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Chen et al.

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(54) **IMAGE CAPTURING LENS ASSEMBLY,
IMAGE CAPTURING DEVICE AND MOBILE
TERMINAL**

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G02B 13/00 (2006.01)
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CPC **G02B 13/0035** (2013.01); **G02B 9/12**
(2013.01); **H01L 27/14625** (2013.01)

(58) **Field of Classification Search**

CPC G02B 9/12; G02B 13/0035
USPC 359/784, 791
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(56) **References Cited**

U.S. PATENT DOCUMENTS

8,094,231 B2 1/2012 Tsai
2004/0021957 A1* 2/2004 Isono 359/791
2005/0041306 A1* 2/2005 Matsuo 359/689
2006/0092529 A1* 5/2006 Zeng et al. 359/784
2007/0279767 A1* 12/2007 Murakami et al. 359/791
2013/0170050 A1 7/2013 Lu et al.
2013/0201380 A1 8/2013 Choi

(Continued)

FOREIGN PATENT DOCUMENTS

JP 200298889 4/2002
JP 2003322792 A 11/2003

(Continued)

OTHER PUBLICATIONS

Intellectual Property Office, Ministry of Economic Affairs, R.O.C.,
"Office Action", Sep. 4, 2014, Taiwan.

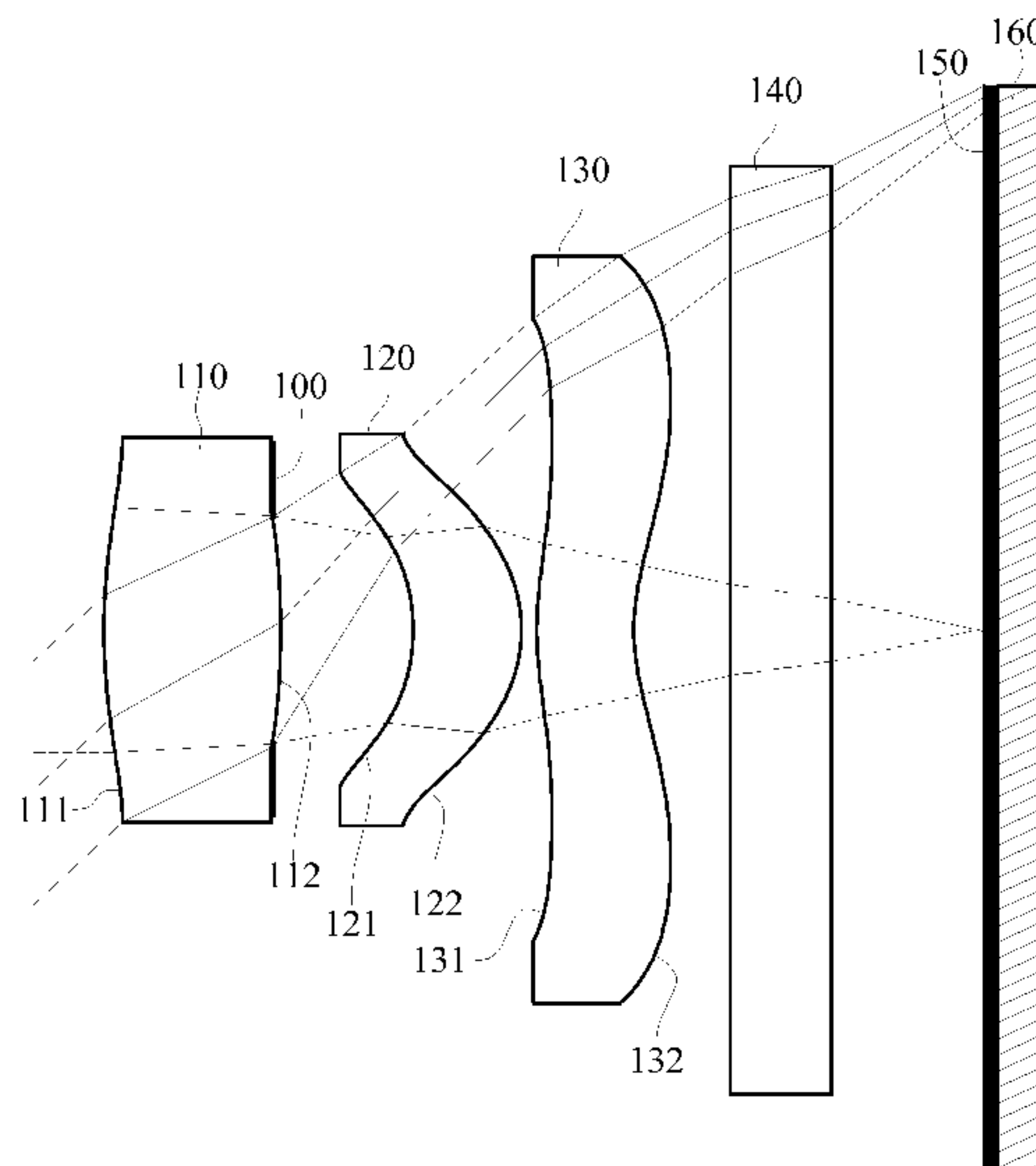
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(57) **ABSTRACT**

An image capturing lens assembly includes, in order from an
object side to an image side, a first lens element, a second lens
element and a third lens element. The first lens element with
positive refractive power has a convex object-side surface and
a convex image-side surface, wherein the surfaces of the first
lens element are aspheric. The second lens element with
positive refractive power has a concave object-side surface
and a convex image-side surface, wherein the surfaces of the
second lens element are aspheric. The third lens element with
negative refractive power has a concave image-side surface in
a paraxial region thereof, wherein the image-side surface of
the third lens element has at least one convex shape in an
off-axis region thereof, and the surfaces of the third lens
element are aspheric. The image capturing lens assembly has
a total of three lens elements with refractive power.

23 Claims, 18 Drawing Sheets



(56)

References Cited

U.S. PATENT DOCUMENTS

2014/0071522 A1 3/2014 Hsu et al.
2014/0247510 A1 9/2014 Kwon
2015/0002727 A1 1/2015 Chen
2015/0029600 A1 1/2015 Kim et al.

FOREIGN PATENT DOCUMENTS

JP 2004163849 A 6/2004
JP 2004163850 A 6/2004

JP 2004302060 A 10/2004
JP 2005242286 A 9/2005
JP 2005250512 A 9/2005
JP 2005250513 A 9/2005
JP 2005258467 A 9/2005
JP 2007127953 A 5/2007
JP 2007127960 A 5/2007
JP 2012108230 A 6/2012
TW 201115180 A 5/2011
WO 2012114970 A1 8/2012
WO 2013048089 A1 4/2013

