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(54) **LIQUID OPTICS IN A ZOOM LENS SYSTEM AND IMAGING APPARATUS**

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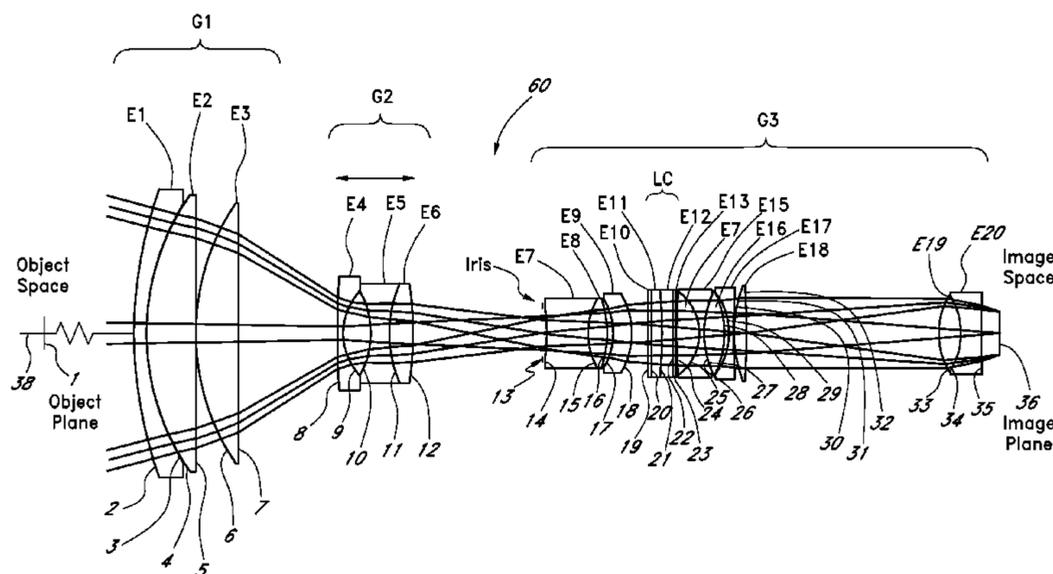
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(57) **ABSTRACT**
A high performance zoom lens system suitable for use with a camera is disclosed. The zoom lens systems includes a movable lens group and a variable power stationary lens group employing liquid optics to provide optical performance over the zoom focal length range at focus distances from close to infinity. The system also provides relatively high quality imaging capability over a wide range of focal lengths and zoom settings.

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20 Claims, 16 Drawing Sheets



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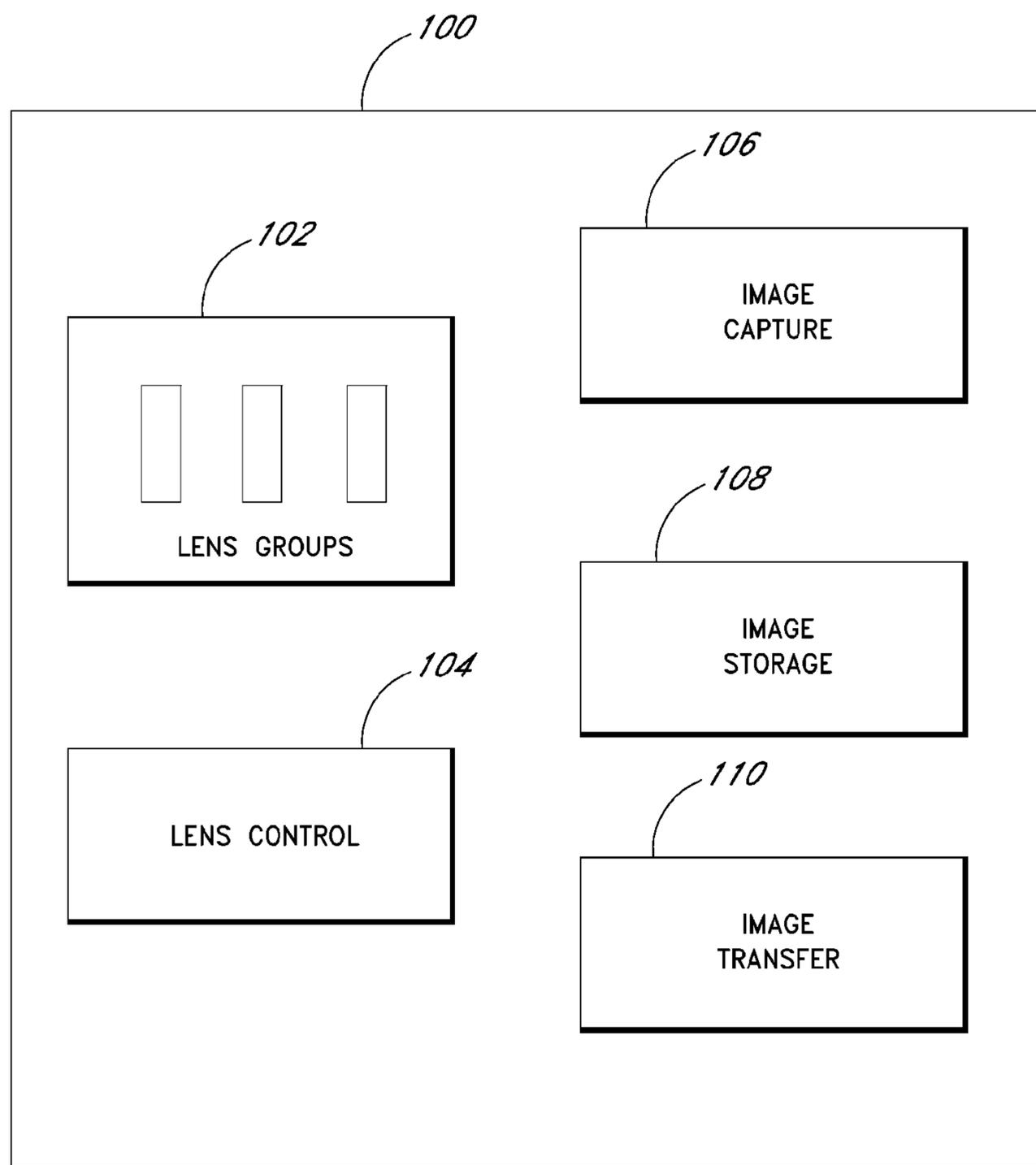
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CAMERA

