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Wynes et al.

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(54) **SOFT RECOIL SYSTEM**

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(73) Assignee: **Mandus Group, Ltd.**, Rock Island, IL (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **14/803,975**

(22) Filed: **Jul. 20, 2015**

(65) **Prior Publication Data**

US 2015/0323277 A1 Nov. 12, 2015

Related U.S. Application Data

(63) Continuation of application No. 13/903,650, filed on May 28, 2013, now Pat. No. 9,115,946, which is a continuation of application No. 13/452,674, filed on Apr. 20, 2012, now Pat. No. 8,468,928.

(60) Provisional application No. 61/478,053, filed on Apr. 21, 2011.

(51) **Int. Cl.**

F41A 25/02	(2006.01)
E05B 63/12	(2006.01)
F41A 5/36	(2006.01)
F41A 25/20	(2006.01)
F16B 17/00	(2006.01)

(52) **U.S. Cl.**
CPC ***F41A 25/02*** (2013.01); ***E05B 63/122*** (2013.01); ***F16B 17/00*** (2013.01); ***F41A 5/36*** (2013.01); ***F41A 25/20*** (2013.01); *Y10T 403/591* (2015.01); *Y10T 403/7075* (2015.01)

(58) **Field of Classification Search**
CPC F41A 25/02; F41A 25/16; F41A 25/20; F41A 5/36
USPC 89/43.01
See application file for complete search history.

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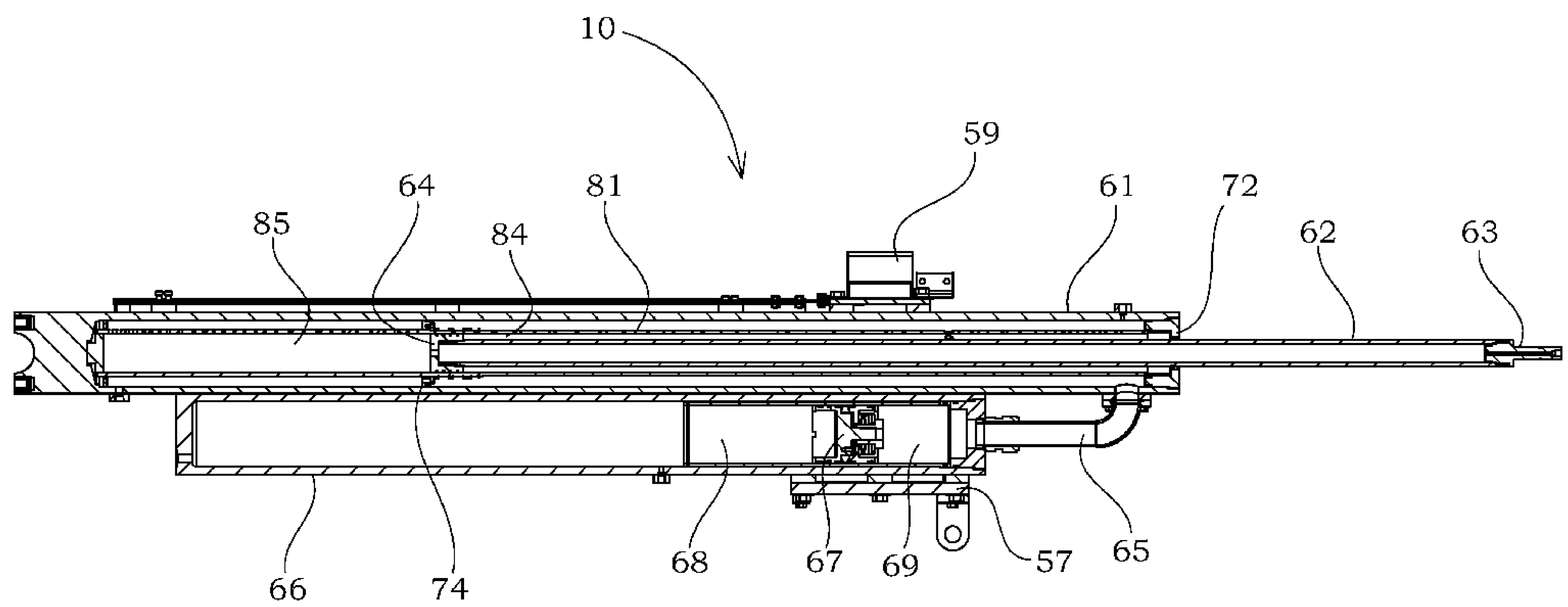
(57) **ABSTRACT**

One embodiment of a gun configured with the soft recoil system comprises a plurality of recoiling parts that initially moves in the direction of the projectile being fired before moving in a direction opposite to that of a projectile during the firing of the round. The soft recoil system throttles the movement of the recoiling parts such that the energy expended during the firing of the round is spread over a longer time period and a longer distance than would normally occur. The soft recoil system stores at least a portion of the energy transferred to the recoiling parts and the user may selectively release at least a part of that portion of energy to offset the energy imparted to the gun during the firing of the next round.

9 Claims, 21 Drawing Sheets



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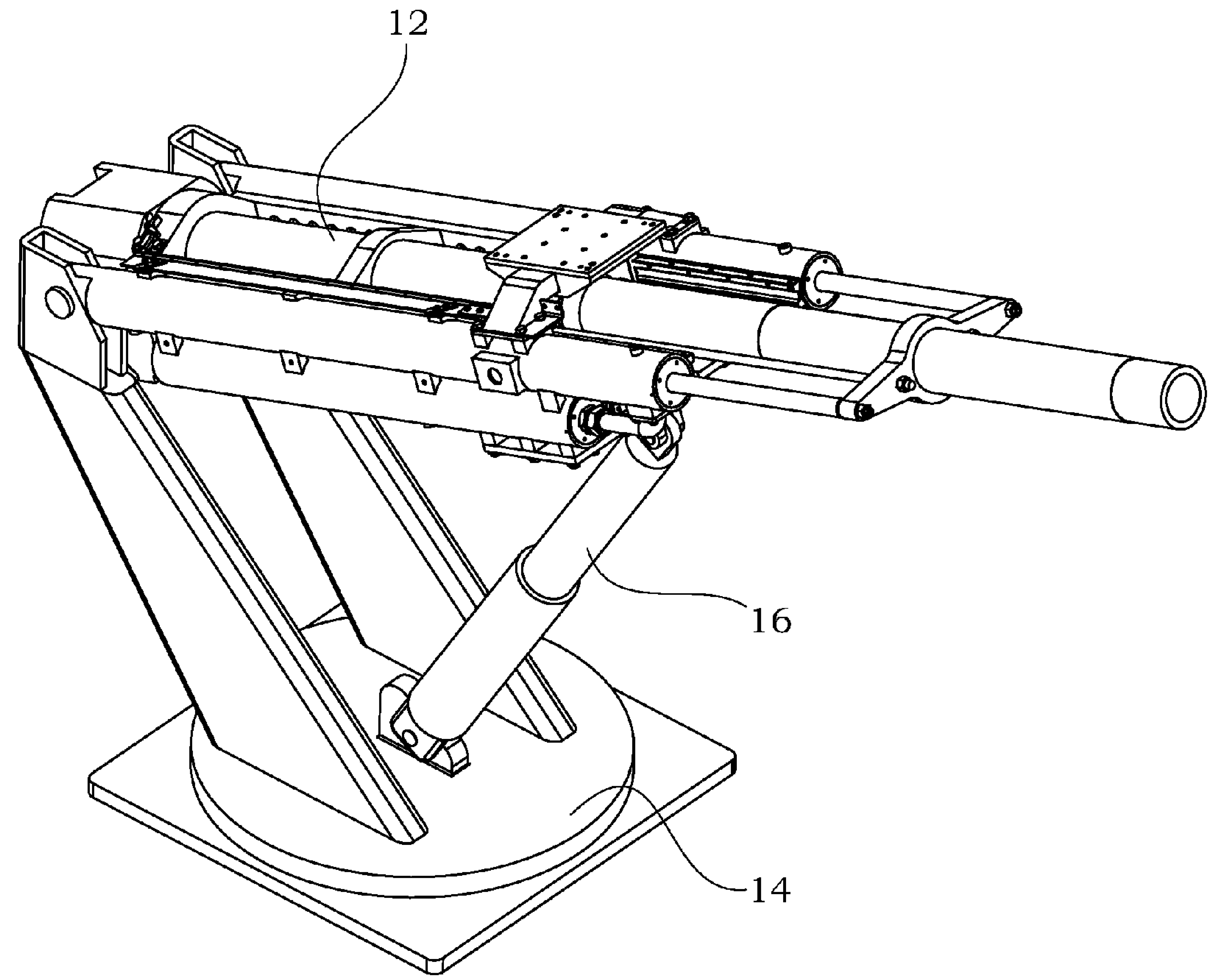