* cited by examiner

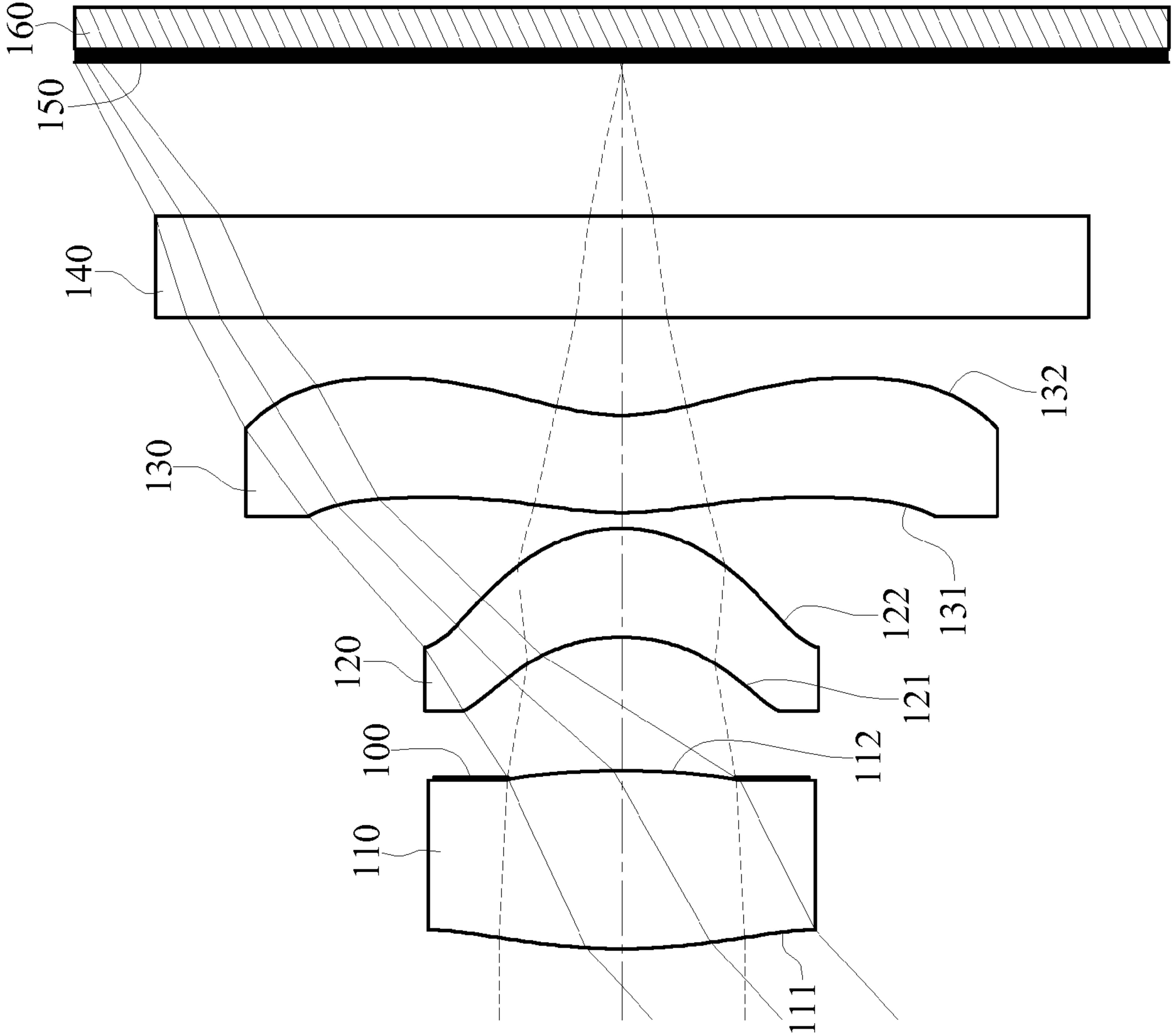


FIG.1

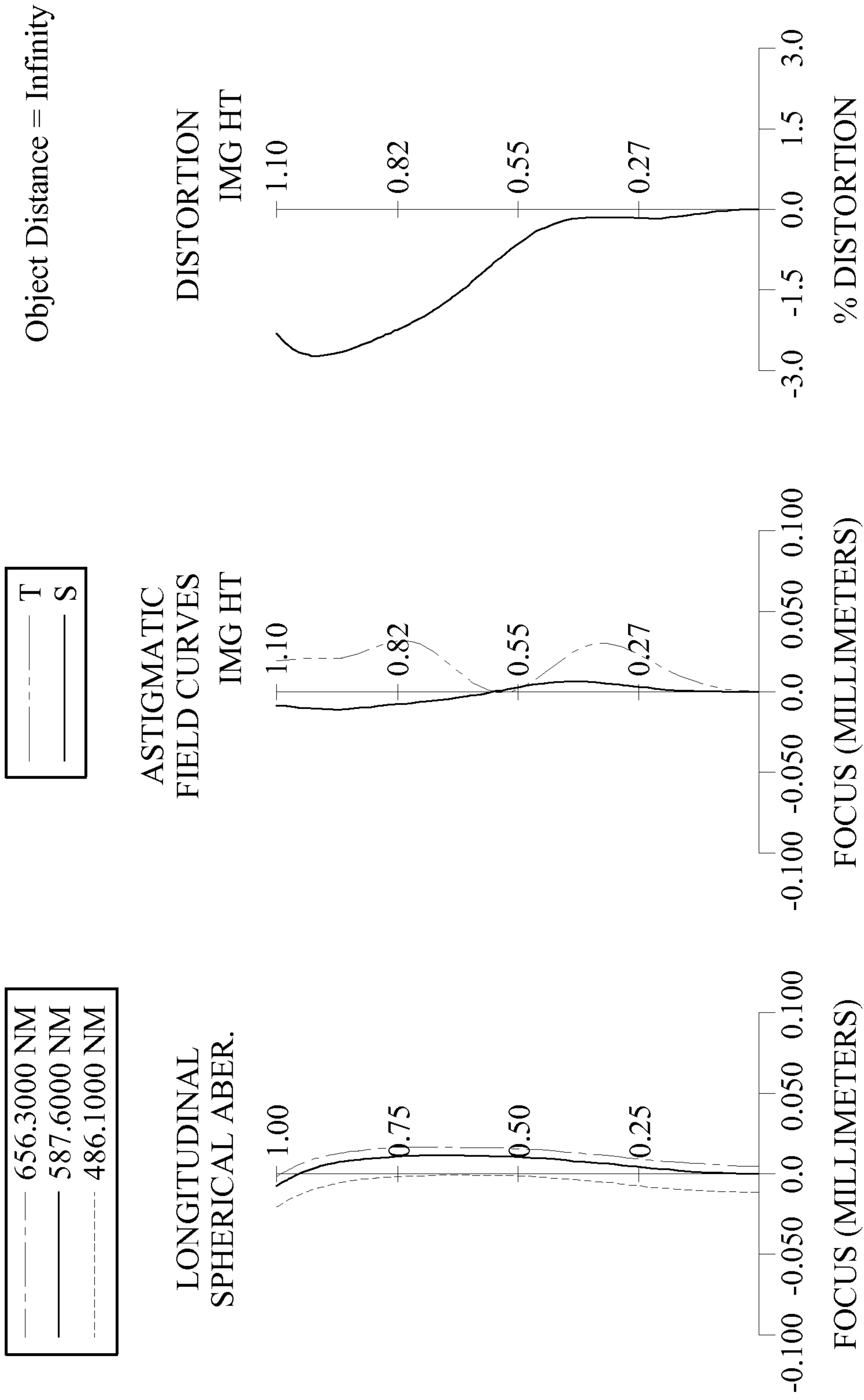


FIG.2

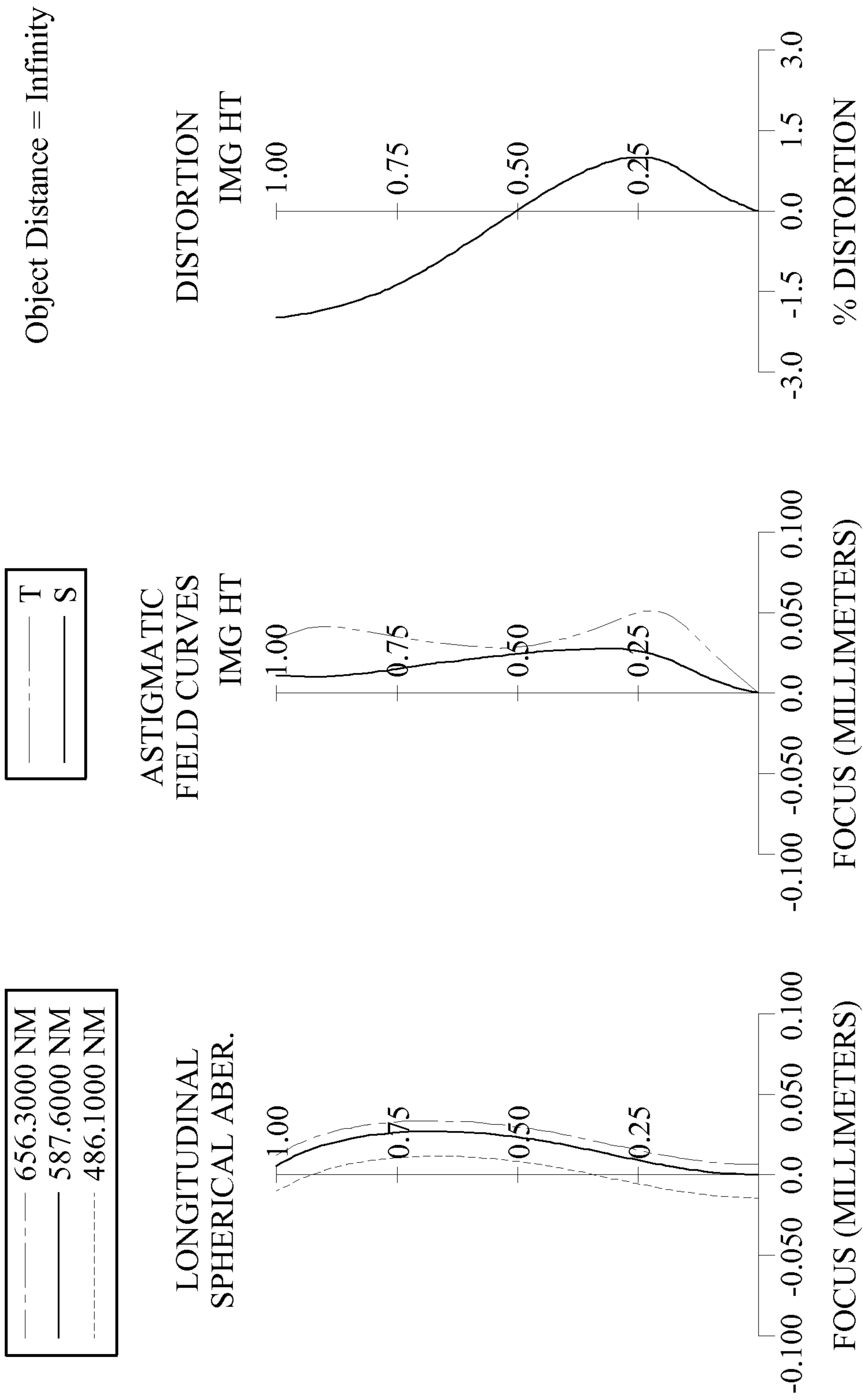


FIG.4

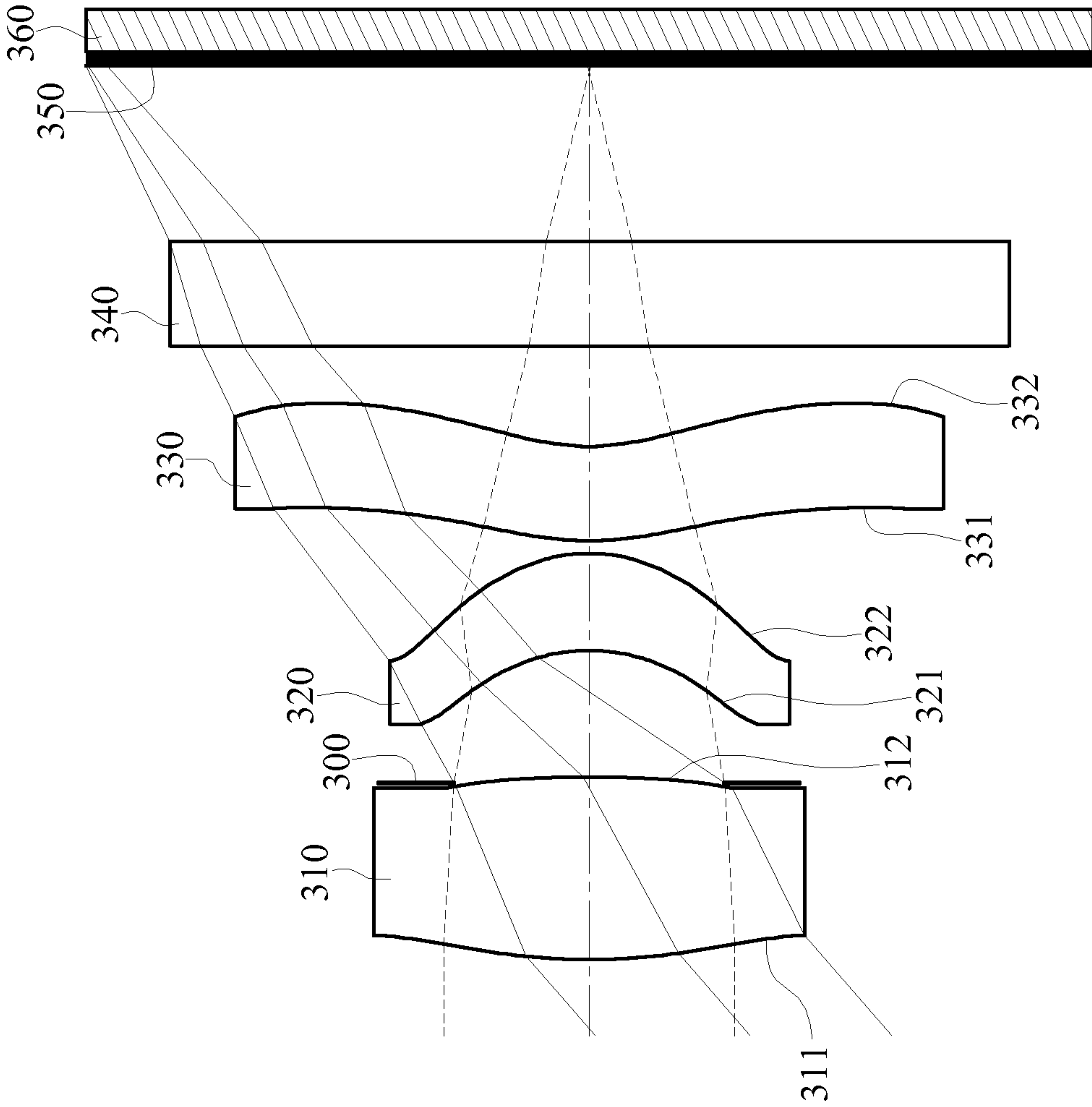


FIG.5

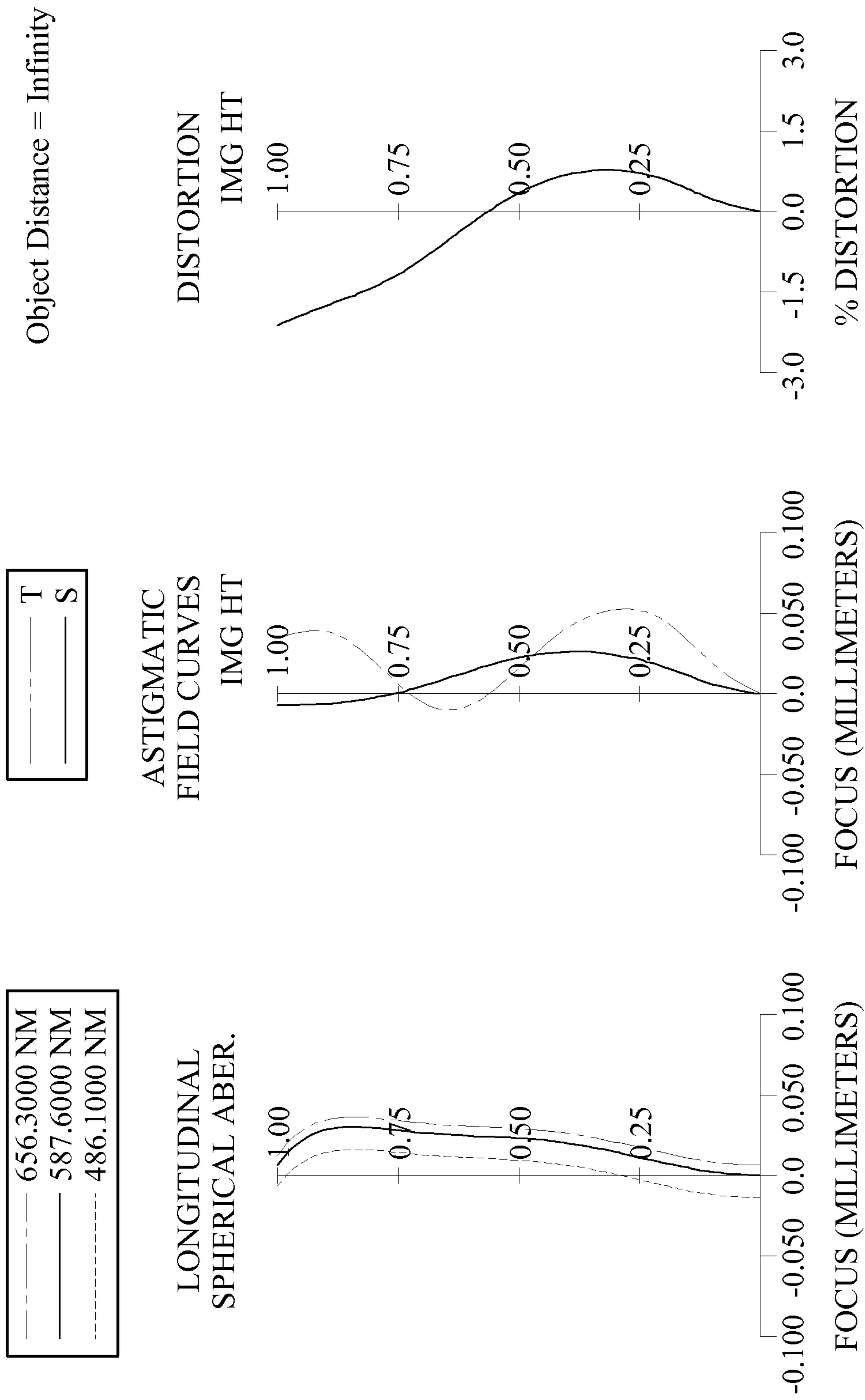


FIG.6

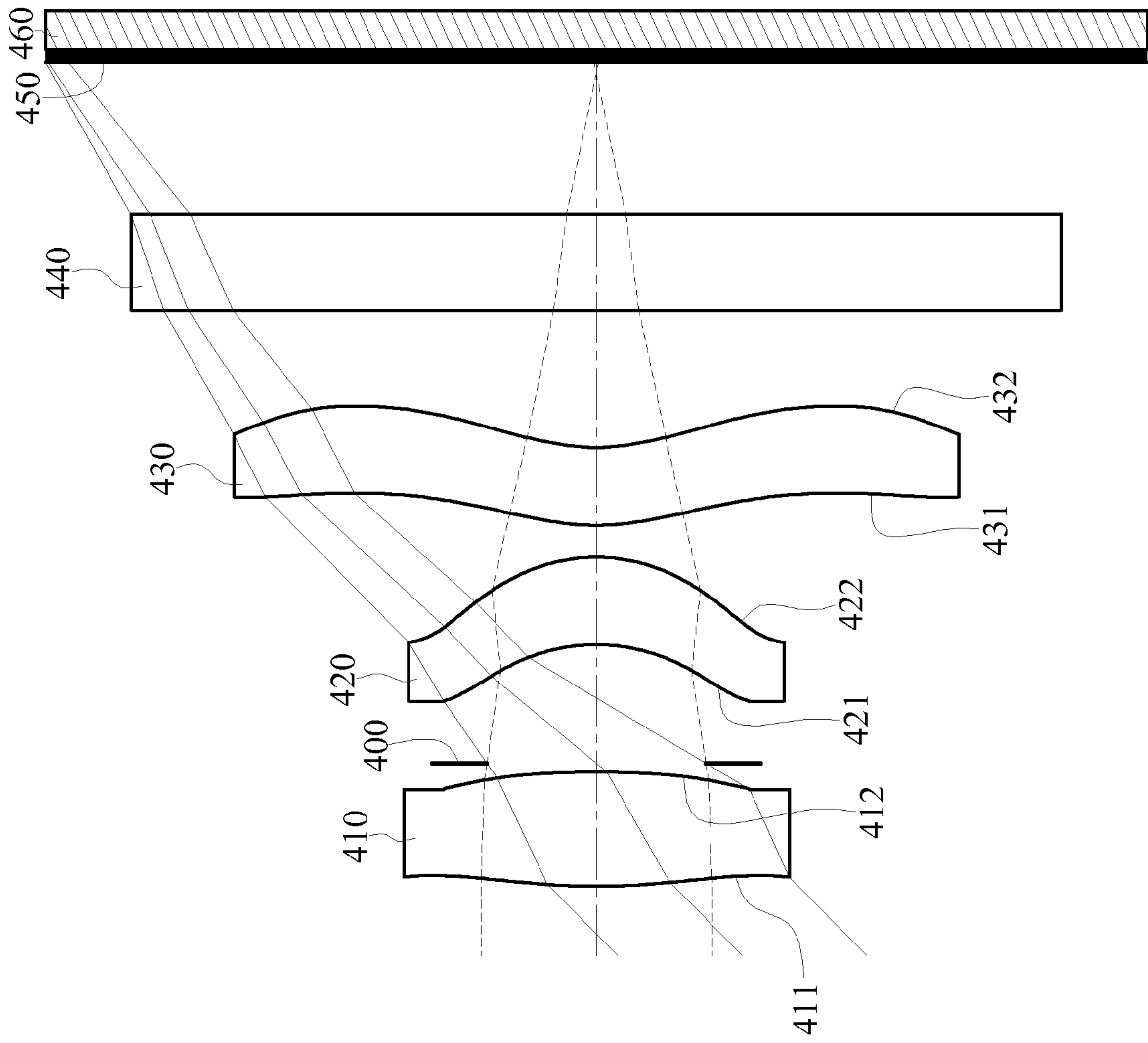


FIG. 7

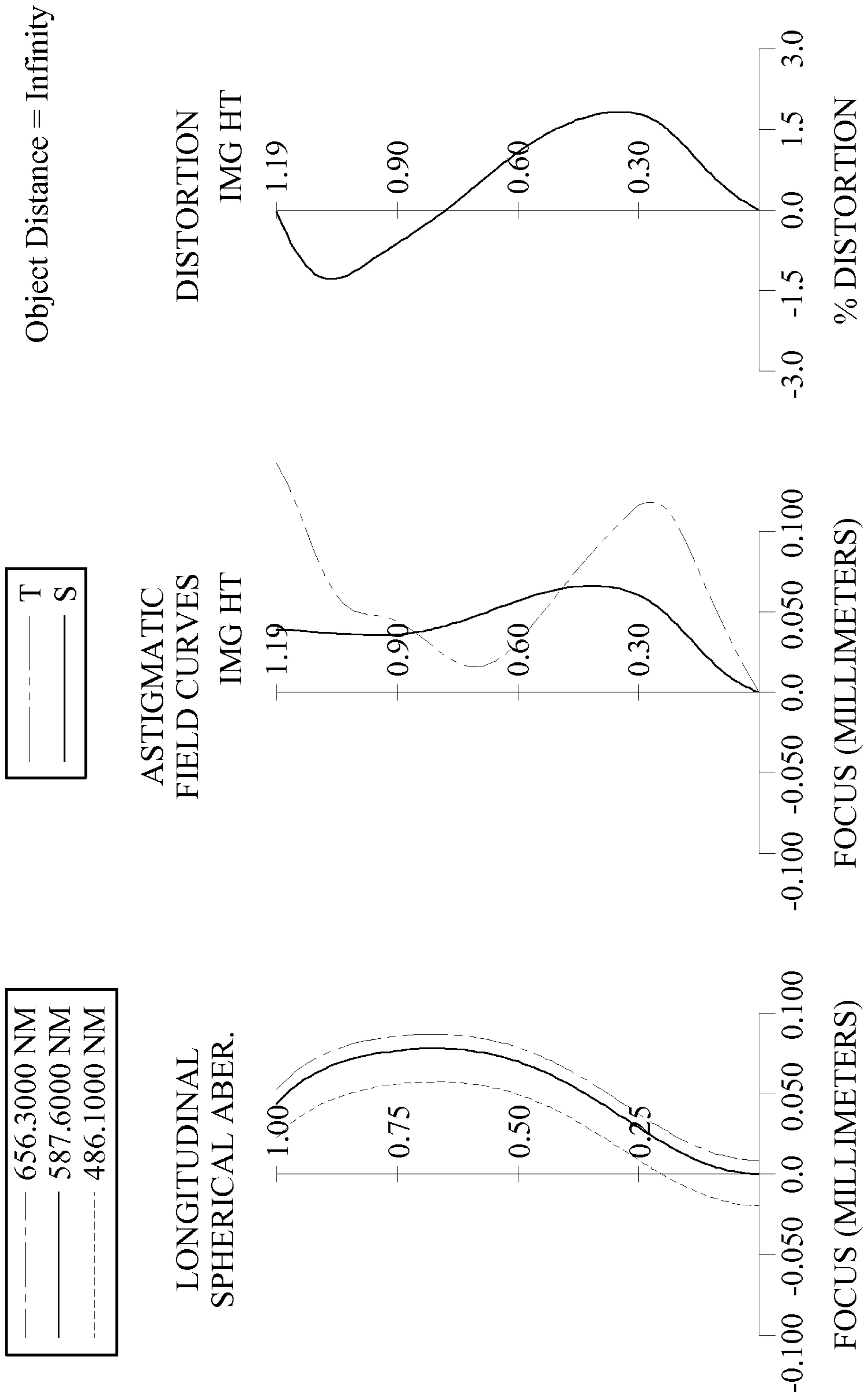


FIG.8

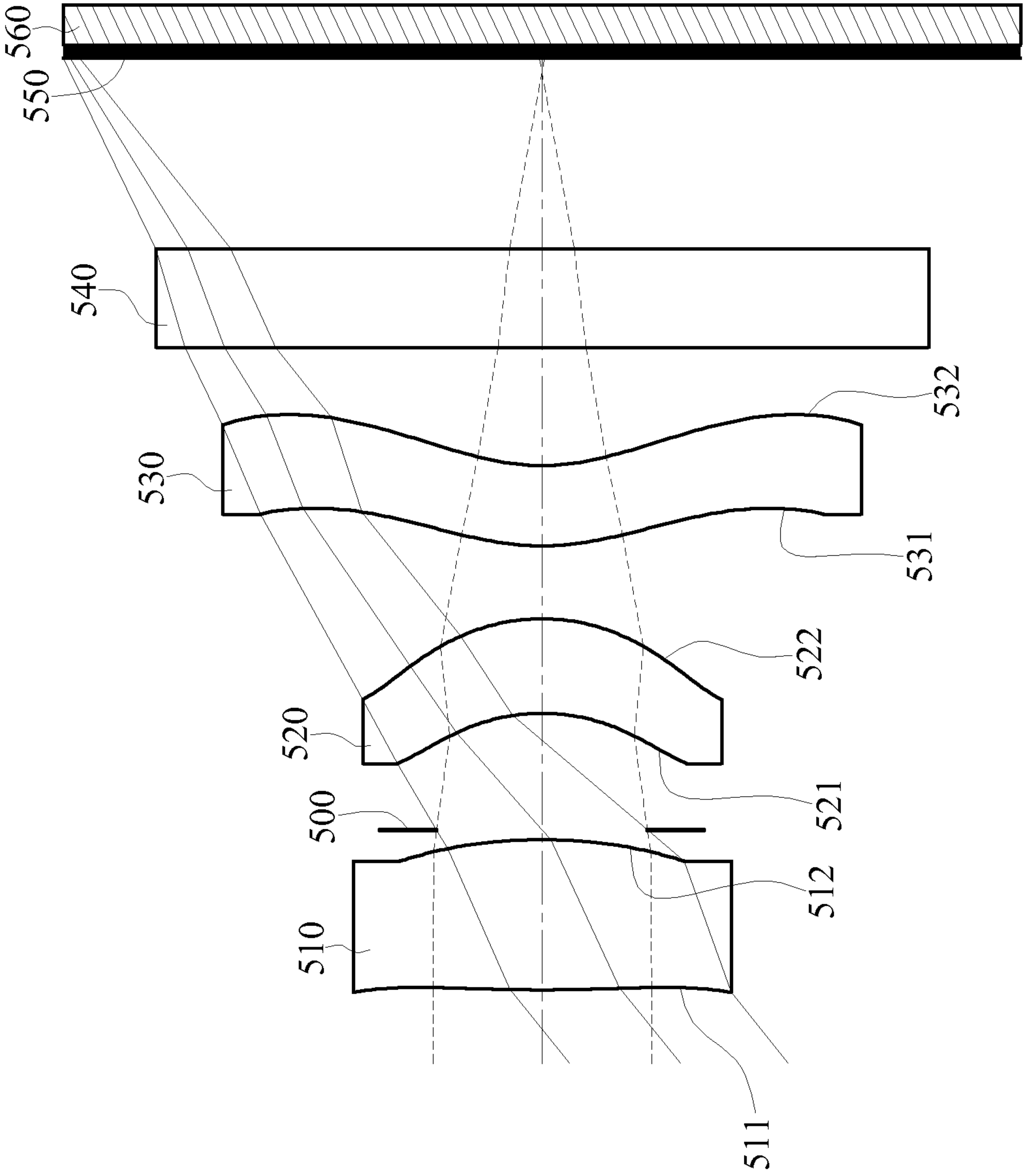


FIG.9

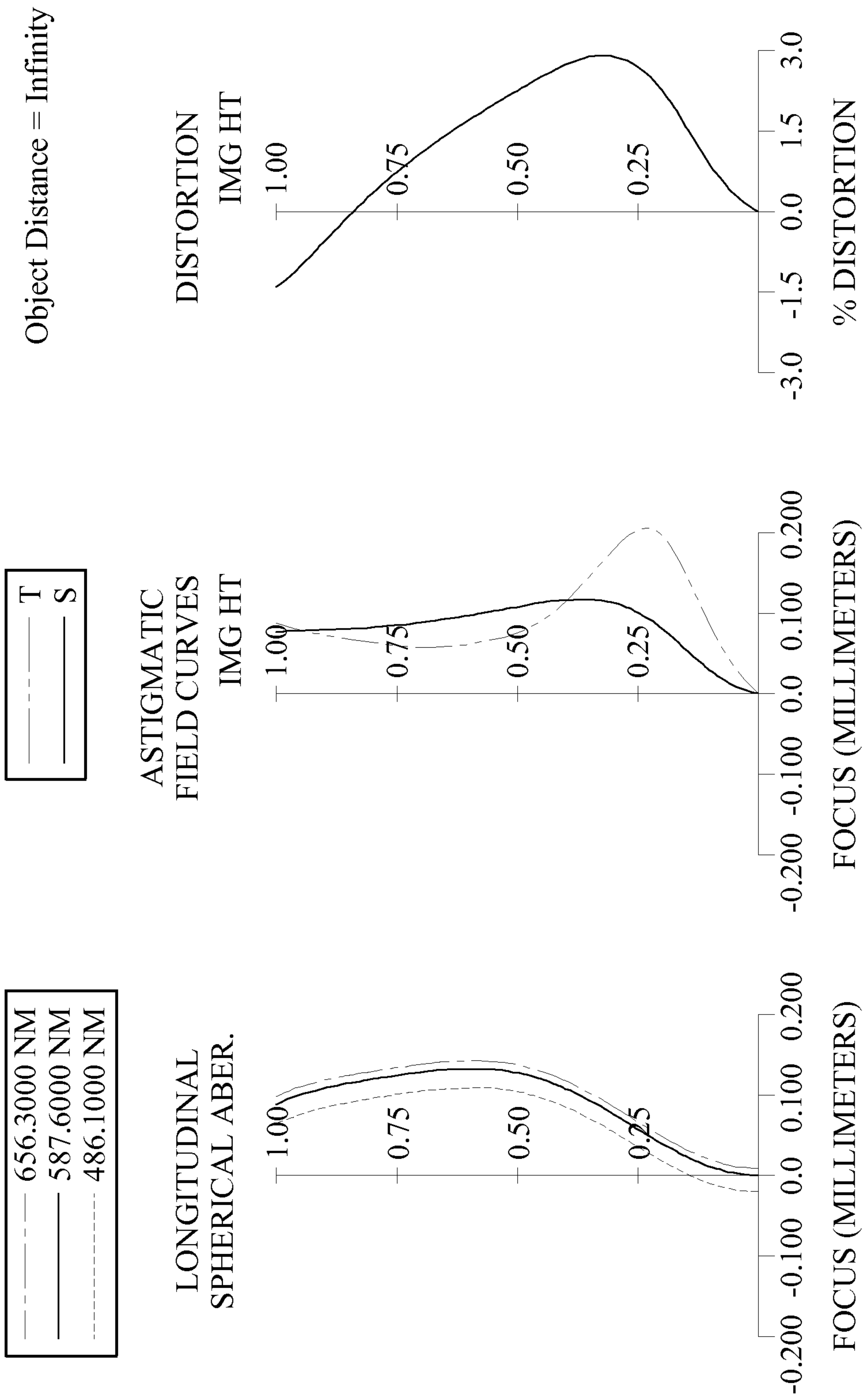


FIG. 10

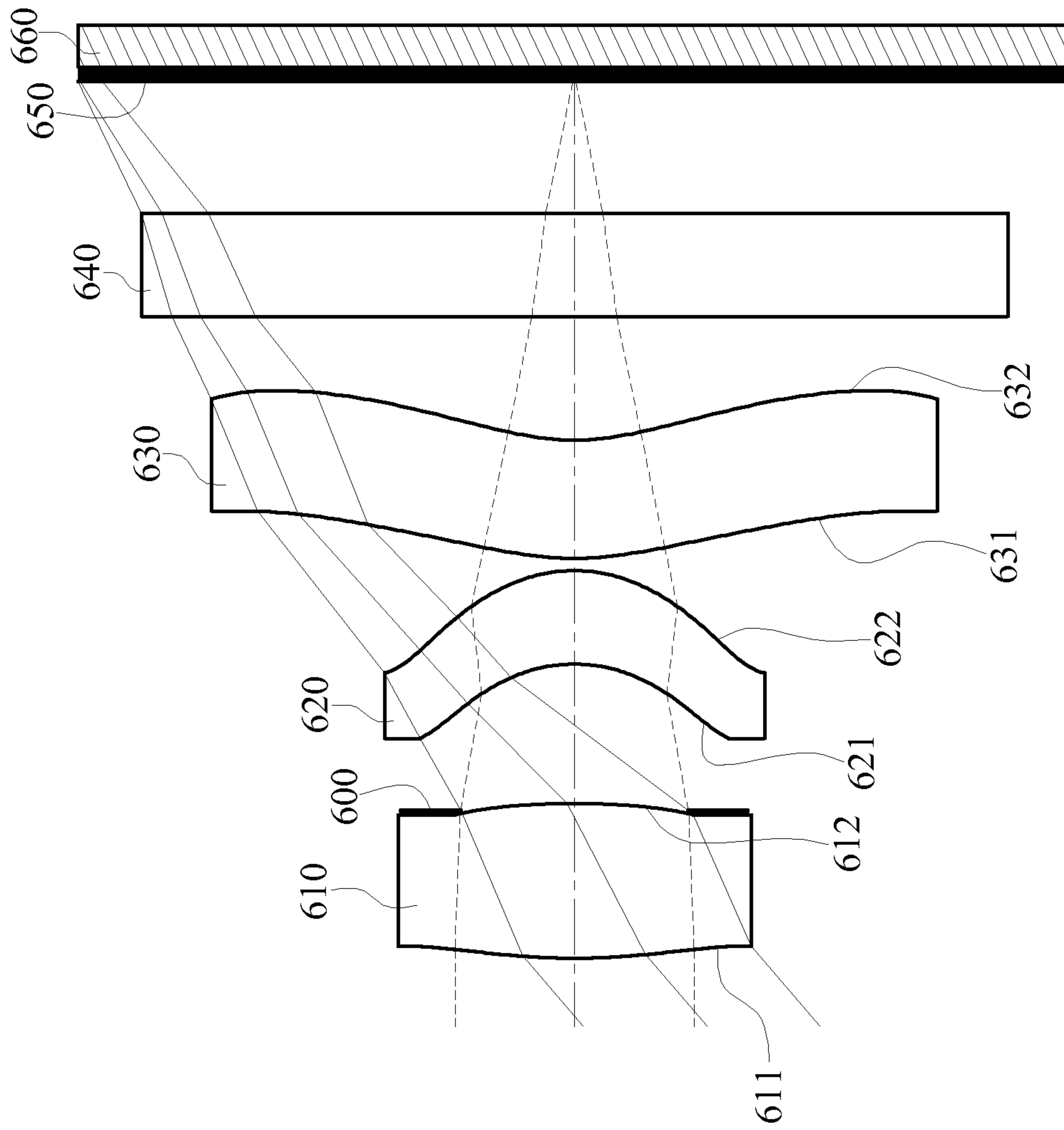


FIG.11

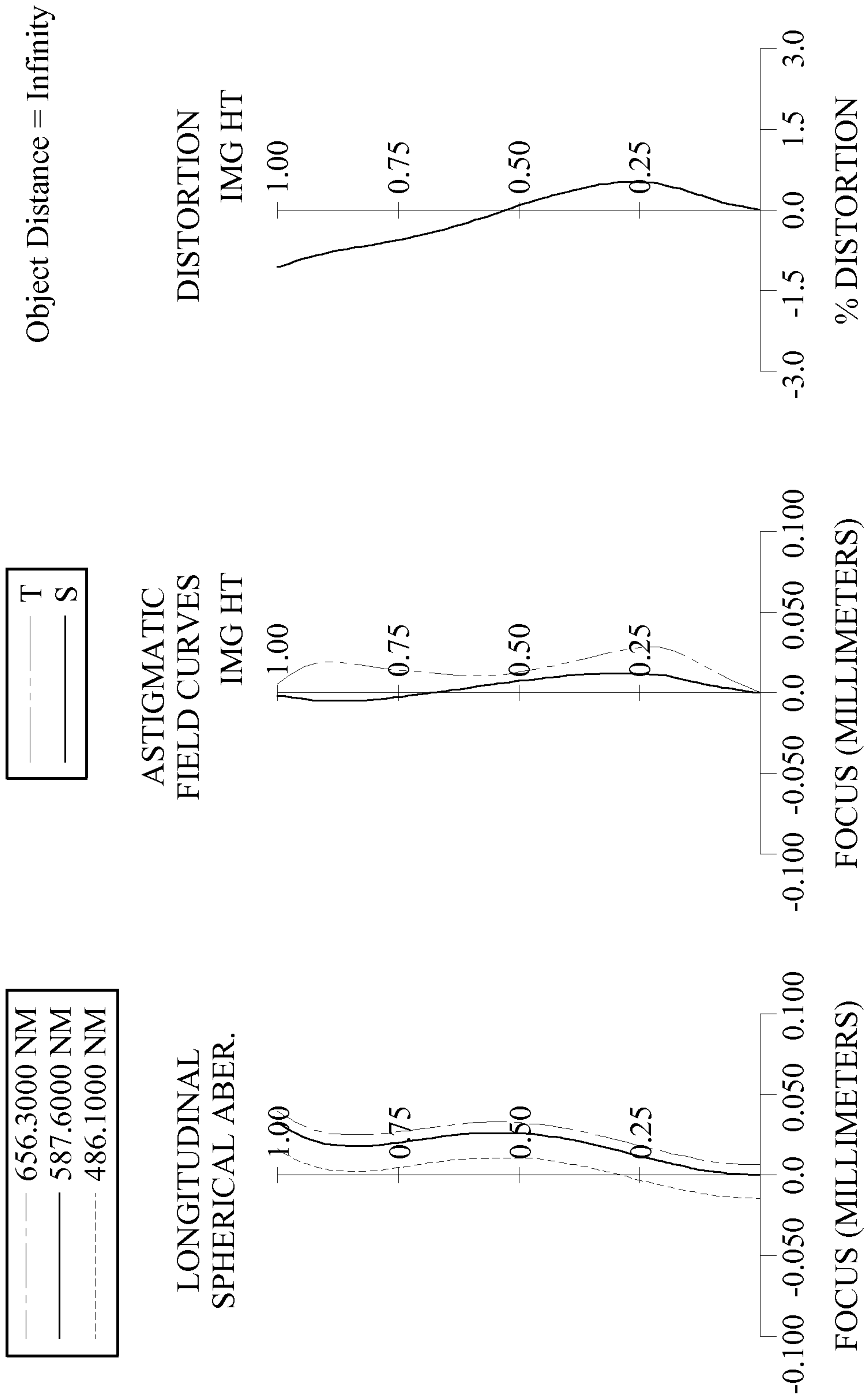


FIG.12

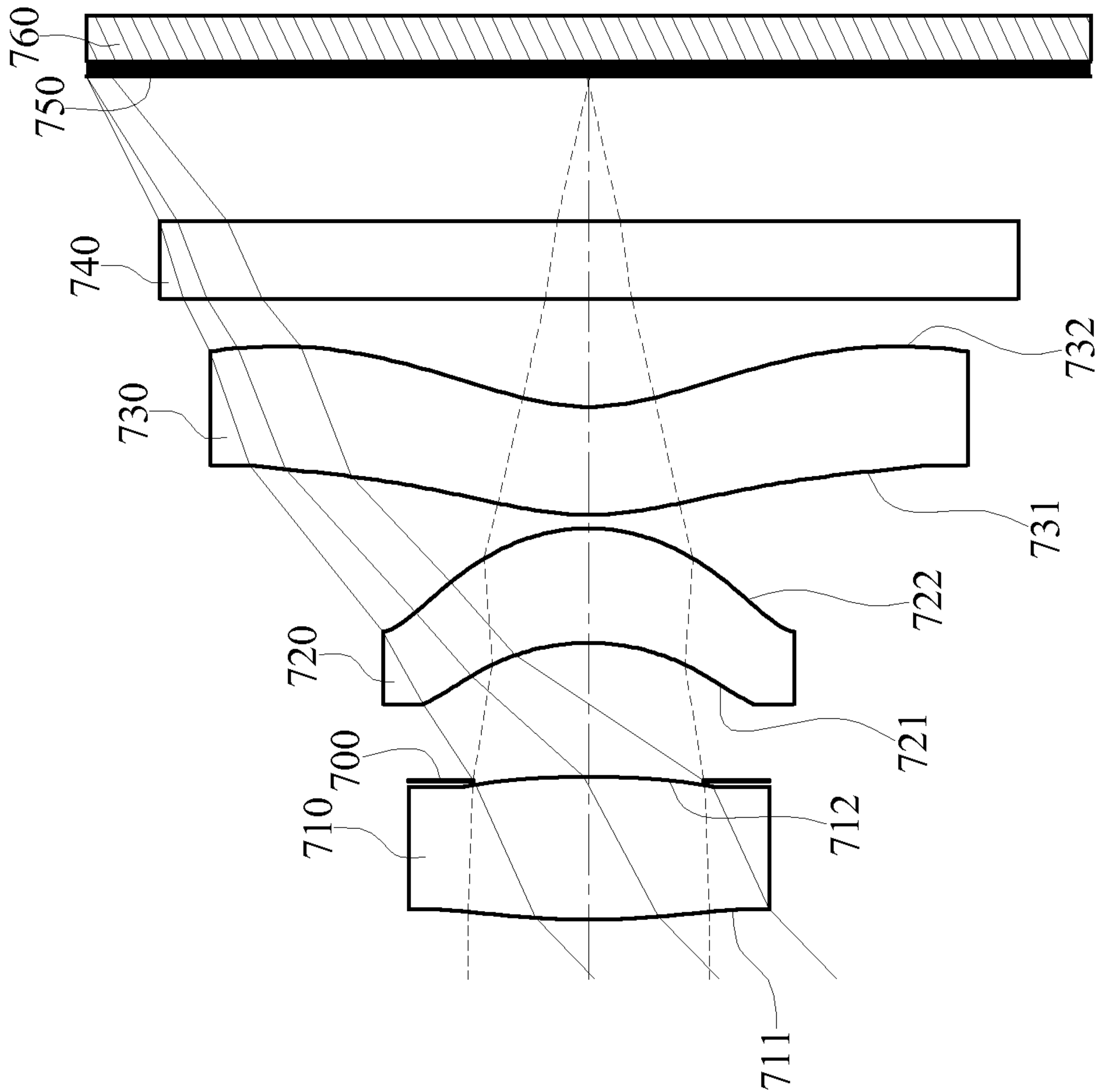


FIG.13

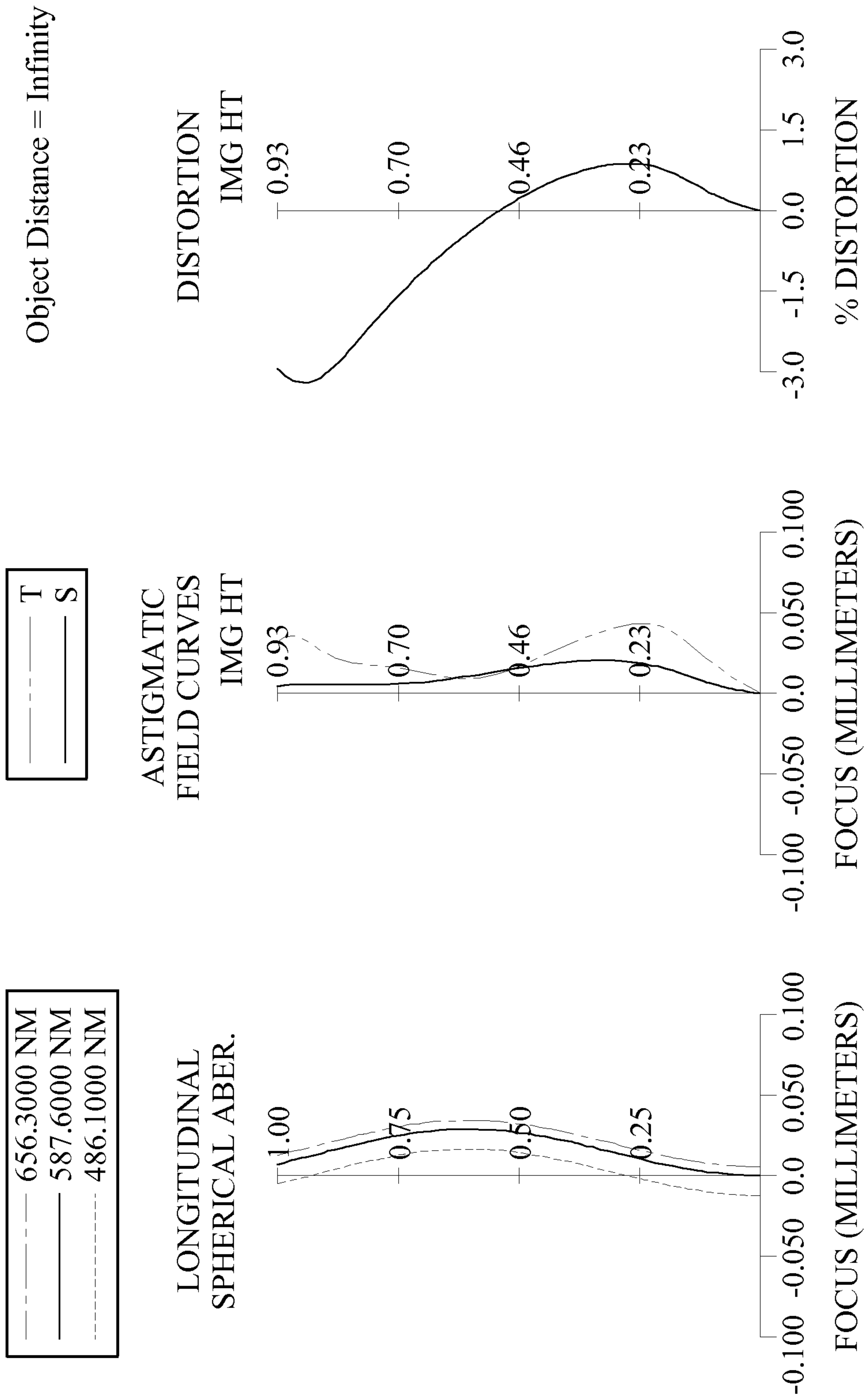


FIG.14

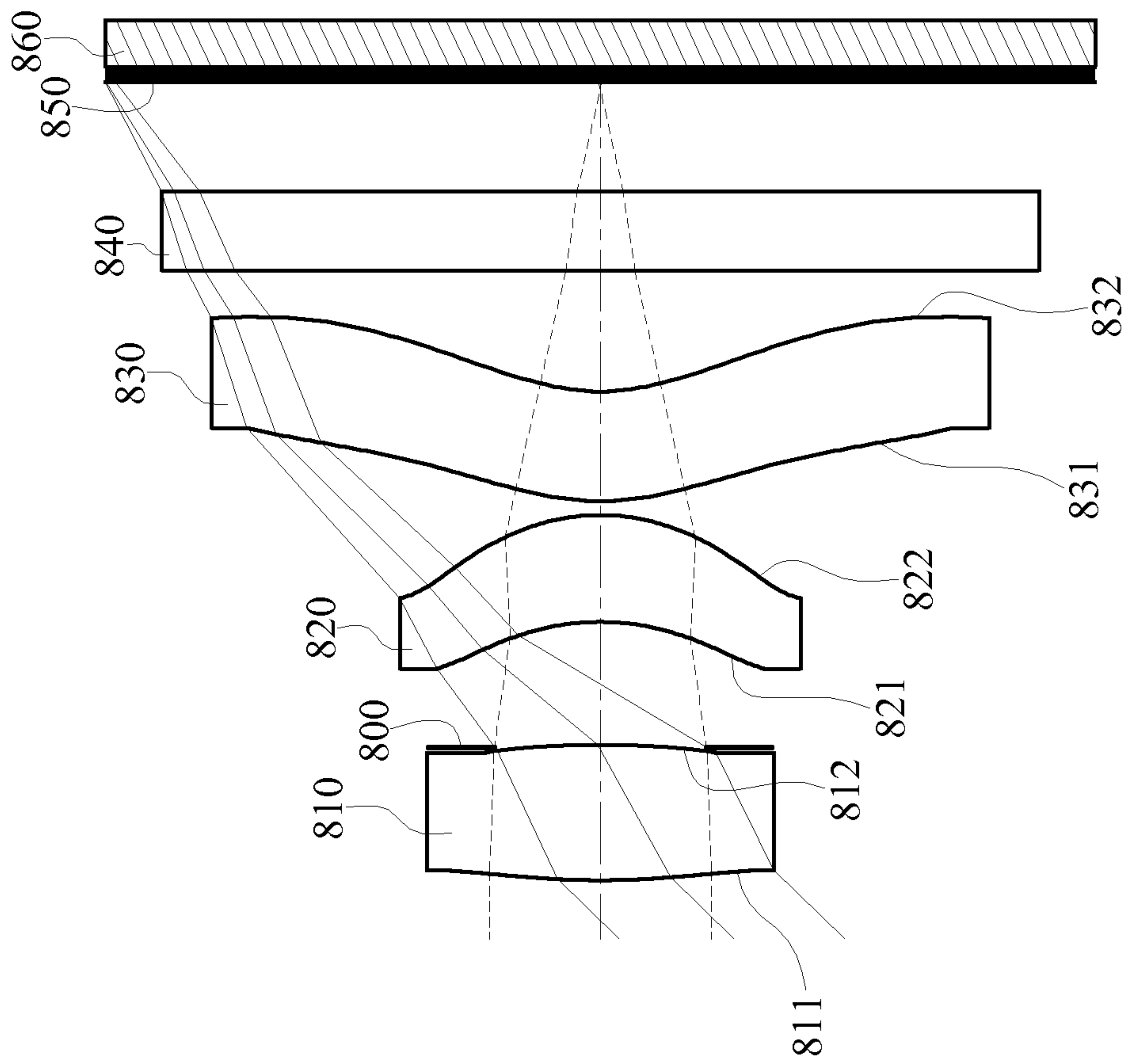


FIG.15

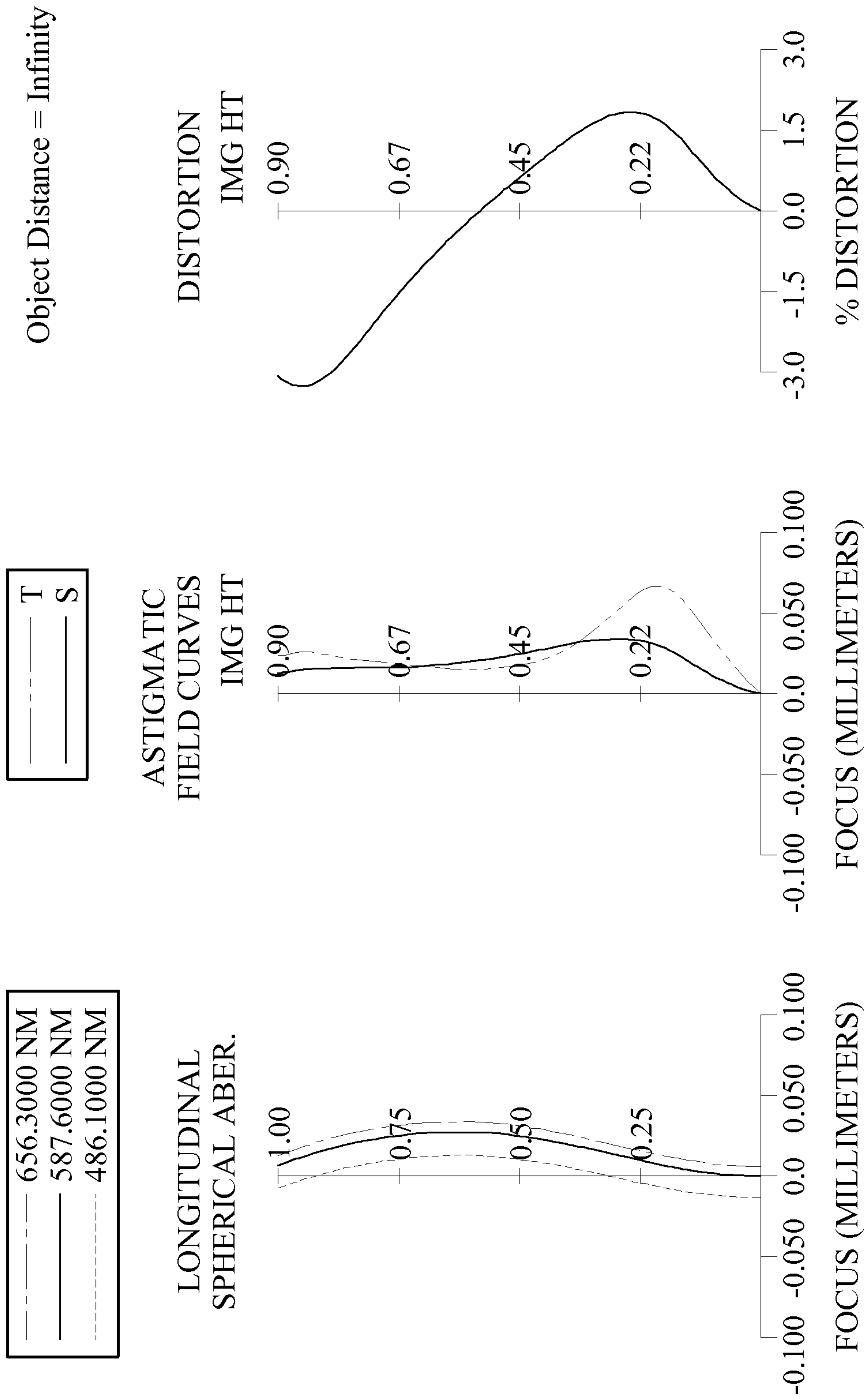


FIG.16

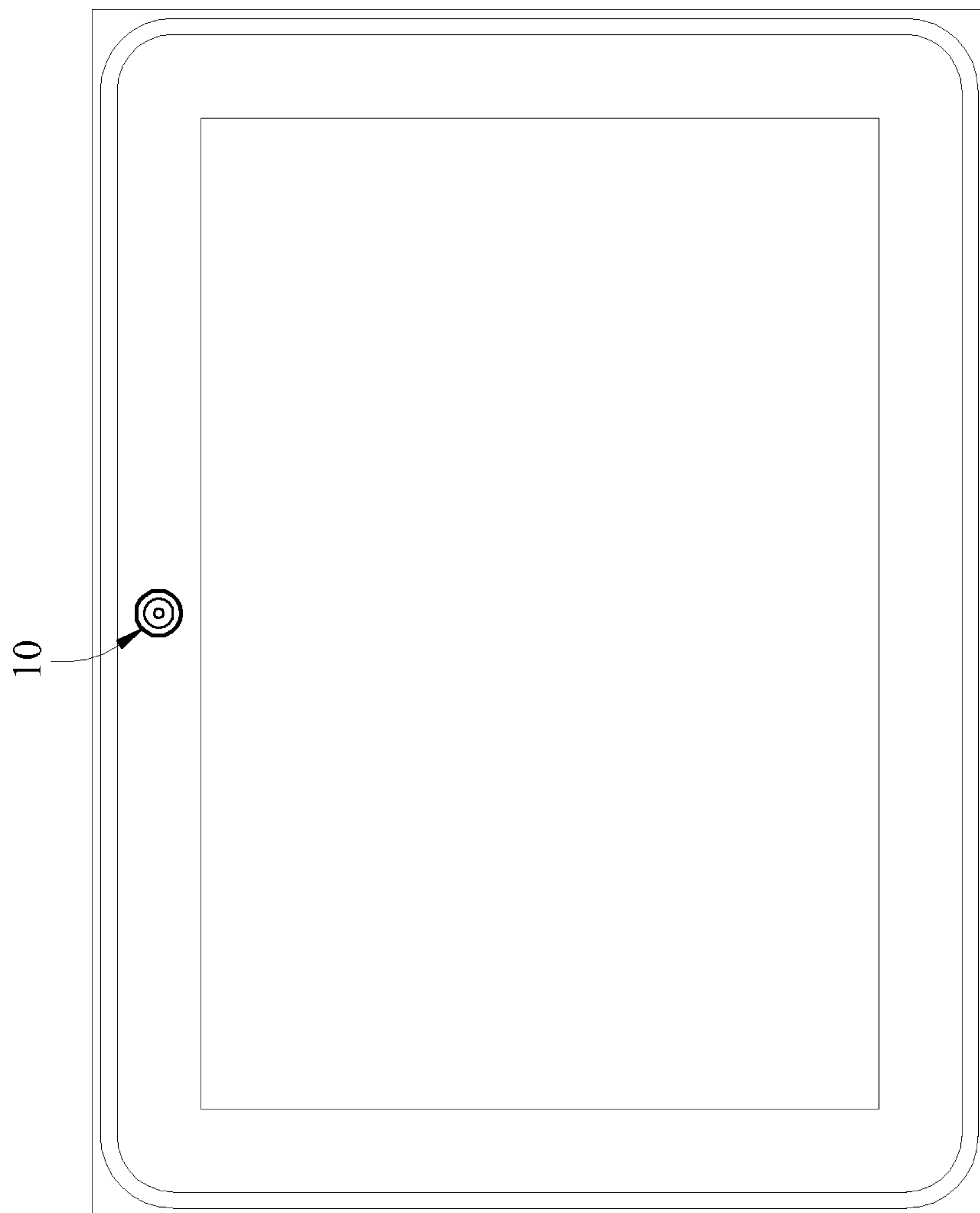


FIG.18



FIG.17

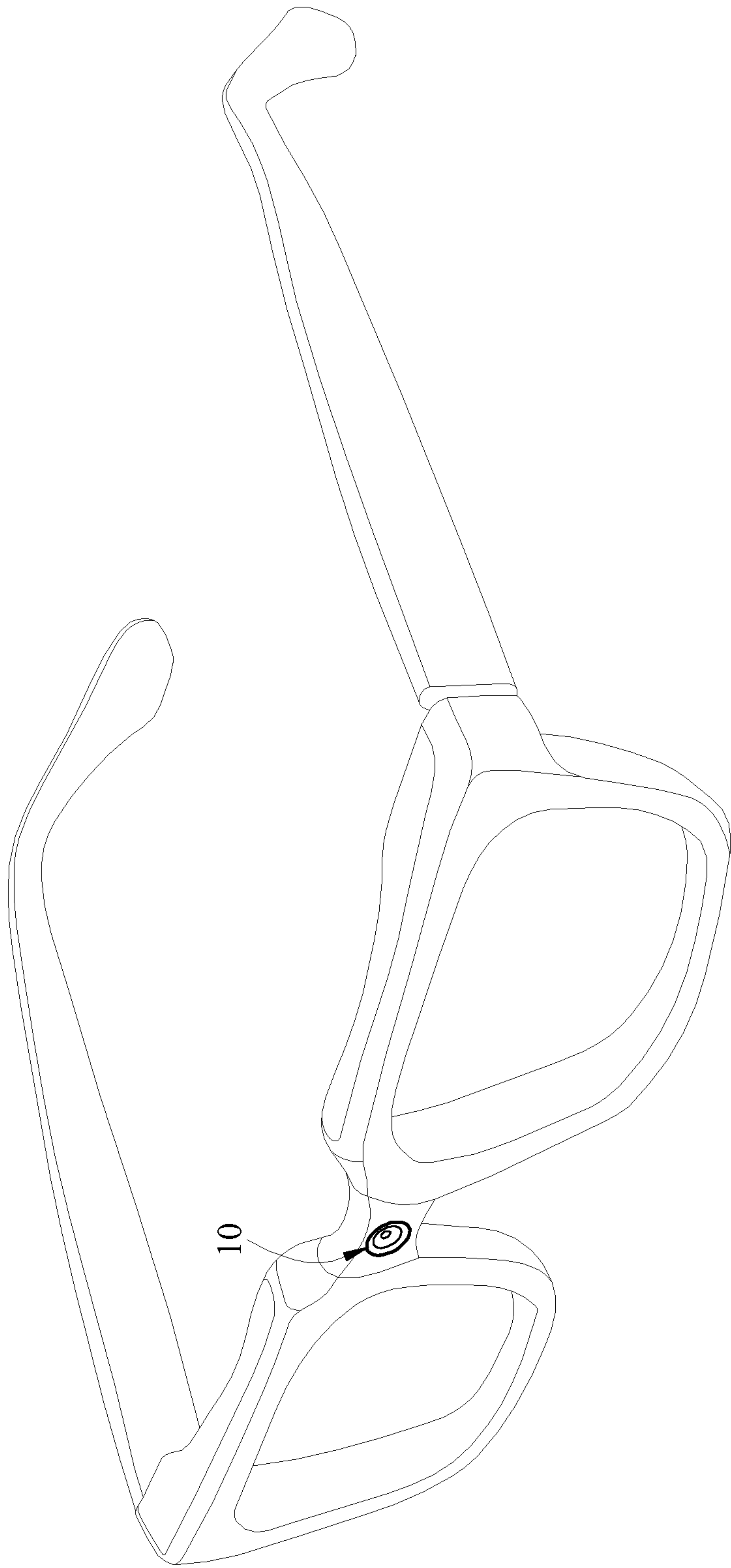


FIG.19

1

**IMAGE CAPTURING LENS ASSEMBLY,
IMAGE CAPTURING DEVICE AND MOBILE
TERMINAL**

RELATED APPLICATIONS

This application claims priority to Taiwan Application Serial Number 102137700, filed Oct. 18, 2013, which is incorporated by reference herein in its entirety.

BACKGROUND

1. Technical Field

The present disclosure relates to an image capturing lens assembly, image capturing device and mobile. More particularly, the present disclosure relates to a compact image capturing lens assembly and image capturing device applicable to mobile terminals.

2. Description of Related Art

In recent years, with the popularity of mobile products having camera functionalities, the demand of miniaturized optical systems has been increasing. The sensor of a conventional optical system is typically a CCD (Charge-Coupled Device) or a CMOS (Complementary Metal-Oxide-Semiconductor) sensor. As the advanced semiconductor manufacturing technologies have allowed the pixel size of sensors to be reduced and compact optical systems have gradually evolved toward the field of higher megapixels, there is an increasing demand for compact optical systems featuring better image quality.

A conventional optical system with three-element lens structure usually has, in order from an object side to an image side, a positive refractive power, a negative refractive power and a positive refractive power. This type of optical system is also usually with a front aperture stop. However, the image scene tends to be confined by this conventional design of refractive powers and aperture stop. It is also not favorable for making a good balance between enlarging the field of view and reducing the total track length.

SUMMARY

According to one aspect of the present disclosure, an image capturing lens assembly includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The first lens element with positive refractive power has a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric. The second lens element with positive refractive power has a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric. The third lens element with negative refractive power has a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and an object-side surface and the image-side surface of the third lens element are aspheric. The image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element. When a focal length of the image capturing lens assembly is f , a focal length of the second lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD , an axial distance between the object-side surface of the first lens element and the image-side surface of

2

