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(12) **United States Patent**  
**Victorine et al.**

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(45) **Date of Patent:** **Dec. 16, 2014**

(54) **CRIMP TERMINATIONS FOR CONDUCTORS IN IMPLANTABLE MEDICAL LEAD AND METHOD OF MAKING SAME**

(58) **Field of Classification Search**  
USPC ..... 607/1-2, 115-116; 600/372-373, 377  
See application file for complete search history.

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(56) **References Cited**

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(73) Assignee: **Pacesetter, Inc.**, Sylmar, CA (US)

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(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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(21) Appl. No.: **14/051,877**

Restriction Requirement, mailed Aug. 20, 2012—U.S. Appl. No. 12/716,552.  
NonFinal Office Action, mailed Nov. 2, 2012—U.S. Appl. No. 12/716,552.  
Notice of Allowance, mailed Sep. 9, 2013—U.S. Appl. No. 12/716,552.

(22) Filed: **Oct. 11, 2013**

(65) **Prior Publication Data**

US 2014/0081364 A1 Mar. 20, 2014

\* cited by examiner

**Related U.S. Application Data**

*Primary Examiner* — Deborah Malamud

(62) Division of application No. 12/716,552, filed on Mar. 3, 2010, now Pat. No. 8,594,761.

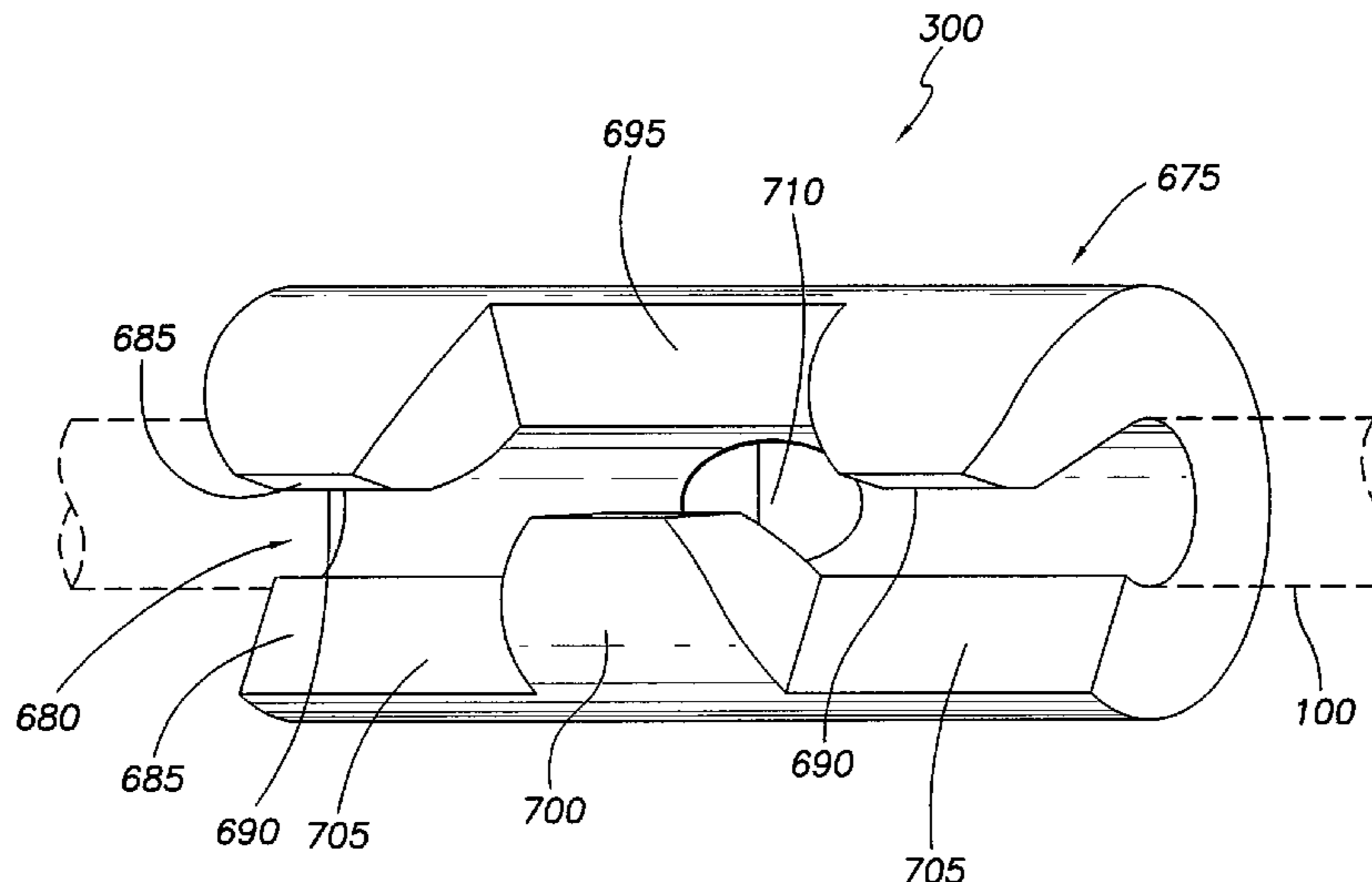
(57) **ABSTRACT**

(51) **Int. Cl.**  
*A61N 1/05* (2006.01)  
*H01R 43/00* (2006.01)  
*H01R 43/048* (2006.01)

A method of manufacturing an implantable medical lead is disclosed herein. The method may include: providing a lead body including a proximal end, a distal end, and an electrode near the distal end; provide a conductor extending between the proximal and distal ends; providing a crimp including a ribbon-like member and extending the ribbon-like member around the conductor; and mechanically and electrically connecting the ribbon-like member to the electrode.

(52) **U.S. Cl.**  
CPC *A61N 1/05* (2013.01); *H01R 43/00* (2013.01); *H01R 43/048* (2013.01)  
USPC ..... **600/373**; 607/1; 607/2; 607/115; 607/116; 600/372; 600/377