FIG. 1

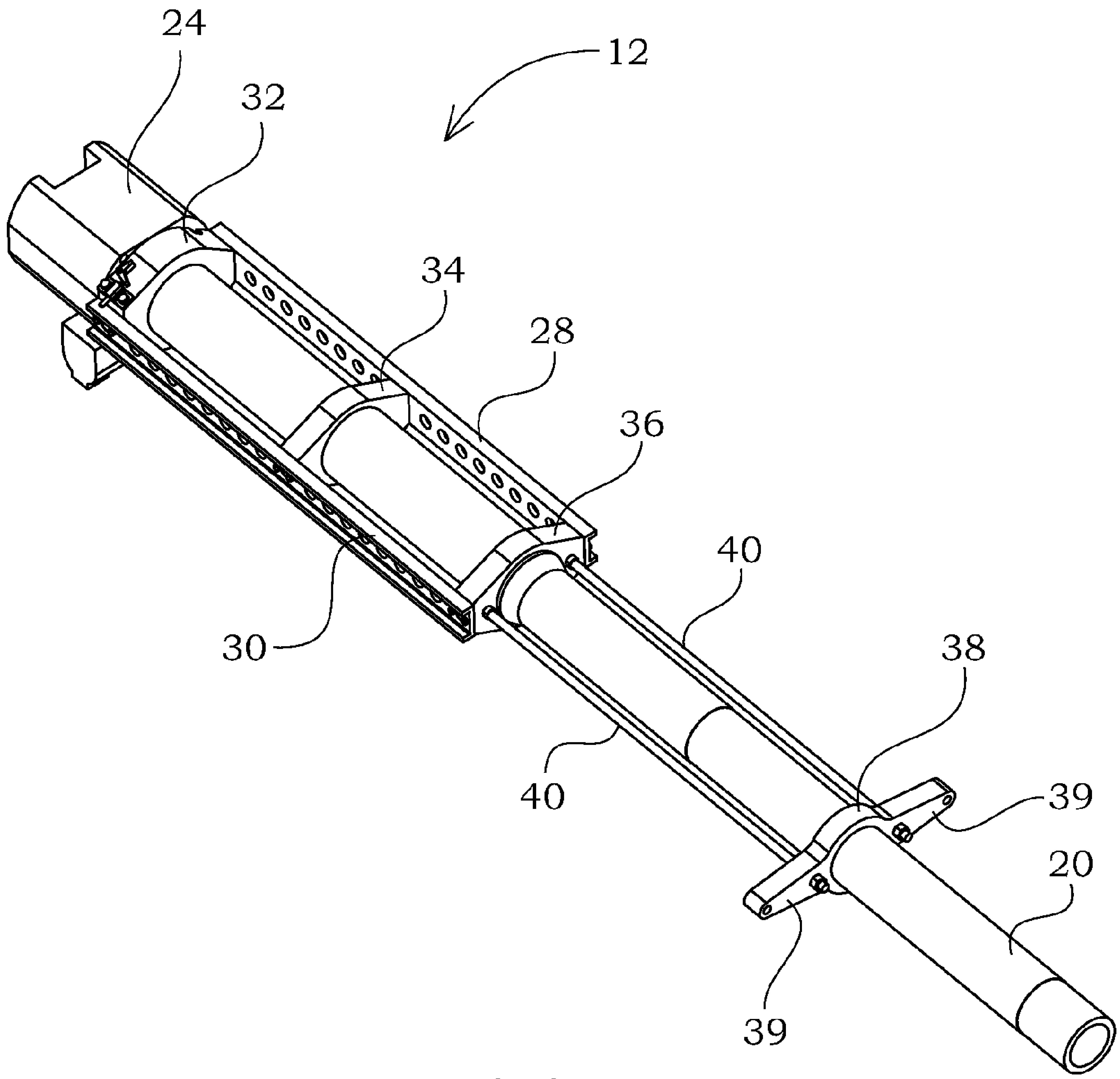

FIG.2

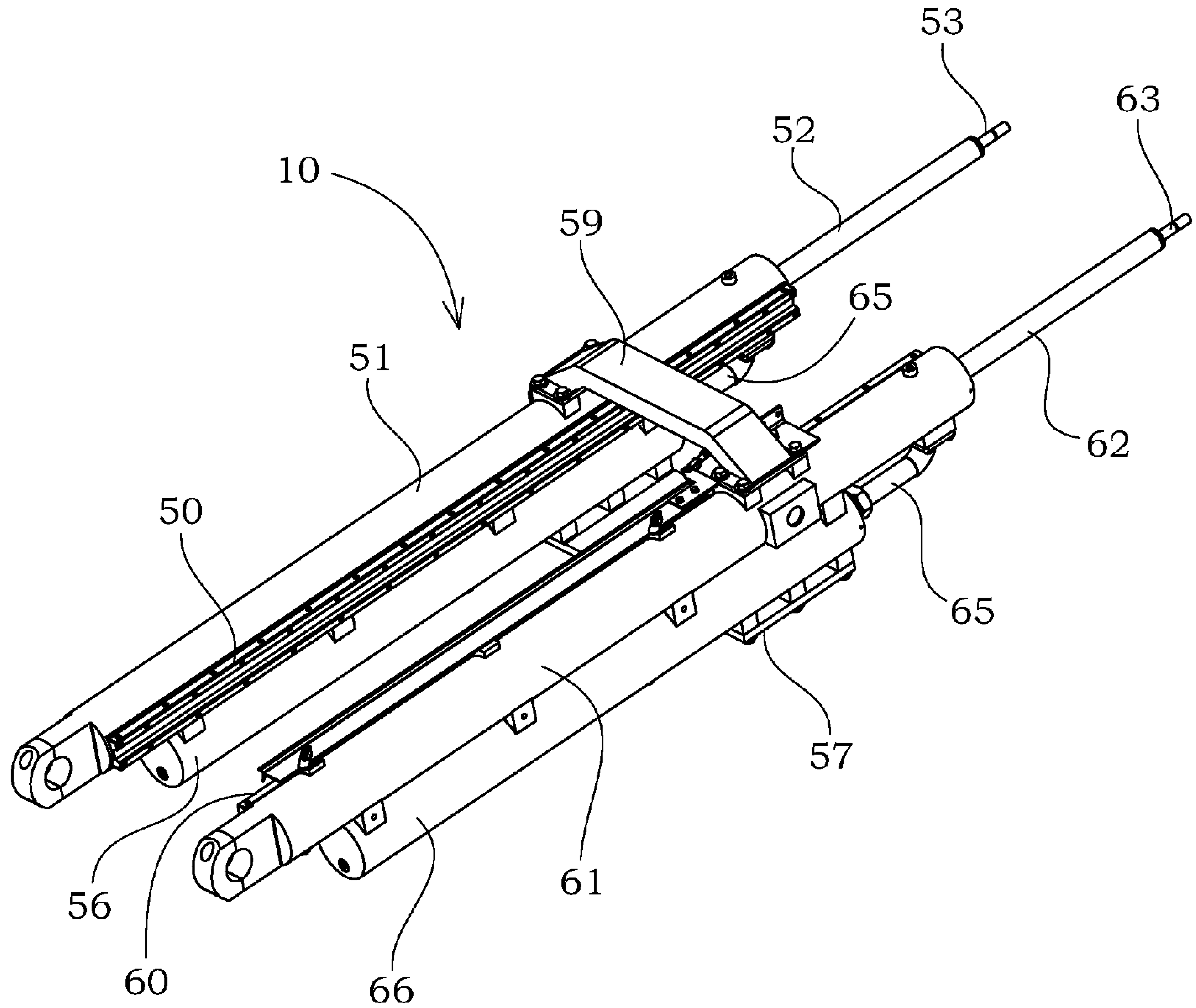

FIG. 3

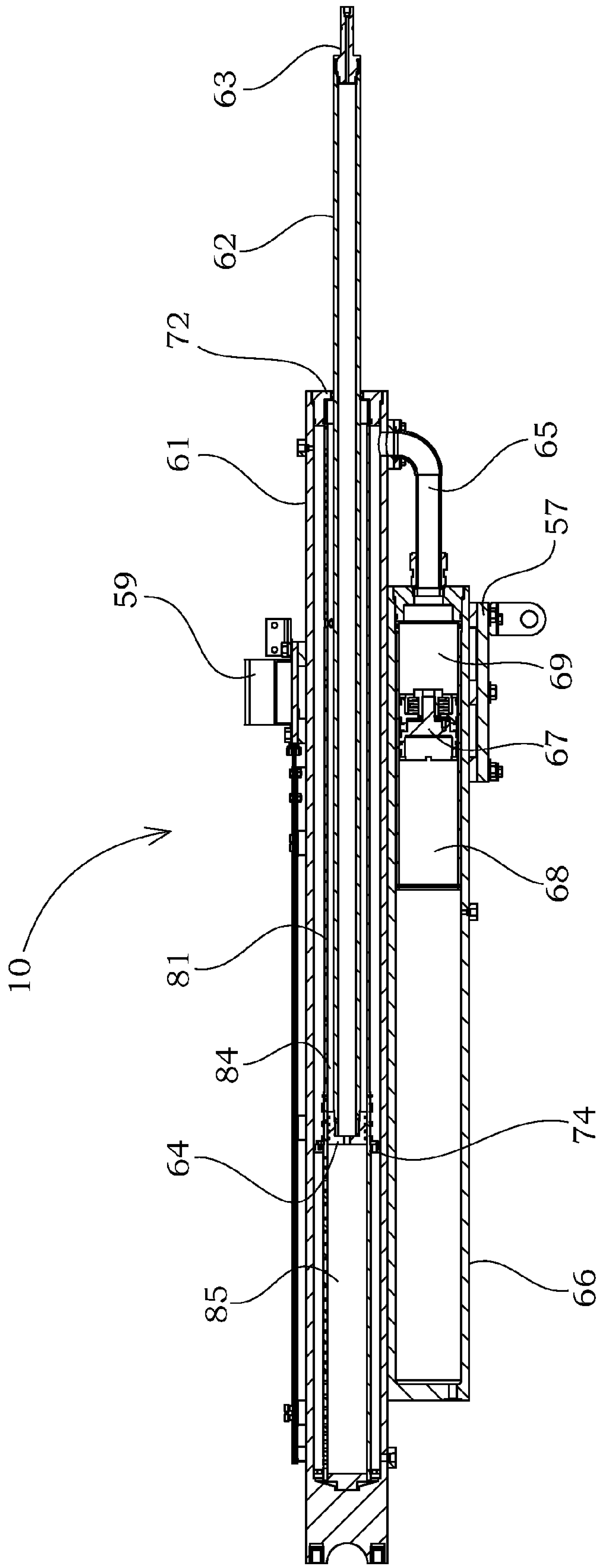

FIG. 4

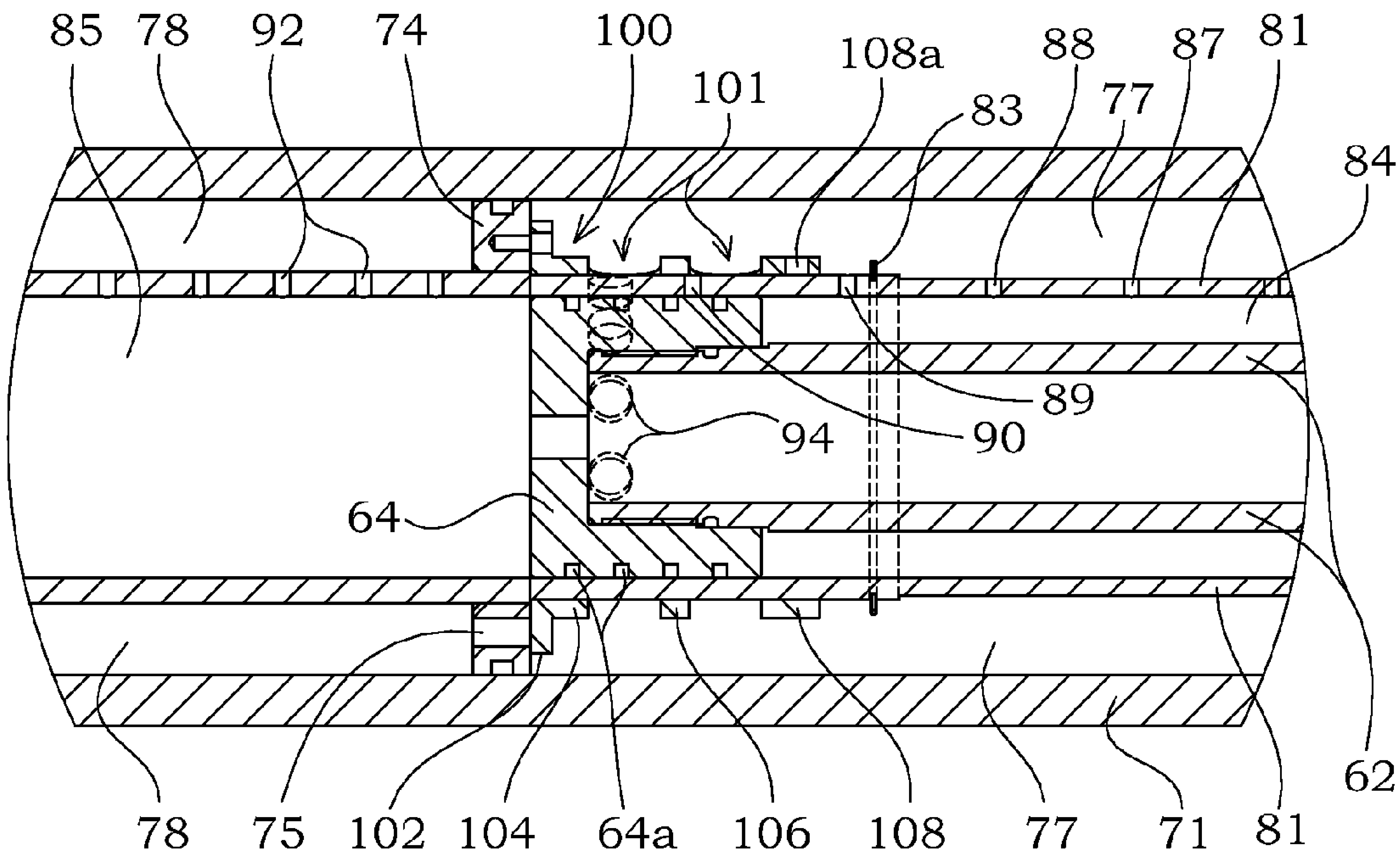

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FIG. 5

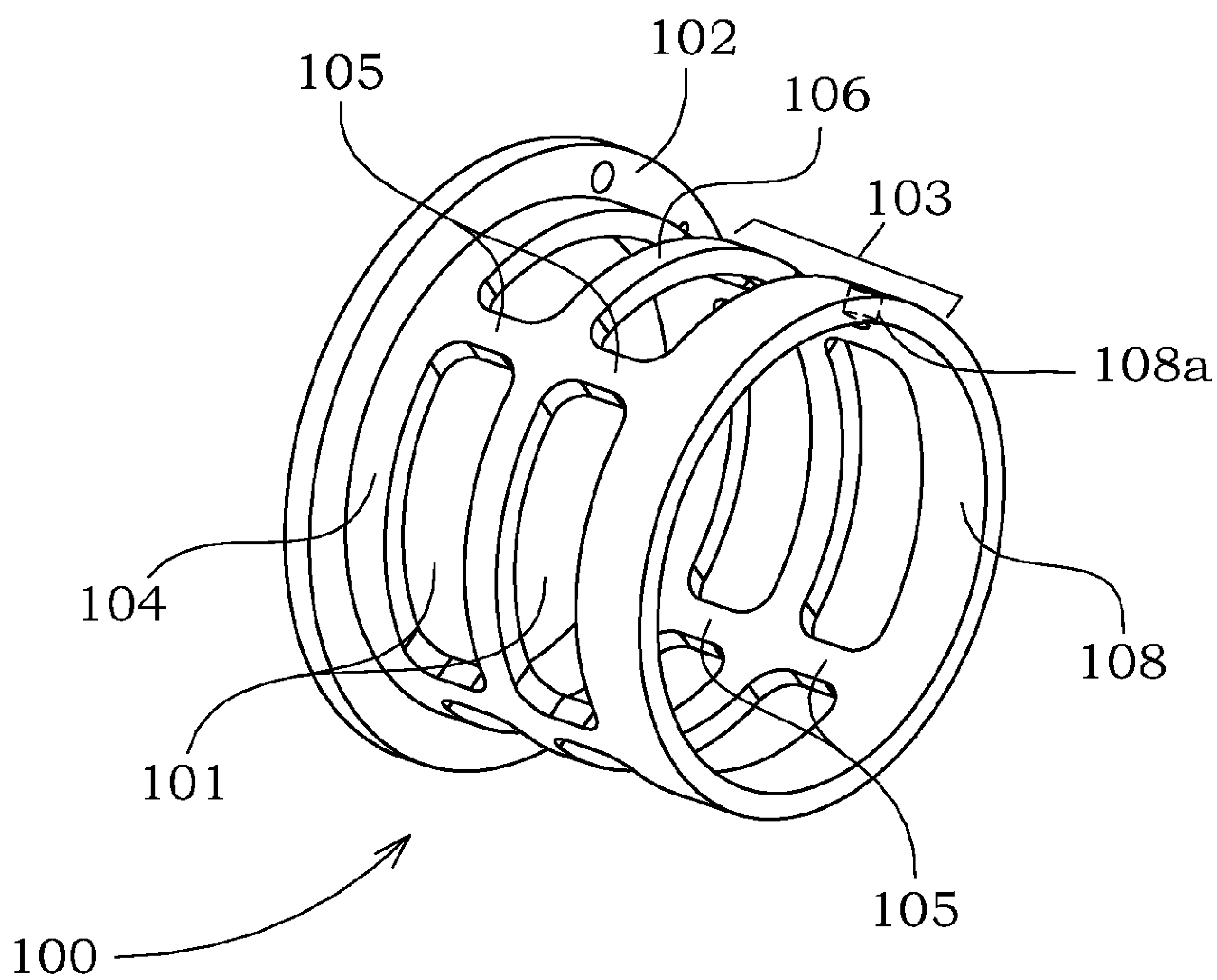

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FIG. 5A

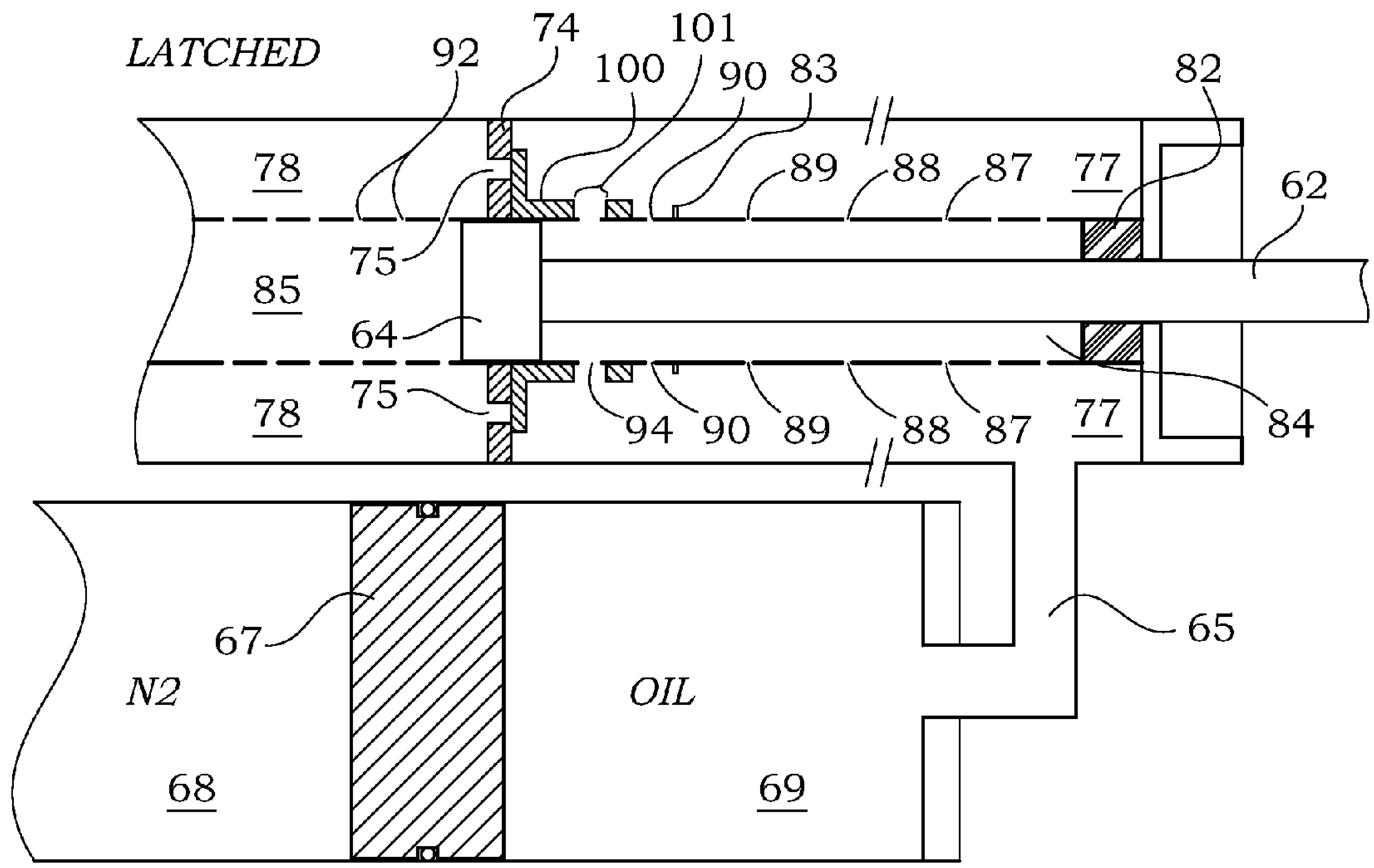
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FIG. 6

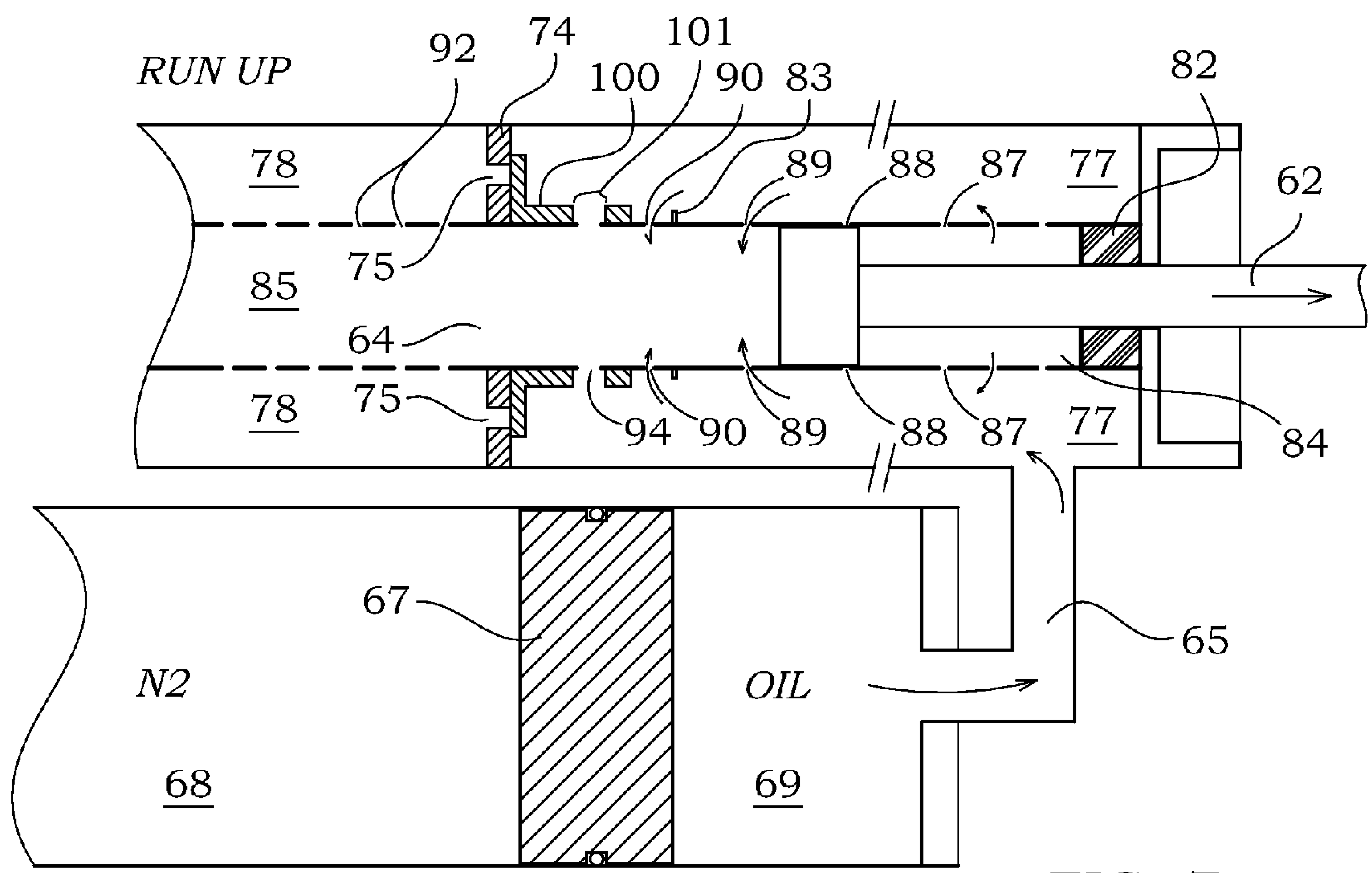
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FIG. 7

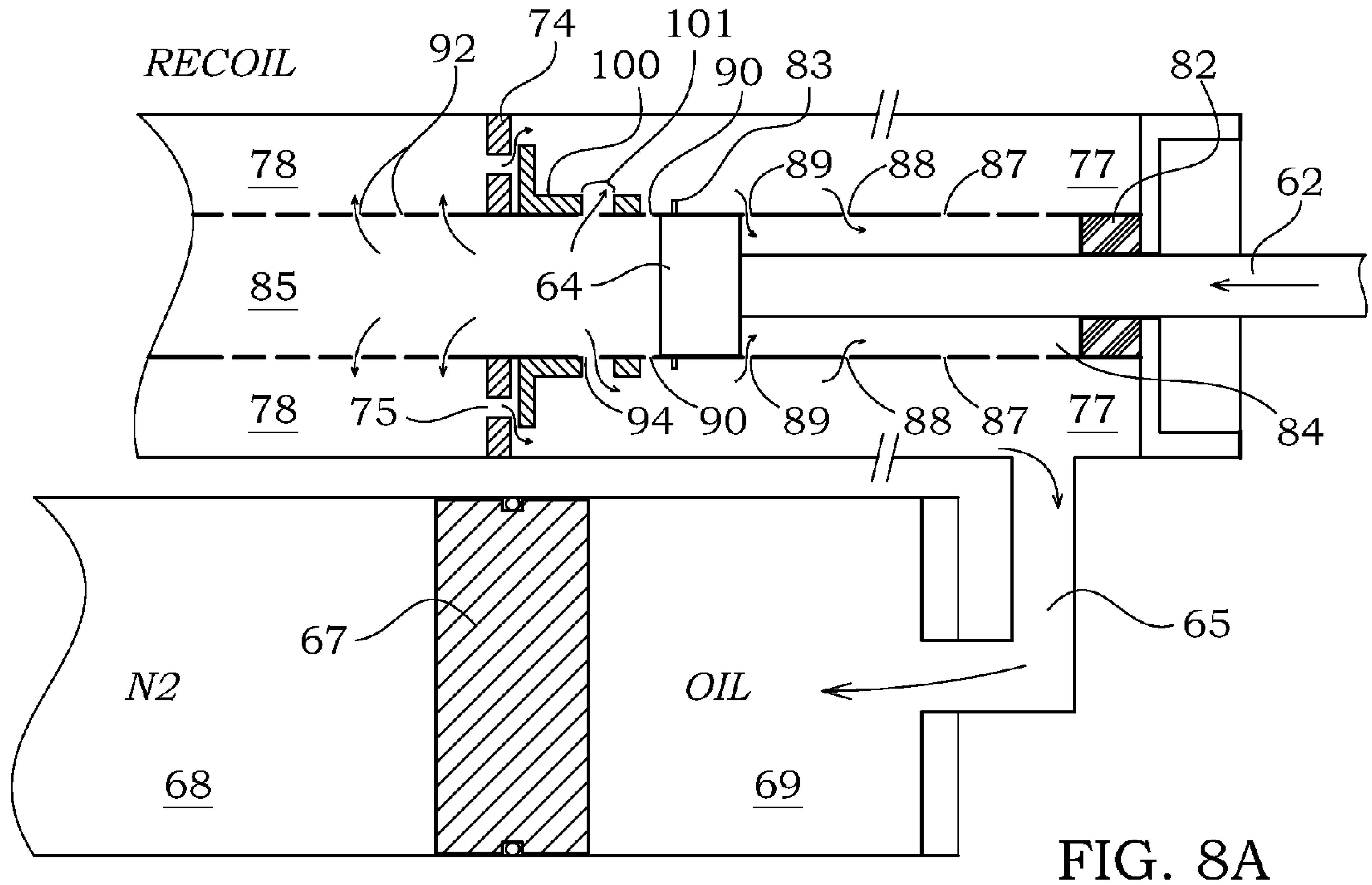
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FIG. 8A

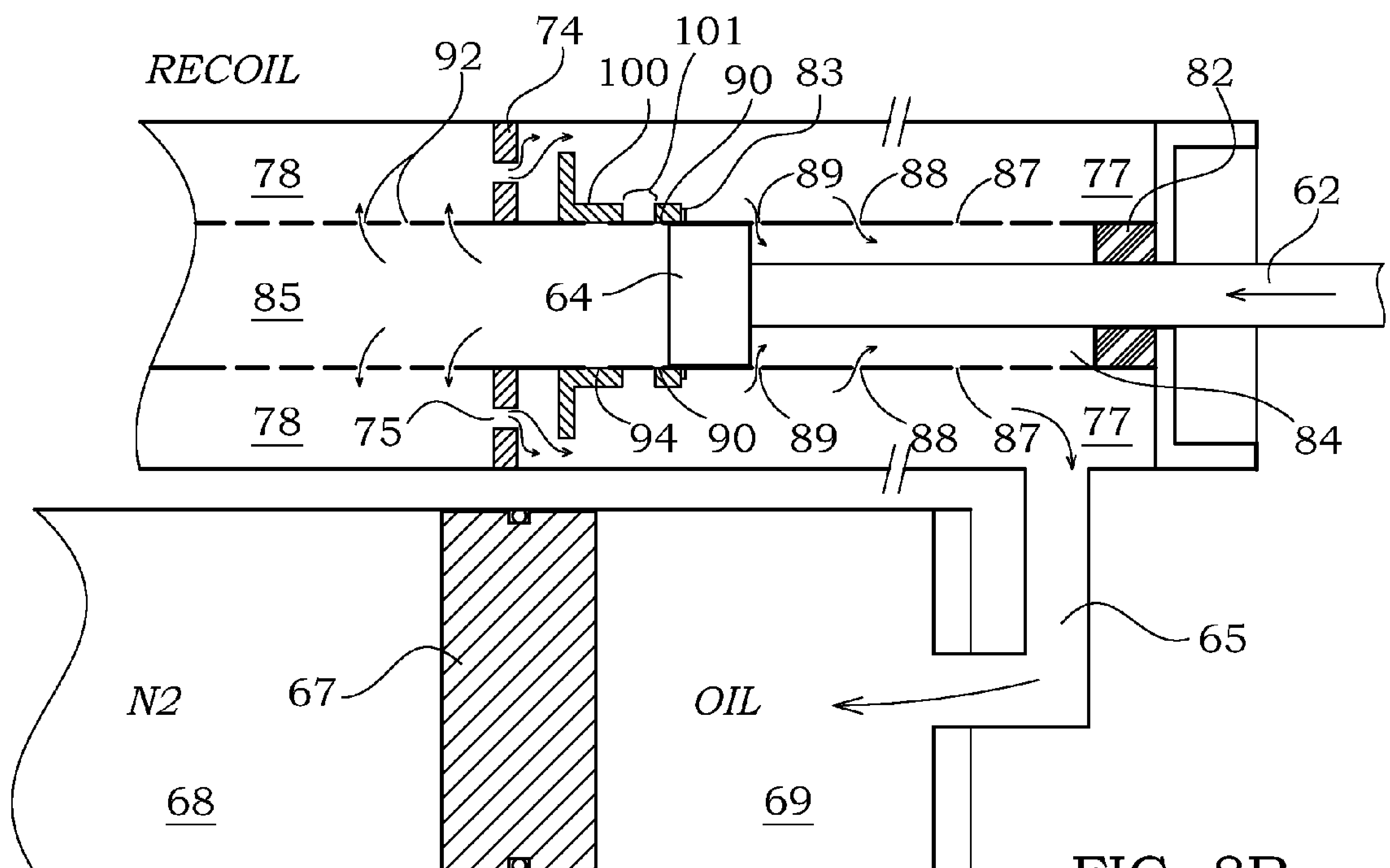
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FIG. 8B

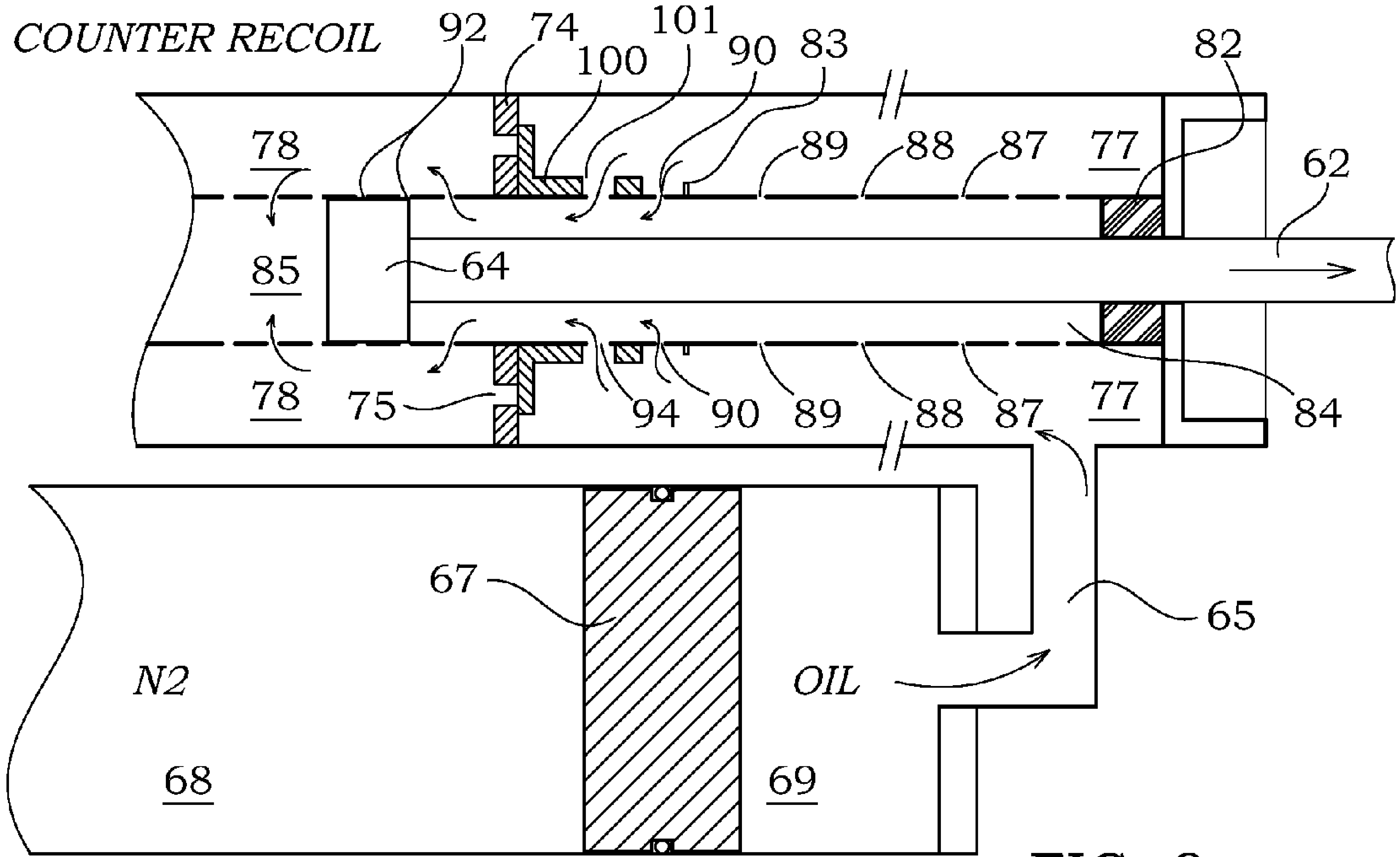
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FIG. 9

