

US009338416B2

(12) **United States Patent**
Suzuki et al.

(10) **Patent No.:** **US 9,338,416 B2**
(45) **Date of Patent:** **May 10, 2016**

(54) **DISCHARGE LAMP DRIVING DEVICE, LIGHT SOURCE DEVICE, PROJECTOR, AND DISCHARGE LAMP DRIVING METHOD**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **14/636,944**

(22) Filed: **Mar. 3, 2015**

(65) **Prior Publication Data**

US 2015/0264786 A1 Sep. 17, 2015

(30) **Foreign Application Priority Data**

Mar. 11, 2014 (JP) 2014-047295

(51) **Int. Cl.**

H05B 41/392 (2006.01)

H04N 9/31 (2006.01)

G03B 21/00 (2006.01)

H05B 41/288 (2006.01)

(52) **U.S. Cl.**

CPC **H04N 9/312** (2013.01); **G03B 21/005** (2013.01); **H05B 41/2883** (2013.01); **H05B 41/3928** (2013.01)

(58) **Field of Classification Search**

CPC H05B 41/2883; H05B 41/3928; H05B 41/2928; H05B 41/36; G03B 21/2026; G03B 21/005; G03B 21/2053

USPC 315/209 R, 224, 246, 287, 291, 307, 308
See application file for complete search history.

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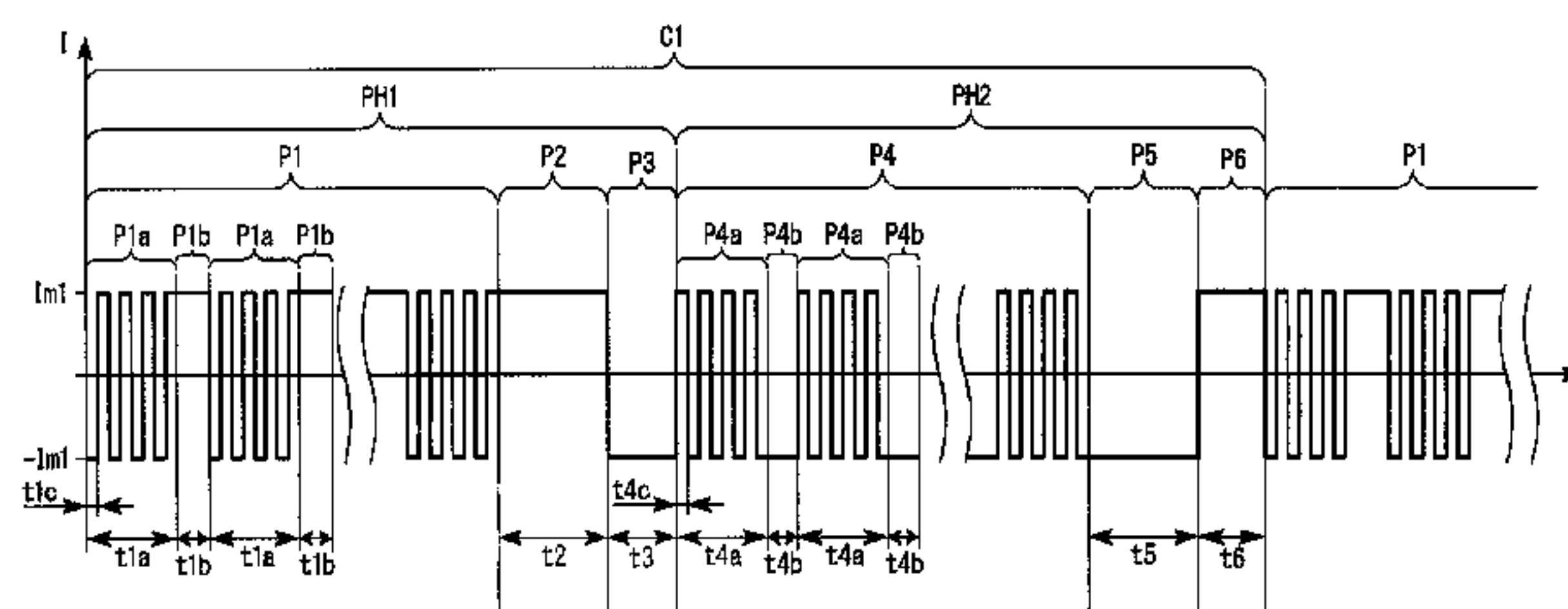
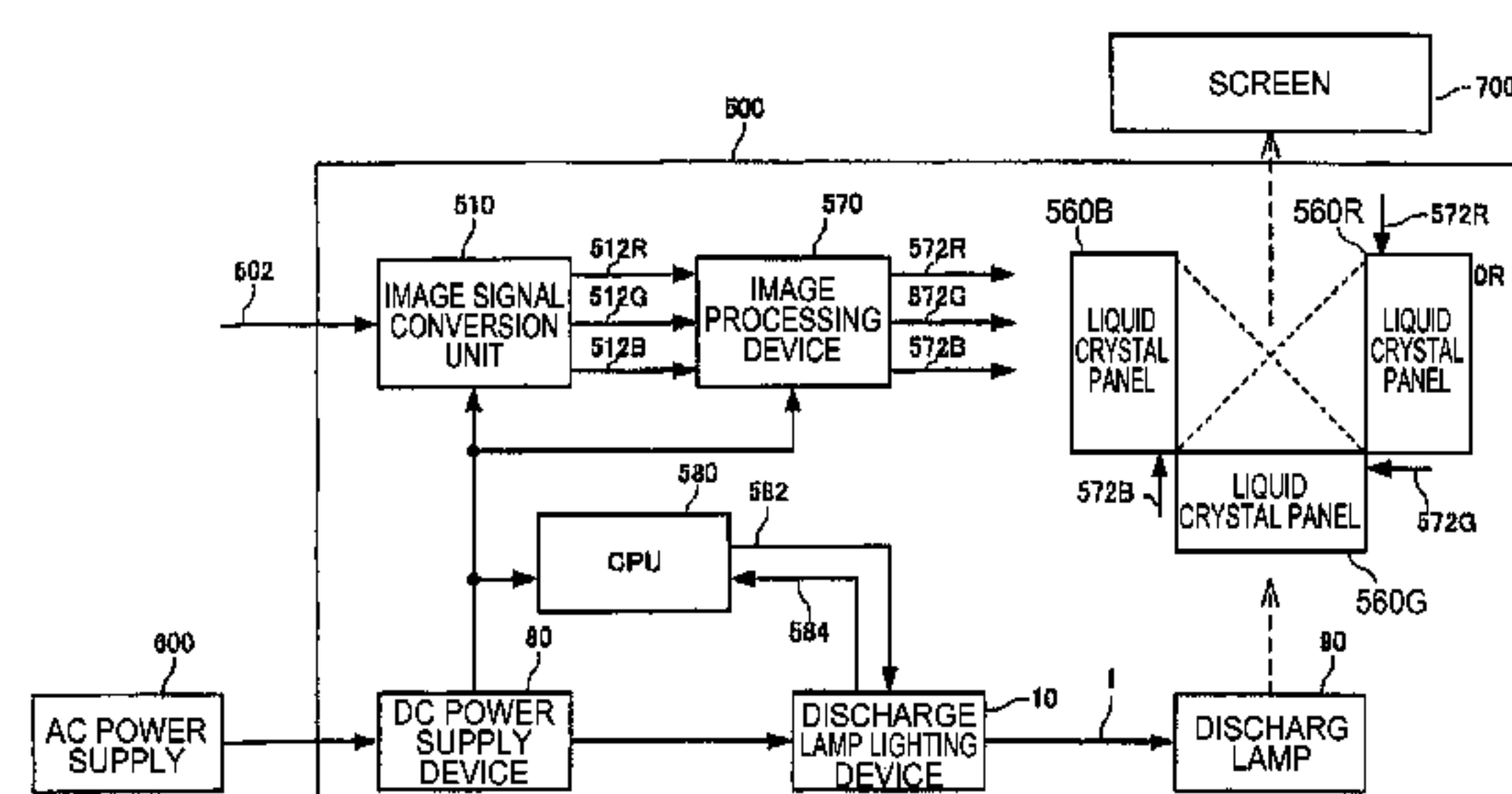
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ABSTRACT

A discharge lamp driving device includes: a discharge lamp driving unit that supplies a driving current to the discharge lamp; and a control unit that controls the discharge lamp driving unit. The driving current having driving periods is supplied, the driving period including: a mixing period which alternately has an AC period in which an alternating current is supplied and a first DC period in which a direct current is supplied, a second DC period which is provided immediately after the mixing period and in which a direct current having a polarity which is the same as that of the direct current in the first DC period is supplied, and a third DC period which is provided immediately after the second DC period and in which a direct current having a polarity opposite to that of the direct current in the second DC period is supplied.

18 Claims, 6 Drawing Sheets



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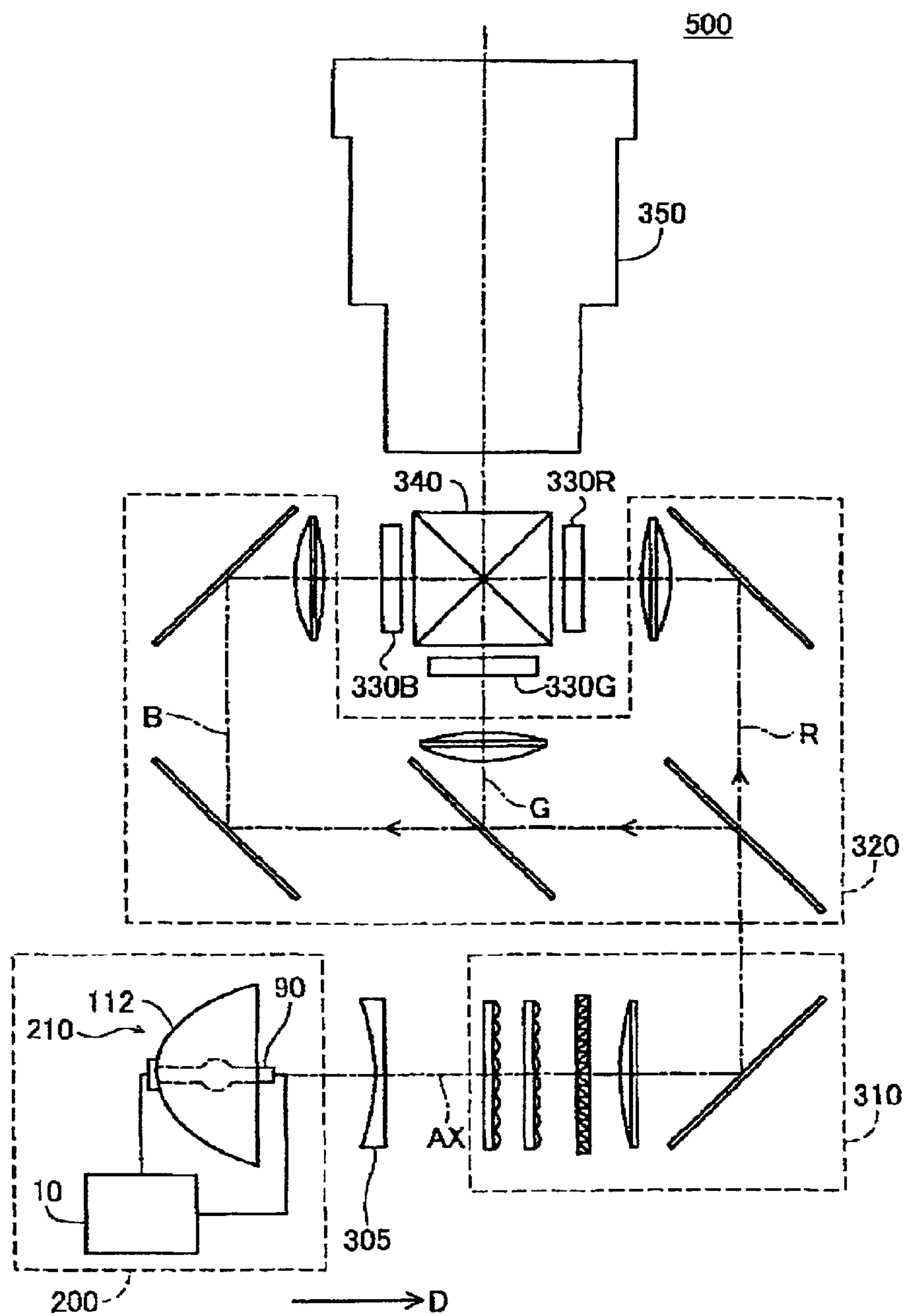


