

US009265949B2

(12) **United States Patent**  
**Salo et al.**

(10) **Patent No.:** **US 9,265,949 B2**  
(45) **Date of Patent:** **Feb. 23, 2016**

(54) **METHOD AND APPARATUS FOR CONTROLLING CARDIAC THERAPY BASED ON ELECTROMECHANICAL TIMING**

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(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 3095 days.

(21) Appl. No.: **11/168,024**

(22) Filed: **Jun. 28, 2005**

(65) **Prior Publication Data**  
US 2006/0293714 A1 Dec. 28, 2006

(51) **Int. Cl.**  
*A61N 1/36* (2006.01)  
*A61N 1/362* (2006.01)  
*A61M 5/142* (2006.01)  
*A61N 1/365* (2006.01)  
*A61N 1/375* (2006.01)

(52) **U.S. Cl.**  
CPC ..... *A61N 1/3627* (2013.01); *A61M 5/14276* (2013.01); *A61N 1/36585* (2013.01); *A61N 1/36521* (2013.01); *A61N 1/3756* (2013.01)

(58) **Field of Classification Search**  
CPC ..... A61N 1/3627; A61N 1/56  
USPC ..... 607/4, 5, 9, 18, 62; 600/509, 513-5  
See application file for complete search history.

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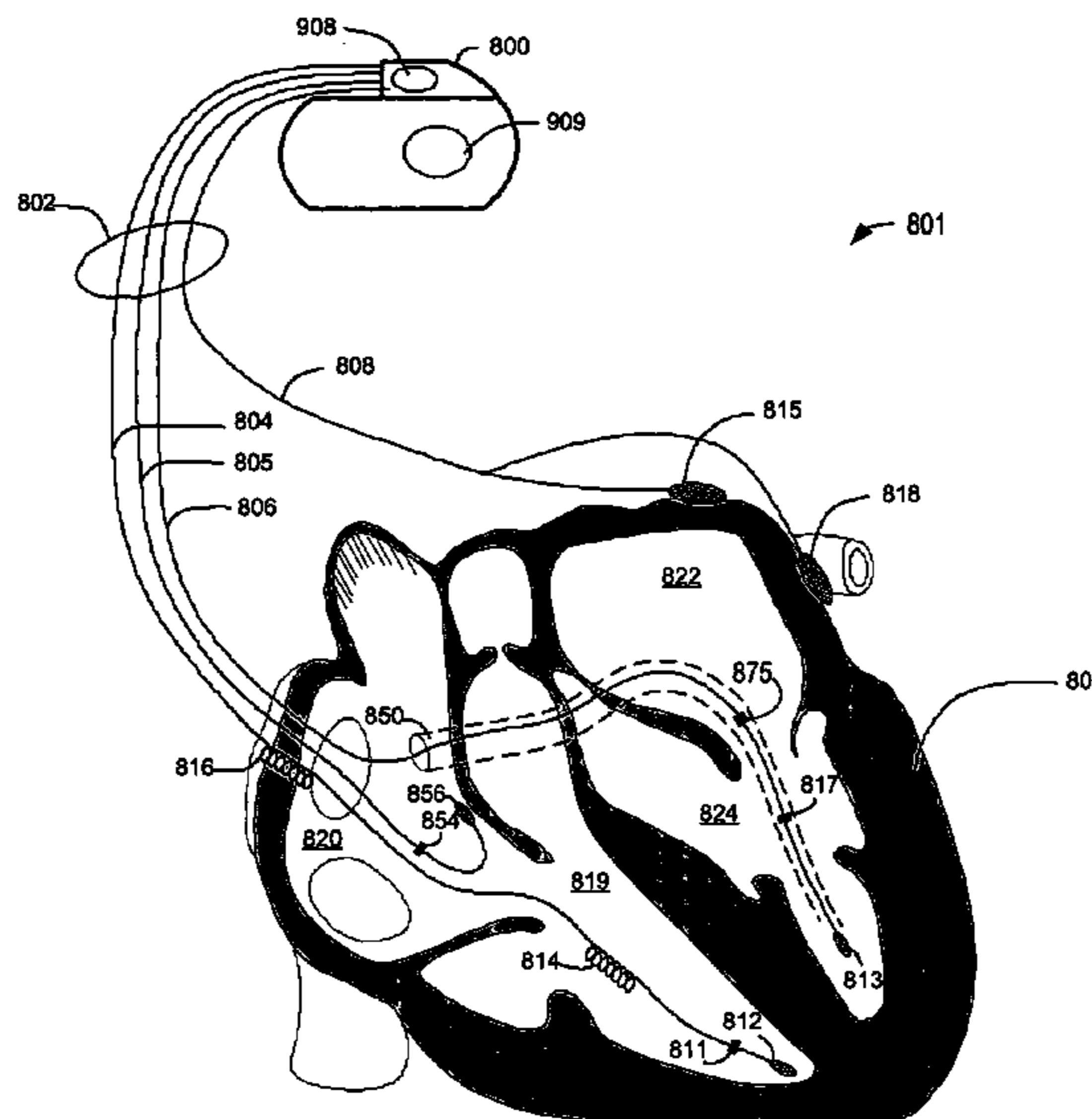
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(57) **ABSTRACT**

Devices and methods for therapy control based on electromechanical timing involve detecting electrical activation of a patient's heart, and detecting mechanical cardiac activity resulting from the electrical activation. A timing relationship is determined between the electrical activation and the mechanical activity. A therapy is controlled based on the timing relationship. The therapy may improve intraventricular dyssynchrony of the patient's heart, or treat at least one of diastolic and systolic dysfunction and/or dyssynchrony of the patient's heart, for example. Electrical activation may be detected by sensing delivery of an electrical stimulation pulse to the heart or sensing intrinsic depolarization of the patient's heart. Mechanical activity may be detected by sensing heart sounds, a change in one or more of left ventricular impedance, ventricular pressure, right ventricular pressure, left atrial pressure, right atrial pressure, systemic arterial pressure and pulmonary artery pressure.

**18 Claims, 5 Drawing Sheets**



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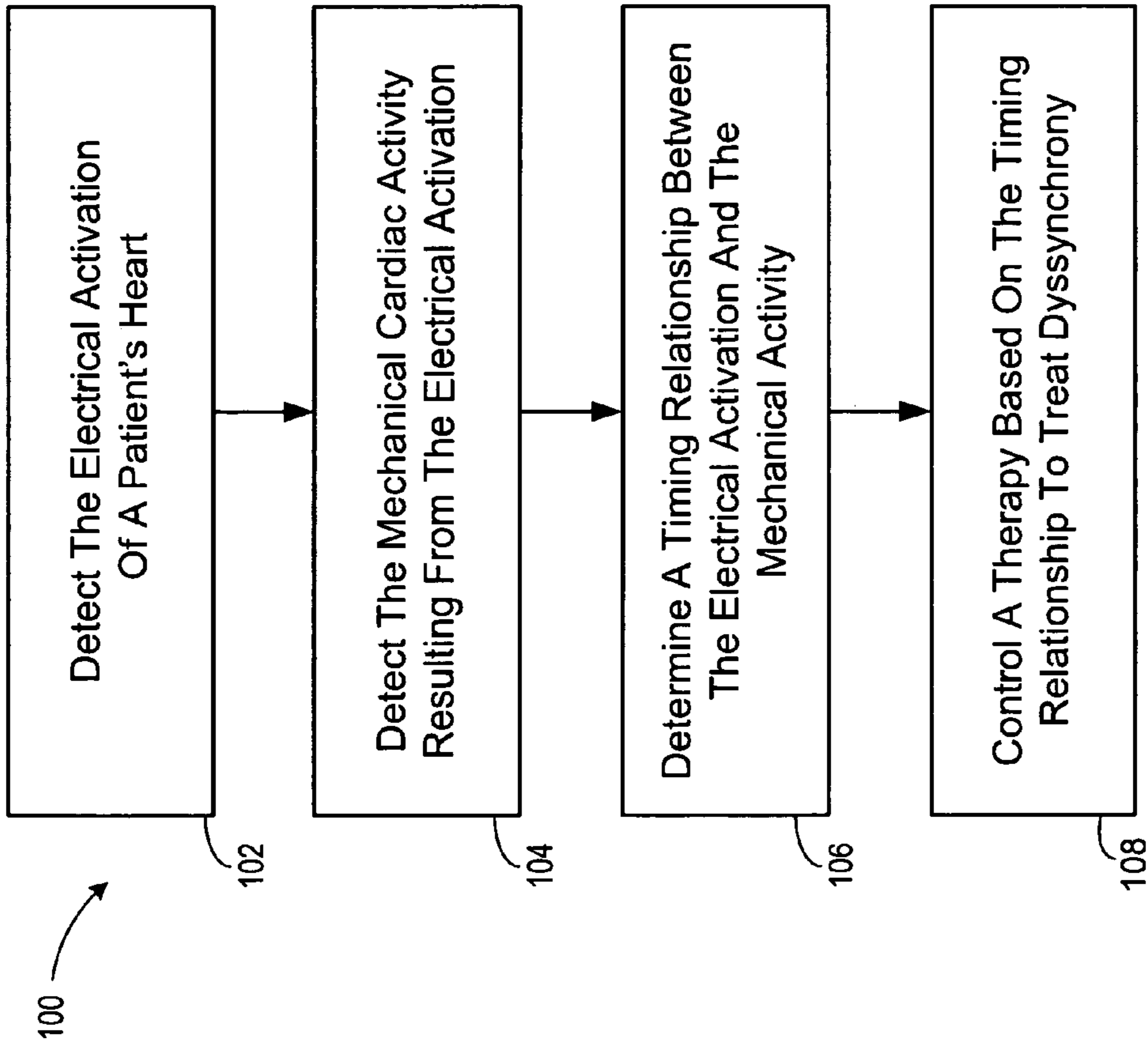