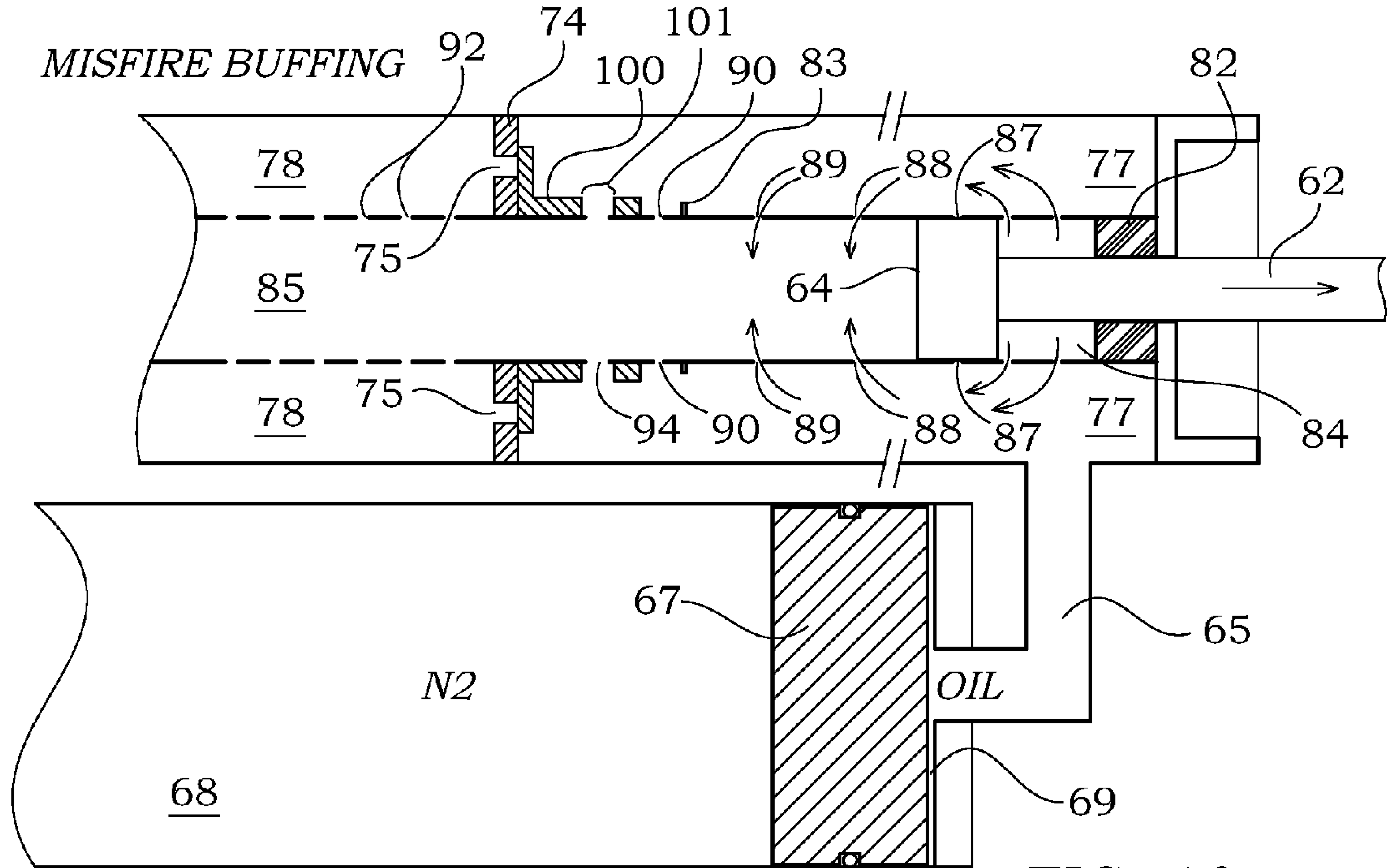
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FIG. 10