FIG. 1

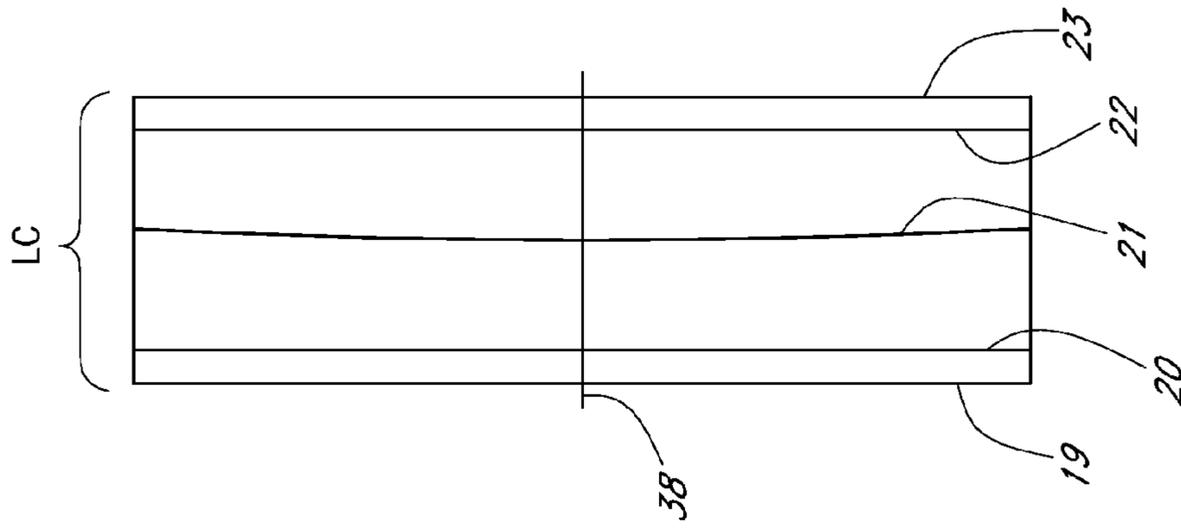


FIG. 3A

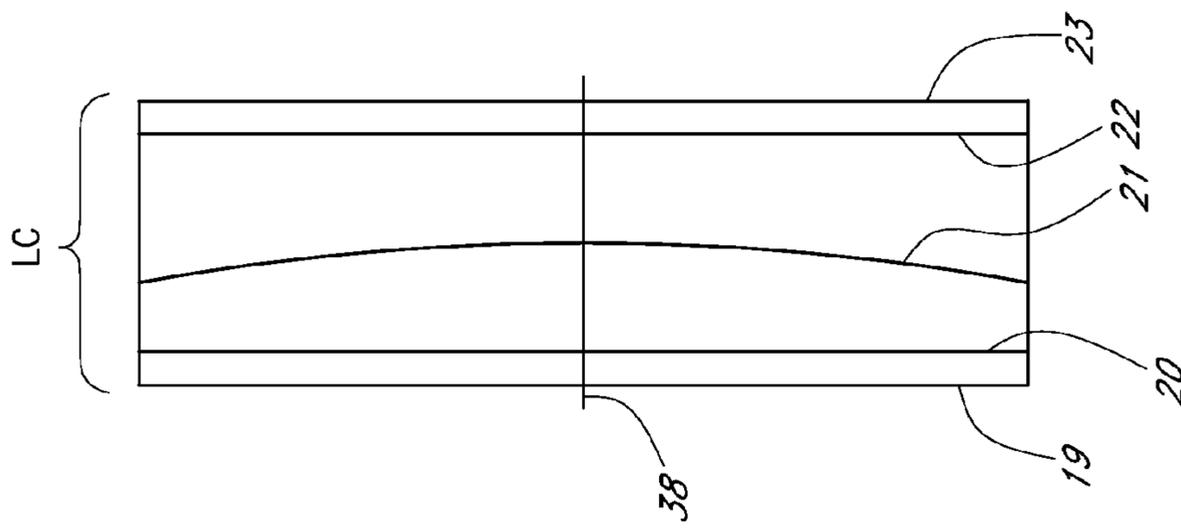


FIG. 3B

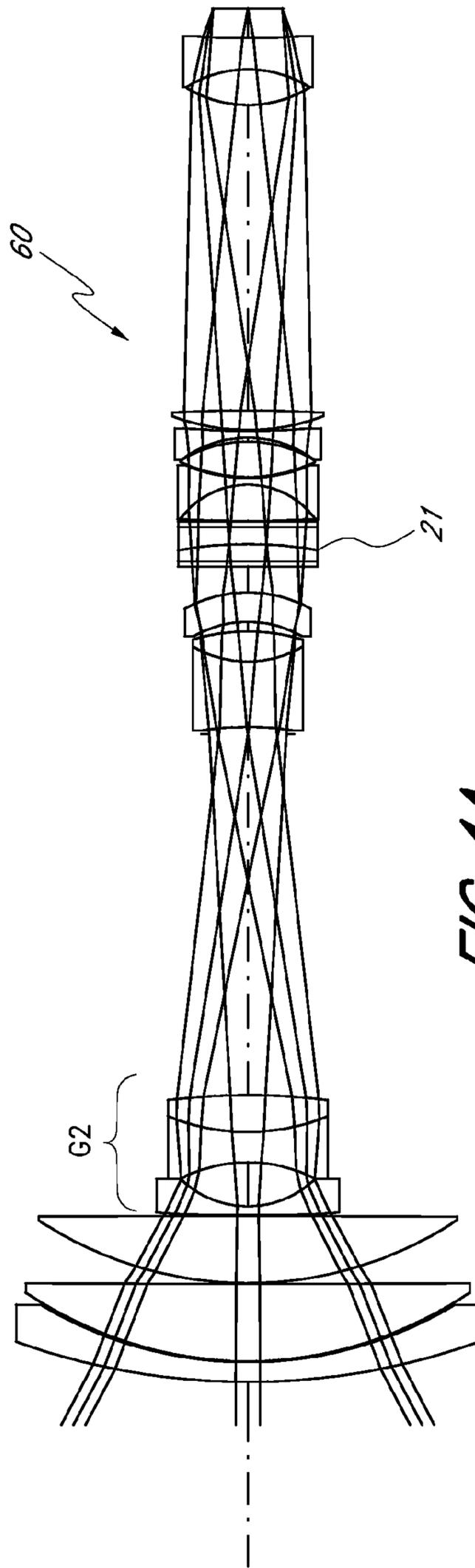
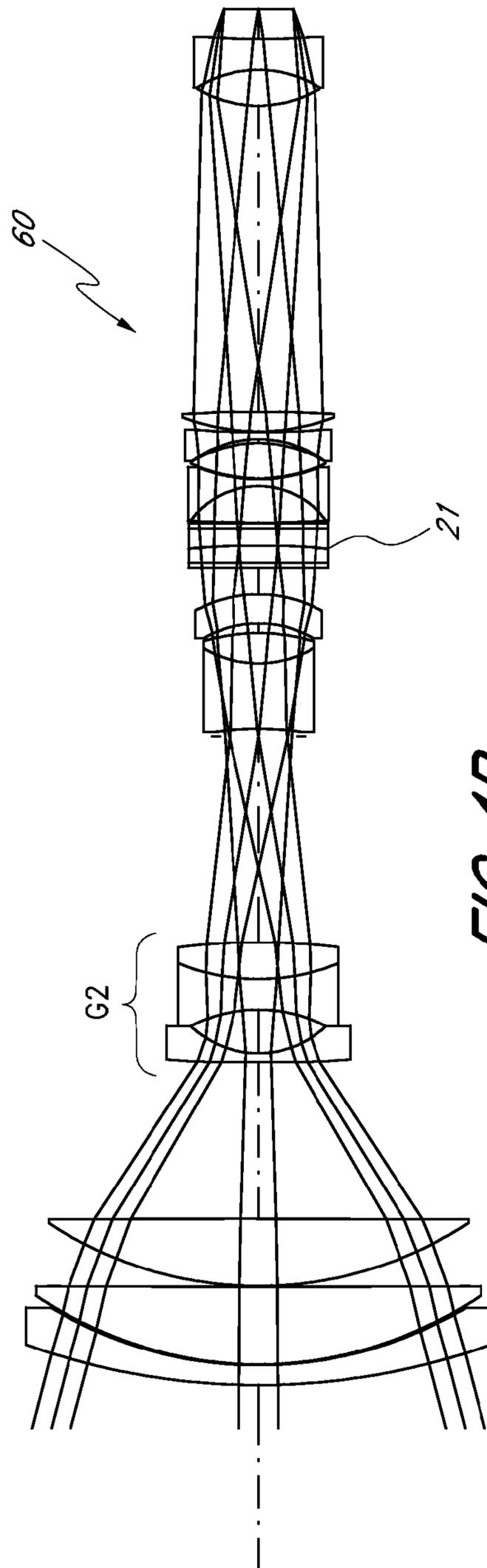


FIG. 4A



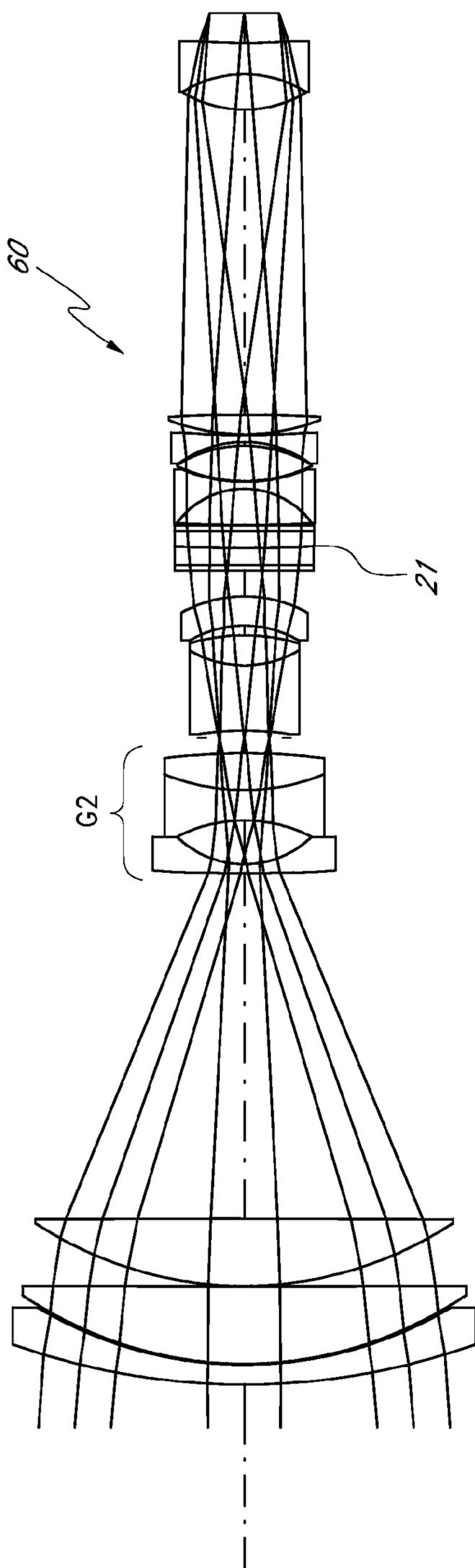
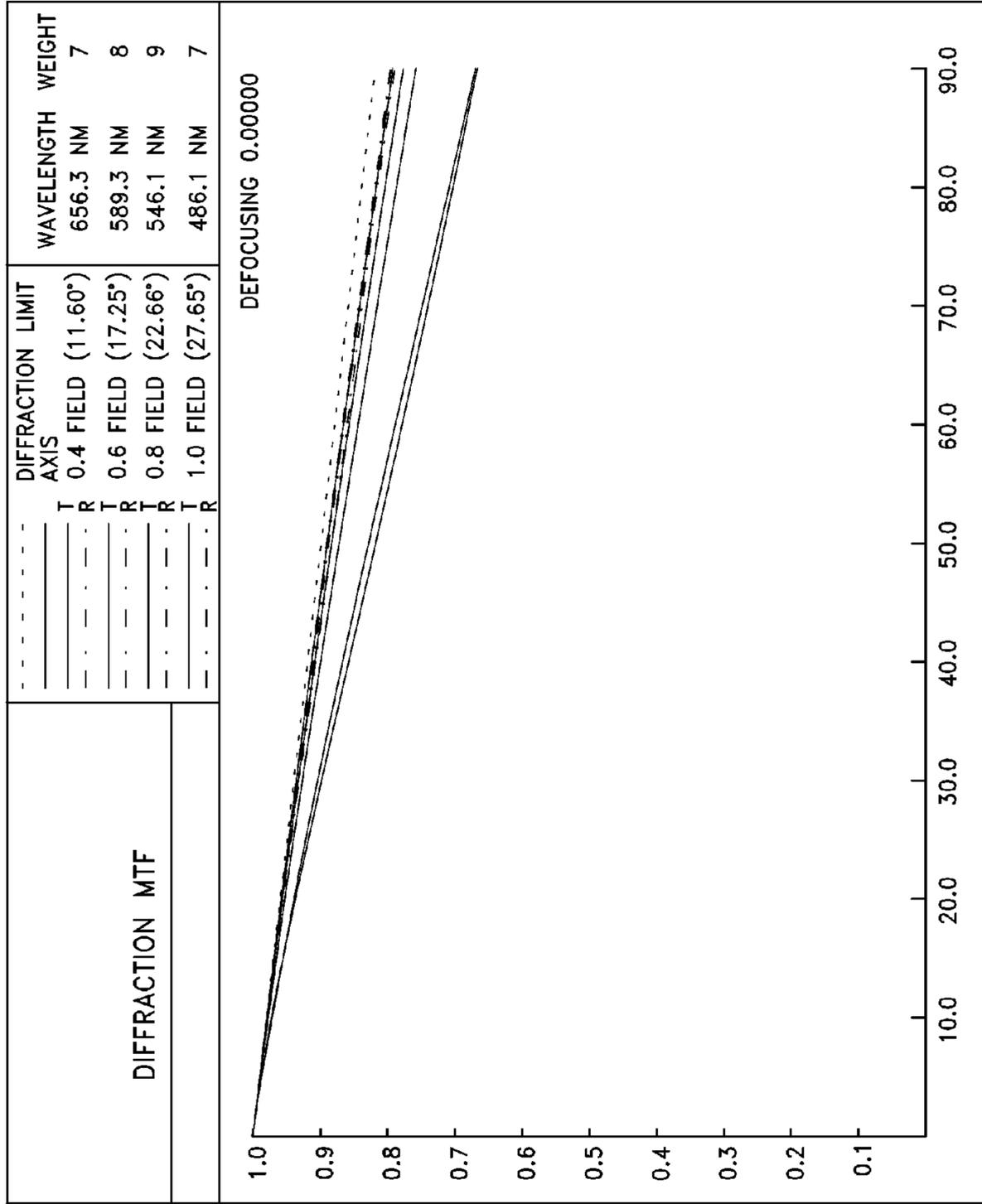


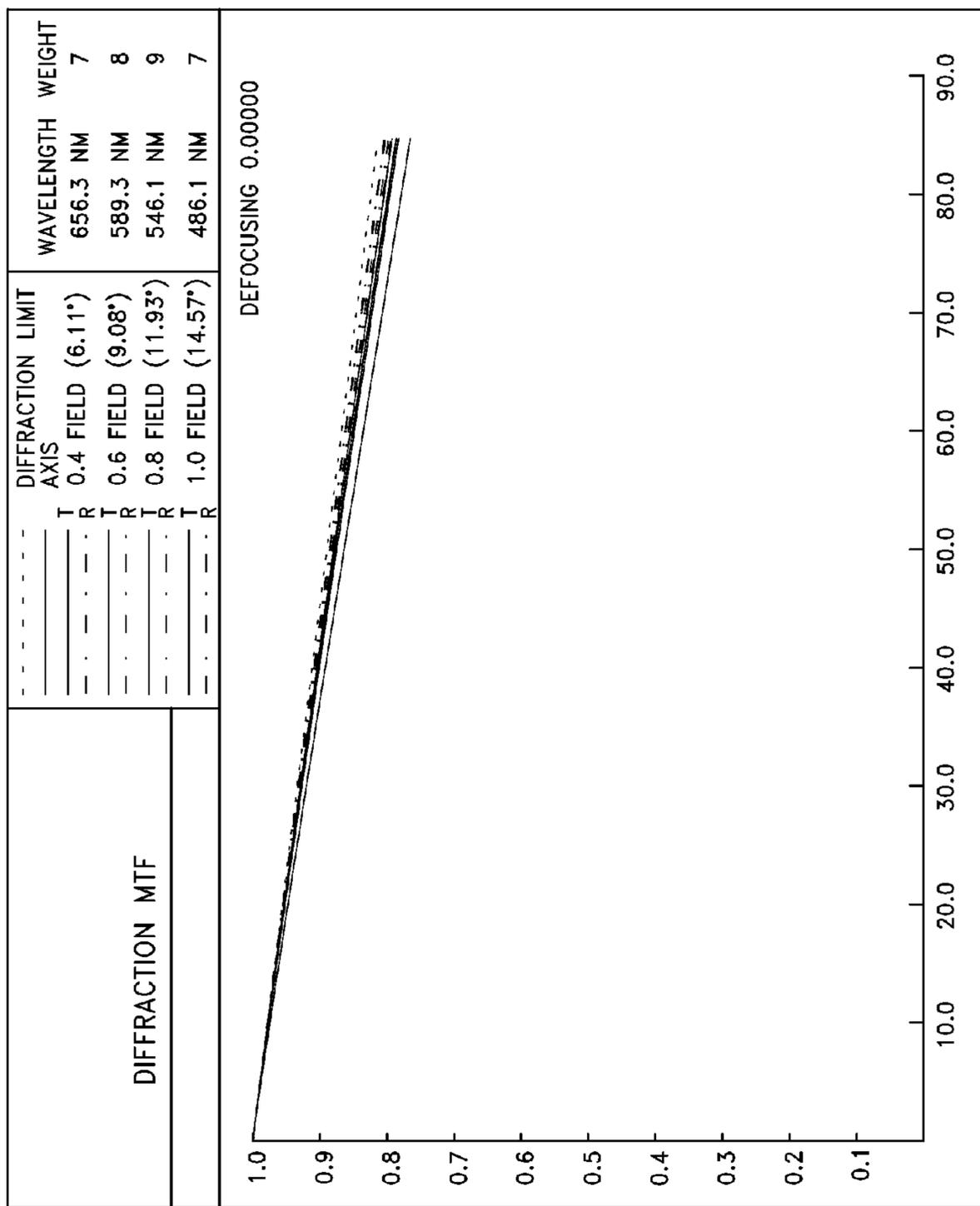
FIG. 4C



SPATIAL FREQUENCY (CYCLES/MM)