Figure 1A

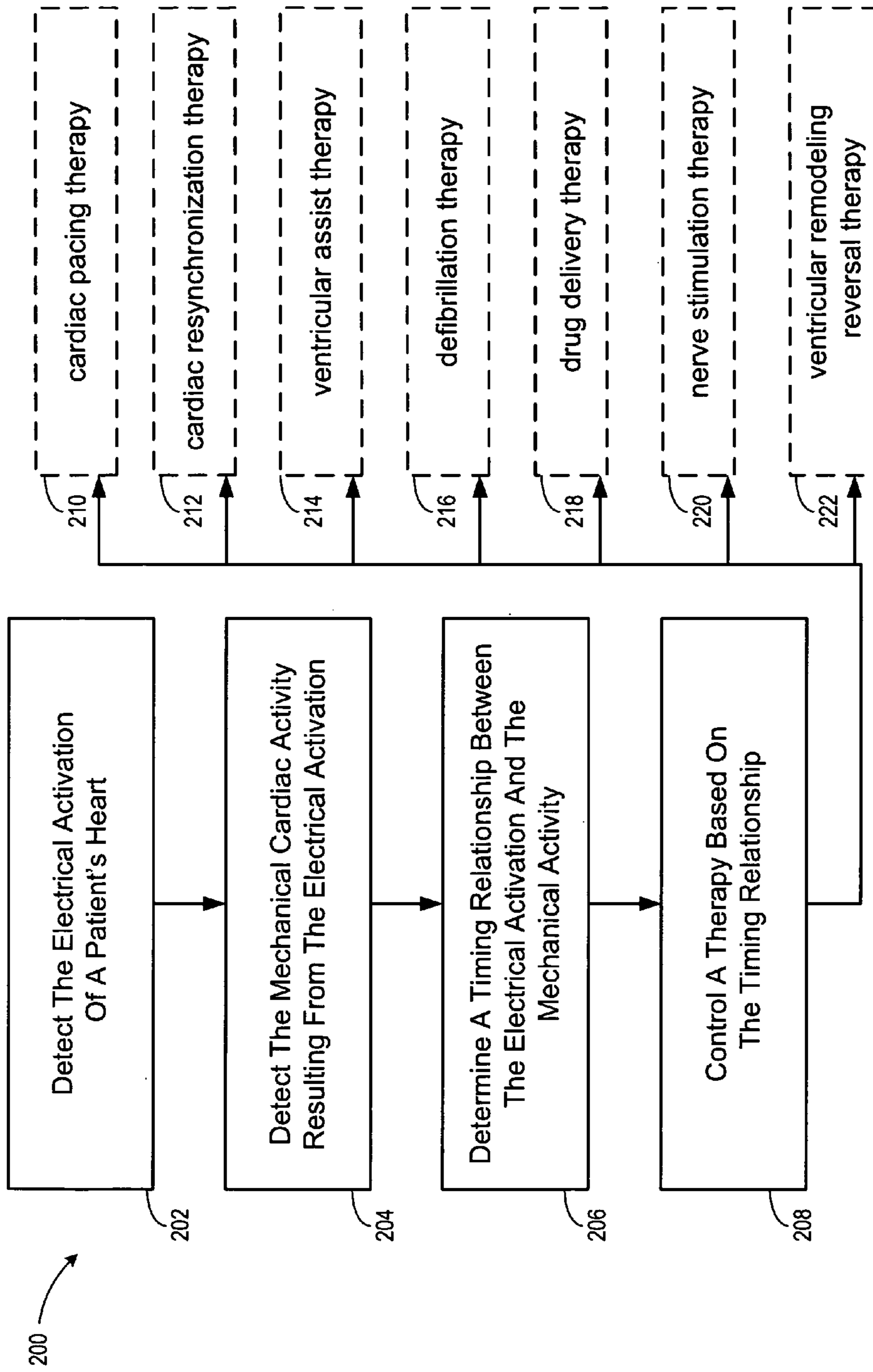


Figure 1B

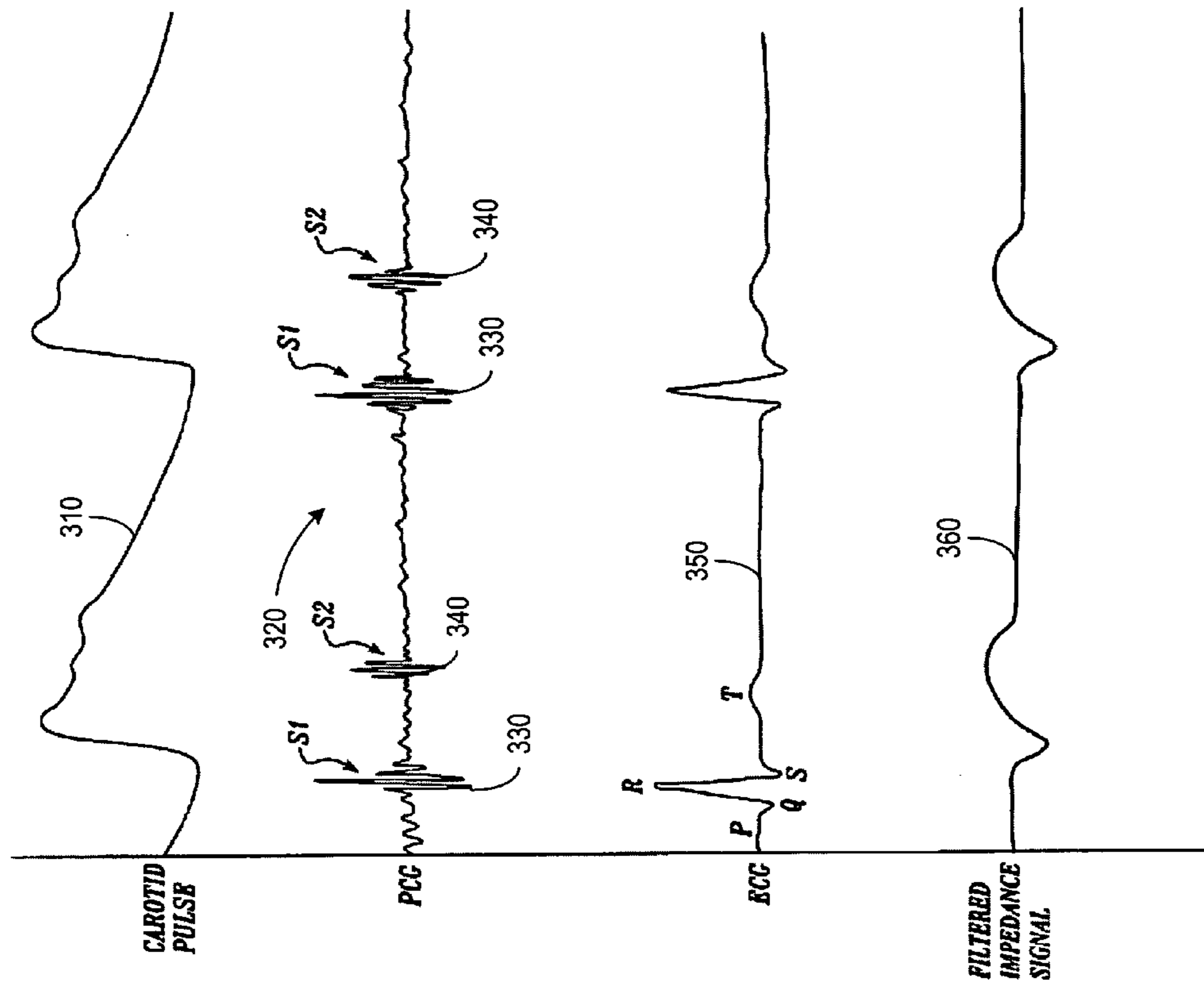


Fig. 2

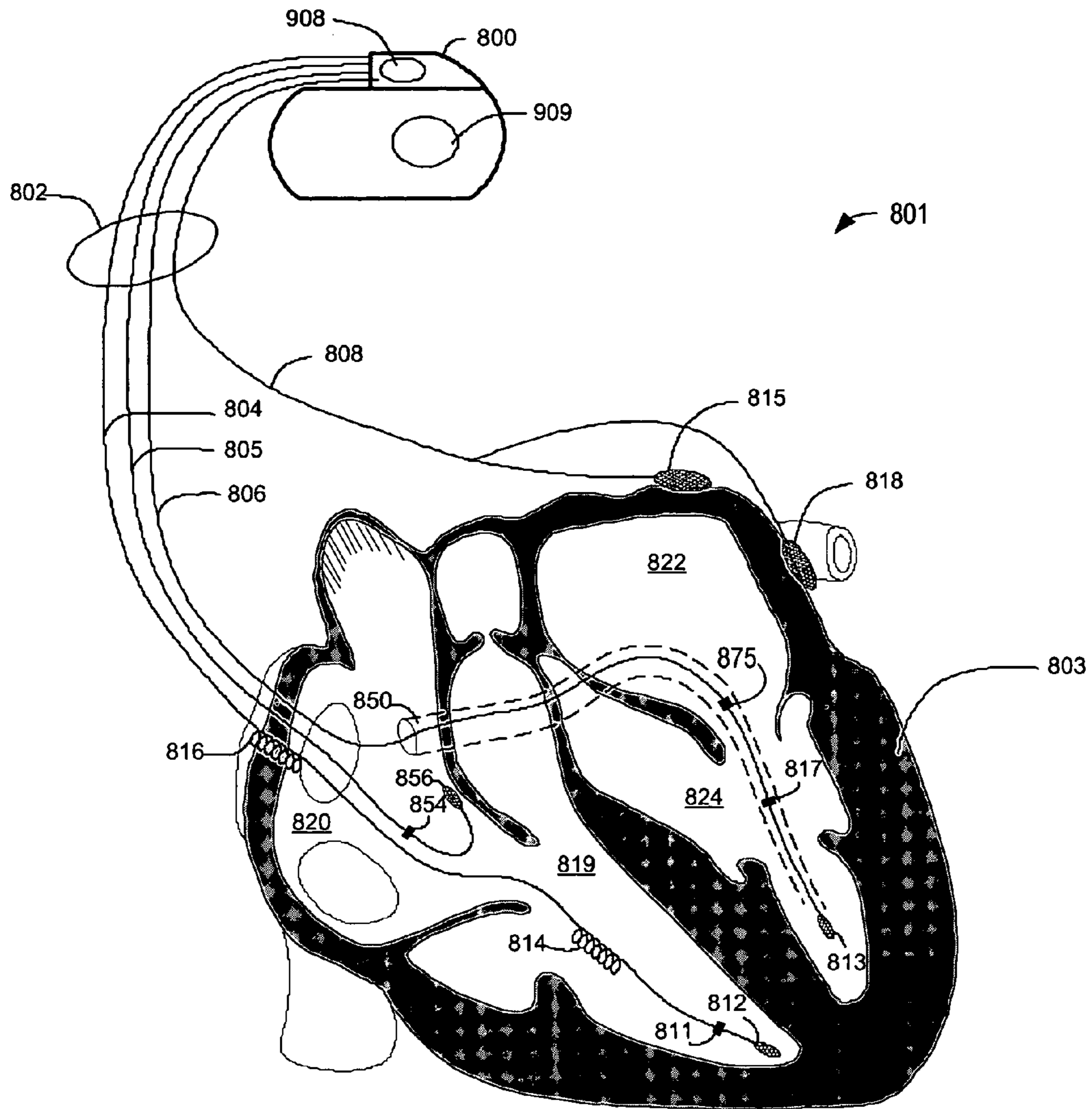


Figure 3

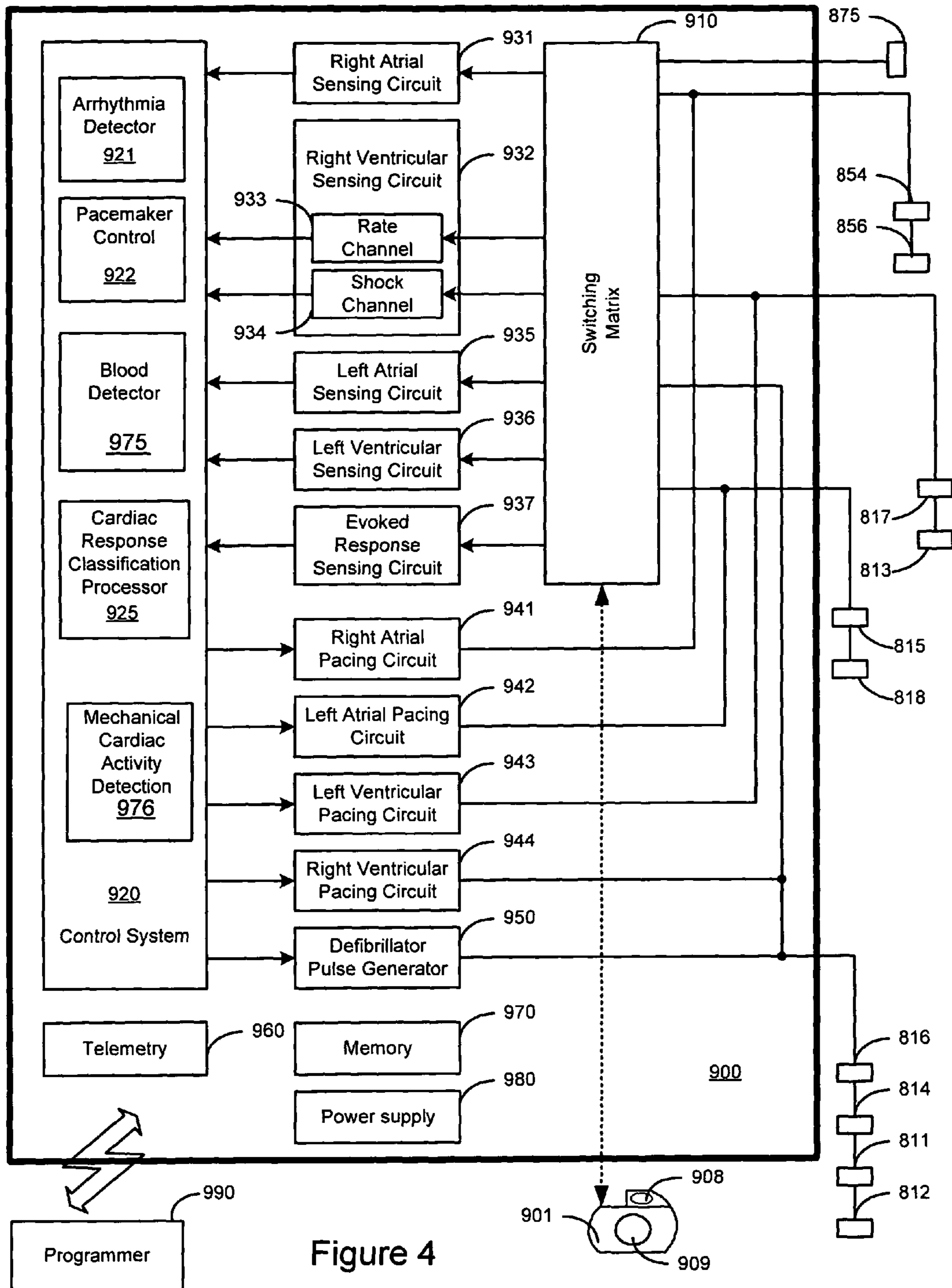


Figure 4

## 1

**METHOD AND APPARATUS FOR  
CONTROLLING CARDIAC THERAPY BASED  
ON ELECTROMECHANICAL TIMING**

FIELD OF THE INVENTION

The present invention relates generally to a method and apparatus for cardiac pacing and, more particularly, to devices and methods for controlling cardiac therapy based on electromechanical timing.