FIG. 1

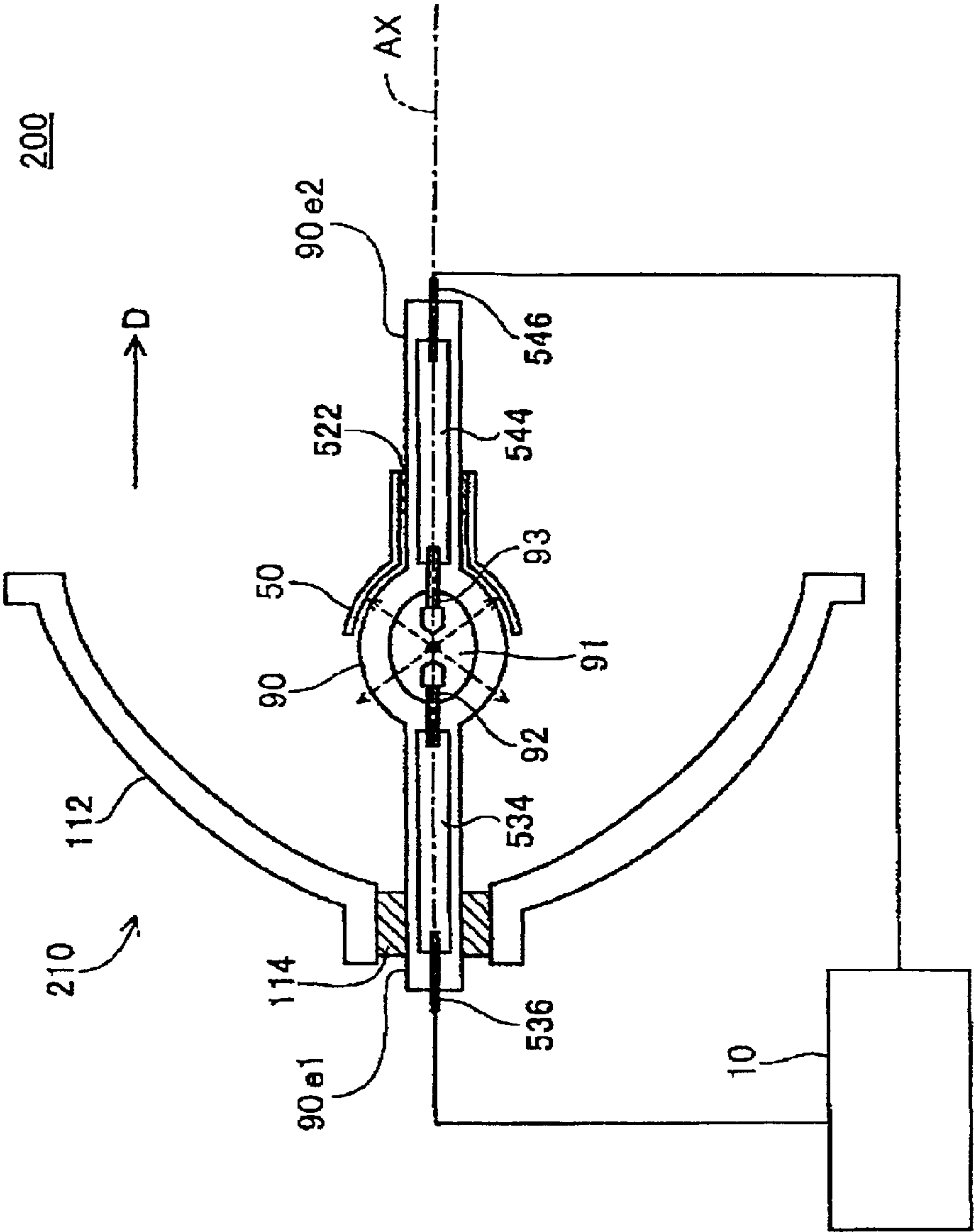


FIG. 2

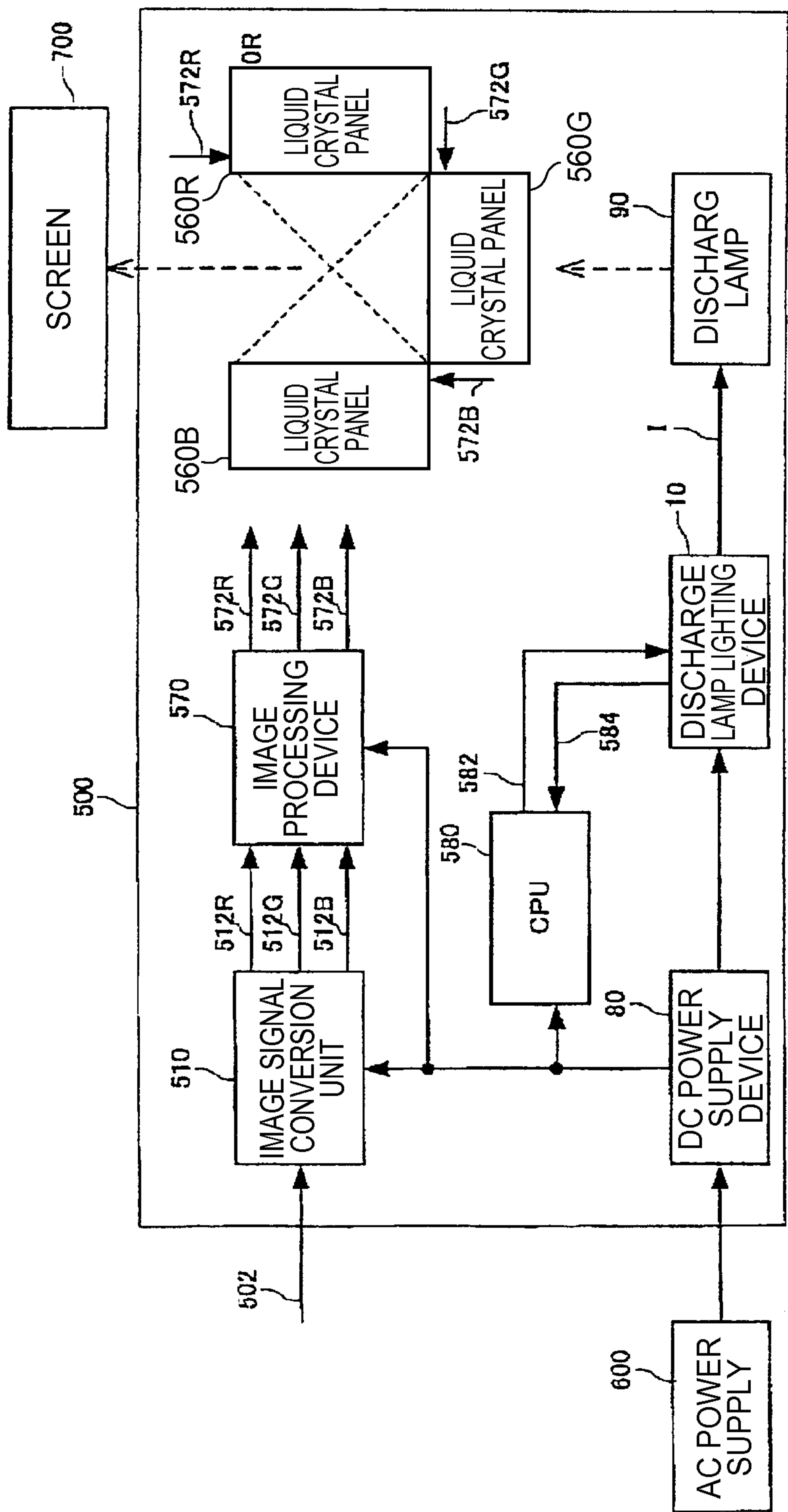


FIG. 3

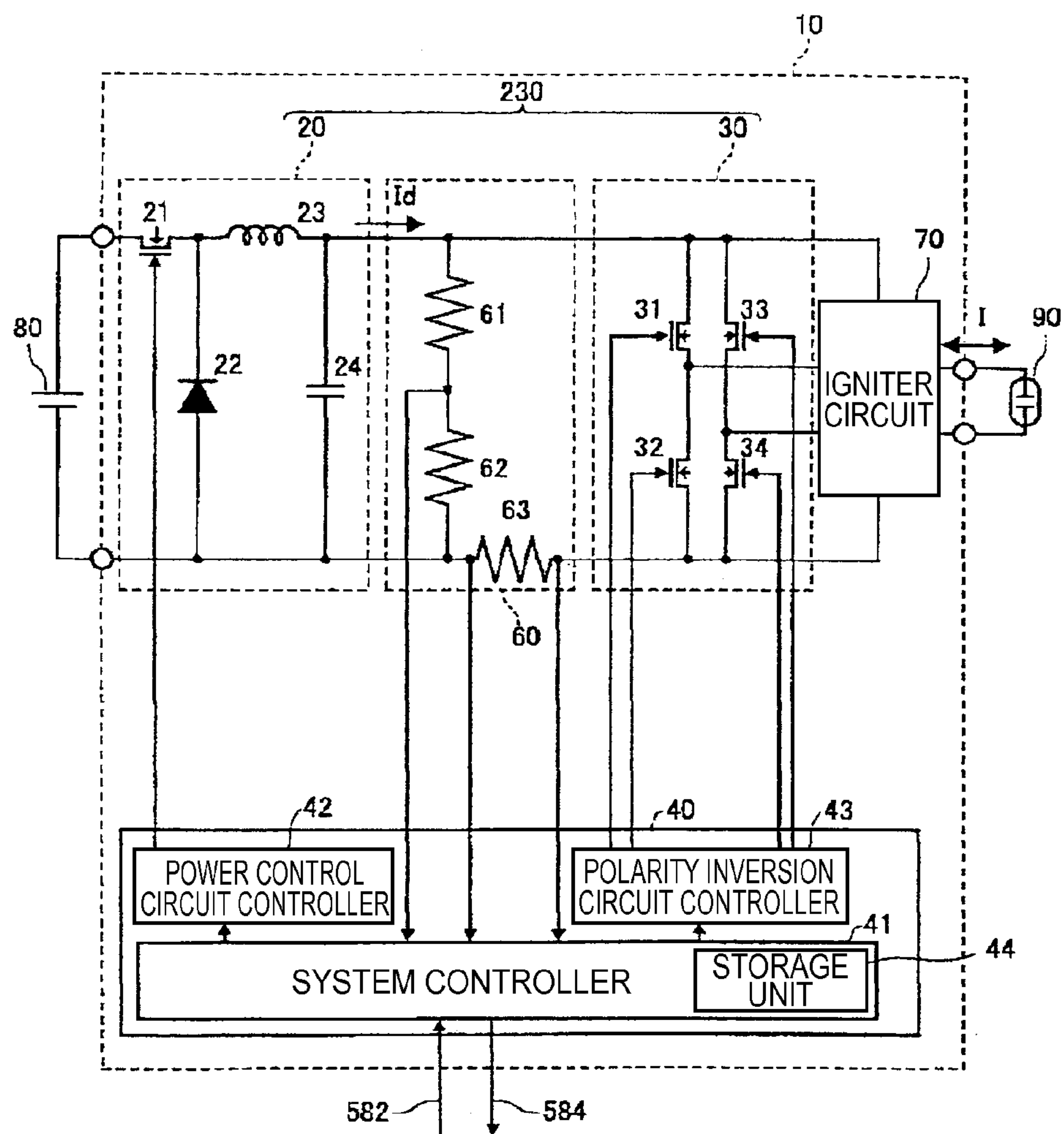


FIG. 4

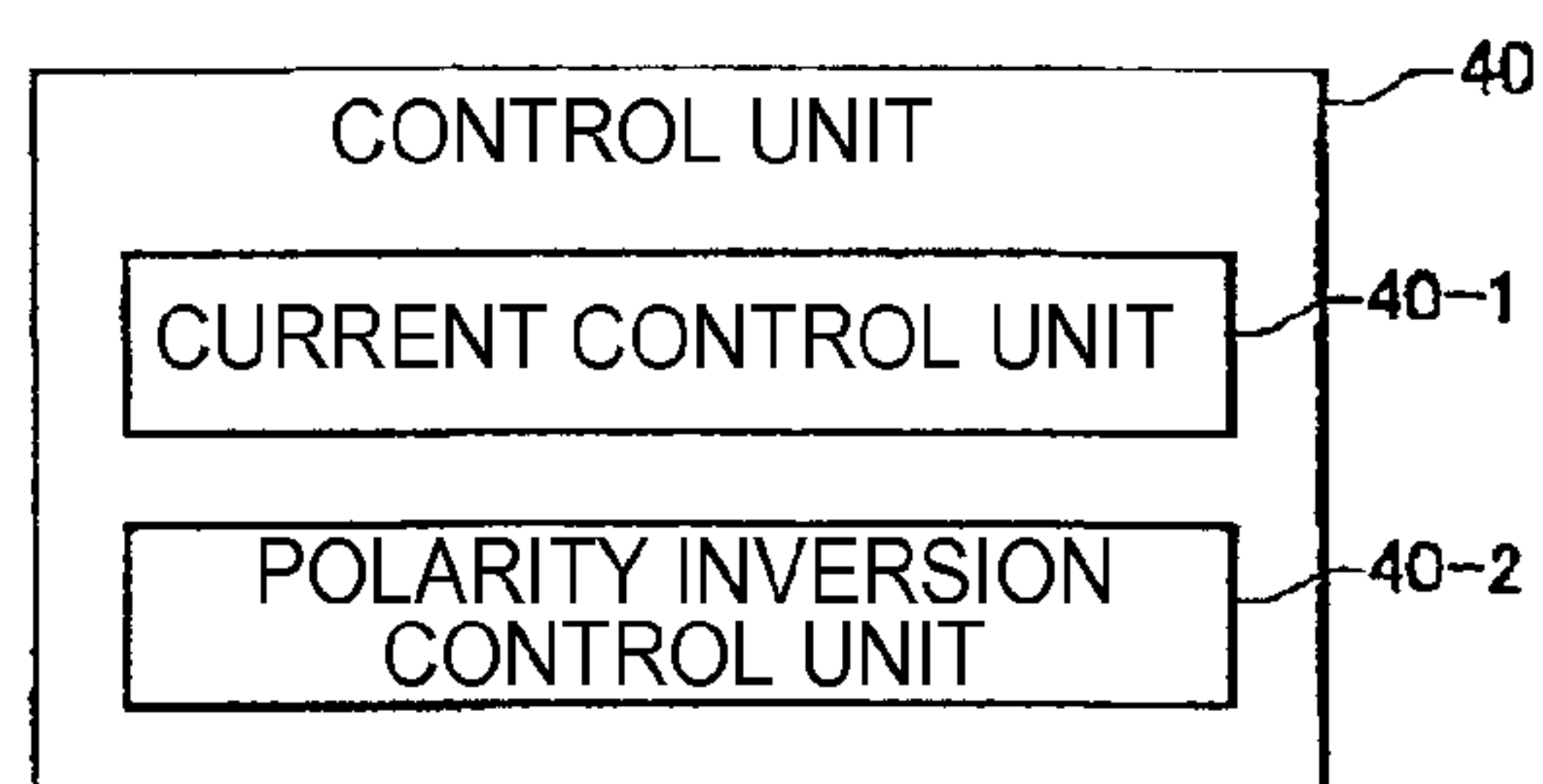


FIG. 5

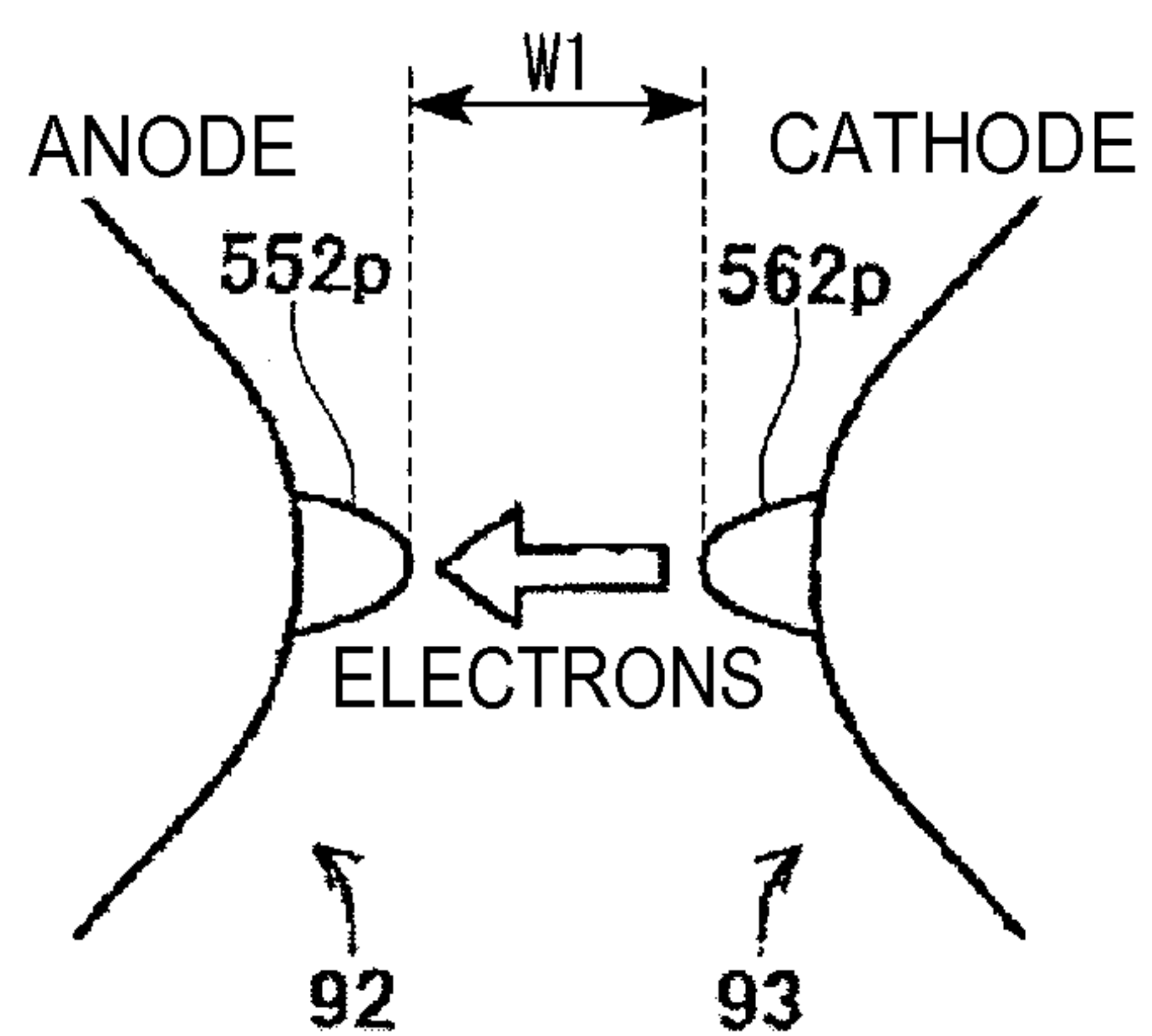


FIG. 6A

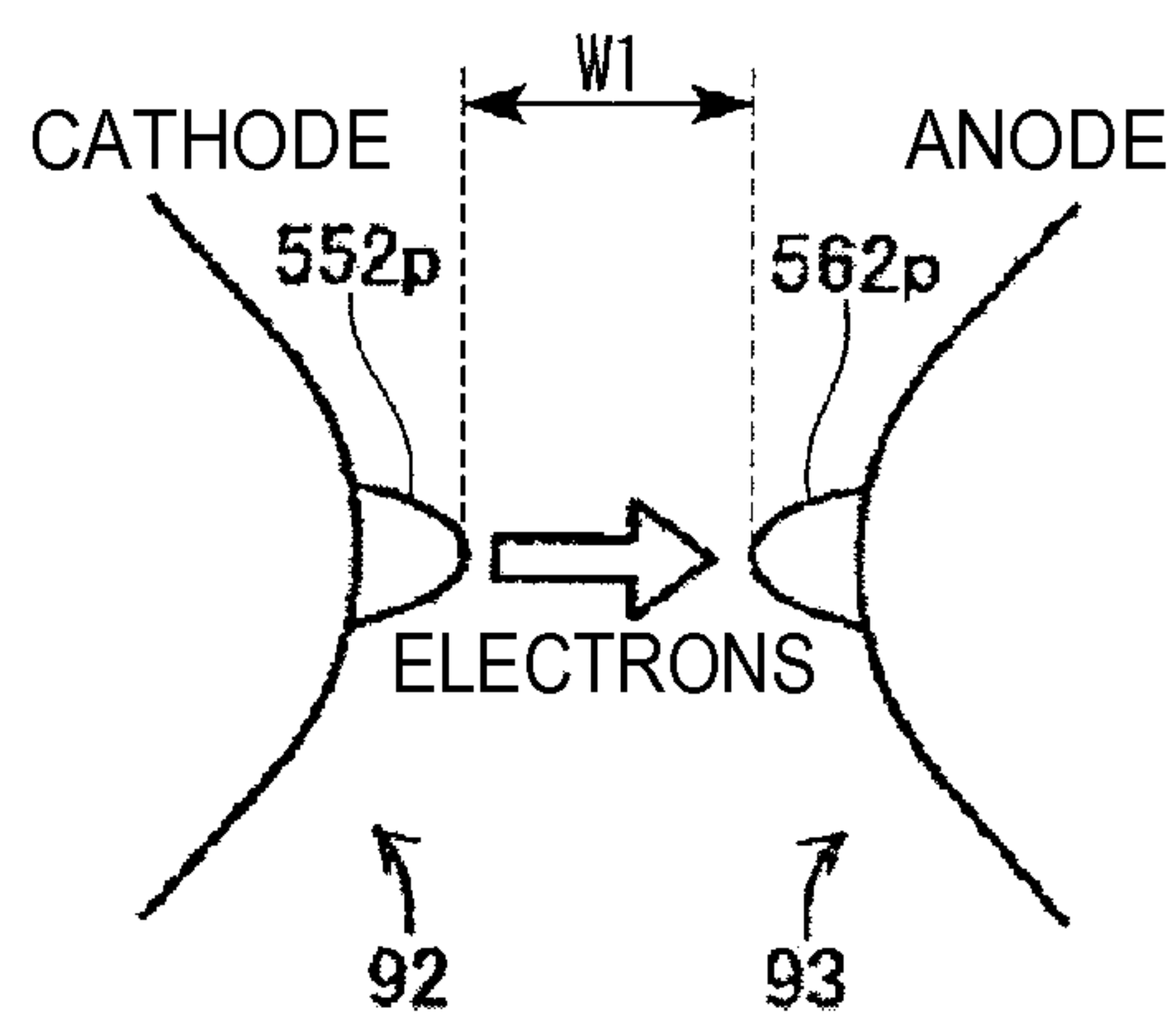


FIG. 6B

FIG. 7A

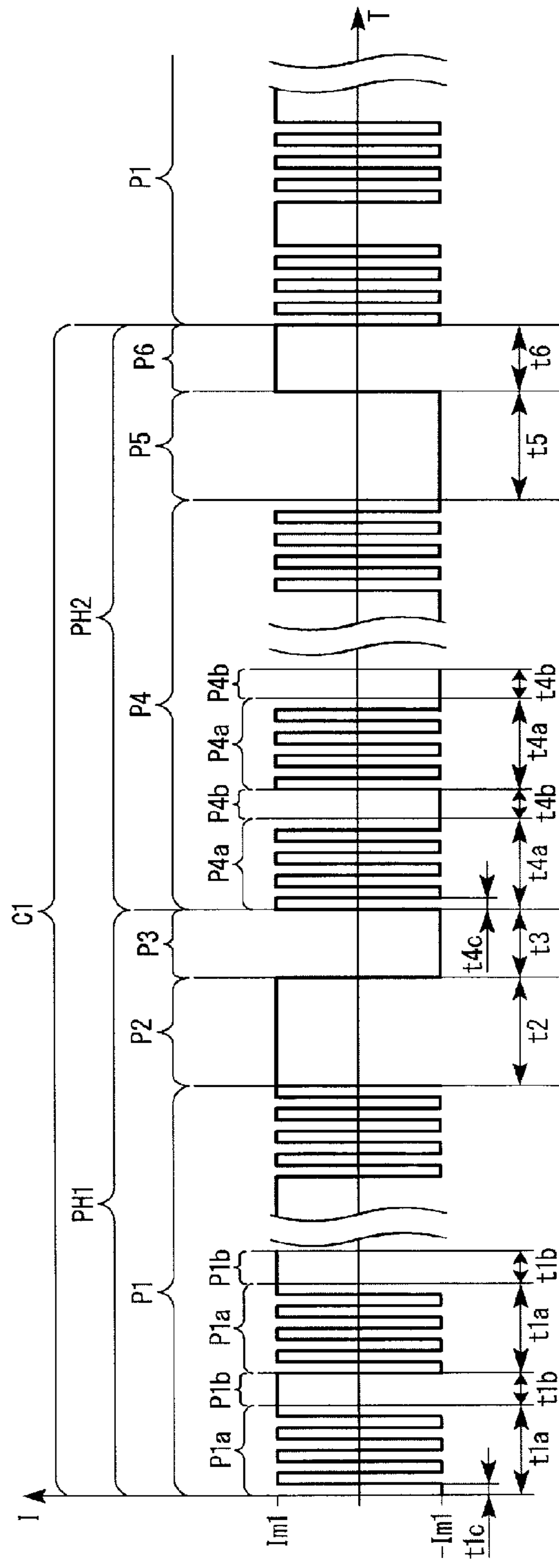
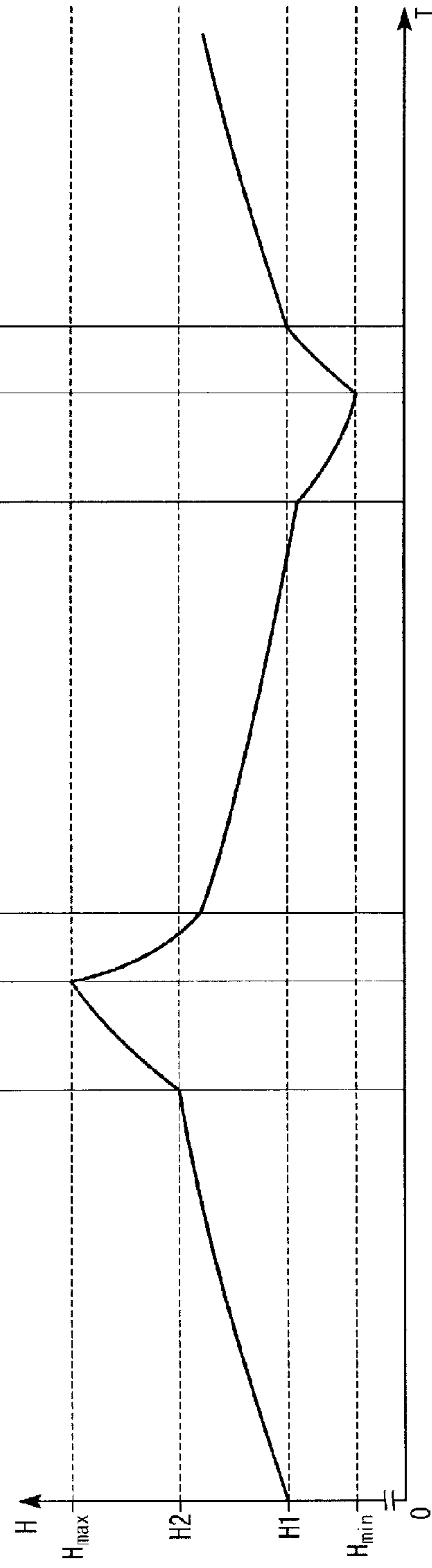


FIG. 7B



DISCHARGE LAMP DRIVING DEVICE, LIGHT SOURCE DEVICE, PROJECTOR, AND DISCHARGE LAMP DRIVING METHOD

BACKGROUND

1. Technical Field

The present invention relates to a discharge lamp driving device, a light source device, a projector, and a discharge lamp driving method.

2. Related Art

It is known that melting and solidifying of an electrode is repeated by making the temperature of an electrode of a discharge lamp fluctuate, and growth of a projection, which is a starting point of discharge, formed on a tip of the electrode can be controlled.

As a method of controlling the growth of such a projection, a method of driving a discharge lamp alternately supplying the direct current and the alternating current to a discharge lamp has been proposed (For example, JP-A-2011-23154).

The growth of a projection on the tip of the electrode becomes easily controlled as the fluctuation in temperature of the electrode is made to be large. However, in the driving method described above, the growth of a projection on the tip of the electrode is unlikely to be appropriately controlled in some cases due to the reason that the fluctuation in temperature may not be made to be sufficiently large. Accordingly, in the driving method described above, the growth of a projection is suppressed and, as a result, a service life of a discharge lamp is shortened in some cases.

SUMMARY

An advantage of some aspects of the invention is to provide a discharge lamp driving device capable of making the temperature of an electrode fluctuate largely, a light source device using such a discharge lamp driving device, a projector using such a light source device, and a method of driving a discharge lamp capable of making the temperature of an electrode fluctuate largely.

