise exposed in preference to the development of silver halide grains having an internal latent image formed by imagewise exposure.

The photographic elements of this invention preferably incorporate a nucleating agent to promote the formation of a direct-positive image upon processing. The nucleating agent can be incorporated in the photographic element during processing, but it is preferably incorporated in manufacture of the photographic element, usually prior to coating. This reduces the quantities of nucleating agent required. The quantities of nucleating agent required can also be reduced by restricting the mobility of the nucleating agent in the photographic element. Large organic substituents capable of performing at least to some extent a ballasting function are commonly employed. Nucleating agents which include one or more groups to promote adsorption to the surface of the silver halide grains have been found to be effective in extremely low concentrations.

A preferred general class of nucleating agents for use in the practice of this invention are aromatic hydra-

Z represents the nonmetallic atoms necessary to complete a basic heterocyclic nucleus of the type found in cyanine dyes;

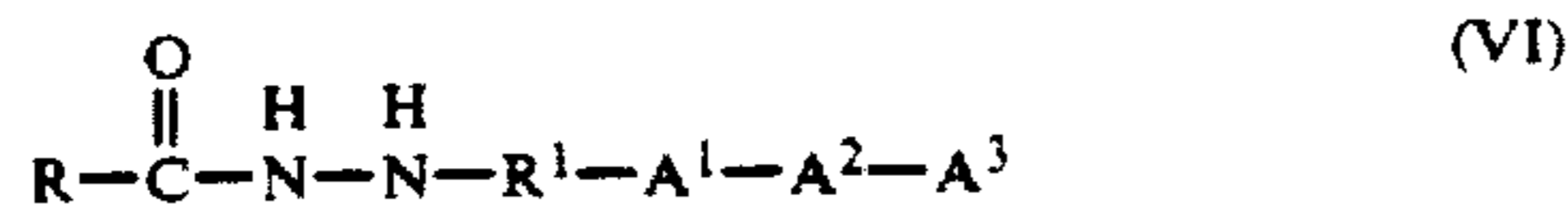
n and d are independently chosen from the integers 1 and 2;

R⁵ and R⁶ are independently chosen from hydrogen, phenyl, alkyl, alkylphenyl, and phenylalkyl; and the alkyl moieties in each instance include from 1 to 6 carbon atoms.

The formula (V) values from Q¹ provide a heterocyclic thioamide nucleus corresponding to a methine substituted form of the nuclei present above in formula (IV) values for Q¹. In a specifically preferred form the heterocyclic thioamide nucleus is preferably a methine substituted 2-thiohydantoin, rhodanine, isorhodanine, or 2-thio-2,4-oxazolidinedione nucleus. The heterocyclic thioamide nucleus of formula (V) is directly, or through an intermediate methine linkage, substituted with a basic heterocyclic nucleus of the type employed in cyanine dyes or a substituted benzylidene nucleus. Z preferably represents the nonmetallic atoms necessary to complete a basic 5- or 6-membered heterocyclic nucleus of the type found in cyanine dyes having ring-forming atoms chosen from the class consisting of carbon, nitrogen, oxygen, sulfur, and selenium.

N-(acylhydrazinophenyl)thioamide nucleating agents and their synthesis are more specifically disclosed in Leone et al U.S. Pat. No. 4,080,207.

Still another preferred class of phenylhydrazide nucleating agents are triazole-substituted phenylhydrazide nucleating agents. More specifically, preferred triazole-substituted phenylhydrazide nucleating agents are those represented by formula VI below:

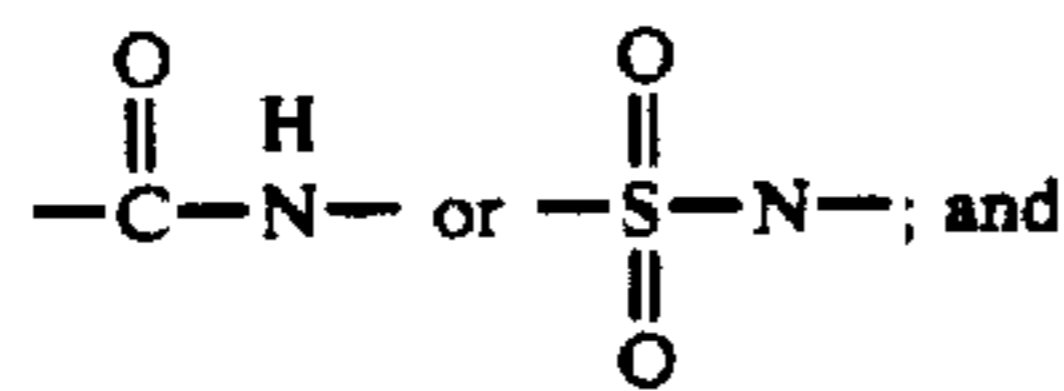


wherein

R and R¹ are as defined in formula (II);

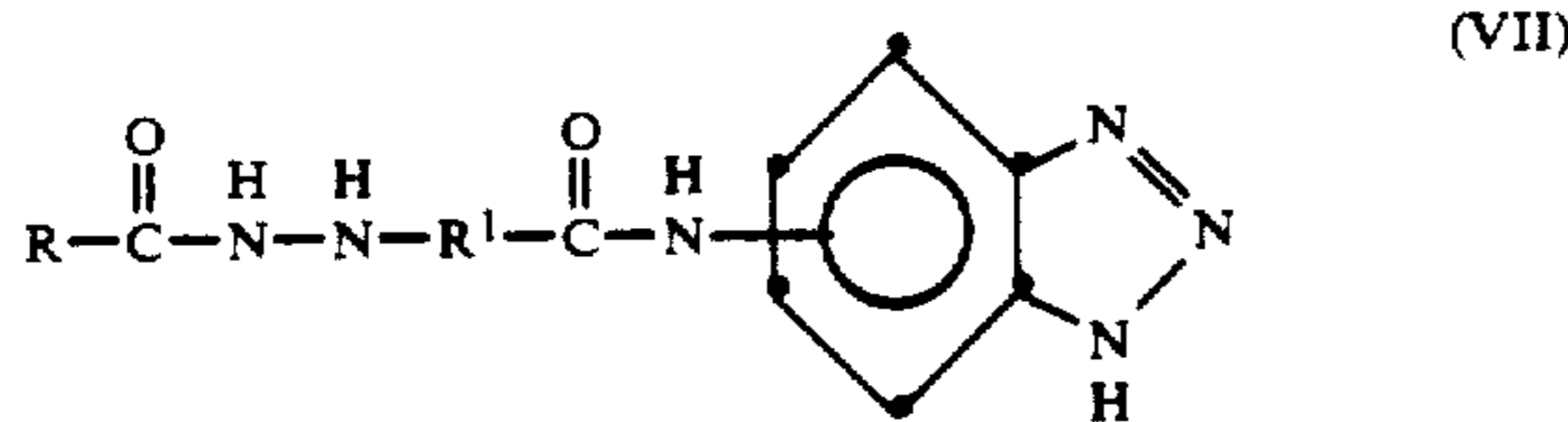
A¹ is alkylene or oxalkylene;

A² is



A³ is a triazolyl or benzotriazolyl nucleus; the alkyl and alkylene moieties in each instance including from 1 to 6 carbon atoms.

