

US009695913B2

(12) **United States Patent**
Goleski

(10) **Patent No.:** **US 9,695,913 B2**
(45) **Date of Patent:** **Jul. 4, 2017**

(54) **MULTIPLE SPEED TRANSMISSION**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 1321 days.

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(21) Appl. No.: **13/569,467**

(22) Filed: **Aug. 8, 2012**

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(65) **Prior Publication Data**

US 2014/0045639 A1 Feb. 13, 2014

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(51) **Int. Cl.**

F16H 3/66 (2006.01)

(52) **U.S. Cl.**

CPC **F16H 3/66** (2013.01); **F16H 2200/0065** (2013.01); **F16H 2200/2012** (2013.01); **F16H 2200/2046** (2013.01); **F16H 2200/2066** (2013.01); **F16H 2200/2097** (2013.01)

(58) **Field of Classification Search**

CPC . F16H 3/66; F16H 3/663; F16H 3/666; F16H 2200/0065; F16H 2200/2012; F16H 2200/2097; F16H 2200/2046; F16H 2200/2066

See application file for complete search history.

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(57)

ABSTRACT

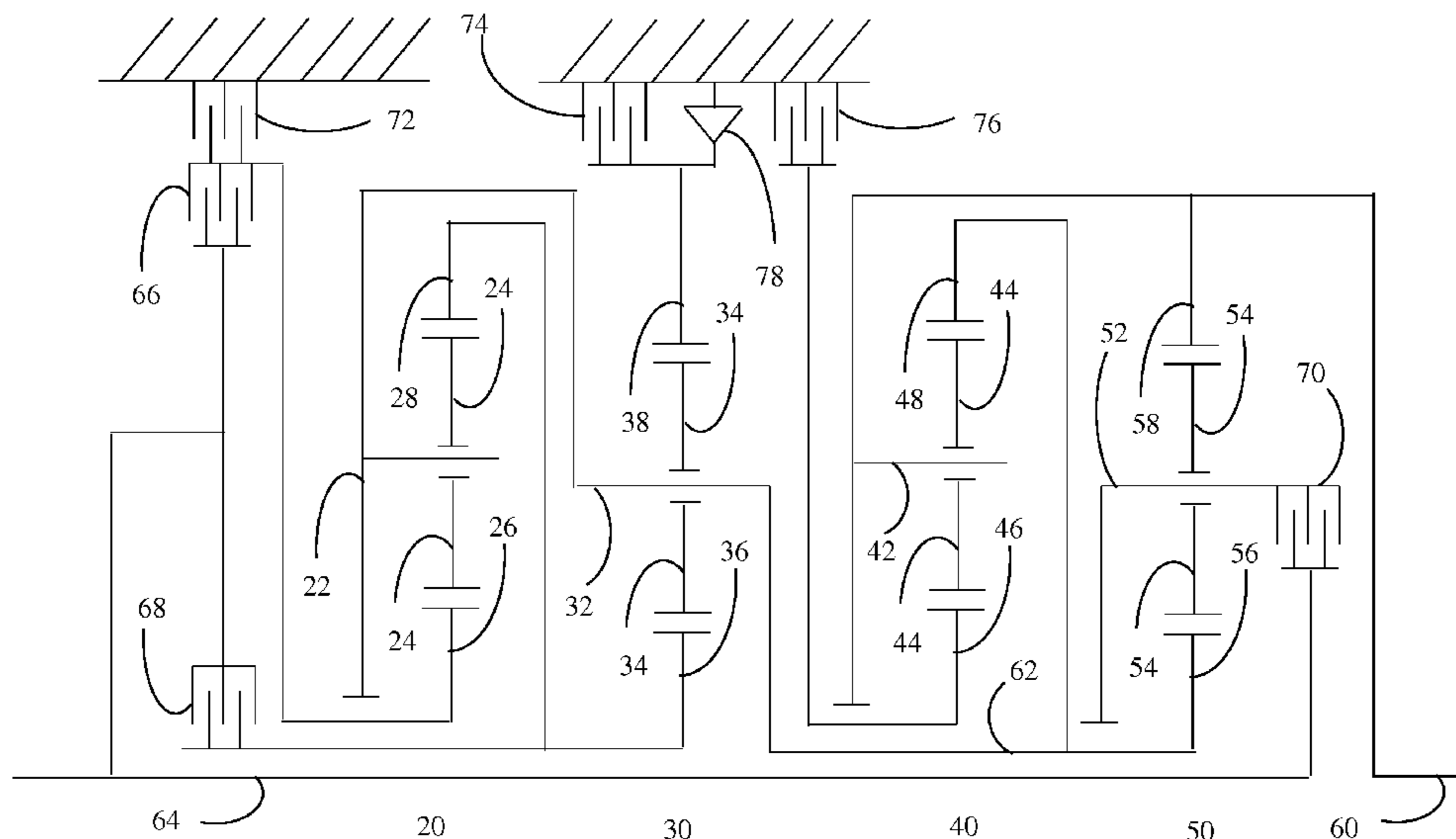
A family of transmission gearing arrangements produces nine forward and one reverse speed ratio by selective engagement of various combinations of three clutches or brakes. Each transmission gearing arrangement includes a front shiftable gearing arrangement configured to establish a variety of speed ratios between an intermediate shaft and an input shaft. These speed ratios include a reverse speed ratio, a zero speed ratio, two underdrive ratios, and a direct ratio. Each transmission also includes a rear shiftable gearing arrangement configured to selectively establish particular speed relationships among the input shaft, the intermediate shaft, and an output shaft.

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13 Claims, 8 Drawing Sheets



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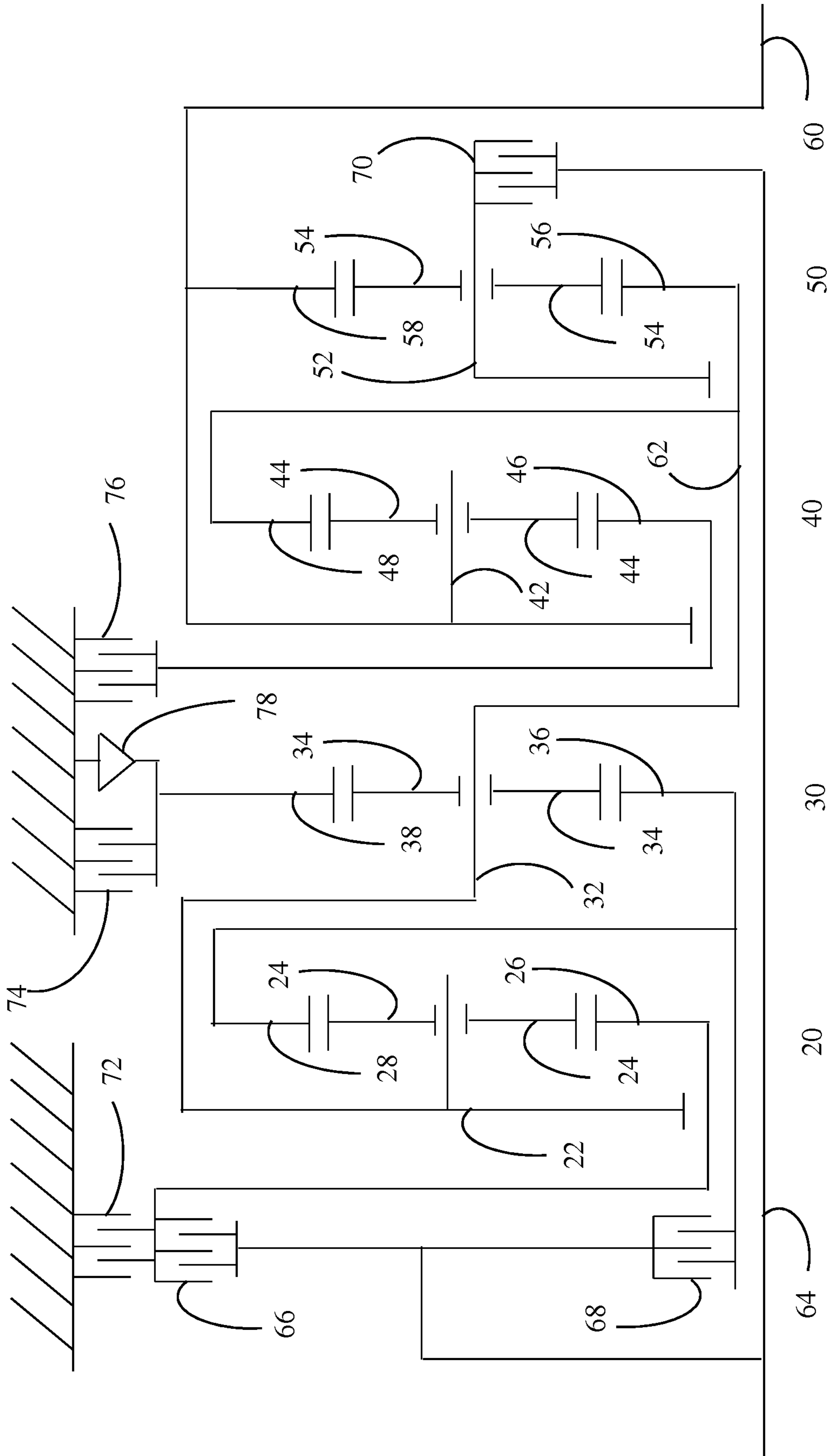


