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### Namii et al.

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## (54) ENDOSCOPE OBJECTIVE OPTICAL SYSTEM

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### (52) **U.S. Cl.**

CPC ..... *A61B 1/00193* (2013.01); *A61B 1/00096* (2013.01); *G02B 13/04* (2013.01);

(Continued)

### (58) Field of Classification Search

### (56) References Cited

(10) Patent No.:

### U.S. PATENT DOCUMENTS

4,688,906 A 8/1987 Hilbert et al. 5,122,650 A 6/1992 McKinley (Continued)

### FOREIGN PATENT DOCUMENTS

IP 62215221 A 9/1987 IP 06194581 A 7/1994 (Continued)

### OTHER PUBLICATIONS

International Search Report (ISR) and Written Opinion dated Oct. 6, 2015 issued in International Application No. PCT/JP2015/068927.

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### (57) ABSTRACT

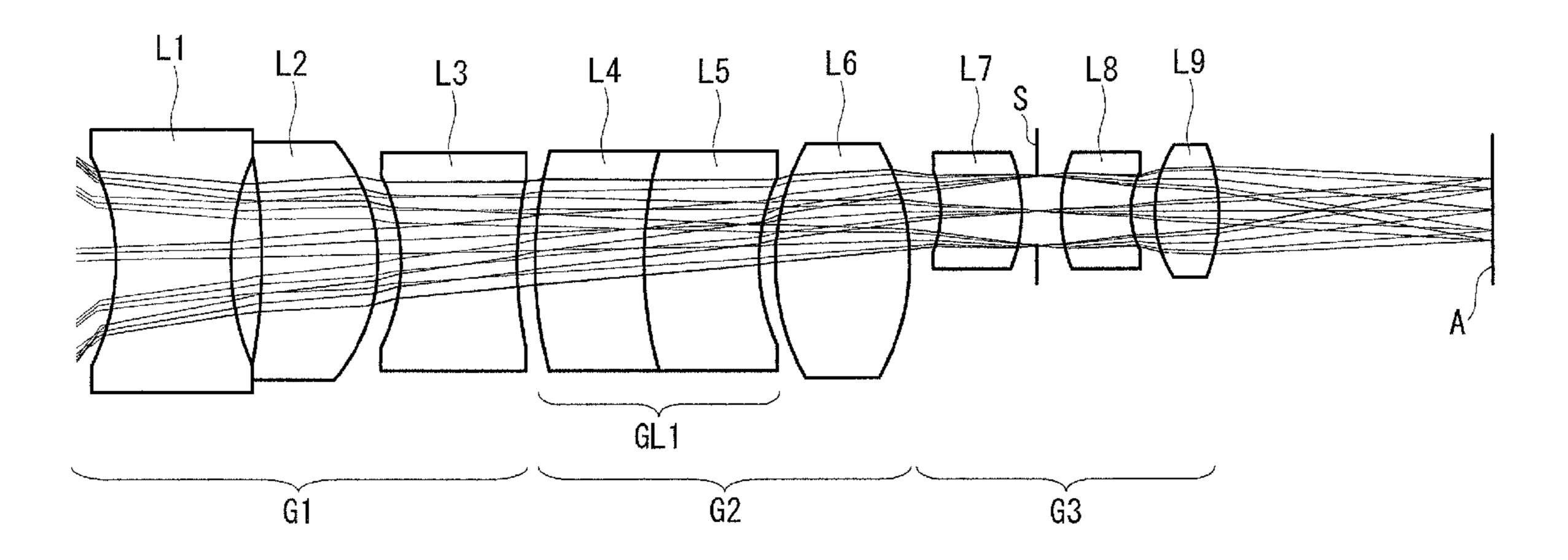
Provided is a small endoscope objective optical system that allows stereoscopic viewing even though a wide angle is used, that reduces the F-number, and that also reduces vignetting.

Provided is an endoscope objective optical system that consists of, sequentially from the object side, a negative first lens group, a positive second lens group, and a pair of third lens groups that are disposed side-by-side in the direction of parallax and that form two optical images with parallax, wherein aperture stops are individually provided in the third lens groups, and conditional expression M below is satisfied:

$$Fob\_n/Fob\_p > -0.5$$
 (1),

where Fob\_n is a focal length of the first lens group, and Fob\_p is a focal length of the second lens group.