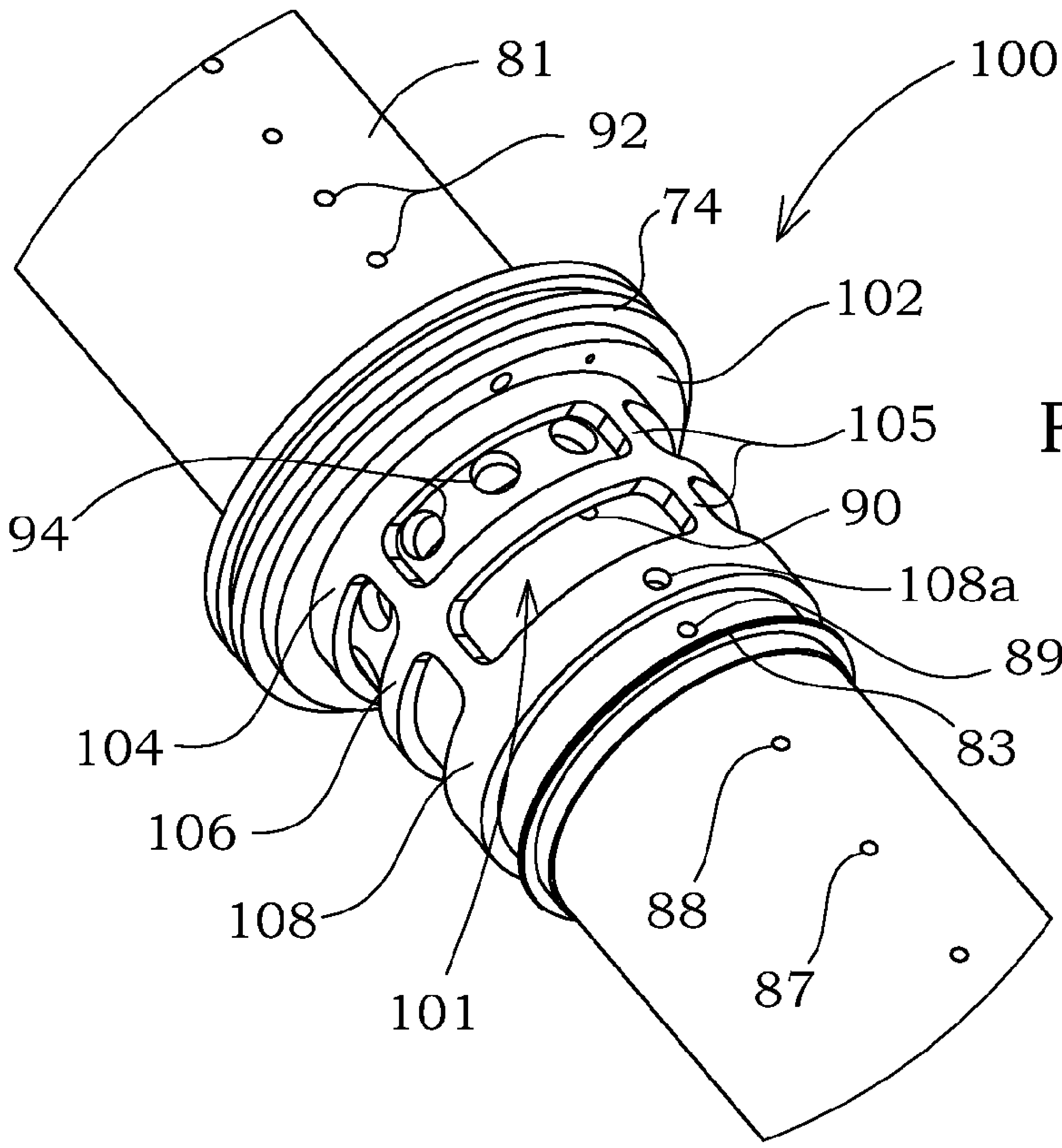

FIG. 11A

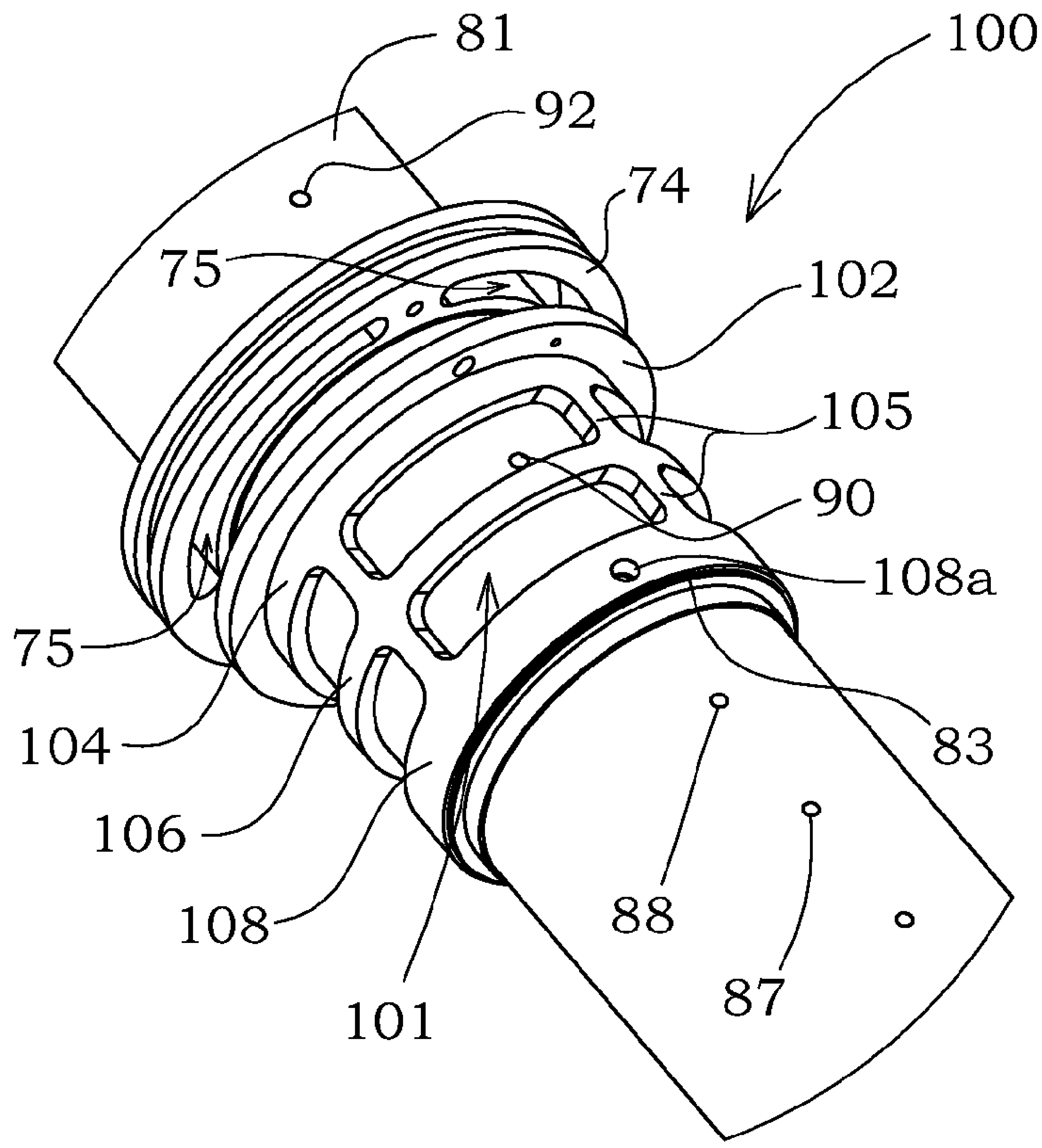

FIG. 11B

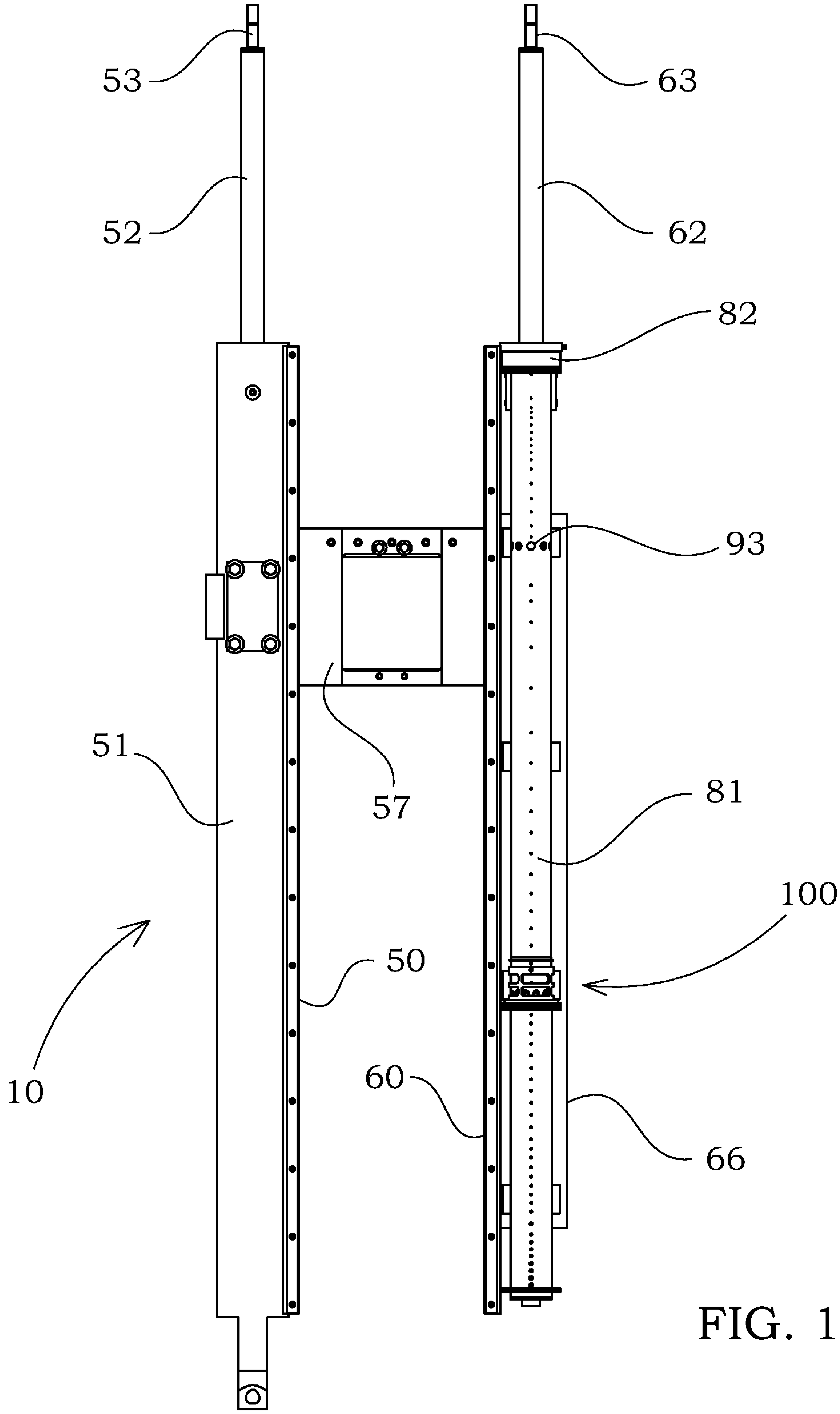

FIG. 12

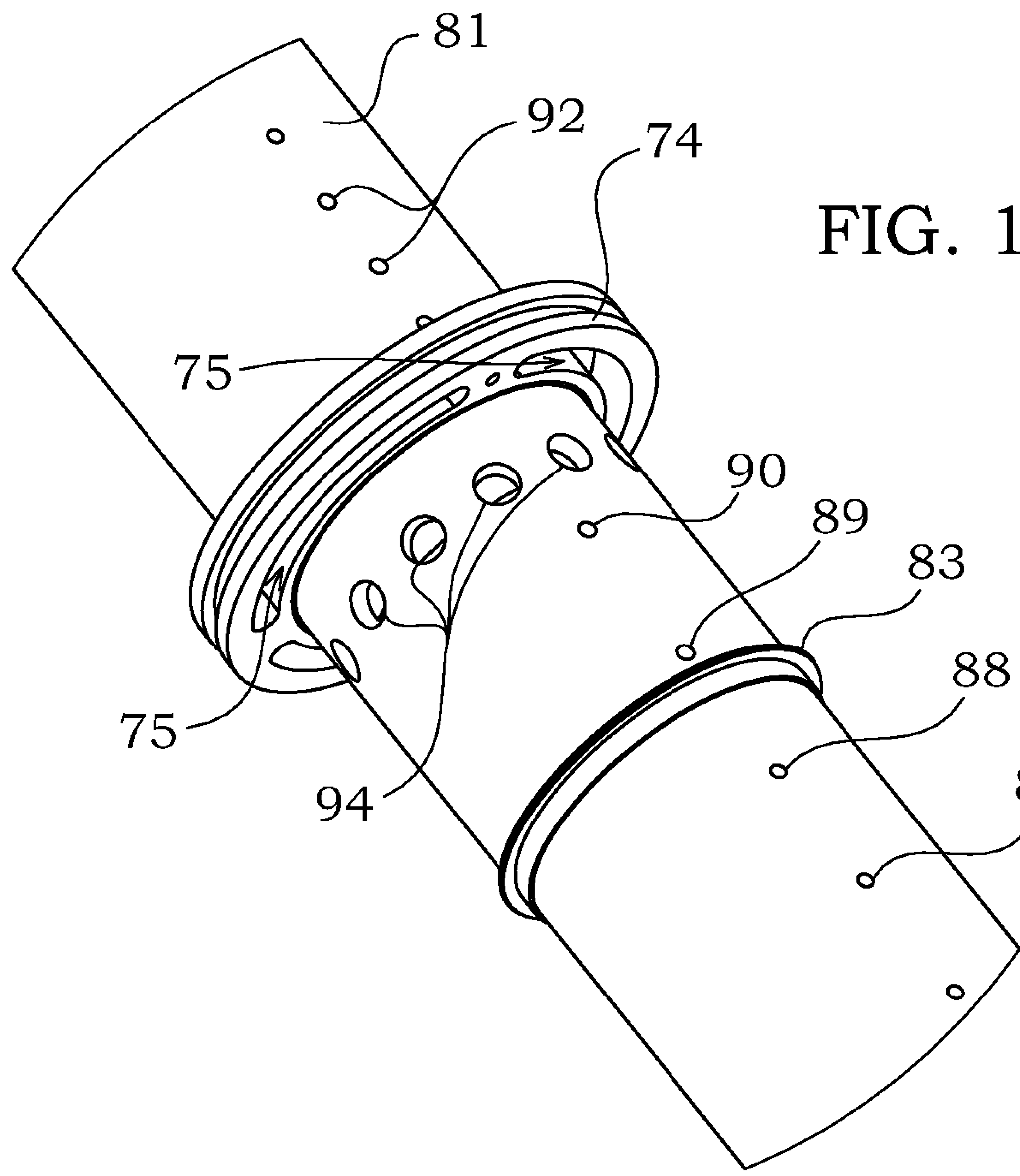

FIG. 13A

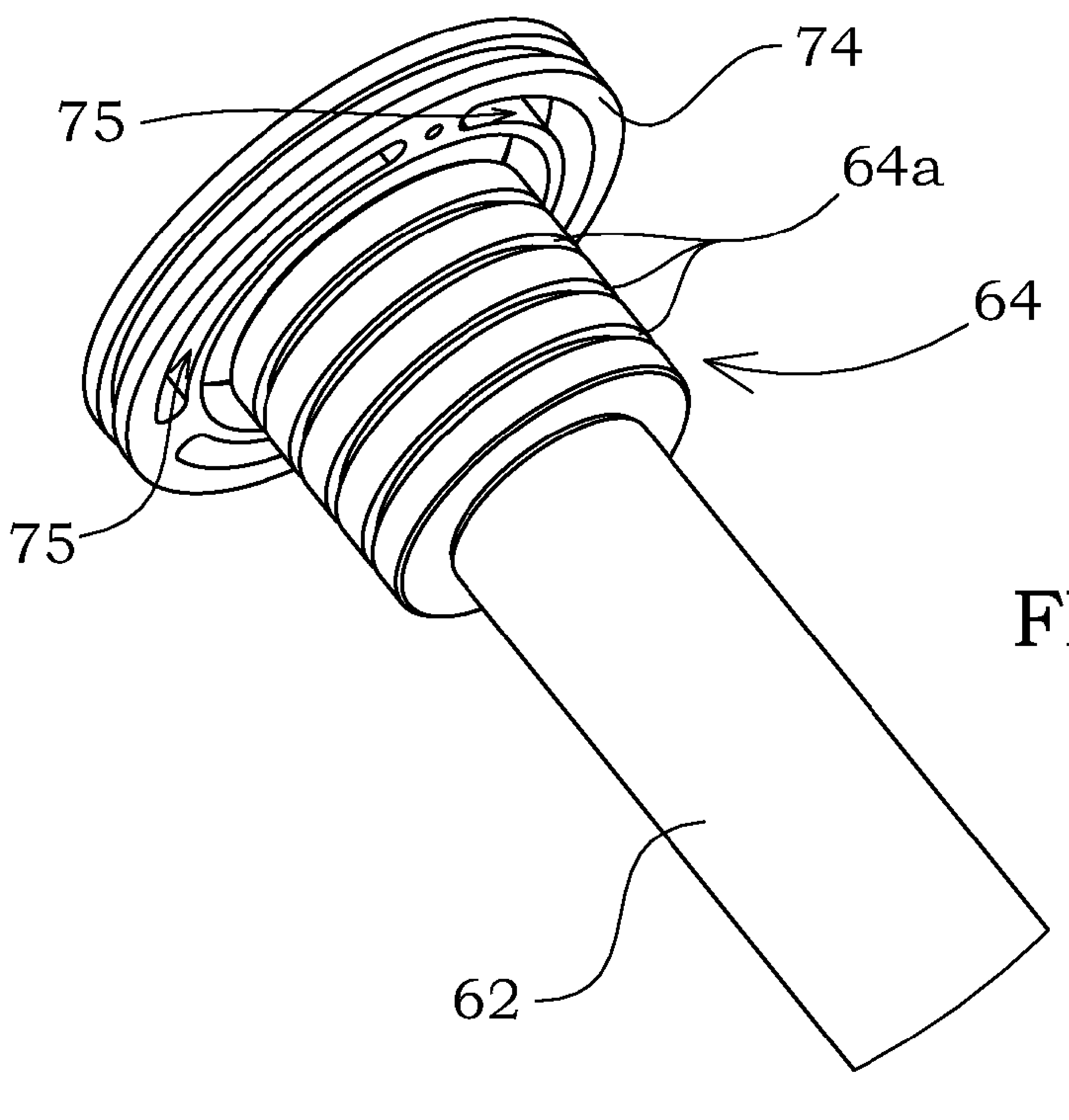

FIG. 13B

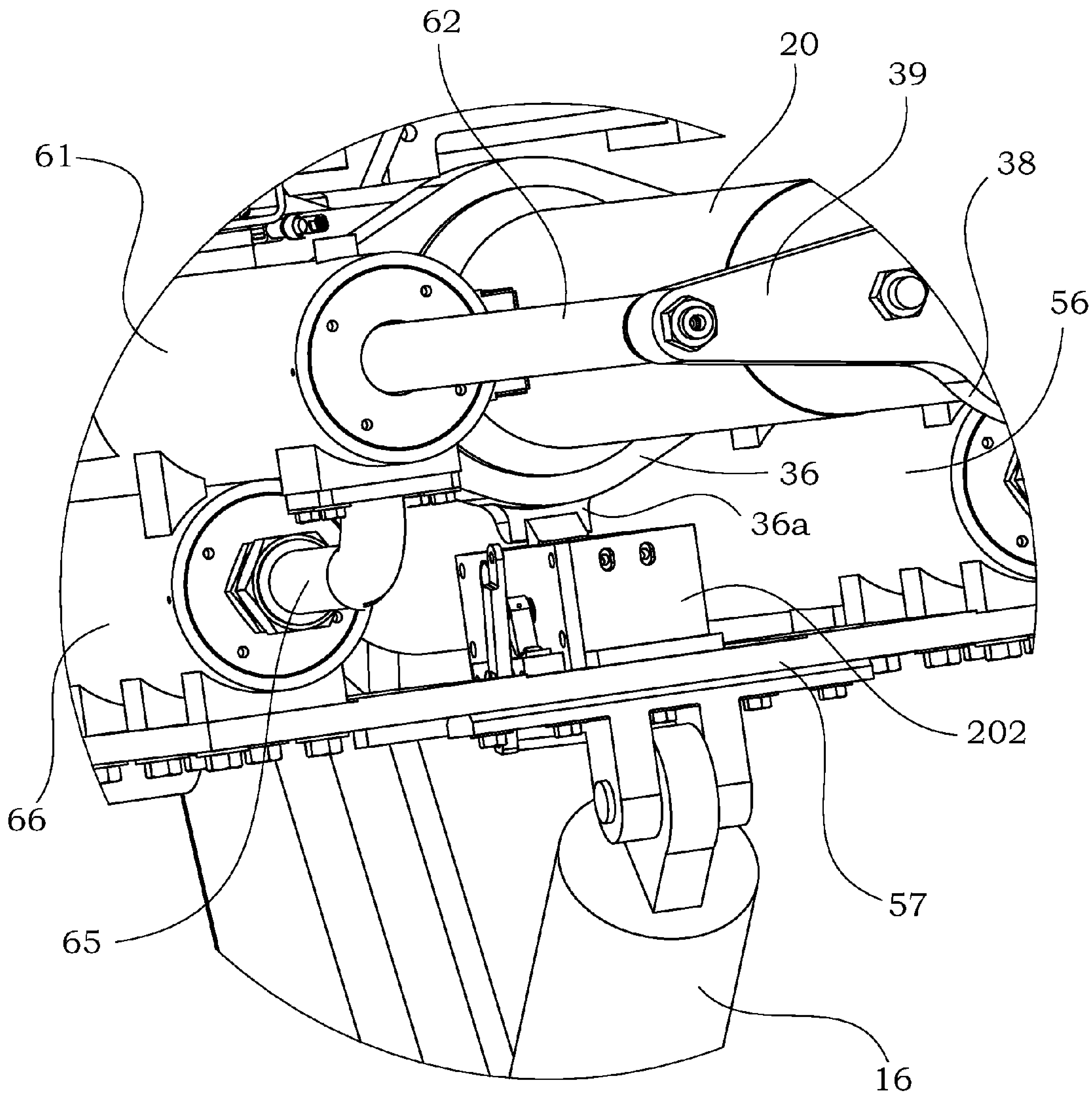

FIG. 14

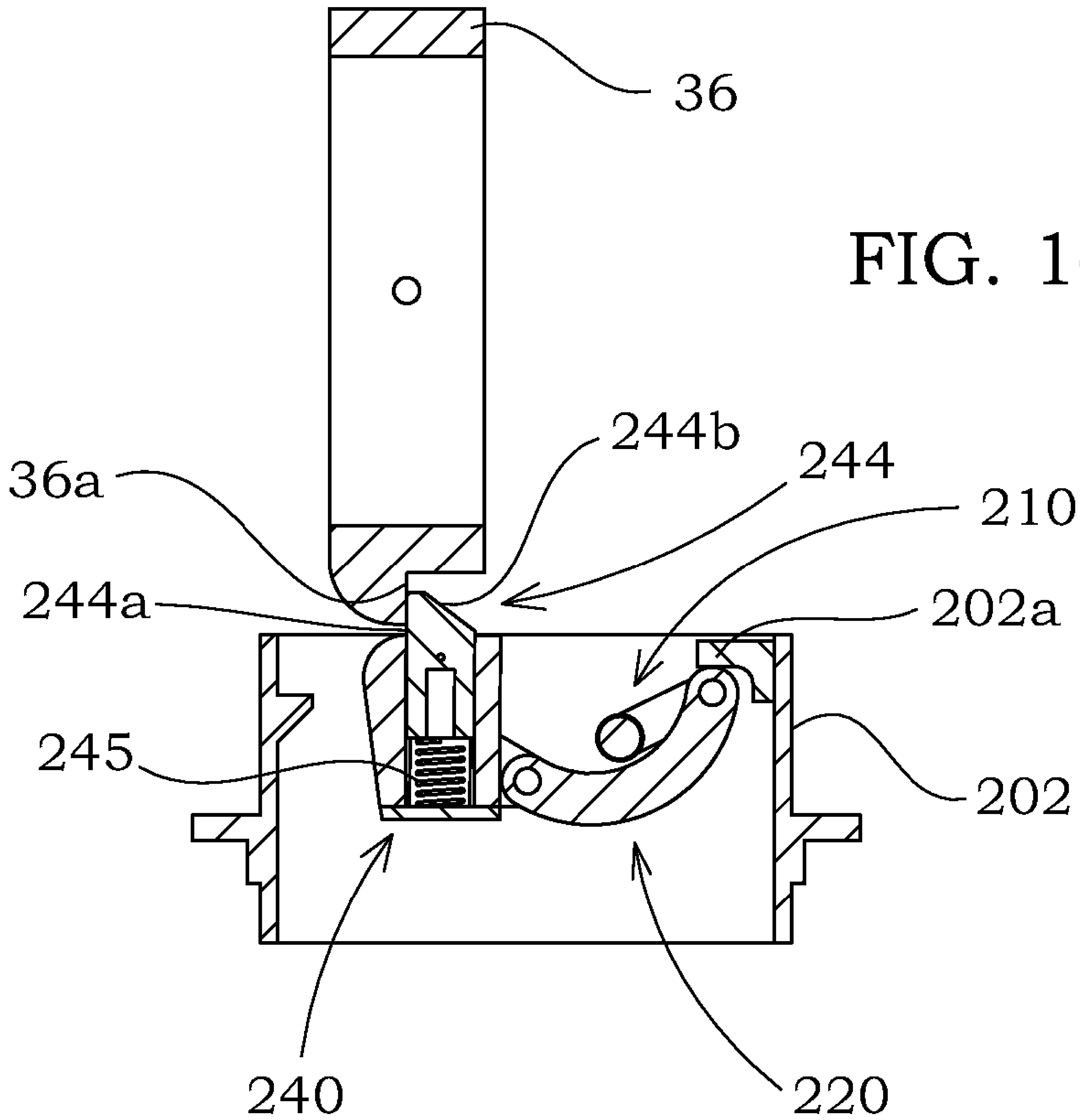

FIG. 14A

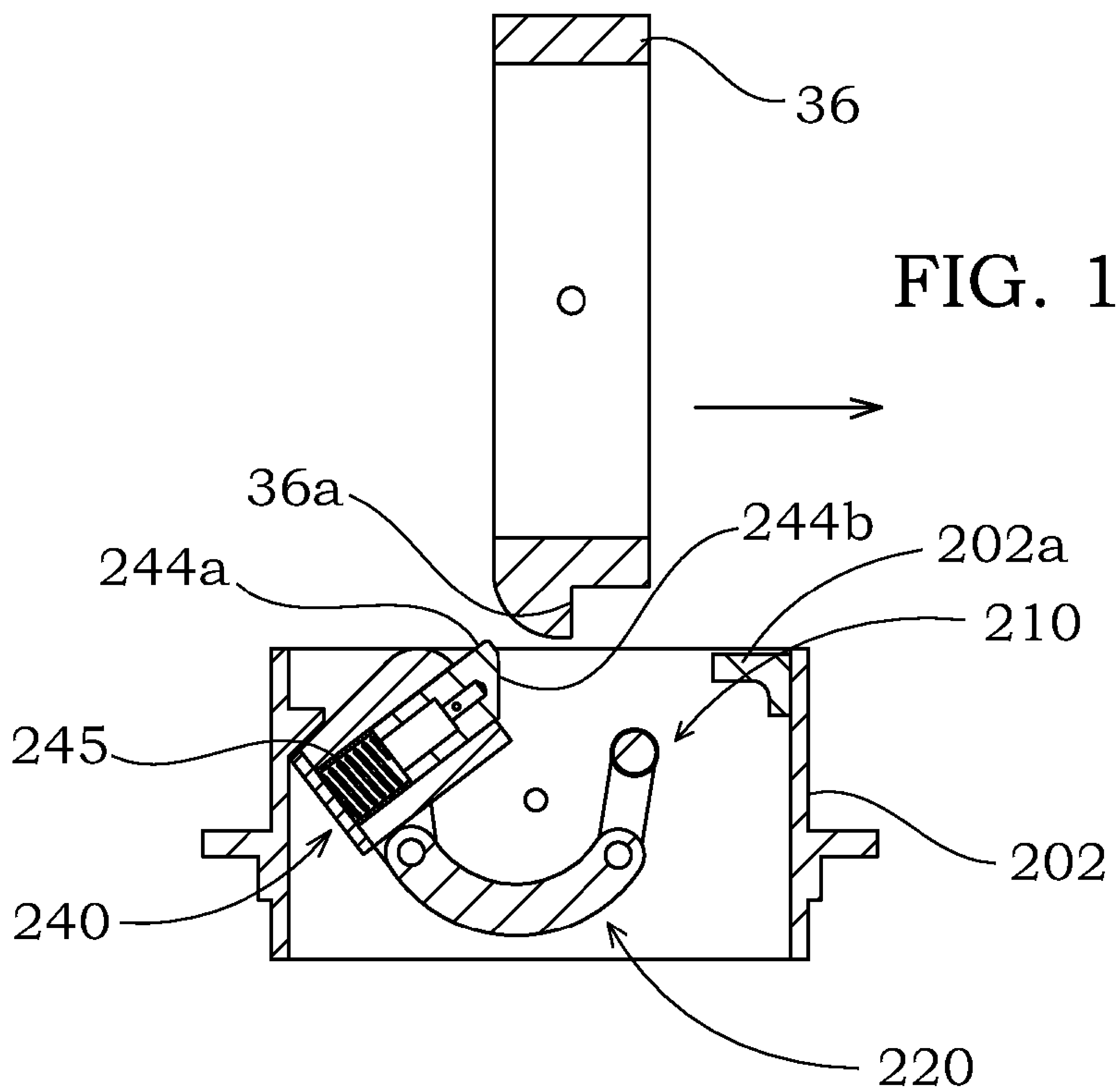

FIG. 14B

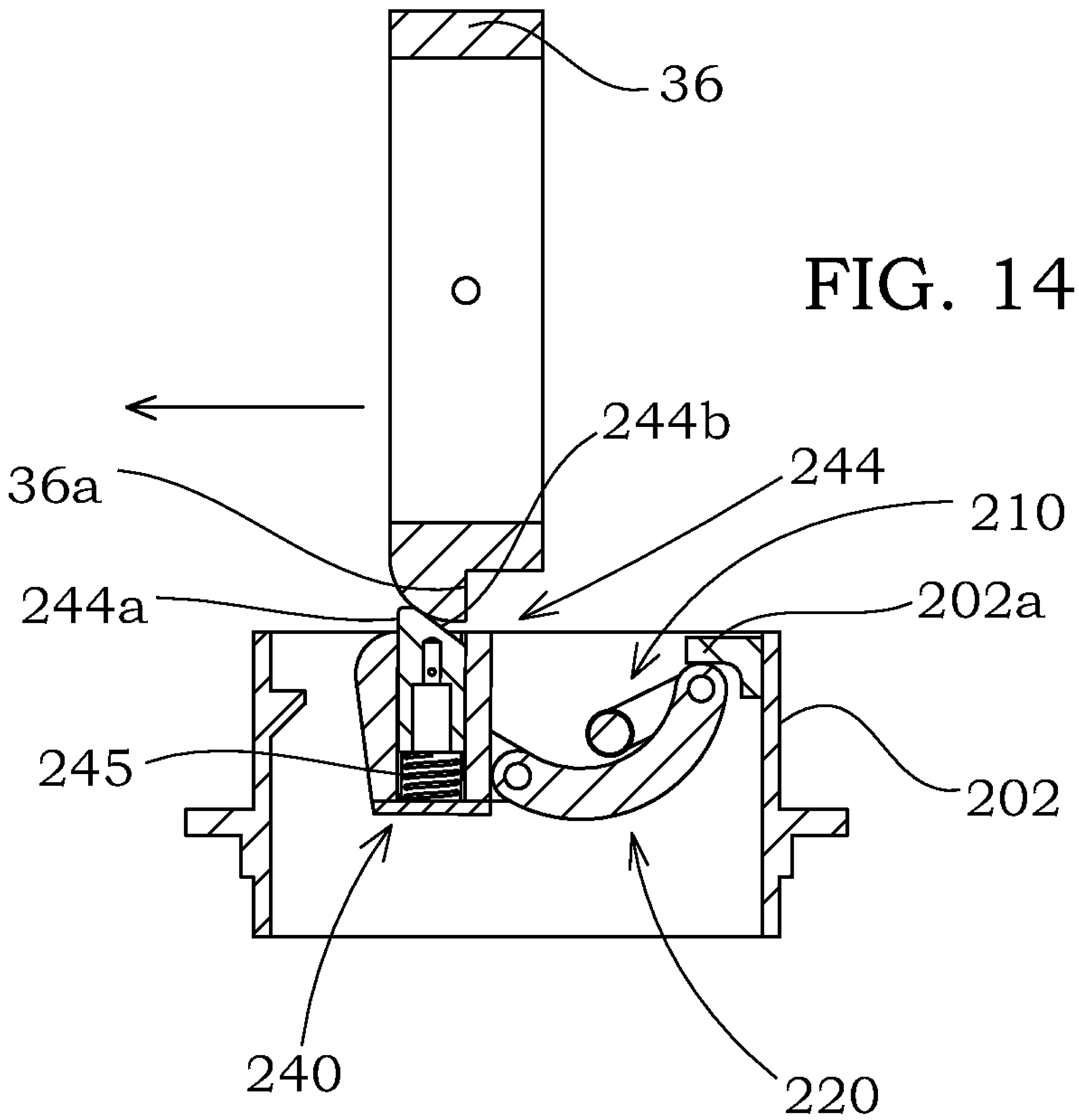

FIG. 14C

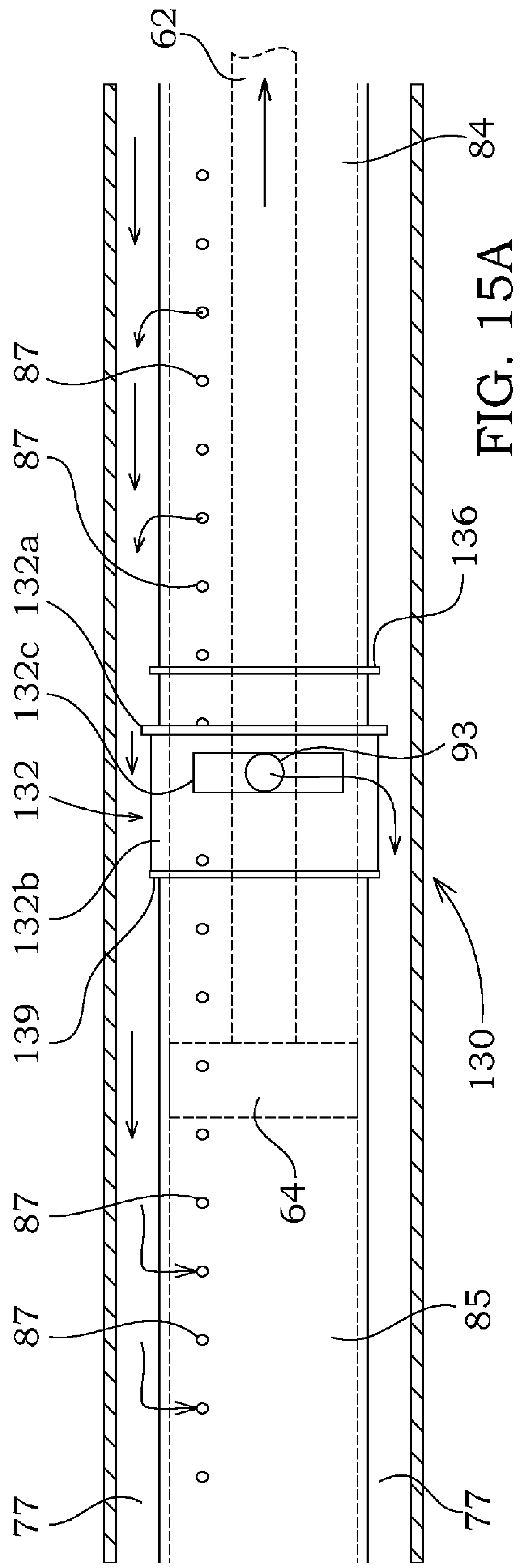

FIG. 15A

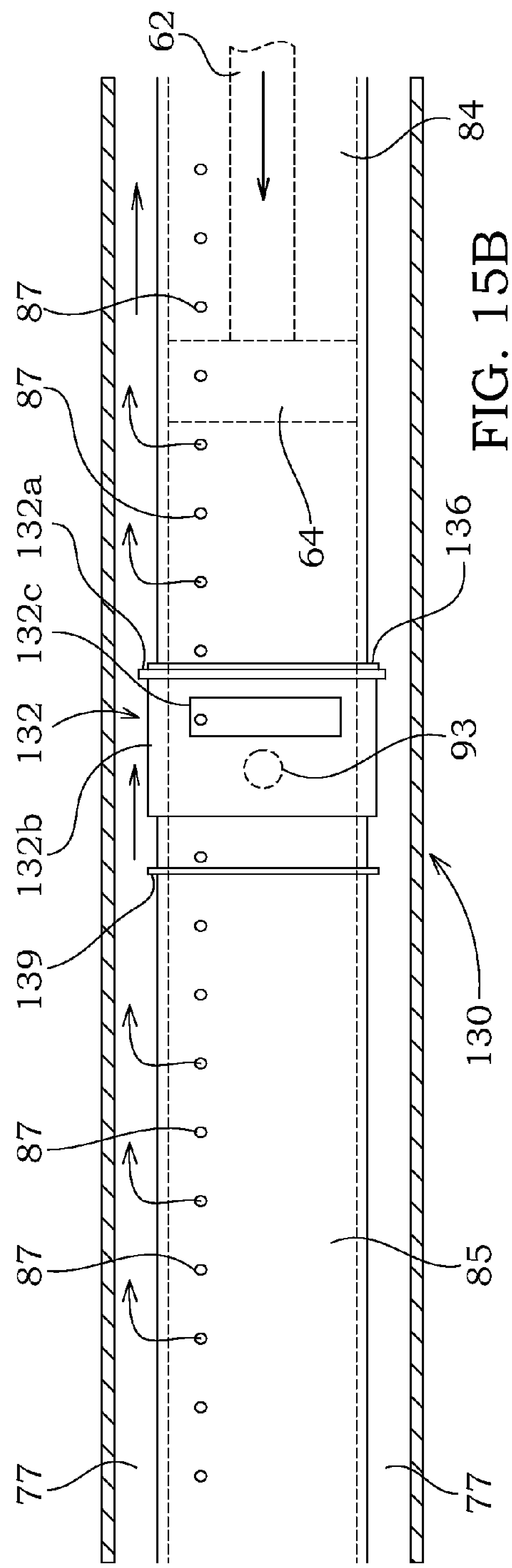

FIG. 15B

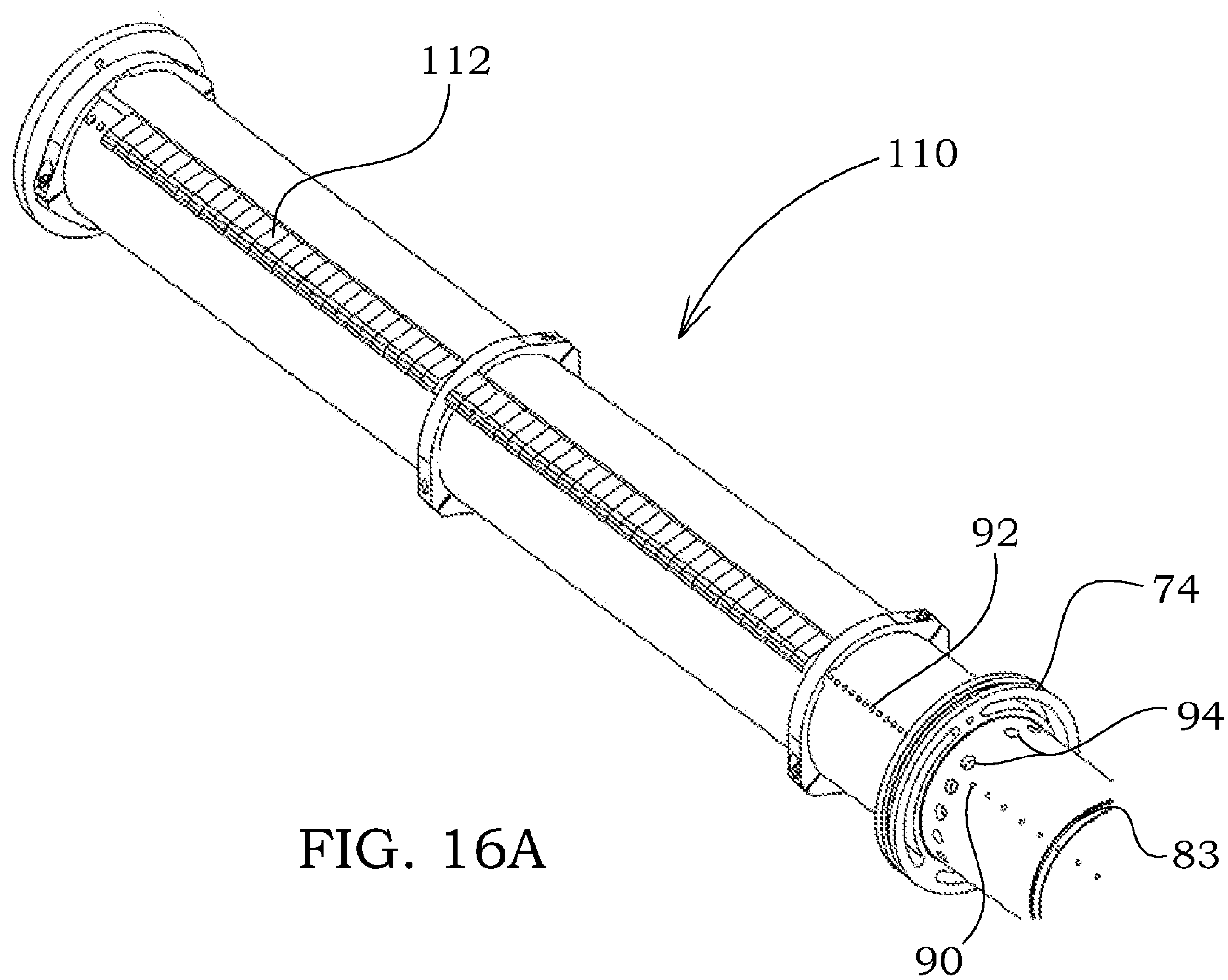

FIG. 16A

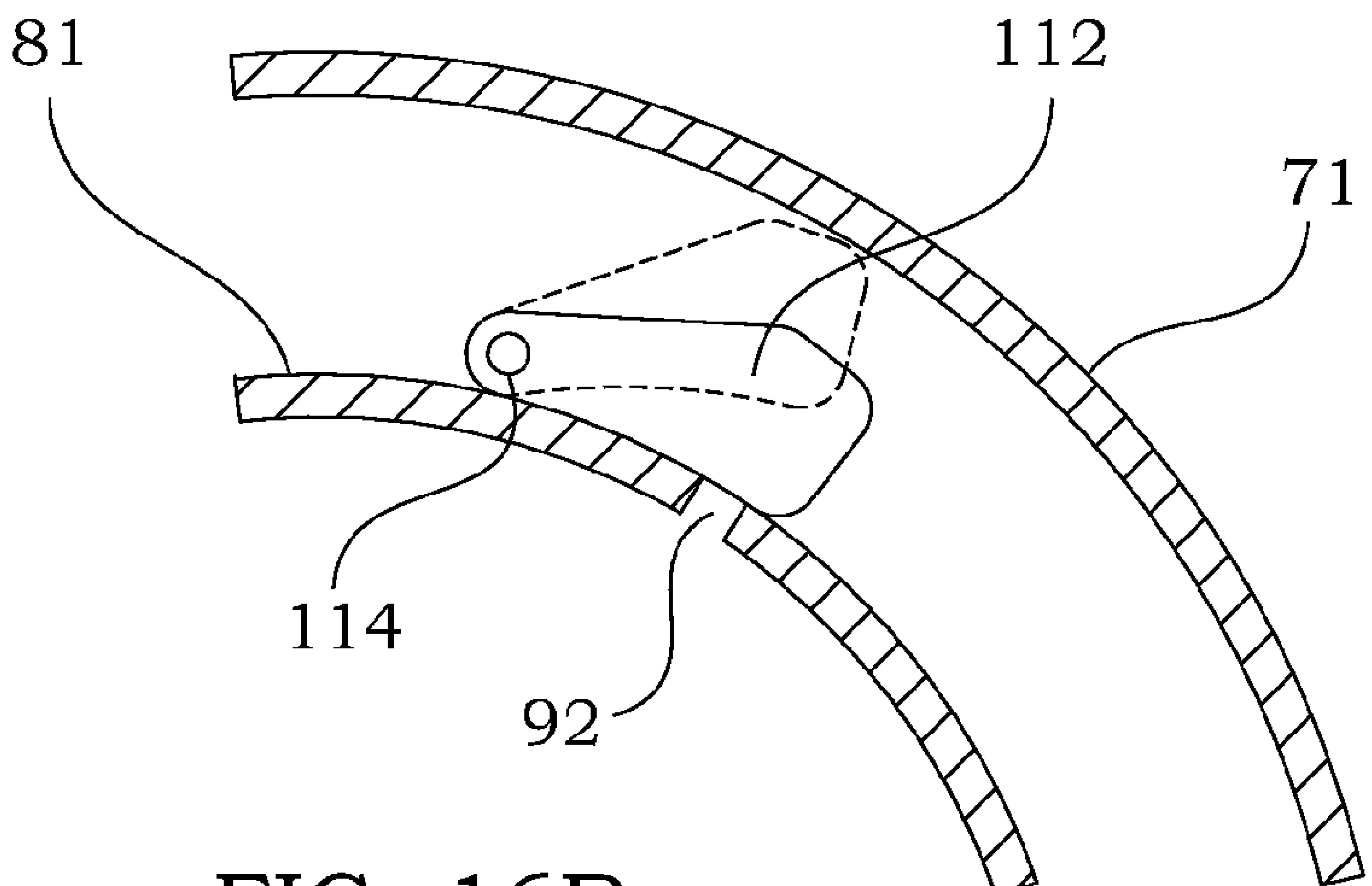

FIG. 16B

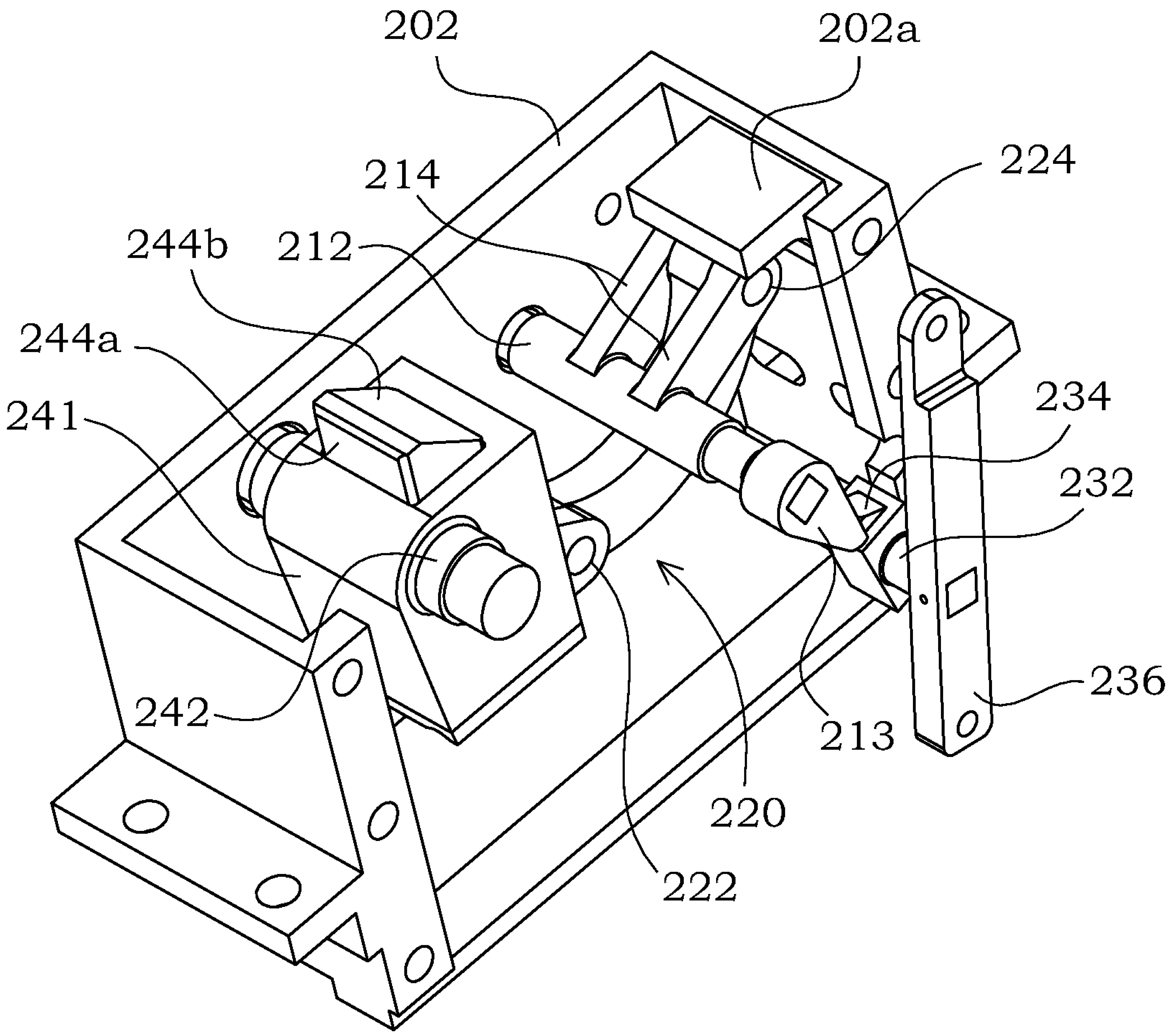

FIG. 17A

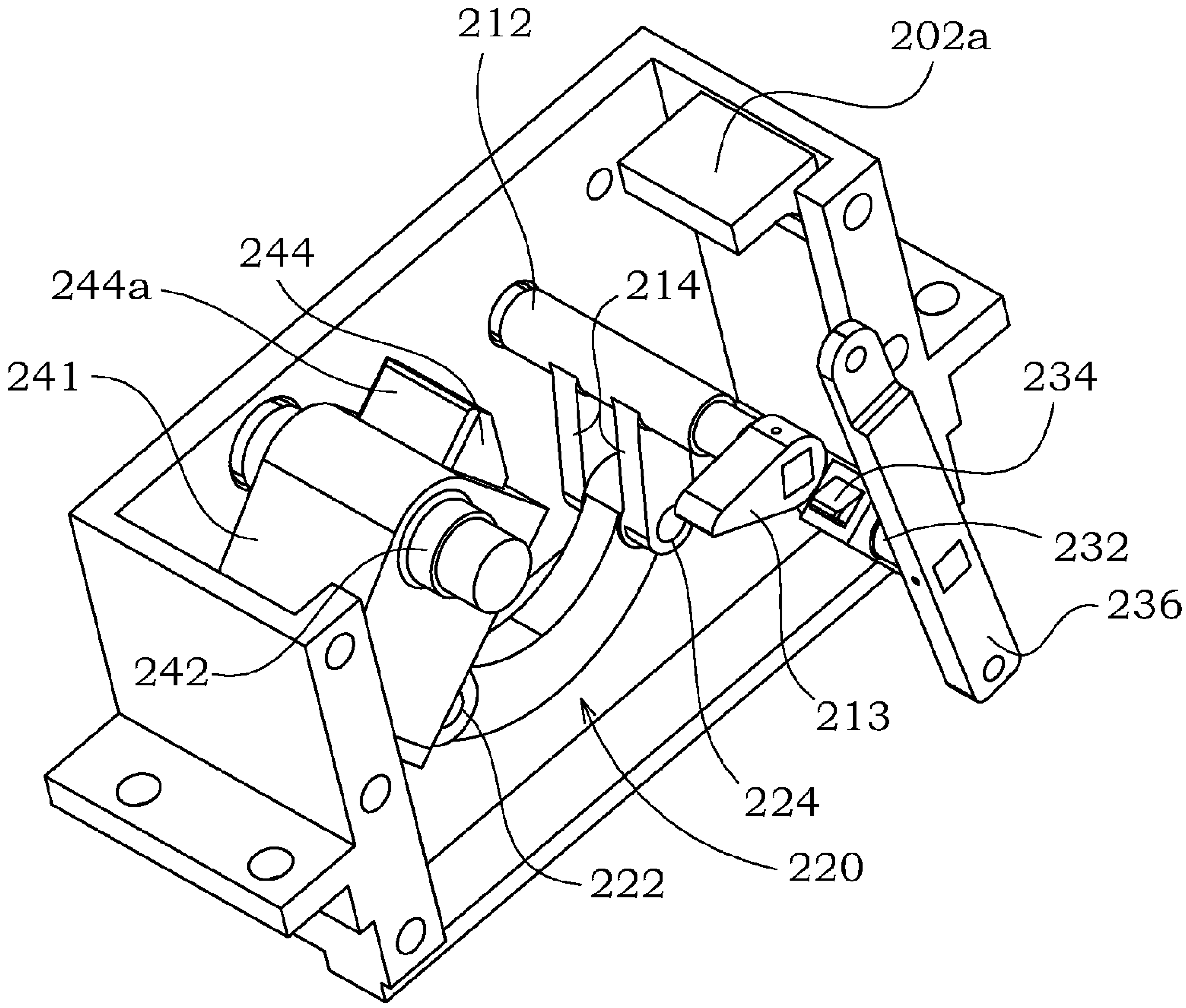

FIG. 17B

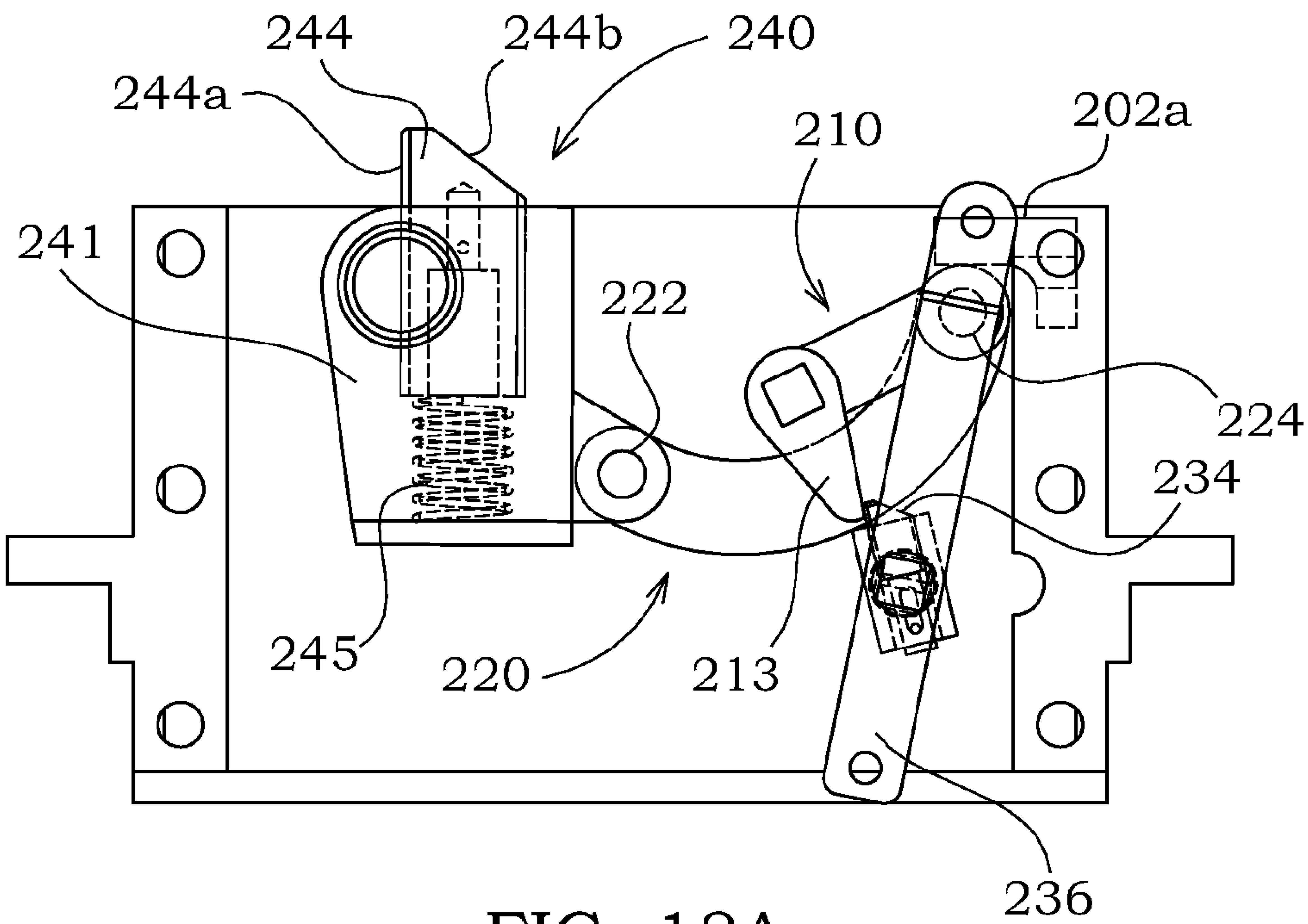