Figure 1

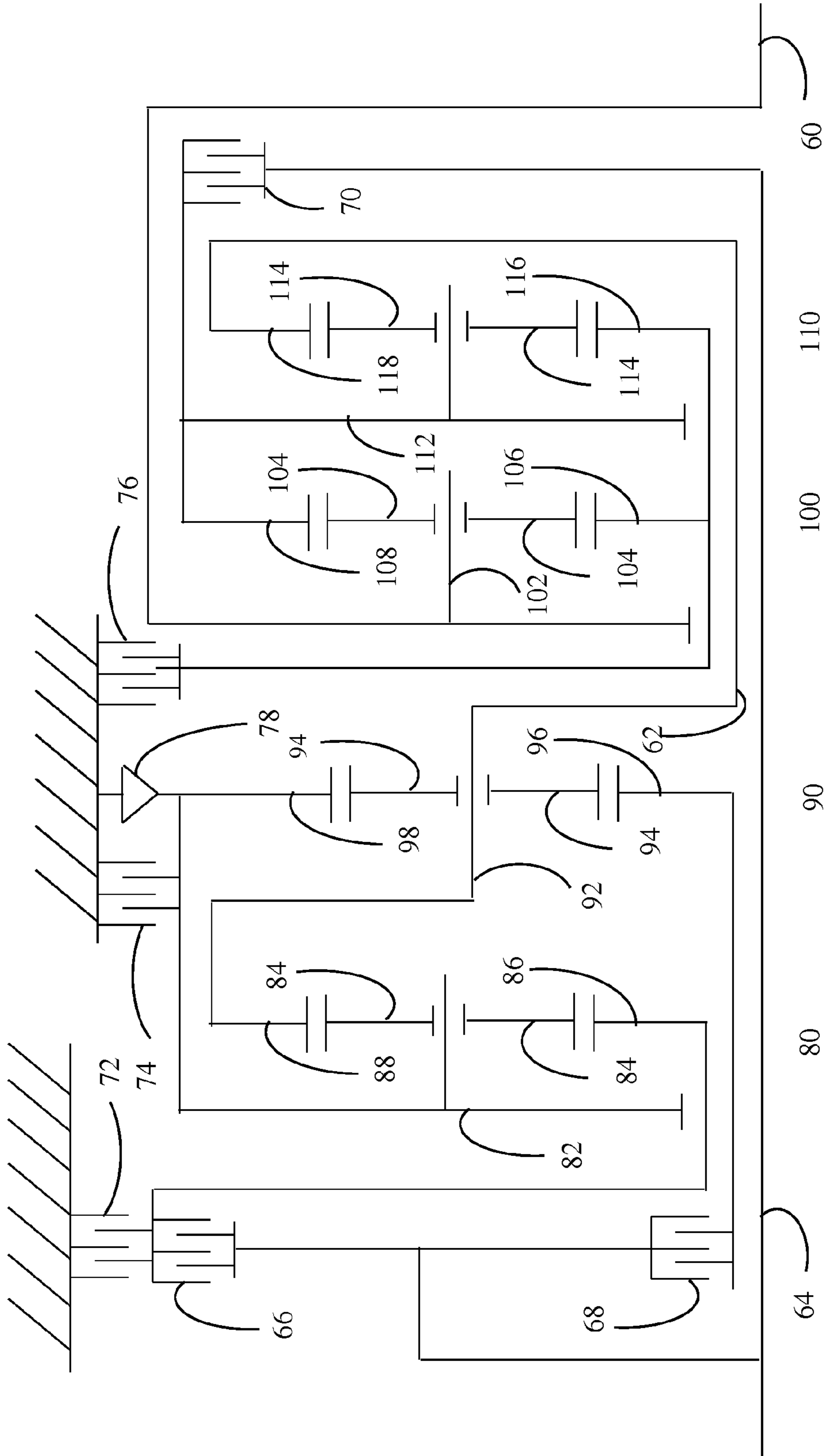


Figure 2

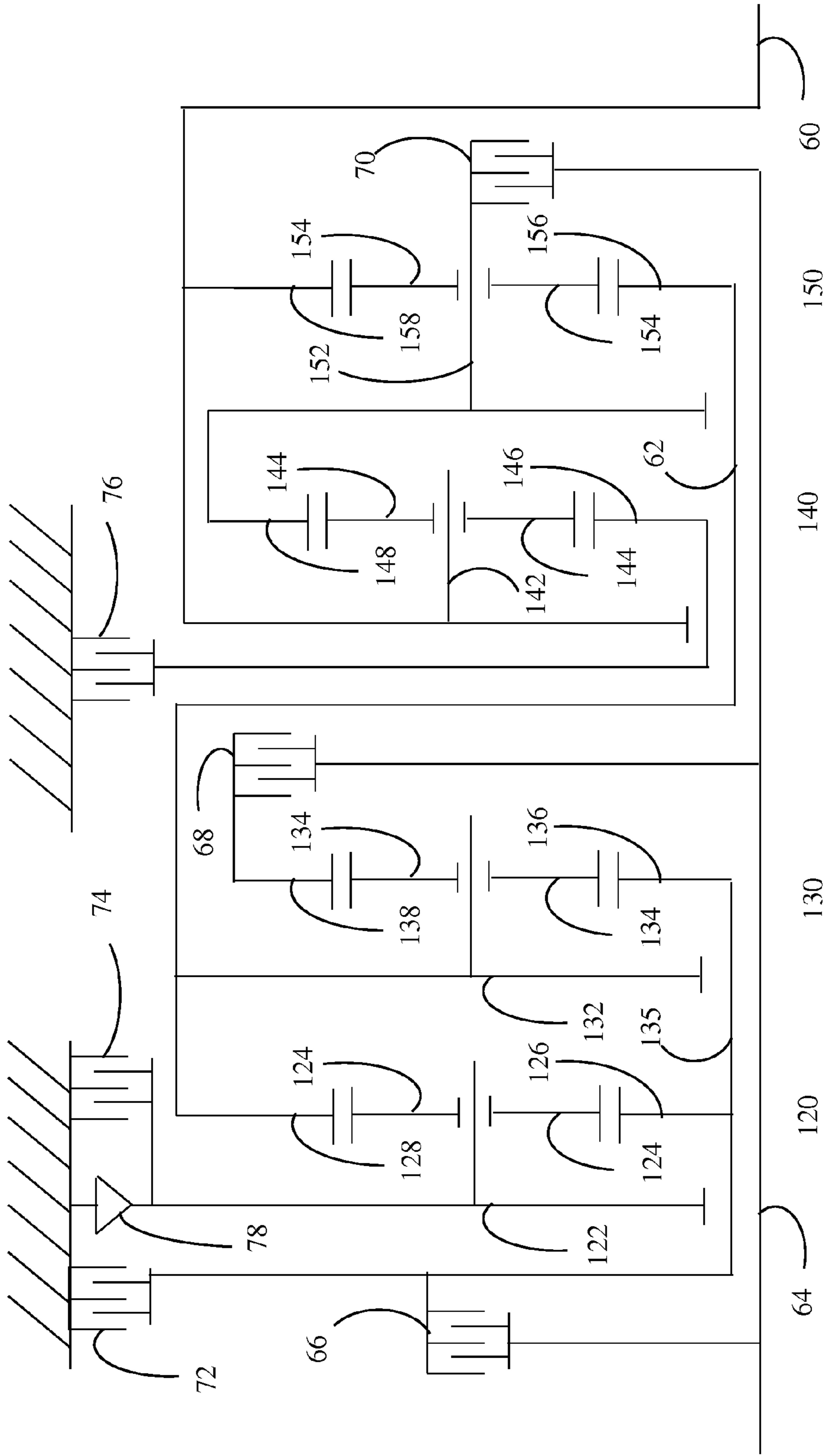


Figure 3

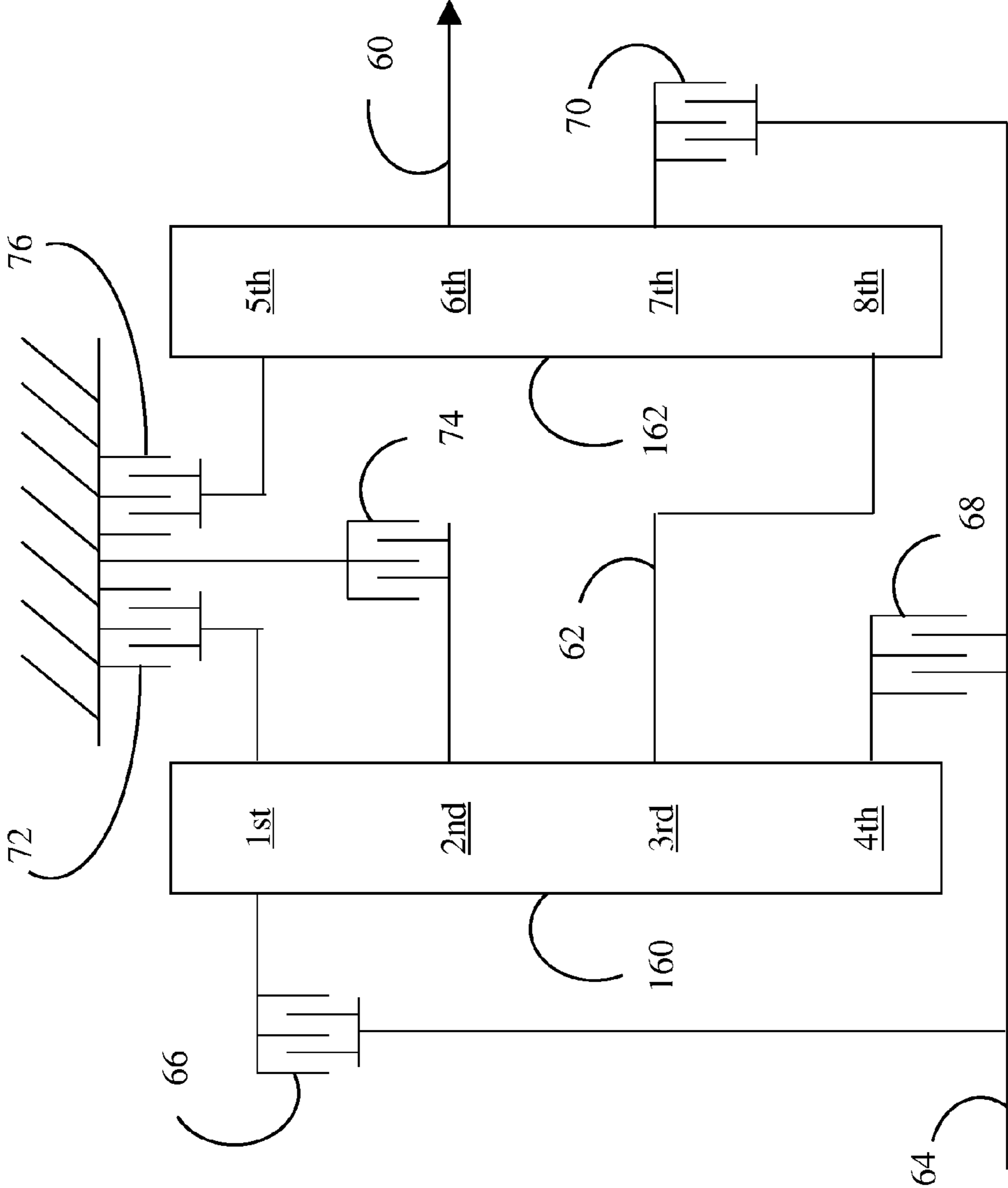


Figure 4

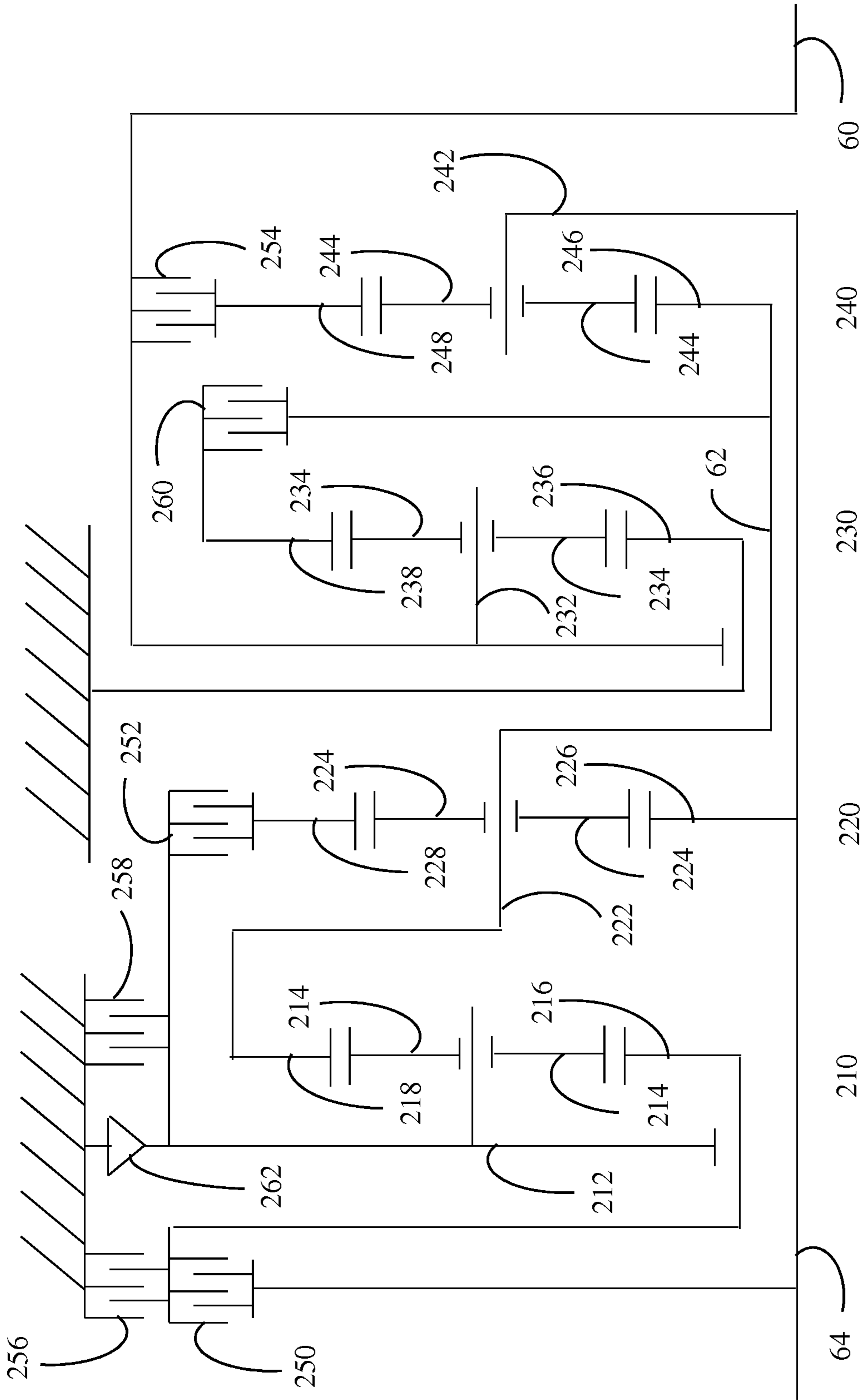


Figure 5

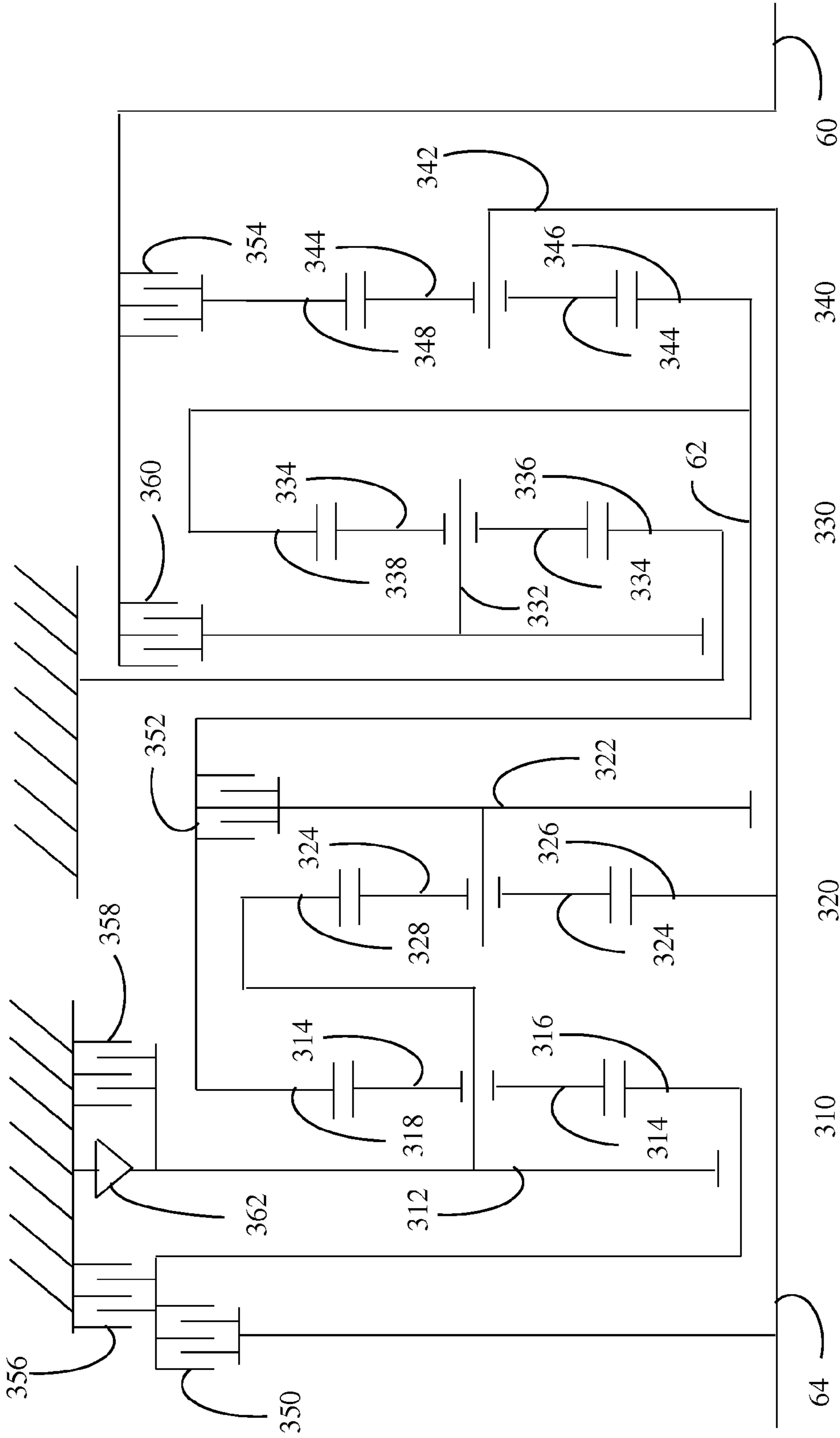


Figure 6

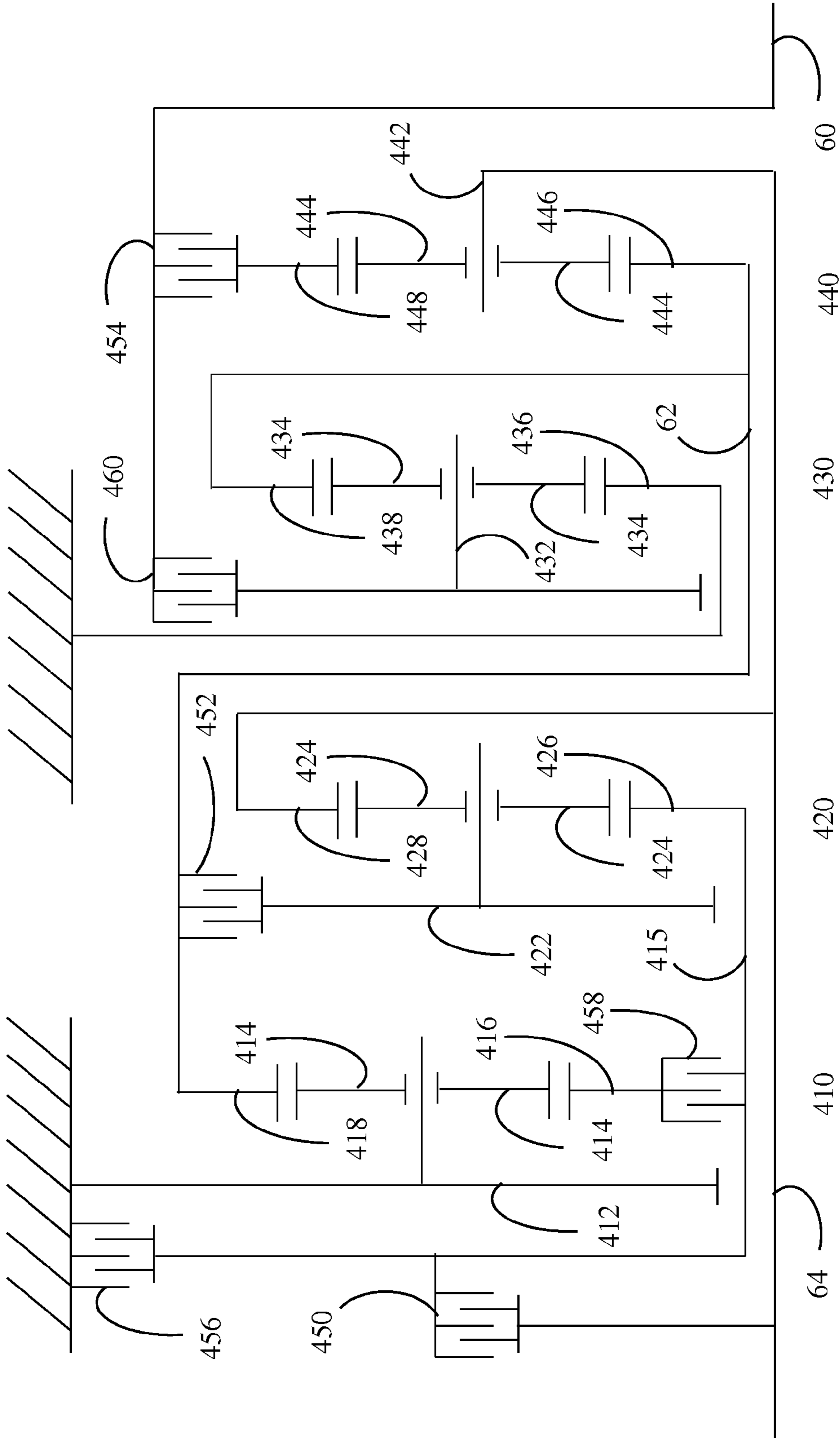


Figure 7

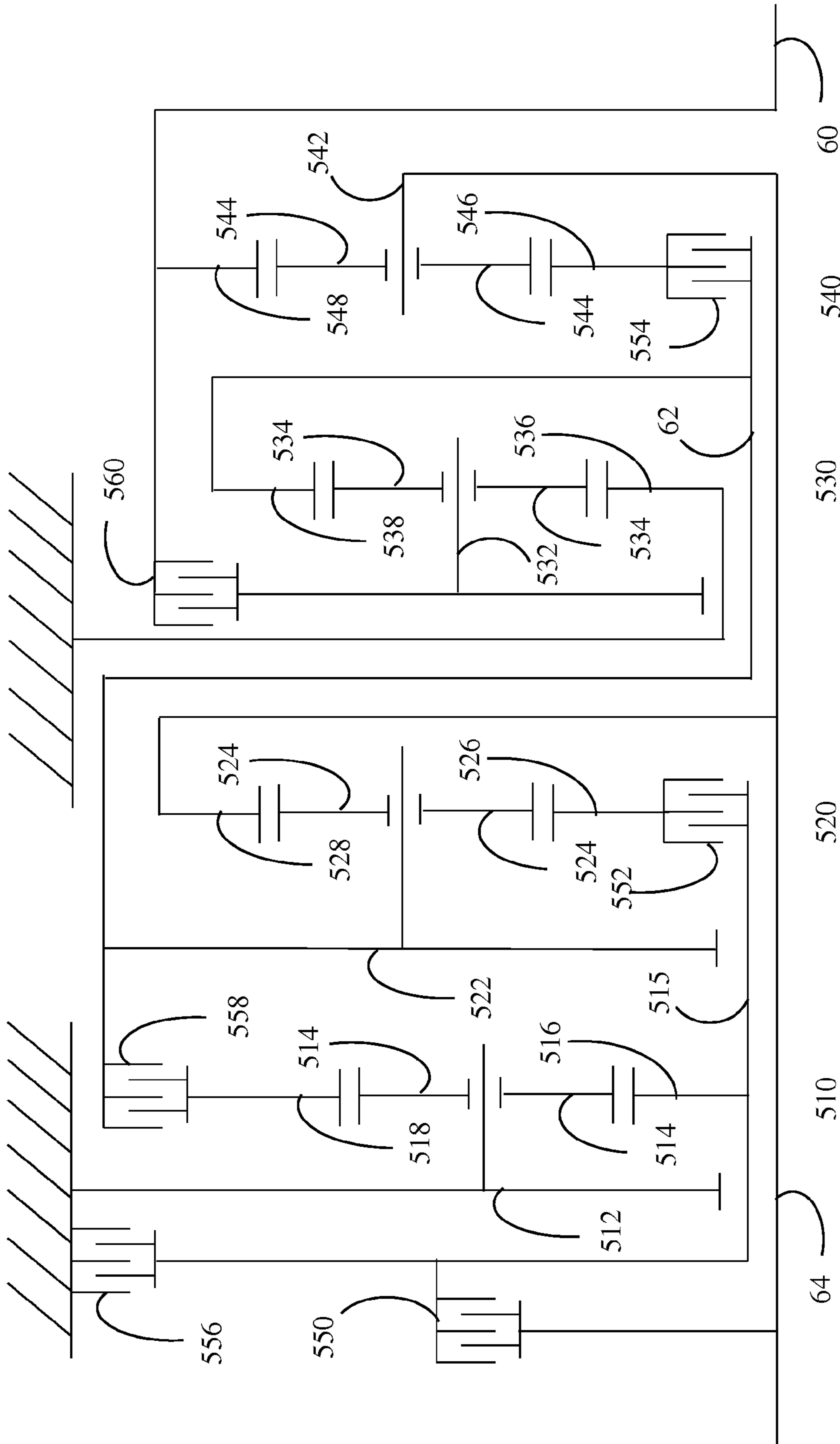


Figure 8

MULTIPLE SPEED TRANSMISSION

TECHNICAL FIELD

This disclosure relates to the field of automatic transmissions for motor vehicles. More particularly, the disclosure pertains to an arrangement of gears, clutches, and the interconnections among them in a power transmission.

BACKGROUND

Many vehicles are used over a wide range of vehicle speeds, including both forward and reverse movement. Some types of engines, however, are capable of operating efficiently only within a narrow range of speeds. Consequently, transmissions capable of efficiently transmitting power at a variety of speed ratios are frequently employed. When the vehicle is at low speed, the transmission is usually operated at a high speed ratio such that it multiplies the engine torque for improved acceleration. At high vehicle speed, operating the transmission at a low speed ratio permits an engine speed associated with quiet, fuel efficient cruising. Typically, a transmission has a housing mounted to the vehicle structure, an input shaft driven by an engine crankshaft, and an output shaft driving the vehicle wheels, often via a differential assembly which permits the left and right wheel to rotate at slightly different speeds as the vehicle turns.