### 4 Claims, 6 Drawing Sheets



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| (51) | Int. Cl.<br>G02B 23/26<br>G02B 23/24   | (2006.01)<br>(2006.01)              | 2009/00                  |             | 4/2009 | McKinley     | G02B 23/2415<br>348/45 |
|------|--|-------------------------------------|--------------------------|-------------|--------|--------------|------------------------|
| (52) | U.S. Cl.   |                                     | 2014/02                  | 239206 A1   | 8/2014 | Namii et al. |                        |
|      | CPC <i>G02B 23/243</i> (2013.01); <i>G02B 23/2415</i> (2013.01); <i>G02B 23/26</i> (2013.01) |                                     | FOREIGN PATENT DOCUMENTS |             |        |              | TS                     |
| (58) | Field of Class   | sification Search                   | JP                       | 06509       | 425 A  | 10/1994      |                        |
|      | USPC   |                                     | JP                       | 06331       | 937 A  | 12/1994      |                        |
|      | See applicatio   | n file for complete search history. | JP                       | 07236       | 610 A  | 9/1995       |                        |
|      | bee application the for complete scarch instory.   |                                     | JP                       | 08082       | 766 A  | 3/1996       |                        |
| (56) |  | References Cited                    | JP                       | 11503       | 844 A  | 3/1999       |                        |
| (56) |  | References Cited                    | JP                       | 2014140     | 593 A  | 8/2014       |                        |
|      | IIC D  | ATENIT EXACTIMENTE                  | WO                       | 9219        | 008 A1 | 10/1992      |                        |
|      | U.S. P   | PATENT DOCUMENTS                    | WO                       | 9633        | 436 A1 | 10/1996      |                        |
|      | 5 101 202 4  | 0/1000 3.5.771.1                    | WO                       | 2013114     | 725 A1 | 8/2013       |                        |
|      | 5,191,203 A  | •                                   | WO                       | 2014038     | 397 A1 | 3/2014       |                        |
|      | 5,496,261 A *  | 3/1996 Sander G02B 23/2438          | WO                       | 2015119     | 007 A1 | 8/2015       |                        |
|      |  | 359/379                             | a)a • . 1                |             |        |              |                        |
|      | 5,673,147 A  | 9/1997 McKinley                     | * cited                  | by examiner |        |              |                        |