**6 Claims, 35 Drawing Sheets**



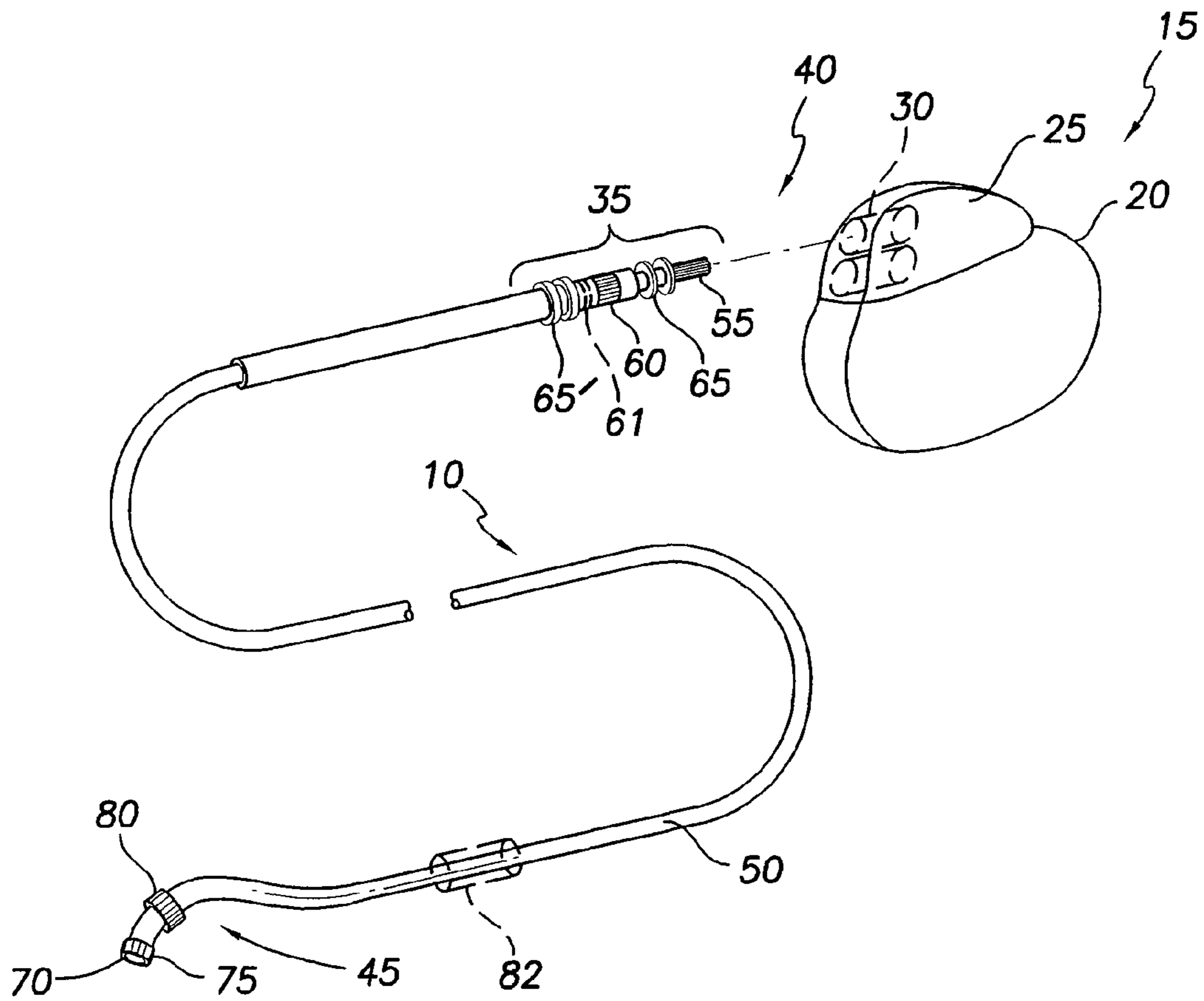


FIG. 1

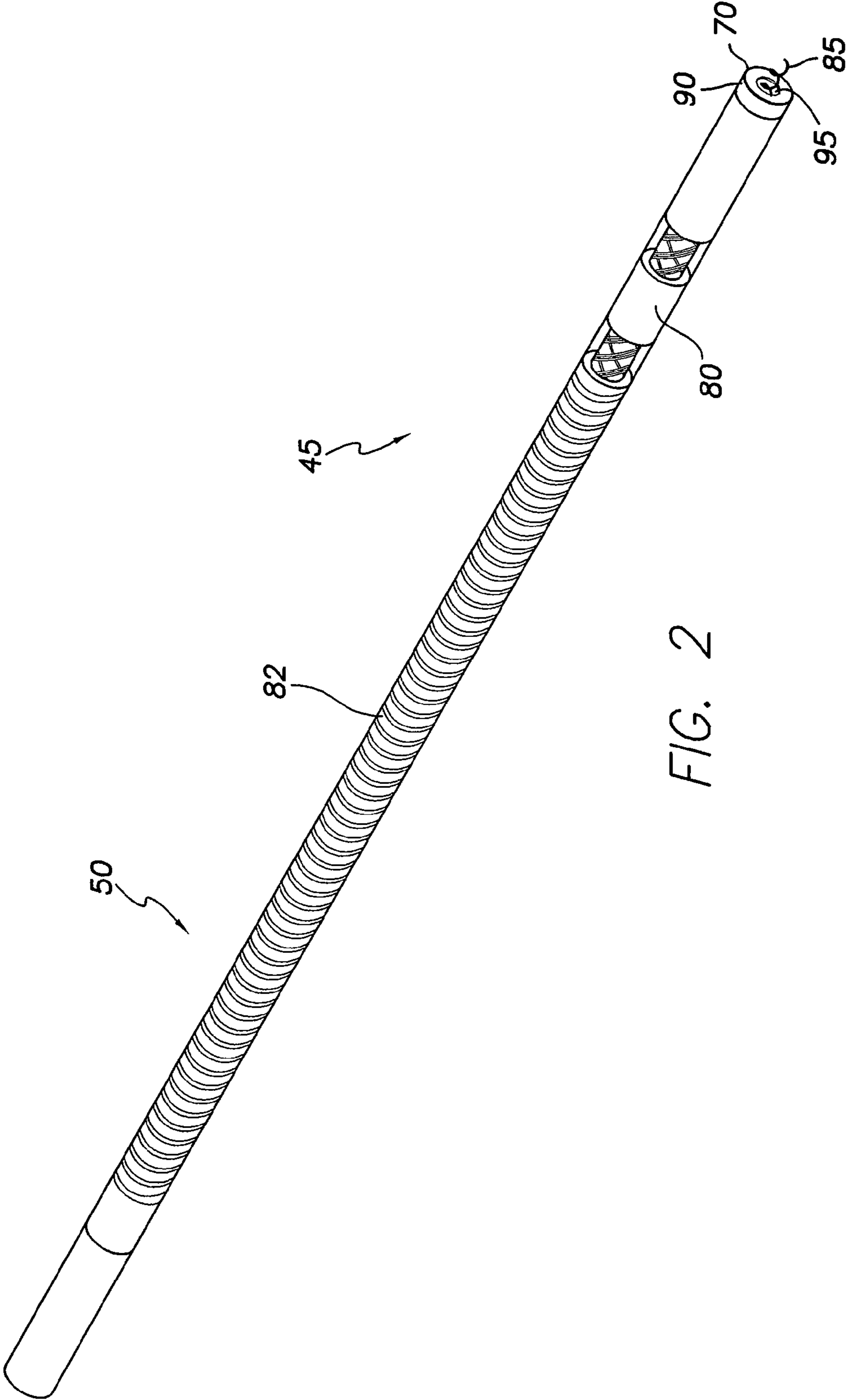


FIG. 2

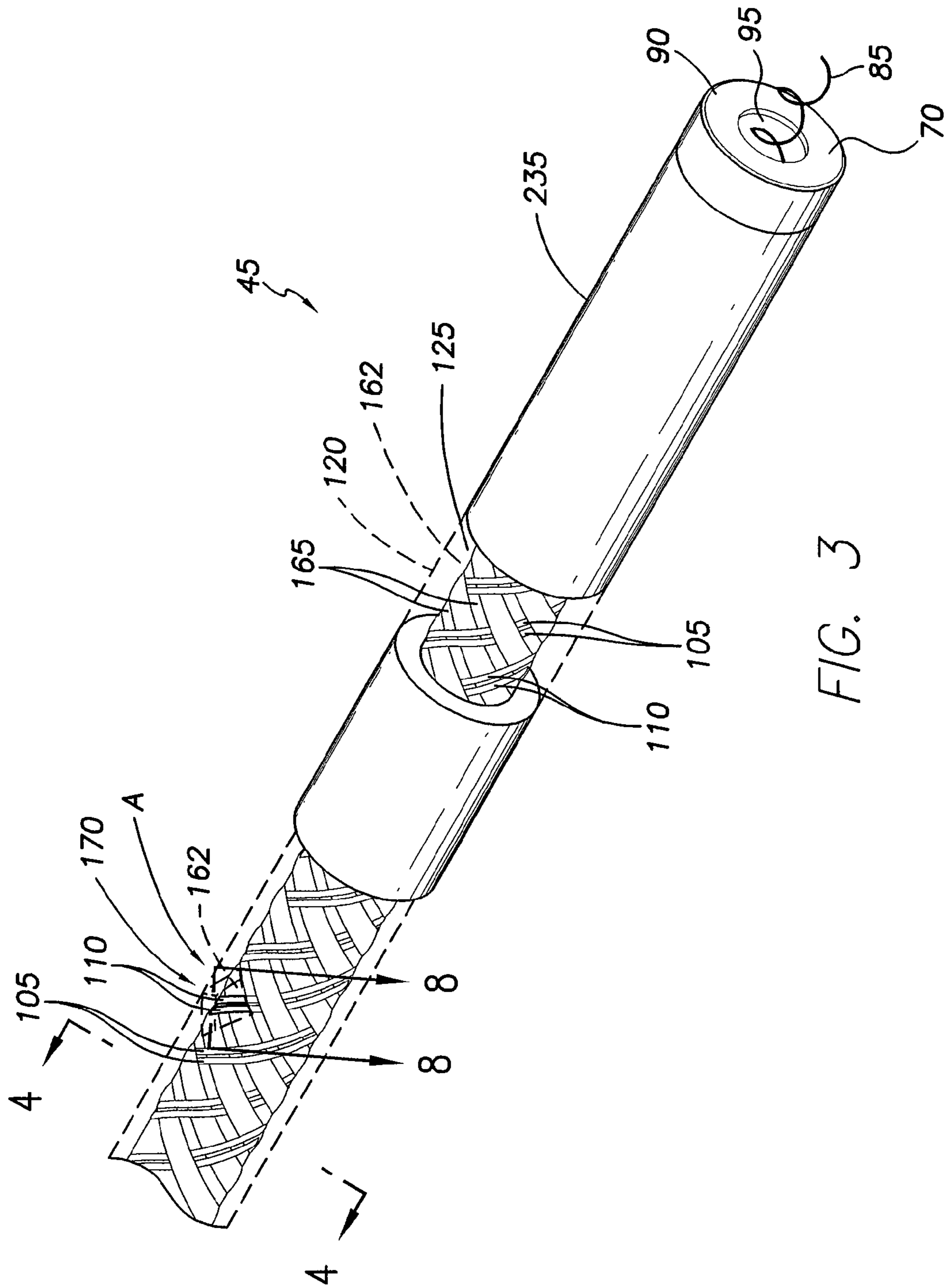