BACKGROUND OF THE INVENTION

Heart disease (cardiomyopathy) can cause a patient to exhibit symptoms of congestive heart failure (CHF). CHF is a result of the weakening of the heart's cardiac function characterized by reduced pumping capacity and efficiency. Chronic cardiac rhythm problems can also be the result of cardiomyopathy. The modification of the heart's structure that causes the reduction in pumping capacity also causes modification of the heart's electrical characteristics. The heart's electrical pathways can become stretched out of shape and chemically damaged. This makes arrhythmias much more likely to occur in CHF patients.

Implantation of a pacemaker is a preferred method of treatment for arrhythmias in CHF patients. Although many types of heart problems may require a pacemaker, one method of treatment suited for CHF patients is known as cardiac resynchronization therapy (CRT). CRT uses a pacemaker with multiple pacing leads to coordinate the heart's chambers to act together in a sequence that will pump blood more efficiently.

It is likely that CRT candidates will have various forms of cardiomyopathy, and these patients may exhibit other measurable symptoms of reduced cardiac function besides arrhythmia. The reduced cardiac function of the heart is taken into account when applying CRT in order to tailor the treatment based on the needs of a particular patient. Various external factors must also be taken into account by the pacing system, one of those factors being the current state of activity of the patient.

Rate adaptive pacemakers are currently used that can estimate body activity by detecting body activity or breathing rate and depth, and therefore modify the pacing rate applied to the heart. These indicators can give a rough estimate of metabolic demand for a given patient. It would be beneficial to have more accurate measures of metabolic demand, especially measures that can determine the pumping capacity and pumping efficiency of a heart in order to measure and improve the efficacy of the therapy for the CHF patient.

SUMMARY OF THE INVENTION

The present invention is directed to a method and apparatus for cardiac pacing and, more particularly, to devices and methods for therapy control based on electromechanical timing. Methods in accordance with embodiments of the present invention involve detecting electrical activation of a patient's heart, and detecting mechanical cardiac activity resulting from the electrical activation. A timing relationship is determined between the detected electrical activation and the detected mechanical cardiac activity. A therapy delivered to the patient is controlled based on the timing relationship to treat dyssynchrony of the patient's heart.

For example, the therapy may be a therapy to improve intraventricular dyssynchrony of the patient's heart, or a therapy to treat at least one of diastolic and systolic dysfunc-

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tion and/or dyssynchrony of the patient's heart. Electrical activation of the heart may be detected by sensing delivery of an electrical stimulation pulse to the heart or sensing intrinsic depolarization of the patient's heart, for example.

Mechanical cardiac activity may be detected by detecting a change in one or more of left ventricular pressure, right ventricular pressure, left atrial pressure, right atrial pressure, systemic arterial pressure and pulmonary artery pressure, indicative of mechanical cardiac activity resulting from the electrical activation, for example. Other embodiments involve detecting the mechanical cardiac activity by detecting a change in blood flow rate or blood perfusion and/or detecting ventricular motion or acceleration indicative of mechanical cardiac activity resulting from the electrical activation. Further methods of detecting the mechanical cardiac activity include transthoracically or intrathoracically detecting a change in ventricular impedance indicative of mechanical cardiac activity resulting from the electrical activation, and detecting heart sounds indicative of mechanical cardiac activity resulting from the electrical activation.

Other embodiments of methods in accordance with the present invention involve detecting electrical activation of a patient's heart using a patient-internal medical device, and detecting mechanical cardiac activity resulting from the electrical activation. A timing relationship is determined between the detected electrical activation and the detected mechanical cardiac activity. A therapy delivered to the patient is controlled based on the timing relationship. The therapy may be one or more of a cardiac pacing therapy, a CRT therapy, a ventricular assist therapy, a defibrillation therapy, a drug delivery therapy, a nerve stimulation therapy, and a ventricular remodeling reversal therapy, for example.

The above summary of the present invention is not intended to describe each embodiment or every implementation of the present invention. Advantages and attainments, together with a more complete understanding of the invention, will become apparent and appreciated by referring to the following detailed description and claims taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1A is a flow chart of a method of therapy control using electromechanical timing information in accordance with the present invention;

FIG. 1B is a flow chart of another method of therapy control using electromechanical timing information in accordance with the present invention;

FIG. 2 is a pictorial diagram of a carotid pulse waveform, a phonocardiogram (PCG) waveform, an electrocardiogram (ECG) waveform, and a filtered transthoracic impedance signal for two consecutive heartbeats;

FIG. 3 is a view of the heart showing an apparatus in accordance with the present invention illustrating a lead system implanted in the heart; and

FIG. 4 is a block diagram of a system in accordance with the present invention.

While the invention is amenable to various modifications and alternative forms, specifics thereof have been shown by way of example in the drawings and will be described in detail below. It is to be understood, however, that the intention is not to limit the invention to the particular embodiments described. On the contrary, the invention is intended to cover all modifications, equivalents, and alternatives falling within the scope of the invention as defined by the appended claims.



### DETAILED DESCRIPTION OF THE VARIOUS EMBODIMENTS

In the following description of the illustrated embodiments, references are made to the accompanying drawings, which form a part hereof, and in which is shown by way of illustration, various embodiments in which the invention may be practiced. It is to be understood that other embodiments may be utilized, and structural and functional changes may be made without departing from the scope of the present invention.

An implanted device in accordance with the present invention may include one or more of the features, structures, methods, or combinations thereof described hereinbelow. For example, a cardiac monitor or a cardiac stimulator may be implemented to include one or more of the advantageous features and/or processes described below. It is intended that such a monitor, stimulator, or other implanted or partially implanted device need not include all of the features described herein, but may be implemented to include selected features that provide for unique structures and/or functionality. Such a device may be implemented to provide a variety of therapeutic or diagnostic functions.

A wide variety of implantable cardiac monitoring and/or stimulation devices may be configured to implement improved cardiac efficiency methodologies of the present invention. A non-limiting, representative list of such devices includes cardiac monitors, pacemakers, cardiovertors, defibrillators, resynchronizers, and other cardiac monitoring and therapy delivery devices. These devices may be configured with a variety of electrode arrangements, including transvenous, endocardial, and epicardial electrodes (i.e., intrathoracic electrodes), and may also include subcutaneous, non-intrathoracic electrodes, including can, header, and indifferent electrodes, and subcutaneous array or lead electrodes (i.e., non-intrathoracic electrodes).

Embodiments of the present invention may be implemented in the context of a wide variety of cardiac devices, such as those listed above, and are referred to herein generally as a patient-internal medical devices (PIMD) for convenience. A PIMD implemented in accordance with the present invention may incorporate one or more of the electrode and sensor types identified herein and/or incorporated herein by reference and/or combinations thereof.

Embodiments of the present invention are directed to devices and methods that use electrical and mechanical timing information to control the operation of a PIMD. The PIMD may also use the electrical and mechanical timing information subsequent to a change in therapy to assess the effectiveness of the therapy. The timing between electrical activity of the heart and the mechanical response of the myocardial tissue is denoted as the electromechanical timing (EMT). The time-period between the electrical stimulation of the myocardial tissue and the mechanical response (e.g. contraction) of the myocardial tissue is denoted as the electromechanical delay (EMD). EMT is a function of sympathetic and parasympathetic balance, as well as the efficiency of the mechanical activation.