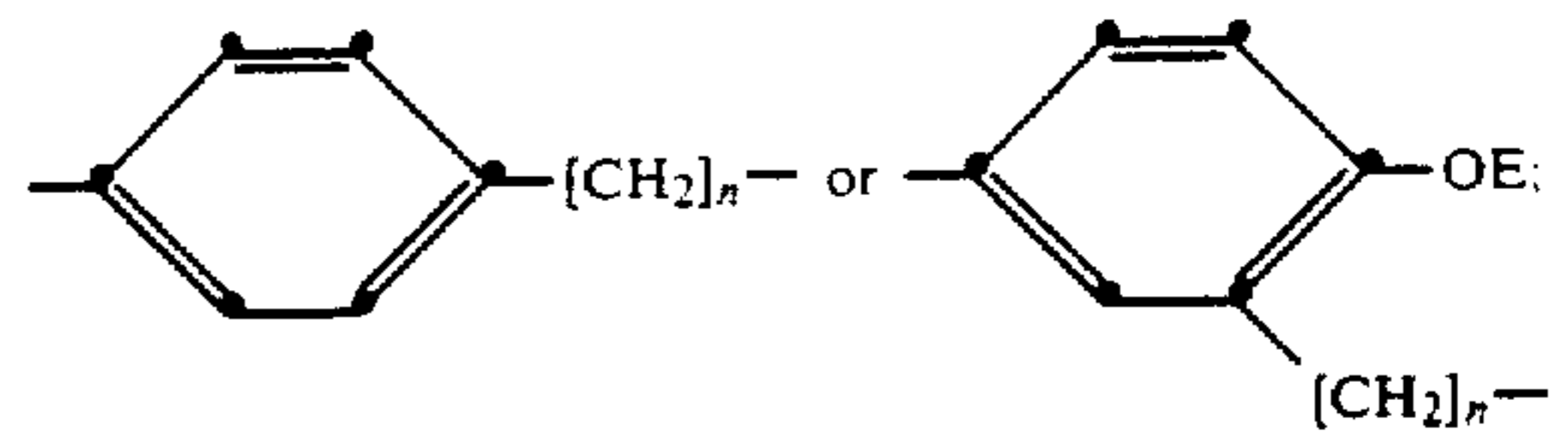
Still more specifically preferred triazole-substituted phenylhydrazide nucleating agents are those represented by formula (VII) below:



wherein

R is hydrogen or methyl;

R¹ is



n is integer of 1 to 4; and

E is alkyl of from 1 to 4 carbon atoms.

Triazole-substituted phenylhydrazide nucleating agents and their synthesis are disclosed by Sidhu et al U.S. Pat. No. 4,278,748, here incorporated by reference. Comparable nucleating agents having a somewhat broader range of adsorption promoting groups are disclosed in corresponding U.K. patent application No. 2,011,391A.

The aromatic hydrazides represented by formulas (II), (III), and (VI) each contain adsorption promoting substituents. In many instances it is preferred to employ in combination with these aromatic hydrazides additional hydrazides or hydrazones which do not contain substituents specifically intended to promote adsorption to silver halide grain surfaces. Such hydrazides or hydrazones, however, often contain substituents to reduce their mobility when incorporated in photographic elements. These hydrazide or hydrazones can be employed as the sole nucleating agent, if desired.

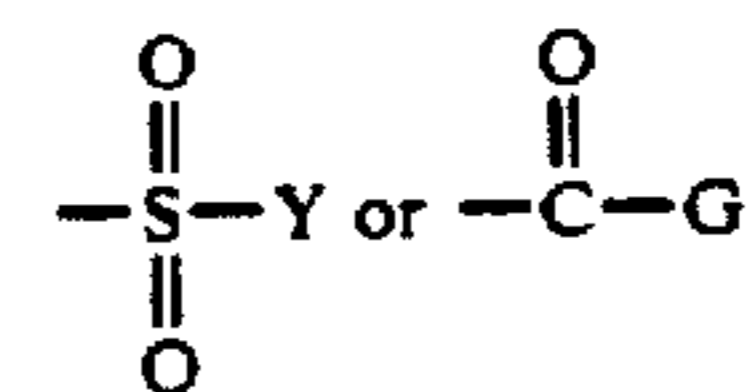
Such hydrazides and hydrazones include those represented by formula (VIII) and (IX) below:



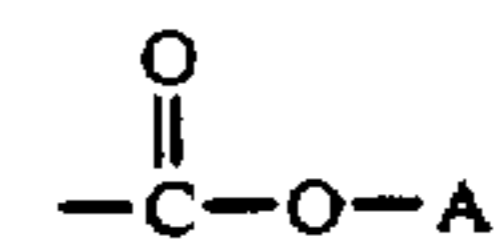
and



wherein T is an aryl radical, including a substituted aryl radical, T¹ is an acyl radical, and T² is an alkylidene radical and including substituted alkylidene radicals. Typical aryl radicals for the substituent T have the formula M-T³, wherein T³ is an aryl radical (such as, phenyl, 1-naphthyl, 2-naphthyl, etc.) and M can be such substituents as hydrogen, hydroxy, amino, alkyl, alkylamino, arylamino, heterocyclic amino (amino containing a heterocyclic moiety), alkoxy, aryloxy, acyloxy, arylcarbonamido, alkylcarbonamido, heterocyclic carbonamido (carbonamido containing a heterocyclic moiety), arylsulfonamido, alkylsulfonamido, and heterocyclic sulfonamido (sulfonamido containing a heterocyclic moiety). Typical acyl radicals for the substituent T¹ have the formula



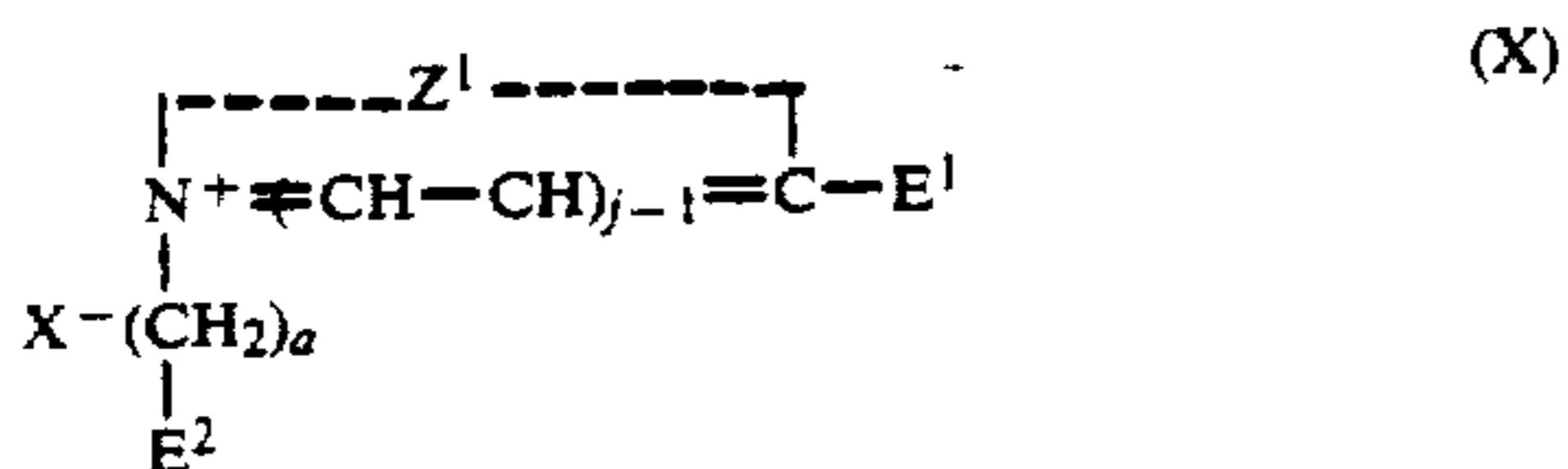
wherein Y can be such substituents as alkyl, aryl, and heterocyclic radicals, G can represent a hydrogen atom or the same substituent as Y as well as radicals having the formula



to form oxalyl radicals wherein A is an alkyl, aryl, or a heterocyclic radical. Typical alkylidene radicals for the substituent T² have the formula =CH—D wherein D can be a hydrogen atom or such radicals as alkyl, aryl, and heterocyclic radicals. Typical aryl substituents for the above-described hydrazides and hydrazones include phenyl, naphthyl, diphenyl, and the like. Typical heterocyclic substituents for the above-described hydrazides and hydrazones include azoles, azines, furan, thiophene, quinoline, pyrazole, and the like. Typical alkyl (or alkylidene) substituents for the above-described hydrazides and hydrazones have 1 to 22 carbon atoms including methyl, ethyl, isopropyl, n-propyl, isobutyl, n-butyl, t-butyl, amyl, n-octyl, n-decyl, n-dodecyl, n-octadecyl, n-eicosyl, and n-docosyl.

The hydrazides and hydrazones represented by formulas (VIII) and (IX) as well as their synthesis are disclosed by Whitmore U.S. Pat. No. 3,227,552, here incorporated by reference.