FIG. 3

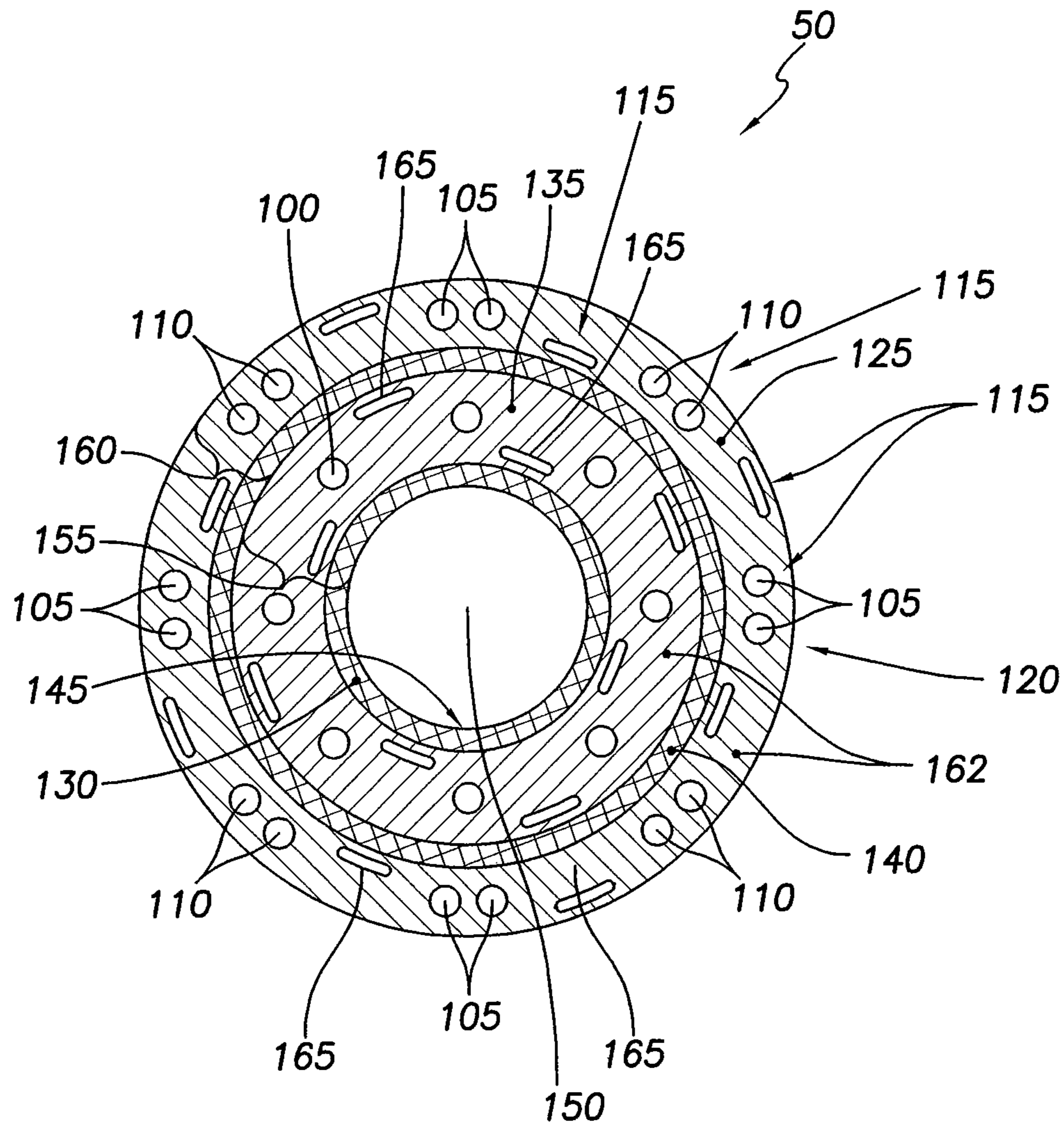


FIG. 4

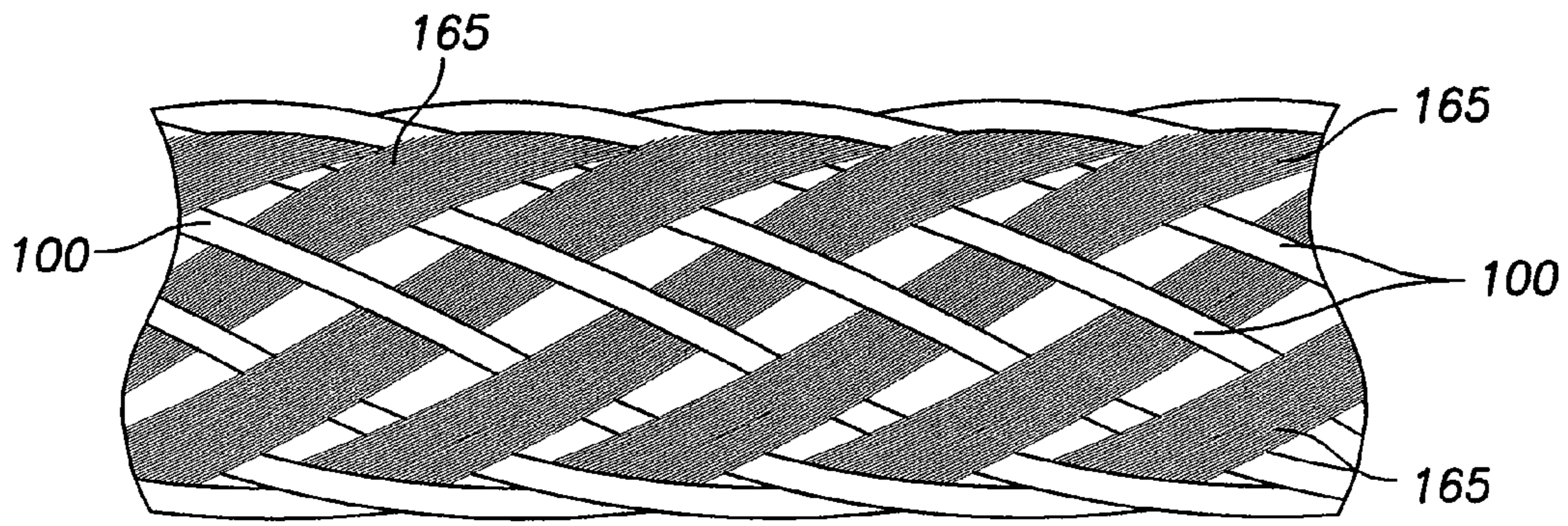


FIG. 5

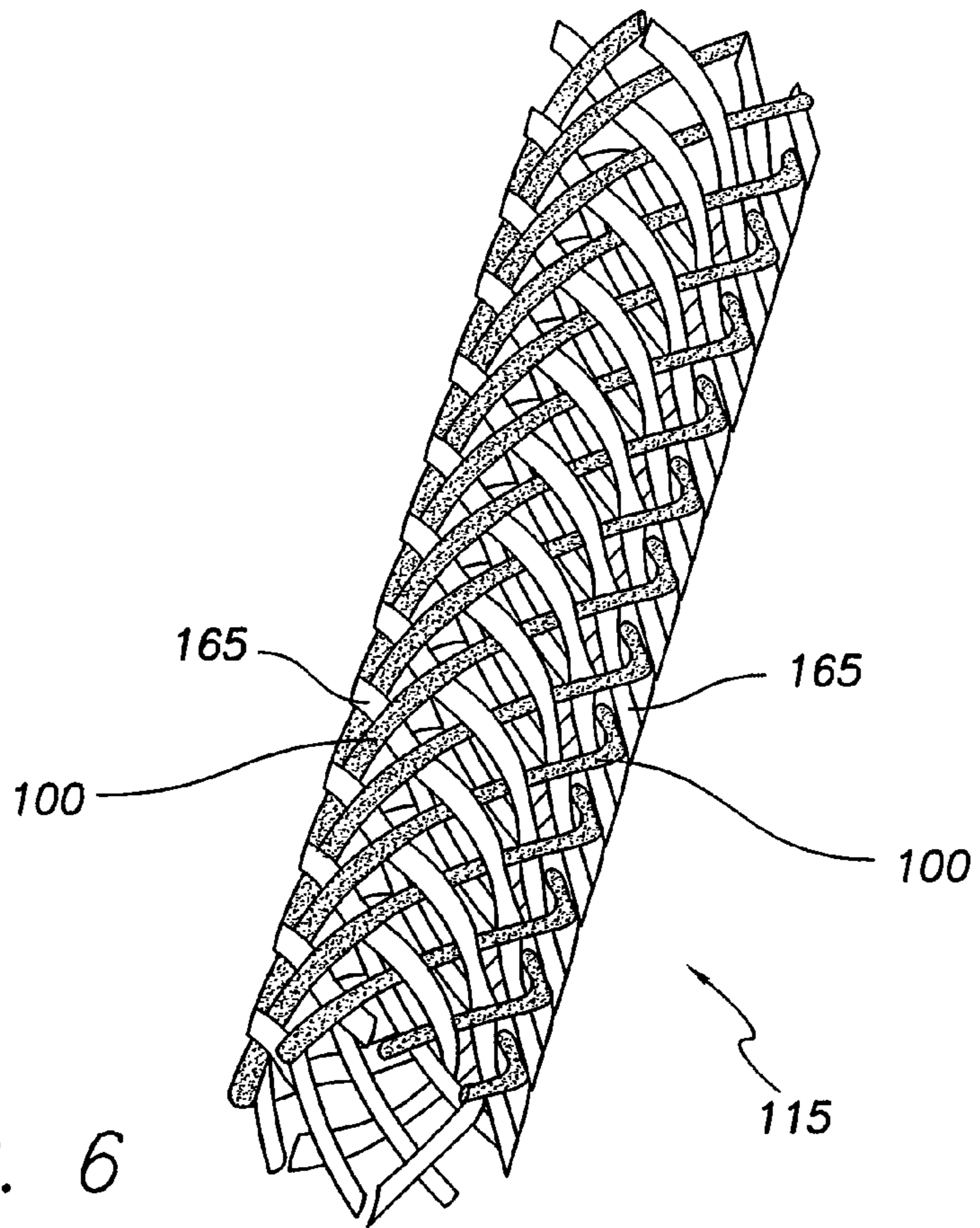


FIG. 6