FIG. 3

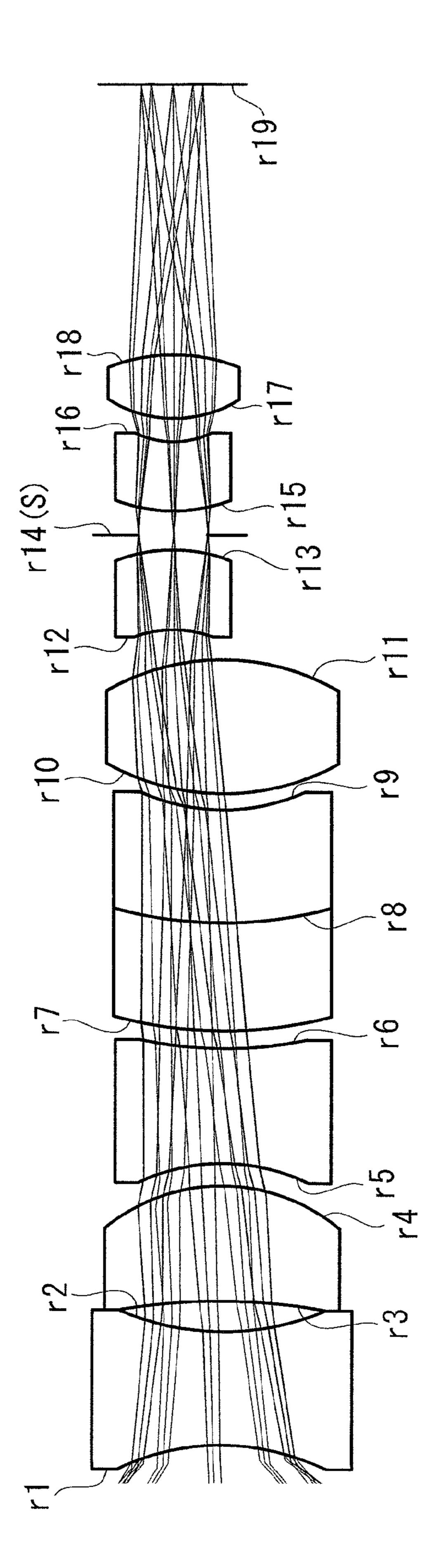


FIG. 4

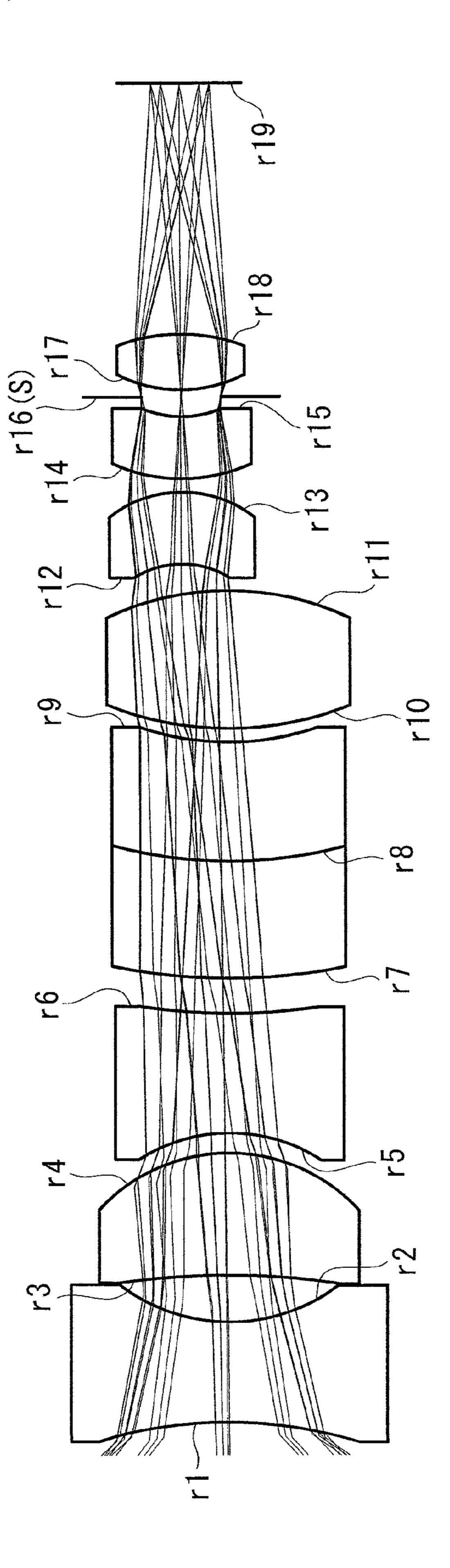
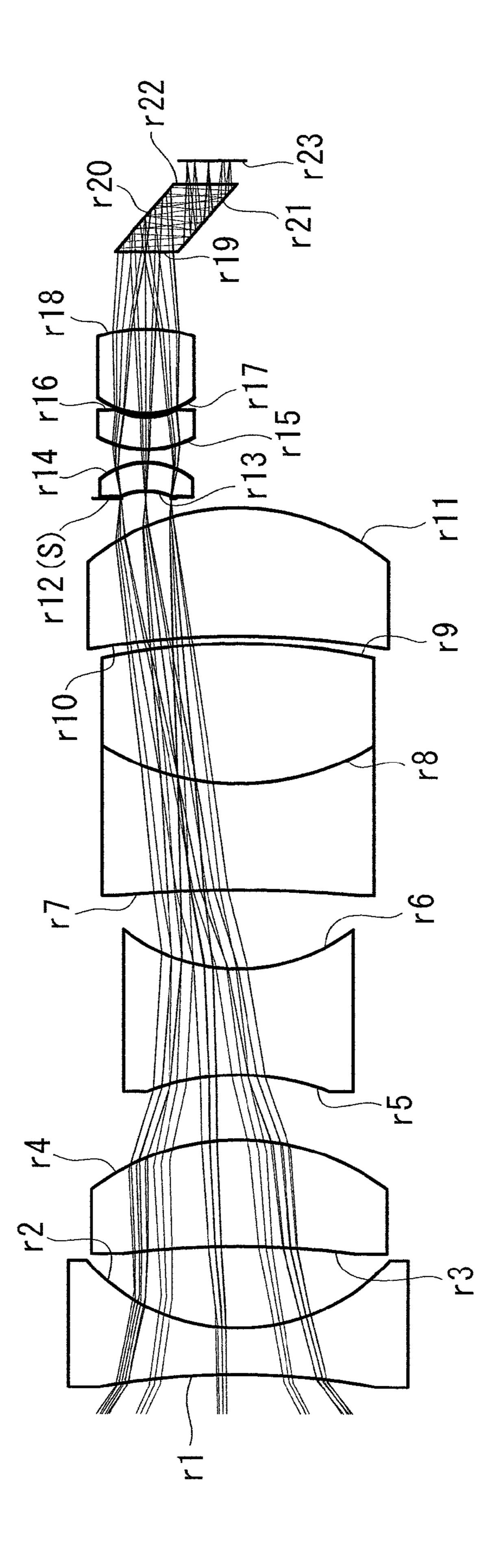


FIG. 5



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## ENDOSCOPE OBJECTIVE OPTICAL SYSTEM

## CROSS-REFERENCE TO RELATED APPLICATIONS

This is a continuation of International Application PCT/ JP2015/068927 which is hereby incorporated by reference herein in its entirety.

This application is based on Japanese Patent Application 10 No. 2014-141517, the contents of which are incorporated herein by reference.

### TECHNICAL FIELD

The present invention relates to an objective optical system, and relates, in particular, to an endoscope objective optical system employed in a medical endoscope.

