United States Patent [19]

Oberhofer

[11] E

Re. 30,066

[45] Reissued

Aug. 7, 1979

METHOD FOR SELECTIVELY REMOVING [54] CHROMATES

[75] Inventor:

Alfred W. Oberhofer, Downers

Grove, Ill.

[73] Assignee:

Nalco Chemical Company, Oak

Brook, Ill.

[21] Appl. No.: 801,075

Filed:

May 27, 1977

Related U.S. Patent Documents

Reissue	of:
	~

[64] Patent No.: 3,414,510

Issued:

Dec. 3, 1968

Appl. No.: Filed:

709,182 Feb. 29, 1968

Int. Cl.² C02B 1/62

U.S. Cl. 210/30 R; 210/37 B

[56]

[58]

References Cited

U.S. PATENT DOCUMENTS

3,147,214 9/1964 Kressman et al. 210/37 3,223,620

3,306,859 2/1967

FOREIGN PATENT DOCUMENTS

626882 7/1949 United Kingdom. 7/1958 United Kingdom 798326

OTHER PUBLICATIONS

Sussman et al., "Metal Recovery by Anion Exchange", Ind. and Eng. Chem., vol. 37, No. 7 (1945), pp. 618-624. Amber-hi-lites, Rohm and Haas Company technical bulletin, vol. 81, May 1964. "Amberlite IRA-93", Rohm and Haas Company tech-

nical bulletin, Dec. 1966. Primary Examiner—Charles N. Hart Assistant Examiner—Ivars Cintins

Attorney, Agent, or Firm—Hume, Clement, Brinks, Willian & Olds, Ltd.

[57] ABSTRACT

Removal of chromate ions from water containing a large amount of total dissolved solids by contacting the water with an acidified weakly basic anion exchange resin, preferably in [microporous] macroporous form, to selectively remove chromates from the water.

11 Claims, No Drawings

METHOD FOR SELECTIVELY REMOVING CHROMATES

Matter enclosed in heavy brackets [] appears in the 5 original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue.

BACKGROUND OF THE INVENTION

Inorganic chromates are frequently employed as corrosion inhibiting materials in industrial waters, particularly in circulating water systems for cooling towers. The chromates are sometimes used alone but frequently are employed in conjunction with molecularly dehydrated phosphates, the combination functioning as scale and corrosion inhibitors to protect metal conduits and other metallic surfaces with which the circulating water comes in contact.

Water being used as a cooling medium in industrial applications frequently is very high in dissolved solids, usually exceeding 1000 parts per million or so. When a cooling tower which has been treated with chromate corrosion inhibitors reaches a certain concentration level of dissolved solids, it is customary to blow it down by discharging a portion of the water and adding fresh makeup water having a lower dissolved solids content. A typical cooling water blow-down might contain, for example, 20 parts per million of a chromate and 1200 parts per million of other dissolved salts such as sodium chloride, calcium sulfate, magnesium nitrate, and the like.

When such waters are discharged into natural water courses or to sewage systems, the high chromate concentration may pose a problem because of local regulations covering the nature of effluents which can be discharged. The presence of the large dissolved solids content, however, makes it quite difficult to remove the chromate ions selectively while leaving the relatively 40 innocuous salts for discharge.

DESCRIPTION OF THE PRIOR ART

Some attempts have been made to use ion exchange resins in the removal of chromate ions from waste waters containing high levels of total dissolved solids but not with complete success. In some cases, the resins have a distinct fouling tendency and some are not stable to oxidation. Furthermore, strongly basic anion exchange materials when used for this purpose do not 50 have particularly high loading capacities nor high regeneration efficiencies.

SUMMARY OF THE INVENTION

The present invention makes use of weakly basic 55 anion exchange resins under certain operating conditions for a selective removal of chromate ions from waters having high total dissolved solid contents. Specifically, it has been found that macroporous weakly basic anion exchange resins which have been at least 60 partially acidified prior to use can selectively remove chromate ions from industrial waters having large amounts of total dissolved solids. The weakly basic resins [have the advantage of providing higher loading capacities,] are less subject to organic fouling, and 65 have a high regeneration efficiency. The best results are obtained in the process of the present invention when the pH of the water being treated is adjusted to a value

of from 3.0 to 5.0 before contacting the same with the resin, and preferably to a value of from 3.0 to 3.5.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The weak base anion exchange resins which provide the best results in the practice of the present invention are those which are macroporous, having pore diameters ranging from about 5 to 100 Angstroms or more. Chemically, these materials can be of different constitution, but should contain an intermediate amine as the exchange site. Particularly good results are obtained when the resin used is a mixture of secondary and tertiary amines, since these resins are considerably more stable to oxidation than are resins which have reaction sites consisting solely of primary and secondary amines.

The best resins found for this purpose are the polystyrene divinyl benzene amines which are prepared by nitration and subsequent reduction of styrene-divinyl benzene copolymers. Other materials which can be used in accordance with the present invention are the weak base anion exchange resins such as the amine derivatives of epichlorohydrin and polyvinylpyrrolidone.

Prior to contacting the water to be treated with the resin, the resin is acidified by treatment with a dilute mineral acid such as sulfuric acid or hydrochloric acid to at least partially convert the amine to its acid form. It is not always necessary that the amine be treated with stoichiometric amounts of acid sufficient to cause complete conversion to the acid form, but satisfactory results can be obtained using an amount of acid ranging from about 10% to 100% of the stoichiometric amount.