FIG. 18A

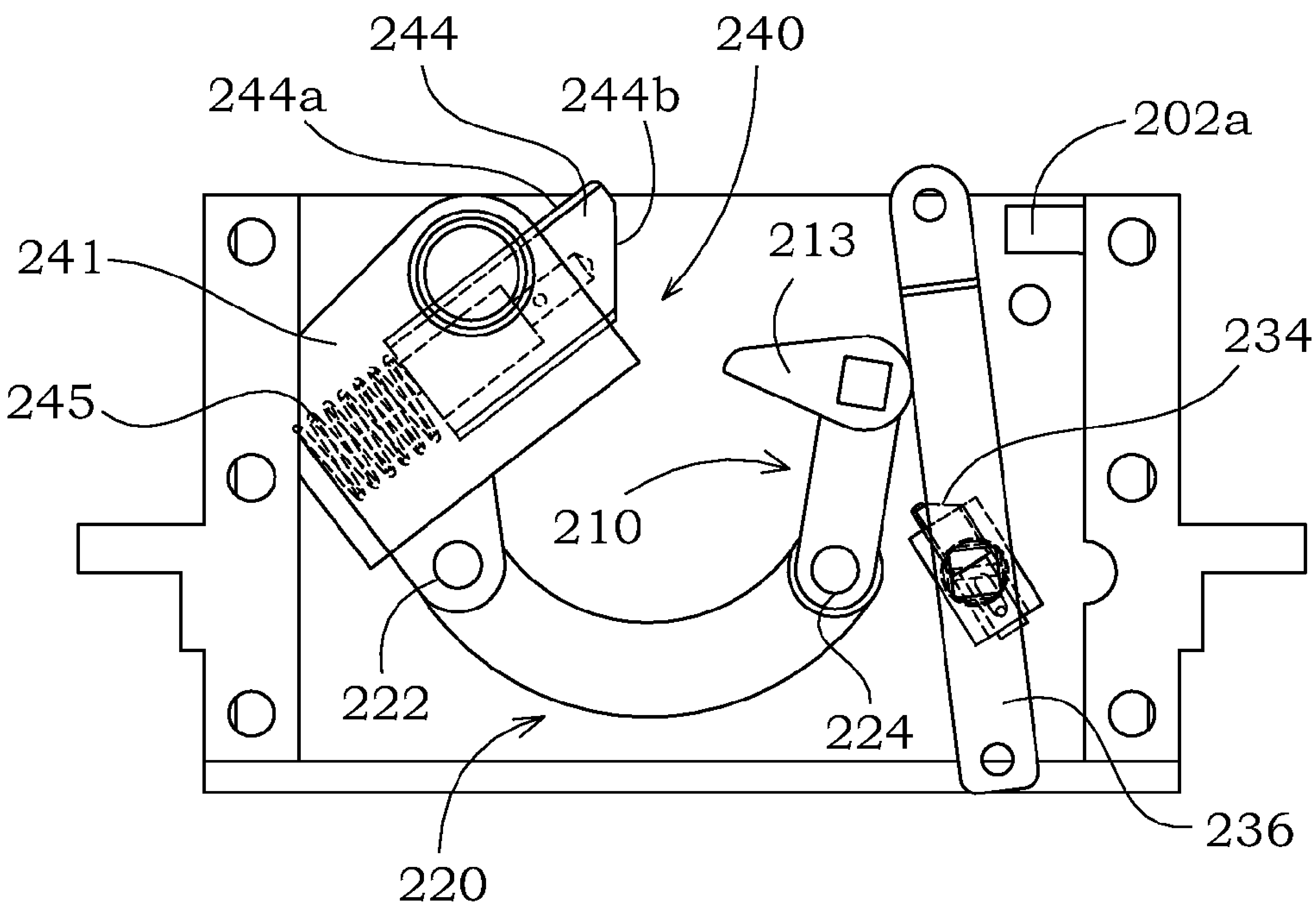

FIG. 18B

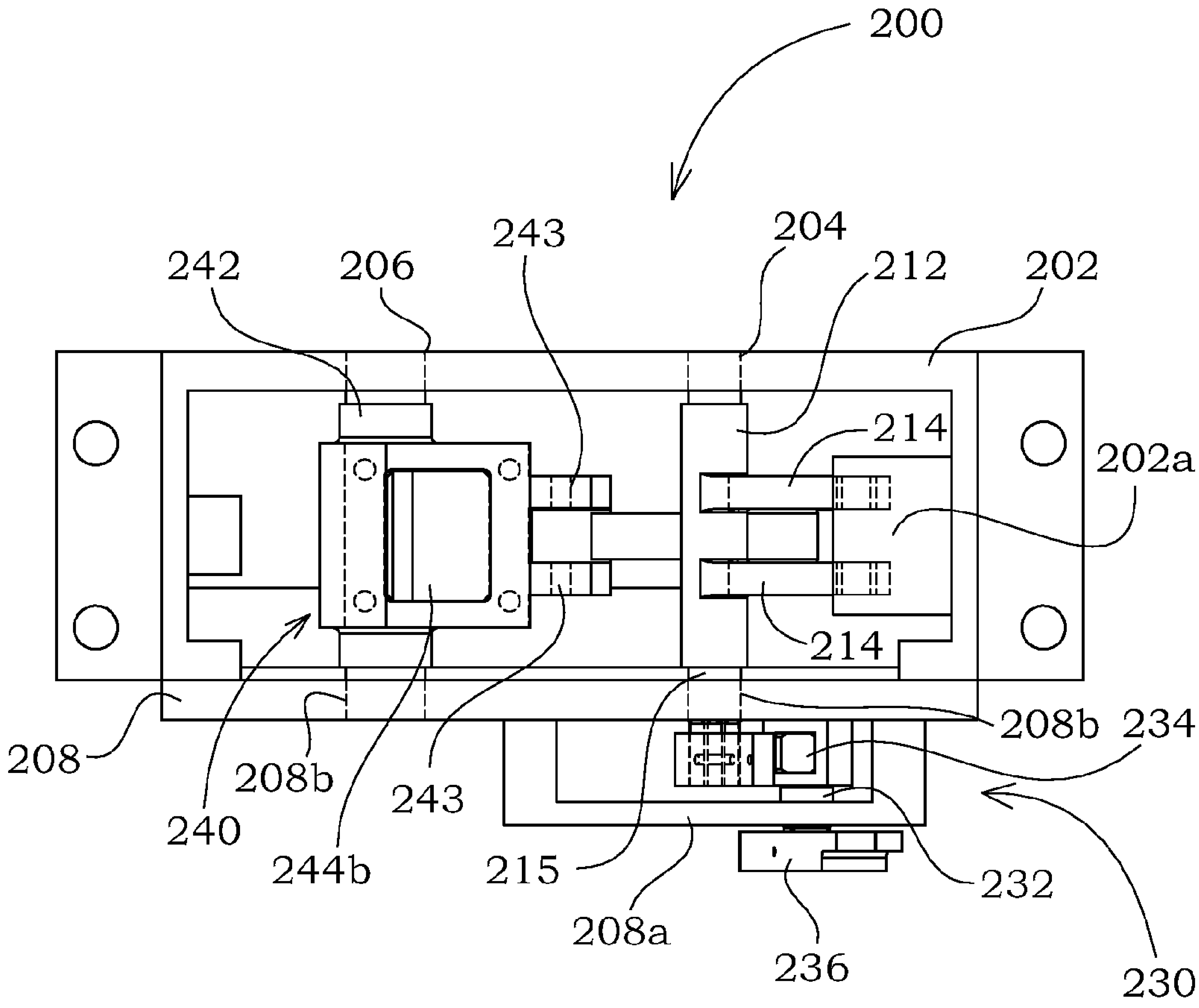
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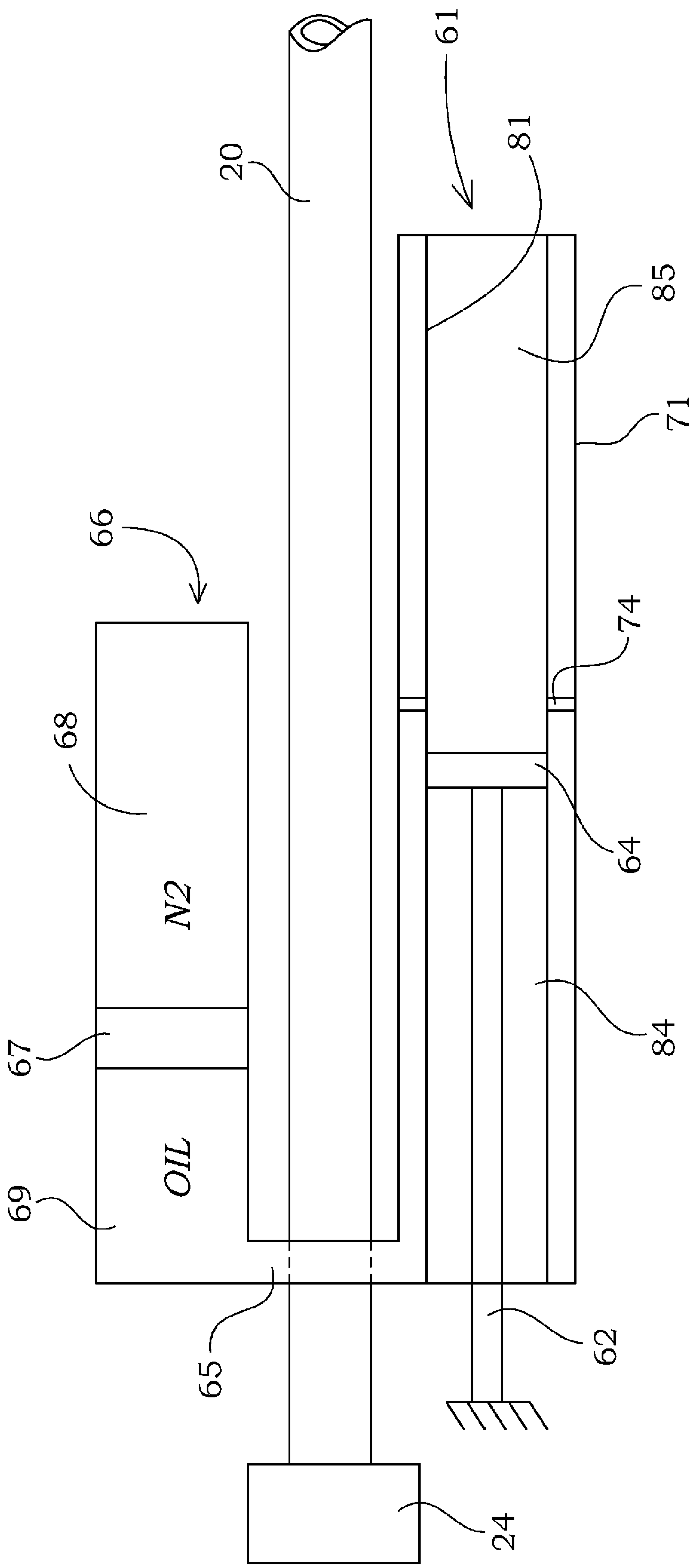
FIG. 18C

FIG. 19



SOFT RECOIL SYSTEM

CROSS REFERENCE TO RELATED APPLICATIONS

This application claims priority from and is a continuation of U.S. patent application Ser. No. 13/903,650 filed on May 28, 2013, now U.S. Pat. No. 9,115,946, which application claimed priority from and was a continuation of U.S. patent application Ser. No. 13/452,674 filed on Apr. 20, 2012, now U.S. Pat. No. 8,468,928, which application claimed the filing benefit under 35 U.S.C. §119(e) of provisional U.S. Pat. App. Ser. No. 61/478,053 filed on Apr. 21, 2011, both of which are incorporated by reference herein in their entireties.