SUMMARY OF THE DISCLOSURE

A family of transmission gearing arrangements is disclosed. Each transmission gearing arrangement includes a front shiftable gearing arrangement configured to establish a variety of speed ratios between an intermediate shaft and an input shaft, including a reverse speed ratio, a zero speed ratio, two underdrive speed ratios, and a direct drive ratio. The front shiftable gearing arrangement can, for example, comprise two simple planetary gear sets and four clutches. Each transmission gearing arrangement also includes a rear shiftable gearing arrangement configured to selectively establish particular speed relationships among the input shaft, the intermediate shaft, and an output shaft. The rear shiftable gearing arrangement can, for example, comprise two simple planetary gear sets and two clutches. Engaging the clutches in various combinations of three establishes nine forward speed ratios and one reverse speed ratio.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic diagram of a first transmission gearing arrangement;

FIG. 2 is a schematic diagram of a second transmission gearing arrangement;

FIG. 3 is a schematic diagram of a third transmission gearing arrangement;

FIG. 4 is a lever diagram corresponding to the first, second, and third transmission gearing arrangements;

FIG. 5 is a schematic diagram of a fourth transmission gearing arrangement;

FIG. 6 is a schematic diagram of a fifth transmission gearing arrangement;

FIG. 7 is a schematic diagram of a sixth transmission gearing arrangement; and

FIG. 8 is a schematic diagram of a seventh transmission gearing arrangement.

DETAILED DESCRIPTION

Embodiments of the present disclosure are described herein. It is to be understood, however, that the disclosed embodiments are merely examples and other embodiments can take various and alternative forms. The figures are not necessarily to scale; some features could be exaggerated or minimized to show details of particular components. Therefore, specific structural and functional details disclosed herein are not to be interpreted as limiting, but merely as a representative basis for teaching one skilled in the art to variously employ the present invention. As those of ordinary skill in the art will understand, various features illustrated and described with reference to any one of the figures can be combined with features illustrated in one or more other figures to produce embodiments that are not explicitly illustrated or described. The combinations of features illustrated provide representative embodiments for typical applications. Various combinations and modifications of the features consistent with the teachings of this disclosure, however, could be desired for particular applications or implementations.