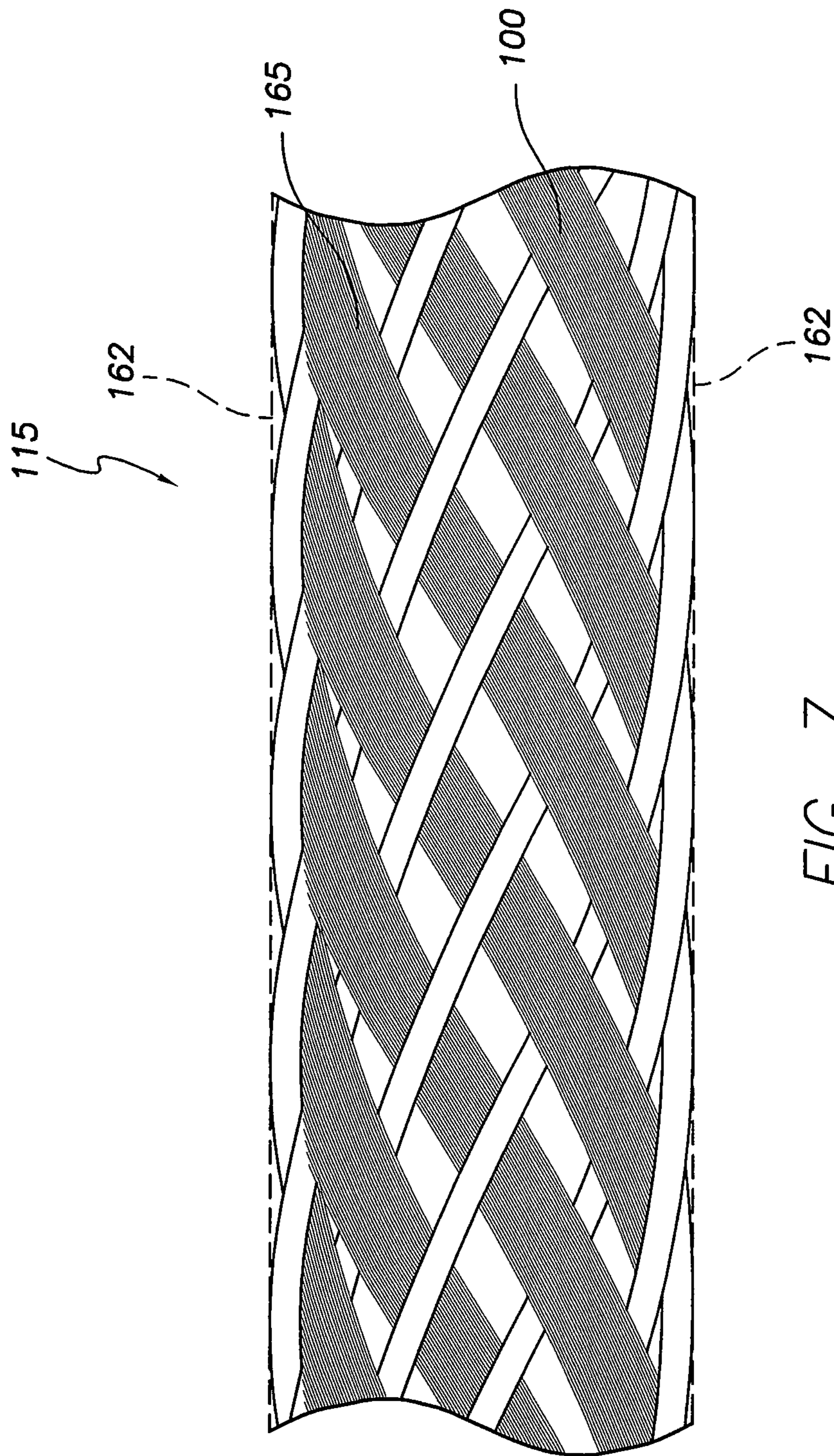


FIG. 7

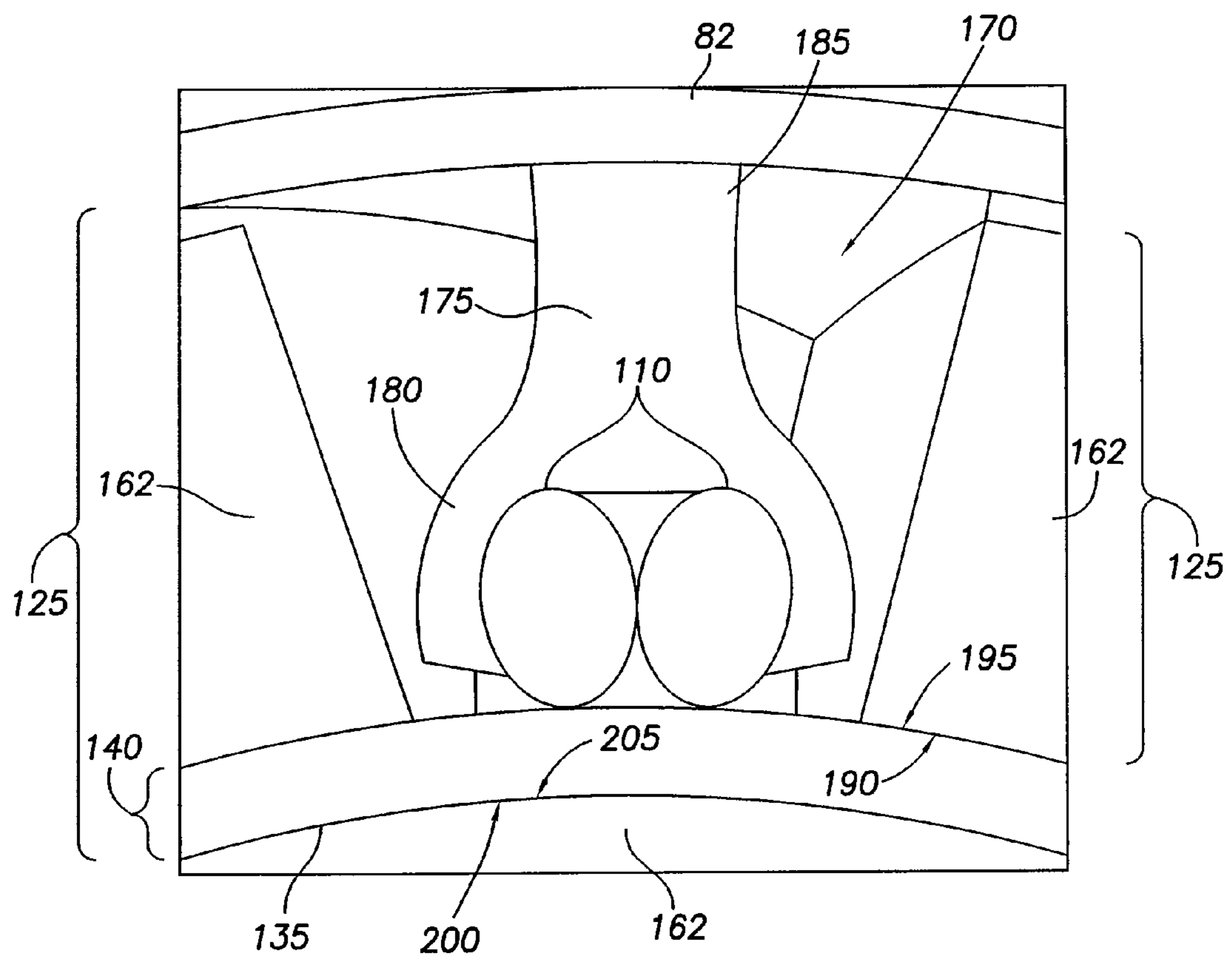


FIG. 8



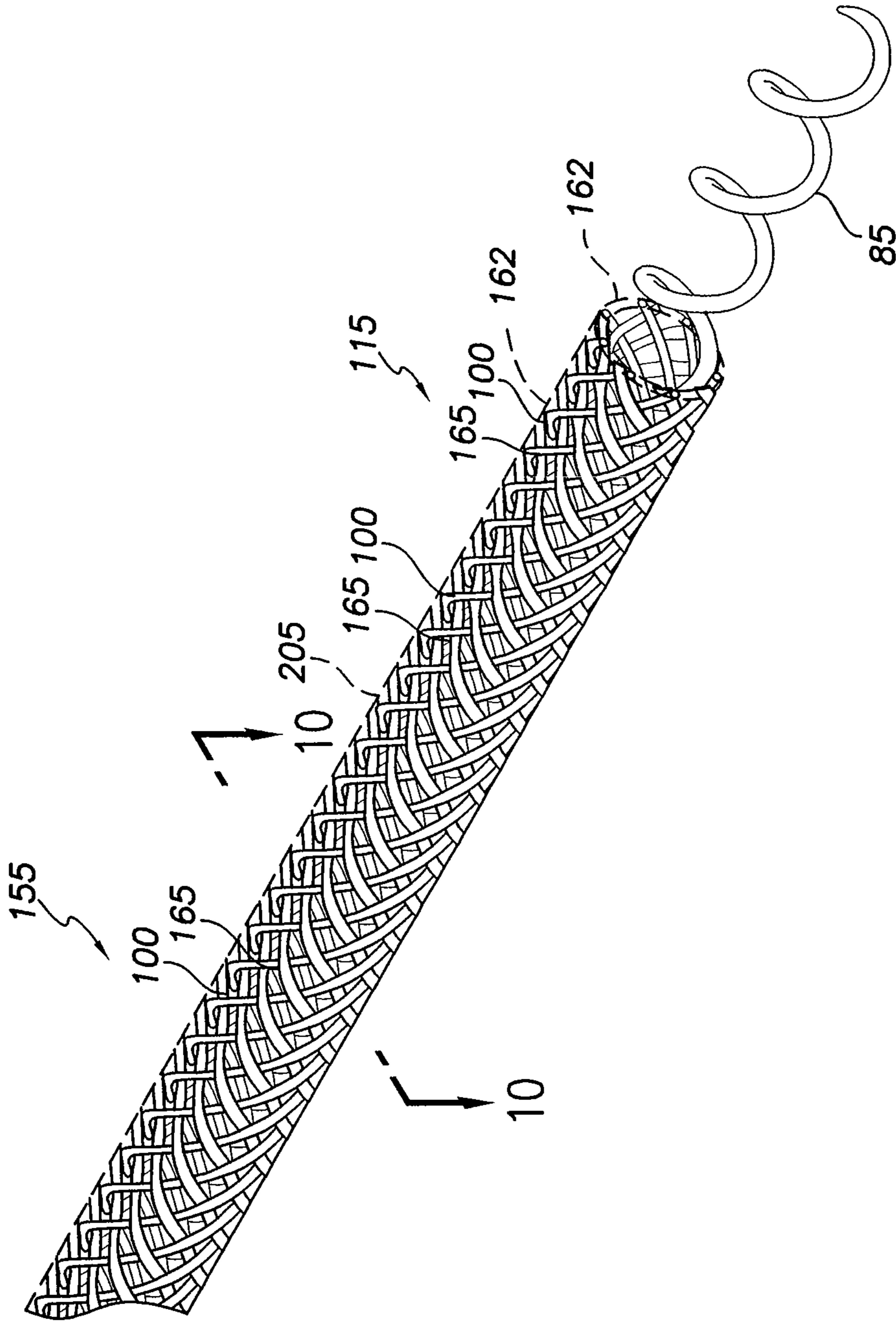


FIG. 9

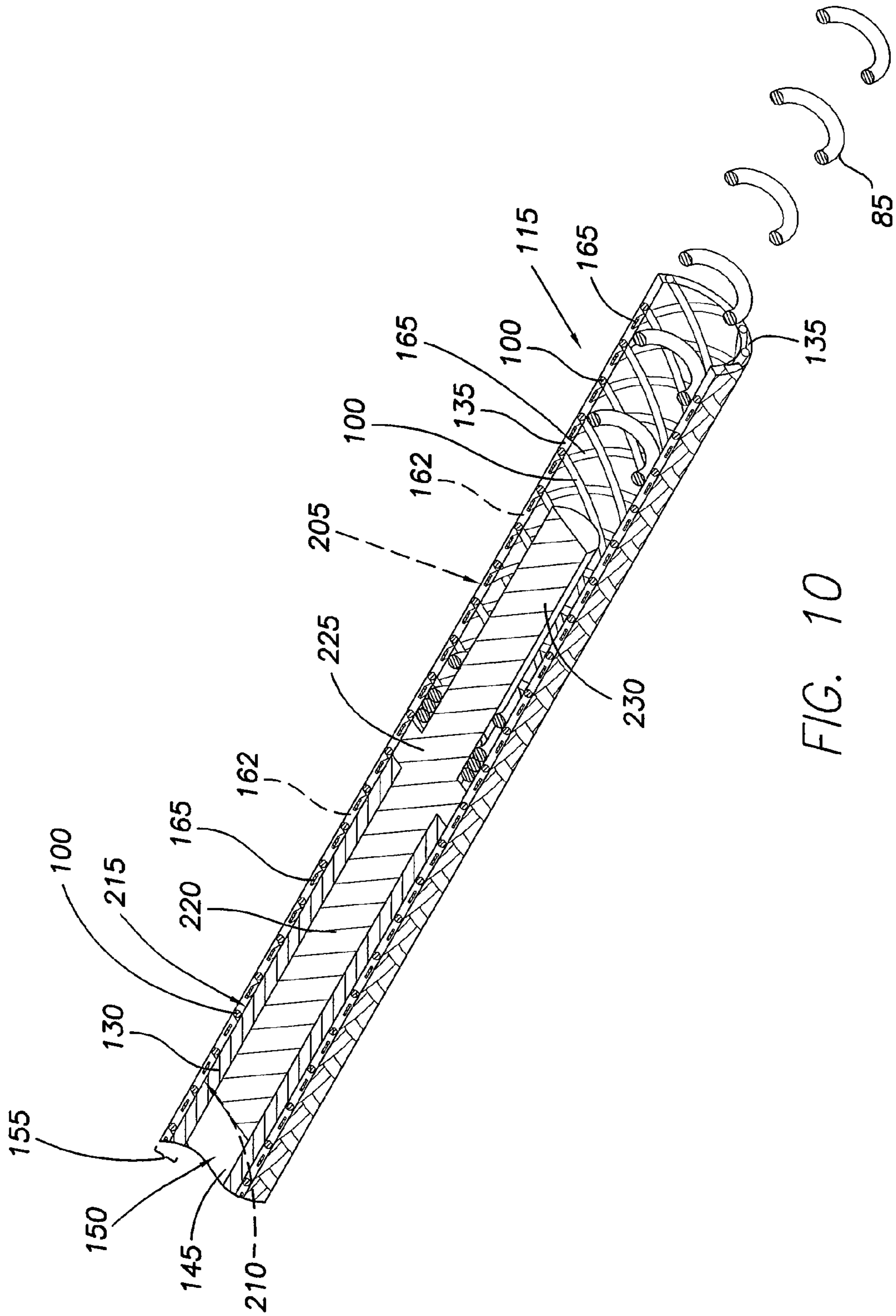