The treatment can be effected in the usual way by passing the water through a bed of particles of the weakly basic anion exchange resin.

To illustrate the beneficial effect of acidification of the resin, a test was made using 140 ml. of a weak base ion exchange resin (IRA-93, a polystyrene-divinyl benzene amine supplied by Rohm and Haas) in a one-half inch internal diameter column, with a forty-two inch bed height at flow rates up to [14,000 gallons per cubic foot] 2 gallons per minute per cubic foot. The following table illustrates the results obtained:

TABLE I

	Ionic form	Influent pH	Flow rate, g.p.m./cu.ft.	Capacity, lbs./cu.ft.	Average CrO ₄ leakage, p.p.m.
	H ₂ SO ₄	3.5	2.0	5.9	< 0.1
•	H ₂ SO ₄	3.5	1.0	6.2	< 0.1
	H ₂ SO ₄	4.5	1.0	4.9	< 0.1
	Free amine	3.5	1.0	5.6	10

The water employed in the above test contained 1400 parts per million of total dissolved solids (calcium, magnesium, sodium, sulfate and chloride) plus 49 parts per million of chromate ion. The temperature of the influent was held between 75° and 85° F.

The resins can be regenerated by treatment with an alkali such as sodium hydroxide, potassium hydroxide, or ammonium hydroxide to remove the chromate ions.

After exhaustion, the column with a loading of 4.9 pounds chromate per cubic foot was regenerated with 560 ml. of 4% sodium hydroxide, amounting to a concentration of 10.3 pounds of sodium hydroxide per cubic foot of resin. This large excess of sodium hydroxide was used to assure a complete regeneration. Samples were taken periodically during the one hour contact of

the sodium hydroxide with the resin. The total chromate loaded on the column was eluted by the regenerant [was 5.14 pounds per cubic foot]. Of this, 96% was eluted by the first 420 ml. of regenerant.

As previously indicated, the best results are obtained using an influent pH of 3.0 to 5.0. However, the resins will remove chromate ions at lower pH values than 3.0 but the stability of the resin is significantly decreased at these pH values. The highest resin loading occurs at an 10 influent pH of 3.5.

The reactions involved are believed to be represented by the following equations:

$$R_3NH$$

Chromate removal:

 R_3NH
 $SO_4 + CrO_4 - R_3NH$
 R_3NH
 R_3NH

It should be evident that various modifications can be 30 made to the described embodiments without departing from the scope of the present invention.

I claim as my invention:

- 1. The method of selectively removing chromate ions from water containing [a large amount] at least 1,000 35 parts per million of total dissolved solids which comprises adjusting the pH of the water being treated to a value from about 3.0 to about 5.0, acidifying a weakly basic anion exchange resin in the macroporous form and thereafter contacting said water with the acidified resin to cause selective removal of chromate ions from said water.
- [2. The method of claim 1 in which said anion exchange resin is in macroporous form.]

- [3. The method of claim 2 in which said resin has pore diameters in the range from about 10 to 100 Angstroms.]
- [4. The method of claim 1 in which the pH of the water being treated is adjusted to a value of from 3.0 to 5.0 before contacting the same with said resin.]
- [5. The method of claim 1 in which the pH of the water being treated is adjusted to a value of from 3.0 to 3.5.]
- 6. The method of claim 1 in which the acidification of the resin consists in treating said resin with sulfuric acid.
- 7. The method of claim 1 in which the acidification of the resin consists in treating said resin with hydrochloric acid.
- 8. The method of claim 1 in which said resin is a polystyrene-divinyl benzene amine resin.
- 9. A method for selectively removing chromate ions from circulating water systems which have been treated with chromate corrosion inhibitors, which comprises:
 - discharging a portion of the water from the system when a level of at least 1,000 parts per million total dissolved solids is present, to obtain a blow-down and adjusting the pH of said blow-down to a value of about 3.0 to about 5.0;
 - acidifying a macroporous weakly basic anion exchange resin; and
 - thereafter contacting the blow-down with said resin to selectively remove the chromate from the blow-down to obtain a blow-down substantially free from chromate ions.
- 10. The method of claim 9 wherein the pH of the blow-down is adjusted from about 3.0 to about 3.5.
- 11. The method of claim 9 wherein said resin is treated with a dilute mineral acid to acidify it prior to contact with the blow-down.
- 12. The method of claim 11 wherein the dilute mineral acid is sulfuric acid.
- 13. The method of claim 11 wherein the dilute mineral acid is hydrochloric acid.
- 14. The method of claim 11 further including treating the resin, after contact with the blow-down, with an alkali to regenerate the resin by removing the chromate ions.
- 15. The method of claim 11 in which said resin is a polystyrene-divinyl benzene amine resin.

50

45

55

60

UNITED STATES PATENT AND TRADEMARK OFFICE CERTIFICATE OF CORRECTION

PATENT NO. : Re 30066

DATED: August 7, 1979

INVENTOR(S): Alfred W. Oberhofer

It is certified that error appears in the above—identified patent and that said Letters Patent are hereby corrected as shown below:

Col. 1, line 30, insert --salt-- after chromate.

Bigned and Sealed this

Thirteenth Day of November 1979

[SEAL]

Attest:

RUTH C. MASON
Attesting Officer

LUTRELLE F. PARKER

Acting Commissioner of Patents and Trademarks