FIELD OF INVENTION

This invention relates generally to recoil systems for weaponry.

STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

N/A

REFERENCE TO SEQUENCE LISTING, A TABLE, OR A COMPUTER PROGRAM LISTING COMPACT DISK APPENDIX

Not Applicable

BACKGROUND OF THE INVENTION

Artillery weapons have been used for hundreds of years. These weapons have been continuously developed to improve accuracy, effectiveness, and efficiency. For example, U.S. Pat. Nos. 4,945,813; 6,024,007; and 6,595,103 disclose various designs for gun systems, all of which patents are incorporated by reference herein in their entireties.

When an artillery weapon is fired, the energy of the round must be absorbed by the weapon's structure and eventually transmitted to the ground. Modern artillery systems incorporate recoil mechanisms to modulate the forces associated with these firings to a level that can be effectively and reliably supported by the structure. With some recoil mechanisms, the energy of the round is dissipated by throttling fluid over the length of the recoil. The minimum level of this modulating force is directly proportional to the length of recoil.

In a soft recoil system, the recoiling parts are accelerated forward prior to the firing of the round by an internal gas spring. When the round is fired, nearly half of the energy of the round is used to stop the forward motion of the recoiling parts and the remaining energy is used to force the recoiling parts rearward, recompressing the gas spring. The recoiling parts are then captured by a latch in preparation for the next firing. This use of momentum exchange and energy conservation by the soft recoil technique results in recoil force reductions as high as 75% when compared to conventional recoil systems.

Although the soft recoil technique offers considerable advantages, there are some drawbacks associated with the cycle. Among these are: (1) A different run-up velocity is required for each of the different zones/charges being fired to maximize the benefits, (2) If the round fails to fire during the run up (known as a misfire), the buffing load required to bring the forward velocity of the recoiling parts to zero may be high enough to cause some weapon instability, and (3) If the round fires prematurely from the latch position (known as a "cookoff"), the conventional recoil-style buffer rearward of the latch point may induce sufficient forces to cause the weapon to slide rearward or become unstable.

BRIEF DESCRIPTION OF THE DRAWINGS

In order that the advantages of the invention will be readily understood, a more particular description of the invention briefly described above will be rendered by reference to specific embodiments illustrated in the appended drawings. Understanding that these drawings depict only typical embodiments of the invention and are not therefore to be considered limited of its scope, the invention will be described and explained with additional specificity and detail through the use of the accompanying drawings.

FIG. **1** is a perspective view of a first embodiment of a gun with a soft recoil system engaged therewith, wherein the gun is mounted to a base.

FIG. **2** is a perspective view of the gun of FIG. **1** wherein various elements of the soft recoil system and base have been removed for clarity.

FIG. **3** is a perspective view of the embodiment of a soft recoil system shown in FIG. **1**.

FIG. **4** is a cross-sectional view of the embodiment of a soft recoil system shown in FIG. **1** along a recoil cylinder.

FIG. **5** is a detailed view of a portion of FIG. **4** adjacent the check valve.

FIG. **5**A is a detailed perspective view of one embodiment of a check valve that may be used with a soft recoil system.

FIG. **6** is a cross-sectional schematic view of a recuperator and recoil cylinder showing the internal details of the embodiment of a soft recoil system shown in FIG. **1** when the gun is in the latched position.

FIG. **7** is a cross-sectional schematic view of the recuperator and recoil cylinder of FIG. **6** when the gun is in the run-up phase.

FIG. **8**A is a cross-sectional schematic view of the recuperator and recoil cylinder of FIG. **6** when the gun is in the beginning of the recoil phase.

FIG. **8**B is a cross-sectional schematic view of the recuperator and recoil cylinder of FIG. **6** when the gun is in the recoil phase.

FIG. **9** is a cross-sectional schematic view of the recuperator and recoil cylinder of FIG. **6** when the gun is in the counter-recoil phase.

FIG. **10** is a cross-sectional schematic view of the recuperator and recoil cylinder of FIG. **6** when the gun is in the misfire buffing phase.

FIG. **11**A is a perspective view of the embodiment of a check valve shown in FIG. **5**A, wherein the check valve is shown relative to a portion of the inner cylinder, and wherein the check valve is positioned to abut the stop partition.

FIG. **11**B is a perspective view of the embodiment of a check valve shown in FIG. **5**A, wherein the check valve is shown relative to a portion of the inner cylinder, and wherein the check valve is positioned to abut the stop element.

FIG. **12** is a top view of the illustrative embodiment of a soft recoil system wherein one of the outer cylinders of a recoil cylinder has been removed to show one configuration of an inner cylinder and various fluid passages.

FIG. **13**A is a detailed view of the illustrative embodiment of the soft recoil system at one recoil cylinder adjacent the partition wherein the outer cylinder and check valve have been removed.

FIG. **13**B is a detailed view of the illustrative embodiment of the soft recoil system at one recoil cylinder adjacent the partition wherein the outer cylinder, check valve, and inner cylinder have been removed.

FIG. **14** is a perspective view of the illustrative embodiment of the soft recoil system and latch mechanism.

FIG. **14**A is a cross-sectional view of how one embodiment of a latch mechanism interfaces with the recoiling parts via a latch point formed in the forward yoke, wherein the latch mechanism is retaining the recoiling parts.

FIG. **14**B is a cross-sectional view of how one embodiment of a latch mechanism interfaces with the recoiling parts via a latch point formed in the forward yoke, wherein the latch mechanism is positioned to release the recoiling parts.

FIG. **14**C is a cross-sectional view of how one embodiment of a latch mechanism interfaces with the recoiling parts via a latch point formed in the forward yoke, wherein the latch point is depressing the plunger.

FIG. **15**A is a longitudinal cross-sectional view of one embodiment of misfire recovery system during the misfire buffering phase, which misfire recovery system may be used with the soft recoil system.

FIG. **15**B is another cross-sectional view of the embodiment of a misfire recovery system shown in FIG. **15**A during the recoil phase.

FIG. **16**A is a perspective view of one embodiment of an inner cylinder outfitted with one embodiment of a counter-recoil control system.

FIG. **16**B is a radial cross-sectional view of the embodiment of the counter-recoil control system shown in FIG. **16**A.

FIG. **17**A is a perspective view of one embodiment of the internal elements of a latch mechanism that may be used with a soft recoil system wherein the latch mechanism is positioned to retain the recoiling parts.

FIG. **17**B is a perspective view of one embodiment of the internal elements of a latch mechanism that may be used with a soft recoil system wherein the latch mechanism is positioned to release the recoiling parts.

FIG. **18**A is a cross-sectional view of the embodiment of the internal elements of the latch mechanism shown in FIG. **17** mounted to a housing, wherein the latch mechanism is positioned to retain the recoiling parts.

FIG. **18**B is a cross-sectional view of the embodiment of the internal elements of the latch mechanism shown in FIG. **17** mounted to a housing, wherein the latch mechanism is positioned to release the recoiling parts.

FIG. **18**C is a top view of the embodiment of the internal elements of the latch mechanism shown in FIG. **17** mounted to a housing, wherein the latch mechanism is positioned to retain the recoiling parts.

FIG. **19** is a cross-sectional, schematic view of a gun cooperatively engaged with another embodiment of a soft recoil system.

ELEMENT DESCRIPTION	ELEMENT #
Soft recoil system	10
Gun	12
Base	14
Actuator	16
Barrel	20

-continued

ELEMENT DESCRIPTION	ELEMENT #
Breech	24
First rail	28
Second rail	30
Rear yoke	32
Middle yoke	34
Forward yoke	36
Latch point	36a
Muzzle yoke	38
Flange	39
Tie rod	40
First rail guide	50
First recoil cylinder	51
First recoil rod	52
First forward end	53
First recuperator	56
Mounting bracket	57
Crossover bracket	59
Second rail guide	60
Second recoil cylinder	61
Second recoil rod	62
Second forward end	63
Recoil piston	64
Lubricant groove	64a
Transfer manifold	65
Second recuperator	66
Floating piston	67
First recuperator chamber	68
Second recuperator chamber	69
Outer cylinder	71
End seal	72
Partition	74
Port	75
Forward outer chamber	77
Rear outer chamber	78
Inner cylinder	81
Stuffing box	82
Stop element	83
Forward inner chamber	84
Rear inner chamber	85
First fluid passage	87
Second fluid passage	88
Third fluid passage	89
Fourth fluid passage	90
Fifth fluid passage	92
Larger fluid passage	93
Sixth fluid passage	94
Check valve	100
Check valve fluid passage	101
Flange portion	102
Sleeve portion	103
First collar portion	104
Finger portion	105
Intermediate collar portion	106
Peripheral collar portion	108
Relief fluid passage	108a
Counter-recoil control system	110
Counter-recoil control valve	112
Control valve pivot point	114
Misfire recovery system	130
Misfire valve	132
Misfire valve flange	132a
Misfire valve sleeve	132b
Misfire valve fluid passage	132c
First barrier	134
Second barrier	136
Latch mechanism	200
Housing	202
Stop wall	202a
Crank aperture	204
Latch assembly aperture	206
Housing cover	208
Trip assembly bracket	208a
Cover aperture	208b
Crank	210
Crank mount	212
Lever member	213
Crank arm	214

-continued

ELEMENT DESCRIPTION	ELEMENT #
Rotational biasing member	215
Link	220
Link first end	222
Link second end	224
Trip assembly	230
Trip mount	232
Lever member engager	234
Bar	236
Latch assembly	240
Latch body	241
Latch assembly mount	242
Link connector	243
Plunger	244
Plunger face	244a
Plunger ramp	244b
Biasing member	245

DESCRIPTION OF THE ILLUSTRATIVE EMBODIMENTS

Before the various embodiments of the present invention are explained in detail, it is to be understood that the invention is not limited in its application to the details of construction and the arrangements of components set forth in the following description or illustrated in the drawings.

The invention is capable of other embodiments and of being practiced or of being carried out in various ways. Also, it is to be understood that phraseology and terminology used herein with reference to device or element orientation (such as, for example, terms like "front", "back", "up", "down", "top", "bottom", and the like) are only used to simplify description of the present invention, and do not alone indicate or imply that the device or element referred to must have a particular orientation. In addition, terms such as "first", "second", and "third" are used herein and in the appended claims for purposes of description and are not intended to indicate or imply relative importance or significance. The term "recoiling parts" as used herein generally refers to those elements of a piece of a gun **12** and/or a soft recoil system **10** that move in response to the energy of expending a round in the gun **12**. This term may encompass, but is not limited to, the barrel **20**, muzzle brake, breech **24**, first rail **28**, second rail **30**, rear yoke **32**, middle yoke **34**, forward yoke **36**, muzzle yoke **38**, flange **39**, tie rod **40**, first recoil rod **52**, second recoil rod **62**, and recoil piston **64** (although the recoil rods **52**, **62** and recoil piston **64** may also be considered as part of the soft recoil system **10**).

One embodiment of an artillery weapon, such as a howitzer (or more generally, gun **12**), may be mounted to a base **14** and include a soft recoil system **10** as shown in FIG. **1**. The base **14** may be rotatable with respect to the structure to which it is mounted to allow a user to change the orientation of the gun **12**. The actuator **16** may be cooperatively engaged at a first end thereof with the base **14** and at a second end thereof with a portion of the gun **12** to adjust the vertical angle of the gun **12** with respect to the base **14**. Other structures and/or methods may be used to change the orientation of the gun **12** without limitation, and will not be discussed further herein for purposes of brevity. The soft recoil system **10** may be mounted in any manner suitable for the use for which the gun **12** is designed. Such mountings include but are not limited to vehicle mounts, chassis mounts, and skid mounts.

A gun **12** without a soft recoil system **10** and removed from a base **14** is shown in FIG. **2**. The gun **12** generally includes an elongated, hollow barrel **20** through which a shell/cartridge/round is fired. The barrel **20** may include a muzzle brake (not shown) at its forward end, and a breech **24** at its rearward end. Rails or channels **28**, **30** may be positioned on opposite sides of the barrel **20** and extend parallel to the longitudinal axis of the barrel **20**.

The rails may be firmly retained in place by a plurality of yokes **32**, **34**, **36**; a first or rear yoke **32**, a second or middle yoke **34**, and a third or forward yoke **36** attached to an intermediate portion of the barrel **20**. The yokes **32**, **34**, **36** circumferentially clasp or are secured to the barrel **20** at positions along its longitudinal axis. The forward yoke **36** may include a latch point **36*a*** to provide an interface between the recoiling parts and the latch mechanism **200**, which is described in detail below.

In addition, a muzzle yoke **38** may circumferentially clasp an intermediate portion of the barrel **20** at a position that is spaced from and forward of the third yoke **36**. The muzzle yoke **38** may be configured to include a pair of opposed end portions or flanges **39**, which extend generally transverse to the longitudinal axis of the barrel **20** as shown in FIG. **2**. Each flange **39** may be formed with a cylindrical-shaped bore or passage formed therein, wherein the central axes of the passages may extend generally parallel to the longitudinal axis of the barrel **20**. At least one tie rod **40**, two of which are shown in FIG. **2**, may be disposed on opposite sides of the barrel **20**. Each tie rod **40** may extend through aligned apertures in yoke **32**, **34**, and/or **36** and flanges **39** of muzzle yoke **38**. The tie rods **40** may be retained in position by a suitable attaching member, such as a lock nut, welding, or other structures and/or methods suitable to the particular embodiment of the gun **12**. In the illustrative embodiment of the soft recoil system **10**, two tie rods **40** are simultaneously engaged with the forward yoke **36** and the muzzle yoke **38**. However, the soft recoil system **10** may include tie rods **40** engaging other and/or additional yokes **32**, **34**, **36**, and **38** without limitation. Alternatively, muzzle yoke **38** may be mounted directly to barrel **20** without tie rods **40**.

FIG. **3** provides a perspective view a soft recoil system **10** having a cradle configuration for use with the embodiment of a gun **12** shown of FIG. **2**. To provide recoil control, the illustrative embodiment of the soft recoil system **10** is formed with two hydro-pneumatic systems that are essentially mirror images of one another about a vertical plane longitudinally bisecting the soft recoil system **10**. The illustrative embodiment of a soft recoil system **10** includes pair of elongate recoil cylinders **51**, **61**, which have longitudinal axes that are generally parallel to each other. The recoil cylinders **51**, **61** are supported in a spaced-apart configuration by a crossover bracket **59** on the top side and a mounting bracket **57** on the bottom side. In one embodiment of a soft recoil system **10** when compared to the prior art, the soft recoil system **10** increases the window of velocities that may be successfully fired for a particular zone/charge, decreases the maximum velocity necessary to successfully fire the top charge (thereby reducing the misfire forces), and provides throttling capability over the entire stroke length (thereby reducing overload forces).

Each recoil cylinder **51**, **61** may be hydro-pneumatically linked to an associated gas reservoir or recuperator **56**, **66** through a fluid transfer manifold, wherein only fluid transfer manifold **65** for the second recoil cylinder **61** and recuperator **66** is shown in FIG. **3**. A first and second rail guide **50**, **60** may be affixed to opposed inner surfaces of the first and second recoil cylinders **51**, **61**, respectively. The rail guides **50**, **60** may be configured to be respectively slideably engaged with the rails **28**, **30** affixed to the barrel **20** as shown in FIG. **2**. This allows the recoiling parts to move linearly with respect to the non-recoiling parts along the rails **28**, **30** and rail guides **50**, **60**. The crossover bracket **59**, which is designed to straddle the barrel **20**, may include an underside surface configured to mate with the curved upper surface of the barrel **20**.

In another embodiment of a soft recoil system **10**, only a single recoil cylinder **61** and recuperator **66** are used. In this embodiment, the recoil cylinder **61** and recuperator **66** may be positioned parallel with respect to the barrel **20** of the gun **12** to which the soft recoil system **10** is cooperatively engaged. It is contemplated that in such an embodiment of a soft recoil system **10** it will be especially advantageous to position the recoil cylinder **61** and/or recuperator **66** either directly above or directly below the barrel **20** such that a vertical plan will bisect the barrel **20**, recoil cylinder **61**, and recuperator **66**. However, other configurations and/or orientations may be used without limitation.

The soft recoil system **10** may include a pair of recoil rods **52**, **62**, which may be positioned within and extend from the forward ends of the recoil cylinders **51**, **61**. When the soft recoil system **10** is fitted onto the gun **12** of FIG. **1**, the forward ends **53**, **63** of the recoil rods **52**, **62** are fitted into the apertures formed in the flanges **39** of the muzzle yoke **38**. In the illustrative embodiment of the soft recoil system **10**, the recoil rods are pneumatically/hydraulically driven, as described in detail below.

FIG. **4** shows a cross-sectional view of the soft recoil system **10** along the longitudinal axis of the recuperators **56**, **66** and recoil cylinders **51**, **61**. FIG. **5** provides a detailed cross-sectional view of a recoil cylinder **51**, **61** in the area of the partition **74**. Referring now to FIG. **6**, which provides a schematic representation of the portion of a recoil cylinder **51**, **61** shown in FIG. **5**, a recuperator **56**, **66**, and a transfer manifold **65**.

For brevity, the following description regarding the internal function, configuration, and/or components of the soft recoil system **10** depicted in FIGS. **6-10** will refer to the second recoil cylinder **61** and associated elements positioned on the corresponding side of the gun **12**. However, it is to be understood that the general function, configuration, and/or components of the first recoil cylinder **51** and associated elements positioned on the corresponding side of the gun **12** is similar to that of the second recoil cylinder **61** and associated elements. In FIGS. **6-10**, the arrows are meant to depict fluid flows at various phases of operation of one soft recoil system **10** in accordance with the present disclosure.

In FIG. **6**, the second recoil cylinder **61** and the associated recoil rod **62** are in fluid communication with the fluid transfer manifold **65**, which is in turn in fluid communication with the second recuperator **66**. The recuperators **56**, **66** in the illustrative embodiment of the soft recoil system **10** are formed with a floating piston **67** therein. The second recoil cylinder **61** may include an outer cylinder **71**, a circular end seal **72**, a circular partition **74**, and a cylindrical inner cylinder **81** that is partially supported within the outer cylinder **71** by the end seal **72** and the partition **74**. In the illustrative embodiment shown in FIGS. **1**, **3**, **4**, & **5** the outer diameter of the inner cylinder **81** may be approximately 50% that of the outer diameter of the outer cylinder **71**. However, in other embodiments of the soft recoil system **10** the relative sizes of the cylinders **71**, **81** and the thicknesses of the walls thereof will vary without limitation depending on the specific embodiment of the soft recoil system **10**.

Still referring to FIG. **6**, a first or forward outer chamber **77** is defined by the outer and inner cylinders **71**, **81** and the partition **74**. A second or rearward outer chamber **77** is defined by the outer and inner cylinders **71**, **81** and a partition **74**, which is circular in the illustrative embodiment. The partition **74** includes ports **75** that allow fluid flow between forward and rear outer chambers **77**, **78**. A recoil piston **64**, which may be cylindrical in shape, may be positioned within the inner cylinder **81** and moveable along the length of the inner cylinder. The recoil piston **64** may be connected to the rear end portion of the recoil rod **62**.

A stuffing box **82**, which may be configured to encircle the recoil rod **62**, may be secured to the end seal **72** to form a fluid bearing and seal element for the reciprocating recoil rod **62**. The recoil piston **64** separates the interior chamber defined by the inner cylinder **81** into a forward inner chamber **84** and rear inner chamber **85**. The tolerances between the recoil piston **64** and the inner cylinder **81** are selected such that a predetermined amount of fluid flow or leakage may occur at the space or interface between the sidewalls of the recoil piston **64** and inner cylinder **81** under certain circumstances. It is contemplated that for most embodiments of the soft recoil system **10** any leakage between the recoil piston **64** and the inner cylinder **81** will be a relatively low volumetric amount compared to that of fluid flowing directly from the forward inner chamber **84** to the rear inner chamber **85** and vice-versa. As shown in FIG. **5**, one embodiment of a recoil piston **64** is formed with a plurality of annular lubricant grooves **64*a*** on the periphery thereof. These lubricant grooves **64*a*** allow for a pressure differential across the length of the recoil piston **64** and provide a reservoir for oil to reduce friction between the recoil piston **64** and interior wall of the inner cylinder **81**. The precise number, configuration, and/or orientation of the recoil piston **64** and/or lubricant grooves **64*a*** will vary from one embodiment of the soft recoil system **10** to the next and are therefore in no way limited to the scope of the soft recoil system **10** as disclosed and claimed herein.

The inner cylinder **81** includes a plurality of fluid passages **87**, **88**, **89**, and **90** (first, second, third, and fourth fluid passages, respectively) spaced along the length thereof on the forward or muzzle side of the partition **74**. The inner cylinder **81** also includes a plurality of fluid passages **92** rearward of the partition **74**. These fifth fluid passages **92** allow the transfer of fluid directly between the rear inner chamber **85** and rear outer chamber **78**, which as shown in FIG. **6** are oriented to the left or rearward of the recoil piston **64** and partition **74**.

Still in general reference to FIG. **6**, the inner cylinder **81** also includes sixth fluid passages **94**, which are larger than the fluid passages **87**, **88**, **89**, **90** and **92**. The fluid passages **94** are located near the partition **74** on the forward (i.e., to the right) side of the recoil cylinder **51**, **61**. A check valve **100** may be positioned to surround the inner cylinder **81** and may be configured to have a right-angle cross-section, a first embodiment of which is shown in cross-section in FIGS. **6-10**. The check valve **100** may include a flange portion **102** for blocking aperture **75** in partition **74** when the check valve **100** is located in a first operative position. Check valve **100** may also include a sleeve portion **103** that surrounds the inner cylinder **81** for selectively obstructing fluid flow through the sixth fluid passage **94**. In a first operative position shown in FIG. **6**, the check valve fluid passages **101** in the sleeve portion **103** are in fluid communication with the sixth fluid passages **94** in the cylindrical inner sleeve **81**. In a second operative position shown in FIG. **8**B the check valve **100** moves to the right toward the front end of the recoil cylinder to engage stop element **83**, thereby obstructing fourth and sixth fluid passages **90**, **94** and not obstructing port **75** in partition **74**.

FIG. **5**A shows a perspective view of a second embodiment of a check valve **100**, and FIG. **5** provides a cross-sectional view thereof in relation to the partition **74** and adjacent elements of the recoil cylinder **51**, **61**. The second embodiment of a check valve **100** in a position such that it abuts partition **74** is shown in FIG. **11**A, and such that it abuts the stop element **83** is shown in FIG. **11**B. The second embodiment of a check valve **100** includes a flange portion **102** and a sleeve portion **103**. The sleeve portion **103** comprises a first collar portion **104** joined **104** to the flange portion **102**. Circumferentially spaced finger portions **105** project from the first collar portion **104** and extend to a peripheral collar portion **108**, wherein an intermediate collar portion **106** is positioned between the first and peripheral collar portions **104**, **108**, all of which collar portions **104**, **106**, **108** may be joined to the finger portions **105**. The first collar portion **104**, finger portions **105**, and intermediate and peripheral collar portions **108** define check valve fluid passages **101** therebetween.