FIG. 10

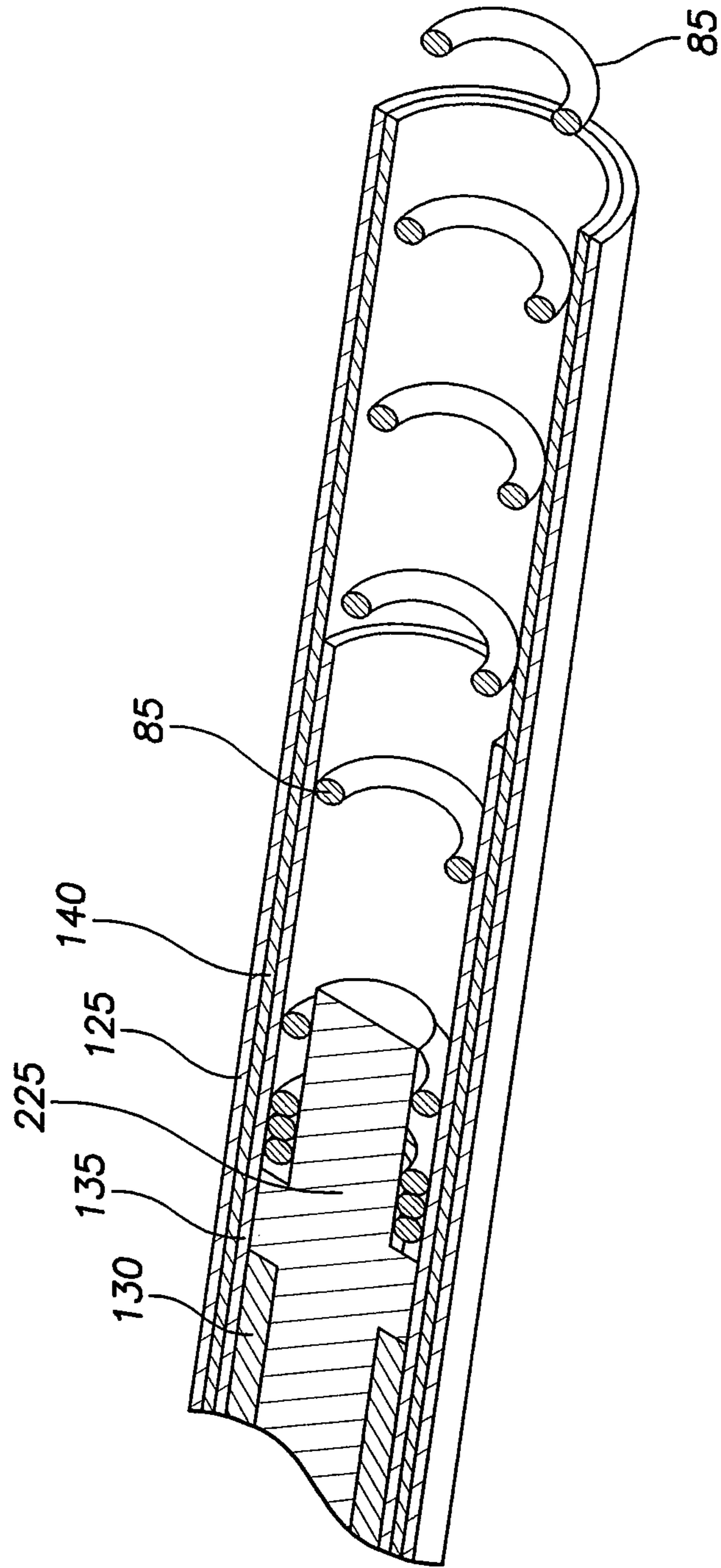
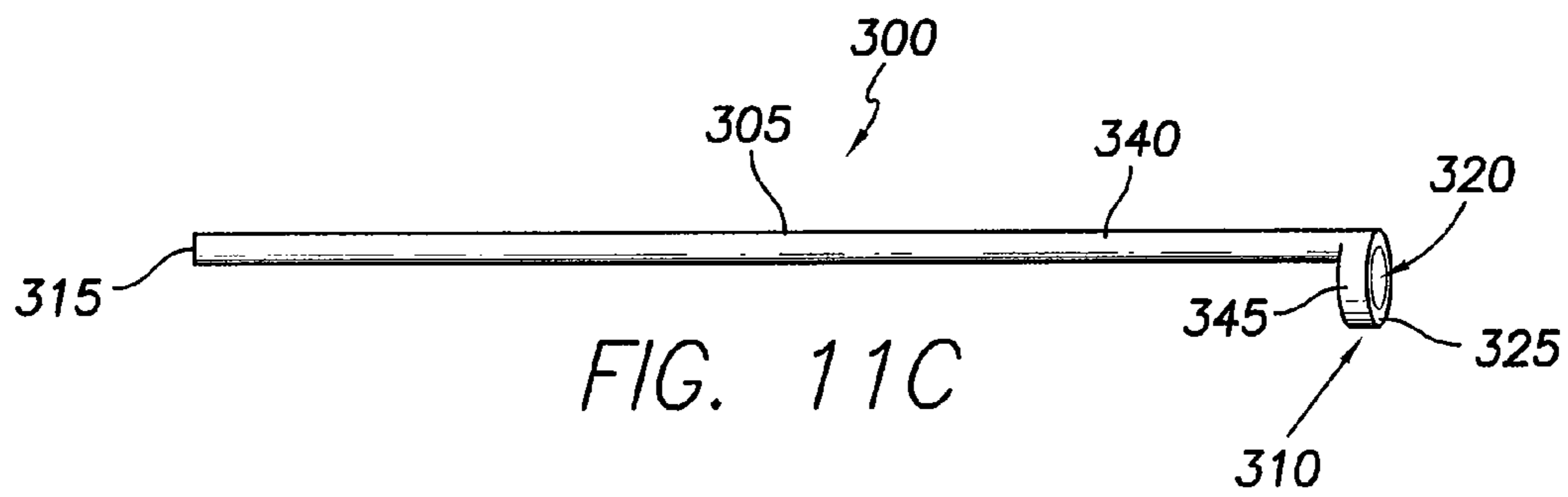
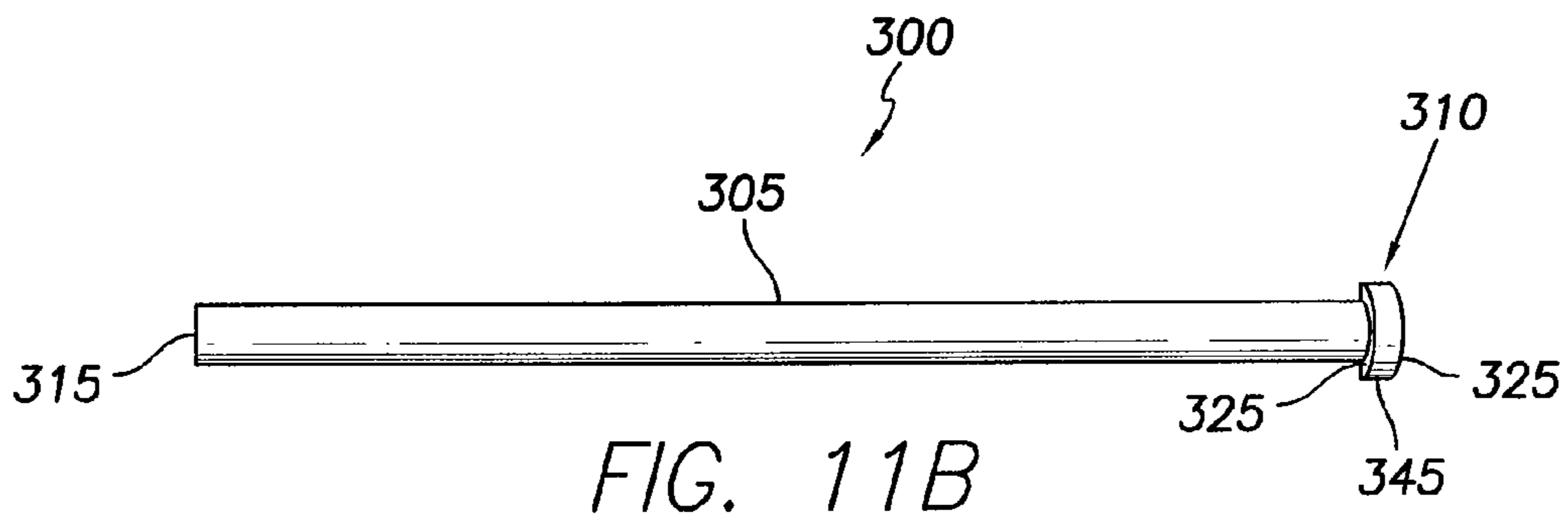
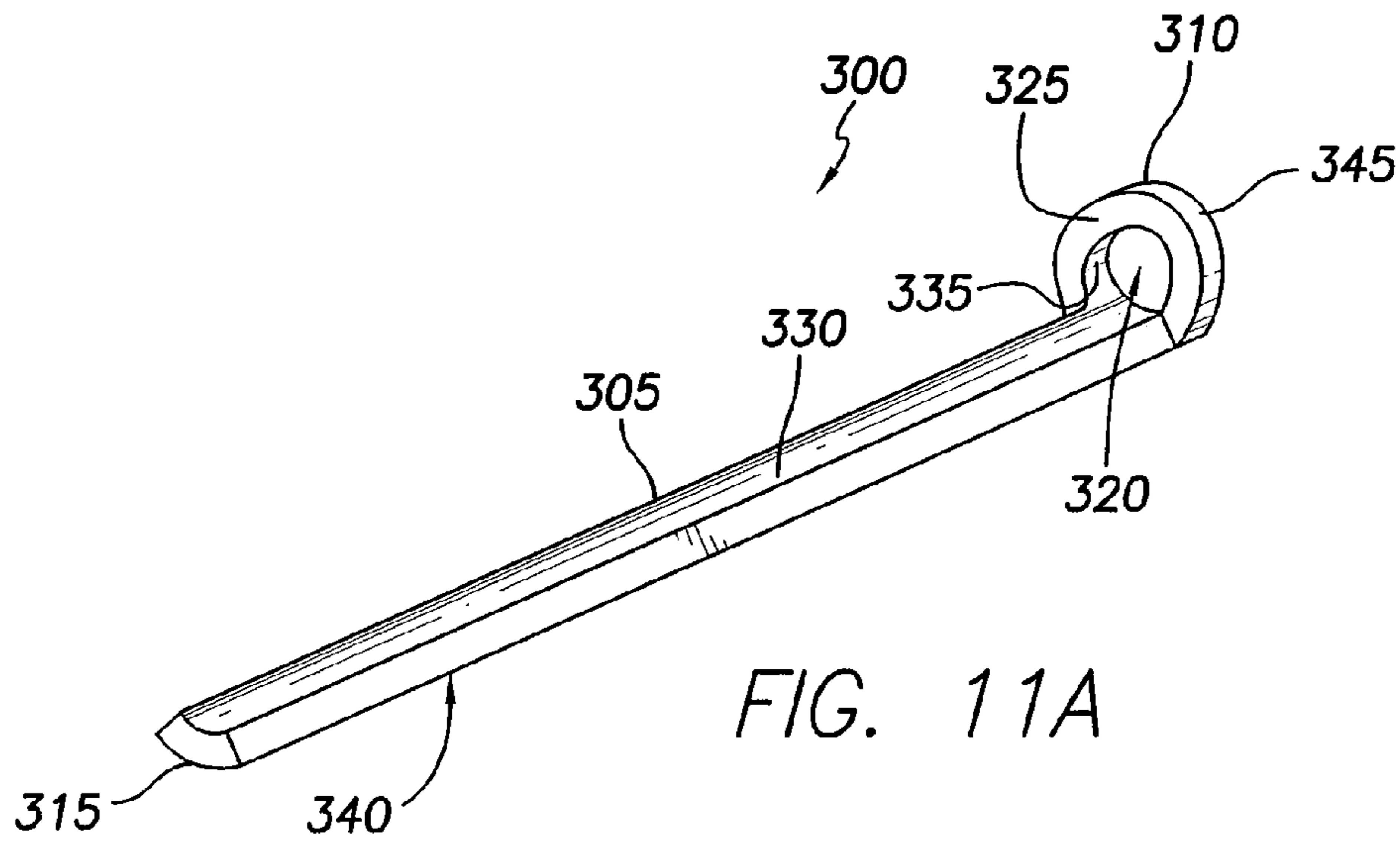