FIG. 5A

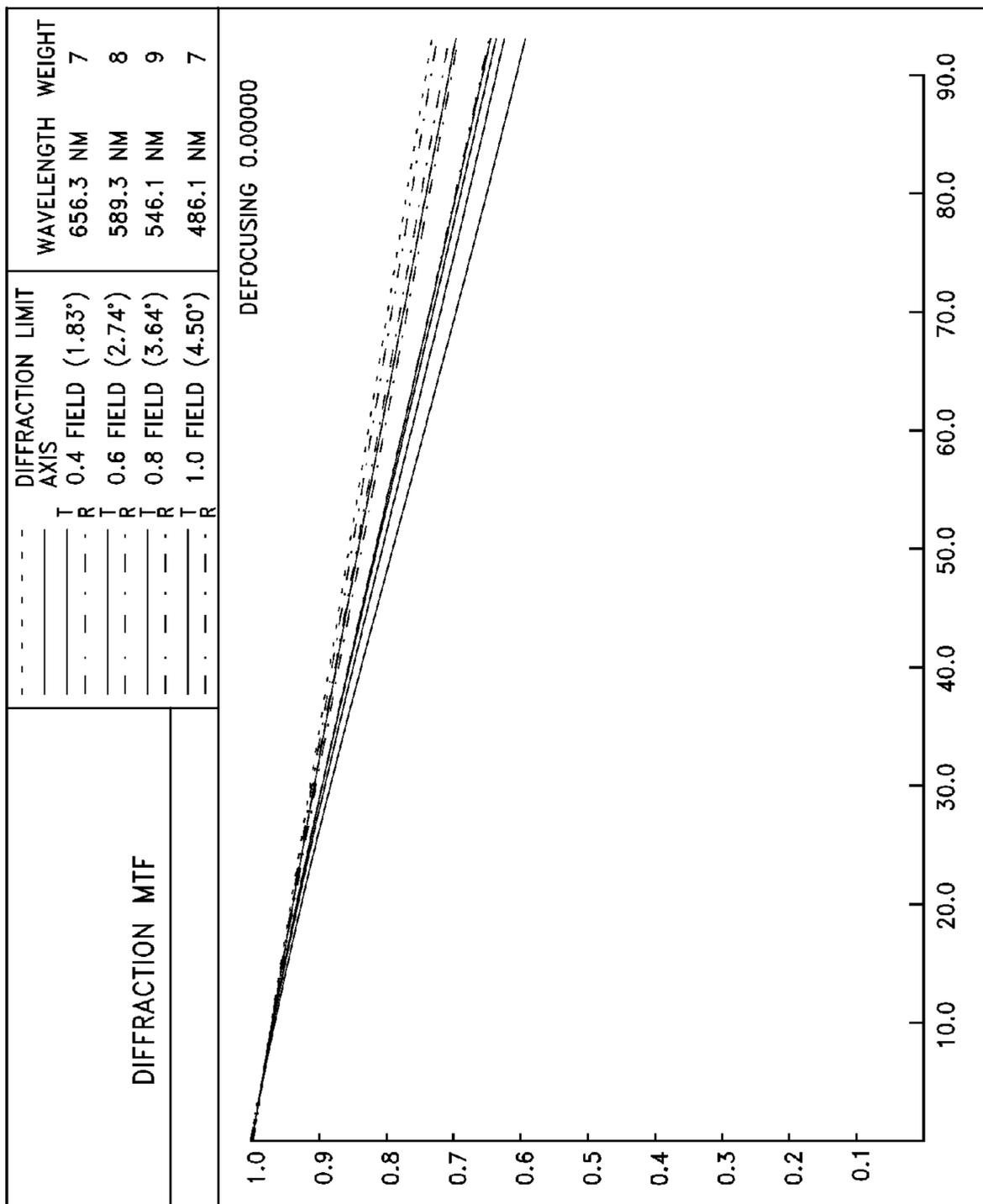
M O D U L A T I O N



SPATIAL FREQUENCY (CYCLES/MM)

FIG. 5B

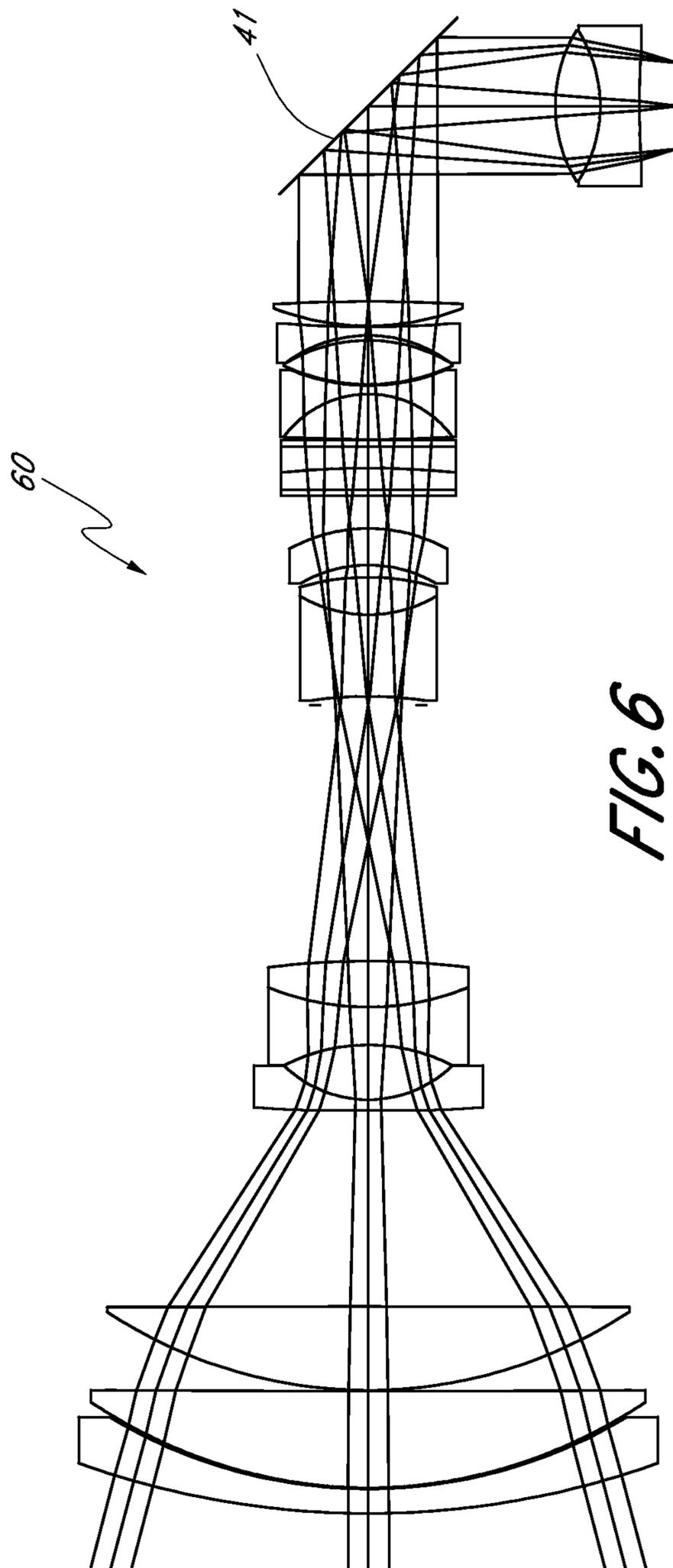
M O D U L A T I O N



SPATIAL FREQUENCY (CYCLES/MM)