A gearing arrangement is a collection of rotating elements and clutches configured to impose specified speed relationships among elements. Some speed relationships, called fixed speed relationships, are imposed regardless of the state of any clutches. A gearing arrangement imposing only fixed relationships is called a fixed gearing arrangement. Other speed relationships are imposed only when particular clutches are fully engaged. A gearing arrangement that selectively imposes speed relationships is called a shiftable gearing arrangement. A discrete ratio transmission has a shiftable gearing arrangement that selectively imposes a variety of speed ratios between an input shaft and an output shaft.

A group of elements are fixedly coupled to one another if they are constrained to rotate as a unit in all operating conditions. Elements can be fixedly coupled by spline connections, welding, press fitting, machining from a common solid, or other means. Slight variations in rotational displacement between fixedly coupled elements can occur such as displacement due to lash or shaft compliance. In contrast, two elements are selectively coupled by a clutch when the clutch constrains them to rotate as a unit whenever the clutch is fully engaged and they are free to rotate at distinct speeds in at least some other operating condition. Clutches include actively controlled devices such as hydraulically or electrically actuated clutches and passive devices such as one way clutches. A clutch that holds an element against rotation by selectively connecting the element to the housing may be called a brake. A group of elements are coupled if they are fixedly coupled or selectively coupled.