### **BACKGROUND ART**

In the related art, objective optical systems for performing stereoscopic viewing by forming two optical images with parallax on a single image-acquisition element have been proposed.

As an example of such an objective optical system, Patent Literature 1 discloses an objective optical system provided with, sequentially from the object side, a front-group optical system shared between the left and right (in two directions of parallax) and a pair of, that is, left and right, imaging 30 optical systems.

### CITATION LIST

### Patent Literature

{PTL 1} Japanese Unexamined Patent Application, Publication No. Hei 8-82766

### SUMMARY OF INVENTION

### Solution to Problem

An aspect of the present invention provides an endoscope objective optical system that consists of, sequentially from the object side, a negative first lens group, a positive second lens group, and a pair of third lens groups that are disposed side-by-side in a direction of parallax and that form two optical images with parallax, wherein aperture stops are individually provided in the third lens groups, and conditional expression (1) below is satisfied:

$$Fob\_n/Fob\_p > -0.5$$
 (1),

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where Fob\_n is a focal length of the first lens group, and Fob\_p is a focal length of the second lens group.

### BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to a first embodiment of the present invention.

FIG. 2 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to a second embodiment of the present invention.

FIG. 3 is a cross-sectional view showing the overall configuration of an endoscope objective optical system 65 according to an example of the first embodiment of the present invention.

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FIG. 4 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to another example of the first embodiment of the present invention.

FIG. 5 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to an example of the second embodiment of the present invention.

FIG. 6 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to another example of the second embodiment of the present invention.

### DESCRIPTION OF EMBODIMENT

### First Embodiments

An endoscope objective optical system according to first embodiment of the present invention, will be described below with reference to the drawings.

FIG. 1 shows a cross-sectional view showing the overall configuration of the endoscope objective optical system. As shown in FIG. 1, the endoscope objective optical system is provided with a plurality of lens groups sequentially from the object side, namely, a negative first lens group G1, a positive second lens group G2, and a pair of third lens groups G3 that are disposed side-by-side in a direction of parallax and that form two optical images with parallax.

Note that, in this embodiment, only one of the pair of optical systems of the third lens groups G3 disposed in the direction of parallax is illustrated for the sake of convenience of explanation.

The first lens group is provided with, sequentially from the object side, a first lens L1, a second lens L2, and a third lens L3, and has negative optical power as a whole.

The second lens group G2 consists of, sequentially from the object side, a cemented lens CL1, formed between a fourth lens L4 and a fifth lens L5, and a sixth lens L6, and has positive optical power as a whole.

The third lens groups G3 are disposed side-by-side in the direction of parallax, individually focus light entering from the imaging subject via the first lens group G1 and the second lens group G2, and make the focused light incident on a light-receiving surface A of an image-acquisition element. Each of the third lens groups G3 consists of, sequentially from the object side, a seventh lens L7, an aperture stop S, an eighth lens L8, and a ninth lens L9. In FIG. 1, only one of the two third lens groups G3 is shown, and the other is omitted from the illustration.

In addition, the endoscope objective optical system according to this embodiment is configured so as to satisfy the following conditional expression (1):

$$Fob\_n/Fob\_p > -0.5 \tag{1},$$

where Fob\_n is the focal length of the first lens group G1, and Fob\_p is the focal length of the second lens group G2.

Conditional expression (1) defines conditions related to a ratio between the focal length of the first lens group G1 and the focal length of the second lens group G2, and, by decreasing the focal length of the first lens group G1, it is possible to form a wide-angle endoscope objective optical system in which the total angle is equal to or greater than 90°. In addition, by individually providing the aperture stops in the third lens groups G3, it is possible to reduce the beam-bundle diameters in the third lens groups G3, and thus, it is possible to achieve stereoscopic viewing even though a

wide angle is used, and it is possible to reduce the F-number and also to reduce vignetting.

In the case in which conditional expression (1) is not satisfied, the negative power due to the first lens group G1 and the second lens group G2 is reduced. Because of this, in 5 order to satisfy the wide-angle conditions, it is necessary to position the third lens groups G3 at positions farther away from the optical axes of the first lens group G1 and the second lens group G2 in the direction of parallax, or it is necessary to expand the beam bundles traveling from the 10 seventh lenses L7 of the third lens groups G3 to the sixth lens L6 of the second lens group G2. However, because in both cases, the beam-bundle diameter at the sixth lens L6 is increased, the size of the lens system as a whole is increased, 15 and, furthermore, it is necessary to correct aberrations at a position far away from the lens center of the second lens group G2, thus making it difficult to achieve a performance level that is compatible with the high pixel counts.

In addition, the endoscope objective optical system is 20 configured so as to satisfy conditional expression (2)

$$fs/fb < 2.5$$
 (2),

where fs is the distance from the position of the aperture stop S to the imaging surface (light-receiving surface A), and fb is the distance from the ninth lens L9, which is the final lens, to the imaging surface.