the third lens element is TD , a central thickness of the first lens element is CT_1 , a central thickness of the second lens element is CT_2 , and an entrance pupil diameter of the image capturing lens assembly is EPD , the following conditions are satisfied:

$$-3.0 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82;$$

$$0.20 < CT_2/CT_1 < 0.85; \text{ and}$$

$$1.20 < f/EPD < 2.80.$$

According to another aspect of the present disclosure, an image capturing lens assembly includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The first lens element with positive refractive power has a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric. The second lens element with positive refractive power has a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric. The third lens element with negative refractive power has a convex object-side surface and a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and the object-side surface and the image-side surface of the third lens element are aspheric. The image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element. When a focal length of the second lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD , an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD , a curvature radius of the object-side surface of the first lens element is R_1 , and a curvature radius of the image-side surface of the first lens element is R_2 , the following conditions are satisfied:

$$-0.90 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82; \text{ and}$$

$$-3.0 < R_2/R_1 < -0.2.$$

According to still another aspect of the present disclosure, an image capturing lens assembly includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The first lens element with positive refractive power has a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric. The second lens element with positive refractive power has a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric. The third lens element with negative refractive power has a convex object-side surface and a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and the object-side surface and the image-side surface of the third lens element are aspheric. The image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element. When a

3

focal length of the second lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD , an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD , and an axial distance between the object-side surface of the first lens element and an image plane is TL , the following conditions are satisfied:

$$-3.0 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82; \text{ and}$$

$$1.0 \text{ mm} < TL < 2.3 \text{ mm}.$$

According to yet another aspect of the present disclosure, an image capturing device includes an image capturing lens assembly according to the still another aspect and an image sensor, wherein the image sensor is located on an image plane of the image capturing lens assembly. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The first lens element with positive refractive power has a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric. The second lens element with positive refractive power has a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric. The third lens element with negative refractive power has a convex object-side surface and a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and the object-side surface and the image-side surface of the third lens element are aspheric. The image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element. When a focal length of the second lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD , an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD , and an axial distance between the object-side surface of the first lens element and an image plane is TL , the following conditions are satisfied:

$$-3.0 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82; \text{ and}$$

$$1.0 \text{ mm} < TL < 2.3 \text{ mm}.$$

According to still yet another aspect of the present disclosure, a mobile terminal includes an image capturing device. The image capturing device includes an image capturing lens assembly according to the still another aspect and an image sensor, wherein the image sensor is located on an image plane of the image capturing lens assembly. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The first lens element with positive refractive power has a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric. The second lens element with positive refractive power has a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric. The third lens element

4

with negative refractive power has a convex object-side surface and a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and the object-side surface and the image-side surface of the third lens element are aspheric. The image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element. When a focal length of the second lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD , an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD , and an axial distance between the object-side surface of the first lens element and an image plane is TL , the following conditions are satisfied:

$$3.0 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82; \text{ and}$$

$$1.0 \text{ mm} < TL < 2.3 \text{ mm}.$$

BRIEF DESCRIPTION OF THE DRAWINGS

The disclosure can be more fully understood by reading the following detailed description of the embodiments, with reference made to the accompanying drawings as follows:

FIG. 1 is a schematic view of an image capturing device according to the 1st embodiment of the present disclosure;

FIG. 2 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 1st embodiment;

FIG. 3 is a schematic view of an image capturing device according to the 2nd embodiment of the present disclosure;

FIG. 4 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 2nd embodiment;

FIG. 5 is a schematic view of an image capturing device according to the 3rd embodiment of the present disclosure;

FIG. 6 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 3rd embodiment;

FIG. 7 is a schematic view of an image capturing device according to the 4th embodiment of the present disclosure;

FIG. 8 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 4th embodiment;

FIG. 9 is a schematic view of an image capturing device according to the 5th embodiment of the present disclosure;

FIG. 10 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 5th embodiment;

FIG. 11 is a schematic view of an image capturing device according to the 6th embodiment of the present disclosure;

FIG. 12 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 6th embodiment;

FIG. 13 is a schematic view of an image capturing device according to the 7th embodiment of the present disclosure;

FIG. 14 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 7th embodiment;

FIG. 15 is a schematic view of an image capturing device according to the 8th embodiment of the present disclosure;

5

FIG. 16 shows spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 8th embodiment;