A secondary preferred general class of nucleating agents for use in the practice of this invention are N-substituted cycloammonium quaternary salts. A particularly preferred species of such nucleating agents is represented by formula (X) below:



wherein

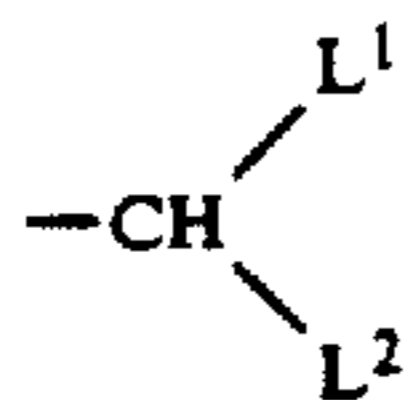
Z¹ represents the atoms necessary to complete a heterocyclic nucleus containing a heterocyclic ring of 5 to 6 atoms including the quaternary nitrogen atoms, with the additional atoms of said heterocyclic ring being selected from carbon, nitrogen, oxygen, sulfur, and selenium;

j represents a positive integer of from 1 to 2;

a represents a positive integer of from 2 to 6;

X⁻ represents an acid anion;

E² represents a member selected from (a) a formyl radical, (b) a radical having the formula



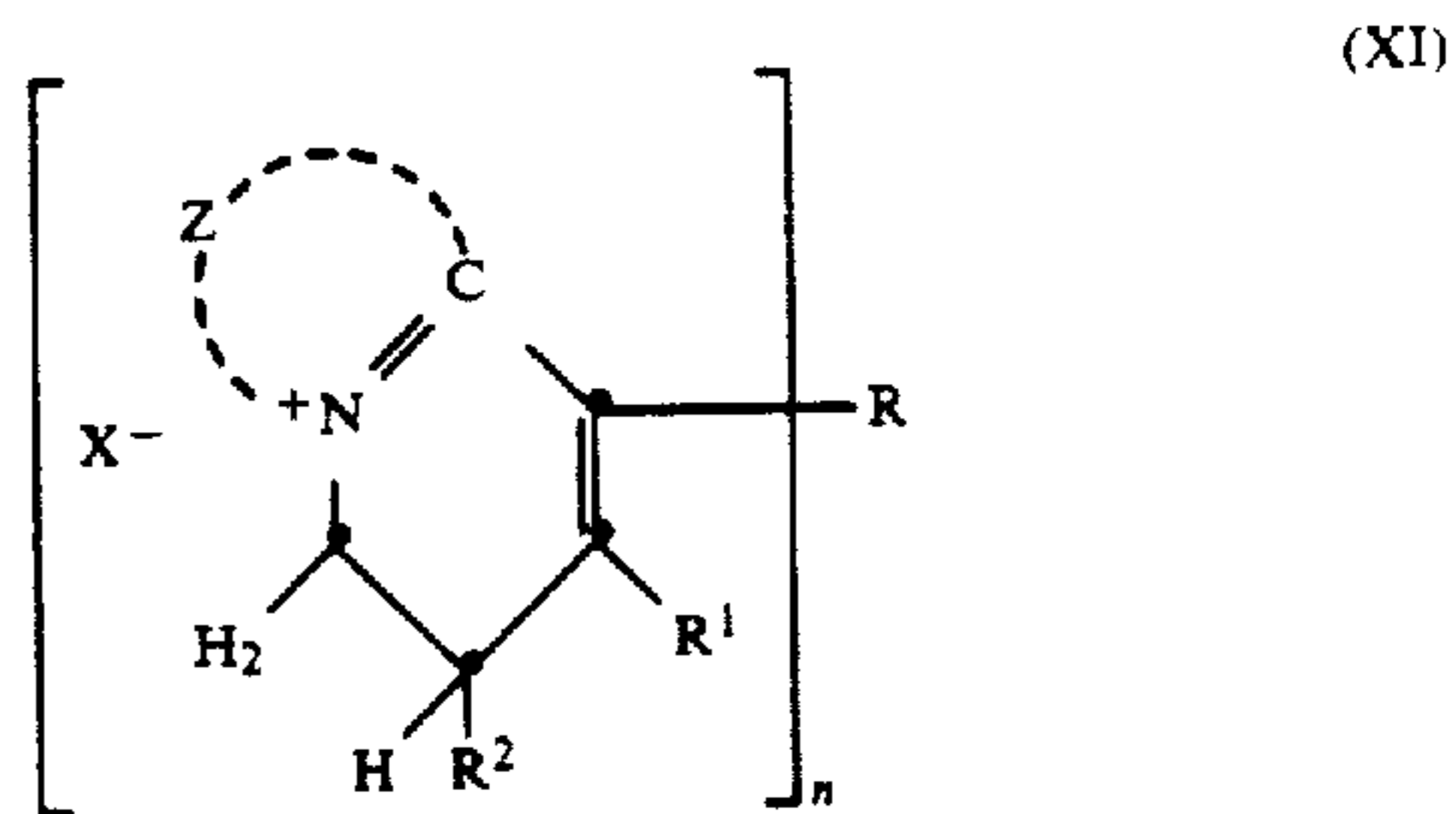
wherein each of L¹ and L², when taken alone, represents a member selected from an alkoxy radical and an alkylthio radical, and L¹ and L², when taken together, represent the atoms necessary to complete a cyclic radical selected from cyclic oxyacetals and cyclic thioacetals having from 5 to 6 atoms in the heterocyclic acetal ring, and (c) a 1-hydrazonoalkyl radical; and

E¹ represents either a hydrogen atom, an alkyl radical, an aralkyl radical, an alkylthio radical, or an aryl radical such as phenyl and naphthyl, and including substituted aryl radicals.

The N-substituted cycloammonium quaternary salt nucleating agents of formula (X) and their synthesis are disclosed by Lincoln and Heseltine U.S. Pat. Nos. 3,615,615 and 3,759,901. In a variant form E¹ can be a divalent alkylene group of from 2 to 4 carbon atoms joining two substituted heterocyclic nuclei as shown in formula (X). Such nucleating agents and their synthesis

are disclosed by Kurtz and Harbison U.S. Pat. No. 3,734,738.

The substituent to the quaternized nitrogen atom of the heterocyclic ring can, in another variant form, itself form a fused ring with the heterocyclic ring. Such nucleating agents are illustrated by dihydroaromatic quaternary salts comprising a 1,2-dihydroaromatic heterocyclic nucleus including a quaternary nitrogen atom. Particularly advantageous 1,2-dihydroaromatic nuclei include such nuclei as a 1,2-dihydropyridinium nucleus. Especially preferred dihydroaromatic quaternary salt nucleating agents include those represented by formula (XI) below:



wherein

Z represents the nonmetallic atoms necessary to complete a heterocyclic nucleus containing a heterocyclic ring of from 5 to 6 atoms including the quaternary nitrogen atom, with the additional atoms of said heterocyclic ring being selected from either carbon, nitrogen, oxygen, sulfur, or selenium;

n represents a positive integer having a value of from 1 to 2;

when n is 1, R represents a member selected from the group consisting of a hydrogen atom, an alkyl radical, an alkoxy radical, an aryl radical, an aryloxy radical, and a carbamido radical and,