Conditional expression (2) defines the range within which the aperture stops S are positioned, and, it is possible to further reduce the beam-bundle diameters by disposing the aperture stops S within the range of conditional expression (2).

In the case in which conditional expression (2) is not satisfied, because the distances from the aperture stops S to 35 the imaging surface are increased, the beam-bundle diameters end up becoming large in the eighth lenses L8 and the ninth lenses L9 of the third lens groups G3. Therefore, in the third lens groups G3, vignetting occurs in the beam bundles, and thus, it becomes difficult to make the optical system 40 compatible with a high pixel count.

As has been described, with this embodiment, it is possible to form a wide-angle endoscope objective optical system in which the total angle is equal to or greater than 90° by decreasing the focal length of the first lens group G1; it 45 is possible to reduce the beam-bundle diameter in each of the third lens groups G3 by disposing the aperture stop S in the predetermined area of the each of the third lens groups G3; stereoscopic viewing is possible even though a wide angle is used; and it is possible to reduce the F-number and to reduce 50 vignetting.

### Second Embodiment

In addition, as a second embodiment of the present 55 invention, it is possible to configure an endoscope objective optical system as follows.

As shown in FIG. 2, an endoscope objective optical system according to this embodiment consists of, sequentially from the object side, the negative first lens group G1, 60 the positive second lens group G2, the pair of third lens groups G3 that are disposed side-by-side in the direction of parallax and that form two optical images with parallax, and reflection optical systems P having two reflection surfaces. In other words, the reflection optical systems P are provided 65 between the third lens groups G3 and the imaging surface A. In addition, in this e diment, the aperture stops S are

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disposed on the object side of the seventh lenses L7, which are the lenses that are closest to the object side in the third lens groups G3.

In addition, the endoscope objective optical system according to this embodiment is configured so as to satisfy conditional expression (3) below, in addition to the above-described conditional expressions (1) and (2):

$$fb/ihy>4$$
 (3),

where fb is the distance from the ninth lens L9, which is the final lens, to the imaging surface A, and ihy is the maximum image height in the direction of parallax.

By employing the reflection optical systems P having the two reflection surfaces, it is possible to form two optical images with parallax on a single image-acquisition element so as to be closer to each other, and, by satisfying conditional expression. (3), it is possible to prevent the occurrence of vignetting in the beam bundles in the reflection optical systems P.

### **EXAMPLES**

Next, Examples 1 to 4 of the endoscope objective optical systems according to one of the above-described embodiments will be described with reference to FIGS. 3 to 6. In lens data described in the Example sections, r is the radius of curvature (unit: mm), d is the surface interval (mm), Ne is the refractive index with respect to the e-line, and vd is the Abbe number with respect to the d-line.

### Example 1

FIG. 3 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to an Example of the first embodiment.

The endoscope objective optical system according to Example 1 consists of, sequentially from the object side, a negative first lens group, a positive second lens group, and a pair of third lens groups that are arranged in the direction of parallax. In addition, the aperture stops S are disposed on the image-surface sides of lenses disposed closest to the object sides of the third lens groups.

Lens data of the endoscope objective optical system according to this Example 1 are shown below.

Lens Data

| Surface Number     | r        | d        | Ne      | $\nu d$ |
|--------------------|----------|----------|---------|---------|
| Object Surface     |          | 15       |         |         |
| 1                  | -3.80837 | 1.5      | 1.883   | 40.7645 |
| 2                  | 4.14645  | 0.400822 |         |         |
| 3                  | -9.69475 | 1.50498  | 1.76182 | 26.5174 |
| 4                  | -2.85208 | 0.288    |         |         |
| 5                  | -3.27565 | 1.50498  | 1.63854 | 55.379  |
| 6                  | 6.22293  | 0.226368 |         |         |
| 7                  | 6.83208  | 1.41587  | 1.84666 | 23.777  |
| 8                  | 6.75522  | 1.46717  | 1.7495  | 35.331  |
| 9                  | 3.18333  | 0.214991 |         |         |
| 10                 | 3.73937  | 1.72575  | 1.603   | 65.442  |
| 11                 | -3.71946 | 0.392832 |         |         |
| 12                 | -1.7681  | 1.04509  | 1.54072 | 47.226  |
| 13                 | -2.48904 | 0.209019 |         |         |
| 14 (Aperture stop) |          | 0.298598 |         |         |
| 15                 | 2.5571   | 0.895795 | 1.92286 | 18.896  |
| 16                 | 1.45226  | 0.298598 |         |         |
| 17                 | 1.98468  | 0.82944  | 1.62041 | 60.288  |
| 18                 | -3.11608 | 3.503161 |         |         |
| 19 (Image Surface) |          |          |         |         |