The width of the collar portions **104**, **106**, **108** and length of the finger portions **105** may be selected so that the sixth fluid passages **94** in the inner cylinder **81** will be exposed when the check valve **100** is in a first operative position (as shown in FIG. **6** for the first embodiment of a check valve **100**), partially exposed when in an intermediate operative position (as shown in FIG. **8**A for the first embodiment of a check valve **100**), and fully obstructed when in a second operative position (as shown in FIG. **8**B, wherein the distal end of the sleeve portion **103** abuts the stop element **83**) for the first embodiment of a check valve **100**.

In the second embodiment of a check valve **100**, the peripheral collar portion **108** may include a relief fluid passage **108*a***. In the illustrative embodiment of the soft recoil system **10**, when the second embodiment of a check valve **100** is in the second operative position, the relief fluid passage **108*a*** is aligned with the third fluid passage **89** (see FIG. **5**) and a check valve fluid passage **101** is aligned with the fourth fluid passage **90**. This configuration allows the third and fourth fluid passages **89**, **90** to be available for fluid throttling even when the check valve **100** is in the second operative position (i.e., the position shown in FIG. **8**B). Other embodiments of the soft recoil system **10** will require check valves **100** configured differently than the embodiments thereof pictured and described herein. Accordingly, the specific configuration, orientation, and/or function of the check valve **100** in no way limits the scope of the soft recoil system **10** as disclosed and claim herein.

As shown in FIGS. **6-10**, the recuperator **66** in the illustrative embodiment of the soft recoil system **10** comprises an elongate hollow cylinder containing a floating piston **67** that divides the cylinder into separate first and second recuperator chambers **68**, **69**. Liquid, vapor, or gas may be positioned in either recuperator chamber **68**, **69**. It is contemplated that the first recuperator chamber **68** will be filled with nitrogen or another compressible gas capable of acting as a fluid spring in conjunction with the floating piston **67**. It is also contemplated that the second recuperator chamber **69** will be filled with an inert oil of sufficient lubriciousness for the particular embodiment of the soft recoil system **10**. The second recuperator chamber is in fluid communication with the fluid transfer manifold **65** and forward outer chamber **77**. The fluid in the recoil cylinder **61**, first recuperator chamber **68**, and/or second recuperator chamber **69** may serve as an energy storage and/or transfer media.

FIGS. **6-10** show different operative steps (sometimes referred to herein as "phases") in the firing of a gun **12** outfitted with the illustrative embodiment of the soft recoil system **10**. The "latched position" of FIG. **6** shows the position of the second recoil rod **62** and second recoil piston **64** relative to inner cylinder **81** and the partition **74**. Since both recoil rods **52**, **62** move together in unison or mirror each other in the illustrative embodiment of the soft recoil system **10** as previously described, the movement of the recoil rods **52**, **62** will be explained in terms of the second recoil rod **62**. The recoiling parts of the soft recoil system **10** are held in this "equilibrium" or "in battery" position by a latch mechanism **200**, partially shown in FIG. **1**, until the gun **12** is ready for firing.

When the external latch mechanism **200** is released, the unbalanced force of the gas pressure in fluid chamber **68** acts upon the floating piston **67** to move the floating piston **67** to the right and to force the fluid out of chamber **69** and into the first or forward outer chamber **77**, as generally depicted in FIG. **7**. The pressurized fluid then begins to flow into the forward inner chamber **84** through the fluid passages **87**, **88**, **89**, **90**, and **94**. Additionally, leakage may occur between the recoil piston **64** and the walls of the inner cylinder **81** such that a certain amount of fluid passes directly from forward inner chamber **84** to rear inner chamber **85**. However, as previously described, it is contemplated that in most embodiments of the soft recoil system **10** this leakage will be relatively small compared to the fluid flow through passages **87**, **88**, **89**, **90**, and **94**. This same action occurs simultaneously in the first recoil cylinder **51**.

As a result of this leakage and the force differential on the opposite axial surfaces of the recoil piston **64**, the recoil piston **64** and the recoil rod **62** are caused to move to the right with respect to the recoil cylinder **61**, as shown in FIG. **7**. The force differential is a result of the area differential between the front and back axial surfaces of the recoil piston **64**. Because the muzzle yoke **38** is connected to the recoil rods **52** and **62**, the attached recoiling parts are also accelerated forward (i.e., to the right in FIG. **7**). As the recoil piston **64** continues to move to the right in FIG. **7**, it passes sixth and fourth fluid passages **94**, **90** so that fluid in forward outer chamber **77** can now flow directly into the expanding rear inner chamber **85** through the sixth and fourth fluid passages **94**, **90**. Partition passage **75** is kept closed by check valve **100** during this forward acceleration phase or "run-up" phase. The sixth fluid passages **94**, which are located just to the rear of the fourth fluid passages **90**, may be sized to minimize pressure drops from forward outer chamber **77** to rear inner chamber **85** during the run-up phase.

The "recoil" phase (shown at the beginning of the phase in FIG. **8**A and later in the phase in FIG. **8**B) begins with the firing of the cartridge during the "run-up" phase. The firing of the cartridge actually occurs at a predetermined position forward of the "latched" or "in battery" position. Part of the energy of the cartridge stops the forward acceleration/momentum of the recoiling parts of the soft recoil system **10** and the remaining energy of the cartridge forces the recoiling parts to begin to accelerate rearward or to recoil. With the recoil phase of FIGS. **8**A & **8**B, recoil rod **62** and recoil piston **64** are forced back into the inner cylindrical **81** (i.e., to the left). As a result, the fluid inside rear inner chamber **85** is forced out of the rear inner chamber **85** through fluid passages **90**, **94**, and **92**. These fluid passages **90**, **94**, and **92** function as throttling orifices wherein the throttling area decreases as the recoil piston **64** moves further and further into the inner cylinder **81**, (i.e., to the right in FIGS. **8**A & **8**B). It is this net force acting on recoil piston **64** that helps to slow and eventually stop the rearward movement of the recoiling parts. While fluid flows through fluid passages **90**, **94**, and **92** the portion flowing out of apertures **92** and into the rear outer chamber **78** causes the pressure in the rear outer chamber **78** to increase until it exceeds the pressure in the forward outer chamber **77**. At this point, fluid pressure differentials on check valve **100** cause it to move forward (the start of which is shown in FIG. **8**A), thereby opening port **75** so that fluid is allowed to flow from the rear outer chamber **78** directly to the forward outer chamber **77** through passage **75** (as shown in FIG. **8**B, wherein the check valve **100** abuts the stop element).

When the check valve **100** does move (i.e., to the right in FIGS. **8**A & **8**B), it effectively closes off sixth fluid passages **94**, thus allowing fluid to flow out of the inner cylinder **81** only through the fourth and fifth fluid passages **90**, **92** to the rear of recoil piston **64**. The rising pressure causes the fluid displaced by recoil piston **64** to flow back through the transfer manifold **65** into the recuperator **66** where it acts upon the floating piston **67** to recompresses the fluid in the first recuperator chamber **68**. This process continues until all the energy of recoil has been absorbed. When this occurs, recoil piston **64** will be to the left or rear of the partition **74**, as shown in FIG. **9**.

The sixth fluid passage **94** may be sized to provide sufficient flow area so that the velocity of the recoiling parts during the run-up phase is only slightly affected by the pressure drop across the sixth fluid passage **94**. As shown in FIG. **12** (which provides a top view of a first embodiment of an inner cylinder **81**), it is contemplated that for the illustrative embodiment of the soft recoil system **10**, the sixth fluid passage **94** will have a larger cross-sectional area than the fluid passages **87**, **88**, **89**, **90**, and **92**. It may also be sized and positioned so that check valve **100** may open and close the sixth fluid passage **94** when the check valve **100** slides rearward and forward along the inner cylinder **81**, respectively. Furthermore, although only seven fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94** are called out and discussed for purposes of clarity and brevity, as is clear from FIG. **12** the inner cylinder may include more than seven fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94**. Additionally, the various fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94** may have different or the same cross-sectional areas as adjacent and/or non-adjacent fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94**. Accordingly, the configuration, orientation, and/or specific function of the fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94** shown herein is in no way limiting to the scope of the soft recoil system **10** as disclosed and claimed herein.

Port **75** may be sized to provide sufficient cross-sectional area for fluid flow through partition **74** so that fluid flowing from the rear outer chamber **78** to the forward outer chamber **77** may pass through the partition **74** with minimal pressure drop when check valve **100** is pushed away from the partition **74**. Port **75** may also be positioned and sized so that it may be closed to fluid flow when the check valve **100** is in its rearward position (i.e., abutting the partition **74**).

The "counter-recoil" phase, which is depicted schematically in FIG. **9**, begins when the increasing gas pressure in the first recuperator chamber **68** stops further movement of the floating piston **67**. At this point the gas pressure in the first recuperator chamber **68** begins to force fluid out of the second recuperator chamber **69** through the transfer manifold **65** into the forward outer chamber **77** (as happens during the run-up phase). As this fluid flow continues, a pressure difference develops between the forward outer chamber **77** and the rear outer chamber **78** that causes the check valve **100** to move rearward and close off port **75**. The resultant force acting on the recoil piston **64** eventually causes the recoil piston **64** and recoil rod **62** to move forward (i.e., to the right). With port **75** closed to fluid flow, the fluid flows from the forward outer chamber **77** into the forward inner chamber **84** through fluid passages **87**, **88**, **89**, and **90**. The fluid may then flow from the forward inner chamber **84** through fifth fluid passages **92** into the rear outer chamber **78**, and from the rear outer chamber **78** to the rear inner chamber **85**, as best shown in FIG. **9**.

The greater surface area on the rear axial surface of the recoil piston **64** compared to the front axial surface thereof and the fluid flow into the rear inner chamber **85** causes the recoil piston **64** to move forward, (i.e., to the right). As the recoil piston **64** moves forward in the inner cylinder **81**, the gas pressure in the first recuperator chamber **68** begins to drop. Also, as the forward edge of recoil piston **64** reaches the position of the partition **74**, the resulting pressure differential and the velocity of the recoiling parts may be controlled by the leakage of fluid at the interface between the recoil piston **64** and the inner cylinder **81**, by the position of fluid passages **92** with respect to adjacent fluid passages **92** and the partition **74**, and/or through a combination thereof. The resulting reduced velocity of the recoiling parts continues until the recoiling parts reach and make contact with the external latch **200** (i.e., when the recoil piston **64** is adjacent the partition **74**). This completes a cycle.

A "misfire buffing" phase may be provided in the event that the round fails to fire during the run-up phase, as depicted in FIG. **10**. The energy or momentum contained in the recoiling parts must be dissipated in a controlled manner to prevent possible damage or unwanted weapon instability. This "misfire buffing" process may be completed internally using the interface of recoil piston **64**, recoil rod **62**, inner cylinder **81**, and fluid passages **87**, **88**, **89** and **90** to provide the necessary buffing via fluid throttling. At a point when the recoil piston **64** has moved to a position just short of the third fluid passage **89**, continued movement results in the recoil piston **64** crossing passage **88**. At this point fluid inside of forward inner chamber **84** is pressurized due to the restricted flow path provided by the first fluid passage **87** (i.e., the only path fluid within the forward inner chamber **84** may take to flow into the forward outer chamber **77**). The resulting increase in the pressure in the forward inner chamber **84** causes the velocity of the recoiling parts to slow. The second fluid passages **88** may be positioned just to the rear of the misfire buffing section of inner cylinder **81** and may be sized to provide sufficient cross-sectional area to allow for the free flow of fluid out of cylinder **81** during the run-up phase of operation.

While FIGS. **6**-**10** provide simplified, schematic depictions of the internal workings of one embodiment of a soft recoil system **10**, FIG. **4** provides a cross-sectional view of a field-ready implementation of the principals from FIGS. **6**-**10**. FIG. **5** provides a cross-sectional view about the check valve **100** with the recoil piston in the latched phase of the field-ready implementation. In light of the description related to FIGS. **6**-**10** contained herein, it will be apparent to those of ordinary skill in the art how the principals described with respect to FIGS. **6**-**10** correlate to the embodiment of a soft recoil system **10** shown in FIGS. **1**, **3**, **4**, **5**, and **11**-**13**.

It is contemplated that the general orientation, elevation, and/or azimuth of the gun **12** may have an active control via a PLC and various sensors, wherein the PLC controls a translator of some sort (e.g., base **14**, actuator **16**, and/or a combination thereof). In an active control situation, the PLC would analyze data from the various sensors and output commands to the translator, which translator would adjust the orientation, elevation, and/or azimuth of the gun **12** accordingly.

The various fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94**, outer cylinder **71**, inner cylinder **81**, ports **75**, and the partition **74** are configured such that the force of the spending the round is distributed over a longer distance of the soft recoil system **10** than that of prior art recoil systems. Additionally, the time over which the force is distributed is longer using the soft recoil system **10** than that of the prior art. One profile of the various fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94** and their respective spacing and areas for an inner cylinder **81** are shown in FIG. **12**. In the orientation shown in FIG. **12** the breech is positioned toward the bottom of the figure. Using principles of fluid mechanics for turbulent incompressible fluid flow (which may be accomplished via Bernoulli's equation in various forms) and equations of motion, one may calculate the appropriate values (e.g., fluid passage size, pressure differential, etc.) for a given system. The specific profile, configuration, and/or orientation of the fluid passages **87**, **88**, **89**, **90**, **92**, **93**, and **94** will vary from one embodiment of the soft recoil system **10** to the next. Accordingly, those variables are in no way limiting to the scope of the soft recoil system **10** as disclosed and claimed herein.

As is apparent from FIG. **12**, it is contemplated that the majority of the fluid passages **87**, **88**, **89**, **90**, **92**, and **93** may be positioned along the top of the inner cylinder **81** (i.e., at the 12 o'clock position) for the illustrative embodiment of the soft recoil system **10**. This configuration allows the bottom surface of the recoil piston **64** to have a smooth surface on which to travel. As shown, the sixth fluid passages **94** and larger fluid passages **93** may be circumferentially distributed around the periphery of the inner cylinder **81**. However, any of the fluid passages **87**, **88**, **89**, **90**, **92**, **93**, or **94** may be positioned at any circumferential position around the inner cylinder **81** without limitation. For certain applications it may be especially important to ensure a lubricant layer exists between the exterior of the recoil piston **64** and the interior of the inner cylinder **81** during the recoil phase to minimize any wear caused by shearing forces. Lubricant grooves **64***a* as shown in FIG. **5** may be especially helpful for such situations.

FIGS. **13**A-**13**B provide detailed views of the area of a recoil cylinder **51**, **61** from the first embodiment of a soft recoil system **10** adjacent the partition **74** at various radial positions. In FIGS. **13**A-**13**B, the soft recoil system **10** is oriented so that for a gun **12** engaged with the soft recoil system **10**, the muzzle yoke **38** would be toward the right side of the figures and the breech **24** would be toward the left side of the figures. In FIG. **13**A, the check valve **100** has been removed so that port **75** in the partition **74** is clearly visible. In FIG. **13**B, the inner cylinder **81** has been removed so that the recoil rod **52**, **62** and recoil piston **64** are clearly visible.

In the embodiment of a soft recoil system **10** shown in FIG. **12**, the recoil piston **64** generally travels the length of the inner cylinder **81** between the partition **74** and the larger fluid passage **93** during the "run-up" phase. It is contemplated that this length may be approximately 25 inches, but this distance is in no way limiting to the scope of the soft recoil system **10** as disclosed and claimed herein, and will vary from one embodiment thereof to the next. Once the recoil piston **64** crosses the larger fluid passage **93** and the gun **12** has not yet fired, the soft recoil system **10** is placed in the misfire buffing phase, which is shown schematically in FIG. **10**.

A "coast" length may be engineered into the inner cylinder **81** so that the recoil piston **64** may be in a window of approximately five inches in length (for the illustrative embodiment of the soft recoil system **10**, but which length will vary from one embodiment of the soft recoil system **10** to the next) along the inner cylinder **81** behind (i.e., toward the breech **24**) of larger fluid passages **93**. If the recoil piston **64** is positioned in at a point in the coast length, the gun **12** may fire and the soft recoil system **10** will perform as designed. In the illustrative embodiment of the soft recoil system **10**, the coast length is substantially located in an area between the larger fluid passage **93** and a point five inches rearward therefrom (i.e., toward the breech **24**). However, in other embodiments of the soft recoil system **10** the coast length may be differently positioned along the inner cylinder **81**, and/or the coast length may be longer or shorter than that shown herein. The embodiment shown in FIG. **12** generally allows the recoiling parts to accelerate during the entire run-up phase, although the acceleration may decrease as the recoil piston **64** approaches the coast length. The fluid passages **87**, **88**, **89**, **90**, and **92** positioned on the top side (i.e., 12 o'clock position) of the inner cylinder **81** most often function to throttle fluid exiting the interior cylinder **81**, though at certain times fluid may enter the interior cylinder **81** via those fluid passages **87**, **88**, **89**, **90**, and **92**.

One embodiment of a misfire recovery system **130** is shown in FIGS. **15**A and **15**B. As shown, the misfire recovery system **130** allows a gun **12** engaged with the soft recoil system **10** to be fired in the event of a misfire, without the need to reposition the recoiling parts to the latch position. The misfire recovery system **130** comprises a misfire valve **132** slideably positioned around the exterior of a portion of the inner cylinder **81**. The misfire valve **132** may be slideable between a first barrier **134** and a second barrier **136**. The misfire valve **132** may include a misfire valve flange **132***a* and a misfire valve sleeve **132***b* projecting from the misfire valve flange **132***a*. The misfire valve sleeve **132***b* may be formed with a plurality of misfire valve fluid passages **132***c* therein, as shown in FIGS. **15**A & **15**B.

During the run-up phase, the misfire valve **132** would typically be positioned as shown in FIG. **15**A, wherein the misfire valve sleeve **132***b* abuts the first barrier **134**. In this position, the misfire recovery system **130** generally does not affect the operation of the soft recoil system **10**. That is, the misfire valve **132** does not impede fluid flow between the inner and outer cylinders **81**, **71** during normal operation of the gun **12**. As shown in FIG. **15**A, the misfire valve **132** is positioned such that the larger fluid passage **93** are unrestricted during the run-up phase such that fluid may freely flow through the larger fluid passages **93** from the inner cylinder **81** to the outer cylinder **71**.

However, in the event of misfire, which situation is depicted in FIG. **15**B (i.e., the recoil piston **64** has traveled past the large fluid passages in the direction toward the muzzle yoke **38**), the misfire recovery system **130** allows the user to fire the gun **12** even though all the recoiling parts may be positioned near their forward-most allowable position. When the gun **12** is fired from such a position, the misfire valve **132** slides forward due to the greater force imparter to the rear (i.e., breech side) of the misfire valve **132** such that the misfire valve flange **132***a* abuts the second barrier **136** (as shown in FIG. **15**B). The force differential is a result in the greater surface area on the rear side of the misfire valve **132** than on the front side thereof. When the misfire valve

132 moves forward, it blocks the larger fluid passages **93** so that fluid may only flow from the inner cylinder **81** to the outer cylinder **71** via the smaller fluid passages **87**, **88**, **89**, and **90**. Accordingly, the energy of the expenditure of the round is transferred to the fluid and dissipated through the throttled pumping of the fluid from the inner cylinder **81** to the outer cylinder **71** via fluid passages **87**, **88**, **89**, and **90**. That is, the misfire recovery system **130** allows a soft recoil system **10** to perform like a traditional recoil dissipating system even in the event of misfire, with no additional movement of the recoiling parts required to fire the gun **12** in the event of misfire.

One embodiment of a counter-recoil control system **110** is shown in perspective in FIG. **16**A, and FIG. **16**B shows a radial cross-sectional view of the same embodiment. In the pictured embodiment of counter-recoil control system **110**, the counter-recoil control valves **112** may be configured to control the maximum counter-recoil velocity by limiting the amount of fluid flow that may be used to drive the recoiling parts forward from their maximum recoil position behind latch to the latch position. At the same time the counter-recoil control system **110** has no influence on the performance of the throttling sleeve (i.e., the portion of the inner cylinder **81** between the maximum recoil position behind latch and the latch position) to successfully bring the recoiling parts to a controlled stop.

As shown in FIGS. **16**A & **16**B, the individual counter-recoil control valves **112** are forced outward via a pivoting action (about a counter-recoil control valve pivot point **114**) during recoil by the fluid flowing out of the inner cylinder **81** as the gun recoils (best shown in FIG. **16**B). After the recoiling parts stop adjacent the maximum recoil position behind latch, the recuperators' **56**, **66** force on the fluid causes the fluid to flow back into the inner cylinder **81** through fluid passages **92** positioned rearward with respect to the partition **74**. The fluid flow during this process causes certain counter-recoil control valves **112** to close, thereby covering the fluid passages **92** to the rear of the recoil piston **64**. As the recoil piston **64** moves forward, more counter-recoil control valves **112** close fluid passages **92**. Since fluid passages **92** to the rear of the recoil piston **64** are progressively closed as the recoil piston **64** and other recoiling parts move forward, the number of fluid passages **92** (and thus the flow area available to accelerate the recoiling parts) is limited, which in turn limits the maximum velocity that the recoiling parts may attain before reaching the latch position. Without the use of a counter-recoil system **110**, in certain embodiments of the soft recoil system **10** the peak counter-recoil velocity may become elevated to the point that slowing of the recoiling parts to a stop at latch position will induce higher than desired forward loading on the carriage or other elements of the piece of the gun **12**.

FIG. **19** provides a cross-sectional schematic view of another embodiment of the soft recoil system **10**. The embodiment shown in FIG. **19** works substantially in the same manner as that of the embodiments of the soft recoil system **10** previously described herein. However, in the embodiment shown in FIG. **19**, the recoil cylinder **61** and recuperator **66** may be directly mounted to the gun **12**. The embodiment in FIG. **19** shows the recuperator **66** mounted above the gun **12** and the recoil cylinder **61** mounted below the gun **12**. However, other orientations and/or configurations may be used without departing from the scope of the soft recoil system **10** as disclosed and claimed herein.

In the embodiment of a soft recoil system **10** shown in FIG. **19**, the recoil cylinder **61** and recuperator **66** may move forward and rearward with the gun **12** in response to run-up, recoil, and counter-recoil forces, respectively. The recoil rod **62** may be secured to a cradle (not shown) and/or base **14**. The gun **12**, recoil cylinder **61**, and/or recuperator **66** may be cooperatively engaged with the cradle and/or base **14** such that the gun **12**, recoil cylinder **61**, and/or recuperator **66** may move linearly in response to run-up, recoil, and counter-recoil forces. This cooperative engagement may be accomplished through the use of corresponding rails **28**, **30** and rail guides **50**, **60**, or through any other structure and/or method suitable for the particular application of the soft recoil system **10**.

In operation, the embodiment of a soft recoil system **10** shown in FIG. **19** may be configured such that all components of the gun **12**, recoil cylinder **61**, and recuperator **66** move forward and rearward in response to run-up, recoil, and counter-recoil forces, and the recoil rod **62** and recoil piston **64** remain static. Accordingly, it will be apparent to those skilled in the art that the embodiment of a soft recoil system **10** shown in FIG. **19** operates according to the same principals as the embodiment shown in FIGS. **6-10** as the recoil piston **64** moves linearly within an inner cylinder **81** in both embodiments. However, in the embodiment shown in FIG. **19**, rather than fixing the position of the recoil cylinder **61** and recuperator **66** with respect to the base **14** and varying the position of the recoil rod **62** and recoil piston **64** with respect thereto, the position of the recoil rod **62** and piston **64** is fixed with respect to the base **14** and/or cradle, and the position of the recoil cylinder **61** and recuperator **66** may vary along a predetermined path. Accordingly, the soft recoil system **10** as disclosed and claimed herein is not limited by the absolute positions of the various components thereof. Furthermore, the embodiment shown in FIG. **19** may be employed with first and second recoil cylinders **51**, **61** and first and second recuperators **56**, **66** in a manner similar to that described for the embodiment of the soft recoil system **10** shown in FIGS. **1**, **3**, **4**, & **12**.