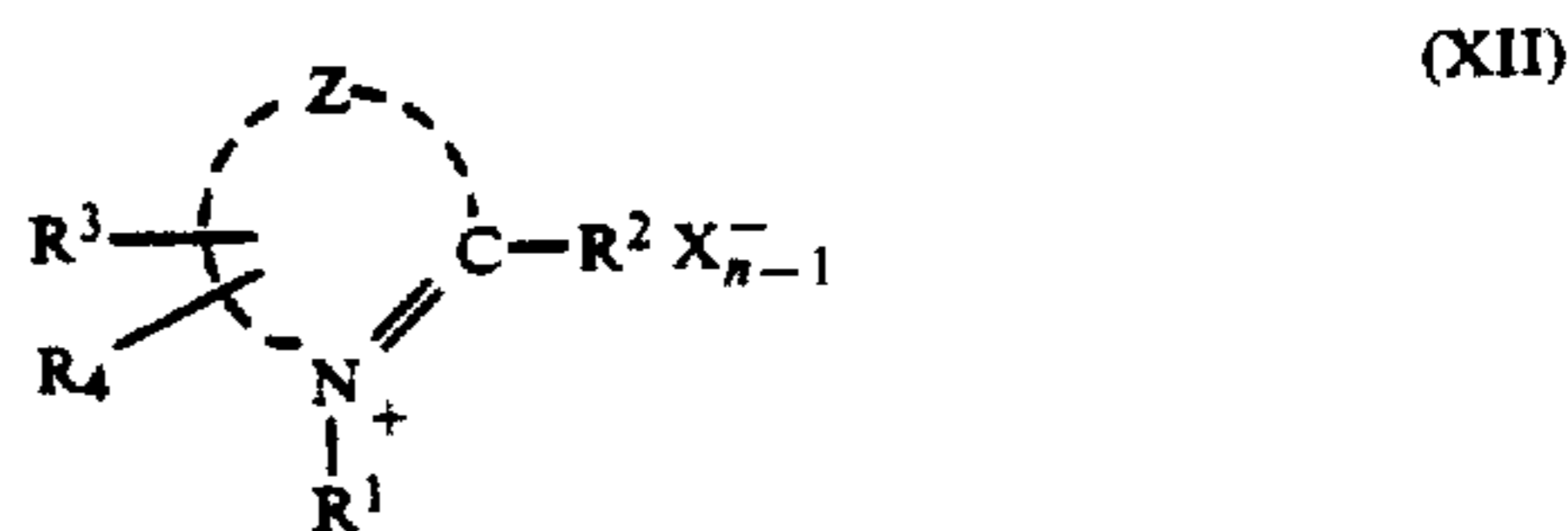
when n is 2, R represents an alkylene radical having from 1 to 4 carbon atoms;

each of R¹ and R² represents a member selected from the group consisting of a hydrogen atom, an alkyl radical, and an aryl radical; and

X⁻ represents an anion.

Dihydroaromatic quaternary salt nucleating agents and their synthesis are disclosed by Kurtz and Heseltine U.S. Pat. No. 3,719,494, here incorporated by reference.

A specifically preferred class of N-substituted cycloammonium quaternary salt nucleating agents are those which include one or more alkynyl substituents. Such nucleating agents include compounds within the generic structural definition set forth in formula (XII) below:



wherein Z represents an atomic group necessary for forming a 5- or 6-membered heterocyclic nucleus, R¹ represents an aliphatic group, R² represents a hydrogen atom or an aliphatic group, R³ and R⁴, which may be the same or different, each represents a hydrogen atom, a halogen atom, an aliphatic group, an alkoxy group, a

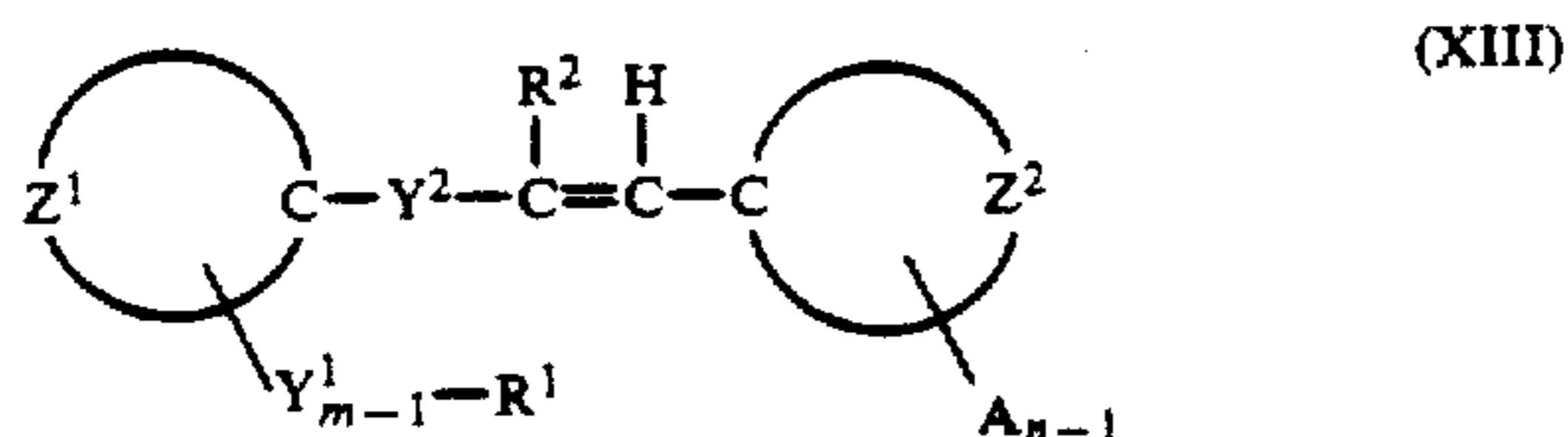
hydroxy group, or an aromatic group, at least one of R¹, R², R³ and R⁴ being a propargyl group, a butynyl group, or a substituent containing a propargyl or butynyl group, X⁻ represents an anion, n is 1 or 2, with n being 1 when the compound forms an inner salt.

Such alkynyl-substituted cycloammonium quaternary salt nucleating agents and their synthesis are illustrated by Adachi et al U.S. Pat. No. 4,115,122 here incorporated by reference.

The specific choice of nucleating agents can be influenced by a variety of factors. The nucleating agents of Leone cited above are particularly preferred for many applications, since they are effective at very low concentrations. Minimum concentrations as low as 0.1 mg of nucleating agent per mole of silver, preferably at least 0.5 mg per silver mole, and optimally at least 1 mg per silver mole are disclosed by Leone. The nucleating agents of Leone are particularly advantageous in reducing speed loss and in some instances permitting speed gain with increasing processing temperatures. When the nucleating agents of Leone are employed in combination with those of Whitmore speed variations as a function of temperature of processing can be minimized.

The aromatic hydrazide nucleating agents are generally preferred for use in photographic elements intended to be processed at comparatively high levels of pH, typically above 13. The alkynyl-substituted cycloammonium quaternary salt nucleating agents are particularly useful for processing at a pH of 13 or less. Adachi et al teaches these nucleating agents to be useful in processing within the pH range of from 10 to 13, preferably 11 to 12.5.

In addition to the nucleating agents described above additional nucleating agents have been identified which are useful in processing at pH levels in the range of from about 10 to 13. An N-substituted cycloammonium quaternary salt nucleating agent which can contain one or more alkynyl substituents is illustrative of one class of nucleating agents useful in processing below pH 13. Such nucleating agents are illustrated by formula (XIII) below:



wherein

Z¹ represents the atoms completing an aromatic carbocyclic nucleus of from 6 to 10 carbon atoms;
Y¹ and Y² are independently selected from among a divalent oxygen atom, a divalent sulfur atom, and



Z² represents the atoms completing a heterocyclic nucleus of the type found in cyanine dyes;

A is an adsorption promoting moiety;