FIG. 11



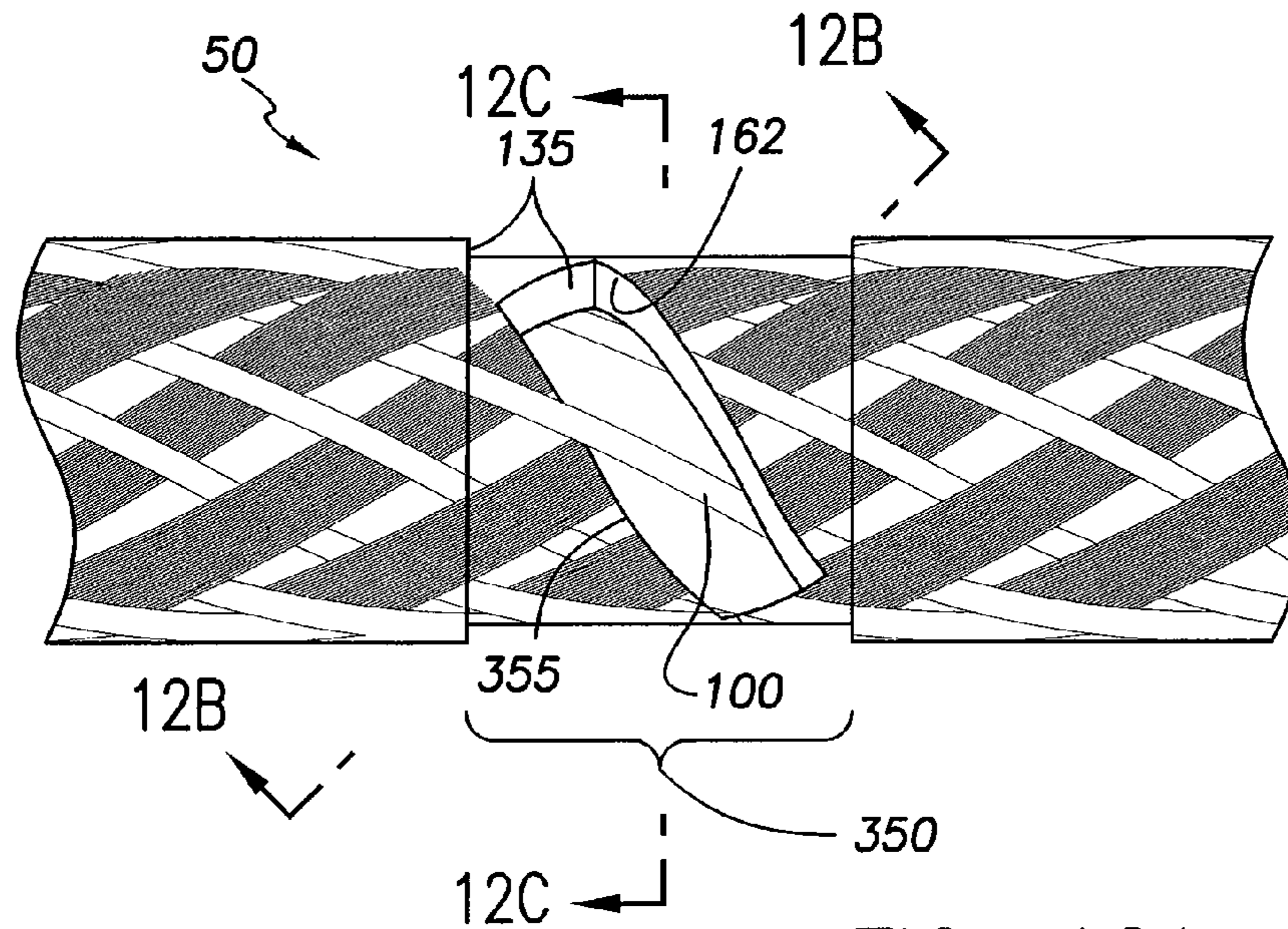


FIG. 12A

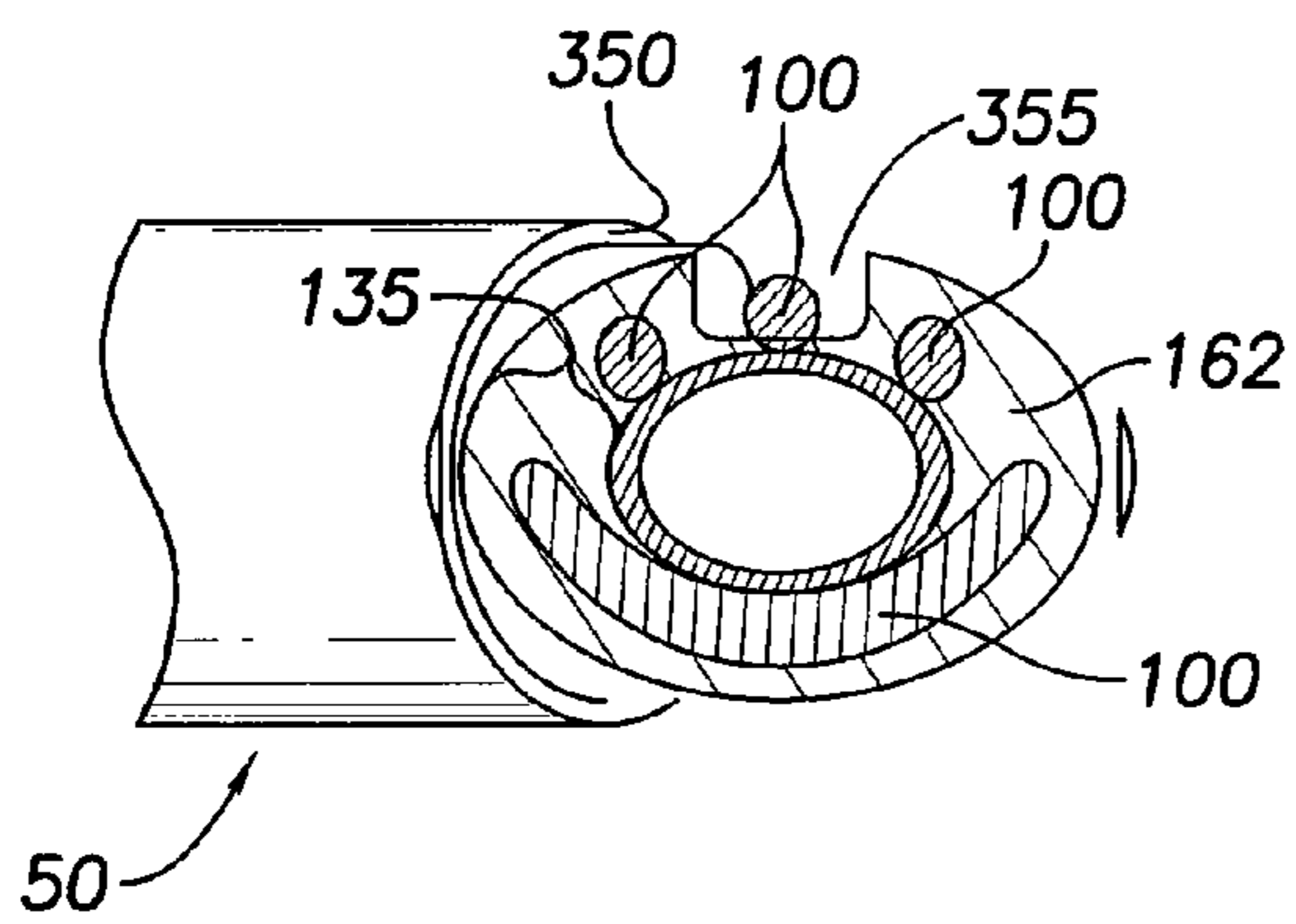


FIG. 12B

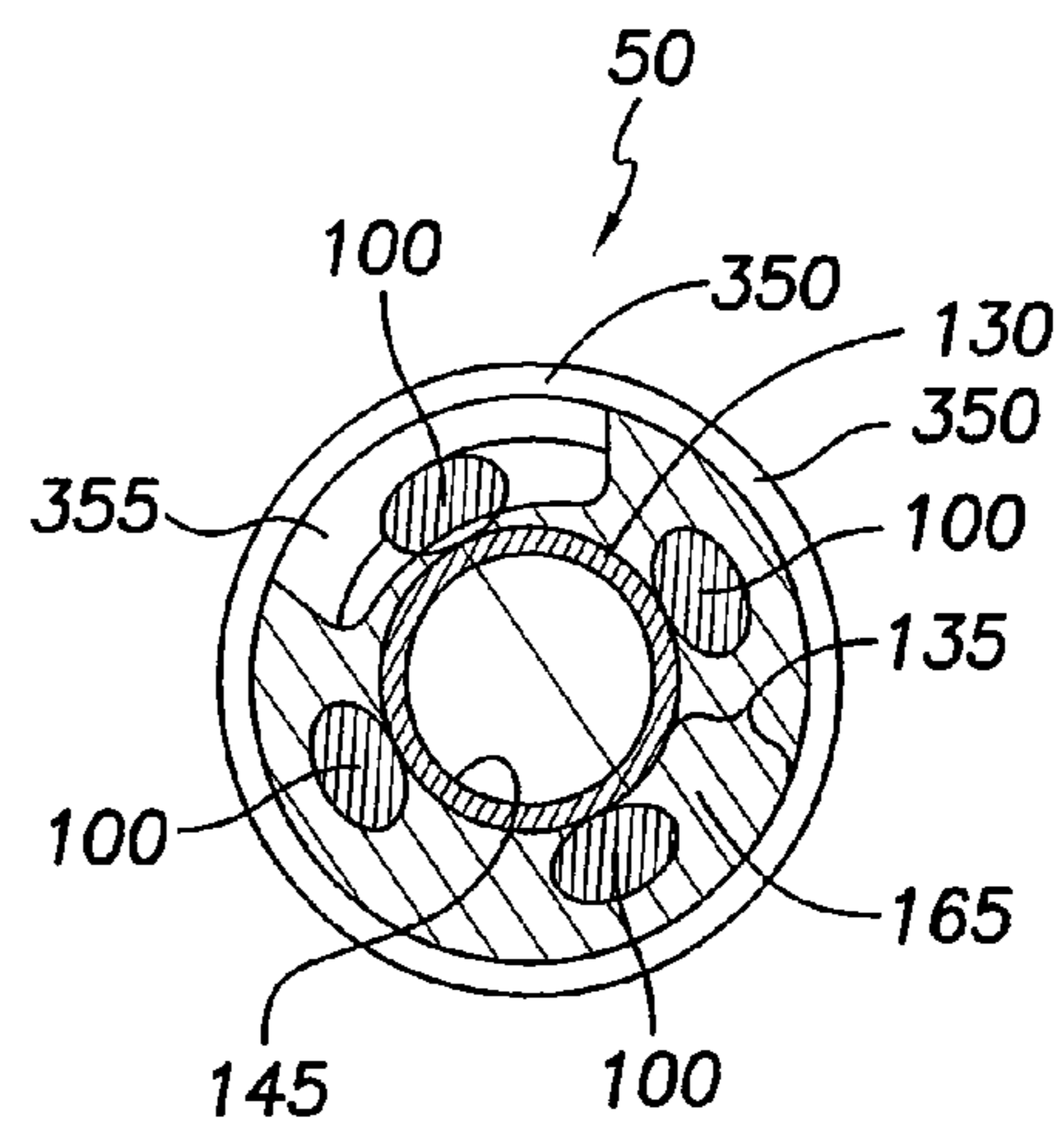


FIG. 12C

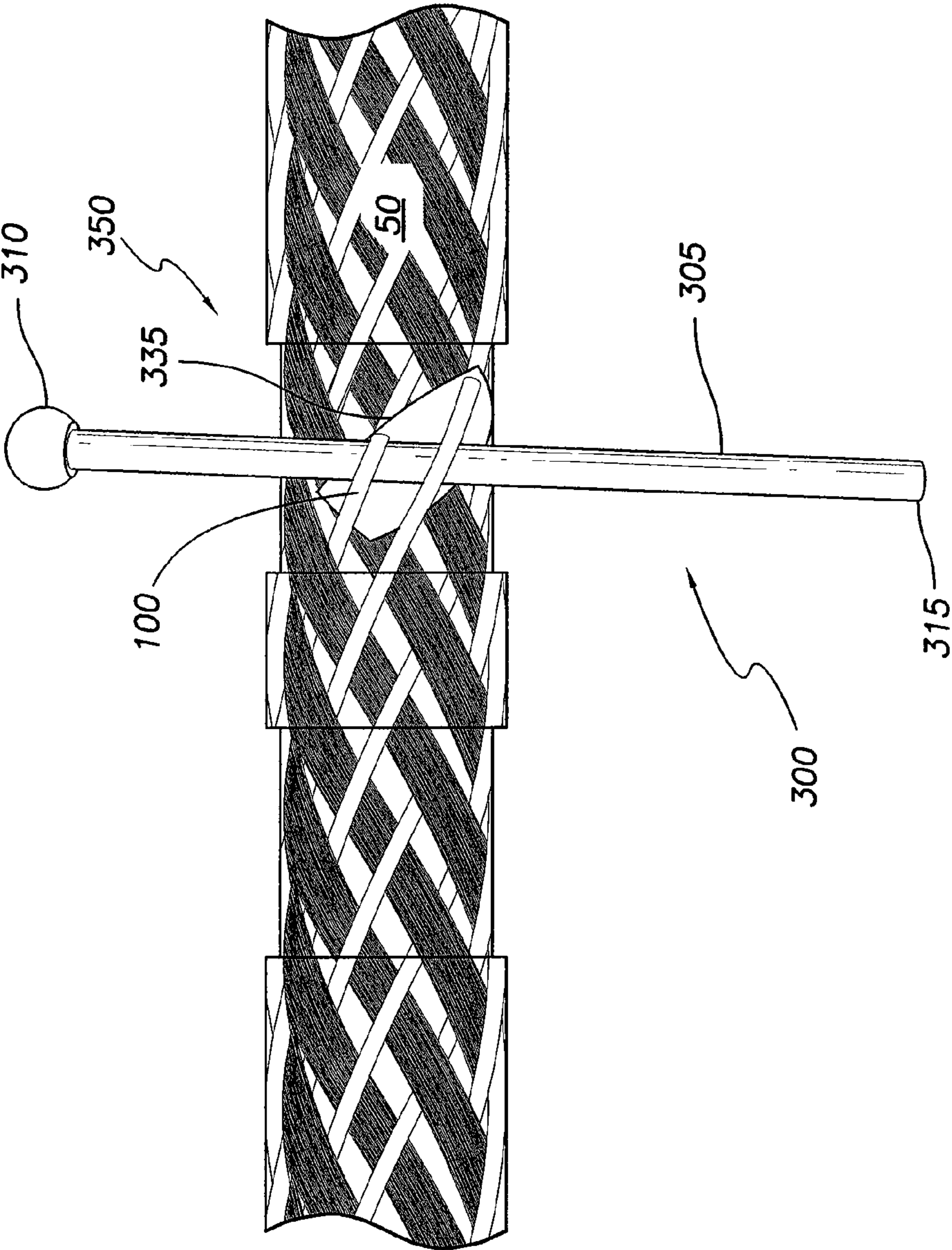


FIG. 13A