It is to be understood that the embodiment of the soft recoil system **10** shown in FIG. **19** may require a modification to the profile of fluid passages **87**, **88**, **89**, **90**, **92**, and **94** as shown for the embodiment pictured in FIGS. **1**, **3**, **4**, & **12**. However, such modification is within the scope of the soft recoil system **10** as disclosed and claimed herein, and in light of the present disclosure will be apparent to a person of ordinary skill in the art.

The latch mechanism **200** may be positioned at any convenient location along the length of the soft recoil system **10** that is suitable for the particular embodiment thereof. In the illustrative embodiment of the soft recoil system **10** pictured herein, the latch mechanism **200** is engaged with the mounting bracket **57**, which is adjacent the forward yoke **36** when the recoiling parts are in the latch position. However, other positions and/or orientations of the latch mechanism **200** may be used with the soft recoil system **10** without limiting the scope thereof.

Generally, the latch mechanism **200** functions to retain the recoiling parts in the latched position (as shown in FIGS. **5** & **6**) prior to the run-up phase, during which the recoiling parts are released and accelerate forward (as shown in FIG. **7**). As previously described herein, when in the latch position, the recoiling parts are possess a certain amount of potential energy from the pressurized fluid in the soft recoil system **10**. Accordingly, the latch mechanism must be robust enough to secure the recoiling parts against the force of this pressurized fluid, yet operate to selectively release the recoiling parts in a manner sufficiently convenient and safe for the user. Furthermore, during the recoil phase the latch mechanism **200** must allow the recoiling parts to pass freely past the latch position (i.e., in a direction from the muzzle yoke **38** to the breech **24**), but stop the recoiling parts at the latch position the end of the counter-recoil phase in preparation for the next cycle.

Various views of one embodiment of a latch mechanism **200** that may be used with a soft recoil system **10** are shown in perspective in FIGS. **17**A & **17**B, wherein the internal elements of the latch mechanism **200** have been removed from a housing **202** for clarity. FIGS. **18**A & **18**B provide cross-sectional views of the embodiment of a latch mechanism **200** shown in FIGS. **17**A & **17**B, and FIG. **18**C provides a top view thereof. The housing **202** pictured herein may be selectively engaged with a housing cover **208**, which has been removed for clarity in FIGS. **17**-**18**B, but which is shown in FIG. **18**C. FIGS. **14**A-**14**C provide a simplified cross-sectional view of how the embodiment of a latch mechanism **200** pictured herein may interface with the recoiling parts of the gun **12** and/or soft recoil system **10** via a latch point **36***a* secured to the forward yoke **36**.

A latch assembly **240** may be pivotally engaged with a housing **202** via a latch assembly aperture **206** formed in the housing **202**, a corresponding cover aperture **208***b* formed in the housing cover **208**, and a latch assembly mount **242** formed in the latch assembly **240**. In the illustrative embodiment of a latch assembly **240** pictured herein the latch assembly mount **242** is generally formed as a tube or rod that fits into the latch assembly aperture **206** and corresponding cover aperture **208***b*. However, the latch mechanism **200** and/or soft recoil system **10** disclosed and claimed herein is not limited by the configuration of the latch assembly aperture **206**, housing cover **208**, and/or the latch assembly mount **242**. The latch assembly **240** may include a latch body **241** that is secured to the latch assembly mount **242**. A link connector **243** (two link connectors **243** are shown in the illustrative embodiment pictured herein) may extend from the latch body **241** to provide a connection point for a link **220** described in detail below.

A plunger **244** may be positioned within a portion of the latch body **241**. The plunger **244** may be selectively moveable in one dimension (i.e., the vertical dimension from the vantage shown in FIGS. **14**A-**14**C, **18**A & **18**B) with respect to the latch body **241**. The plunger **244** may be biased with respect to the latch body **241** in an upward direction via a biasing member **245**, which is configured as a spring in the illustrative embodiment of the latch mechanism **200**. The plunger **244** may include a plunger face **244***a* that interfaces the latch point **36***a* of the forward yoke **36** when the latch mechanism **200** is positioned to retain the recoiling parts in the latch position (as shown in FIGS. **14**A, **17**A & **18**A). In the illustrative embodiment of the soft recoil system **10** pictured herein, the latch point **36***a* is configured to have an angled surface on the rearward side and a flat face on the forward side. The plunger **244** may also include a plunger ramp **244***b* opposite the plunger face **244***a* to interface the latch point **36***a* of the forward yoke **36** when the recoiling parts are moving rearward (i.e., toward the breech **24**) during the recoil phase, which is shown in FIG. **14**C.

The complimentary surfaces of the plunger **244** and latch point **36***a* facilitate movement of the recoiling parts in a rearward direction even when the latch point **36***a* contacts the plunger ramp **244***b* via the interaction between the angled surface of the latch point **36***a* and the plunger ramp **244***b* in conjunction with the biasing member **245**, which is shown in FIG. **14**C. The plunger face **244***a* interacts with the flat face of the latch point **36***a* to retain the recoiling parts (and/or stop the recoiling parts when they are moving forward during the counter-recoil phase) when the plunger **244** is in the extended position, which is shown in FIG. **14**A. Other structures and/or methods of allowing relative movement of the recoiling parts with respect to the latch mechanism **200** in a first direction while limiting the amount of relative movement there between in a second direction may be employed with the latch mechanism **200** and/or soft recoil system **10** as disclosed herein without limitation.

The plunger ramp **244***b* in cooperation with the biasing member **245** allow a portion of the recoiling parts to move past the plunger **244** in a direction from the front of the gun **12** to the rear of the gun **12** when the latch point **36***a* overcomes the biasing force of the biasing member **245** (thereby pushing the plunger **244** down against the biasing force of the biasing member **245** as shown in FIG. **14**C). The force required by the recoiling parts to overcome the upward biasing force of the biasing member **245** may be adjusted at least by the configuration of the latch point **36***a* (e.g., the angle of the surface that contacts the plunger **244**), the configuration of the plunger ramp **244***b* (e.g., the angle of the plunger ramp **244***a* with respect to the surface of the latch point **36***a* that contacts the plunger ramp **244***b*), and the upward biasing force the biasing member **245** imparts to the plunger **244**.

A crank **210** may be pivotally engaged with the housing **202** via a crank aperture **204** formed in the housing, a corresponding cover aperture **208***b* formed in the housing cover **208**, and a crank mount **212** formed in the crank **210**. In the illustrative embodiment of a crank **210** pictured herein, the crank mount **212** is generally formed as a tube or rod that fits into the crank aperture **204** and corresponding cover aperture **208***b*. However, the latch mechanism **200** and/or soft recoil system **10** disclosed and claimed herein is not limited by the configuration of the crank aperture **204**, housing cover **208**, and/or the crank mount **212**. The crank may include a crank arm **214** (two of which are shown in the illustrative embodiment of a latch mechanism **200** pictured herein) extending from the crank mount **212**.

A lever member **213** may be cooperatively engaged with the crank **210** such that the lever member **213** communicates mechanical forces to the crank **210** and vice versa. In the illustrative embodiment of the latch mechanism **200**, the lever member **213** is operable to communicate at least rotational forces to the crank **210** via the crank mount **212**, and is positioned on the exterior of the housing cover **208**. A rotational biasing member **215**, which may be configured as a torsion spring in certain embodiments of the latch mechanism **200**, may bias the crank **210** in a counterclockwise direction from the vantage shown in FIGS. **18**A & **18**B. The housing **202** may be configured with a stop wall **202***a* to limit the degree of rotation the crank **210** may experience with respect to the housing **202**. Generally the stop wall **202***a* will provide a limit to the rotation of the crank **210** due to rotational biasing force that the rotation biasing member **215** imparts to the crank **210**. The position of the stop wall **202***a* may be adjustable to optimize how the latch mechanism **200** functions for a specific application of the soft recoil system **10**.

A link **220** may communicate mechanical forces between the crank **210** and the latch assembly **240**. A link first end **222** may be pivotally engaged with the latch assembly **240** at the link connector(s) **243**. A link second end **224** may be pivotally engaged with the crank **210** at the distal end of the lever member(s) **213**. In the illustrative embodiment of a latch mechanism **200** pictured herein, the link **220** is curved downward from the vantage depicted in FIGS. **18**A & **18**B. This allows the axis of rotation of the crank **210** (generally the radial centerline of the crank aperture **204** and crank mount **212**) to be positioned below a line connecting the rotational axis of the link first end **222** and the rotational axis of the link second end **224** (referred to herein as "the connecting line").

When the latch mechanism **200** is in the position shown in FIGS. **14**A, **17**A, and **18**A, the latch mechanism **200** prevents the recoiling parts from moving forward (i.e., to the right from the vantage depicted in FIGS. **14**A, **18**A & **18**B). In this position, the latch point **36***a* directly contacts the plunger face **244***a*, and imparts a rotational biasing force in the clockwise direction to the latch assembly **240**. However, as long as axis of rotation of the crank mount **212** with respect to the crank aperture **204** remains below the connecting line (as defined above), that rotational biasing force will not result in any linear or rotational motion of any parts of the gun **12** and/or soft recoil system **10**.

A trip assembly **230** may be pivotally engaged with a housing cover **208** via a trip assembly bracket **208***a* formed in the housing cover **208** and a trip mount **232** formed in the trip assembly **230**. In the illustrative embodiment of a trip assembly **230** pictured herein, the trip assembly bracket **208***a* is generally formed as a channel bracket having at least one aperture, wherein the trip assembly bracket **208***a* is engaged with the exterior surface of the housing cover **208**, and the trip mount **232** is generally formed as a tube or rod that fits into the aperture formed in the trip assembly bracket **208***a* and a corresponding cover aperture **208***b*. However, the latch mechanism **200** and/or soft recoil system **10** disclosed and claimed herein is not limited by the configuration of the trip assembly bracket **208***a*, housing cover **208**, and/or the trip mount **232**. A lever member engager **234** may extend from the trip assembly **230** to engage the lever member **213** when the crank **210** and trip assembly **230** are in a certain orientation with respect to one another.

To release the recoiling parts (and thereby begin the run-up phase), a user may rotate the trip assembly **230** in a counterclockwise direction. This may be done manually via pulling a lanyard that is connected to the trip assembly **230**. The illustrative embodiment of the trip assembly **230** includes a bar **236** engaged with the trip assembly such that rotating the bar **236** causes the trip assembly **230** to rotate. The bar **236** may serve as an attachment point for a lanyard. Additionally, a safety mechanism may be engaged with the housing **202** adjacent the bar **236** to prevent an unwanted release of the latch mechanism **200**.

The rotation of the trip assembly **230** causes the lever member engager **234** to contact the lever member **213**. Continuing to rotation the trip assembly **230** in a counterclockwise direction causes the lever member **213** to rotate in a clockwise direction, which causes the crank **210** to rotation in a clockwise direction. This rotation of the crank **210** causes the link second end **224** to move down with respect to the link first end **222**. When the connecting line passes below the axis of rotation of the crank mount **212** with respect to the crank aperture **204**, the rotational biasing force the latch point **36***a* imparts to the latch assembly **240** via the plunger **244** will cause the latch assembly **240** to rotate clockwise, thereby releasing the recoiling parts and beginning the run-up phase (which position of the latch mechanism **200** is depicted in FIGS. **14**B, **17**B & **18**B).

After the recoiling parts have been released from the latch mechanism **200** and the run-up phase has begun, the rotational biasing member **215** may be configured such that it causes the crank **210** to rotate counterclockwise until the distal end of the crank arm(s) **214** and/or link second end **224** engage the stop wall **202***a*, which resets the latch mechanism **200**.

When the recoiling parts are moving rearward during the recoil phase, the latch point **36***a* on the recoiling parts will typically pass the latch position. The latch point **36***a* will typically overcome the biasing force that the biasing member **245** places on the plunger **244** due to the kinetic energy of the recoiling parts, thereby depressing the plunger **244** and allowing the recoiling parts to pass freely rearward of the latch position (as shown in FIG. **14**C). After the latch point **36***a* has passed rearward of the latch position, the biasing member **245** is designed to return the plunger **244** to the extended position (shown in FIGS. **14**A, **17**A & **18**A) so it may engage the latch point **36***a* during the counter-recoil phase.

The link **220** in the illustrative embodiment of the latch mechanism **200** is designed to serve two functions, both of which may be achieved through a curved configuration of the link **220** as shown for the illustrative embodiment of a latch mechanism **200** as pictured herein. First, as part of the over-centered linkage system comprised of the crank **210**, link **220**, and latch assembly **240**, the link **220** cooperates to hold the latch assembly **240** in position to overcome the potential energy of the compressed fluid in the soft recoil system **10** and thereby selectively prevent the recoiling parts from accelerating forward (i.e., entering the run-up phase). Secondly, the link **220** provides a shock absorbing capacity to the latch mechanism **200**. When the recoiling parts impact the plunger **244** during the counter-recoil phase, the tensile load imparted to the link **220** causes the curvature of the link **200** to straighten, thereby slightly lengthening the link **220**. This lengthening of the link **220** absorbs a portion of the impact energy recoiling parts impart to the latch mechanism in much the same way a spring would absorb that energy. It is contemplated that in the illustrative embodiment of the latch mechanism **200**, the link **220** will absorb normal impact loads without permanent deformation. It is also contemplated that the link **220** in the illustrative embodiment of the latch mechanism **200** will provide additional protection from damage to the various elements of the latch mechanism **200** (which damage may be caused by excessive impact loads) by straightening to the point that the over-center distance in the retaining position of the latch mechanism (shown in FIGS. **17**A & **18**A) is reduced to the point that it becomes negative. At this point the latch mechanism **200** would release the recoiling parts preventing possible damage to the latch mechanism **200**. Such excessive impact loads may be caused by counter-recoil control problems, and it is contemplated that a user should investigate the cause of such counter-recoil control problems before resuming normal operation.

Although the latch mechanism **200** pictured herein is generally manually operated, the latch mechanism **200** and/or soft recoil system **10** as disclosed and claimed herein is not so limited. The latch mechanism **200** may be outfitted with multiple layers of automation and/or actuation. For example, in an embodiment not pictured herein, the rotation of the trip assembly **230** may be caused by an electrical, pneumatic, or other type of powered actuator. Additionally, the rotational biasing member **215** and biasing member **245** may be electrical, pneumatic, or otherwise externally powered as opposed to being configured as mechanical springs.

The magnitude of the force(s) the rotational biasing member **215** imparts to the crank **210** and that the biasing member **245** imparts to the plunger **244** will vary from one embodiment of the latch mechanism **200** to the next, and are therefore in no way limiting to the scope thereof or to the scope of the soft recoil system **10**. Similarly, the force required to rotate the lever member **213** to a point at which the over-center orientation of the crank **210**, link **220**, and latch assembly **240** is eliminated will vary from one embodiment of the latch mechanism **200** to the next, and are therefore in no way limiting to the scope thereof or to the scope of the soft recoil system **10**.

In the embodiment pictured herein, it is contemplated that the latch mechanism **200** may be secured to the mounting bracket **57** adjacent the end of the actuator **16** opposite the base **14**. However, the latch mechanism **200** may be secured to any other suitable structure for the particular embodiment of the gun **12**, base **14**, and/or soft recoil system **10** without limitation. The various components of the latch mechanism **200** may be constructed of any suitable material for the particular application of the latch mechanism **200**. Such materials include but are not limited to metal, metallic alloys, synthetic materials, and combinations thereof.

The optimal dimensions and/or configuration of the yokes **32**, **34**, **36**, flange **39**, tie rods **40**, rail guides **50**, **60**, recoil cylinders **51**, **61**, recoil rods **52**, **62**, recuperators **56**, **66**, recoil piston(s) **64**, mounting bracket **57**, crossover bracket **59**, floating piston **67**, outer cylinder **71**, partition **74**, inner cylinder **81**, stop element **83**, check valve **100**, latch mechanism **200**, counter-recoil control valve **110**, misfire recovery system **130**, and various components thereof or interacting there with will vary from one embodiment of the soft recoil system **10** to the next, and are therefore in no way limiting to the scope thereof.

A gun **12** outfitted with the illustrative embodiment of the soft recoil system **10** disclosed herein conserves a portion of the energy from the firing of the round rather than simply dissipating that energy. The soft recoil system **10** then uses that conserved energy to offset the recoil from the firing of the next round. This allows for a faster cycle time in firing (with cycle times being reduced by as much as 50%) and longer periods of effective use. Because less energy is transferred to the fluid in the soft recoil system **10** than that in prior art systems (which reduction is equal to the energy required to stop the recoiling parts during the “run-up” phase), the fluid stays cooler during use as compared to prior arty systems.

The components of the soft recoil system **10** may be made any materials having the desired characteristics for the specific application of the soft recoil system **10** including but not limited to metals, metallic alloys, synthetic materials, and/or combinations thereof. For example, it is contemplated that for some applications of the soft recoil system **10** it will be advantages to construct the inner cylinder **81** using high-strength steel. Since the internal surfaces of the outer and inner cylinders **71**, **81** may be exposed to high pressures, the internal surface of the cylinders **71**, **81** must be strong enough to resist bursting. Additionally, it is contemplated that the inner cylinder **81** must be configured so that it resists deformation to mitigate leakage between it and recoil piston **64**. The material used for the inner cylinder **81** must also exhibit a high degree of wear resistance as the recoil piston **64** moves forward and rearward repeatedly therein. While other materials might be selected (including but not limited to metal, metallic alloys, synthetic materials, and/or combinations thereof), high-strength steel may be a preferred choice for various embodiments of the soft recoil system **10** when considering cost, weight, and performance.

In certain applications of the soft recoil system **10** the recoil rods **52**, **62** may be made from high-strength steel with a chrome-plated outside diameter. The high-strength steel provides the necessary strength and resistance to buckling. The chrome plating provides the degree of corrosion resistance necessary and functions efficiently for the dynamic seal interface purposes. It is contemplated that in the illustrative embodiment of the soft recoil system **10** the recoil piston **64** may be made from materials such as nodular cast iron or bronze. Both of these materials provide a certain amount of natural lubricity for sliding on materials such as steel. However, other materials may be used without limitation.

It is contemplated that for the illustrative embodiment of the soft recoil system **10**, the outer cylinder **71** may be made from medium-strength aluminum. Since the high-pressure operations are generally confined to the inside of the inner cylinder **81**, lower strength, lighter weight materials may be used for fluid transfer functions and lighter structural requirements. However, other materials may be used without limitation. Inasmuch as the soft recoil system **10** described and disclosed herein is subject to many variations, modifications and changes in detail, it is intended that all matter contained in the forgoing description or shown in the accompanying drawings shall be interpreted as illustrative and not in a limiting sense.

Although the specific embodiments pictured and herein pertain to a soft recoil system **10** adapted for use with a howitzer artillery piece, the soft recoil system **10** may be adapted for use with other types of gun **12**, such as mortars. Additionally, it is contemplated that the soft recoil system **10** may be adapted for use with artillery pieces other than those shown herein, wherein those artillery pieces fire different rounds, have barrels **20** of differing lengths, are mounted to different structures, or are generally designed for different uses than the gun **12** pictured herein. Accordingly, it is contemplated that certain embodiments of the soft recoil system **10** may be adapted for use with artillery weapons of various sizes and mortar weapons of various sizes, regardless of whether such weapons are vehicle mounted or otherwise.

The soft recoil system **10** may be configured with other orientations and/or with different quantities of the various elements having different shapes and/or orientations than those shown and described herein without limitation. Accordingly, the scope of the soft recoil system **10** is in no way limited by the specific shape and/or dimensions of the barrel **20**, rails **28**, **30**, yokes **32**, **34**, **36**, flange **39**, tie rods **40**, rail guides **50**, **60**, recoil cylinders **51**, **61**, recoil rods **52**, **62**, recuperators **56**, **66**, recoil piston(s) **64**, mounting bracket **57**, crossover bracket **59**, floating piston **67**, outer cylinder **71**, partition **74**, inner cylinder **81**, stop element **83**, check valve **100**, or the relative quantities and/or positions thereof.

Having described the preferred embodiment, other features, advantages, and/or efficiencies of the soft recoil system **10** will undoubtedly occur to those versed in the art, as will numerous modifications and alterations of the disclosed embodiments and methods, all of which may be achieved without departing from the spirit and scope of the soft recoil system **10** as disclosed and claimed herein. It should be noted that the soft recoil system **10** is not limited to the specific embodiments pictured and described herein, but are intended to apply to all similar apparatuses for mitigating recoil force and/or conserving the energy expended during the firing of a round. Modifications and alterations from the described embodiments will occur to those skilled in the art without departure from the spirit and scope of the soft recoil system **10**.

The invention claimed is:

1. A method for conserving the energy expended during the firing of a round in a gun using a recoil system, said method comprising the steps of:

a. operably engaging a recoil piston with said gun, wherein said recoil piston is slideably positioned in a first fluid chamber of said recoil system such that said piston may move linearly with respect to said first fluid chamber, wherein a fluid is positioned in said first fluid chamber, and wherein said recoil system comprises:
   i. a recuperator and a floating piston positioned in said recuperator, wherein said floating piston divides said recuperator into a first recuperator chamber and a second recuperator chamber each having a variable volume, wherein said fluid is in fluid communication with said second recuperator chamber, and wherein a second fluid is positioned in said first recuperator chamber;

b. using said recoil piston to displace a first volume of said fluid positioned in said first fluid chamber in response to the firing of said round;

c. throttling the rate at which said recoil piston displaces said first volume of said fluid;

d. capturing a first portion of the energy required to displace said first volume of said fluid,

e. storing said first portion of the energy required to displace said first volume of said fluid, wherein said storing said first portion of the energy required to displace said first volume of said fluid is performed using said second fluid, wherein said second fluid is compressible, wherein said recoil system further comprises a latch mechanism, and wherein said latch mechanism is configured to prevent movement of said recoil piston during the step of storing said first portion of the energy required to displace said first volume of said fluid;

f. releasing at least a part of said first portion of the energy required to displace said first volume of said fluid such that said at least a part of said first portion of the energy causes said recoil piston to move with respect to said first fluid chamber.

2. The method according to claim **1** wherein said first fluid chamber is further defined as an inner cylinder having a forward inner chamber and a rear inner chamber, wherein said inner cylinder is positioned within an outer cylinder having a forward outer chamber and a rear outer chamber, wherein said forward inner and outer chambers are formed with a fluid passage therein to allow fluid to pass from said inner cylinder to said outer cylinder and vice versa.

3. The method according to claim **2** wherein said forward outer chamber and said rear outer chamber are further defined as being separated by a partition, and wherein said partition is formed with a port therein to allow fluid to pass between said forward outer chamber and said rear outer chamber.

4. The method according to claim **3** wherein the throttling step is accomplished via movement of said fluid from said inner cylinder to said outer cylinder through said fluid passage.

5. The method according to claim **4** wherein said recoil system further comprises a check valve positioned in said forward outer chamber.

6. The method according to claim **5** wherein said check valve further comprises a flange portion and a sleeve portion, and wherein said sleeve portion is formed with a check valve fluid passage therein.

7. The method according to claim **6** wherein the releasing step is further defined as configuring said latch mechanism to allow said recoil piston to move with respect to said inner cylinder.

8. The method according to claim **7** wherein said releasing step is further defined as allowing said second fluid to expand.

9. The method according to claim **8** wherein allowing said second fluid to expand causes said floating piston to increase said volume of said first recuperator chamber and decrease said volume of said second recuperator chamber.

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