FIG. 5C

M O D U L A T I O N



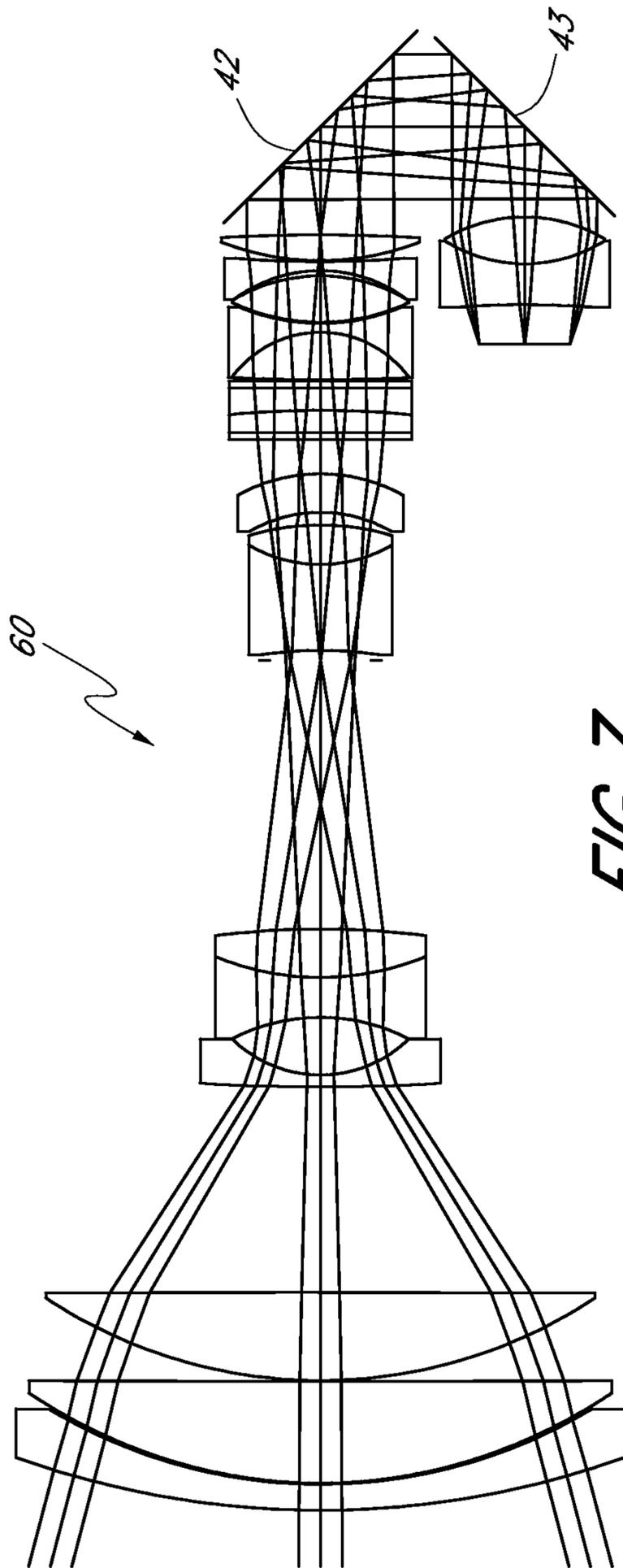
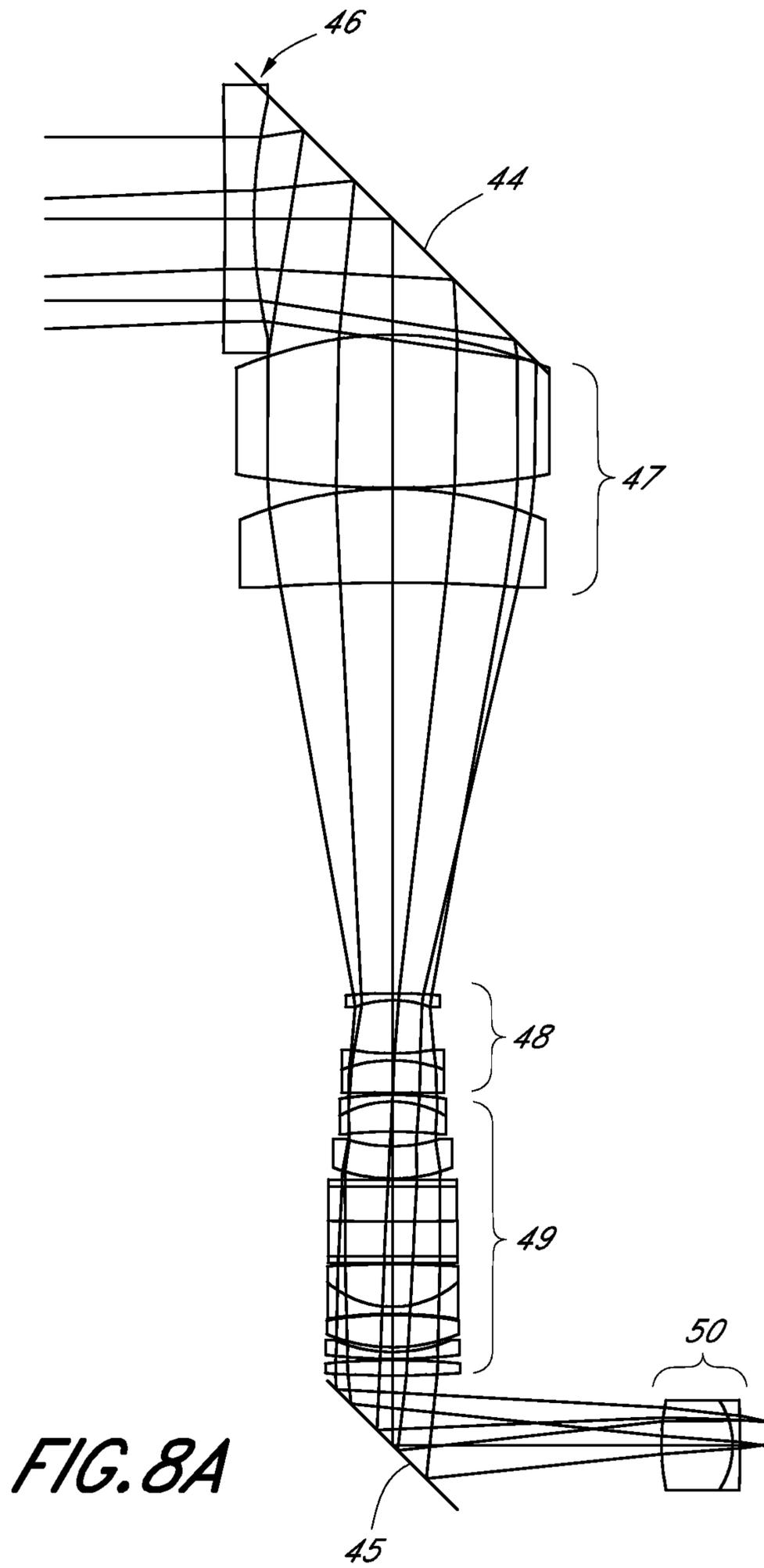