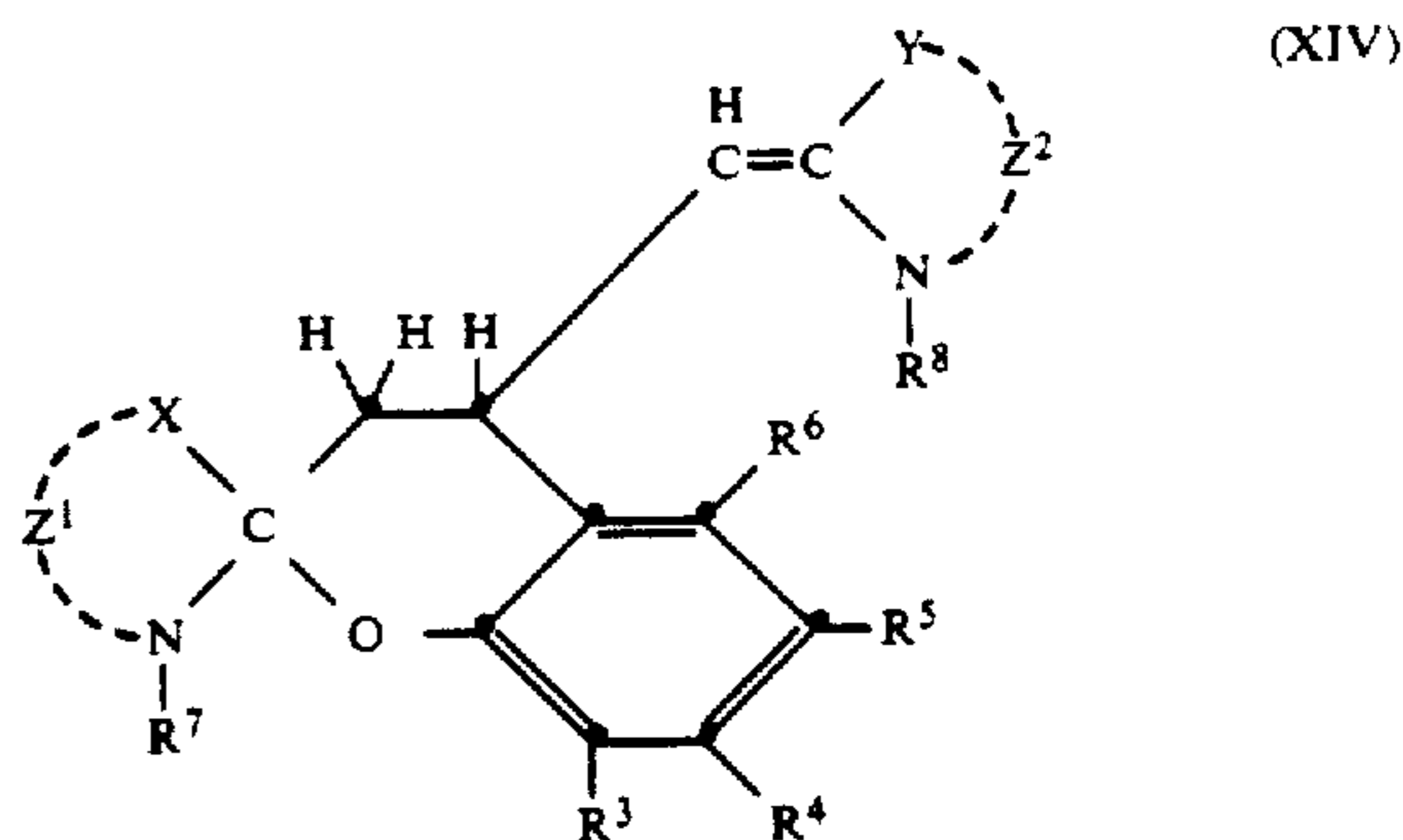
m and n are 1 or 2; and

R¹, R², and R³ are independently chosen from the group consisting of hydrogen, alkyl, aryl, alkaryl, and aralkyl and R¹ and R³ are additionally independently chosen from the group consisting of acyl, alkenyl, and alkynyl, the aliphatic moieties containing up to 5 carbon atoms and the aromatic moieties

containing 6 to 10 carbon atoms. A preferred processing pH when these nucleating agents are employed is in the range of from 10.2 to 12.0.

Nucleating agents of the type represented by formula (XIII) and their synthesis are disclosed by Baralle et al U.S. Pat. No. 4,306,016, here incorporated by reference.

Another class of nucleating agents effective in the pH range of from 10 to 13, preferably 10.2 to 12, are dihydrospiropyran bis-condensation products of salicylic aldehyde and at least one heterocyclic ammonium salt. In a preferred form such nucleating agents are represented by formula (XIV) below:



wherein

X and Y each independently represent a sulfur atom, a selenium atom or a —C(R¹R²)— radical,

R¹ and R² independently represent lower alkyl of from 1 to 5 carbon atoms or together represent an alkylene radical of 4 or 5 carbon atoms,

R³, R⁴, R⁵, and R⁶ each represent hydrogen, a hydroxy radical or a lower alkyl or alkoxy radical of from 1 to 5 carbon atoms,

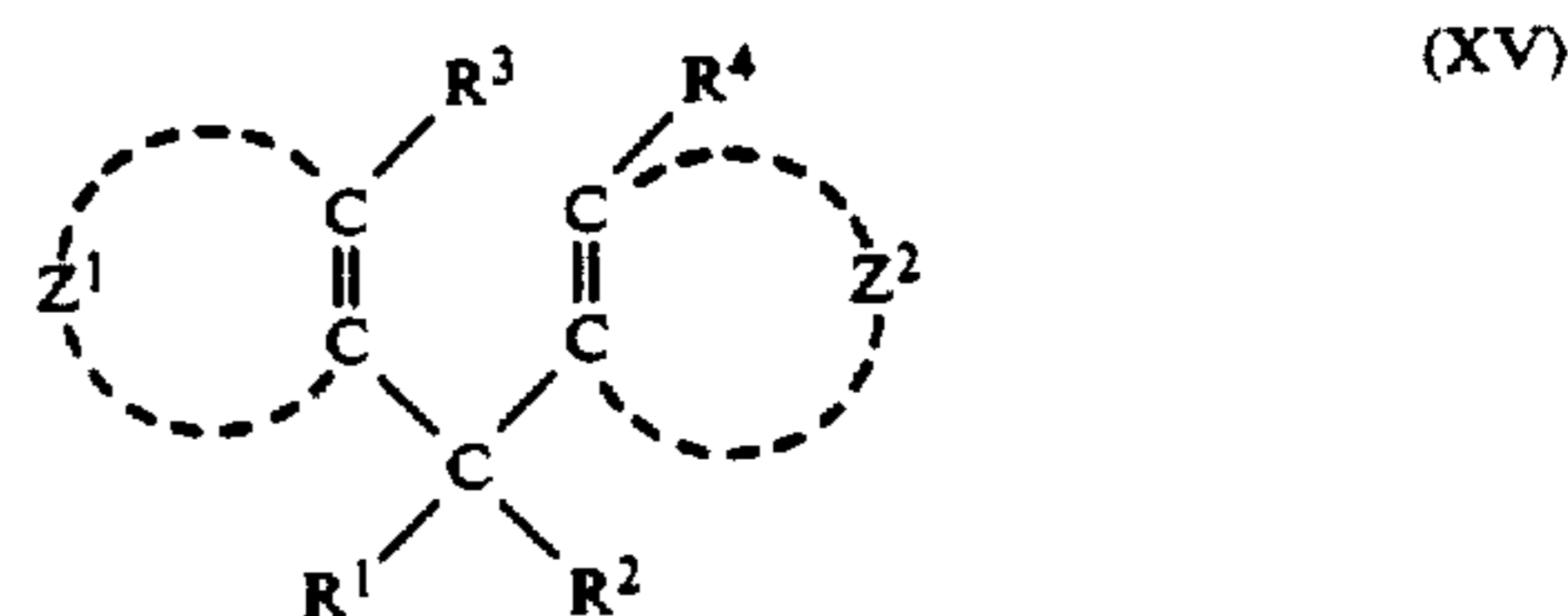
Z¹ and Z² each represents the nonmetallic atoms completing a nitrogen-containing heterocyclic nucleus of the type found in cyanine dyes and

R⁷ and R⁸ each represent a ring nitrogen substituent of the type found in cyanine dyes.

Z¹ and Z² in a preferred form each completes a 5- or 6-membered ring, preferably fused with at least one benzene ring, containing in the ring structure carbon atoms, a single nitrogen atom and, optionally, a sulfur or selenium atom.

Nucleating agents of the type represented by formula (XIV) and their synthesis are disclosed by Baralle et al U.S. Pat. No. 4,306,017, here incorporated by reference

Still another class of nucleating agents effective in the pH range of from 10 to 13, preferably 10.2 to 12, are diphenylmethane nucleating agents. Such nucleating agents are illustrated by formula (XV) below:

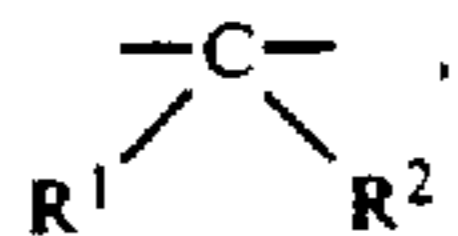


wherein

Z¹ and Z² represent the atoms completing a phenyl nucleus;

R¹ represents hydrogen or alkyl of from 1 to 6 carbon atoms; and

R², R³, and R⁴ are independently selected from among hydrogen, halogen, alkyl, hydroxy, alkoxy, aryl, alkaryl, and aralkyl or R³ and R⁴ together form a covalent bond, a divalent chalcogen linkage, or



wherein each alkyl moiety contains from 1 to 6 carbon atoms and each aryl moiety contains 6 to 10 carbon atoms.