An example transmission is schematically illustrated in FIG. 1. The transmission utilizes four simple planetary gear sets **20**, **30**, **40**, and **50**. A simple planetary gear set is a type of fixed gearing arrangement. A planet carrier **22** rotates about a central axis and supports a set of planet gears **24** such that the planet gears rotate with respect to the planet carrier. External gear teeth on the planet gears mesh with external gear teeth on a sun gear **26** and with internal gear teeth on a ring gear **28**. The sun gear and ring gear are supported to rotate about the same axis as the carrier. A simple planetary gear set imposes the fixed speed relationship that the speed of the carrier is between the speed of the sun gear and the speed of the ring gear. (This relationship is defined to include the condition in which all three rotate at the same speed.) More specifically, the speed of the carrier is a

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weighted average of the speed of the sun gear and the speed of the ring gear with weighting factors determined by the number of teeth on each gear. Similar speed relationships are imposed by other known types of fixed gearing arrangements. For example, a double pinion planetary gear set

constrains the speed of the ring gear to be a weighted average between the speed of the sun gear and the speed of the carrier. Carrier **22** is fixedly coupled to carrier **32** and ring gear **28** is fixedly coupled to sun gear **34**. This produces a four element fixed gearing arrangement. The first element, sun gear **26**, and the fourth element, the combination of ring gear **28** and sun gear **36**, always have the most extreme speeds. The speeds of the second element, ring gear **38**, and the third element, the combination of carrier **22** and carrier **32**, have speeds that are a weighted average of the speeds of the first and fourth elements. Similarly, carrier **42** is fixedly coupled to ring gear **58** and ring gear **48** is fixedly coupled to sun gear **56**, producing a second four element fixed gearing arrangement. The fifth element, sun gear **46**, and the eighth element, the combination of ring gear **48** and sun gear **56**, always have the most extreme speeds. The speeds of the sixth element, the combination of carrier **42** and ring gear **58**, and the seventh element, carrier **52**, have speeds that are a weighted average of the speeds of the fifth and eighth elements.

A suggested ratio of gear teeth for each planetary gear set in FIG. 1 is listed in Table 1.

TABLE 1

Ring 28/Sun 26	1.85
Ring 38/Sun 36	1.75
Ring 48/Sun 46	1.60
Ring 58/Sun 56	2.30

The sixth element, **42** and **58**, is fixedly coupled to output shaft **60**. The third element, **22** and **32**, is fixedly coupled to the eighth element, **48** and **56**, by intermediate shaft **62**. Input shaft **64** is selectively coupled to the first element **26** by clutch **66**, selectively coupled to the fourth element, **28** and **36**, by clutch **68**, and selectively coupled to the seventh element **52** by clutch **70**. The first element **26** is selectively held against rotation by brake **72**, the second element **38** is selectively held against rotation by brake **74**, and the fifth element **46** is selectively held against rotation by brake **76**.

As shown in Table 2, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft **64** and output shaft **60**. An X indicates that the clutch is required to establish the speed ratio. An (X) indicates the clutch can be applied but is not required. When the gear sets of FIG. 1 have tooth numbers as indicated in Table 1, the speed ratios have the values indicated in Table 2. Gear sets **20** and **30**, clutches **66** and **68**, and brakes **72** and **74** form a front shiftable gearing arrangement that establishes a variety of speed ratios between intermediate shaft **62** and input shaft **64**. Specifically, engaging clutch **66** and brake **74** establishes a reverse speed ratio in which intermediate shaft **62** rotates in the opposite direction of input shaft **64**. Engaging both brakes **72** and **74** holds intermediate shaft **62** stationary. Engaging clutch **68** in combination with brake **72** and brake **74** respectively establishes two underdrive ratios in which intermediate shaft **62** rotates slower than input shaft **64**. Finally, engaging both clutches **66** and **68** establishes a direct drive ratio in which intermediate shaft **62** rotates at the same speed as input shaft **64**. Gear sets **40** and **50**, clutch **70**,

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and brake **76** form a rear shiftable gearing arrangement that establishes selectable speed relationships among input shaft **64**, intermediate shaft **62**, and output shaft **60**. Specifically, when brake **76** is engaged, an underdrive ratio is established between intermediate shaft **62** and output shaft **60**. This underdrive ratio, in combination with various speed ratios established by the front gearing arrangement, establishes the reverse ratio and the first three forward speed ratios of the transmission. When clutch **70** is engaged, the speed of input shaft **64** is constrained to be a weighted average between the speeds of intermediate shaft **62** and output shaft **60**. This speed relationship, in combination with various speed ratios established by the front gearing arrangement, establishes the top five forward speed ratios of the transmission. The remaining transmission ratio, 4th, is established by engaging clutch **70** and brake **76** together. The front gearing arrangement is not involved in establishing the 4th transmission ratio, but one of the clutches or brakes of the front gearing arrangement can be engaged if desired.

TABLE 2

	66	68	70	72	74/78	76	Ratio	Step
Rev	X				X	X	-3.64	81%
1 st		X			X	X	4.47	
2 nd		X		X		X	2.50	1.79
3 rd	X	X				X	1.63	1.54
4 th		(X)	X			X	1.19	1.37
5 th	X	X	X				1.00	1.19
6 th		X	X	X			0.87	1.15
7 th		X	X		X		0.78	1.11
8 th			X	X	X		0.70	1.12
9 th	X		X		X		0.61	1.14

Optional one way brake **78** passively holds second element **38** against rotation in one direction while allowing rotation in the other direction. Including this element simplifies the shift from 1st to 2nd gear. If one way brake **78** is present, brake **74** is not engaged in 1st gear. The shift to 2nd gear merely requires the gradual engagement of brake **72**. Once the torque capacity of brake **72** is sufficient, one way brake **78** will passively overrun. If one way brake **78** is omitted, then brake **74** is engaged in 1st gear. The shift from 1st gear to 2nd gear is then accomplished by the coordinated release of brake **74** and engagement of brake **72**. All remaining shift are accomplished by the coordinated release of one clutch or brake and the engagement of another clutch or brake.

Another example transmission is illustrated in FIG. 2. The transmission utilizes four simple planetary gear sets **80**, **90**, **100**, and **110**. Carrier **82** is fixedly coupled to ring gear **98** and ring gear **88** is fixedly coupled to carrier **92**, producing a four element fixed gearing arrangement. The first element, sun gear **86**, and the fourth element, sun gear **96**, always have the most extreme speeds. The speeds of the second element, the combination of carrier **82** and ring gear **98**, and the third element, the combination of ring gear **88** and carrier **92**, have speeds that are a weighted average of the speeds of the first and fourth elements. Similarly, sun gear **106** is fixedly coupled to sun gear **116** and ring gear **108** is fixedly coupled to carrier **112**, producing a second four element fixed gearing arrangement. The fifth element, the combination of sun gear **106** and sun gear **116**, and the eighth element, ring gear **118**, always have the most extreme speeds. The speeds of the sixth element, the combination of carrier **102** and ring gear **58**, and the seventh element, the

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combination of ring gear **108** and carrier **112**, have speeds that are a weighted average of the speeds of the fifth and eighth elements.

A suggested ratio of gear teeth for each planetary gear set in FIG. 2 is listed in Table 3.

TABLE 3

Ring 88/Sun 86	1.85
Ring 98/Sun 96	1.70
Ring 108/Sun 106	3.70
Ring 118/Sun 116	2.30

The sixth element, **102**, is fixedly coupled to output shaft **60**. The third element, **88** and **92**, is fixedly coupled to the eighth element **118** by intermediate shaft **62**. Input shaft **64** is selectively coupled to the first element **86** by clutch **66**, selectively coupled to the fourth element **96** by clutch **68**, and selectively coupled to the seventh element, **108** and **112**, by clutch **70**. The first element **86** is selectively held against rotation by brake **72**, the second element, **82** and **98**, is selectively held against rotation by brake **74**, and the fifth element, **106** and **116** is selectively held against rotation by brake **76**. Optionally, one way brake **78** passively holds second element, **82** and **98**, against rotation in one direction while allowing rotation in the other direction.

As shown in Table 4, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft **64** and output shaft **60**. When the gear sets of FIG. 2 have tooth numbers as indicated in Table 3, the speed ratios have the values indicated in Table 4.

TABLE 4

	66	68	70	72	74/78	76	Ratio	Step
Rev	X				X	X	-3.37	69%
1 st		X			X	X	4.92	
2 nd		X		X		X	2.91	1.69
3 rd	X	X				X	1.82	1.60
4 th		(X)	X			X	1.27	1.44
5 th	X	X	X				1.00	1.27
6 th		X	X	X			0.85	1.18
7 th		X	X		X		0.76	1.11
8 th			X	X	X		0.67	1.14
9 th	X		X		X		0.57	1.18

A third example transmission is illustrated in FIG. 3. The transmission utilizes four simple planetary gear sets **120**, **130**, **140**, and **150**. Sun gear **126** is fixedly coupled to sun gear **136** by intermediate shaft **135** and ring gear **128** is fixedly coupled to carrier **132**, producing a four element fixed gearing arrangement. The first element, the combination of sun gear **126** and sun gear **136**, and the fourth element, ring gear **138**, always have the most extreme speeds. The speeds of the second element, carrier **122**, and the third element, the combination of ring gear **128** and carrier **132**, have speeds that are a weighted average of the speeds of the first and fourth elements. Similarly, carrier **142** is fixedly coupled to ring gear **158** and ring gear **148** is fixedly coupled to carrier **152**, producing a second four element fixed gearing arrangement. The fifth element, sun gear **146**, and the eighth element, sun gear **156**, always have the most extreme speeds. The speeds of the sixth element, the combination of carrier **142** and ring gear **158**, and the seventh element, the combination of ring gear **148** and carrier **152**, have speeds that are a weighted average of the speeds of the fifth and eighth elements.