FIG. 7



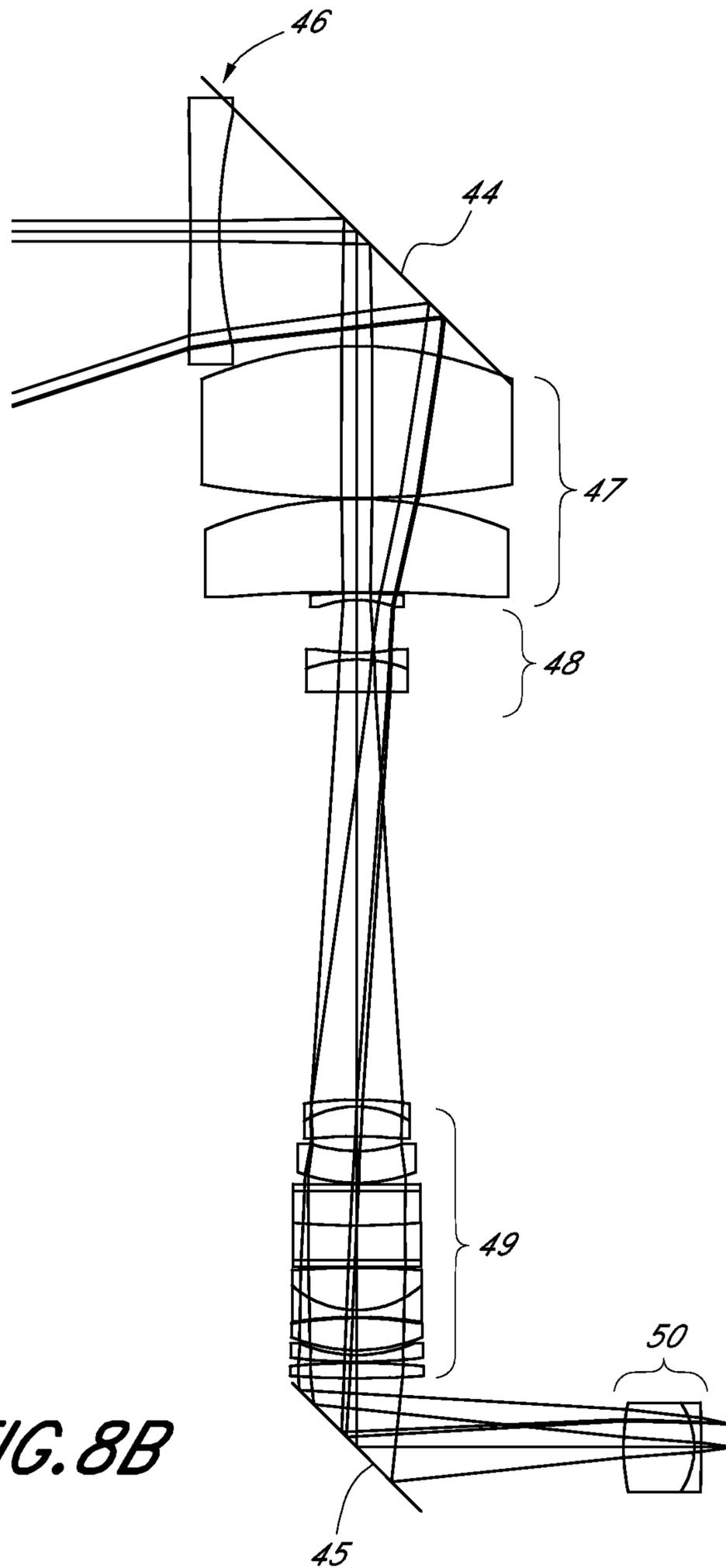


FIG. 8B

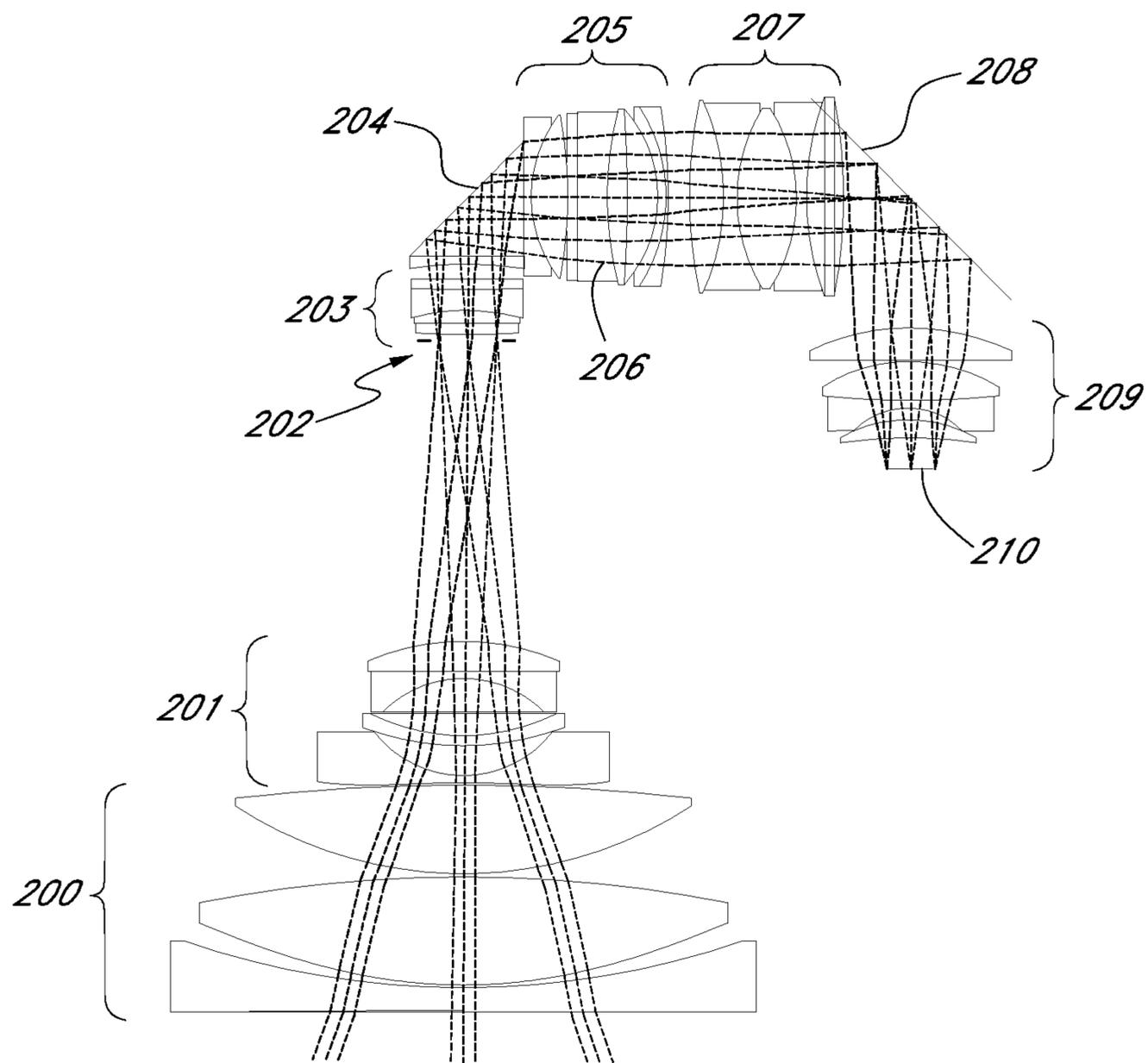


FIG. 9A

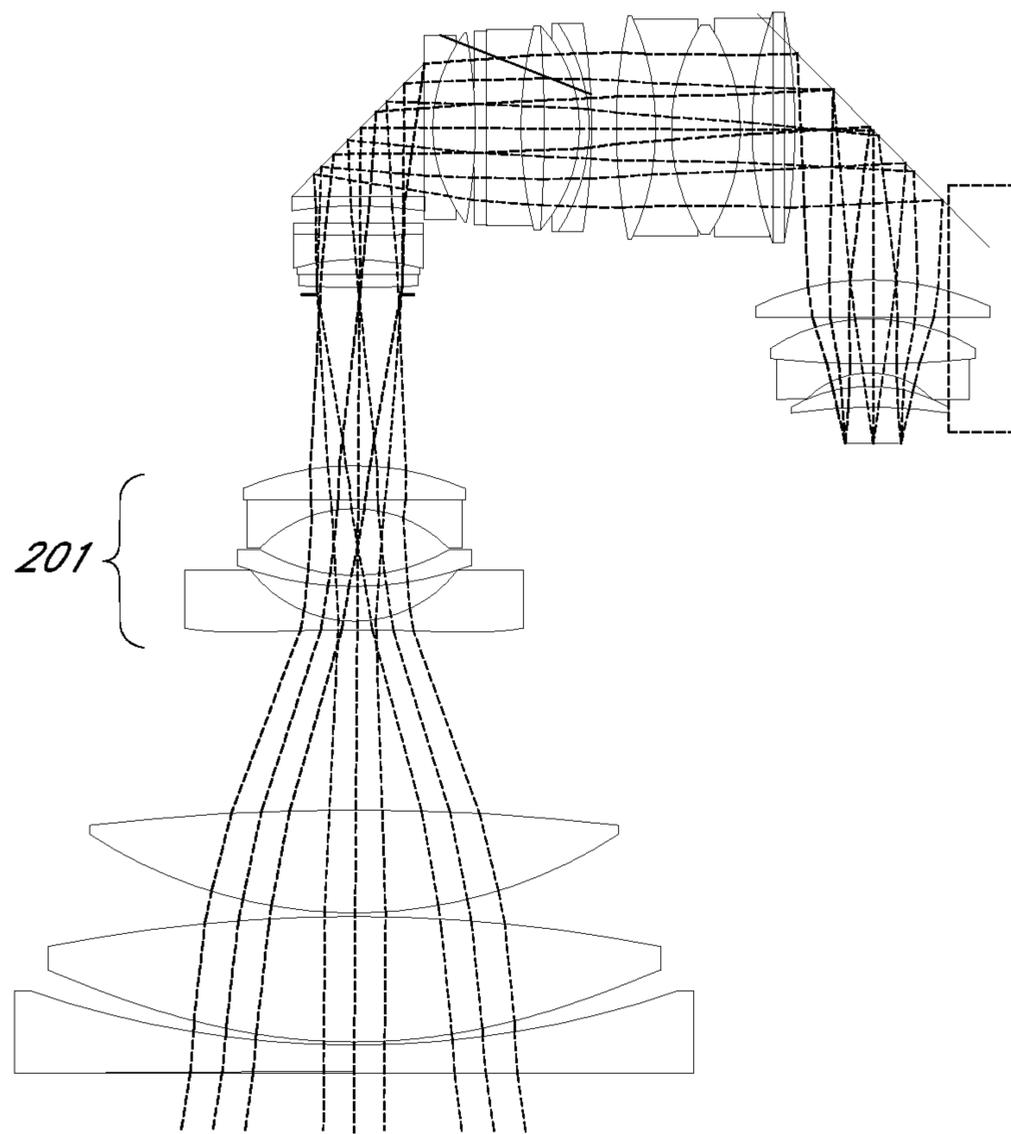


FIG. 9B

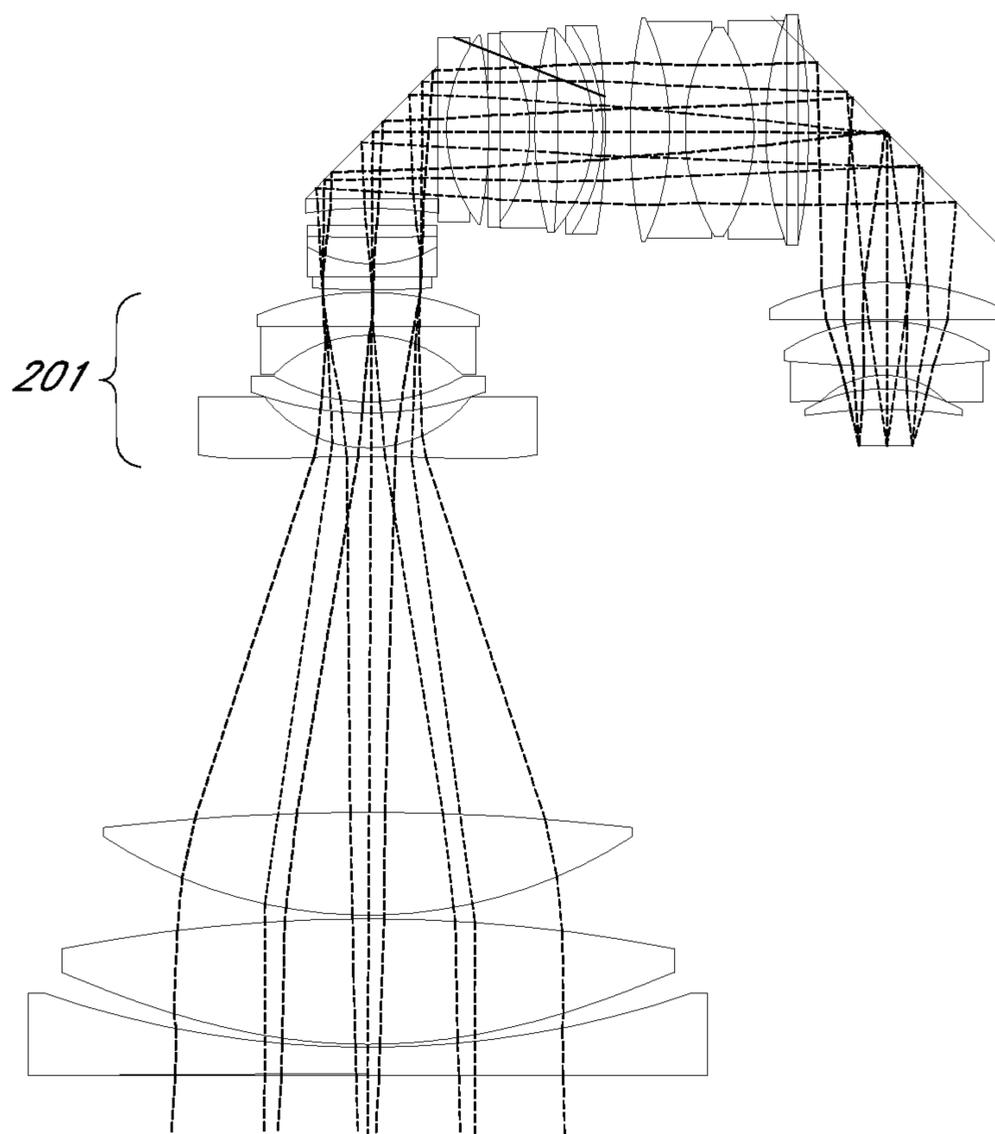


FIG. 9C

LIQUID OPTICS IN A ZOOM LENS SYSTEM AND IMAGING APPARATUS

RELATED APPLICATIONS

This application is a continuation of U.S. patent application Ser. No. 12/327,651, entitled "Liquid Optics with Folds Lens and Imaging Apparatus," filed Dec. 3, 2008, which claims the benefit of U.S. Provisional 60/992,244 filed Dec. 4, 2007, the entirety of which is hereby incorporated by reference herein and made a part of the present specification.

BACKGROUND

Field of the Invention

This invention relates to an optical lens system employing liquid optics and redirection of a radiation axis.

Description of the Related Art

Imaging applications have historically used two or more movable zoom lens groups to provide zooming and different focal lengths. An additional lens group for focusing may also be needed.

However, there are intrinsic disadvantages associated in using zoom and focus lens systems with moving lens groups. In particular, having moving zoom lens groups implies the need for complex mechanically moving parts. Each movable lens group requires support structures and drive mechanics such as cams and motors and in some cases control electronics to facilitate the movements. This system complexity may add size, weight and cost and may make the system operation unreliable over a period of time. These disadvantages together with undesirable limitations, such as a limited range of focal lengths, the inability to focus adequately over the entire focal length range, the inability to focus on close objects, the lack of adequate optical performance over the entire focal length range and focus distance, are present in some previously available zoom lenses having at least two moving zoom lens groups. A mechanically less complex but high performance zoom lens system is needed.

SUMMARY

Liquid lens cells comprise two or more fluids in a chamber. The fluids contact to form a surface that variable by, for example, electrical nodes. A fluid may be, for example, one or more gases, one or more liquids, or a mixture of one or more solids and one or more liquids. Using liquid lens cells to replace one or more moving lens groups results in additional configuration options for the optical path. Replacing moving lens groups with liquid lens cells results in a more compact system. However, a linear optical design may result in a lens that is longer than desired. The use of liquid lens cells instead of a moving group facilitates the use of optical elements such as folds to reduce the physical length of a lens. Although the overall length of the optical path through the lens may remain the same, the liquid lens cells provide strategic space for redirection of the radiation axis that reduces the length in one or more directions. This allows longer overall lens lengths to be used in smaller camera packages. For example, many point and shoot cameras and cell phone cameras do not have large amounts of space for a long lens. Using liquid cells in combination with folds or redirection of the radiation axis allows for better lens systems in these small camera packages. Larger cameras can also benefit from reducing the camera package length that would be required for a lens system that do not redirect the radiation axis.

It should be understood that the embodiments described herein are for explanation purposes, and the scope of the invention is not constrained to the described embodiments.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of a camera.

FIG. 2 is an optical diagram of a zoom lens system employing liquids.

FIGS. 3A and 3B are optical diagrams of the liquid cell of the zoom lens system of FIG. 2 showing the surface shape between the liquids.

FIGS. 4A, 4B and 4C are optical diagrams of the zoom lens system of FIG. 2 illustrating different positions of the zoom lens groups and surface shapes between the liquids to produce different focal lengths and focus distances.

FIGS. 5A, 5B and 5C are modulation transfer function performance diagrams of the zoom lens system of FIGS. 4A, 4B and 4C.

FIG. 6 is an optical diagram of a zoom lens system employing liquids and a single fold.

FIG. 7 is an optical diagram of a zoom lens system employing liquids and a dual fold.

FIGS. 8A and 8B are optical diagrams of a zoom lens system with folds illustrating different positions of the zoom lens group and surface shapes between the liquids.

FIGS. 9A, 9B and 9C are optical diagrams of a zoom lens system illustrating redirection of the radiation axis with different positions of the zoom lens group and surface shapes between the liquids to produce different focal lengths and focus distances.

DETAILED DESCRIPTION

In the following description of preferred embodiments, reference is made to the accompanying drawings that form a part hereof, and in which is shown by way of illustration specific embodiments in which the invention may be practiced. It is to be understood that other embodiments may be utilized and structural changes may be made without departing from the scope of the invention.

U.S. Provisional Patent Application No. 60/783,338 filed on Oct. 8, 2007 and titled "Liquid Optics Zoom Lens and Imaging Apparatus," herein incorporated by reference in its entirety, discloses a zoom lens system that employs liquid optics to provide zoom and focus functionality. The use of liquid optics for zooming and focusing provides for alternative lens configurations with redirection of the radiation axis. An exemplary zoom lens system employing liquid optics to provide zoom and focus functionality is described first, followed by embodiments employing redirection of the radiation axis.

Liquid Optics in a Zoom Lens System

FIG. 1 illustrates a block diagram of a camera **100** with a zoom lens **102**. A zoom lens is an assembly of lens elements with the ability to vary focal length. The individual lens elements may be fixed in place, or slide axially along the body of the lens. A lens group may consist of one or more lens elements. At least one movable lens group provides variation of the magnification of an object. As the at least one lens group moves to accomplish magnification, the position of the focal plane may also move. At least one other movable lens group may move to compensate for the movement of the focal plane to maintain a constant focal plane position. Compensation for the movement of the focal

plane may also be achieved mechanically by moving the complete lens assembly as the magnification of the lens changes.

The individual lens elements may be constructed from solid-phase materials, such as glass, plastic, crystalline, or semiconductor materials, or they may be constructed using liquid or gaseous materials such as water or oil. The space between lens elements could contain one or more gases. For example normal air, nitrogen or helium could be used. Alternatively the space between the lens elements could be a vacuum. When "Air" is used in this disclosure, it is to be understood that it is used in a broad sense and may include one or more gases, or a vacuum.

A zoom lens will often have three or more moving lens groups to achieve the zoom and focusing functions. A mechanical cam may link two movable lens groups to perform zooming, and a third movable lens group may be used for focus.