An aspect of the invention is directed to a discharge lamp driving device including: a discharge lamp driving unit that supplies a driving current for driving a discharge lamp to the discharge lamp; and a control unit that controls the discharge lamp driving unit, wherein the control unit controls the discharge lamp driving unit such that the driving current having driving periods is supplied to the discharge lamp, the driving period including: a mixing period which alternately has an AC period in which an alternating current is supplied to the discharge lamp and a first DC period in which a direct current is supplied to the discharge lamp, a second DC period which is provided immediately after the mixing period and in which a direct current having a polarity which is the same as that of the direct current in the first DC period is supplied to the discharge lamp, and a third DC period which is provided immediately after the second DC period and in which a direct current having a polarity opposite to that of the direct current in the second DC period is supplied to the discharge lamp, and the length of the second DC period is longer than the length of the first DC period and the length of the third DC period is longer than or equal to the length of the first DC period and shorter than the length of the second DC period.

According to the discharge lamp driving device of the aspect of the invention, the second DC period for which the direct current having a polarity which is the same as that of the direct current of the first DC period in the mixing period is supplied to the discharge lamp is provided immediately after

the mixing period. Accordingly, the temperature of the electrode which is increased in the mixing period is further drastically increased in the second DC period. Further, the third DC period for which the direct current having a polarity opposite to that of the direct current in the second DC period is supplied to the discharge lamp is provided immediately after the second DC period. In this manner, the temperature of the electrode in the third DC period is drastically decreased. Therefore, according to the aspect of the discharge lamp driving device of the invention, since the third DC period for which the temperature of the electrode is drastically decreased is provided immediately after the second DC period for which the temperature of the electrode is drastically increased, the fluctuation in temperature of the electrode can be made large.

In the discharge lamp driving device, the driving current may have a plurality of the driving periods, and the direct currents in the first DC periods of the adjacent driving periods may have different polarities from each other.

According to this configuration, the fluctuation in temperature of both electrodes can be made large.