Nucleating agents of the type represented by formula (XV) and their synthesis are disclosed by Baralle et al U.S. Pat. No. 4,315,986, here incorporated by reference.

Instead of being incorporated in the photographic element during manufacture, nucleating agents can alternatively or additionally be incorporated in the developer solution. Hydrazine (H₂N—NH₂) is an effective nucleating agent which can be incorporated in the developing solution. As an alternative to the use of hydrazine, any of a wide variety of water-soluble hydrazine derivatives can be added to the developing solution. Preferred hydrazine derivatives for use in developing solutions include organic hydrazine compounds of the formula:



where R¹ is an organic radical and each of R², R³ and R⁴ is a hydrogen atom or an organic radical. Organic radicals represented by R¹, R², R³ and R⁴ include hydrocarbyl groups such as an alkyl group, an aryl group, an aralkyl group, an alkaryl group, and an alicyclic group, as well as hydrocarbyl groups substituted with substituents such as alkoxy groups, carboxy groups, sulfonamido groups, and halogen atoms.

Particularly preferred hydrazine derivatives for incorporation in developing solutions include alkylsulfonamidoaryl hydrazines such as p-(methylsulfonamido) phenylhydrazine and alkylsulfonamidoalkyl aryl hydrazines such as p-(methylsulfonamidomethyl) phenylhydrazine.

The hydrazine and hydrazide derivatives described above are disclosed in Smith et al U.S. Pat. No. 2,410,690, Stauffer et al U.S. Pat. No. 2,419,975, and Hunsberger U.S. Pat. No. 2,892,715. The preferred hydrazines for incorporation in developers are described in Nothnagle U.S. Pat. No. 4,269,929. Another preferred class of nucleating agents that can be incorporated in the developer correspond to formula (I) above, but with the moiety M capable of restricting mobility absent. Nucleating agents of this type are disclosed in Okutsu et al U.S. Pat. No. 4,221,857 and Takada et al U.S. Pat. No. 4,224,401.

SILVER IMAGING

Once the emulsions for the first and second emulsion layers have been prepared as described above, preparation of the photographic elements of this invention can be completed by the optional incorporation of nucleating agents, described above, and conventional photographic addenda. In one preferred form the photographic elements can be usefully applied to photo-

graphic applications requiring a silver image to be produced—e.g., conventional black-and-white photography.

The first and second emulsion layers are each comprised of a dispersing medium in which the silver halide grains are dispersed. The dispersing medium present in the emulsion layers can also be present in other layers of the photographic elements, such as layers lying above or below one or both emulsion layers, and can contain various colloids alone or in combination as vehicles (which include both binders and peptizers). Preferred peptizers are hydrophilic colloids, which can be employed alone or in combination with hydrophobic materials. Preferred peptizers are gelatin—e.g., alkali-treated gelatin (cattle bone or hide gelatin) and acid-treated gelatin (pigskin gelatin) and gelatin derivatives—e.g., acetylated gelatin, phthalated gelatin, and the like. Useful vehicles are illustrated by those disclosed in Research Disclosure, Item 176643, cited above, Section IX, here incorporated by reference. The layers of the photographic elements containing crosslinkable colloids, particularly the gelatin-containing layers, can be hardened by various organic and inorganic hardeners, as illustrated by Research Disclosure, Item 17643, cited above, Section X.

Instability which decreases maximum density in direct-positive emulsion coatings can be protected against by incorporation of stabilizers, antifoggants, antikinking agents, latent image stabilizers and similar addenda in the emulsion and contiguous layers prior to coating. A variety of such addenda are disclosed in Research Disclosure, Item 17643, cited above, Section VI. Many of the antifoggants which are effective in emulsions can also be used in developers and can be classified under a few general headings, as illustrated by C. E. K. Mees, *The Theory of the Photographic Process*, 2nd Ed., Macmillan, 1954, pp. 677-680.

In some applications improved results can be obtained when the direct-positive emulsions are processed in the presence of certain antifoggants, as disclosed in Stauffer U.S. Pat. No. 2,497,917, here incorporated by reference. Typical useful antifoggants of this type include benzotriazoles, such as benzotriazole, 5-methylbenzotriazole and 5-ethylbenzotriazole; benzimidazoles such as 5-nitrobenzimidazole; benzothiazoles such as 5-nitrobenzothiazole and 5-methylbenzothiazole; heterocyclic thiones such as 1-methyl-2-tetrazoline-5-thione; triazines such as 2,4-dimethylamino-6-chloro-5-triazine; benzoxazoles such as ethylbenzoxazole; and pyrroles such as 2,5-dimethylpyrrole.

In certain embodiments, good results are obtained when the elements are processed in the presence of high levels of the antifoggants mentioned above. When antifoggants such as benzotriazoles are used, good results can be obtained when the processing solution contains up to 5 grams per liter and preferably 1 to 3 grams per liter; when they are incorporated in the photographic element, concentrations of up to 1,000 mg per mole of silver and preferably concentrations of 100 to 500 mg per mole of silver are employed.

In addition to sensitizers, hardeners, and antifoggants and stabilizers, a variety of other conventional photographic addenda can be present. The specific choice of addenda depends upon the exact nature of the photographic application and is well within the capability of the art. A variety of useful addenda are disclosed in Research Disclosure, Item 17643, cited above, here

incorporated by reference. Optical brighteners can be introduced, as disclosed by Item 17643 at Section V. Absorbing and scattering materials can be employed in the emulsions of the invention and in separate layers of the photographic elements, as described in Section VIII. Coating aids, as described in section XI, and plasticizers and lubricants, as described in Section XII, can be present. Antistatic layers, as described in Section XIII, can be present. Methods of addition of addenda are described in Section XIV. Matting agents can be incorporated, as described in Section XVI. Developing agents and development modifiers can, if desired, be incorporated, as described in Sections XX and XXI. The first and second emulsion layers, as well as other, conventional silver halide emulsion layers, interlayers, overcoats, and subbing layers, if any, present in the photographic elements can be coated and dried as described in Item 17643, Section XV.

The layers of the photographic elements can be coated on a variety of supports. Typical photographic supports include polymeric film, wood fiber—e.g., paper, metallic sheet and foil, glass and ceramic supporting elements provided with one or more subbing layers to enhance the adhesive, antistatic, dimensional, abrasive, hardness, frictional, antihalation and/or other properties of the support surface. Suitable photographic supports are illustrated by Research Disclosure, Item 17643, cited above, Section XVII, here incorporated by reference.

It is generally contemplated that the first and second emulsion layers can be coated onto the support in any desired order. That is, either the first emulsion layer or the second emulsion layer can be coated to overlie the remaining of the two emulsion layers. It is essential that the two emulsion layers be coated so that they are adjacent—that is, preferably in direct contact or at least in interactive proximity, if a processing liquid permeable interlayer separates the two emulsion layers.

The photographic elements of the present invention can be imagewise exposed in any conventional manner. Attention is directed to Research Disclosure Item 17643, cited above, Section XVIII, here incorporated by reference. The present invention is particularly advantageous when imagewise exposure is undertaken with electromagnetic radiation within the region of the spectrum in which the spectral sensitizers present exhibit absorption maxima. When the photographic elements are intended to record blue, green, red, or infrared exposures, spectral sensitizer absorbing in the blue, green, red, or infrared portion of the spectrum is present. As noted above, for black-and-white imaging applications it is preferred that the photographic elements be orthochromatically or panchromatically sensitized to permit light to extend sensitivity within the visible spectrum. Radiant energy employed for exposure can be either noncoherent (random phase) or coherent (in phase), produced by lasers. Imagewise exposures at ambient, elevated or reduced temperatures and/or pressures, including high or low intensity exposures, continuous or intermittent exposures, exposure times ranging from minutes to relatively short durations in the millisecond to microsecond range, can be employed within the useful response ranges determined by conventional sensitometric techniques, as illustrated by T. H. James, *The Theory of the Photographic Process*, 4th Ed., Macmillan, 1977, Chapters 4, 6, 17, 18 and 23.