The zoom range is determined in part by the range of movement for the movable lens elements. Greater zoom ranges require additional space for movement of the lens elements. One or more of the movable lens groups may be replaced by a lens group that implements liquid cell technology. Because liquid cells do not require space for axial movement, the length of the lens design which contains the movable lens groups may be reduced. Alternatively, the space that would have been used for axial movement of the movable lens groups can be used to include additional optical elements or folds. Although a liquid cell does not require space for movement, it may be part of a movable lens group.

A liquid cell may be used for both zooming and focusing. In one embodiment, a movable lens group is used with a lens group that implements liquid cell technology. There is no need for a mechanical cam with one movable lens group. Not having a cam allows for additional movements.

One or more movable lens groups are used with one or more liquid cells to achieve zooming and focusing. A single movable lens group and a single liquid cell can perform both zooming, focusing and compensation for thermal effects. In one implementation, a zoom system has at least a first and second lens group. The first lens group is relatively high power, and the second lens group is relatively low power, the lens power being equivalent to the inverse of the focal length of the lens. The first lens group comprises conventional glass or other solid lenses and the second lens group comprises at least one liquid lens.

A liquid cell uses two or more liquids to form a lens. The focal length of the lens is partly determined by the angle of contact between the liquids and the difference in the refractive index of the liquids. The range of power variation is limited by the difference in the refractive index of the liquids employed and the finite range of radius of curvature at the surface interface between the liquids due to space constraints. U.S. Patent Application Publication No. 2006/0126190, herein incorporated by reference, discloses a lens employing the deformation of a drop of liquid through electrowetting.

Presently contemplated liquid lens systems will have a difference in refractive index of at least about 0.2, preferably at least about 0.3, and in some embodiments at least about 0.4. Water has a refractive index of about 1.3, and adding salt may allow varying the refractive index to about 1.48.

Suitable optical oils may have a refractive index of at least about 1.5. Even by utilizing liquids with higher, lower or higher and lower refractive indices, for example a higher refractive index oil, the range of power variation remains limited. This limited range of power variation usually provides less magnification change than that of a movable lens group. Therefore, in a simple zoom lens system, to provide zooming while maintaining a constant image plane position most of the magnification change may be provided by one movable lens group and most of the compensation of defocus at the image plane during the magnification change may be provided by one liquid cell. However, it should be noted that more movable lens groups or more liquid cells, or both, may be utilized.

The movable lens group can have a positive or negative power. The liquid cell can have a range of variable power where the power is always positive, always negative or goes from positive to negative, or vice versa. Proper arrangement of the movable lens group and the liquid cell provides an extended zoom ratio of greater than 2× and preferably greater than 3× while offering good image quality throughout the zoom range. The arrangement, in addition to zooming, may also provide focusing at different object distances over an extended focus range by utilizing additional available power variation from the liquid cell, the movable lens group or both. This additional power variation provided by the liquid cell or the movable lens group or both for focusing is readily available. Since one movable lens group does not necessarily require a cam with a fixed locus of movement, the position of the movable zoom lens group can be adjusted for zooming and focusing. High performance imaging is achieved by utilizing both the movable zoom lens group and the liquid cell for zooming and focusing.

It is also possible to replace the movable zoom lens group with at least one liquid cell. This would increase the complexity of the optical system and may cause the optical system to have other disadvantages, such as reduced magnification change.

FIG. 1 also illustrates a lens control module 104 that controls the movement and operation of the lens groups in lens 102. The control module 104 includes electronic circuitry that controls the radius of curvature in the liquid lens cell. Electronic circuitry may also control the position of the movable lens group. The appropriate electronic signal levels for various focus positions and zoom positions can be determined in advance and placed in a lookup table. Alternatively, analog circuitry or a combination of circuitry and a lookup table can generate the appropriate signal levels. In one embodiment, a polynomial is used to determine the appropriate electronic signal levels. Points along the polynomial could be stored in a lookup table or the polynomial could be implemented with circuitry.

Thermal effects may also be considered in the control of the radius of curvature of surface between the liquids or the position of movable lens groups or both. The polynomial or lookup table may include an additional variable related to the thermal effects.

The control module 104 may include preset controls for specific zoom settings or focal lengths. These settings may be stored by the user or camera manufacturer.

FIG. 1 further illustrates an image capture module 106 that receives an optical image corresponding to an external object. The image is transmitted along an optical axis through the lens 102 to the image capture module 106. The image capture module 106 may use a variety of formats, such as film (e.g., film stock or still picture film), or electronic image detection technology (e.g., a CCD array,

CMOS device or video pickup circuit). The optical axis may be linear, or it may include folds or other redirection of the radiation axis. It should be understood that a fold as used herein is intended to be interpreted broadly. A variety of optical elements are available that redirect the radiation axis, and the scope of the invention should not be limited to a specific type of optical element.

Image storage module **108** maintains the captured image in, for example, on-board memory or on film, tape or disk. In one embodiment, the storage medium is removable (e.g., flash memory, film canister, tape cartridge or disk).

Image transfer module **110** provides transferring of the captured image to other devices. For example, the image transfer module **110** may use one or a variety of connections such as a USB port, IEEE 1394 multimedia connection, Ethernet port, Bluetooth wireless connection, IEEE 802.11 wireless connection, video component connection, or S-Video connection.

The camera **100** may be implemented in a variety of ways, such as a video camera, a cell phone camera, a digital photographic camera, or a film camera.

An embodiment of a zoom lens will now be described by way of a design example. Referring first to FIG. 2, each lens element is identified by the letter "E" followed by a numeral from 1 through 20 and the general configuration of each lens element is depicted, but the actual radius of each lens surface is set forth below in TABLE 1. The lens, object, stop or iris and image surfaces are identified by a numeral from 1 through 36. The three lens groups are identified in FIG. 2 by the letter "G" followed by a numeral from 1 through 3 and the liquid lens cell is identified by the letters "LC" and comprises optical surfaces **19** through **23**. The optical axis is identified in FIG. 2 by a numeral **38**.

Each lens element has its opposite surfaces identified by a separate but consecutive surface number as, for example, lens element E**1** has lens surfaces **2** and **3**, lens element E**9** has lens surfaces **17** and **18** and so forth, as shown in FIG. 2. The location of the object to be imaged, particularly as it relates to focus distance, is identified by a vertical line and the numeral **1** on the optical axis **38** and the real image surface is identified by the numeral **36**. All of the lens surfaces are spherical or plano except lens surfaces **4** and **8** which are aspheric surfaces that are non-spherical, non-plano but rotationally symmetrical about the optical axis.

Before describing the detailed characteristics of the lens elements, a broad description of the lens groups and their axial positions and movement, and, the liquid lens cell and the variation in surface shape of contacting liquids will be given for the zoom lens system **60**.

The positive or negative power of each lens group is defined as the inverse of the focal length. The resultant optical power of each group of lenses is as follows: the objective lens group G**1** is positive, the zoom lens group G**2** is negative and the rear lens group G**3** is positive, from a lower positive value to a higher positive value as the shape of the surface in the liquid cell is varied. The horizontal arrow with arrowheads on both ends in the upper portion of FIG. 2 indicates that the zoom lens group G**2** is movable in both axial directions.

While only the lens elements are physically shown in FIG. 2, it is to be understood that mechanical devices and

mechanisms are provided for supporting the lens elements and for causing axial movement of the movable zoom lens group in a lens housing or barrel. In addition, it is to be understood that electronic circuitry changes the profile of the variably shaped optical surface in the liquid lens cell.

The lens construction and fabrication data for the above described zoom lens system **60** is set forth below in TABLE 1. The data in TABLE 1 is given at a temperature of 25° C. (77° F.) and standard atmospheric pressure (760 mm Hg). Throughout this specification measurements are in millimeters (mm) with the exception of wavelengths which are in nanometers (nm). In TABLE 1, the first column "Item" identifies each optical element and each location, i.e. object plane, image plane, etc., with the same numeral or label as used in FIG. 2. The second column identifies the "Group" to which that optical element (lens) belongs with the same numerals used in FIG. 2. The third column "Surface" is a list of the surface numbers of the object (line "1" in FIG. 2 and "Object" in TABLE 1), the Stop (iris) **13** and each of the actual surfaces of the lenses, as identified in FIG. 2. The fourth column "Focus Position" identifies three typical focus positions (F**1**, F**2** and F**3**) for the zoom lens system **60** wherein there are changes in the distance (separation) between some of the surfaces listed in the third column and there are changes in the radius of curvature of the surface **21** listed in the third column, as described below more thoroughly. The fifth column "Separation" is the axial distance between that surface (third column) and the next surface. For example, the distance between surface S**2** and surface S**3** is 1.725 mm.

The sixth column, headed by the legend "Radius of Curvature," is a list of the optical surface radius of curvature for each surface, with a minus sign (-) meaning the center of the radius of curvature is to the left of the surface, as viewed in FIG. 2 and "Infinity" meaning an optically flat surface. The asterisk (*) for surfaces **4** and **8** indicate these are aspheric surfaces for which the "radius of curvature" is a base radius. Use of aspherical surfaces provides for the correction of aberrations in the zoom lens while enabling a smaller overall size and a simpler configuration. The formula and coefficients for the surface profiles of aspheric surfaces **4** and **8** are governed by the following equation:

$$z = \frac{cy^2}{1 + [1 - (1 + \kappa)c^2y^2]^{1/2}} + Ay^4 + By^6 + Cy^8 + Dy^{10} + Ey^{12} + Fy^{14}$$

where:

c=surface curvature (c=1/r where r is the radius of curvature)

y=radial aperture height of surface measured from the X and Y axis, where:

$$y=(X^2+Y^2)^{1/2}$$

κ=conic coefficient

A, B, C, D, E, F=4th, 6th, 8th, 10th, 12th and 14th, respectively, order deformation coefficients

z=position of a surface profile for a given y value or measured along the optical axis from the pole (i.e., axial vertex) of the surface

7

The coefficients for surface 4 are:

$$\begin{aligned}\kappa &= -0.6372 \\ A &= +0.9038 \times 10^{-6} \\ B &= +0.2657 \times 10^{-8} \\ C &= -0.1105 \times 10^{-10} \\ D &= +0.4301 \times 10^{-13} \\ E &= -0.8236 \times 10^{-16} \\ F &= +0.6368 \times 10^{-19}\end{aligned}$$

The coefficients for surface 8 are:

$$\begin{aligned}\kappa &= +0.0000 \\ A &= +0.5886 \times 10^{-4} \\ B &= -0.5899 \times 10^{-6} \\ C &= +0.8635 \times 10^{-8} \\ D &= -0.5189 \times 10^{-10} \\ E &= -0.1186 \times 10^{-11} \\ F &= +0.1631 \times 10^{-13}\end{aligned}$$

Columns seven through nine of TABLE 1 relate to the “Material” between that surface (third column) and the next surface to the right in FIG. 2, with the column “Type” indicating whether there is a lens (Glass) or empty space (Air) or liquid lens (Liquid) between those two surfaces. The glass and liquid lenses are identified by optical glass or liquid in the column “Code”. For convenience, all of the lens glass has been selected from glass available from Ohara Corporation and the column “Name” lists the Ohara iden-

8

tification for each glass type, but it is to be understood that any equivalent, similar or adequate glass may be used. Also, the lens liquid of oil has been selected from a liquid available from Cargille Laboratories, Inc., and water is commonly available from various sources, but it is to be understood that any equivalent, similar or adequate liquid may be used. The water liquid at surface 20 has the following refractive indices 1.331152, 1.332987, 1.334468 and 1.337129 at respective wavelengths 656.27, 589.29, 546.07 and 486.13 nanometers. The oil liquid at surface 21 has the following refractive indices 1.511501, 1.515000, 1.518002 and 1.523796 at respective wavelengths 656.27, 589.29, 546.07 and 486.13 nanometers.