The length of the first DC period may be shorter than the length of the AC period, longer than the length of a half cycle of the alternating current in the AC period, and may be shorter than the length of the second DC period.

According to this configuration, while the electrode is heated during the mixing period, it is possible to prevent a projection on the tip portion of the electrode from being extremely melted.

The length of the first DC period may be equal to or greater than 0.5 ms and equal to or less than 7.0 ms.

According to this configuration, while the electrode is heated during the mixing period, it is possible to prevent a projection on the tip portion of the electrode from being extremely melted.

The length of the first DC period may be equal to or greater than 1.0 ms and equal to or less than 5.0 ms.

According to this configuration, it is possible to increase the temperature of the electrode more preferably in the mixing period.

The number of the first DC periods included in the mixing period may be equal to or greater than 5 and equal to or less than 50.

According to this configuration, it is possible to increase the temperature of the electrode more preferably in the mixing period.

A frequency of the alternating current in the AC period may be equal to or greater than 1 kHz.

According to this configuration, it is possible to prevent a fluctuation in temperature of the electrode in the AC period.

The length of the AC period may be equal to or greater than 1 cycle and equal to or less than 20 cycles.

According to this configuration, it is possible to prevent the temperature of the electrode from being drastically increased in the mixing period.

Another aspect of the invention is directed to a light source device including: a discharge lamp that emits light, and the discharge lamp driving device described above.

According to the light source device of the aspect of the invention, since the above-described discharge lamp driving device is included, a light source device capable of making the fluctuation in temperature of the electrode large can be obtained.

Still another aspect of the invention is directed to a projector including: the light source device described above; a light modulation element that modulates light emitted from the

light source device according to a video signal; and a projection optical system that projects the light modulated by the light modulation element.

According to the projector of the aspect of the invention, since the above-described light source device is included, a projector with excellent reliability can be obtained.