FIG. 17 shows a smart phone with an image capturing device of the present disclosure installed therein;

FIG. 18 shows a tablet personal computer with an image capturing device of the present disclosure installed therein; and

FIG. 19 shows a wearable device with an image capturing device of the present disclosure installed therein.

DETAILED DESCRIPTION

An image capturing lens assembly includes, in order from an object side to an image side, a first lens element, a second lens element and a third lens element. The image capturing lens assembly has a total of three lens elements with refractive power.

The first lens element has positive refractive power, so that it is favorable for effectively reducing the total track length of the image capturing lens assembly. The first lens element has a convex object-side surface and a convex image-side surface, so that it is favorable for further reducing the total track length so as to keep a compact size.

The second lens element has positive refractive power, so that it is favorable for reducing the photosensitivity of the image capturing lens assembly. The second lens element has a concave object-side surface and a convex image-side surface, so that it is favorable for correcting astigmatism.

The third lens element has negative refractive power, so that it is favorable for correcting the aberrations. The third lens element can have a convex object-side surface and has a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof. Therefore, it is favorable for correcting the astigmatism and further correcting the aberrations of the off-axis.

When a focal length of the second lens element is f_2 , and a focal length of the third lens element is f_3 , the following condition is satisfied: $-3.0 < f_2/f_3 < 0$. Therefore, it is favorable for further reducing the total track length of the image capturing lens assembly effectively. Preferably, the following condition is satisfied: $-1.5 < f_2/f_3 < 0$. More preferably, the following condition is satisfied: $-0.90 < f_2/f_3 < 0$.

When an axial distance between a stop and the image-side surface of the third lens element is SD , and an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD , the following condition is satisfied: $0.58 < SD/TD < 0.82$. Therefore, the stop is close to the image plane which is favorable for increasing the field of view so as to obtain more of the image scene under a limited distance.

When a central thickness of the first lens element is CT_1 , and a central thickness of the second lens element is CT_2 , the following condition is satisfied: $0.20 < CT_2/CT_1 < 0.85$. Therefore, it is favorable for assembling the lens elements and increasing the manufacturing yield rate. Preferably, the following condition is satisfied: $0.30 < CT_2/CT_1 < 0.75$.

When a focal length of the image capturing lens assembly is f , and an entrance pupil diameter of the image capturing lens assembly is EPD , the following condition is satisfied: $1.20 < f/EPD < 2.80$. Therefore, it is favorable for increasing exposure so as to improve image resolving power. Preferably, the following condition is satisfied: $1.60 < f/EPD < 2.45$.

When a curvature radius of the object-side surface of the first lens element is R_1 , and a curvature radius of the image-side surface of the first lens element is R_2 , the following

6

condition is satisfied: $-3.0 < R_2/R_1 < -0.2$. Therefore, it is favorable for correcting spherical aberration. Preferably, the following condition is satisfied: $-2.0 < R_2/R_1 < -0.2$.