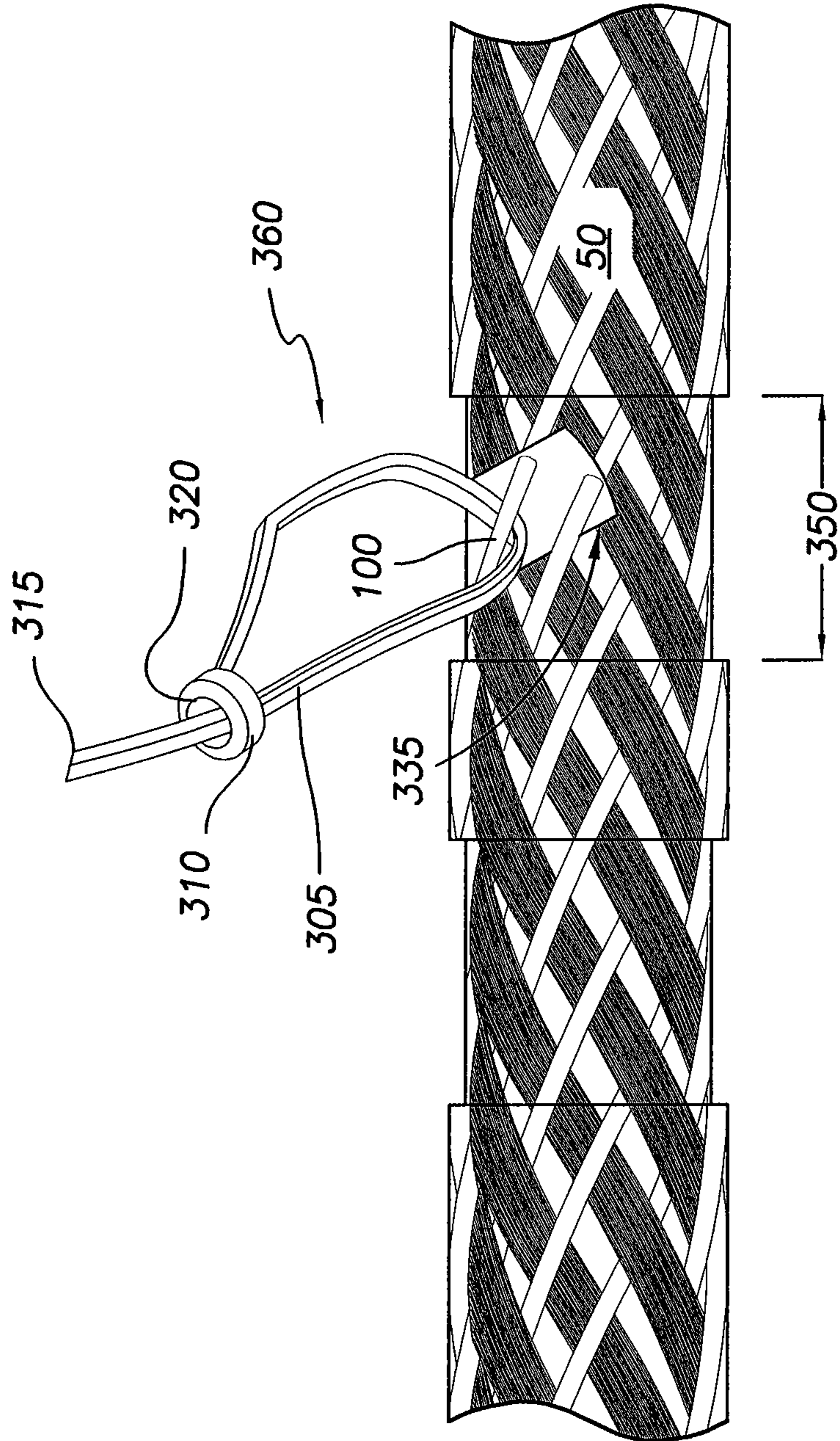


FIG. 13B

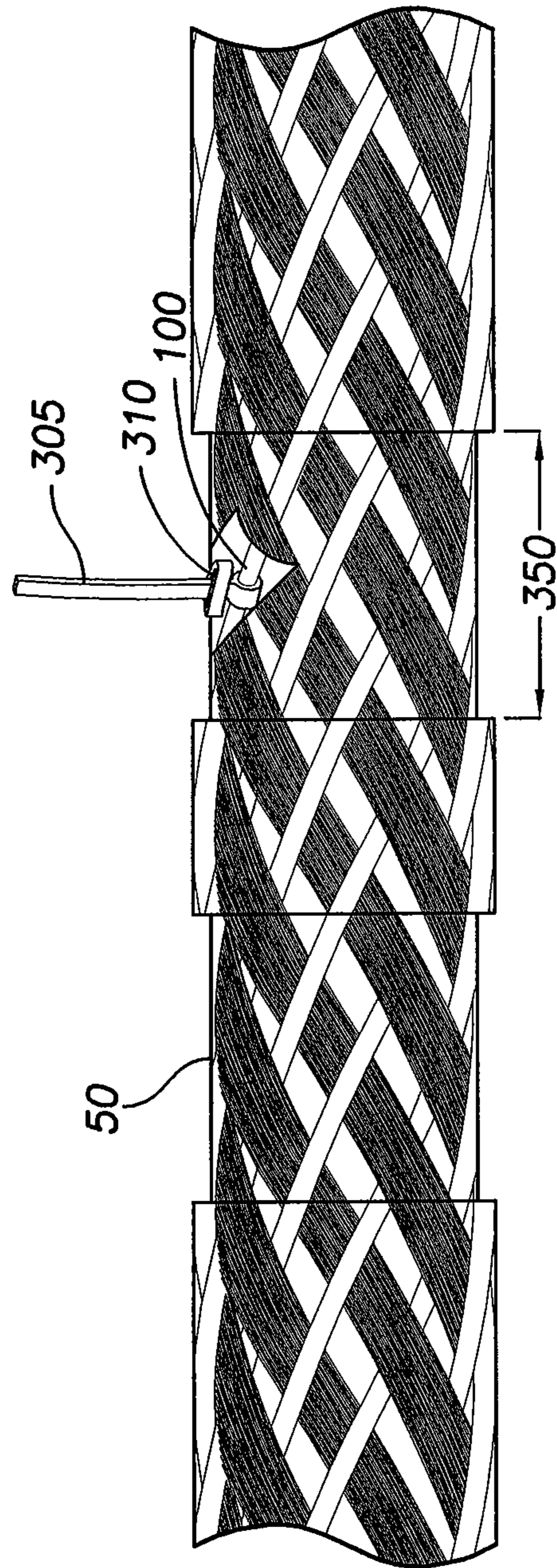


FIG. 13C



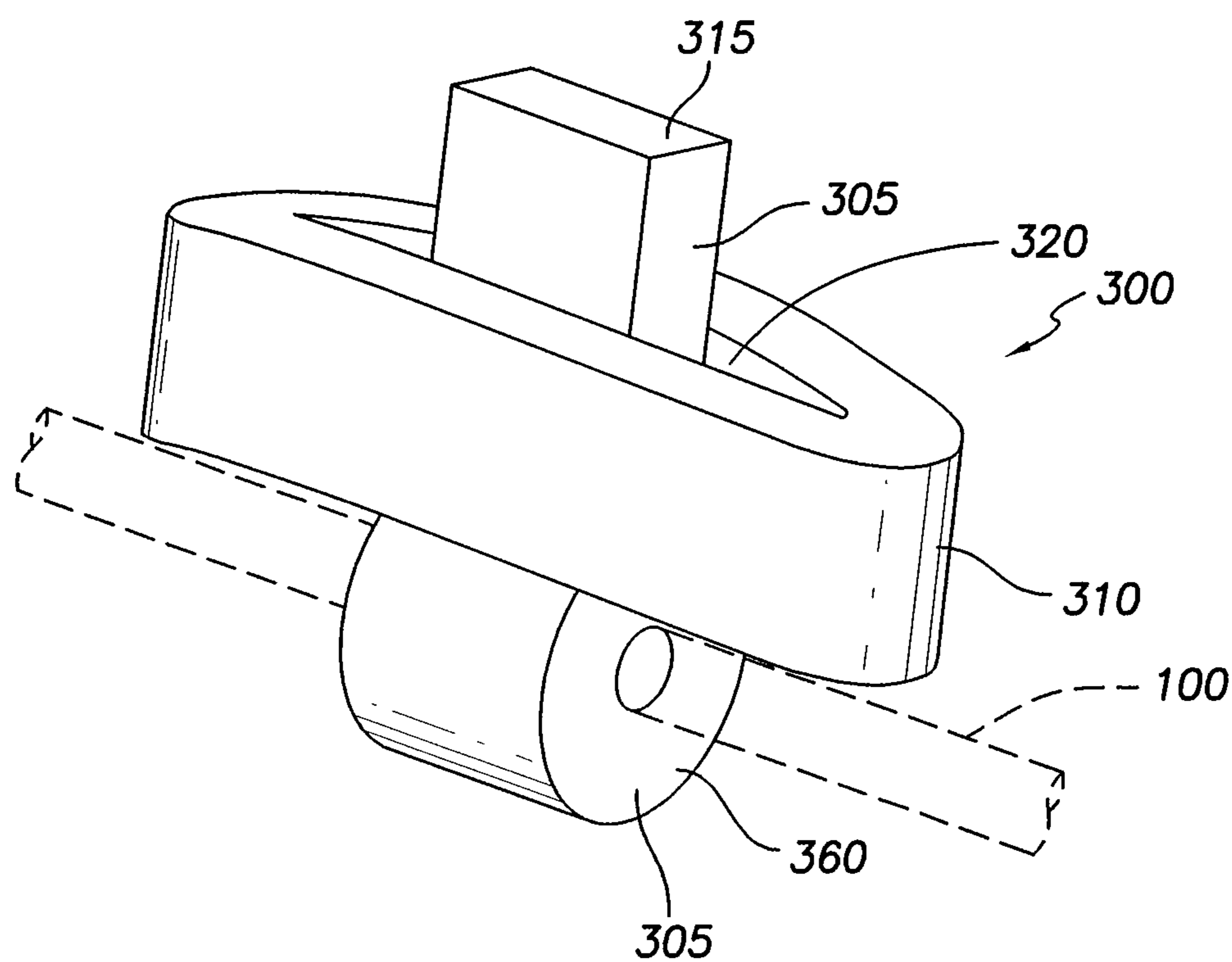
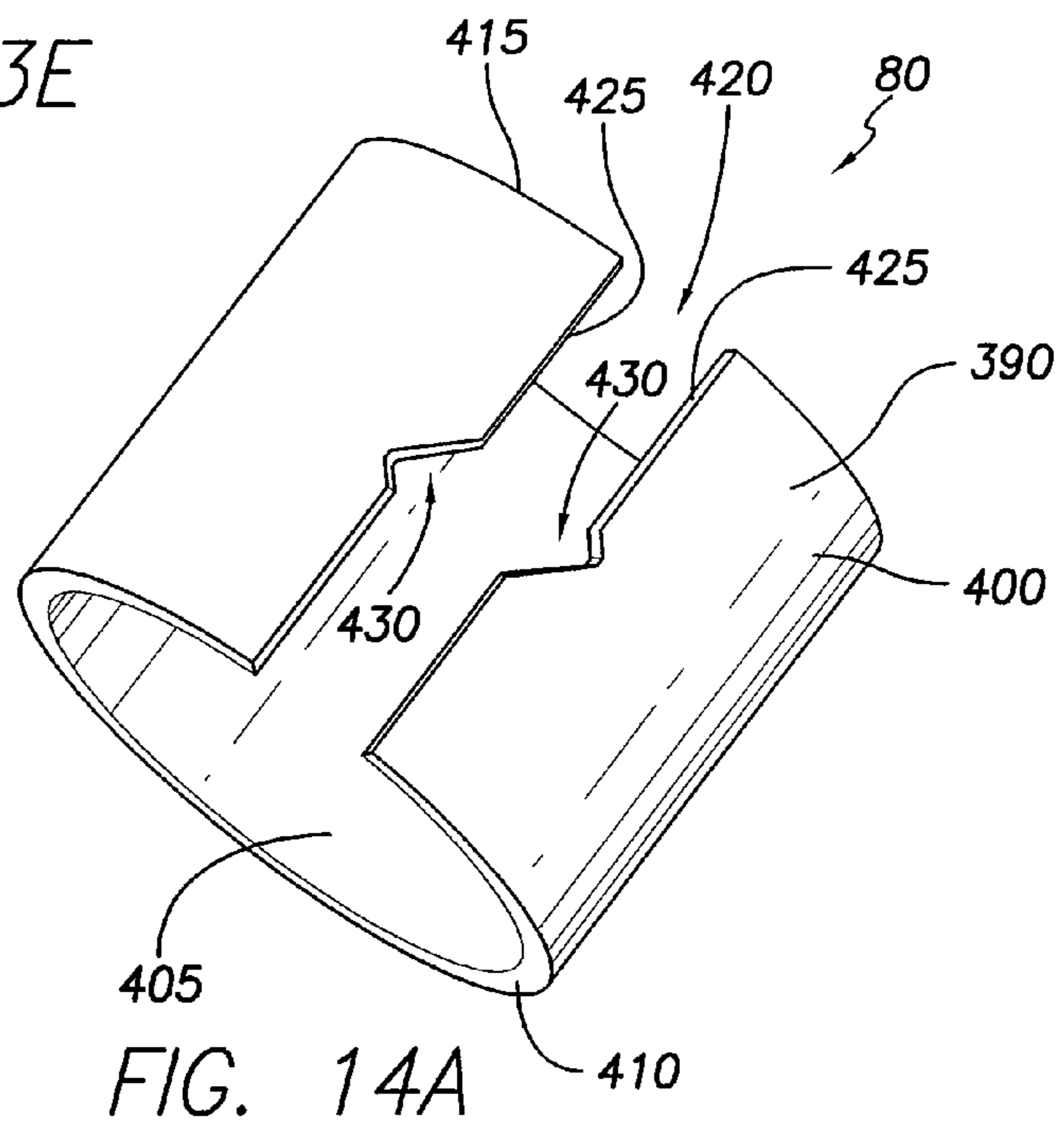
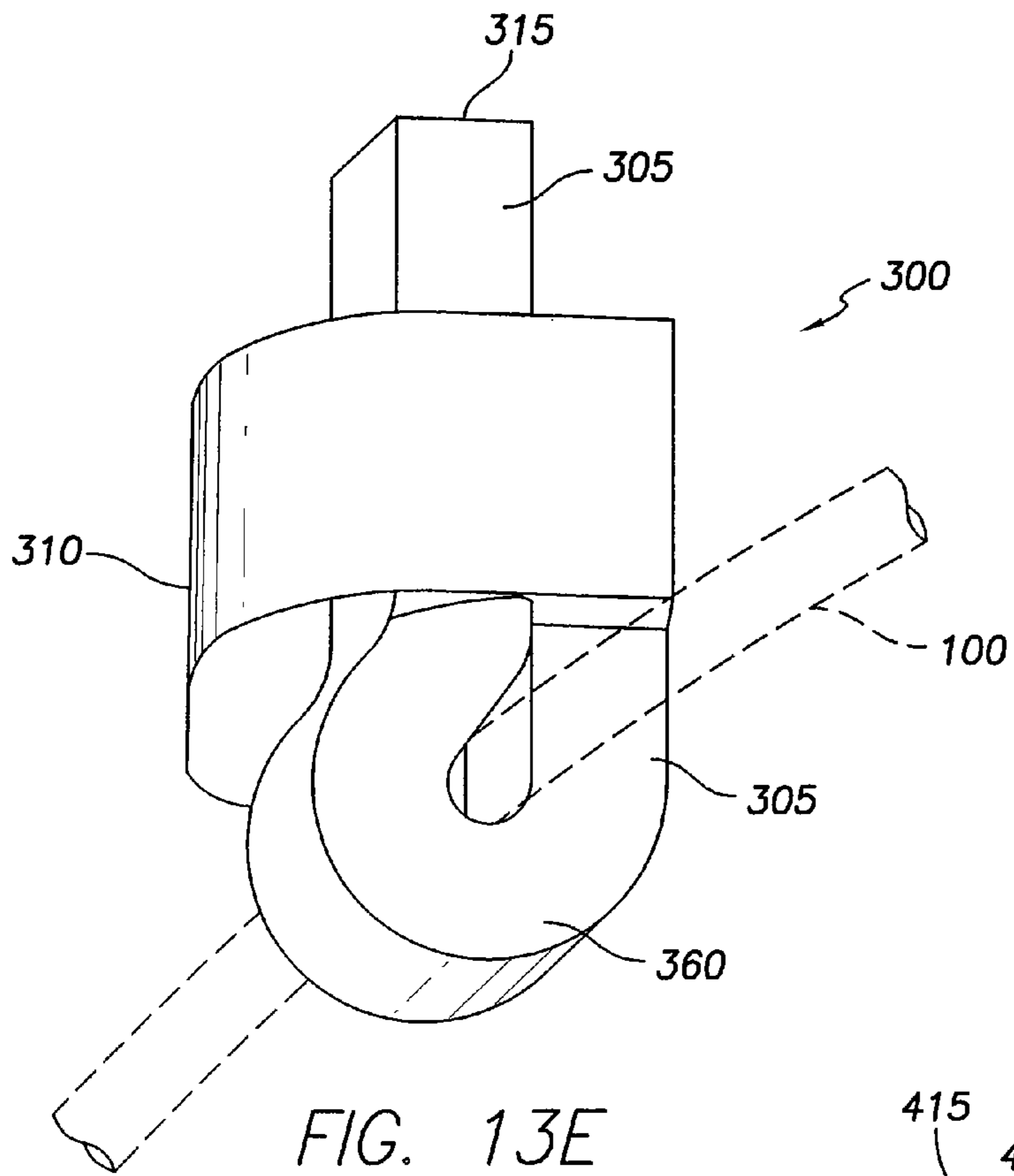