Yet another aspect of the invention is directed to a method of driving a discharge lamp that is driven by supplying a driving current to the discharge lamp, the method including: supplying the driving current having driving periods to the discharge lamp, the driving period including: a mixing period which alternately has an AC period in which an alternating current is supplied to the discharge lamp and a first DC period in which a direct current is supplied to the discharge lamp, a second DC period which is provided immediately after the mixing period and in which a direct current having a polarity which is the same as that of the direct current in the first DC period is supplied to the discharge lamp, and a third DC period which is provided immediately after the second DC period and in which a direct current having a polarity opposite to that of the direct current in the second DC period is supplied to the discharge lamp, wherein the length of the second DC period is longer than the length of the first DC period, and the length of the third DC period is longer than or equal to the length of the first DC period and shorter than the length of the second DC period.

According to the method of driving a discharge lamp of the aspect of the invention, it is possible to make the fluctuation in temperature of the electrode large in the same manner as described above.

The driving current may have a plurality of the driving periods, and the direct currents in the first DC periods of the adjacent driving periods may have different polarities from each other.

According to the method with this configuration, the fluctuation in temperature of both electrodes can be made large.

BRIEF DESCRIPTION OF THE DRAWINGS

The invention will be described with reference to the accompanying drawings, wherein like numbers reference like elements.

FIG. 1 is a view schematically illustrating a configuration of a projector according to the present embodiment.

FIG. 2 is a view illustrating a discharge lamp according to the present embodiment.

FIG. 3 is a block diagram illustrating various kinds of constituent elements of the projector according to the present embodiment.

FIG. 4 is a circuit diagram of a discharge lamp lighting device of the present embodiment.

FIG. 5 is a block diagram illustrating an example of a configuration of a control unit according to the present embodiment.

FIGS. 6A and 6B are views illustrating states of projections on tip ends of electrodes of the discharge lamp.

FIGS. 7A and 7B are diagrams illustrating an example of a driving current waveform of the discharge lamp according to the present embodiment.

DESCRIPTION OF EXEMPLARY EMBODIMENTS

Hereinafter, a projector according to an embodiment of the invention will be described with reference to the accompanying drawings.

Further, the range of the invention is not limited to the embodiments described below and can be arbitrarily changed within the range of the technical scope of the invention. In addition, for the sake of easy description of each configuration, in the drawings below, the scales or the numerical values of each structure may be different from those of the actual structure.

As illustrated in FIG. 1, a projector 500 of the present embodiment includes a light source device 200, a collimating lens 305, an illumination optical system 310, a color separation optical system 320, three liquid crystal light valves (light modulation elements) 330R, 330G, and 330B, a cross dichroic prism 340, and a projection optical system 350.

Light emitted from the light source device 200 passes through the collimating lens 305 and is incident on the illumination optical system 310. The collimating lens 305 has a function of collimating light from the light source device 200.

The illumination optical system 310 has a function of adjusting illumination of light emitted from the light source device 200 such that the illumination becomes uniform on the liquid crystal light valves 330R, 330G, and 330B. The illumination optical system 310 has a function of aligning polarization directions of light emitted from the light source device 200 to one direction. The reason is that the light emitted from the light source device 200 is effectively used in the liquid crystal light valves 330R, 330G, and 330B.

Light whose illuminance distribution and polarization direction are adjusted is incident to the color separation optical system 320. The color separation optical system 320 separates the incident light into three colored light beams of red light (R), green light (G), and blue light (B). Three colored light beams are modulated by the liquid crystal light valves 330R, 330G, and 330B in correspondence to respective colors. The liquid crystal light valves 330R, 330G, and 330B include liquid crystal panels 560R, 560G, and 560B, and polarizing plates (not illustrated) described below. The polarizing plates are arranged on respective light incident sides and light emitting sides of the liquid crystal panels 560R, 560G, and 560B.

The modulated three colored light beams are synthesized by the cross dichroic prism 340. The synthetic light is incident on the projection optical system 350. The projection optical system 350 projects the incident light on a screen 700 (see FIG. 3). In this manner, video is displayed on the screen 700. Further, as each of the configurations of the collimating lens 305, the illumination optical system 310, the color separation optical system 320, the cross dichroic prism 340, and the projection optical system 350, various known configurations can be employed.

FIG. 2 is a view illustrating the configuration of the light source device 200. The light source device 200 includes a light source unit 210 and a discharge lamp lighting device (discharge lamp driving device) 10. FIG. 2 is a cross-sectional view illustrating the light source unit 210. The light source unit 210 includes a main reflecting mirror 112, a discharge lamp 90, and a sub-reflecting mirror 50.

The discharge lamp lighting device 10 supplies a driving current (driving power) to the discharge lamp 90 and lights the discharge lamp 90. The main reflecting mirror 112 reflects light discharged from the discharge lamp 90 toward an irradiation direction D. The irradiation direction D is parallel with an optical axis AX of the discharge lamp 90.

The discharge lamp 90 has a rod shape extending along the irradiation direction D. One end portion (end portion on the left side of the figure) of the discharge lamp 90 is set as a first end portion 90e1 and another end portion (end portion on the right side of the figure) of the discharge lamp 90 is set as a

second end portion **90e2**. As materials of the discharge lamp **90**, translucent materials such as quartz glass and the like are used. The middle portion of the discharge lamp **90** is swollen in a spherical shape and the inside thereof is a discharge space **91**. In the discharge space **91**, gas which is a discharge medium containing rare gas and a metal halogen compound is sealed.

Tips of a first electrode **92** and a second electrode **93** protrude in the discharge space **91**. The first electrode **92** is arranged on the first end portion **90e1** side of the discharge space **91**. The second electrode **93** is arranged on the second end portion **90e2** side of the discharge space **91**. The shape of the first electrode **92** and the second electrode **93** is a rod shape along the optical axis **AX**. The tip portions of the first electrode **92** and the second electrode **93** are arranged in the discharge space **91** such that the tip portions thereof are separated from each other by a predetermined distance and face each other. The materials of the first electrode **92** and the second electrode **93** are metals such as tungsten.

A first terminal **536** is provided on the first end portion **90e1** of the discharge lamp **90**. The first terminal **536** and the first electrode **92** are electrically connected by a conductive member **534** penetrating the inside of the discharge lamp **90**. In the same manner, a second terminal **546** is provided on the second end portion **90e2** of the discharge lamp **90**. The second terminal **546** and the second electrode **93** are electrically connected by a conductive member **544** penetrating the inside of the discharge lamp **90**. The materials of the first terminal **536** and the second terminal **546** are, for example, metals such as tungsten. As the materials of the conductive members **534** and **544**, molybdenum foil can be used.

The first terminal **536** and the second terminal **546** are connected to the discharge lamp lighting device **10**. The discharge lamp lighting device **10** supplies the driving current for driving the discharge lamp **90** to the first terminal **536** and the second terminal **546**. As a result, arc discharge occurs between the first electrode **92** and the second electrode **93**. The light (discharge light) generated due to the arc discharge is radiated toward all directions from a discharge position as indicated by a dashed arrow.

The main reflecting mirror **112** is fixed to the first end portion **90e1** of the discharge lamp **90** by a fixing member **114**. The main reflecting mirror **112** reflects light among discharge light, which travels toward the opposite side of the irradiation direction **D**, toward the irradiation direction **D**. The shape of the reflecting surface (surface on the discharge lamp **90** side) of the main reflecting mirror **112** is not particularly limited as long as discharge light can be reflected toward the irradiation direction **D**, and examples thereof include a spheroidal shape and a rotary parabolic shape. For example, in the case where the shape of the reflecting surface of the main reflecting mirror **112** is set as a rotary parabolic shape, the main reflecting mirror **112** can convert discharge light into light approximately parallel to the optical axis **AX**. In this manner, the collimating lens **305** can be omitted.

The sub-reflecting mirror **50** is fixed to the second end portion **90e2** side of the discharge lamp **90** by a fixing member **522**. The shape of the reflecting surface (surface of the discharge lamp **90** side) of the sub-reflecting mirror **50** is a spherical surface shape surrounding a portion of the second end portion **90e2** side of the discharge space **91**. The sub-reflecting mirror **50** reflects light among discharge light, which travels toward the opposite side of the side on which the main reflecting mirror **112** is arranged, toward the main reflecting mirror **112**. In this manner, utilization efficiency of light radiated from the discharge space **91** can be improved.

The materials of the fixing member **114** and **522** are not particularly limited as long as the materials are heat-resistant materials withstanding generation of heat from the discharge lamp **90**, and an inorganic adhesive can be exemplified. As a method of fixing the arrangement of the discharge lamp **90** with the main reflecting mirror **112** and the sub-reflecting mirror **50**, an arbitrary method can be employed without limiting a method of fixing the main reflecting mirror **112** and the sub-reflecting mirror **50** to the discharge lamp **90**. For example, the discharge lamp **90** and the main reflecting mirror **112** may be independently fixed to a housing (not illustrated) of the projector **500**. The same applies to the sub-reflecting mirror **50**.

Hereinafter, a circuit configuration of the projector **500** will be described.

FIG. **3** is a view illustrating an example of a circuit configuration of the projector **500** according to the present embodiment. The projector **500** includes an image signal conversion unit **510**, a DC power supply device **80**, the liquid crystal panels **560R**, **560G**, and **560B**, an image processing device **570**, and a central processing unit (CPU) **580** in addition to the optical system illustrated in FIG. **1**.

The image signal conversion unit **510** generates image signals **512R**, **512G**, and **512B** by converting an image signal **502** (a brightness-color difference signal or an analog RGB signal) input from the outside into a digital RGB signal having a predetermined word length and supplies the generated signals to the image processing device **570**.

The image processing device **570** performs image processing with respect to three image signals **512R**, **512G**, and **512B** respectively. The image processing device **570** supplies driving signals **572R**, **572G**, and **572B** for respectively driving the liquid crystal panels **560R**, **560G**, and **560B** to the liquid crystal panels **560R**, **560G**, and **560B**.

The DC power supply device **80** converts an AC voltage supplied from an external AC power supply **600** into a constant DC voltage. The DC power supply device **80** supplies the DC voltage to the image signal conversion unit **510** and the image processing device **570** positioned on the secondary side of a transformer (not illustrated and included in the DC power supply device **80**) and to the discharge lamp lighting device **10** positioned on the primary side of the transformer.

The discharge lamp lighting device **10** generates a high voltage between the electrodes of the discharge lamp **90** at startup and causes insulation breakdown to form a discharge path. Subsequently, the discharge lamp lighting device **10** supplies a driving current **I** for the discharge lamp **90** maintaining discharge.

The liquid crystal panels **560R**, **560G**, and **560B** are respectively included in the above-described liquid crystal light valves **330R**, **330G**, and **330B**. The liquid crystal panels **560R**, **560G**, and **560B** modulate transmittance (brightness) of colored light incident on respective liquid crystal panels **560R**, **560G**, and **560B** through the above-described optical system based on respective driving signals **572R**, **572G**, and **572B**.

The CPU **580** controls various operations from the start of lighting of the projector **500** to turning the light off. For example, in the example of FIG. **3**, a light-on instruction or a light-off instruction is output to the discharge lamp lighting device **10** through a communication signal **582**. The CPU **580** receives lighting information of the discharge lamp **90** through the communication signal **584** from the discharge lamp lighting device **10**.

Hereinafter, the configuration of the discharge lamp lighting device **10** will be described.

FIG. 4 is a view illustrating an example of a circuit configuration of the discharge lamp lighting device 10.