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A suggested ratio of gear teeth for each planetary gear set in FIG. 3 is listed in Table 5.

TABLE 5

Ring 128/Sun 126	2.00
Ring 138/Sun 136	1.90
Ring 148/Sun 146	3.70
Ring 158/Sun 156	1.70

The sixth element, **142** and **158**, is fixedly coupled to output shaft **60**. The third element, **128** and **132**, is fixedly coupled to the eighth element **156** by intermediate shaft **62**. Input shaft **64** is selectively coupled to the first element, **126** and **136**, by clutch **66**, selectively coupled to the fourth element **138** by clutch **68**, and selectively coupled to the seventh element, **148** and **152**, by clutch **70**. The first element, **126** and **136**, is selectively held against rotation by brake **72**, the second element **122** is selectively held against rotation by brake **74**, and the fifth element **146** is selectively held against rotation by brake **76**. Optionally, one way brake **78** passively holds second element **122** against rotation in one direction while allowing rotation in the other direction.

As shown in Table 6, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft **64** and output shaft **60**. When the gear sets of FIG. 3 have tooth numbers as indicated in Table 5, the speed ratios have the values indicated in Table 6.

TABLE 6

	66	68	70	72	74/78	76	Ratio	Step
Rev	X				X	X	-3.46	78%
1 st		X			X	X	4.46	
2 nd		X		X		X	2.64	1.69
3 rd	X	X				X	1.73	1.53
4 th		(X)	X			X	1.27	1.36
5 th	X	X	X				1.00	1.27
6 th		X	X	X			0.83	1.20
7 th		X	X		X		0.74	1.13
8 th			X	X	X		0.63	1.17
9 th	X		X		X		0.53	1.19

FIG. 4 describes the transmissions of FIGS. 1, 2, and 3 in the form of a lever diagram. Gear elements which rotate about a common axis and have speeds with a fixed linear relationship are shown along a lever according to their relative speeds. The two elements that have the most extreme speeds are shown at the endpoints of the lever. The remaining elements are shown at intermediate points according to the weighting factors. Lever **160** corresponds to gear sets **20** and **30** of FIG. 1, gear sets **80** and **90** of FIG. 2, and gear sets **120** and **130** of FIG. 3. Any four element fixed gearing arrangement that imposes the designated speed relationships with appropriate weighting factors can be substituted for the corresponding gear sets without impacting the transmission speed ratios. In addition to the fixed gearing arrangements illustrated in FIG. 1-3, many others are known. Any combination of two planetary gear sets with two elements of each fixedly connected to two elements of the other forms a four element fixed gearing arrangement. Some fixed gearing arrangements will be preferable to others in terms of packaging, efficiency, and planet gear speeds. Similarly, lever **162** corresponds to gear sets **40** and **50** of FIG. 1, gear sets **100** and **110** of FIG. 2, and gear sets **140** and **150** of FIG. 3. Any four element fixed gearing

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arrangement that imposes the designated speed relationships can be substituted for the corresponding gear sets.

A fourth example transmission is illustrated in FIG. 5. The transmission utilizes four simple planetary gear sets 210, 220, 230, and 240. Ring gear 218 and carrier 222 are fixedly coupled to sun gear 246 by intermediate shaft 62. Carrier 232 is fixedly coupled to output shaft 60. Sun gear 226 and carrier 242 are fixedly coupled to input shaft 64. Sun gear 236 is fixedly held against rotation. A suggested ratio of gear teeth for each planetary gear set in FIG. 5 is listed in Table 7.

TABLE 7

Ring 218/Sun 216	1.85
Ring 228/Sun 226	1.70
Ring 238/Sun 236	1.60
Ring 248/Sun 246	2.30

Sun gear 216 is selectively coupled to input shaft 64 by clutch 250 and selectively held against rotation by brake 256. Carrier 212 is selectively coupled to ring gear 228 by clutch 252 and selectively held against rotation by brake 258. Ring gear 238 is selectively coupled to sun gear 246 and intermediate shaft 62 by clutch 260. Ring gear 248 is selectively coupled to carrier 232 and output shaft 60 by clutch 254. Optionally, one way brake 262 passively holds carrier 212 against rotation in one direction while allowing rotation in the other direction.

As shown in Table 8, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft 64 and output shaft 60. When the gear sets of FIG. 5 have tooth numbers as indicated in Table 7, the speed ratios have the values indicated in Table 8.

TABLE 8

	250	252	254	256	258/262	260	Ratio	Step
Rev	X				X	X	-3.01	69%
1 st		X			X	X	4.39	
2 nd		X		X		X	2.59	1.69
3 rd	X	X				X	1.63	1.60
4 th		(X)	X			X	1.19	1.37
5 th	X	X	X				1.00	1.19
6 th		X	X	X			0.86	1.16
7 th		X	X		X		0.79	1.10
8 th			X	X	X		0.70	1.13
9 th	X		X		X		0.60	1.16

A fifth example transmission is illustrated in FIG. 6. The transmission utilizes four simple planetary gear sets 310, 320, 330, and 340. Ring gear 318 is fixedly coupled to ring gear 338 and sun gear 346 by intermediate shaft 62. Carrier 312 is fixedly coupled to ring gear 328. Sun gear 326 and carrier 342 are fixedly coupled to input shaft 64. Sun gear 336 is fixedly held against rotation. A suggested ratio of gear teeth for each planetary gear set in FIG. 5 is listed in Table 9.

TABLE 9

Ring 318/Sun 316	1.85
Ring 328/Sun 326	1.70
Ring 338/Sun 336	1.60
Ring 348/Sun 346	2.30

Sun gear 316 is selectively coupled to input shaft 64 by clutch 350 and selectively held against rotation by brake

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356. Carrier 312 and ring gear 328 are selectively held against rotation by brake 358. Carrier 322 is selectively coupled to ring gear 318 and intermediate shaft 62 by clutch 352. Output shaft 60 is selectively coupled to carrier 332 by clutch 360 and selectively coupled to ring gear 348 by clutch 354. Optionally, one way brake 362 passively holds carrier 312 and ring gear 328 against rotation in one direction while allowing rotation in the other direction.

As shown in Table 10, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft 64 and output shaft 60. When the gear sets of FIG. 6 have tooth numbers as indicated in Table 9, the speed ratios have the values indicated in Table 10.

TABLE 10

	350	352	354	356	358/362	360	Ratio	Step
Rev	X				X	X	-3.01	69%
1 st		X			X	X	4.39	
2 nd		X		X		X	2.59	1.69
3 rd	X	X				X	1.63	1.60
4 th		(X)	X			X	1.19	1.37
5 th	X	X	X				1.00	1.19
6 th		X	X	X			0.86	1.16
7 th		X	X		X		0.79	1.10
8 th			X	X	X		0.70	1.13
9 th	X		X		X		0.60	1.16

A sixth example transmission is illustrated in FIG. 7. The transmission utilizes four simple planetary gear sets 410, 420, 430, and 440. Ring gear 418 is fixedly coupled to ring gear 438 and sun gear 446 by intermediate shaft 62. Sun gear 426 is fixedly coupled to intermediate shaft 415. Ring gear 428 and carrier 442 are fixedly coupled to input shaft 64. Carrier 412 and sun gear 436 are fixedly held against rotation. A suggested ratio of gear teeth for each planetary gear set in FIG. 7 is listed in Table 11.

TABLE 11

Ring 418/Sun 416	2.00
Ring 428/Sun 426	1.90
Ring 438/Sun 436	1.60
Ring 448/Sun 446	2.30

Intermediate shaft 415 is selectively coupled to input shaft 64 by clutch 450, selectively coupled to sun gear 416 by clutch 458, and selectively held against rotation by brake 456. Carrier 422 is selectively coupled to ring gear 418 and intermediate shaft 62 by clutch 452. Output shaft 60 is selectively coupled to carrier 432 by clutch 460 and selectively coupled to ring gear 448 by clutch 454.