The last column of TABLE 1 headed “Aperture Diameter” provides the maximum diameter for each surface through which the light rays pass. All of the maximum aperture diameters, except for the Stop surface 13, are given at a wavelength of 546.1 nanometers for a maximum image diameter of about 6 mm and F-numbers of F/2.8 to F/4.0 at the Image Plane, for all Zoom and Focus Positions. The maximum aperture diameter of the Stop surface 13 is given in TABLE 1 at a wavelength of 546.1 nanometers and an F-number of F/2.8 at the Image Plane for Zoom Position Z1 and Focus Position F1. At the Image Plane 36, the Maximum Aperture Diameter is given as an approximate value.

TABLE 1

Optical Prescription										
Item	Group	Surface	Focus		Radius of Curvature (mm)	Material			Aperture Diameter (mm)	
			Position	Separation		Type	Name	Code		
Object		1	F1	Infinity	Infinity	Air				
			F2	1016.2500						
			F3	378.7500						
E1	G1	2	All	1.7250	59.1716	Glass	SLAM66	801350	37.161	
				All	0.0750	34.5954	Air			35.567
E2	G1	4	All	6.7565	*33.0488	Glass	SFPL51	497816	35.618	
				All	0.0750	2758.9929	Air			35.182
E3	G1	6	All	5.8657	32.7151	Glass	SFPL53	439950	33.680	
				F1	TABLE 2	-2981.4301	Air			33.034
				F2	TABLE 2					
E4	G2	8	All	0.7652	*461.6464	Glass	SLAH64	788474	14.273	
				All	3.8333	8.3339	Air			11.605
				All	2.6582	-12.6370	Glass	SFPL53	439950	11.587
E5	G2	10	All	3.2165	18.1883	Glass	SLAM66	801350	12.383	
E6	G2	12	F1	TABLE 3	-55.4718	Air			12.337	
				F2	TABLE 3					
				F3	TABLE 3					
Stop/ Iris	G3	13	All	0.6371	Infinity				6.708	
E7	G3	14	All	5.7168	-26.3844	Glass	SLAH65	804466	6.757	
E8	G3	15	All	2.6250	9.3177	Glass	STIH53	847238	8.304	
				All	0.8432	-16.3366	Air			8.533
E9	G3	17	All	2.5647	-9.2859	Glass	SLAH58	883408	8.508	
				All	2.2767	-11.1961	Air			9.665
E10	G3	19	All	0.4500	Infinity	Glass	SBSL7	516641	10.151	
E11	G3	20	All	1.5000	Infinity	Liquid	WATER		10.201	
E12	G3	21	F1	1.5000	TABLE 4	Liquid	OIL	T300	10.367	
								04091- AB		
				F2	TABLE 4					
E13	G3	22	All	0.4500	Infinity	Glass	SBSL7	516641	10.584	
				All	0.0750	Infinity	Air			10.642
E14	G3	24	All	3.1583	120.2680	Glass	SLAH65	804466	10.680	
E15	G3	25	All	0.6000	-7.2241	Glass	STIH10	728285	10.724	
				All	0.0750	13.8153	Air			10.634
E16	G3	27	All	3.0844	13.7118	Glass	SBSM10	623570	10.696	
				All	0.3424	-11.1618	Air			10.713
E17	G3	29	All	0.6000	-9.5071	Glass	STIH13	741278	10.652	
				All	0.0750	68.8748	Air			11.180

TABLE 1-continued

Optical Prescription									
Item	Group	Focus		Separation	Radius of Curvature (mm)	Material			Aperture Diameter (mm)
		Surface	Position			Type	Name	Code	
E18	G3	31	All	1.7063	18.2078	Glass	SLAL13	694532	11.589
		32	All	26.6908	-115.6915	Air			11.592
E19	G3	33	All	3.1085	10.2784	Glass	SNPH1	808228	9.888
E20	G3	34	All	2.7193	-9.9003	Glass	SLAH58	883408	9.581
		35	All	2.6192	58.0014	Air			7.805
Image		36	All	0.0000	Infinity	Air			6.008

Zoom lens system **60** is provided with an optical stop at the surface **13** which controls the diameter of the aperture through which light rays may pass at that point. The optical stop is the location at which a physical iris (or diaphragm) is located. The iris is located before the rear lens group **G3** and is axially stationary with that lens group. Note that in FIG. **4A**, the rim rays pass through the axis side of the tic marks of the optical stop surface **13** such that the zoom lens system has no vignetting of light beams at any field position, zoom position and focus position. However, note that the F-number varies through zoom and focus positions and the iris opens or closes accordingly. The diameter of the iris at zoom positions **Z1-Z8** for focus position **F1** is 6.71, 6.39, 5.96, 5.53, 5.18, 4.84, 4.63 and 4.61. This shows that the iris located at **13** should close as the focal length increases. As compared to focus position **F1**, the diameter of the iris at zoom positions **Z1-Z8** for focus positions **F2** and **F3** changes by a small amount of less than 0.3 mm diameter to maintain the same F-numbers as for focus position **F1**.

Referring to TABLE 1, for illustrating the scope and versatility of the design there are eight different Zoom Positions **Z1, Z2, Z3, Z4, Z5, Z6, Z7** and **Z8** and three

different Focus Positions **F1, F2** and **F3** set forth in the data which, in effect, provides specific data for twenty four (8×3=24) different combinations of positions for the movable zoom lens group **G2** and the variable shape optical surface **21**.

The focal lengths of zoom lens system **60** for zoom positions **Z1-Z8** at focus position **F1**, at a wavelength of 546.1 nanometers are; 5.89, 7.50, 11.25, 15.00, 18.75, 30.00, 41.25 and 45.00 mm, respectively. The corresponding F-numbers for the focal lengths for data positions **Z1-Z8**, at a wavelength of 546.1 nanometers are; 2.80, 2.90, 3.05, 3.25, 3.45, 3.70, 3.95 and 4.00, respectively.

For Focus Position **F1** the Object Plane **1** is assumed to be at infinity, for **F2** the Object Plane **1** is at an intermediate distance of about 1016.25 mm, and for **F3** the Object Plane **1** is at a close distance of about 378.75 mm (i.e., 378.75 mm away from the image plane). At each of these three Focus Positions **F1, F2** and **F3**, the lens groups **G1** and **G3** remain in the same position throughout the full range of movement of the zoom lens group **G2**. TABLES 2 and 3 provide separation values of surfaces **7** and **12** and TABLE 4 provides the radii of curvature of surface **21** for zoom positions **Z1-Z8** and **F1-F3**.

TABLE 2

Separation Values for Surface 7									
Surface	Focus	Z1	Z2	Z3	Z4	Z5	Z6	Z7	Z8
7	F1	0.0832	5.7132	13.7126	18.4633	21.6974	27.4007	30.5400	31.3096
7	F2	0.0902	5.7486	13.6468	18.3289	21.5154	27.0776	30.0174	30.7361
7	F3	0.0750	5.6942	13.4674	18.1217	21.3355	26.7467	29.5798	30.2701

TABLE 3

Separation Values for Surface 12									
Surface	Focus	Z1	Z2	Z3	Z4	Z5	Z6	Z7	Z8
12	F1	31.5294	25.8992	17.8996	13.1486	9.9140	4.2101	1.0701	0.3000
12	F2	31.5178	25.8581	17.9590	13.2762	10.0892	4.5268	1.5870	0.8729
12	F3	31.5324	25.9120	18.1380	13.4831	10.2689	4.8577	2.0248	1.3384

TABLE 4

Radii of Curvature for Surface 21									
Surface	Focus	Z1	Z2	Z3	Z4	Z5	Z6	Z7	Z8
21	F1	-33.9902	-40.9700	-60.9667	-84.8892	-106.7630	-101.7297	-58.3998	-48.6792
21	F2	-34.3890	-42.0587	-65.5384	-101.1799	-154.9184	-370.2777	-263.5374	-212.3139
21	F3	-35.0134	-43.6001	-72.6330	-133.7178	-351.2333	214.4454	125.5481	115.8049

It will be understood that continuous focusing is available between the extreme Focus Positions F1 and F3, that continuous zooming is available between the extreme Zoom Positions Z1 and Z8, and that any combination of continuous focusing and zooming is available within the described focus and zoom ranges with the lens system 60.

The zoom lens system 60 shown in FIG. 2 and prescribed in TABLE 1 has focal lengths for lens groups G1 and G2 of 54.30 and -12.25 mm respectively. Also, lens group G3, due to the variable shape of the optical surface 21 between the liquids, has a variable focal length which has a minimum value of +30.18 mm and a maximum value of +38.97 mm at zoom position Z1 and focus position F1, and, zoom position Z8 and focus position F3 respectively. The liquid cell LC of zoom lens system 60 is shown in FIGS. 3A and 3B, demonstrating the two extreme radii of curvature from TABLE 1 of the variable shape optical surface 21 between the liquids. In FIGS. 3A and 3B the two radii of curvature of surface 21 are about -33.99 and +115.80 mm respectively. The two extreme focal lengths of the liquid cell LC, in FIGS. 3A and 3B, are -185.20 and 630.97 mm respectively. This difference happens at zoom position Z1 and focus position F1, and, zoom position Z8 and focus position F3. In this embodiment the volume of the two liquids between surfaces 20, 21 and 21, 22 varies as the shape of the variable surface changes. However, it is also possible to maintain a constant volume for each liquid by applying small, equal but opposite, changes to the axial separation between surfaces 20, 21 and 21, 22.

Referring now to FIGS. 4A, 4B, and 4C, the zoom lens system 60 is shown with the zoom lens group in various positions, the shape of the variable surface in the liquid cell in various positions and with light ray traces for those positions. FIG. 4A represents the focus position F1 and zoom position Z1 for which data is set forth above in TABLE 1 with infinity focus and a small focal length of about 5.9 mm. FIG. 4B represents the focus position F2 and zoom position Z3 from TABLE 1 with an intermediate focus and a focal length of about 11.3 mm. FIG. 4C represents the focus position F3 and zoom position Z8 from TABLE 1 with close focus and a focal length of about 44.8 mm.

FIGS. 4A, 4B and 4C show three axial locations of the zoom lens group G2 with corresponding three surface shapes for the variable optical surface 21 for the respective zoom and focus positions; Z1, F1 and Z3, F2 and Z8, F3.

The optical performance of zoom lens system 60 is given in FIGS. 5A, 5B and 5C wherein the diffraction based polychromatic modulation transfer function ("MTF") data (modulation versus spatial frequency) is shown in percent (%) for five different Field Positions in three different combinations of the zoom and focus positions set forth in TABLE 1, namely (Z1, F1), (Z3, F2) and (Z8, F3) which are representative examples. The Field Positions are set forth in two values, both the normalized image height (mm) and the actual object space angle (degree) from the optical axis. The MTF percentages are at the wavelengths and weightings set forth in the top right-hand corner of FIGS. 5A, 5B and 5C and are graphically shown for tangential (T) and radial (R) directions of measurement at the image plane 36. Note that the tangential and radial values are equal at the axial field position (AXIS) and are depicted with only one plot. The maximum spatial frequency shown is 90 cycles/mm which given the image diameter of about 6 mm and choice of detector pixel size may provide high quality images at least up to high definition television (HDTV) resolution, namely 1920 pixels horizontally by 1080 pixels vertically. MTF at a spatial frequency is a relatively standard measurement of

optical performance, wherein the value "90 cycles/mm" means 90 pairs of black and white lines per millimeter on a chart from which the clarity is determined. The highest MTF value is about 89% at the full radial field for zoom position Z1 and focus position F2. The lowest MTF value is about 58% at the full tangential field for zoom position Z8 and focus position F3. The minimum relative illumination is about 75% at zoom position Z1 and focus position F1. In general, higher relative illumination values are better, because a low number means that light is falling off in the corners of the picture. High full field relative illumination is preferred for state of the art detectors, which have a constant response to light in all areas and will faithfully reproduce shading in the corners of the image along with changes to the image during zooming. Illumination less than 50% may result in shading in an electronic detector, but will likely be acceptable for film. The highest positive distortion is +3.04% at zoom position Z3 and focus position F1 and the lowest negative distortion is -2.98% at zoom position Z1 and focus position F3. The so-called "breathing" problem of lenses in general (but which may be more prevalent in zoom lenses) wherein the image changes size from far to close focus is virtually absent in zoom lens system 60 at the short focal length of the zoom range where it is most noticeable due to the large depth of field. The lowest breathing is -0.2% at zoom position Z1 and focus position F3 and the highest breathing is -19.5% at zoom position Z8 and focus position F3. Breathing is the percentage change in maximum field angle from infinity focus to a selected focus. Accordingly, at infinity focus (F1), breathing is zero because that is the reference field of view.