When an axial distance between the object-side surface of the first lens element and an image plane is TL , the following condition is satisfied: $1.0 \text{ mm} < TL < 2.3 \text{ mm}$. Therefore, it is favorable for keeping the image capturing lens assembly compact so as to be applied to mobile terminals. Preferably, the following condition is satisfied: $1.0 \text{ mm} < TL < 2.0 \text{ mm}$.

When a maximal field of view of the image capturing lens assembly is FOV , the following condition is satisfied: $76 \text{ degrees} < FOV < 120 \text{ degrees}$. Therefore, it is favorable for enlarging the field of view so as to obtain more of the image scene.

When a curvature radius of the object-side surface of the third lens element is R_5 , and a curvature radius of the image-side surface of the third lens element is R_6 , the following condition is satisfied: $|(R_5 - R_6)/(R_5 + R_6)| < 0.35$. Therefore, it is favorable for correcting aberrations. Preferably, the following condition is satisfied: $|(R_5 - R_6)/(R_5 + R_6)| < 0.25$.

When the focal length of the image capturing lens assembly is f , and the focal length of the second lens element is f_2 , the following condition is satisfied: $0.4 < f/f_2 < 1.0$. Therefore, it is favorable for reducing photosensitivity.

When a curvature radius of the object-side surface of the second lens element is R_3 , and a curvature radius of the image-side surface of the second lens element is R_4 , the following condition is satisfied: $|(R_3 - R_4)/(R_3 + R_4)| < 0.15$. Therefore, it is favorable for correcting the astigmatism.

When the axial distance between the object-side surface of the first lens element and the image plane is TL , and a maximum image height of the image capturing lens assembly (half of a diagonal length of an effective photosensitive area of an image sensor) is $ImgH$, the following condition is satisfied: $TL/ImgH < 1.90$. Therefore, it is favorable for keeping the image capturing lens assembly compact so as to be applied to compact mobile terminals.

When the axial distance between the object-side surface of the first lens element and the image plane is TL , and half of the maximal field of view of the image capturing lens assembly is $HFOV$, the following condition is satisfied: $1.0 \text{ mm} < TL/\tan(HFOV) < 3.0 \text{ mm}$. Therefore, it is favorable for keeping the image capturing lens assembly compact and obtaining a proper field of view.

According to the image capturing lens assembly of the present disclosure, the lens elements thereof can be made of glass or plastic material. When the lens elements are made of glass material, the distribution of the refractive power of the image capturing lens assembly may be more flexible to design. When the lens elements are made of plastic material, the manufacturing cost can be effectively reduced. Furthermore, surfaces of each lens element can be arranged to be aspheric, since the aspheric surface of the lens element is easy to form a shape other than spherical surface so as to have more controllable variables for eliminating the aberration thereof, and to further decrease the required number of the lens elements. Therefore, the total track length of the image capturing lens assembly can also be reduced.

According to the image capturing lens assembly of the present disclosure, each of an object-side surface and an image-side surface has a paraxial region and an off-axis region. The paraxial region refers to the region of the surface where light rays travel close to the optical axis, and the off-axis region refers to the region of the surface where light rays travel away from the optical axis. Particularly, when the lens element has a convex surface, it indicates that the surface is

convex in the paraxial region thereof; when the lens element has a concave surface, it indicates that the surface is concave in the paraxial region thereof.

According to the image capturing lens assembly of the present disclosure, the image capturing lens assembly can include at least one stop, such as an aperture stop, a glare stop or a field stop. Said glare stop or said field stop is for eliminating the stray light and thereby improving the image resolution thereof.

According to the image capturing lens assembly of the present disclosure, an aperture stop can be configured as a middle stop. A middle stop disposed between the first lens element and the second lens element is favorable for enlarging the field of view of the image capturing lens assembly and thereby provides a wider field of view for the same.

The present image capturing lens assembly can be optionally applied to moving focus or zoom optical systems. According to the image capturing lens assembly of the present disclosure, the image capturing lens assembly is featured with good correction ability and high image quality, and can be applied to 3D (three-dimensional) image capturing applications, in products such as digital cameras, mobile devices, digital tablets, wearable devices and other mobile terminals.

According to the present disclosure, an image capturing device is provided. The image capturing device includes the image capturing lens assembly according to the aforementioned image capturing lens assembly of the present disclosure, and an image sensor, wherein the image sensor is disposed on an image plane of the aforementioned image capturing lens assembly. It is favorable for reducing the total track length so as to keep a compact size. Furthermore, the stop can be close to the image plane which is favorable for increasing the field of view so as to obtain more of the image scene under a limited distance. Preferably, the image capturing device can further include a barrel member and/or a holding member.

According to the present disclosure, a mobile terminal is provided, wherein the mobile terminal includes an image capturing device. In FIGS. 17-19, the image capturing device 10 can be applied to a smart phone (as shown in FIG. 17), a tablet personal computer (as shown in FIG. 18) or a wearable device (as shown in FIG. 19). It is favorable for reducing the total track length so as to keep a compact size. Furthermore, the stop can be close to the image plane which is favorable for increasing the field of view so as to obtain more of the image scene under a limited distance. Preferably, the mobile terminal can further include but not limited to display, control unit, random access memory unit (RAM) and/or read only memory unit (ROM).

According to the above description of the present disclosure, the following 1st-8th specific embodiments are provided for further explanation.

1st Embodiment

FIG. 1 is a schematic view of an image capturing device according to the 1st embodiment of the present disclosure. FIG. 2 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 1st embodiment.

In FIG. 1, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor 160. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element 110, an aperture stop 100, a second lens element 120, a third lens element 130, an IR-cut filter 140 and an image plane 150, wherein the image capturing lens assembly has a total of three lens elements (110-130) with refractive power.

The first lens element 110 with positive refractive power has a convex object-side surface 111 and a convex image-side surface 112, which are both aspheric, and the first lens element 110 is made of plastic material.

The second lens element 120 with positive refractive power has a concave object-side surface 121 and a convex image-side surface 122, which are both aspheric, and the second lens element 120 is made of plastic material.

The third lens element 130 with negative refractive power has a convex object-side surface 131 in a paraxial region thereof and a concave image-side surface 132 in a paraxial region thereof, which are both aspheric, and the third lens element 130 is made of plastic material. Moreover, the object-side surface 131 of the third lens element 130 has at least one concave shape in an off-axis region thereof, and the image-side surface 132 of the third lens element 130 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 140 is made of glass and located between the third lens element 130 and the image plane 150, and will not affect the focal length of the image capturing lens assembly. The image sensor 160 is disposed on the image plane 150 of the image capturing lens assembly.

The equation of the aspheric surface profiles of the aforementioned lens elements of the 1st embodiment is expressed as follows:

$$X(Y) = (Y^2/R)/(1 + \sqrt{1 - (1+k) \times (Y/R)^2}) + \sum_i (A_i) \times (Y^i),$$

where,

X is the relative distance between a point on the aspheric surface spaced at a distance Y from the optical axis and the tangential plane at the aspheric surface vertex on the optical axis;

Y is the vertical distance from the point on the aspheric surface to the optical axis;

R is the curvature radius;

k is the conic coefficient; and

A_i is the i-th aspheric coefficient.

In the image capturing lens assembly according to the 1st embodiment, when a focal length of the image capturing lens assembly is f, an f-number of the image capturing lens assembly is F_{no}, and half of a maximal field of view of the image capturing lens assembly is HFOV, these parameters have the following values: f=1.21 mm; F_{no}=2.40; and HFOV=42.8 degrees.

In the image capturing lens assembly according to the 1st embodiment, when a central thickness of the first lens element 110 is CT1, and a central thickness of the second lens element 120 is CT2, the following condition is satisfied: CT2/CT1=0.61.

In the image capturing lens assembly according to the 1st embodiment, when a curvature radius of the object-side surface 111 of the first lens element 110 is R1, a curvature radius of the image-side surface 112 of the first lens element 110 is R2, the following condition is satisfied: R2/R1=-1.48.

In the image capturing lens assembly according to the 1st embodiment, when a curvature radius of the object-side surface 121 of the second lens element 120 is R3, and a curvature radius of the image-side surface 122 of the second lens element 120 is R4, the following condition is satisfied:

$$|(R3-R4)/(R3+R4)|=0.11.$$

In the image capturing lens assembly according to the 1st embodiment, when a curvature radius of the object-side surface 131 of the third lens element 130 is R5, and a curvature radius of the image-side surface 132 of the third lens element 130 is R6, the following condition is satisfied: |(R5-R6)/(R5+R6)|=0.31.

In the image capturing lens assembly according to the 1st embodiment, when the focal length of the image capturing lens assembly is f , and a focal length of the second lens element **120** is f_2 , the following condition is satisfied: $f/f_2=0.95$.

In the image capturing lens assembly according to the 1st embodiment, when the focal length of the second lens element **120** is f_2 , and a focal length of the third lens element **130** is f_3 , the following condition is satisfied: $f_2/f_3=-0.74$.

In the image capturing lens assembly according to the 1st embodiment, when the focal length of the image capturing lens assembly is f , and an entrance pupil diameter of the image capturing lens assembly is EPD, the following condition is satisfied: $f/EPD=2.40$.

In the image capturing lens assembly according to the 1st embodiment, when an axial distance between the aperture stop **100** and the image-side surface **132** of the third lens element **130** is SD, and an axial distance between the object-side surface **111** of the first lens element **110** and the image-side surface **132** of the third lens element **130** is TD, the following condition is satisfied: $SD/TD=0.68$.

In the image capturing lens assembly according to the 1st embodiment, when an axial distance between the object-side surface **111** of the first lens element **110** and the image plane **150** is TL, the following condition is satisfied: $TL=1.82$ mm.

In the image capturing lens assembly according to the 1st embodiment, when the maximal field of view of the image capturing lens assembly is FOV, the following condition is satisfied: $FOV=85.6$ degrees.

In the image capturing lens assembly according to the 1st embodiment, when the axial distance between the object-side surface **111** of the first lens element **110** and the image plane **150** is TL, and half of the maximal field of view of the image capturing lens assembly is HFOV, the following condition is satisfied: $TL/\tan(HFOV)=1.97$ mm.

In the image capturing lens assembly according to the 1st embodiment, when the axial distance between the object-side surface **111** of the first lens element **110** and the image plane **150** is TL, and a maximum image height of the image capturing lens assembly (half of a diagonal length of an effective photosensitive area of the image sensor **160**) is $ImgH$, the following condition is satisfied: $TL/ImgH=1.66$.

The detailed optical data of the 1st embodiment are shown in Table 1 and the aspheric surface data are shown in Table 2 below.

TABLE 1

1st Embodiment								
$f = 1.21$ mm, $Fno = 2.40$, $HFOV = 42.8$ deg.								
Surface #		Curvature	Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Plano		Infinity				
1	Lens 1	1.261	ASP	0.366	Plastic	1.535	56.3	1.47
2		-1.867	ASP	-0.014				
3	Ape. Stop	Plano		0.288				
4	Lens 2	-0.359	ASP	0.224	Plastic	1.544	55.9	1.28
5		-0.289	ASP	0.032				
6	Lens 3	0.790	ASP	0.200	Plastic	1.632	23.4	-1.74
7		0.414	ASP	0.200				
8	IR-cut filter	Plano		0.210	Glass	1.517	64.2	—
9		Plano		0.316				
10	Image	Plano		—				

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 2

Aspheric Coefficients			
Surface #	1	2	4
k =	4.8360E+00	1.8616E+01	-3.2555E+00
A4 =	-1.1002E+00	-5.5725E-01	-6.6979E+00
A6 =	1.0455E-01	-8.8597E+00	-1.1550E+01
A8 =	-1.6045E+01	1.2150E+02	-6.9606E+02
A10 =	—	—	2.0016E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-3.3149E+00	-9.9668E-01	-7.5252E+00
A4 =	-1.0013E+01	-5.0461E+00	-1.8150E+00
A6 =	9.4283E+01	2.1423E+01	4.3915E+00
A8 =	-1.2697E+03	-5.4967E+01	-5.9887E+00
A10 =	9.6278E+03	8.3535E+01	2.3408E+00
A12 =	-2.2990E+04	-7.9954E+01	1.9759E+00
A14 =	—	3.6659E+01	-2.5290E+00

In Table 1, the curvature radius, the thickness and the focal length are shown in millimeters (mm). Surface numbers 0-10 represent the surfaces sequentially arranged from the object-side to the image-side along the optical axis. In Table 2, k represents the conic coefficient of the equation of the aspheric surface profiles. A4-A14 represent the aspheric coefficients ranging from the 4th order to the 14th order. This information related to Table 1 and Table 2 applies also to the Tables for the remaining embodiments, and so an explanation in this regard will not be provided again.

2nd Embodiment

FIG. 3 is a schematic view of an image capturing device according to the 2nd embodiment of the present disclosure. FIG. 4 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 2nd embodiment.

In FIG. 3, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor **260**. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element **210**, an aperture stop **200**, a second lens element **220**, a third lens element **230**, an IR-cut filter **240** and an image plane **250**, wherein the image capturing lens assembly has a total of three lens elements (**210-230**) with refractive power.

11

The first lens element **210** with positive refractive power has a convex object-side surface **211** and a convex image-side surface **212**, which are both aspheric, and the first lens element **210** is made of plastic material.

The second lens element **220** with positive refractive power has a concave object-side surface **221** and a convex image-side surface **222**, which are both aspheric, and the second lens element **220** is made of plastic material.

The third lens element **230** with negative refractive power has a convex object-side surface **231** in a paraxial region thereof and a concave image-side surface **232** in a paraxial region thereof, which are both aspheric, and the third lens element **230** is made of plastic material. Moreover, the object-side surface **231** of the third lens element **230** has at least one concave shape in an off-axis region thereof, and the image-side surface **232** of the third lens element **230** has at least one convex shape in an off-axis region thereof.

The IR-cut filter **240** is made of glass and located between the third lens element **230** and the image plane **250**, and will not affect the focal length of the image capturing lens assembly. The image sensor **260** is disposed on the image plane **250** of the image capturing lens assembly.

The detailed optical data of the 2nd embodiment are shown in Table 3 and the aspheric surface data are shown in Table 4 below.

TABLE 3

2nd Embodiment								
f = 1.10 mm, Fno = 2.40, HFOV = 42.6 deg.								
Surface #		Curvature	Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Plano		Infinity				
1	Lens 1	2.850	ASP	0.273	Plastic	1.535	55.7	1.37
2		-0.950	ASP	-0.014				
3	Ape. Stop	Plano		0.317				
4	Lens 2	-0.269	ASP	0.194	Plastic	1.530	55.8	2.55
5		-0.280	ASP	0.025				
6	Lens 3	0.583	ASP	0.227	Plastic	1.543	56.5	-9.65
7		0.453	ASP	0.200				
8	IR-cut filter	Plano		0.210	Glass	1.517	64.2	—
9		Plano		0.317				
10	Image	Plano		—				

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 4

Aspheric Coefficients			
Surface #	1	2	4
k =	-9.0000E+01	1.2854E+00	-2.2784E+00
A4 =	-1.2880E+00	-1.7043E+00	-6.3308E+00
A6 =	-2.3330E+00	4.4927E+00	-2.5192E+00
A8 =	-3.5006E+01	-8.5048E+00	-3.5717E+02
A10 =	—	—	1.7561E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-3.5621E+00	-1.6507E+00	-6.6831E+00
A4 =	-1.1946E+01	-4.2389E+00	-1.4062E+00
A6 =	1.0824E+02	1.9340E+01	3.7828E+00
A8 =	-1.1616E+03	-5.4668E+01	-5.4794E+00
A10 =	9.0021E+03	8.9851E+01	1.5150E+00
A12 =	-2.2990E+04	-8.1882E+01	3.4034E+00
A14 =	—	3.0924E+01	-2.8318E+00

In the image capturing lens assembly according to the 2nd embodiment, the definitions of these parameters shown in the

12

following table are the same as those stated in the 1st embodiment with corresponding values for the 2nd embodiment. Moreover, these parameters can be calculated from Table 3 and Table 4 as the following values and satisfy the following conditions:

2nd Embodiment			
f [mm]	1.10	f2/f3	-0.26
Fno	2.40	f/EPD	2.40
HFOV [deg.]	42.6	SD/TD	0.75
CT2/CT1	0.71	TL [mm]	1.75
R2/R1	-0.33	FOV [deg.]	85.2
$(R3 - R4)/(R3 + R4)$	0.02	TL/tan(HFOV) [mm]	1.90
$(R5 - R6)/(R5 + R6)$	0.13	TL/ImgH	1.75
f/f2	0.43		

3rd Embodiment

FIG. 5 is a schematic view of an image capturing device according to the 3rd embodiment of the present disclosure. FIG. 6 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 3rd embodiment.