The discharge lamp lighting device 10 includes a power control circuit 20, a polarity inversion circuit 30, a control unit 40, an operation detecting unit 60, and an igniter circuit 70 as illustrated in FIG. 4.

The power control circuit 20 generates driving power supplied to the discharge lamp 90. In the present embodiment, the power control circuit 20 is configured of a step down chopper circuit that inputs a voltage from the DC power supply device 80 and outputs a direct current I_d by lowering the input voltage.

The power control circuit 20 includes a switch element 21, a diode 22, a coil 23, and a capacitor 24. The switch element 21 is configured of, for example, a transistor. In the present embodiment, one end of the switch element 21 is connected to a positive voltage side of the DC power supply device 80 and another end is connected to a cathode terminal of the diode 22 and one end of the coil 23.

One end of the capacitor 24 is connected to the other end of the coil 23 and the other end of the capacitor 24 is connected to an anode terminal of the diode 22 and a negative voltage side of the DC power supply device 80. A current control signal is input to a control terminal of the switch element 21 from the control unit 40 described below so that ON/OFF of the switch element 21 is controlled. As the current control signal, for example, a pulse width modulation (PWM) control signal may be used.

When the switch element 21 is turned ON, the current flows in the coil 23 and energy is stored in the coil 23. Next, when the switch element 21 is turned OFF, the energy stored in the coil 23 is released through a path passing through the capacitor 24 and the diode 22. As a result, a direct current I_d is generated according to a ratio of an ON-time of the switch element 21.

The polarity inversion circuit 30 inverts the polarity of the direct current I_d input from the power control circuit 20 at a predetermined timing. In this manner, the polarity inversion circuit 30 generates a driving current I which is a direct current continuing for a controlled amount of time or a driving current I which is an alternating current having an arbitrary frequency and outputs the current. In the present embodiment, the polarity inversion circuit 30 is configured of an inverter bridge circuit (full-bridge circuit).

The polarity inversion circuit 30 includes a first switch element 31, a second switch element 32, a third switch element 33, and a fourth switch element 34 configured of a transistor or the like. The polarity inversion circuit 30 has a configuration in which the first switch element 31 and the second switch element 32 connected in series to each other and the third switch element 33 and the fourth switch element 34 connected in series to each other are connected in parallel with each other. Polarity inversion control signals are respectively input to control terminals of the first switch element 31, the second switch element 32, the third switch element 33, and the fourth switch element 34 from the control unit 40. An ON/OFF operation of the first switch element 31, the second switch element 32, the third switch element 33, and the fourth switch element 34 is controlled based on the polarity inversion control signals.

In the polarity inversion circuit 30, an operation of alternately turning ON and OFF the first switch element 31 and the fourth switch element 34, and the second switch element 32 and the third switch element 33 is repeatedly performed. In this manner, the polarity of the direct current I_d output from the power control circuit 20 is alternately inverted. The polarity inversion circuit 30 generates a driving current I which is

a direct current that maintains the same polarity state for a controlled amount of time or a driving current I that is an alternating current having a controlled frequency from a common connection point between the first switch element 31 and the second switch element 32 and a common connection point between the third switch element 33 and the fourth switch element 34 and outputs the current.

That is, the polarity inversion circuit 30 is controlled such that the second switch element 32 and the third switch element 33 are turned OFF when the first switch element 31 and the fourth switch element 34 are turned ON and the second switch element 32 and the third switch element 33 are turned ON when the first switch element 31 and the fourth switch element 34 are turned OFF. Accordingly, when the first switch element 31 and the fourth switch element 34 are turned ON, a driving current I flowing through one end of the capacitor 24, the first switch element 31, the discharge lamp 90, and the fourth switch element 34 in order is generated. When the second switch element 32 and the third switch element 33 are turned ON, a driving current I flowing through one end of the capacitor 24, the third switch element 33, the discharge lamp 90, and the second switch element 32 in order is generated.

In the present embodiment, a portion combining the power control circuit 20 and the polarity inversion circuit 30 corresponds to the discharge lamp driving unit 230. That is, the discharge lamp driving unit 230 supplies the driving current I driving the discharge lamp 90 to the discharge lamp 90.

The control unit 40 controls the discharge lamp driving unit 230. In the example of FIG. 4, the control unit 40 controls a retention time for which the driving current I maintains the same polarity, the current value of the driving current I , the frequency, and the like by controlling the power control circuit 20 and the polarity inversion circuit 30. The details will be described below.

The control unit 40 performs polarity inversion control of controlling the retention time for which the driving current I maintains the same polarity, the frequency of the driving current I , and the like with respect to the polarity inversion circuit 30 at a polarity inversion timing of the driving current I . Further, the control unit 40 performs current control of controlling the current value of the direct current I_d to be output with respect to the power control circuit 20.

The configuration of the control unit 40 is not particularly limited. In the present embodiment, the control unit 40 includes a system controller 41, a power control circuit controller 42, and a polarity inversion circuit controller 43. Further, a part or the entire control unit 40 may be configured of a semiconductor integrated circuit.

The system controller 41 controls the power control circuit 20 and the polarity inversion circuit 30 by controlling the power control circuit controller 42 and the polarity inversion circuit controller 43. The system controller 41 may control the power control circuit controller 42 and the polarity inversion circuit controller 43 based on the lamp voltage detected by the operation detecting unit 60 and the driving current I .

In the present embodiment, the system controller 41 includes a storage unit 44. The storage unit 44 may be provided independently from the system controller 41.

The system controller 41 may control the power control circuit 20 and the polarity inversion circuit 30 based on information stored in the storage unit 44. Further, information related to driving parameters such as the retention time for which the driving current I maintains the same polarity, the current value of the driving current I , the frequency, the waveform, and a modulation pattern may be stored in the storage unit 44.

The power control circuit controller **42** controls the power control circuit **20** by outputting a current control signal to the power control circuit **20** based on the control signal from the system controller **41**.

The polarity inversion circuit controller **43** controls the polarity inversion circuit **30** by outputting a polarity inversion control signal to the polarity inversion circuit **30** based on the control signal from the system controller **41**.

The control unit **40** can perform the above-described control and various controls of processes described below by being realized using a dedicated circuit. The control unit **40** functions as a computer by the CPU executing control programs stored in the storage unit **44** and can perform various controls of these processes.

FIG. **5** is a view for describing another example of the configuration of the control unit **40**. As illustrated in FIG. **5**, the control unit **40** may be configured so as to function as a current control unit **40-1** that controls the power control circuit **20** and as a polarity inversion control unit **40-2** that controls the polarity inversion circuit **30** using control programs.

In the example illustrated in FIG. **4**, the control unit **40** is configured as a part of the discharge lamp lighting device **10**. Meanwhile, some of the functions of the control unit **40** may be carried out by the CPU **580**.

The operation detecting unit **60** may include a voltage detecting unit that detects the lamp voltage of the discharge lamp **90** and outputs driving voltage information to the control unit **40** and a current detecting unit that detects the driving current **I** and outputs driving current information to the control unit **40**. In the present embodiment, the operation detecting unit **60** includes a first resistor **61**, a second resistor **62**, and a third resistor **63**.

In the present embodiment, the voltage detecting unit detects the lamp voltage using a voltage divided by the first resistor **61** and the second resistor **62** which are connected in parallel with the discharge lamp **90** and connected to each other in series. Further, in the present embodiment, the current detecting unit detects the driving current **I** using a voltage generated in the third resistor **63** connected to the discharge lamp **90** in series.

The igniter circuit **70** is only operated at the start of lighting of the discharge lamp **90**. The igniter circuit **70** supplies a high voltage (a voltage higher than the voltage at normal lighting of the discharge lamp **90**) necessary for forming a discharge path by causing insulation breakdown between electrodes (between the first electrode **92** and the second electrode **93**) of the discharge lamp **90** at the start of lighting of the discharge lamp **90** to a portion between electrodes of the discharge lamp **90** (between the first electrode **92** and the second electrode **93**). In the present embodiment, the igniter circuit **70** is connected to the discharge lamp **90** in parallel.

Hereinafter, a relationship between the polarity of the driving current **I** and the temperature of the electrodes will be described.

FIGS. **6A** and **6B** are views illustrating an operation state of the first electrode **92** and the second electrode **93**.

FIGS. **6A** and **6B** illustrate tip portions of the first electrode **92** and the second electrode **93**. A projection **552p** and a projection **562p** are respectively formed on the tips of the first electrode **92** and the second electrode **93**. The discharge generated between the first electrode **92** and the second electrode **93** is mainly generated between the projection **552p** and the projection **562p**.

FIG. **6A** illustrates a first polarity state in which the first electrode **92** is operated as an anode and the second electrode **93** is operated as a cathode. In the first polarity state, electrons

are moved due to discharge from the second electrode **93** (cathode) to the first electrode **92** (anode). Electrons are released from the cathode (second electrode **93**). The electrons released from the cathode (second electrode **93**) collide with the tip of the anode (first electrode **92**). Due to this collision, heat is generated so that the temperature of the tip (projection **552p**) of the anode (first electrode **92**) is increased. Meanwhile, the temperature of the tip (projection **562p**) of the cathode (second electrode **93**) which is the side of releasing electrons is decreased.

FIG. **6B** illustrates a second polarity state in which the first electrode **92** is operated as the cathode and the second electrode **93** is operated as the anode. In the second polarity state, contrary to the first polarity state, electrons are moved from the first electrode **92** to the second electrode **93**. As a result, the temperature of the tip (projection **562p**) of the second electrode **93** is increased. Meanwhile, the temperature of the tip (projection **552p**) of the first electrode **92** is decreased.

As described above, the temperature of the anode with which electrons collide is increased and the temperature of the cathode releasing electrons is decreased. That is, in the first polarity state, the temperature of the first electrode **92** is increased and the temperature of the second electrode **93** is decreased. In the second polarity state, the temperature of the second electrode **93** is increased and the temperature of the first electrode **92** is decreased.

A distance **W1** between electrodes of the first electrode **92** and the second electrode **93** is the distance between the projection **552p** and the projection **562p**. When the distance **W1** between electrodes is increased, the lamp voltage of the discharge lamp **90** is increased and the illuminance of the discharge lamp **90** is decreased during constant power driving. For this reason, by controlling the growth of the projection **552p** and the projection **562p** and maintaining the distance **W1** between electrodes, it is possible to suppress a decrease in illuminance of the discharge lamp **90** so that the service life of the discharge lamp **90** can be improved.

Next, control of the discharge lamp driving unit **230** performed by the control unit **40** will be described.

FIG. **7A** is a timing chart showing the driving current **I** to be supplied to the discharge lamp **90** in the present embodiment. The horizontal axis indicates a time **T** and the vertical axis indicates a current value of the driving current **I**. The driving current **I** indicates the current flowing in the discharge lamp **90**. The positive value indicates the first polarity state and the negative value indicates the second polarity state.

FIG. **7B** is a graph showing a change in temperature of the first electrode **92** corresponding to FIG. **7A**. The horizontal axis indicates the time **T** and the vertical axis indicates a temperature **H** of the first electrode **92**.

Further, since the temperatures of the first electrode **92** and the second electrode **93** are changed by drawing the same curve except that the changing timing of the first electrode is shifted from the changing timing of the second electrode, only the first electrode **92** is described as a typical example in some cases in the description below.

The control unit **40** controls the discharge lamp driving unit **230** such that the driving current **I** illustrated in FIG. **7A** is supplied to the discharge lamp **90**. That is, the control unit **40** controls the discharge lamp driving unit **230** such that a cycle **C1** is repeated.