Miscellaneous Data

Focal length Fob\_n of the first lens group -1.4266 mm

Focal length Fob\_p of the second lens group 5.60043 mm

Distance fs from the imaging surface to the aperture stop

5.8256 mm

Distance fb from the final lens to the imaging surface 3.503161 mm

Maximum image height ihy in the direction of parallax 0.45 mm

Amounts of displacement between the optical axis of the third lens group and the optical axes of the first and second lens groups 0.72 mm

F-number 4
Angle of view 59.9433°
Fob\_n/Fob\_p -0.25473044
fs/lb 1.662955257
fb/ihy 7.784802222

### Example 2

FIG. 4 is a cross-sectional view showing the overall configuration of an endoscope objective optical tem according to another Example of the first embodiment.

The endoscope objective optical system according to this 25 Example consists of, sequentially from the object side, a negative first lens group, a positive second lens group, and a pair of third lens groups that are arranged in the direction of parallax. In addition, the aperture stops S are disposed at the object sides of lenses disposed closest to the imagesurface sides of the third lens groups.

Lens data of the endoscope objective optical system according to this Example 2 are shown below.

Lens Data

| Surface Number     | $\mathbf{r}$ | d        | Ne      | νd      |
|--------------------|--------------|----------|---------|---------|
| Object Surface     |              | 15       |         |         |
| 1                  | -6.95702     | 1.5      | 1.883   | 40.7645 |
| 2                  | 2.98074      | 0.689341 |         |         |
| 3                  | -11.5723     | 1.7935   | 1.76182 | 26.5174 |
| 4                  | -2.83423     | 0.288    |         |         |
| 5                  | -2.74912     | 1.7935   | 1.63854 | 55.3792 |
| 6                  | 11.0428      | 0.514887 |         |         |
| 7                  | 10.0787      | 1.70439  | 1.84666 | 23.7775 |
| 8                  | 7.26287      | 1.75569  | 1.7495  | 35.3319 |
| 9                  | 4.59815      | 0.214991 |         |         |
| 10                 | 5.33836      | 2.01427  | 1.603   | 65.4427 |
| 11                 | -4.52516     | 0.392832 |         |         |
| 12                 | -1.47378     | 1.04509  | 1.54072 | 47.2264 |
| 13                 | -2           | 0.209019 |         |         |
| 14                 | 2.70984      | 0.895795 | 1.92286 | 18.8966 |
| 15                 | 1.49409      | 0.298598 |         |         |
| 16 (Aperture stop) |              | 0.1      |         |         |
| 17                 | 2.19475      | 0.82944  | 1.62041 | 60.2887 |
| 18                 | -2.97994     | 3.68799  |         |         |
| 19 (Image Surface) |              |          |         |         |

Focal length Fob\_n of the first lens group -1.61395 mm
Focal length Fob\_p of the second lens group 7.10026 mm
Distance fs from the imaging surface to the aperture stop
4.61743 mm

Distance fb from the final lens to the imaging surface 3.68799 mm

Maximum image height ihy in the direction of parallax 0.45 mm

Amounts of displacement between the optical axis of the 65 third lens group and the optical axes of the first and second lens groups 0.72 mm

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F-number 3

Angle of view 59.9961°

Fob\_n/Fob\_p -0.227308577

5 f/fb 1.252018037

fb/ihy 8.195533333

Example 3

FIG. 5 is a cross-sectional view showing the overall configuration of an endoscope objective optical system according to an Example of the second embodiment.

The endoscope objective optical system according to this Example consists of, sequentially from the object side, a negative first lens group, a positive second lens group, a pair of third lens groups that are arranged in the direction parallax, and reflection optical systems having two reflection surfaces. In addition, the aperture stops S are disposed at the object sides of lenses disposed closest to the object sides of the third lens groups.

Lens data of the endoscope objective optical system according to this Example 3 are shown bellow.