The mechanical response of the myocardial tissue may be determined using implantable and/or external sensors. Examples of suitable sensors include pressure sensors, impedance sensors, blood-flow sensors, acoustic sensors, and motion and/or acceleration sensors.

The electrical timing may be established using the timing of stimulation pulses from a PIMD and/or the measured evoked and/or intrinsic electrical activity. EMT/EMD information may be used to initiate, change, and/or titrate thera-

pies for PIMDs, such as intra and/or inter-ventricular delays, atrio-ventricular (AV) delay, pacing therapy, ventricular assist device control, as well as therapies such as neural stimulation, cardiac resynchronization therapy, defibrillation therapy, drug delivery therapy, and ventricular remodeling reversal therapy, for example.

In embodiments of the present invention, the use of EMT/EMD to control therapy may be performed periodically, regularly, or continuously. In other embodiments of the present invention, the use of EMT/EMD to control therapy may be performed only on command, such as from a patient-external device, or only upon existence of a predetermined condition and/or state of the PIMD. It may be desirable to only use mechanical sensors that consume significant energy sparingly, to conserve energy. In other embodiments, the EMT/EMD may be determined using sensors, such as transthoracic impedance sensors, without incremental energy loss from the sensor. For example, the sensor may be patient-external, such as a wearable sensor, that may have an independent power source.

One example of a device that may benefit from EMT/EMD control in accordance with the present invention is a rate adaptive pacing system that may be controlled to increase rate during decreased EMD. In another example, a cardiac resynchronization therapy (CRT) system may use EMT/EMD information to minimize EMD during patient rest periods, thereby maximizing synchrony of the heart. In a further example, a sudden change in EMD along with increase in heart rate may be used to confirm a ventricular tachycardia. Further, a sudden increase in EMD may indicate a loss of capture, and initiate a capture threshold algorithm, for example. EMT/EMD information may also be useful to monitor a patient's left heart/global function, including contractility and intracardiac synchrony, as another example.

EMT/EMD measurement for PIMD control in accordance with the present invention is applicable to patients receiving therapy for inter or intraventricular dyssynchrony. This includes patients currently indicated for CRT as well as patients with diastolic dysfunction and dyssynchrony, as well as post myocardial infarction (MI) patients undergoing remodeling control therapy.

A particular embodiment in accordance with the present invention involves measuring the time interval between paced or intrinsic electrical activation of the left ventricle, and the beginning of global mechanical activation as measured by an increase in the impedance between a coronary vein electrode on the lateral wall and an electrode in either the right ventricle or right atrium.

In a patient with dyssynchronous contraction and relaxation of the heart (e.g. patients undergoing CRT therapy), the EMD shortens as the activation of the ventricle becomes more synchronous. Under resting or other steady-state conditions, therapy parameters may be varied to search for the combination that results in the shortest (or shortened) EMD. The EMD may also be monitored to assess the worsening or improving cardiac dyssynchrony of the patient. This information may be recorded locally, or transmitted via telemetry to a patient-external device, as will be further described below.

FIG. 1A is a flow chart of a method 100 of therapy control to treat dyssynchrony of a patient's heart using electromechanical timing information in accordance with the present invention. The method 100 involves detecting 102 electrical activation of a patient's heart, and detecting 104 mechanical cardiac activity resulting from the electrical activation. A timing relationship is determined 106 between the detected electrical activation 102 and the detected mechanical cardiac

activity **104**. A therapy delivered to the patient is controlled **108** based on the timing relationship to treat dyssynchrony of the patient's heart.

For example, the therapy may be a therapy to improve intraventricular dyssynchrony of the patient's heart, or a therapy to treat at least one of diastolic and systolic dysfunction and/or dyssynchrony of the patient's heart. Electrical activation of the heart may be detected **102** by sensing delivery of an electrical stimulation pulse to the heart or sensing intrinsic depolarization of the patient's heart.

Mechanical cardiac activity may be detected **104** by detecting a change in at least one of left ventricular pressure, right ventricular pressure, left atrial pressure, right atrial pressure, systemic arterial pressure and pulmonary artery pressure, indicative of mechanical cardiac activity resulting from the electrical activation, for example. Detecting **104** the mechanical cardiac activity may also be done by transthoracically or intrathoracically detecting a change in ventricular impedance indicative of mechanical cardiac activity resulting from the electrical activation, or by detecting heart sounds indicative of mechanical cardiac activity resulting from the electrical activation. Other ways of detecting **104** the mechanical cardiac activity include detecting a change in blood flow rate or blood perfusion and/or detecting ventricular motion or acceleration indicative of mechanical cardiac activity resulting from the electrical activation.

FIG. **1B** is a flow chart of a method **200** of therapy control using electromechanical timing information in accordance with the present invention. The method **200** involves detecting electrical activation **202** of a patient's heart using a patient-internal medical device, and detecting mechanical cardiac activity **204** resulting from the electrical activation. A timing relationship is determined **206** between the detected electrical activation **202** and the detected mechanical cardiac activity **204**. A therapy delivered to the patient is controlled **208** based on the timing relationship. The therapy may be one or more of a cardiac pacing therapy **210**, a CRT therapy **212**, a ventricular assist therapy **214**, a defibrillation therapy **216**, a drug delivery therapy **218**, a nerve stimulation therapy **220**, and a ventricular remodeling reversal therapy **222**, for example.

Ventricular assist therapy **214** may include a left ventricular assist device (LAVD) that either takes over or assists the pumping role of the left ventricle, the heart's main pumping chamber. LVADs may be permanent in people with severe heart failure. In an LAVD, part of the device is implanted in a patient's heart and abdomen, and part remains outside the body. The external part of the device may be carried on a belt around the patient's waist or on a shoulder strap. Typically, LVADs have an electric pump, an electronic controller, an energy supply (usually a battery weighing about 8 pounds) and 2 tubes. One tube carries blood from the left ventricle into the device. The other tube takes blood pumped from the device into the aorta (artery) to be circulated throughout the body.

LVADs are used to "unload" the heart (by taking over some of the pumping activity) to allow it to recover from some injury, or to assist for patients with chronic heart failure (CHF). The electromechanical timing in accordance with the present invention may be used to control the degree of unloading that takes place, and permits the heart to handle more load as it recovers, or less load if a relapse occurs.

Drug delivery therapy **218** may include a drug-delivery system for local delivery of inotropes, Angiotensin II receptor blockers (ARBs), or other drugs through cardiac veins to

control contractility. This system may use feedback control via electromechanical interval measurement in accordance with the present invention.

Nerve stimulation therapy **220** may be performed using a Vagus nerve stimulator that reduces contractility in the context of hypertension or cardiac injury, for example. Nerve stimulation therapy **220** may be used to retard or prevent adverse remodeling. Feedback (via EMT/EMD) may be used in accordance with the present invention to maintain the desired degree of therapy during daily activities such as exercise, sleep, etc.

Detecting mechanical cardiac activity **204** resulting from the electrical activation may be done using a subcutaneous sensor, such as an accelerometer or acoustic transducer, which may be used to detect heart sounds as will be described in more detail below. The heart sounds may be used to determine EMD information and timing in accordance with the present invention. A PIMD device may utilize one or more of the presence, characteristics, and frequency of occurrence of the heart sound combined with ECG information when determining EMT and EMD.

A heart rate determined from the ECG signal may, for example, be analyzed along with heart sound information. It should also be noted that other sensor-derived signals could replace heart sounds. For example, impedance, pulse pressure, blood volume/flow, or cardiac accelerations could be used.

Various types of acoustic sensors may be used to detect heart sounds. Examples of such acoustic sensors include diaphragm based acoustic sensors, MEMS-based acoustic sensors such as a MEMS-based acoustic transducer, fiber optic acoustic sensors, piezoelectric sensors, and accelerometer based acoustic sensors and arrays. These sensors may be used to detect the audio frequency pressure waves associated with the heart sounds, and may also be used to detect other non-electrophysiologic cardiac related signals.