The cycle **C1** alternately has a first driving period (driving period) **PH1** and a second driving period (driving period) **PH2** illustrated in FIG. **7A**. The first driving period **PH1** is a driving period for which the projection **552p** of the first

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electrode 92 is melted and the second driving period PH2 is a driving period for which the projection 562p of the second electrode 93 is melted.

The first driving period PH1 includes a mixing period P1, a second DC period P2, and a third DC period P3.

The mixing period P1 is a period for which the temperature of the first electrode 92 is gradually increased. The mixing period P1 is a period alternately having an AC period P1a and a first DC period P1b.

The AC period P1a is a period for which the alternating current whose polarity is inverted between a current value I_{m1} and a current value $-I_{m1}$ is supplied to the discharge lamp 90 as the driving current I. In the present embodiment, the alternating current in the AC period P1a is a rectangular wave alternating current. The frequency of the alternating current of the AC period P1a can be set to be 1 kHz or more. By setting the frequency of the alternating current in the AC period P1a in this manner, a fluctuation in temperature H of the first electrode 92 in the AC period P1a can be suppressed. The frequency of the alternating current in the AC period P1a may be constant or modulated.

The number of AC periods P1a included in the mixing period P1 is, for example, in the range of 5 to 50, and a length $t1a$ of each AC period P1a is in the range of 1 cycle to 20 cycles. By setting the number and the length thereof in this manner, it is possible to suppress a drastic increase in temperature H of the first electrode 92 in the mixing period P1.

The first DC period P1b is a period for which the direct current of the current value I_{m1} is supplied to the discharge lamp 90 as the driving current I. In the present embodiment, the direct current in the first DC period P1b is a direct current having the first polarity whose current value is constant (I_{m1}). The number of the first DC periods P1b included in the mixing period P1 is, for example, in the range of 5 to 50. By setting in this manner, it is possible to sufficiently increase the temperature H of the first electrode 92 in the mixing period P1.

In a case where the number of the first DC periods P1b (AC periods P1a) included in the mixing period P1 is less than 5, it is difficult to sufficiently increase the temperature H of the first electrode 92. In addition, in a case where the number of the first DC periods P1b (AC periods P1a) included in the mixing period P1 is more than 50, there is a concern that the projection 552p is extremely melted or a fluctuation in brightness of the discharge lamp 90 is visually recognized and flickering occurs when the mixing period P1 is switched to the second DC period P2.

A length $t1b$ of each first DC period P1b is set such that the length $t1b$ is shorter than the length $t1a$ of the AC period P1a, longer than a length $t1c$ of a half cycle of the AC period P1a, shorter than a length $t2$ of the second DC period P2, and in the range of 0.5 ms (millisecond) to 7.0 ms. Further, more preferably, the length $t1b$ of the first DC period P1b is set to be in the range of 1 ms to 5.0 ms.

By setting the first DC period P1b in this manner, the temperature H of the first electrode 92 is gradually increased in the mixing period P1.

The second DC period P2 is provided immediately after the mixing period P1 and immediately before the third DC period P3. That is, the second DC period P2 is provided so as to be interposed between the mixing period P1 and the third DC period P3.

The second DC period P2 is a period for which the direct current of the current value I_{m1} is supplied to the discharge lamp 90 as the driving current I. The polarity of the direct current in the second DC period P2 is the same as that of the direct current in the first DC period P1b. That is, the direct

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current in the second DC period P2 is a direct current having the first polarity. In the present embodiment, the direct current in the second DC period P2 has a constant current value (I_{m1}).

The length $t2$ of the second DC period P2 is longer than the length $t1b$ of the first DC period P1b in the mixing period P1. The length $t2$ of the second DC period P2 is, for example, in the range of 3 ms to 15 ms. By setting the length in this manner, the temperature H of the first electrode 92 can be preferably increased.

The third DC period P3 is provided immediately after the second DC period P2 and immediately before the mixing period P4 in the second driving period PH2 described below. That is, the third DC period P3 is provided so as to be interposed between the second DC period P2 and the mixing period P4.

The third DC period P3 is a period for which the direct current whose current value is $-I_{m1}$ is supplied to the discharge lamp 90 as the driving current I. The polarity of the direct current in the third DC period P3 is opposite to that of the direct current in the second DC period P2. That is, the direct current in the third DC period P3 is a direct current having the second polarity. In the present embodiment, the direct current in the third DC period P3 has a constant current value ($-I_{m1}$).

A length $t3$ of the third DC period P3 is longer than or equal to the length $t1b$ of the first DC period P1b in the mixing period P1 and shorter than the length $t2$ of the second DC period P2. The length $t3$ of the third DC period P3 is, for example, in the range of 1 ms to 10 ms. By setting the length in this manner, the temperature H of the first electrode 92 can be preferably decreased.

The second driving period PH2 includes the mixing period P4, a second DC period P5, and a third DC period P6.

The mixing period P4 is a period alternately having an AC period P4a and a first DC period P4b.

The AC period P4a is a period for which the alternating current whose polarity is inverted between the current value I_{m1} and the current value $-I_{m1}$ is supplied to the discharge lamp 90 as the driving current I. In the present embodiment, the alternating current in the AC period P4a is a rectangular wave alternating current. The frequency of the alternating current of the AC period P4a can be set to be 1 kHz or more in the same manner as that of the AC period P1a. The frequency of the alternating current in the AC period P4a may be constant or modulated.

The number of AC periods P4a included in the mixing period P4 is, for example, in the range of 5 to 50, and a length $t4a$ of each AC period P4a is in the range of 1 cycle to 20 cycles in the same manner as that of the AC period P1a.

The first DC period P4b is a period for which the direct current having the current value $-I_{m1}$ is supplied to the discharge lamp 90 as the driving current I. The polarity of the direct current in the first DC period P4b is opposite to that of the direct current in the first DC period P1b of the first driving period PH1. That is, the direct current in the first DC period P4b is a direct current having the second polarity. In other words, the direct currents in the first DC periods in the adjacent driving periods have different polarities from each other. In the present embodiment, the direct current in the first DC period P4b has a constant current value ($-I_{m1}$).

The number of the AC periods P4a included in the mixing period P4 is, for example, in the range of 5 to 50 in the same manner as that of the AC period P1a.

A length $t4b$ of each first DC period P4b is set such that the length $t4b$ is shorter than the length $t4a$ of the AC period P4a, longer than a length $t4c$ of a half cycle of the AC period P4a,

shorter than a length t_5 of the second DC period P_5 , and in the range of 0.5 ms (millisecond) to 7.0 ms. Further, more preferably, the length t_{4b} of the first DC period P_{4b} is set to be in the range of 1 ms to 5.0 ms.

By setting the first DC period P_{4b} in this manner, the temperature H of the second electrode 93 is gradually increased in the mixing period P_4 .

The second DC period P_5 is provided immediately after the mixing period P_4 and immediately before the third DC period P_6 . That is, the second DC period P_5 is provided so as to be interposed between the mixing period P_4 and the third DC period P_6 .

The second DC period P_5 is a period for which the direct current having the current value $-Im_1$ is supplied to the discharge lamp 90 as the driving current I . The polarity of the direct current in the second DC period P_5 is the same as that of the direct current in the first DC period P_{4b} . That is, the direct current in the second DC period P_5 is a direct current having the second polarity. The polarity of the direct current in the second DC period P_5 is opposite to that of the direct current in the second DC period P_2 of the first driving period PH_1 . In other words, the direct currents in the second DC periods in the adjacent driving periods have different polarities from each other. In the present embodiment, the direct current in the second DC period P_5 has a constant current value ($-Im_1$).

The length t_5 of the second DC period P_5 is, for example, in the range of 3 ms to 15 ms in the same manner as that of the second DC period P_2 .

The third DC period P_6 is provided immediately after the second DC period P_5 and immediately before the mixing period P_1 in the first driving period PH_1 . That is, the third DC period P_6 is provided so as to be interposed between the second DC period P_5 and the mixing period P_1 .

The third DC period P_6 is a period for which the direct current having the current value Im_1 is supplied to the discharge lamp 90 as the driving current I . The polarity of the direct current in the third DC period P_6 is opposite to that of the direct current in the second DC period P_5 . That is, the direct current in the third DC period P_6 is a direct current having the first polarity. The polarity of the direct current in the third DC period P_6 is opposite to that of the direct current in the third DC period P_3 of the first driving period PH_1 . In other words, the direct currents in the third DC periods in the adjacent driving periods have different polarities from each other. In the present embodiment, the direct current in the third DC period P_6 has a constant current value (Im_1).

A length t_6 of the third DC period P_6 is longer than or equal to the length t_{4b} of the first DC period P_{4b} in the mixing period P_4 and shorter than the length t_5 of the second DC period P_5 in the same manner as that of the third DC period P_3 . The length t_6 of the third DC period P_6 is, for example, in the range of 1 ms to 10 ms.

The frequencies of the alternating currents in the AC periods P_{1a} and P_{4a} may be the same as or different from each other.

The numbers included in the lengths t_{1a} and t_{4a} and the mixing periods P_1 and P_4 of the AC periods P_{1a} and P_{4a} may be the same as or different from each other.

The numbers included in the lengths t_{1b} and t_{4b} and the mixing periods P_1 and P_4 of the first DC periods P_{1b} and P_{4b} may be the same as or different from each other.

The number of the AC periods P_{1a} and P_{4a} included in the mixing periods P_1 and P_4 may be the same as or different from the number of the first DC periods P_{1b} and P_{4b} included in the mixing periods P_1 and P_4 .

The lengths t_2 and t_5 of the second DC periods P_2 and P_5 may be the same as or different from each other.

The lengths t_3 and t_6 of the third DC periods P_3 and P_6 may be the same as or different from each other.

Next, an increase in temperature of the first electrode 92 when the driving current I of the present embodiment is supplied to the discharge lamp 90 will be described.

First, in the mixing period P_1 of the first driving period PH_1 , the temperature H of the first electrode 92 is gradually increased from H_1 to H_2 as illustrated in FIG. 7B because the direct current in the first DC period P_{1b} has the first polarity.

Here, since the first polarity and the second polarity are alternately exchanged in the AC period P_{1a} of the mixing period P_1 , the temperature H of both electrodes is easily held to be constant. As the frequency of the alternating current of the AC period P_{1a} is increased, the temperature H of both electrodes is easily held to be constant. Specifically, as described above, it is preferable that the frequency of the AC period P_{1a} is 1 kHz or more.

Next, in the second DC period P_2 , since the direct current having the same polarity as that of the direct current in the first DC period P_{1b} of the mixing period P_1 is supplied to the discharge lamp 90 , the temperature H of the first electrode 92 is drastically increased and becomes H_{max} .

Next, in the third DC period P_3 , since the direct current having the polarity (second polarity) opposite to that of the direct current in the second DC period P_2 is supplied to the discharge lamp 90 , the temperature H of the first electrode 92 is drastically decreased.

Next, in the mixing period P_4 of the second driving period PH_2 , since the polarity of the direct current in the first DC period P_{4b} is the second polarity, the temperature H of the first electrode 92 is gradually decreased.

Next, even in the second DC period P_5 , since the direct current of the second polarity is supplied to the discharge lamp 90 , the temperature H of the first electrode 92 is drastically decreased and becomes H_{min} .

Next, in the third DC period P_6 , since the polarity of the direct current is the first polarity, the temperature H of the first electrode 92 is drastically increased and becomes H_1 from H_{min} .