As shown in Table 12, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft 64 and output shaft 60. When the gear sets of FIG. 7 have tooth numbers as indicated in Table 11, the speed ratios have the values indicated in Table 12.

TABLE 12

	450	452	454	456	458	460	Ratio	Step
Rev	X				X	X	-3.25	78%
1 st		X			X	X	4.19	
2 nd		X		X		X	2.48	1.69
3 rd	X	X				X	1.63	1.53
4 th		(X)	X			X	1.19	1.37

TABLE 12-continued

	450	452	454	456	458	460	Ratio	Step
5 th	X	X	X				1.00	1.19
6 th		X	X	X			0.87	1.15
7 th		X	X		X		0.79	1.10
8 th			X	X	X		0.70	1.13
9 th	X		X		X		0.61	1.15

A seventh example transmission is illustrated in FIG. 8. The transmission utilizes four simple planetary gear sets **510**, **520**, **530**, and **540**. Carrier **522** is fixedly coupled to ring gear **538** by intermediate shaft **62**. Sun gear **516** is fixedly coupled to intermediate shaft **515**. Ring gear **548** is fixedly coupled to output shaft **60**. Ring gear **528** and carrier **542** are fixedly coupled to input shaft **64**. Carrier **512** and sun gear **536** are fixedly held against rotation. A suggested ratio of gear teeth for each planetary gear set in FIG. 8 is listed in Table 13.

TABLE 13

Ring 518/Sun 516	2.00
Ring 528/Sun 526	1.90
Ring 538/Sun 536	1.60
Ring 548/Sun 546	2.30

Intermediate shaft **515** is selectively coupled to input shaft **64** by clutch **550**, selectively coupled to sun gear **526** by clutch **552**, and selectively held against rotation by brake **556**. Ring gear **518** is selectively coupled to carrier **522** and intermediate shaft **62** by clutch **558**. Output shaft **60** is selectively coupled to carrier **532** by clutch **560**. Sun gear **546** is selectively coupled to intermediate shaft **62** by clutch **554**.

As shown in Table 14, engaging the clutches and brakes in combinations of three establishes nine forward speed ratios and one reverse speed ratio between input shaft **64** and output shaft **60**. When the gear sets of FIG. 8 have tooth numbers as indicated in Table 13, the speed ratios have the values indicated in Table 14.

TABLE 14

	550	552	554	556	558	560	Ratio	Step
Rev	X				X	X	-3.25	78%
1 st		X			X	X	4.19	
2 nd		X		X		X	2.48	1.69
3 rd	X	X				X	1.63	1.53
4 th		(X)	X			X	1.19	1.37
5 th	X	X	X				1.00	1.19
6 th		X	X	X			0.87	1.15
7 th		X	X		X		0.79	1.10
8 th			X	X	X		0.70	1.13
9 th	X		X		X		0.61	1.15

While exemplary embodiments are described above, it is not intended that these embodiments describe all possible forms encompassed by the claims. The words used in the specification are words of description rather than limitation, and it is understood that various changes can be made without departing from the spirit and scope of the disclosure. As previously described, the features of various embodiments can be combined to form further embodiments of the invention that may not be explicitly described or illustrated. While various embodiments could have been described as providing advantages or being preferred over other embodiments or prior art implementations with respect to one or

more desired characteristics, those of ordinary skill in the art recognize that one or more features or characteristics can be compromised to achieve desired overall system attributes, which depend on the specific application and implementation. These attributes can include, but are not limited to cost, strength, durability, life cycle cost, marketability, appearance, packaging, size, serviceability, weight, manufacturability, ease of assembly, etc. As such, embodiments described as less desirable than other embodiments or prior art implementations with respect to one or more characteristics are not outside the scope of the disclosure and can be desirable for particular applications.

What is claimed is:

1. A transmission comprising:

input, output, and first intermediate shafts;

a first shiftable gearing arrangement configured to selectively establish at least five speed ratios between the first intermediate shaft and the input shaft, the at least five speed ratios comprising a reverse ratio, a zero ratio, two distinct underdrive ratios, and a direct drive ratio;

a second shiftable gearing arrangement configured to selectively constrain the input shaft to rotate at a speed between speeds of the first intermediate shaft and the output shaft; and

a first fixed gearing arrangement configured to fixedly constrain a sixth element to rotate at a speed between speeds of a fifth element and the first intermediate shaft, wherein the fifth element is coupled to a stationary member and the sixth element is coupled to the output shaft.

2. The transmission of claim 1 wherein the fifth element is fixedly held against rotation; and

a first clutch selectively couples the sixth element to the output shaft.

3. The transmission of claim 1 wherein the sixth element is fixedly coupled to the output shaft; and

a first clutch selectively holds the fifth element against rotation.

4. The transmission of claim 1 wherein the first shiftable gearing arrangement comprises

a second intermediate shaft;

a third shiftable gearing arrangement configured to selectively constrain the first intermediate shaft and second intermediate shaft to rotate in opposite directions or to both be stationary;

a fourth shiftable gearing arrangement configured to selectively constrain the first intermediate shaft to rotate at a speed between the speeds of the input shaft and the second intermediate shaft;

a second clutch selectively coupling the second intermediate shaft to the input shaft; and

a first brake selectively holding the second intermediate shaft against rotation.

5. The transmission of claim 4 wherein the third shiftable gearing arrangement comprises

a simple planetary gear set having a sun gear, a planet carrier fixedly held against rotation, a ring gear fixedly coupled to the first intermediate shaft, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and

a third clutch selectively coupling the sun gear to the second intermediate shaft.

6. The transmission of claim 4 wherein the third shiftable gearing arrangement comprises

a simple planetary gear set having a sun gear fixedly coupled to the second intermediate shaft, a planet

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- carrier fixedly held against rotation, a ring gear, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a third clutch selectively coupling the ring gear to the first intermediate shaft. 5
7. The transmission of claim 4 wherein the fourth shift-able gearing arrangement comprises
 a simple planetary gear set having a sun gear fixedly coupled to the second intermediate shaft, a planet carrier, a ring gear fixedly coupled to the input shaft, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a third clutch selectively coupling the planet carrier to the first intermediate shaft. 10
8. The transmission of claim 4 wherein the fourth shift-able gearing arrangement comprises
 a simple planetary gear set having a sun gear, a planet carrier fixedly coupled to the first intermediate shaft, a ring gear fixedly coupled to the input shaft, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a third clutch selectively coupling the sun gear to the second intermediate shaft. 15
9. The transmission of claim 1 wherein the first shiftable gearing arrangement comprises
 a second fixed gearing arrangement configured to fixedly constrain a second element to rotate at a speed between the speeds of a first element and the intermediate shaft; a third shiftable gearing arrangement configured to selectively constrain the first intermediate shaft to rotate at a speed between the speeds of the second element and the input shaft; 20
 a second clutch selectively coupling the first element to the input shaft; 25
 a first brake selectively holding the first element against rotation; and
 a second brake selectively holding the second element against rotation. 30
 35
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10. The transmission of claim 9 wherein the third shiftable gearing arrangement comprises
 a simple planetary gear set having a sun gear fixedly coupled to the input shaft, a planet carrier, a ring gear fixedly coupled to the second element, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a third clutch selectively coupling the carrier to the first intermediate shaft.
11. The transmission of claim 1 wherein the second shiftable gearing arrangement comprises
 a simple planetary gear set having a sun gear fixedly coupled to the first intermediate shaft, a planet carrier, a ring gear fixedly coupled to the output shaft, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a fourth clutch selectively coupling the planet carrier to the input shaft.
12. The transmission of claim 1 wherein the second shiftable gearing arrangement comprises
 a simple planetary gear set having a sun gear fixedly coupled to the first intermediate shaft, a planet carrier fixedly coupled to the input shaft, a ring gear, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a fourth clutch selectively coupling the ring gear to the output shaft.
13. The transmission of claim 1 wherein the second shiftable gearing arrangement comprises
 a simple planetary gear set having a sun gear, a planet carrier fixedly coupled to the input shaft, a ring gear fixedly coupled to the output shaft, and a plurality of planet gears supported for rotation relative to the planet carrier and in continuous meshing engagement with both the sun gear and the ring gear; and
 a fourth clutch selectively coupling the sun gear to the first intermediate shaft.

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