The presence of cardiac pulse, or heartbeat, in a patient is generally detected by palpating the patient's neck and sensing changes in the volume of the patient's carotid artery due to blood pumped from the patient's heart. A graph of a carotid pulse signal **310**, representative of the physical expansion and contraction of a patient's carotid artery during two consecutive pulses, or heartbeats, is shown at the top of FIG. **2**. When the heart's ventricles contract during a heartbeat, a pressure wave is sent throughout the patient's peripheral circulation system. The carotid pulse signal **310** shown in FIG. **2** rises with the ventricular ejection of blood at systole and peaks when the pressure wave from the heart reaches a maximum. The carotid pulse signal **310** falls off again as the pressure subsides toward the end of each pulse.

The opening and closing of the patient's heart valves during a heartbeat causes high-frequency vibrations in the adjacent heart wall and blood vessels. These vibrations can be heard in the patient's body as heart sounds, and may be detected by sensors, as described earlier. A conventional phonocardiogram (PCG) transducer placed on a patient converts the acoustical energy of the heart sounds to electrical energy, resulting in a PCG waveform **320** that may be recorded and displayed, as shown by the graph in the upper middle portion of FIG. **2**.

As indicated by the PCG waveform **320** shown in FIG. **2**, a typical heartbeat produces two main heart sounds. A first heart sound **330**, denoted **S1**, is generated by vibration generally associated with the closure of the tricuspid and mitral valves at the beginning of systole. Typically, the heart sound **330** is about 14 milliseconds long and contains frequencies up to approximately 500 Hz. A second heart sound **340**, denoted

S2, is generally associated with vibrations resulting from the closure of the aortic and pulmonary valves at the end of systole. While the duration of the second heart sound **340** is typically shorter than the first heart sound **330**, the spectral bandwidth of the second heart sound **340** is typically larger than that of the first heart sound **330**.

An electrocardiogram (ECG) waveform **350** describes the electrical activity of a patient's heart. The graph in the lower middle portion of FIG. 2 illustrates an example of the ECG waveform **350** for two heartbeats and corresponds in time with the carotid pulse signal **310** and PCG waveform **320** also shown in FIG. 2. Referring to the first shown heartbeat, the portion of the ECG waveform **350** representing depolarization of the atrial muscle fibers is referred to as the "P" wave. Depolarization of the ventricular muscle fibers is collectively represented by the "Q," "R," and "S" waves of the ECG waveform, referred to as the QRS complex. Finally, the portion of the waveform representing repolarization of the ventricular muscle fibers is known as the "T" wave. Between heartbeats, the ECG waveform **350** returns to an isopotential level.

Fluctuations in a patient's transthoracic impedance signal **360** also correlate with the patient's electromechanical timing and EMD. The bottom graph of FIG. 2 illustrates an example of a filtered transthoracic impedance signal **360** for a patient in which fluctuations in impedance correspond in time with the carotid pulse signal **310**, the PCG waveform **320**, and ECG waveform **350**, also shown in FIG. 2. Impedance signals that may be useful in accordance with the present invention include transthoracic impedance, measured between the PIMD housing and an electrode, or may include local impedance measurements from implanted electrodes, such as bipolar electrodes, for example.

Given that EMD information can be a useful indicator of heart performance, the EMD information can be beneficially applied to adaptively change therapy parameters, for example, of a cardiac pacing or defibrillation system. Further, analyzing EMD information can provide a pacing system with the ability to measure and adapt to heart activity over a long period of time in order to measure and improve the efficacy of the pacing treatment for the CHF patient.

Turning now to FIG. 3, a system in accordance with the present invention is shown having a lead system deployed within a heart. A PIMD system **801** includes a PIMD **800** with a lead system **802** that is designed for implantation in a coronary vein for purposes of CRT. The lead system **802** is coupled to a detection/energy delivery system **900** (illustrated in FIG. 4) that actively measures and controls the implanted lead system to provide cardiac pacing therapy to a patient's heart **803**.

The detector/energy delivery system **900** typically includes a power supply and programmable circuit (e.g., microprocessor) coupled to an analog to digital (A-D) converter. Various lead system devices, such as electrodes and pressure sensors, can interface to the A-D converter for sensing/data collection. Alternatively, analog conditioning (e.g., filtering) may be applied to sensor signals before interfacing with the A-D converter. The detector/energy delivery system **900** also utilizes an energy delivery system. The energy delivery system may include charge capacitors and signal conditioning circuitry known in the art. The energy system may interface to the programmable circuit through a D-A converter. Components and functionality of the detector/energy delivery system **900** will be further described below with reference to FIG. 4.

Still referring to FIG. 3, the lead system **802** may be implanted into the coronary sinus using various techniques. One such technique, as illustrated in FIG. 3, involves creating

an opening in a percutaneous access vessel such as the left subclavian or left cephalic vein. The pacing lead is guided into a right atrial chamber **820** of the heart via the superior vena cava. From the right atrial chamber **820**, the lead system **802** is sent into the coronary sinus ostium. The ostium is the opening of a coronary sinus **850** into the right atrial chamber **820**. The lead system **802** is guided through the coronary sinus **850** to a coronary vein of the left ventricle **824**. A distal end of the lead system **802** may be lodged into the coronary vein.

The PIMD system **801** may be used to implement methods for therapy control based on electromechanical timing in accordance with the present invention. The PIMD system **801** in FIG. 3 is illustrated having the PIMD **800** electrically and physically coupled to the lead system **802**. The housing and/or header of the PIMD **800** may incorporate one or more electrodes **908**, **909** used to provide electrical stimulation energy to the heart and to sense cardiac electrical activity. The PIMD **800** may utilize all or a portion of the PIMD housing as a can electrode **909**. The PIMD **800** may include an indifferent electrode positioned, for example, on the header or the housing of the PIMD **800**. If the PIMD **800** includes both a can electrode **909** and an indifferent electrode **908**, the electrodes **908**, **909** typically are electrically isolated from each other.

The lead system **802** is used to provide pacing signals to the heart **803**, detect electric cardiac signals produced by the heart **803**, sense blood oxygen saturation, and may also be used to provide electrical energy to the heart **803** under certain predetermined conditions to treat cardiac arrhythmias. The lead system **802** may include one or more electrodes used for pacing, sensing, and/or defibrillation. In the embodiment shown in FIG. 3, the lead system **802** includes an intracardiac right ventricular (RV) lead system **804**, an intracardiac right atrial (RA) lead system **805**, an intracardiac left ventricular (LV) lead system **806**, and an extracardiac left atrial (LA) lead system **808**. The lead system **802** of FIG. 3 illustrates one embodiment that may be used in connection with therapy control based on electromechanical timing methodologies described herein. Other leads and/or electrodes may additionally or alternatively be used.

The lead system **802** may include intracardiac leads **804**, **805**, **806** implanted in a human body with portions of the intracardiac leads **804**, **805**, **806** inserted into a heart **803**. The intracardiac leads **804**, **805**, **806** include various electrodes positionable within the heart for sensing electrical activity of the heart and for delivering electrical stimulation energy to the heart, for example, pacing pulses and/or defibrillation shocks to treat various arrhythmias of the heart.

As illustrated in FIG. 3, the lead system **802** may include one or more extracardiac leads **808** having electrodes, e.g., epicardial electrodes or sensors **815**, **818**, positioned at locations outside the heart for sensing and/or pacing one or more heart chambers.

The right ventricular lead system **804** illustrated in FIG. 3 includes an SVC-coil **816**, an RV-coil **814**, an RV-ring electrode **812**, and an RV-tip electrode **811**. The right ventricular lead system **804** extends through the right atrium **820** and into the right ventricle **819**. In particular, the RV-tip electrode **811**, RV-ring electrode **812**, and RV-coil electrode **814** are positioned at appropriate locations within the right ventricle **819** for sensing and delivering electrical stimulation pulses to the heart. The SVC-coil **816** is positioned at an appropriate location within the right atrium chamber **820** of the heart **803** or a major vein leading to the right atrial chamber **820** of the heart **803**.

In one configuration, the RV-tip electrode **811** referenced to the can electrode **909** may be used to implement unipolar pacing and/or sensing in the right ventricle **819**. Bipolar pacing and/or sensing in the right ventricle may be implemented using the RV-tip **811** and RV-ring **812** electrodes. In yet another configuration, the RV-ring **812** electrode may optionally be omitted, and bipolar pacing and/or sensing may be accomplished using the RV-tip electrode **811** and the RV-coil **814**, for example. The right ventricular lead system **804** may be configured as an integrated bipolar pace/shock lead. The RV-coil **814** and the SVC-coil **816** are defibrillation electrodes.