Moreover, in the mixing period P_1 of the first driving period PH_1 again, the temperature H of the first electrode 92 is gradually increased and the same temperature change is repeated hereinafter.

The change in temperature H of the second electrode 93 is symmetrical with the change in temperature H of the first electrode 92 . Specifically, the temperature H of the second electrode 93 is changed in the same manner as that of the temperature H of the first electrode 92 in the second driving period PH_2 illustrated in FIG. 7B in the first driving period PH_1 and is changed in the same manner as that of the temperature H of the first electrode 92 in the first driving period PH_1 illustrated in FIG. 7B in the second driving period PH_2 .

As described above, the control unit 40 of the present embodiment controls the discharge lamp driving unit 230 such that the current is supplied to the discharge lamp 90 according to respective periods described above.

Controlling of the discharge lamp driving unit 230 performed by the control unit 40 can be expressed as a discharge lamp driving method. That is, the method of driving a discharge lamp of the present embodiment is a method of supplying the driving current I to the discharge lamp 90 to be driven, and the driving current includes the first driving period PH_1 and the second driving period PH_2 having the mixing periods P_1 and P_4 which alternately have AC periods P_{1a} and P_{4a} for which the alternating current is supplied to the dis-

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charge lamp **90** and first DC periods **P1b** and **P4b** for which the direct current is supplied to the discharge lamp **90**, second DC periods **P2** and **P5** which are provided immediately after the mixing periods **P1** and **P4** and for which the direct current having a polarity which is the same as that of the direct current in the first DC periods **P1b** and **P4b** is supplied to the discharge lamp **90**, and third DC periods **P3** and **P6** which are provided immediately after the second DC periods **P2** and **P5** and for which the direct current having a polarity opposite to that of the direct current in the second DC periods **P2** and **P5** is supplied to the discharge lamp **90**, and the length of the second DC periods **P2** and **P5** is longer than the length of the first DC periods **P1b** and **P4b**, and the length of the third DC periods **P3** and **P6** is longer than or equal to the length of the first DC periods **P1b** and **P4b** and shorter than the length of the second DC periods **P2** and **P5**.

According to the present embodiment, the discharge lamp driving unit **230** is controlled such that the second DC period **P2** is provided immediately after the mixing period **P1** and the third DC period **P3** is provided immediately after the second DC period **P2**. Since the second DC period **P2** has the same polarity as that of the first DC period **P1b** in the mixing period **P1**, the temperature **H** of the first electrode **92** is drastically increased in the second DC period **P2**. Further, since the third DC period **P3** has the polarity opposite to that of the first DC period **P1b** in the mixing period **P1**, the temperature **H** of the first electrode **92** is drastically decreased in the third DC period **P3**. In this manner, according to the present embodiment, the fluctuation in temperature **H** of the first electrode **92** can be made large in the third DC period **P3**.

The growth of projections on tips of the electrodes is controlled by repeating melting and solidifying of the electrodes. At this time, when the fluctuation in temperature added to the electrodes is small, the shape of the projections is unlikely to be controlled.

Meanwhile, according to the present embodiment, since the fluctuation in temperature added to the first electrode **92** can be made large in the manner described above, growth of the projection **552p** of the first electrode **92** can be easily controlled. Therefore, according to the present embodiment, the service life of the discharge lamp can be improved.

In addition, since the value of the current supplied to the discharge lamp is small at the time of a low-power mode (eco-mode) or when the discharge lamp is deteriorated, it is difficult to increase the temperature of the electrodes and to allow the projections of the electrodes to grow. On the contrary, according to the present embodiment, since the fluctuation in temperature added to the first electrode **92** can be made large, the growth of the projection **552p** of the first electrode **92** is easily controlled at the time of the low-power mode or when the discharge lamp is deteriorated. That is, the effect is particularly significant at the time of the low-power mode or when the discharge lamp is deteriorated in the present embodiment.

In addition, according to the present embodiment, the length **t1b** of the first DC period **P1b** is set to be smaller than the length **t1a** of the AC period **P1a**, larger than the length **t1c** of a half cycle of the AC period **P1a**, smaller than the length **t2** of the second DC period **P2**, and in the range of 0.5 ms to 7.0 ms. In this manner, it is possible to prevent the first electrode **92** from being extremely melted and to increase the temperature of the first electrode **92**. Hereinafter, the details will be described.

In the mixing period alternately having the alternating current and the direct current, when the length of a period for which the direct current is supplied is large, the temperature of the electrodes is rapidly increased and only the projections

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of the electrodes are extremely melted in some cases. In such a case, there is a concern that the growth of the projections is difficult, the electrodes are consumed, and thus, the service life of the discharge lamp is shortened when the projections melted due to a decrease in temperature of the electrodes are solidified again.

Meanwhile, according to the present embodiment, it is possible to suppress a drastic increase in the temperature **H** of the first electrode **92** by setting the length **t1b** of the first DC period **P1b** in the mixing period **P1** in the above-described manner. It is considered that the reason is based on the following principle.

In the present embodiment, since the length **t1b** of the first DC period **P1b** is sufficiently small, the increased width of the temperature **H** of the first electrode **92** in the first DC period **P1b** is small. In this manner, it is possible to prevent the projection **552p** from being extremely melted.

In addition, in the AC period **P1a**, the temperature **H** of the first electrode **92** is maintained and the temperature **H** of the first electrode **92** is increased again due to the first DC period **P1b**. In the present embodiment, since the length **t1a** of the AC period **P1a** is set to be longer than the length **t1b** of the first DC period **P1b**, a temperature gradient with respect to the time **T** of the first electrode **92** becomes gentle.

Further, in the case where the length **t1b** of the first DC period **P1b** is shorter than the length **t1c** of a half cycle of the AC period **P1a**, it is considered that the temperature **H** of the first electrode **92** is not increased or is decreased because the AC period **P1a** is largely affected compared to the first DC period **P1b** in terms of an increase in temperature **H** of the first electrode **92**.

On the contrary, according to the present embodiment, since the length **t1b** of the first DC period **P1b** is longer than the length **t1c** of a half cycle of the AC period **P1a**, the temperature **H** of the first electrode **92** can be increased in the mixing period **P1**.

As described above, according to the present embodiment, it is possible to prevent the projection **552p** of the first electrode **92** from being extremely melted in the mixing period **P1** and to gradually increase the temperature **H** of the first electrode **92**.

Further, since the electrodes of the discharge lamp are deteriorated with time and the projections are easily melted, it is difficult to control the extreme melting of the projections and the growth of the projections. Meanwhile, in the present embodiment, since extreme melting of the projection **552p** can be prevented, a significant effect can be obtained when the discharge lamp **90** is deteriorated with time.

Further, in the present embodiment, for example, the length of each period may be changed in response to deterioration of the discharge lamp **90** and switching a driving mode to the low-power mode. More specifically, in the present embodiment, the length **t2** of the second DC period **P2** and the length **t3** of the third DC period **P3** may be increased in response to deterioration of the discharge lamp **90**. By performing control in this manner, it is possible to allow the projection **552p** of the first electrode **92** to grow appropriately according to a state in which the discharge lamp **90** is deteriorated. Further, in the present embodiment, the discharge lamp driving unit **230** may be controlled such that the length **t1b** of the first DC period **P1b** is decreased in response to the deterioration of the discharge lamp **90**. By performing control in this manner, it is possible to appropriately increase the temperature **H** of the first electrode **92** within the range in which the projection **552p** is not extremely melted in response to a change in ease of melting of the projection **552p**.

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Furthermore, in the embodiment described above, the length $t1b$ of each first DC period $P1b$ is set to be shorter than the length $t1a$ of the AC period $P1a$, longer than the length $t1c$ of a half cycle of the AC period $P1a$, shorter than the length $t2$ of the second DC period $P2$, and in the range of 0.5 ms to 7.0 ms, but the length thereof is not limited thereto. In the present embodiment, for example, the length $t1b$ of the first DC period $P1b$ may be set to be longer than 7.0 ms.

The entire disclosure of Japanese Patent Application No. 2014-047295, filed Mar. 11, 2014 is expressly incorporated by reference herein.

What is claimed is:

1. A discharge lamp driving device comprising:
a discharge lamp driving unit that supplies a driving current for driving a discharge lamp to the discharge lamp; and
a control unit that controls the discharge lamp driving unit, wherein the control unit controls the discharge lamp driving unit such that the driving current having driving periods is supplied to the discharge lamp, the driving period including:
a mixing period which alternately has an AC period in which an alternating current is supplied to the discharge lamp and a first DC period in which a direct current is supplied to the discharge lamp,
a second DC period which is provided immediately after the mixing period and in which a direct current having a polarity which is the same as that of the direct current in the first DC period is supplied to the discharge lamp, and
a third DC period which is provided immediately after the second DC period and in which a direct current having a polarity opposite to that of the direct current in the second DC period is supplied to the discharge lamp,
the length of the second DC period is longer than the length of the first DC period, and
the length of the third DC period is longer than or equal to the length of the first DC period and shorter than the length of the second DC period.
2. The discharge lamp driving device according to claim 1, wherein the driving current has a plurality of the driving periods, and
the direct currents in the first DC periods of the adjacent driving periods have different polarities from each other.
3. The discharge lamp driving device according to claim 1, wherein the length of the first DC period is shorter than the length of the AC period, longer than the length of a half cycle of the alternating current in the AC period, and is shorter than the length of the second DC period.
4. The discharge lamp driving device according to claim 3, wherein the length of the first DC period is equal to or greater than 0.5 ms and equal to or less than 7.0 ms.
5. The discharge lamp driving device according to claim 4, wherein the length of the first DC period is equal to or greater than 1.0 ms and equal to or less than 5.0 ms.
6. The discharge lamp driving device according to claim 1, wherein the number of the first DC periods included in the mixing period is equal to or greater than 5 and equal to or less than 50.
7. The discharge lamp driving device according to claim 1, wherein a frequency of the alternating current in the AC period is equal to or greater than 1 kHz.
8. The discharge lamp driving device according to claim 1, wherein the length of the AC period is equal to or greater than 1 cycle and equal to or less than 20 cycles.
9. A projector comprising:
a discharge lamp that emits light,

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the discharge lamp driving device according to claim 1;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

10. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 2;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

11. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 3;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

12. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 4;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

13. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 5;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

14. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 6;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

15. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 7;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

16. A projector comprising:

a discharge lamp that emits light,
the discharge lamp driving device according to claim 8;
a light modulation element that modulates light emitted from the discharge lamp according to a video signal; and
a projection optical system that projects the light modulated by the light modulation element.

17. A method of driving a discharge lamp that is driven by supplying a driving current to the discharge lamp, the method comprising:

supplying the driving current having driving periods to the discharge lamp, the driving period including:
a mixing period which alternately has an AC period in which an alternating current is supplied to the discharge lamp and a first DC period in which a direct current is supplied to the discharge lamp,
a second DC period which is provided immediately after the mixing period and in which a direct current having

a polarity which is the same as that of the direct
current in the first DC period is supplied to the dis-
charge lamp, and
a third DC period which is provided immediately after
the second DC period and in which a direct current 5
having a polarity opposite to that of the direct current
in the second DC period is supplied to the discharge
lamp,
wherein the length of the second DC period is longer than
the length of the first DC period, and 10
the length of the third DC period is longer than or equal to
the length of the first DC period and shorter than the
length of the second DC period.
18. The method of driving a discharge lamp according to
claim 17, 15
wherein the driving current has a plurality of the driving
periods, and
the direct currents in the first DC periods of the adjacent
driving periods have different polarities from each other.

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