45

In FIG. 5, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor **360**. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element **310**, an aperture stop **300**, a second lens element **320**, a third lens element **330**, an IR-cut filter **340** and an image plane **350**, wherein the image capturing lens assembly has a total of three lens elements (**310-330**) with refractive power.

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The first lens element **310** with positive refractive power has a convex object-side surface **311** and a convex image-side surface **312**, which are both aspheric, and the first lens element **310** is made of plastic material.

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The second lens element **320** with positive refractive power has a concave object-side surface **321** and a convex image-side surface **322**, which are both aspheric, and the second lens element **320** is made of plastic material.

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The third lens element **330** with negative refractive power has a convex object-side surface **331** in a paraxial region thereof and a concave image-side surface **332** in a paraxial region thereof, which are both aspheric, and the third lens element **330** is made of plastic material. Moreover, the object-

65

13

side surface **331** of the third lens element **330** has at least one concave shape in an off-axis region thereof, and the image-side surface **332** of the third lens element **330** has at least one convex shape in an off-axis region thereof.

The IR-cut filter **340** is made of glass and located between the third lens element **330** and the image plane **350**, and will not affect the focal length of the image capturing lens assembly. The image sensor **360** is disposed on the image plane **350** of the image capturing lens assembly.

The detailed optical data of the 3rd embodiment are shown in Table 5 and the aspheric surface data are shown in Table 6 below.

TABLE 5

3rd Embodiment								
f = 1.16 mm, Fno = 2.00, HFOV = 41.0 deg.								
Surface #		Curvature Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Plano	Infinity					
1	Lens 1	1.198	ASP	0.365	Plastic	1.544	55.9	1.55
2		-2.548	ASP	-0.012				
3	Ape. Stop	Plano	0.264					
4	Lens 2	-0.340	ASP	0.194	Plastic	1.544	55.9	1.78
5		-0.302	ASP	0.025				
6	Lens 3	0.612	ASP	0.188	Plastic	1.650	21.4	-3.81
7		0.431	ASP	0.200				
8	IR-cut filter	Plano	0.210	Glass	1.517	64.2		—
9		Plano	0.350					
10	Image	Plano	—					

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 6

Aspheric Coefficients			
Surface #	1	2	4
k =	3.8272E+00	1.0821E+00	-2.5999E+00
A4 =	-9.8411E-01	-8.8268E-01	-1.6553E+00
A6 =	-4.7804E-01	-7.3306E+00	-3.4803E+01
A8 =	-8.8081E+00	7.9430E+01	-1.0526E+03
A10 =	—	—	2.2780E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-3.9950E+00	-1.4796E+00	-7.3194E+00
A4 =	-9.2922E+00	-4.8511E+00	-1.5871E+00
A6 =	9.4768E+01	2.0893E+01	4.0171E+00
A8 =	-1.2940E+03	-5.5039E+01	-5.5575E+00
A10 =	9.7163E+03	8.4686E+01	1.5444E+00
A12 =	-2.2990E+04	-7.0605E+01	2.7996E+00
A14 =	—	2.5077E+01	-1.6519E+00

In the image capturing lens assembly according to the 3rd embodiment, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 3rd embodiment. Moreover, these parameters can be calculated from Table 5 and Table 6 as the following values and satisfy the following conditions:

3rd Embodiment			
f [mm]	1.16	f2/f3	-0.47
Fno	2.00	f/EPD	2.00
HFOV [deg.]	41.0	SD/TD	0.66
CT2/CT1	0.53	TL [mm]	1.78
R2/R1	-2.13	FOV [deg.]	82.0

14

-continued

3rd Embodiment			
5	$ (R3 - R4)/(R3 + R4) $	0.06	TL/tan(HFOV) [mm]
	$ (R5 - R6)/(R5 + R6) $	0.17	TL/ImgH
	f/f2	0.65	

4th Embodiment

FIG. 7 is a schematic view of an image capturing device according to the 4th embodiment of the present disclosure.

FIG. 8 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 4th embodiment.

In FIG. 7, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor **460**. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element **410**, an aperture stop **400**, a second lens element **420**, a third lens element **430**, an IR-cut filter **440** and an image plane **450**, wherein the image capturing lens assembly has a total of three lens elements (**410-430**) with refractive power.

The first lens element **410** with positive refractive power has a convex object-side surface **411** and a convex image-side surface **412**, which are both aspheric, and the first lens element **410** is made of plastic material.

The second lens element **420** with positive refractive power has a concave object-side surface **421** and a convex image-side surface **422**, which are both aspheric, and the second lens element **420** is made of plastic material.

The third lens element **430** with negative refractive power has a convex object-side surface **431** in a paraxial region thereof and a concave image-side surface **432** in a paraxial region thereof, which are both aspheric, and the third lens element **430** is made of plastic material. Moreover, the object-side surface **431** of the third lens element **430** has at least one concave shape in an off-axis region thereof, and the image-side surface **432** of the third lens element **430** has at least one convex shape in an off-axis region thereof.

The IR-cut filter **440** is made of glass and located between the third lens element **430** and the image plane **450**, and will not affect the focal length of the image capturing lens assembly. The image sensor **460** is disposed on the image plane **450** of the image capturing lens assembly.

The detailed optical data of the 4th embodiment are shown in Table 7 and the aspheric surface data are shown in Table 8 below.

TABLE 7

4th Embodiment								
f = 1.16 mm, Fno = 2.30, HFOV = 44.8 deg.								
Surface #		Curvature	Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Plano		Infinity				
1	Lens 1	1.484	ASP	0.250	Plastic	1.544	55.9	1.65
2		-2.150	ASP	0.019				
3	Ape. Stop	Plano		0.260				
4	Lens 2	-0.385	ASP	0.191	Plastic	1.583	30.2	2.26
5		-0.352	ASP	0.070				
6	Lens 3	0.561	ASP	0.170	Plastic	1.640	23.3	-9.09
7		0.451	ASP	0.300				
8	IR-cut filter	Plano		0.210	Glass	1.517	64.2	—
9		Plano		0.334				
10	Image	Plano		—				

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 8

Aspheric Coefficients			
Surface #	1	2	4
k =	8.1209E+00	1.2985E+01	-1.2813E+00
A4 =	-1.1355E+00	-9.8992E-01	-2.8666E-01
A6 =	-4.7695E+00	-1.3495E+00	-1.6785E+00
A8 =	3.5546E+00	3.2741E+01	-1.0289E+03
A10 =	—	—	2.0894E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-6.9632E+00	-1.0267E+00	-5.5750E+00
A4 =	-1.2407E+01	-5.2527E+00	-1.8038E+00
A6 =	1.3333E+02	2.0417E+01	4.6696E+00
A8 =	-1.3978E+03	-5.3565E+01	-7.0755E+00
A10 =	9.5730E+03	8.5818E+01	2.1729E+00
A12 =	-2.2990E+04	-7.3875E+01	5.8650E+00
A14 =	—	2.6000E+01	-4.4869E+00

In the image capturing lens assembly according to the 4th embodiment, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 4th embodiment. Moreover, these parameters can be calculated from Table 7 and Table 8 as the following values and satisfy the following conditions:

4th Embodiment			
f [mm]	1.16	f2/f3	-0.25
Fno	2.30	f/EPD	2.30
HFOV [deg.]	44.8	SD/TD	0.72
CT2/CT1	0.77	TL [mm]	1.80
R2/R1	-1.45	FOV [deg.]	89.6
(R3 - R4)/(R3 + R4)	0.04	TL/tan(HFOV) [mm]	1.82
(R5 - R6)/(R5 + R6)	0.11	TL/ImgH	1.50
f/f2	0.51		

5th Embodiment

FIG. 9 is a schematic view of an image capturing device according to the 5th embodiment of the present disclosure.

25

FIG. 10 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 5th embodiment.

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In FIG. 9, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor 560. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element 510, an aperture stop 500, a second lens element 520, a third lens element 530, an IR-cut filter 540 and an image plane 550, wherein the image capturing lens assembly has a total of three lens elements (510-530) with refractive power.

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The first lens element 510 with positive refractive power has a convex object-side surface 511 and a convex image-side surface 512, which are both aspheric, and the first lens element 510 is made of plastic material.

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The second lens element 520 with positive refractive power has a concave object-side surface 521 and a convex image-side surface 522, which are both aspheric, and the second lens element 520 is made of plastic material.

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The third lens element 530 with negative refractive power has a convex object-side surface 531 in a paraxial region thereof and a concave image-side surface 532 in a paraxial region thereof, which are both aspheric, and the third lens element 530 is made of plastic material. Moreover, the object-side surface 531 of the third lens element 530 has at least one concave shape in an off-axis region thereof, and the image-side surface 532 of the third lens element 530 has at least one convex shape in an off-axis region thereof.

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The IR-cut filter 540 is made of glass and located between the third lens element 530 and the image plane 550, and will not affect the focal length of the image capturing lens assembly. The image sensor 560 is disposed on the image plane 550 of the image capturing lens assembly.

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The detailed optical data of the 5th embodiment are shown in Table 9 and the aspheric surface data are shown in Table 10 below.

TABLE 9

5th Embodiment								
f = 1.16 mm, Fno = 2.50, HFOV = 39.1 deg.								
Surface #		Curvature	Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Plano		Infinity				
1	Lens 1	3.746	ASP	0.318	Plastic	1.535	56.3	1.59
2		-1.070	ASP	0.020				
3	Ape. Stop	Plano		0.247				
4	Lens 2	-0.394	ASP	0.200	Plastic	1.607	26.6	2.74
5		-0.380	ASP	0.154				
6	Lens 3	0.542	ASP	0.170	Plastic	1.640	23.3	-15.88
7		0.451	ASP	0.250				
8	IR-cut filter	Plano		0.210	Glass	1.517	64.2	—
9		Plano		0.403				
10	Image	Plano		—				

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 10

Aspheric Coefficients			
Surface #	1	2	4
k =	-5.5472E+01	-2.2584E+01	-1.9330E+00
A4 =	-4.8228E-01	-2.5880E+00	-1.3780E+00
A6 =	-5.2370E+00	9.9413E+00	-1.2585E+01
A8 =	1.4252E+01	-2.8688E+00	-4.6697E+02
A10 =	—	—	1.6829E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-1.2134E+01	-9.0117E-01	-4.8320E+00
A4 =	-1.5378E+01	-4.6457E+00	-1.3271E+00
A6 =	1.8895E+02	1.6834E+01	2.8468E+00
A8 =	-1.7808E+03	-5.1818E+01	-5.8304E+00
A10 =	1.0315E+04	9.0692E+01	4.0911E+00
A12 =	-2.2990E+04	-5.8273E+01	5.2831E+00
A14 =	—	-1.4871E+01	-7.3697E+00

In the image capturing lens assembly according to the 5th embodiment, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 5th embodiment. Moreover, these parameters can be calculated from Table 9 and Table 10 as the following values and satisfy the following conditions:

5th Embodiment			
f [mm]	1.16	f2/f3	-0.17
Fno	2.50	f/EPD	2.50
HFOV [deg.]	39.1	SD/TD	0.70
CT2/CT1	0.63	TL [mm]	1.97
R2/R1	-0.29	FOV [deg.]	78.2
(R3 - R4)/(R3 + R4)	0.02	TL/tan(HFOV) [mm]	2.43
(R5 - R6)/(R5 + R6)	0.09	TL/ImgH	1.97
f/f2	0.42		

6th Embodiment

FIG. 11 is a schematic view of an image capturing device according to the 6th embodiment of the present disclosure. FIG. 12 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 6th embodiment.

In FIG. 11, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor 660. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element 610, an aperture stop 600, a second lens element 620, a third lens element 630, an IR-cut filter 640 and an image plane 650, wherein the image capturing lens assembly has a total of three lens elements (610-630) with refractive power.

The first lens element 610 with positive refractive power has a convex object-side surface 611 and a convex image-side surface 612, which are both aspheric, and the first lens element 610 is made of plastic material.

The second lens element 620 with positive refractive power has a concave object-side surface 621 and a convex image-side surface 622, which are both aspheric, and the second lens element 620 is made of plastic material.

The third lens element 630 with negative refractive power has a convex object-side surface 631 in a paraxial region thereof and a concave image-side surface 632 in a paraxial region thereof, which are both aspheric, and the third lens element 630 is made of plastic material. Moreover, the object-side surface 631 of the third lens element 630 has at least one concave shape in an off-axis region thereof, and the image-side surface 632 of the third lens element 630 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 640 is made of glass and located between the third lens element 630 and the image plane 650, and will not affect the focal length of the image capturing lens assembly. The image sensor 660 is disposed on the image plane 650 of the image capturing lens assembly.

The detailed optical data of the 6th embodiment are shown in Table 11 and the aspheric surface data are shown in Table 12 below.

TABLE 11

6th Embodiment								
f = 1.16 mm, Fno = 2.40, HFOV = 40.7 deg.								
Surface #		Curvature	Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Plano		Infinity				
1	Lens 1	1.371	ASP	0.313	Plastic	1.544	55.9	1.40
2		-1.589	ASP	-0.015				
3	Ape. Stop	Plano		0.297				
4	Lens 2	-0.292	ASP	0.189	Plastic	1.544	55.9	2.63
5		-0.298	ASP	0.025				
6	Lens 3	0.655	ASP	0.239	Plastic	1.544	55.9	-7.32
7		0.490	ASP	0.250				
8	IR-cut filter	Plano		0.210	Glass	1.517	64.2	—
9		Plano		0.267				
10	Image	Plano		—				

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 12

Aspheric Coefficients			
Surface #	1	2	4
k =	-3.5816E+00	-8.9231E+01	-2.5357E+00
A4 =	-9.3307E-01	-3.3670E+00	-5.9941E+00
A6 =	2.2485E-01	-2.7292E-02	-1.1447E+01
A8 =	-2.1919E+01	1.4295E+02	-4.1117E+02
A10 =	—	—	1.8241E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-3.6715E+00	-2.1994E+00	-7.2018E+00
A4 =	-1.0995E+01	-3.7022E+00	-1.2793E+00
A6 =	1.0433E+02	1.8609E+01	3.6037E+00
A8 =	-1.1556E+03	-5.5221E+01	-5.4395E+00
A10 =	9.0166E+03	9.1726E+01	1.5935E+00
A12 =	-2.2990E+04	-7.8819E+01	3.2563E+00
A14 =	—	2.7336E+01	-2.2184E+00

In the image capturing lens assembly according to the 6th embodiment, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 6th embodiment. Moreover, these parameters can be calculated from Table 11 and Table 12 as the following values and satisfy the following conditions:

6th Embodiment			
f [mm]	1.16	f2/f3	-0.36
Fno	2.40	f/EPD	2.40
HFOV [deg.]	40.7	SD/TD	0.72
CT2/CT1	0.60	TL [mm]	1.77
R2/R1	-1.16	FOV [deg.]	81.4
$(R3 - R4)/(R3 + R4)$	0.01	TL/tan(HFOV) [mm]	2.06
$(R5 - R6)/(R5 + R6)$	0.14	TL/ImgH	1.77
f/f2	0.44		

7th Embodiment

FIG. 13 is a schematic view of an image capturing device according to the 7th embodiment of the present disclosure. FIG. 14 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 7th embodiment.

In FIG. 13, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor 760. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element 710, an aperture stop 700, a second lens element 720, a third lens element 730, an IR-cut filter 740 and an image plane 750, wherein the image capturing lens assembly has a total of three lens elements (710-730) with refractive power.

The first lens element 710 with positive refractive power has a convex object-side surface 711 and a convex image-side surface 712, which are both aspheric, and the first lens element 710 is made of plastic material.