The light-sensitive silver halide contained in the photographic elements can be processed following expo-

sure to form a visible image by associating the silver halide with an aqueous alkaline medium in the presence of a developing agent contained in the medium or the element. Processing formulations and techniques are described in L. F. Mason, *Photographic Processing Chemistry*, Focal Press, London, 1966; *Processing Chemicals and Formulas*, Publication J-1, Eastman Kodak Company, 1973; *Photo-Lab Index*, Morgan and Morgan, Inc., Dobbs Ferry, New York, 1977, and *Neblette's Handbook of Photography and Reprography Materials, Processes and Systems*, VanNostrand Reinhold Company, 7th Ed., 1977.

Included among the processing methods are web processing, as illustrated by Tregillus et al U.S. Pat. No. 3,179,517; stabilization processing, as illustrated by Herz et al U.S. Pat. No. 3,220,839, Cole U.S. Pat. No. 3,615,511, Shipton et al U.K. Pat. No. 1,258,906 and Haist et al U.S. Pat. No. 3,647,453; monobath processing as described in Haist, *Monobath Manual*, Morgan and Morgan, Inc., 1966, Schuler U.S. Pat. No. 3,240,603, Haist et al U.S. Pat. Nos. 3,615,513 and 3,628,955 and Price U.S. Pat. No. 3,723,126; infectious development, as illustrated by Milton U.S. Pat. Nos. 3,294,537, 3,600,174, 3,615,519 and 3,615,524, Whiteley U.S. Pat. No. 3,516,830, Drago U.S. Pat. No. 3,615,488, Salesin et al U.S. Pat. No. 3,625,689, Illingsworth U.S. Pat. No. 3,632,340, Salesin U.K. Pat. No. 1,273,030 and U.S. Pat. No. 3,708,303; hardening development, as illustrated by Allen et al U.S. Pat. No. 3,232,761; roller transport processing, as illustrated by Russell et al U.S. Pat. Nos. 3,025,779 and 3,515,556, Masseth U.S. Pat. No. 3,573,914, Taber et al U.S. Pat. No. 3,647,459 and Rees et al U.K. Pat. No. 1,269,268; alkaline vapor processing, as illustrated by Product Licensing Index, Vol. 97, May 1972, Item 9711, Goffe et al U.S. Pat. No. 3,816,136 and King U.S. Pat. No. 3,985,564; metal ion development as illustrated by Price, *Photographic Science and Engineering*, Vol. 19, Number 5, 1975, pp. 283-287 and Vought Research Disclosure, Vol. 150, October 1976, Item 15034; and surface application processing, as illustrated by Kitze U.S. Pat. No. 3,418,132.

Although development is preferably undertaken in the presence of a nucleating agent, as described above, giving the photographic elements an over-all light exposure either immediately prior to or, preferably, during development can be undertaken as an alternative. When an over-all flash exposure is used, it can be of high intensity and short duration or of lower intensity for a longer duration.

The silver halide developers employed in processing are surface developers. It is understood that the term "surface developer" encompasses those developers which will reveal the surface latent image centers on a silver halide grain, but will not reveal substantial internal latent image centers in an internal latent image-forming emulsion under the conditions generally used to develop a surface-sensitive silver halide emulsion. The surface developers can generally utilize any of the silver halide developing agents or reducing agents, but the developing bath or composition is generally substantially free of a silver halide solvent (such as water-soluble thiocyanates, water-soluble thioethers, thiosulfates, and ammonia) which will disrupt or dissolve the grain to reveal substantial internal image. Low amounts of excess halide are sometimes desirable in the developer or incorporated in the emulsion as halide-releasing compounds, but high amounts of iodide or iodide-

releasing compounds are generally avoided to prevent substantial disruption of the grain.

Typical silver halide developing agents which can be used in the developing compositions of this invention include hydroquinones, catechols, aminophenols, 3-pyrazolidinones, ascorbic acid and its derivatives, reductones, phenylenediamines, or combinations thereof. The developing agents can be incorporated in the photographic elements wherein they are brought into contact with the silver halide after imagewise exposure; however, in certain embodiments they are preferably employed in the developing bath.

Once a silver image has been formed in the photographic element, it is conventional practice to fix the undeveloped silver halide. The use of high aspect ratio tabular grains in the first emulsion layers is particularly advantageous in allowing fixing to be accomplished in a shorter time period. This allows processing to be accelerated.

DYE IMAGING

The photographic elements and the techniques described above for producing silver images can be readily adapted to provide a colored image through the use of dyes. Photographic elements according to the present invention capable of forming conventional retained or image transfer multicolor dye images are within the contemplation of the invention. In multicolor photographic elements according to the invention the first and second emulsion layers are both present in at least one color forming layer unit. Color and multicolor photographic elements which can be adapted for use in the practice of this invention are disclosed in Silverman and Hoyen U.S. Ser. No. 320,093 and in the continuing application filed concurrently with the present patent application, both cited above, and in Research Disclosure, Item 17643, cited above. Paragraphs VII and XXIII, each here incorporated by reference.

The invention can be better appreciated by reference to the following specific examples:

CONTROL COATING I

A 0.7 μm octahedral core-shell AgBr emulsion was prepared by a double-jet precipitation technique. The core consisted of a 0.50 μm octahedral AgBr chemically sensitized with 0.78 mg Na₂S₂O₃·5H₂O/mole Ag and 1.18 mg KAuCl₄/mole Ag for 30 minutes at 85° C. The core-shell emulsion was chemically sensitized with 1.0 mg Na₂S₂O₃·5H₂O/mole Ag for 30 minutes at 74° C. The emulsion was coated on a polyester film support at 6.46 g/m² silver and 4.84 g/m² gelatin. The emulsion layer also contained spectral sensitizing dyes anhydro-5,5'-dimethoxy-3,3'-bis(3-sulfopropyl)selenocyanine hydroxide sodium salt (Dye A) and anhydro-5,5'-dichloro-3,9-diethyl-3'-sulfopropyl oxocyanine hydroxide (Dye B) each at 200 mg/mole Ag. This radiation-sensitive core-shell emulsion is designated RSLGE, to indicate that it is the emulsion relied upon for radiation-sensitivity and the larger grain emulsion of the two emul-

sions employed. To a portion of this emulsion, RSLGE, was added a 3-propynylquinaldinium trifluoromethyl sulfonate nucleating agent (NA) at 30 mg/mole Ag, followed by coating on a transparent film support. The element was overcoated with 1% bis(vinylsulfonylmethyl)ether by weight based on total gel content. The nucleating agent, its quantity, the support, and the overcoat were all held constant in the subsequent coatings, except as specifically indicated.

INVENTION COATING II

A 0.25 μm cubic core-shell AgBr emulsion was prepared by a double-jet precipitation technique. The core consisted of a 0.20 μm cubic AgBr chemically sensitized with 12 mg Na₂S₂O₃·5H₂O/mole Ag and 10 mg KAuCl₄/mole Ag for 40 minutes at 70° C. The core-shell emulsion was not intentionally surface chemically sensitized. This emulsion is designated SGE, to indicate that it is the smaller grain emulsion of the two emulsions employed.

Portions of the RSLGE and SGE emulsions were coated, but, instead of blending the emulsion prior to coating, as taught by Silverman and Hoyen, cited above, the nucleating agent NA was incorporated in the RSLGE emulsion and the two emulsions were sequentially coated on a polyester film support at 4.31 g/m² total silver coverage and 3.23 g/m² total gelatin coverage to form first and second adjacent emulsion layers with the SGE emulsion being coated first to lie nearer the support surface.

INVENTION COATING III

In this coating the RSLGE emulsion layer was coated nearer the support, and NA was incorporated in the overlying SGE emulsion layer.