The left ventricular lead **806** includes an LV distal electrode **817** and an LV proximal electrode **813** located at appropriate locations in or about the left ventricle **824** for pacing and/or sensing the left ventricle **824**. The left ventricular lead **806** may be guided into the right atrium **820** of the heart via the superior vena cava. From the right atrium **820**, the left ventricular lead **806** may be deployed into the coronary sinus ostium, the opening of the coronary sinus **850**. The lead **806** may be guided through the coronary sinus **850** to a coronary vein of the left ventricle **824**. This vein is used as an access pathway for leads to reach the surfaces of the left ventricle **824** which are not directly accessible from the right side of the heart, and to sense blood oxygen levels in the blood leaving the myocardium. Lead placement for the left ventricular lead **806** may be achieved via subclavian vein access and a preformed guiding catheter for insertion of the LV electrodes **817**, **813** adjacent to the left ventricle.

Unipolar pacing and/or sensing in the left ventricle may be implemented, for example, using the LV distal electrode referenced to the can electrode **909**. The LV distal electrode **817** and the LV proximal electrode **813** may be used together as bipolar sense and/or pace electrodes for the left ventricle. The left ventricular lead **806** and the right ventricular lead **804**, in conjunction with the PIMD **800**, may be used to provide cardiac resynchronization therapy such that the ventricles of the heart are paced substantially simultaneously, or in phased sequence, to provide enhanced cardiac pumping efficiency in accordance with the present invention for patients suffering from chronic heart failure.

The right atrial lead **805** includes a RA-tip electrode **854** and an RA-ring electrode **856** positioned at appropriate locations in the right atrium **820** for sensing and pacing the right atrium **820**. In one configuration, the RA-tip **854** referenced to the can electrode **909**, for example, may be used to provide unipolar pacing and/or sensing in the right atrium **820**. In another configuration, the RA-tip electrode **854** and the RA-ring electrode **856** may be used to provide bipolar pacing and/or sensing.

The left ventricular lead **806**, as shown in FIG. 3, may include a pressure transducer **875**. The pressure transducer **875** used in this application can be a micro-electrical-mechanical system (MEMS), for example. MEMS technology uses semiconductor techniques to build microscopic mechanical devices in silicon or similar materials. The pressure transducer **875** can include a micromachined capacitive or piezoresistive transducer exposed to the bloodstream. Other pressure transducer technologies, such as resistive strain gages, are known in the art and can also be employed as a pressure transducer **875**. The pressure transducer **875** is coupled to one or more conductors disposed along the length of the left ventricular lead **806**. In the configuration shown in FIG. 3, the pressure transducer **875** is integrated with the left ventricular lead **806**. Transducers such as the pressure transducer **875** may be used to determine pulmonary arterial (PA) pressure information useful for determining EMD informa-

tion in accordance with the present invention. Pressure sensor devices and methodologies are further described in U.S. Pat. No. 6,237,398, which is hereby incorporated herein by reference.

Referring now to FIG. 4, there is shown an embodiment of a PIMD **900** suitable for therapy control based on electromechanical timing in accordance with the present invention. FIG. 4 shows the PIMD **900** divided into functional blocks. It is understood by those skilled in the art that there exist many possible configurations in which these functional blocks can be arranged. The example depicted in FIG. 4 is one possible functional arrangement. Other arrangements are also possible. For example, more, fewer or different functional blocks may be used to describe a PIMD suitable for implementing the methodologies for adaptive windowing in accordance with the present invention. In addition, although the PIMD **900** depicted in FIG. 4 contemplates the use of a programmable microprocessor-based logic circuit, other circuit implementations may be utilized.

The PIMD **900** depicted in FIG. 4 includes circuitry for receiving cardiac signals from a heart and delivering electrical stimulation energy to the heart in the form of pacing pulses and/or defibrillation shocks. In one embodiment, the circuitry of the PIMD **900** is encased and hermetically sealed in a housing **901** suitable for implanting in a human body. Power to the PIMD **900** is supplied by an electrochemical battery **980**. A connector block (not shown) is attached to the housing **901** of the PIMD **900** to allow for the physical and electrical attachment of the lead system conductors to the circuitry of the PIMD **900**.

The PIMD **900** may be a programmable microprocessor-based system, including a controller **920** and a memory **970**. The memory **970** may store parameters for various pacing, defibrillation, and sensing modes, along with other parameters. Further, the memory **970** may store data indicative of signals received by other components of the PIMD **900**. The memory **970** may be used, for example, for storing historical EMT/EMD information, blood oxygen levels, blood flow information, perfusion information, heart sounds, heart movement, EGM, and/or therapy data. The historical data storage may include, for example, data obtained from long-term patient monitoring used for trending or other diagnostic purposes. Historical data, as well as other information, may be transmitted to an external programmer unit **990** as needed or desired.

The controller **920** and memory **970** may cooperate with other components of the PIMD **900** to control the operations of the PIMD **900**. The control system depicted in FIG. 4 incorporates a processor **925** for classifying cardiac responses to pacing stimulation. The controller **920** may include additional functional components including a pacemaker control circuit **922**, an arrhythmia detector **921**, and a template processor for cardiac signal morphology analysis, along with other components for controlling the operations of the PIMD **900**. The controller **920** may include blood detector circuitry **975** configured to determine blood perfusion, blood flow, and/or blood pressure based on one or more sensors. The controller **920** may optionally, or additionally, include mechanical cardiac activity detection circuitry **976** configured to detect mechanical cardiac activity using sensor information from, for example, an accelerometer, a microphone, a pressure transducer, impedance sensors, or other motion or sound sensing arrangements.

Telemetry circuitry **960** may be implemented to provide communications between the PIMD **900** and an external programmer unit **990**. In one embodiment, the telemetry circuitry **960** and the programmer unit **990** communicate using

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a wire loop antenna and a radio frequency telemetric link, as is known in the art, to receive and transmit signals and data between the programmer unit **990** and the telemetry circuitry **960**. In this manner, programming commands and other information may be transferred to the controller **920** of the PIMD **900** from the programmer unit **990** during and after implant. In addition, stored cardiac data pertaining to EMT/EMD, capture threshold, capture detection and/or cardiac response classification, for example, along with other data, may be transferred to the programmer unit **990** from the PIMD **900**.

The telemetry circuitry **960** may also allow the PIMD device to communicate with one or more receiving devices or systems situated external to the PIMD device. By way of example, the PIMD device may communicate with a patient-worn, portable or bedside communication system via the telemetry circuitry **960**. In one configuration, one or more physiologic or non-physiologic sensors (subcutaneous, cutaneous, or external of patient) may be equipped with a short-range wireless communication interface, such as an interface conforming to a known communications standard, such as Bluetooth or IEEE 802 standards. Data acquired by such sensors may be communicated to the PIMD device via the telemetry circuitry **960**. It is noted that physiologic or non-physiologic sensors equipped with wireless transmitters or transceivers may communicate with a receiving system external of the patient. The external sensors in communication with the PIMD may be used to determine electromechanical timing and/or delays in accordance with embodiments of the present invention.

In the embodiment of the PIMD **900** illustrated in FIG. 3, electrodes RA-tip **854**, RA-ring **856**, RV-tip **811**, RV-ring **812**, RV-coil **814**, SVC-coil **816**, LV distal electrode **817**, LV proximal electrode **813**, LA distal electrode **818**, LA proximal electrode **815**, indifferent electrode **908**, and can electrode **909** are coupled through a switch matrix **910** to sensing circuits **931-937**.

A right atrial sensing circuit **931** serves to detect and amplify electrical signals from the right atrium of the heart. Bipolar sensing in the right atrium may be implemented, for example, by sensing voltages developed between the RA-tip **854** and the RA-ring **856**. Unipolar sensing may be implemented, for example, by sensing voltages developed between the RA-tip **854** and the can electrode **909**. Outputs from the right atrial sensing circuit are coupled to the controller **920**.