The second lens element 720 with positive refractive power has a concave object-side surface 721 and a convex image-side surface 722, which are both aspheric, and the second lens element 720 is made of plastic material.

The third lens element 730 with negative refractive power has a convex object-side surface 731 in a paraxial region thereof and a concave image-side surface 732 in a paraxial region thereof, which are both aspheric, and the third lens element 730 is made of plastic material. Moreover, the object-side surface 731 of the third lens element 730 has at least one concave shape in an off-axis region thereof, and the image-side surface 732 of the third lens element 730 has at least one convex shape in an off-axis region thereof.

The IR-cut filter 740 is made of glass and located between the third lens element 730 and the image plane 750, and will not affect the focal length of the image capturing lens assembly. The image sensor 760 is disposed on the image plane 750 of the image capturing lens assembly.

The detailed optical data of the 7th embodiment are shown in Table 13 and the aspheric surface data are shown in Table 14 below.

TABLE 13

7th Embodiment								
f = 0.98 mm, Fno = 2.20, HFOV = 43.9 deg.								
Surface #		Curvature Radius	Thickness	Material	Index	Abbe #	Focal Length	
0	Object	Plano	Infinity					
1	Lens 1	1.427	ASP	0.265	Plastic	1.586	55.0	1.40
2		-1.800	ASP	-0.008				
3	Ape. Stop	Plano	0.256					
4	Lens 2	-0.391	ASP	0.212	Plastic	1.586	55.0	1.57
5		-0.329	ASP	0.025				
6	Lens 3	0.576	ASP	0.200	Plastic	1.614	25.6	-3.89
7		0.403	ASP	0.200				
8	IR-cut filter	Plano	0.145	Glass	1.517	64.2		—
9		Plano	0.268					
10	Image	Plano	—					

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 14

Aspheric Coefficients			
Surface #	1	2	4
k =	-4.1987E+00	-5.1392E+01	-3.7701E+00
A4 =	-1.2265E+00	-2.1580E+00	-4.7585E+00
A6 =	2.0408E+00	-1.1633E+01	1.4589E+00
A8 =	-3.6093E+01	1.8104E+02	-8.0701E+02
A10 =	—	—	1.9921E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-4.9440E+00	-1.0998E+00	-5.2427E+00
A4 =	-1.1258E+01	-5.0724E+00	-1.6137E+00
A6 =	1.1334E+02	2.0963E+01	4.3583E+00
A8 =	-1.2871E+03	-5.4591E+01	-7.5428E+00
A10 =	9.4669E+03	8.4302E+01	4.4368E+00
A12 =	-2.2990E+04	-6.6919E+01	4.0930E+00
A14 =	—	2.1379E+01	-3.2659E+00
A16 =	—	-2.9673E+00	-1.6683E+00

In the image capturing lens assembly according to the 7th embodiment, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 7th embodiment. Moreover, these parameters can be calculated from Table 13 and Table 14 as the following values and satisfy the following conditions:

7th Embodiment			
f [mm]	0.98	f2/f3	-0.40
Fno	2.20	f/EPD	2.20
HFOV [deg.]	43.9	SD/TD	0.73
CT2/CT1	0.80	TL [mm]	1.56
R2/R1	-1.26	FOV [deg.]	87.8
(R3 - R4)/(R3 + R4)	0.09	TL/tan(HFOV) [mm]	1.62
(R5 - R6)/(R5 + R6)	0.18	TL/ImgH	1.68
f/f2	0.63		

8th Embodiment

FIG. 15 is a schematic view of an image capturing device according to the 8th embodiment of the present disclosure. FIG. 16 shows, in order from left to right, spherical aberration curves, astigmatic field curves and a distortion curve of the image capturing device according to the 8th embodiment.

In FIG. 15, the image capturing device includes the image capturing lens assembly (not otherwise herein labeled) of the present disclosure and an image sensor **860**. The image capturing lens assembly includes, in order from an object side to an image side, a first lens element **810**, an aperture stop **800**, a second lens element **820**, a third lens element **830**, an IR-cut filter **840** and an image plane **850**, wherein the image capturing lens assembly has a total of three lens elements (**810-830**) with refractive power.

The first lens element **810** with positive refractive power has a convex object-side surface **811** and a convex image-side surface **812**, which are both aspheric, and the first lens element **810** is made of glass material.

The second lens element **820** with positive refractive power has a concave object-side surface **821** and a convex image-side surface **822**, which are both aspheric, and the second lens element **820** is made of plastic material.

The third lens element **830** with negative refractive power has a convex object-side surface **831** in a paraxial region thereof and a concave image-side surface **832** in a paraxial region thereof, which are both aspheric, and the third lens element **830** is made of plastic material. Moreover, the object-side surface **831** of the third lens element **830** has at least one concave shape in an off-axis region thereof, and the image-side surface **832** of the third lens element **830** has at least one convex shape in an off-axis region thereof.

The IR-cut filter **840** is made of glass and located between the third lens element **830** and the image plane **850**, and will not affect the focal length of the image capturing lens assembly. The image sensor **860** is disposed on the image plane **850** of the image capturing lens assembly.

The detailed optical data of the 8th embodiment are shown in Table 15 and the aspheric surface data are shown in Table 16 below.

TABLE 15

8th Embodiment								
f = 0.89 mm, Fno = 2.20, HFOV = 45.9 deg.								
Surface #		Curvature	Radius	Thickness	Material	Index	Abbe #	Focal Length
0	Object	Plano		Infinity				
1	Lens 1	1.469	ASP	0.247	Glass	1.603	38.0	1.42
2		-1.912	ASP	-0.004				
3	Ape. Stop	Plano		0.228				
4	Lens 2	-0.408	ASP	0.195	Plastic	1.586	55.0	1.95
5		-0.353	ASP	0.025				
6	Lens 3	0.469	ASP	0.200	Plastic	1.586	55.0	-43.35
7		0.388	ASP	0.220				
8	IR-cut filter	Plano		0.145	Glass	1.517	64.2	—
9		Plano		0.198				
10	Image	Plano		—				

Note:

Reference wavelength is 587.6 nm (d-line).

TABLE 16

Aspheric Coefficients			
Surface #	1	2	4
k =	-1.2224E+00	-2.0696E+01	-6.9503E+00
A4 =	-1.3055E+00	-1.7420E+00	-4.7868E+00
A6 =	5.5074E-01	-7.1560E-01	2.1451E+01
A8 =	-2.8141E+01	2.8621E+01	-7.9739E+02
A10 =	—	—	1.9005E+04
A12 =	—	—	-9.4560E+04
Surface #	5	6	7
k =	-7.6226E+00	-9.9558E-01	-3.9951E+00
A4 =	-1.2148E+01	-5.6843E+00	-1.6872E+00
A6 =	1.2627E+02	2.1530E+01	4.3809E+00
A8 =	-1.2443E+03	-5.3532E+01	-7.3765E+00
A10 =	9.1595E+03	8.3998E+01	4.6844E+00
A12 =	-2.2990E+04	-7.0743E+01	3.4379E+00
A14 =	—	2.0601E+01	-2.5197E+00
A16 =	—	2.3995E+00	-2.6819E+00

In the image capturing lens assembly according to the 8th embodiment, the definitions of these parameters shown in the following table are the same as those stated in the 1st embodiment with corresponding values for the 8th embodiment. Moreover, these parameters can be calculated from Table 15 and Table 16 as the following values and satisfy the following conditions:

8th Embodiment			
f [mm]	0.89	f2/f3	-0.04
Fno	2.20	f/EPD	2.20
HFOV [deg.]	45.9	SD/TD	0.73
CT2/CT1	0.79	TL [mm]	1.45
R2/R1	-1.30	FOV [deg.]	91.8
(R3 - R4)/(R3 + R4)	0.07	TL/tan(HFOV) [mm]	1.41
(R5 - R6)/(R5 + R6)	0.09	TL/ImgH	1.61
f/f2	0.46		

The aforementioned image capturing device can be installed in the mobile terminals. The first lens element of the image capturing lens assembly can have a convex object-side surface and a convex image-side surface, so that it is favorable for reducing the total track length of the image capturing device. In addition, the aperture stop can be close to the image plane which is favorable for increasing the field of view so as to obtain more of the image scene under a limited distance.

The foregoing description, for purpose of explanation, has been described with reference to specific embodiments. It is to be noted that TABLES 1-16 show different data of the different embodiments; however, the data of the different embodiments are obtained from experiments. The embodiments were chosen and described in order to best explain the principles of the disclosure and its practical applications, to thereby enable others skilled in the art to best utilize the disclosure and various embodiments with various modifications as are suited to the particular use contemplated. The embodiments depicted above and the appended drawings are exemplary and are not intended to be exhaustive or to limit the scope of the present disclosure to the precise forms disclosed. Many modifications and variations are possible in view of the above teachings.

What is claimed is:

1. An image capturing lens assembly comprising, in order from an object side to an image side:
 - a first lens element with positive refractive power having a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric;
 - a second lens element with positive refractive power having a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric; and
 - a third lens element with negative refractive power having a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and an object-side surface and the image-side surface of the third lens element are aspheric;
 wherein the image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element, a focal length of the image capturing lens assembly is f, a focal length of the second lens element is f2, a focal length of the third lens element is f3, an axial distance between the stop and the image-side surface of the third lens element is SD, an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD, a central thickness of the first lens element is CT1, a central thickness of the second lens

25

element is CT2, an entrance pupil diameter of the image capturing lens assembly is EPD, and the following conditions are satisfied:

$$-3.0 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82;$$

$$0.20 < CT_2/CT_1 < 0.85; \text{ and}$$

$$1.20 < f/EPD < 2.80.$$

2. The image capturing lens assembly of claim 1, wherein the third lens element has the object-side surface being convex in a paraxial region thereof, and the object-side surface of the third lens element has at least one concave shape in an off-axis region thereof.

3. The image capturing lens assembly of claim 1, wherein the focal length of the second lens element is f_2 , the focal length of the third lens element is f_3 , and the following condition is satisfied:

$$-1.5 < f_2/f_3 < 0.$$

4. The image capturing lens assembly of claim 1, wherein the central thickness of the first lens element is CT1, the central thickness of the second lens element is CT2, and the following condition is satisfied:

$$0.30 < CT_2/CT_1 < 0.75.$$

5. The image capturing lens assembly of claim 1, wherein a maximal field of view of the image capturing lens assembly is FOV, and the following condition is satisfied:

$$76 \text{ degrees} < \text{FOV} < 120 \text{ degrees}.$$

6. The image capturing lens assembly of claim 1, wherein an axial distance between the object-side surface of the first lens element and an image plane is TL, and the following condition is satisfied:

$$1.0 \text{ mm} < TL < 2.3 \text{ mm}.$$

7. The image capturing lens assembly of claim 1, wherein a curvature radius of the object-side surface of the third lens element is R5, a curvature radius of the image-side surface of the third lens element is R6, and the following condition is satisfied:

$$|(R_5 - R_6)/(R_5 + R_6)| < 0.35.$$

8. An image capturing lens assembly comprising, in order from an object side to an image side:

a first lens element with positive refractive power having a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric;

a second lens element with positive refractive power having a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric;

a third lens element with negative refractive power having a convex object-side surface and a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and the object-side surface and the image-side surface of the third lens element are aspheric; and

wherein the image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element, a focal length of the second

26

lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD, an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD, a curvature radius of the object-side surface of the first lens element is R1, and a curvature radius of the image-side surface of the first lens element is R2, the following conditions are satisfied:

$$-0.90 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82; \text{ and}$$

$$-3.0 < R_2/R_1 < -0.2.$$

9. The image capturing lens assembly of claim 8, wherein the curvature radius of the object-side surface of the first lens element is R1, the curvature radius of the image-side surface of the first lens element is R2, the following condition is satisfied:

$$-2.0 < R_2/R_1 < -0.2.$$

10. The image capturing lens assembly of claim 8, wherein a focal length of the image capturing lens assembly is f , the focal length of the second lens element is f_2 , and the following condition is satisfied:

$$0.4 < f/f_2 < 1.0.$$

11. The image capturing lens assembly of claim 8, wherein a curvature radius of the object-side surface of the second lens element is R3, a curvature radius of the image-side surface of the second lens element is R4, and the following condition is satisfied:

$$|(R_3 - R_4)/(R_3 + R_4)| < 0.15.$$

12. The image capturing lens assembly of claim 8, wherein an axial distance between the object-side surface of the first lens element and an image plane is TL, a maximum image height of the image capturing lens assembly is $ImgH$, and the following condition is satisfied:

$$TL/ImgH < 1.90.$$

13. The image capturing lens assembly of claim 8, wherein a focal length of the image capturing lens assembly is f , an entrance pupil diameter of the image capturing lens assembly is EPD, and the following condition is satisfied:

$$1.60 < f/EPD < 2.45.$$

14. The image capturing lens assembly of claim 8, wherein a curvature radius of the object-side surface of the third lens element is R5, a curvature radius of the image-side surface of the third lens element is R6, and the following condition is satisfied:

$$|(R_5 - R_6)/(R_5 + R_6)| < 0.25.$$

15. The image capturing lens assembly of claim 8, wherein an axial distance between the object-side surface of the first lens element and an image plane is TL, half of a maximal field of view of the image capturing lens assembly is HFOV, and the following condition is satisfied:

$$1.0 \text{ mm} < TL/\tan(\text{HFOV}) < 3.0 \text{ mm}.$$

16. An image capturing lens assembly comprising, in order from an object side to an image side:

a first lens element with positive refractive power having a convex object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the first lens element are aspheric;

27

a second lens element with positive refractive power having a concave object-side surface and a convex image-side surface, wherein the object-side surface and the image-side surface of the second lens element are aspheric;

a third lens element with negative refractive power having a convex object-side surface and a concave image-side surface in a paraxial region thereof, wherein the image-side surface of the third lens element has at least one convex shape in an off-axis region thereof, and the object-side surface and the image-side surface of the third lens element are aspheric; and

wherein the image capturing lens assembly has a total of three lens elements with refractive power and further includes a stop disposed between the first lens element and the second lens element, a focal length of the second lens element is f_2 , a focal length of the third lens element is f_3 , an axial distance between the stop and the image-side surface of the third lens element is SD , an axial distance between the object-side surface of the first lens element and the image-side surface of the third lens element is TD , an axial distance between the object-side surface of the first lens element and an image plane is TL , and the following conditions are satisfied:

$$-3.0 < f_2/f_3 < 0;$$

$$0.58 < SD/TD < 0.82; \text{ and}$$

$$1.0 \text{ mm} < TL < 2.0 \text{ mm}.$$

17. The image capturing lens assembly of claim 16, wherein a curvature radius of the object-side surface of the third lens element is R_5 , a curvature radius of the image-side

28

surface of the third lens element is R_6 , and the following condition is satisfied:

$$|(R_5 - R_6)/(R_5 + R_6)| < 0.35.$$

18. The image capturing lens assembly of claim 16, wherein a curvature radius of the object-side surface of the first lens element is R_1 , a curvature radius of the image-side surface of the first lens element is R_2 , and the following condition is satisfied:

$$-2.0 < R_2/R_1 < -0.2.$$

19. The image capturing lens assembly of claim 16, wherein the focal length of the second lens element is f_2 , the focal length of the third lens element is f_3 , and the following condition is satisfied:

$$-0.90 < f_2/f_3 < 0.$$

20. The image capturing lens assembly of claim 16, wherein a central thickness of the first lens element is CT_1 , a central thickness of the second lens element is CT_2 , and the following condition is satisfied:

$$0.20 < CT_2/CT_1 < 0.85.$$

21. The image capturing lens assembly of claim 16, wherein an axial distance between the object-side surface of the first lens element and the image plane is TL , half of a maximal field of view of the image capturing lens assembly is $HFOV$, and the following condition is satisfied:

$$1.0 \text{ mm} < TL/\tan(HFOV) < 3.0 \text{ mm}.$$

22. An image capturing device comprising, in order from an object side to an image side:

the image capturing lens assembly of claim 16; and
an image sensor.

23. A mobile terminal comprising,
the image capturing device of claim 22.

* * * * *