INVENTION COATING IV

In this coating the SGE emulsion layer was coated nearer the support and also contained NA. The RSLGE emulsion was coated as a separate layer overlying the SGE emulsion layer.

INVENTION COATING V

In this coating the RSLGE emulsion layer was coated nearer the support and also contained NA. The SGE emulsion layer was coated as a separate layer overlying the RSLGE emulsion layer.

The coating were exposed to a Xenon lamp for 10-5 seconds through a 0-3.0 density step tablet (0.15 density steps) plus a 0.86 neutral density filter and with a filter to simulate a P11 phosphor emitting at a wavelength maximum of 465 nm. The coatings were processed in a temperature controlled tray which was automatically rocked for agitation at 38° C. in Developer I. Coatings I and II were processed for 90 seconds, Coatings III and IV were processed for 75 seconds, and Coating V was processed for 60 seconds. Antifoggant levels were optimized for each coating. Results are shown below.

No.	Coating Variables	Silver Coverage (g/m ²)	Developer Antifoggant Level (g/L)		D _{max}	D _{min}	Speed
			MBT ¹ ±	PMT ²			
I.	RSLGE + NA (No SGE) (Control)	6.46	0.10	0.12	4.3	0.06	270
II.	RSLGE + NA/SGE/Support	4.31	0.10	0.12	4.0	0.06	340
III.	SGE + NA/RSLGE/Support	4.31	0.05	0.08	5.1	0.38	220
IV.	RSLGE/SGE + NA/Support	4.31	0.10	0.12	4.9	0.10	240

-continued

No.	Coating Variables	Silver Coverage (g/m ²)	Developer Antifoggant Level (g/L)		D _{max}	D _{min}	Speed
			MBT ¹	± PMT ²			
V.	SGE/RSLGE + NA/Support	4.31	0.10	0.14	2.4	0.09	245

¹5-Methylbenzotriazole²1-Phenyl-2-tetrazoline-5-thione

By reference to the table above it is apparent that Coating II constitutes a preferred embodiment of the present invention for obtaining increased photographic speeds. A substantially higher speed was realized as compared to the control Coating I, but without incurring any increase in minimum density. This demonstrates that an advantage can be realized by coating the smaller grain emulsion layer beneath the larger grain, radiation sensitive core-shell emulsion containing a nucleating agent. Both nucleating agent and developer antifoggant reach the smaller grain emulsion layer at approximately the same time in this arrangement. Coatings III and IV demonstrate that an increase in maximum density (directly related to covering power in black-and-white photographic elements) can be realized by placing the nucleating agent in the smaller grain emulsion layer. Further, the advantage can be realized whether the smaller grain emulsion layer is coated above or below the larger grain, radiation-sensitive core-shell emulsion layer. However, having the nucleating agent adsorbed to the surfaces of the second grain population can increase minimum density. The failure to realize an advantage with Coating V is attributed to the smaller grain emulsion layer being positioned to receive antifoggant prior to receiving nucleating agent. By reaching the second grain population contained in the smaller grain emulsion layer ahead of the nucleating agent the antifoggants significantly reduced its development. If nucleating agent had been additionally present in the smaller grain emulsion layer of Coating V, its maximum density should have been improved to a level comparable to Coatings III and IV.

It should be noted that the comparisons presented above place the inventive coatings at an unfair disadvantage, since the control coating contains three times the silver coverage of radiation-sensitive core-shell emulsion of any of the inventive coatings and one third more silver coverage than the total silver coverage of any of the inventive coatings. Had the silver coverages been equalized, Coating II would have showed an improvement in covering power as compared to Coating I and should have shown an even larger speed increase. Similarly, the maximum density increases of Coatings III and IV would have been still larger.

APPENDIX Developer I	
Component ¹	Grams per Liter
Water, tap	850.0
(Ethylenedinitrilo)tetraacetic acid, disodium salt (EDTA)	1.0
Potassium Hydroxide, 45%	22.0
5-Methylbenzotriazole ³ (MBT)	0.05-0.15
1-Phenyl-2-tetrazoline-5-thione (PMT) ³	0.04-0.16
Sodium Sulfite, Anhydrous	75.0
4,4'-Dimethyl-1-phenyl-3-pyrazolidionone	0.4
Sodium bromide	8.0
Sodium bicarbonate	7.0
2-Ethylaminoethanol	58.6

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APPENDIX Developer I	
Component ¹	Grams per Liter
3,3-Diaminodipropylamine	4.0
Hydroquinone	40.0
Potassium hydroxide, 45%	7.0 ²
Water to 1 liter	

¹Add each component in the order given and allow to dissolve before the next addition.

²Sufficient to adjust pH to 10.70 at 80° C.

³Level adjusted to optimize sensitometric response for individual coatings.

The invention has been described in detail with particular reference to preferred embodiments thereof, but it will be understood that variations and modifications can be effected within the spirit and scope of the invention.

What is claimed is:

1. A photographic element particularly adapted to forming a direct-positive image comprised of a support and, located on said support, a first, radiation-sensitive emulsion layer containing core shell silver halide grain population having a coefficient of variation of less than 20%, and a second silver halide emulsion layer substantially incapable of forming a surface latent image within the direct-positive exposure latitude of the first emulsion layer and containing a second grain population capable of internally forming a latent image by internally trapping photolytically generated electrons, said second grain population having an average diameter less than 70% that of said first grain population, and said first and second silver halide grain populations being present in a weight ratio of from 5:1 to 1:5.
2. A photographic element according to claim 1 additionally including a nucleating agent incorporated therein.
3. A photographic element according to claim 1 wherein said first, core-shell grain population is sensitized with at least one of sulfur, selenium, and gold.
4. A photographic element according to claim 1 wherein said second silver halide grain population is comprised of core-shell silver halide grains.
5. A photographic element according to claim 4 wherein said core-shell grains of said second grain population are substantially free of surface chemical sensitization.
6. A photographic element according to claim 1 wherein at least said core-shell grains of said first grain population are comprised of bromide.
7. A photographic element according to claim 6 wherein said bromide containing silver halide grains are additionally comprised of iodide.
8. A photographic element according to claim 1 wherein said second grain population has an average

diameter less than 50% that of said first grain population.

9. A photographic element according to claim 8 wherein said second grain population has an average diameter less than 40% total of said first grain population.

10. A photographic element according to claim 1 wherein said first and second silver halide grain populations are present in a weight ratio of from 2:1 to 1:3.

11. A photographic element according to claim 1 wherein said first, core-shell grain population is comprised of tabular grains.

12. A photographic element according to claim 11 wherein said grains of said first grain population having a thickness of less than 0.5 micron and a diameter greater than 0.6 micron have an average aspect ratio greater than 8:1 and account for greater than 50% of the total projected surface area of said first grain population.

13. A photographic element according to claim 1 wherein said second emulsion layer nearer said support than said first emulsion layer.

14. A photographic element according to claim 13 wherein said first emulsion layer contains a nucleating agent.

15. A photographic element according to claim 1 wherein said second emulsion layer is positioned to be contacted during processing with a nucleating agent no later than being contacted with an antifoggant.

16. A photographic element according to claim 15 wherein said second emulsion layer contains a nucleat-

ing agent adsorbed to the surfaces of said second grain population.

17. A photographic element according to claim 1 in which said second core-shell grain population increases the minimum density of said emulsion layers to no more than 20% of their maximum density.

18. A photographic element according to claim 1 in which said first core-shell grain population contains a divalent or trivalent metal ion chosen from the group consisting of cadmium, lead, and erbium in an amount sufficient to reduce rereversal.

19. A photographic element according to claim 1 in which said first core-shell grain population exhibits a coefficient of variation of less than 10% and said photographic element is capable of producing a contrast of greater than 10.

20. A photographic element according to claim 1 in which said second core-shell grain population increases the minimum density of the photographic element to no more than 5% of its maximum density.

21. A photographic element according to claim 1 in which said second grain population is comprised of converted halide silver halide grains.

[22. A photographic element according to claim 1 in which said second grain population is comprised of internally fogged silver halide grains.]

23. Processing in a surface developer an imagewise exposed photographic element according to any one of claims 1 through [22] 21

- (a) in the presence of a nucleating agent, or
- (b) with light flashing of the exposed photographic element during processing.

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