A right ventricular sensing circuit **932** serves to detect and amplify electrical signals from the right ventricle of the heart. The right ventricular sensing circuit **932** may include, for example, a right ventricular rate channel **933** and a right ventricular shock channel **934**. Right ventricular cardiac signals sensed through use of the RV-tip **811** electrode are right ventricular near-field signals and are denoted RV rate channel signals. A bipolar RV rate channel signal may be sensed as a voltage developed between the RV-tip **811** and the RV-ring **812**. Alternatively, bipolar sensing in the right ventricle may be implemented using the RV-tip electrode **811** and the RV-coil **814**. Unipolar rate channel sensing in the right ventricle may be implemented, for example, by sensing voltages developed between the RV-tip **811** and the can electrode **909**.

Right ventricular cardiac signals sensed through use of the RV-coil electrode **814** are far-field signals, also referred to as RV morphology or RV shock channel signals. More particularly, a right ventricular shock channel signal may be detected as a voltage developed between the RV-coil **814** and the SVC-coil **816**. A right ventricular shock channel signal may also be detected as a voltage developed between the RV-coil **814** and the can electrode **909**. In another configuration the can electrode **909** and the SVC-coil electrode **816** may be

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electrically shorted and a RV shock channel signal may be detected as the voltage developed between the RV-coil **814** and the can electrode **909**/SVC-coil **816** combination.

Left atrial cardiac signals may be sensed through the use of one or more left atrial electrodes **815**, **818**, which may be configured as epicardial electrodes. A left atrial sensing circuit **935** serves to detect and amplify electrical signals from the left atrium of the heart. Bipolar sensing and/or pacing in the left atrium may be implemented, for example, using the LA distal electrode **818** and the LA proximal electrode **815**. Unipolar sensing and/or pacing of the left atrium may be accomplished, for example, using the LA distal electrode **818** to can vector **909** or the LA proximal electrode **815** to can vector **909**.

Referring still to FIG. 4, a left ventricular sensing circuit **936** serves to detect and amplify electrical signals from the left ventricle of the heart. Bipolar sensing in the left ventricle may be implemented, for example, by sensing voltages developed between the LV distal electrode **817** and the LV proximal electrode **813**. Unipolar sensing may be implemented, for example, by sensing voltages developed between the LV distal electrode **817** or the LV proximal electrode **813** and the can electrode **909**.

Optionally, an LV coil electrode (not shown) may be inserted into the patient's cardiac vasculature, e.g., the coronary sinus, adjacent the left heart. Signals detected using combinations of the LV electrodes, **817**, **813**, LV coil electrode (not shown), and/or can electrodes **909** may be sensed and amplified by the left ventricular sensing circuitry **936**. The output of the left ventricular sensing circuit **936** is coupled to the controller **920**.

Measuring LVP may be useful in accordance with the present invention to measure the EMD. For example, in cardiac therapy using bi-ventricular pacing (e.g., CRT), benefits are obtained from synchronizing the contractions of the right and left ventricle using pacing electrodes. If a method or apparatus for acquiring a right ventricular pressure (RVP) signal is provided (for example, via a pressure transducer incorporated into a right ventricular pacing lead) and the left ventricular pressure signal is acquired from a coronary venous lead, the degree of synchronization of these two chambers can be assessed by plotting RVP versus the LVP and determining the area of the resulting approximately elliptical shape. This elliptical shape is referred to as a PP Loop. Methods and systems for measuring the left ventricular pressure are further described in U.S. Pat. No. 6,666,826, which is hereby incorporated herein by reference.

A method and apparatus for using the PP Loop for characterizing therapy for CHF patients is described in commonly owned U.S. Pat. No. 6,280,389, which is hereby incorporated herein by reference. A given parameter (e.g., atrioventricular delay or interventricular delay) associated with CRT may be optimized by varying the parameter(s) to minimize the PP Loop area. This process can be carried out periodically to correct for physiological changes that may occur in the course of the disease or therapy. The relative timing or phase of these pressure signals may be extracted by analysis of maximum or minimum threshold values from time domain pressure readings. Relative phasing can also be determined from the frequency domain by analyzing the fundamental of a Fourier analysis, such as by use of a Fast Fourier Transform (e.g., FFT) analysis. The computation required to perform FFT and/or extract timing values from pressure signals is known in the art and can be readily implemented in the controller.

Various PIMD embodiments described herein may be used in connection with advanced patient management. Methods, structures, and/or techniques described herein, which may be

adapted to provide for remote patient/device monitoring, diagnosis, therapy, or other APM related methodologies, may incorporate features of one or more of the following references: U.S. Pat. Nos. 6,221,011; 6,270,457; 6,277,072; 6,280,380; 6,312,378; 6,336,903; 6,358,203; 6,368,284; 6,398,728; and 6,440,066, which are hereby incorporated herein by reference.

Various modifications and additions can be made to the preferred embodiments discussed hereinabove without departing from the scope of the present invention. Accordingly, the scope of the present invention should not be limited by the particular embodiments described above, but should be defined only by the claims set forth below and equivalents thereof.

What is claimed is:

1. A method of treating dyssynchrony of a patient's heart, comprising:

detecting electrical depolarization of a patient's ventricular tissue;

detecting mechanical cardiac activity of the ventricular tissue resulting from the electrical depolarization;

determining a timing relationship between the detected electrical depolarization and the detected mechanical cardiac activity; and

controlling a therapy delivered to the patient based on the timing relationship to treat at least one of intraventricular dyssynchrony and dyssynchrony between the left and right ventricles, wherein at least one of the steps of determining and controlling is implemented at least in part by a circuit.

2. The method of claim 1, wherein the detected mechanical cardiac activity comprises at least one of contraction and relaxation of the patient's heart.

3. The method of claim 1, wherein the therapy comprises a therapy to improve interventricular dyssynchrony of the patient's heart.

4. The method of claim 1, wherein the therapy comprises a therapy to treat at least one of diastolic and systolic dysfunction of the patient's heart.

5. The method of claim 1, wherein the therapy comprises a therapy to treat at least one of diastolic and systolic dyssynchrony.

6. The method of claim 1, wherein the therapy comprises a ventricular remodeling reversal therapy.

7. The method of claim 1, wherein the therapy comprises a therapy to improve dyssynchrony between the left and right ventricles.

8. The method of claim 1, wherein detecting the mechanical cardiac activity comprises detecting a change in at least one of left ventricular pressure, right ventricular pressure, left

atrial pressure, right atrial pressure, systemic arterial pressure and pulmonary artery pressure, indicative of mechanical cardiac activity resulting from the electrical depolarization.

9. The method of claim 1, wherein detecting the mechanical cardiac activity comprises transthoracically or intrathoracically detecting a change in ventricular impedance indicative of mechanical cardiac activity resulting from the electrical depolarization.

10. The method of claim 1, wherein detecting the mechanical cardiac activity comprises detecting heart sounds indicative of mechanical cardiac activity resulting from the electrical depolarization.

11. The method of claim 1, wherein detecting the mechanical cardiac activity comprises detecting a change in blood flow rate or blood perfusion indicative of mechanical cardiac activity resulting from the electrical depolarization.

12. The method of claim 1, wherein detecting the mechanical cardiac activity comprises detecting ventricular motion or acceleration indicative of mechanical cardiac activity resulting from the electrical depolarization.

13. The method of claim 1, wherein each of detecting electrical depolarization and detecting mechanical cardiac activity is performed patient-internally.

14. The method of claim 1, wherein the electrical depolarization of the patient's ventricular tissue is evoked by a pace pulse.

15. The method of claim 1, wherein the electrical depolarization of the patient's ventricular tissue is caused by intrinsic electrical activation of the patient's heart.

16. The method of claim 1, wherein controlling the therapy delivered to the patient comprises controlling the therapy to reduce a time interval between the detected electrical depolarization and the detected mechanical cardiac activity.

17. The method of claim 1, further comprising performing a capture test and detecting capture using the timing relationship.

18. An implantable cardiac device, comprising:  
means for detecting electrical depolarization of a patient's ventricular tissue;

means for detecting mechanical cardiac activity of the ventricular tissue resulting from the electrical depolarization;

means for determining a timing relationship between the detected electrical depolarization and the detected mechanical cardiac activity; and

means for controlling a therapy delivered to the patient based on the timing relationship to treat at least one of intraventricular dyssynchrony and dyssynchrony between the left and right ventricles.

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