Lens Data

| Surface Number     | r           | d        | Ne          | $\nu d$ |
|--------------------|-------------|----------|-------------|---------|
| Object Surface     |             | 15       |             |         |
| 1                  | -12.5697    | 0.6      | 1.883       | 40.764  |
| 2                  | 3.12377     | 1.04167  |             |         |
| 3                  | -15.47      | 1.36097  | 1.92286     | 18.896  |
| 4                  | -3.84137    | 0.801512 |             |         |
| 5                  | -4.20218    | 1.36097  | 1.63854     | 55.379  |
| 6                  | 2.89504     | 1.00414  |             |         |
| 7                  | -19.4523    | 1.33611  | 1.84666     | 23.777  |
| 8                  | 4.08815     | 1.78599  | 1.7495      | 35.331  |
| 9                  | -11.1098    | 0.1      |             |         |
| 10                 | -14.0755    | 1.6083   | 1.603       | 65.442  |
| 11                 | -3.71871    | 0.12     |             |         |
| 12 (Aperture stop) |             | 0.1      |             |         |
| 13                 | -1.00081    | 0.35     | 1.78472     | 25.683  |
| 14                 | -1.19388    | 0.17     |             |         |
| 15                 | 1.59833     | 0.4      | 1.92286     | 18.896  |
| 16                 | 1.05853     | 0.05     |             |         |
| 17                 | 1.22734     | 1.08349  | 1.51633     | 64.141  |
| 18                 | -2.30257    | 0.965003 |             |         |
| 19                 | $\infty$    | 0.45     | 1.51633     | 64.141  |
| 20                 | $\infty$    | 0.9      | 1.51633     | 64.141  |
|                    | (Reflection |          |             |         |
|                    | Surface)    |          |             |         |
| 21                 | ∞ ×         | 0.4      | 1.51633     | 64.141  |
|                    | (Reflection |          | 110 1 0 0 0 | 0       |
|                    | Surface)    |          |             |         |
| 22                 | ∞ ∞         | 0.3      |             |         |
| 23 (Image Surface) |             | J.D      |             |         |

Miscellaneous Data

Focal length Fob\_n of the first lens group -1.36547 mm

Focal length Fob\_p of the second lens group 6.93611 mm

Distance fs from the imaging surface to the aperture stop 5.16849 mm

Distance fb from the final lens to the imaging surface fb 3.015003 mm

Maximum image height ihy in the direction of parallax 0.3 mm

Amounts of displacement between the optical axis of the third lens group and the optical axes of the first and second lens groups 1.3 mm

F-number 3.5 Angie of view 47° Fob\_n/Fob\_p -0.196863948 fs/fb 1.714257001 fb/ihy 10.05001

### Example 4

FIG. **6** is a cross-sectional view showing the overall second lens configuration of an endoscope objective optical system 10 F-number 3.5 according to another Example of the second embodiment. Angle of view

The endoscope objective optical system according to this Example consists of, sequentially from the object side, a negative first lens group, a positive second lens group, and a pair of third lens groups that are arranged in the direction of parallax, and reflection optical systems having two reflection surfaces. In addition, the aperture stops S are disposed

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Distance Fs from the imaging surface to the aperture stop 4.76563 mm

Distance Fb from the final lens to the imaging surface 2.695411 mm

5 Maximum image height ihy in the direction of parallax 0.35 mm

Amounts of displacement between the optical axis of the third lens group and the optical axes of the first and second lens groups 1.3 mm

F-number 3.5 Angle of view 700116° Fob\_n/Fob\_p -0.211482323 fs/fb 1.768053184 fb/ihy 7.701174286

Table 1 shows values related to the above-described conditional expressions (1) to (3) in the above-described Examples 1 to 4.

TABLE 1

|   | Example 1   | Example 2    | Example 3    | Example 4    |
|---|-------------|--------------|--------------|--------------|
| Conditional expression (1) Fob_n/Fob_p > -0.5 | -0.25473044 | -0.227308577 | -0.196863948 | -0.211482323 |
| Conditional expression (2) fs/fb < 2.5        | 1.662955257 | 1.252018037  | 1.714257001  | 1.768053184  |
| Conditional expression (3) fb/ihy > 4         | 7.784802222 | 8.195533333  | 10.05001     | 7.701174286  |
|   |             |              |              |              |

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at the image-surface sides of lenses disposed closest to the object sides of the third lens groups.

Lens data of the endoscope objective optical system according to this Example 4 are shown below.

Lens Data

| Surface Number     | r           | d        | Ne      | νd      |
|--------------------|-------------|----------|---------|---------|
| Object Surface     |             | 15       |         |         |
| 1                  | -8.92789    | 0.864    | 1.883   | 40.7645 |
| 2                  | 2.72124     | 0.953406 |         |         |
| 3                  | -3.02092    | 1.64979  | 1.92286 | 18.8966 |
| 4                  | -2.99104    | 0.844168 |         |         |
| 5                  | -2.80703    | 1.64979  | 1.63854 | 55.3792 |
| 6                  | -15.6192    | 1.13595  |         |         |
| 7                  | 6.11084     | 1.61398  | 1.84666 | 23.7775 |
| 8                  | 3.56736     | 1.79002  | 1.7495  | 35.3319 |
| 9                  | 4.60374     | 0.2      |         |         |
| 10                 | 5.72221     | 2.00594  | 1.603   | 65.4427 |
| 11                 | -6.89945    | 0.17     |         |         |
| 12                 | -1.50531    | 0.504    | 1.78472 | 25.683  |
| 13                 | -1.77592    | 0.1008   |         |         |
| 14 (Aperture stop) |             | 0.144    |         |         |
| 15                 | 1.51588     | 0.576    | 1.92286 | 18.8966 |
| 16                 | 0.903019    | 0.1      |         |         |
| 17                 | 1.06837     | 1.25022  | 1.51633 | 64.1411 |
| 18                 | -1.94052    | 0.645411 |         |         |
| 19                 | $\infty$    | 0.45     | 1.51633 | 64.1411 |
| 20                 | $\infty$    | 0.9      | 1.51633 | 64.1411 |
|                    | (Reflection |          |         |         |
|                    | Surface)    |          |         |         |
| 21                 | ∞ ´         | 0.4      | 1.51633 | 64.1411 |
|                    | (Reflection |          |         |         |
|                    | Surface)    |          |         |         |
| 22                 | ∞ ´         | 0.3      |         |         |
| 23 (Image Surface) |             |          |         |         |