All of the performance data is given at a temperature of 25° C. (77° F.), standard atmospheric pressure (760 mm Hg), and at the full apertures available in the zoom lens system 60. However, the zoom lens system 60 does provide substantially constant performance, as for example the MTF values, over a temperature range of 0° to 40° C. (32° to 104° F.) and, if a small degradation in performance (MTF) is acceptable, the operable temperature range can be extended to -10° to 50° C. (14° to 122° F.) or more. For a change in temperature the optimum performance may be achieved by further axial adjustment of the zoom lens group G2 or further change of shape of the contacting optical surface 21 or a combination of both together. This may happen at all zoom and focus positions. At low temperatures of about 0° C. (32° F.) or below, to avoid freezing (forming a solid), the liquids may need to be heated or be replaced with doped liquids in a similar way to anti-freeze being added to water in a car radiator for low temperature operation. However, note that these material temperature changes preferably should not significantly change the optical characteristics of the liquids.

While the described embodiment using zoom lens system 60 is of the appropriate dimensions for use with a 6 mm diameter (so called third inch chip sensor), the dimensions of this zoom lens system may be appropriately scaled up or down for use with various film and electronic detector image formats.

Liquid lens cells may have a limited clear aperture diameter. If a sufficiently small detector is used, the liquid lens cell may be located near the detector. Alternatively, the liquid lens cell may be located near an intermediate image where the light beam "waist" is sufficiently narrow. The liquid lens cell could be placed before the intermediate image, after the intermediate image, or liquid lens cells could be placed both before and after the intermediate image. The waist effect can happen near the stop or the iris.

As shown in Table 2, the diameter at the iris is approximately 6.7 mm. Because of the small diameter at the stop or iris, it may be appropriate to place a liquid lens cell in the vicinity of the stop or iris.

Among the many advantages of the zoom lens system **60** is that of providing zooming over a wide range of focal lengths utilizing only one axially moving zoom lens group. The design of the zoom lens system **60** creates a high performance and mechanically less complex lens system than most conventional high performance zoom lens systems which require at least two axially movable zoom lens groups and corresponding mechanics. The unique lens design of the zoom lens system **60** provides focusing over a large region of focus distance without additional movable lens groups and corresponding mechanics. The disclosed design of zoom lens system **60** is exemplary, and other designs will fall within the scope of the invention. Other features and advantages of the zoom lens system **60** will appear to those skilled in the art from the foregoing description and the accompanying drawings.

Liquid Optics and Redirection of the Radiation Axis in a Zoom Lens System

Using liquid lens cells to replace one or more moving lens groups results in additional configuration options for the optical path. Replacing moving lens groups with liquid lens cells results in a more compact system. However, a linear optical design may result in a lens that is longer than desired. The use of liquid lens cells instead of a moving group facilitates the use of optical elements such as folds to redirect of the radiation axis reduce the physical length of a lens. Although the overall length of the optical path through the lens may remain the same, the liquid lens cells provide strategic space for folding that reduces the length in one or more directions. This allows longer overall lens lengths to be used in smaller camera packages. For example, many point and shoot cameras and cell phone cameras do not have large amounts of space for a long lens. Using liquid cells in combination with folds allows for better lens systems in these small camera packages. Larger cameras can also benefit from reducing the camera package length that would be required for a lens system that did not use folds.

FIG. **6** shows an optical diagram of a zoom lens system employing liquids and a single fold **41**. The use of liquids instead of movable lens groups reduces the space requirements and provides additional options for strategic placement of airspaces for fold minors or prisms. This figure shows placement of folds where they will not interfere with moving lens groups.

Overall length of zoom lens system **60** may be reduced with some degradation in performance unless increased optical complexity such as more lens elements and/or aspherical surfaces are introduced. However, a reduced length may be achieved by folding of the zoom lens system. FIG. **6** shows a single 45 degree fold **41** in the large airspace in the rear lens group **G3**, to redirect the radiation path by 90 degrees.

FIG. **7** is an optical diagram of a zoom lens system employing liquids and a dual fold. FIG. **7** shows dual 45 degree folds **42** and **43** in the large airspace in the rear lens group **G3**, to redirect the radiation path two times by a total of 180 degrees so that the radiation has reversed direction. This arrangement may be preferred for packaging of the zoom lens system **60** in a camera box. Also, the zoom lens system may have a constant aperture of F/2.8 through all zoom and focus positions but to maintain about the same zoom lens system diameter, some vignetting may occur. In this case, some degradation of image quality may appear but

may be partially corrected by re-optimization of the prescription of the zoom lens system. The zoom lens system may be arranged so that vignetting does not occur.

FIGS. **8A** and **8B** are optical diagrams of a zoom lens system illustrating redirection of the radiation axis with different positions of the zoom lens group and surface shapes between the liquids. This embodiment is illustrative of an alternative lens layout. FIG. **8A** illustrates a zoom position that enlarges the image to a point that the optic traces exceed parameters of the lens system. This embodiment is illustrative of one design option, and minor changes could be made to the design to correct this effect.

Folds **44** and **45** are substantially parallel, so that light rays leaving lens elements **50** are substantially parallel to light rays entering the lens system through lens **46**. Lens group **47** remains fixed, while lens group **48** moves to substantially provide zooming. Lens group **49** comprises a liquid lens cell that performs zooming and focusing functions.

FIGS. **9A**, **9B** and **9C** are optical diagrams of a zoom lens system where the liquid lens cells and folds have been strategically placed to advantageously shorten the length of the lens system. Light enters the lens system through lens group **200**. Lens group **201** moves to substantially provide zooming. The light rays pass through the iris or stop **202** and enter lens group **203** comprising a liquid lens cell. Fold **204** directs the light through lens group **205**, which comprises a liquid lens cell having a variable surface **206**. The light rays then pass through lens group **207**. Fold **208** redirects the light rays through lens group **209** and towards an image plane **210**. FIG. **9A** illustrates a focal length of approximately 6 mm, F/2.8, and infinity focus. FIG. **9B** illustrates a focal length of approximately 15 mm, F/2.8, and infinity focus. FIG. **9C** illustrates a focal length of approximately 51 mm, F/2.8 and infinity focus.

The first liquid lens cell in lens group **203** has a largest clear aperture diameter of approximately 10 mm. The second liquid lens cell in lens group **205** has a largest clear aperture diameter of approximately 16 mm. By including a camera flash to slow down the taking aperture at or near the long focal length, it may be possible to revert to one liquid lens cell.

It is to be noted that various changes and modifications will become apparent to those skilled in the art. Such changes and modifications are to be understood as being included within the scope of the invention as defined by the appended claims.

What is claimed is:

1. A zoom lens system comprising:

a zoom lens group that is axially movable and that has a negative optical power, the zoom lens group comprising a plurality of optical elements of fixed optical power, the zoom lens group comprising an aspheric surface; and

a variable power rear lens group that is axially stationary and that has an optical power that varies between a first optical power and a second optical power, the variable power lens group positioned on an image side of the zoom lens group, the variable power lens group comprising a plurality of optical elements including a liquid lens cell, the liquid lens cell comprising a first contacting liquid and a second contacting liquid, a contacting optical surface between the first contacting liquid and the second contacting liquid configured to change shape to change an optical power of the variable power lens group,

15

- wherein the zoom lens group and the variable power rear lens group are aligned on a common optical axis and configured to collect radiation emanating from an object side space of the zoom lens system, deliver the radiation to an image side space without forming an intermediate image, and focus an image of an object in the image side space at a plurality of focus positions of the zoom lens system,
- wherein the magnitude of the negative optical power of the zoom lens group is greater than the magnitude of the first and second optical powers of the variable power rear lens group,
- wherein a percentage change in maximum field angle for each focus position relative to an infinity focus position is between -0.2% and -19.5% .
2. The zoom lens system of claim 1, further comprising an objective lens group that is axially stationary and that has a positive optical power.
3. The zoom lens system of claim 1, wherein both the first optical power and the second optical power of the variable power rear lens group are positive.
4. The zoom lens system of claim 1, wherein the zoom lens system has an f-number that varies between F/2.8 to F/4.0.
5. The zoom lens system of claim 1, wherein a zoom ratio of the zoom lens system is greater than $2.75\times$.
6. The zoom lens system of claim 5, wherein the zoom ratio of the zoom lens system is less than $8.5\times$.
7. The zoom lens system of claim 1, wherein the zoom lens system provides a modulation transfer function at a spatial frequency of 90 cycles/mm of at least about 58%.
8. The zoom lens system of claim 7, wherein the modulation transfer function at a spatial frequency of 90 cycles/mm is about 89%.
9. The zoom lens system of claim 1, further comprising an adjustable iris that is stationary on the common optical axis, the adjustable iris positioned on the common optical axis between the zoom lens group and the variable power rear lens group.
10. The zoom lens system of claim 9, wherein the adjustable iris is configured to decrease a diameter with an increase in zoom.
11. The zoom lens system of claim 10, wherein the diameter of the adjustable iris is at least 4.61 mm and less than 6.71 mm.
12. A method of zooming using a zoom lens system, the method comprising:
moving a zoom lens group that has a negative optical power along an optical axis, the zoom lens group comprising a plurality of optical elements of fixed optical power, the zoom lens group comprising an aspheric surface; and

16

- varying a shape of a contact surface in a variable power rear lens group to vary an optical power of the variable power rear lens group between a first optical power and a second optical power, the variable power lens group being stationary on the optical axis and positioned on an image side of the zoom lens group, the variable power lens group comprising a plurality of optical elements including a liquid lens cell, the liquid lens cell comprising a first contacting liquid and a second contacting liquid, a contacting optical surface between the first contacting liquid and the second contacting liquid having a variable shape,
- wherein the zoom lens group and the variable power rear lens group are aligned on the optical axis and configured to collect radiation emanating from an object side space of the zoom lens system, deliver the radiation to an image side space without forming an intermediate image, and focus an object in the image side space at a plurality of focus positions of the zoom lens system,
- wherein the magnitude of the negative optical power of the zoom lens group is greater than the magnitude of the first and second optical powers of the variable power rear lens group,
- wherein a percentage change in maximum field angle for each focus position relative to an infinity focus position is between -0.2% and -19.5% .
13. The method of claim 12, wherein an axially stationary positively powered objective lens group is aligned along the optical axis with the zoom lens group and the variable power rear lens group.
14. The method of claim 12, wherein both the first optical power and the second optical power of the variable power rear lens group are positive.
15. The method of claim 12, wherein the zoom lens system has an f-number that varies between F/2.8 to F/4.0.
16. The method of claim 12, wherein a zoom ratio of the zoom lens system is greater than $2.75\times$.
17. The method of claim 16, wherein the zoom ratio of the zoom lens system is less than $8.5\times$.
18. The method of claim 12, further comprising adjusting a diameter of an adjustable iris that is axially stationary, the adjustable iris positioned on the optical axis between the zoom lens group and the variable power rear lens group.
19. The method of claim 18, further comprising increasing the diameter of the adjustable iris when a zoom of the zoom lens system decreases.
20. The method of claim 19, wherein the diameter of the adjustable iris is at least 4.61 mm and less than 6.71 mm.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

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INVENTOR(S) : James H. Jannard

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

On the Title Page

In Column 1 (*) Notice: at Line 17, Delete “This patent is subject to a terminal disclaimer.”.

In the Specification

In Column 13 at Line 46, Change “minors” to --mirrors--.

Signed and Sealed this
Twelfth Day of September, 2017



Joseph Matal
*Performing the Functions and Duties of the
Under Secretary of Commerce for Intellectual Property and
Director of the United States Patent and Trademark Office*