### Miscellaneous Data

Focal length Fob\_n of the first lens group -1.62639 mm Focal length Fob\_p of the second lens group 7.69043 mm

The above-described embodiment leads to the following inventions.

An aspect of the present invention provides an endoscope objective optical system that consists of, sequentially from the object side, a negative first lens group, a positive second lens group, and a pair of third lens groups that are disposed side-by-side in a direction of parallax and that form two optical images with parallax, wherein aperture stops are individually provided in the third lens groups, and conditional expression (1) below is satisfied:

$$Fob\_n/Fob\_p > -0.5 \tag{1},$$

where Fob\_n is a focal length of the first lens group, and Fob\_p is a focal length of the second lens group.

In this aspect, conditional expression (1) defines conditions related to a ratio between the focal length of the first lens group and the focal length of the second lens group, and, by decreasing the focal length of the first lens group, it is possible to form a wide-angle objective optical system in which the total angle is equal to or greater than 90°. In addition, by individually providing the aperture stops in the third lens groups, because it is possible to reduce the beam-bundle diameters in the third lens groups, it is possible to achieve stereoscopic viewing even though a wide angle is used, and it is possible to reduce the F-number and also to reduce vignetting.

In, the above-described aspect, it is preferable that conditional expression (2) below be satisfied:

$$fs/fb < 2.5$$
 (2),

where fs is a distance from a position of the aperture stop to an imaging surface, and fb is a distance from a final lens to the imaging surface.

By setting the position of the aperture stop within the range of conditional expression (2) in this way, it is possible to further reduce the beam-bundle diameter.

In addition, in the above-described aspect, it is preferable that reflection optical systems having two reflection surfaces be individually disposed between the third lens groups and the imaging surface.

By employing the reflection optical systems having two 5 reflection surfaces in this way, it becomes possible to form two optical images with parallax on a single image-acquisition element so as to be closer to each other.

In addition, in the above-described aspect, it is preferable that conditional expression (3) below be satisfied:

$$fb/ihy>4$$
 (3),

where fb is a distance from a final lens to an imaging surface, and ihy is a maximum image height in the direction of parallax.

By doing so, it is possible to prevent the occurrence of vignetting in beam bundles in the reflection optical systems.

### REFERENCE SIGNS LIST

G1 first lens group

G2 second lens group

G3 third lens group

P reflection, optical system

S aperture stop

L1 first lens

L2 second lens

L3 third lens

L4 fourth lens

L5 fifth lens

L6 sixth lens

L7 seventh lens

L8 eighth lens

L9 ninth lens

CL1 cemented lens

The invention claimed is:

1. An endoscope objective optical system that consists of, sequentially from the object side, a negative first lens group

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having a single central axis, a positive second lens group having a single central axis, and a pair of third lens groups that are disposed side-by-side in a direction of parallax and that form two optical images with parallax,

wherein the negative first lens group consists of, sequentially from the object side, a negative lens, a positive lens, and a negative lens;

wherein the positive second lens group consists of, sequentially from the object side, a cemented lens and a positive lens; and

wherein aperture stops are individually provided in the third lens groups, and

conditional expression (1) below is satisfied:

$$Fob\_n/Fob\_p > -0.5 \tag{1},$$

where Fob\_n is a focal length of the first lens group, and Fob\_p is a focal length of the second lens group.

2. An endoscope objective optical system according to claim 1 that satisfies conditional expression (2) below:

$$fs/fb < 2.5$$
 (2),

where fs is a distance from a position of the aperture stop to an imaging surface, and fb is a distance from a final lens to the imaging surface.

3. An endoscope objective optical system according to claim 1, wherein reflection optical systems having two reflection surfaces are individually disposed between the third lens groups and the imaging surface.

4. An endoscope objective optical system according to claim 3 that satisfies conditional expression (3):

$$fb/ihy>4$$
 (3),

where fb is a distance from a final lens to an imaging surface, and ihy is a maximum image height in the direction of parallax.

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