FIG. 13D



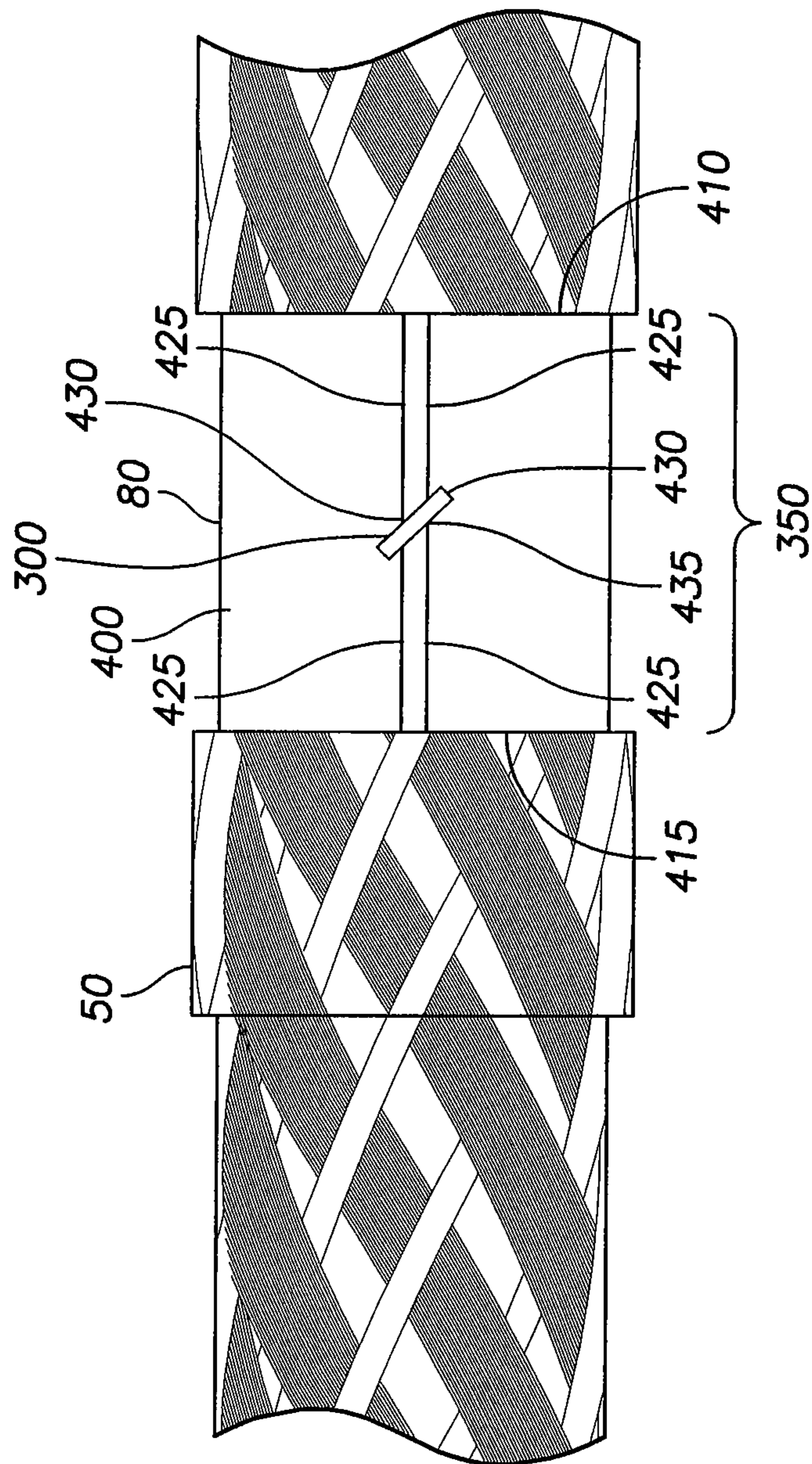


FIG. 14B

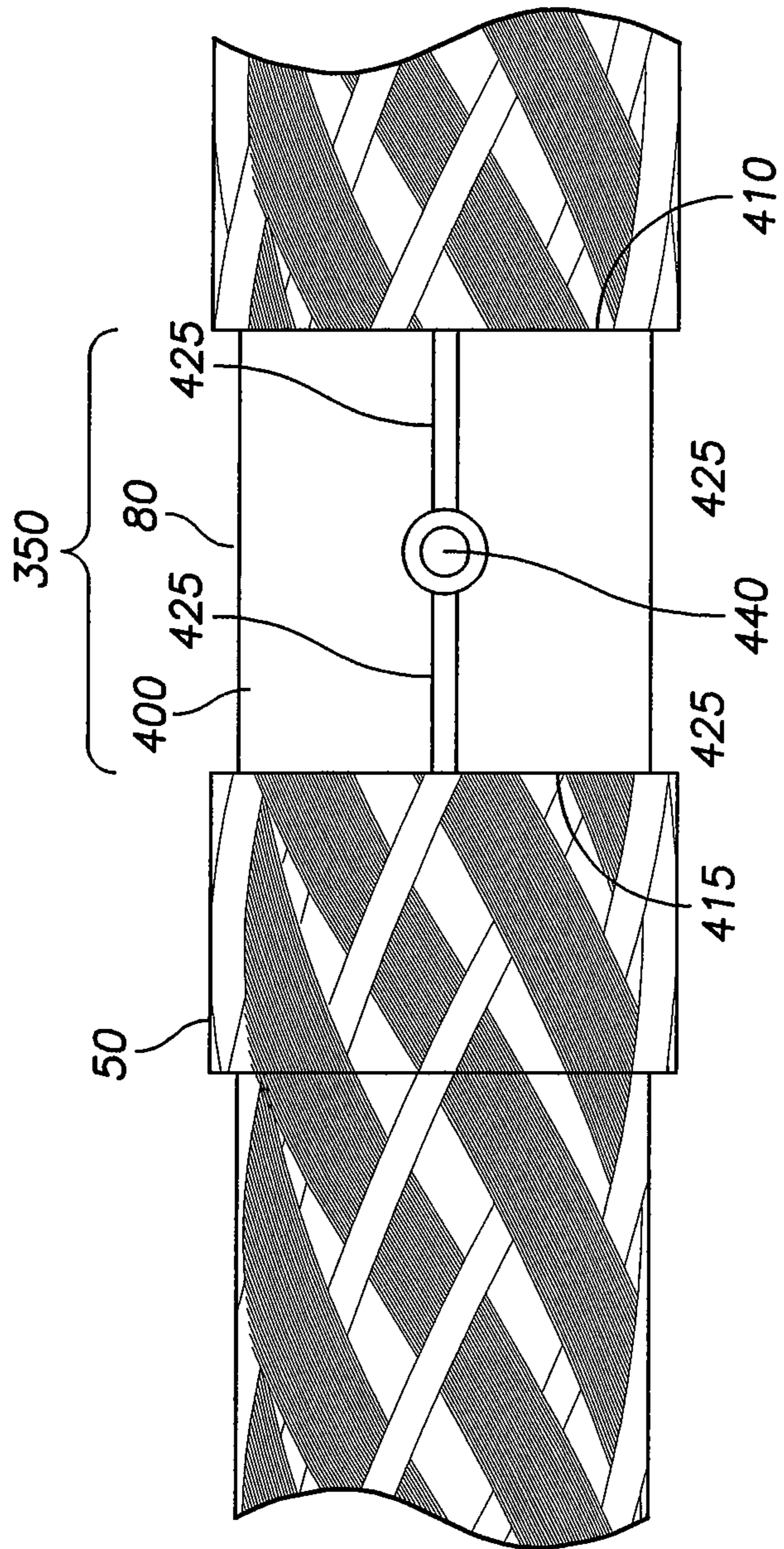


FIG. 14C

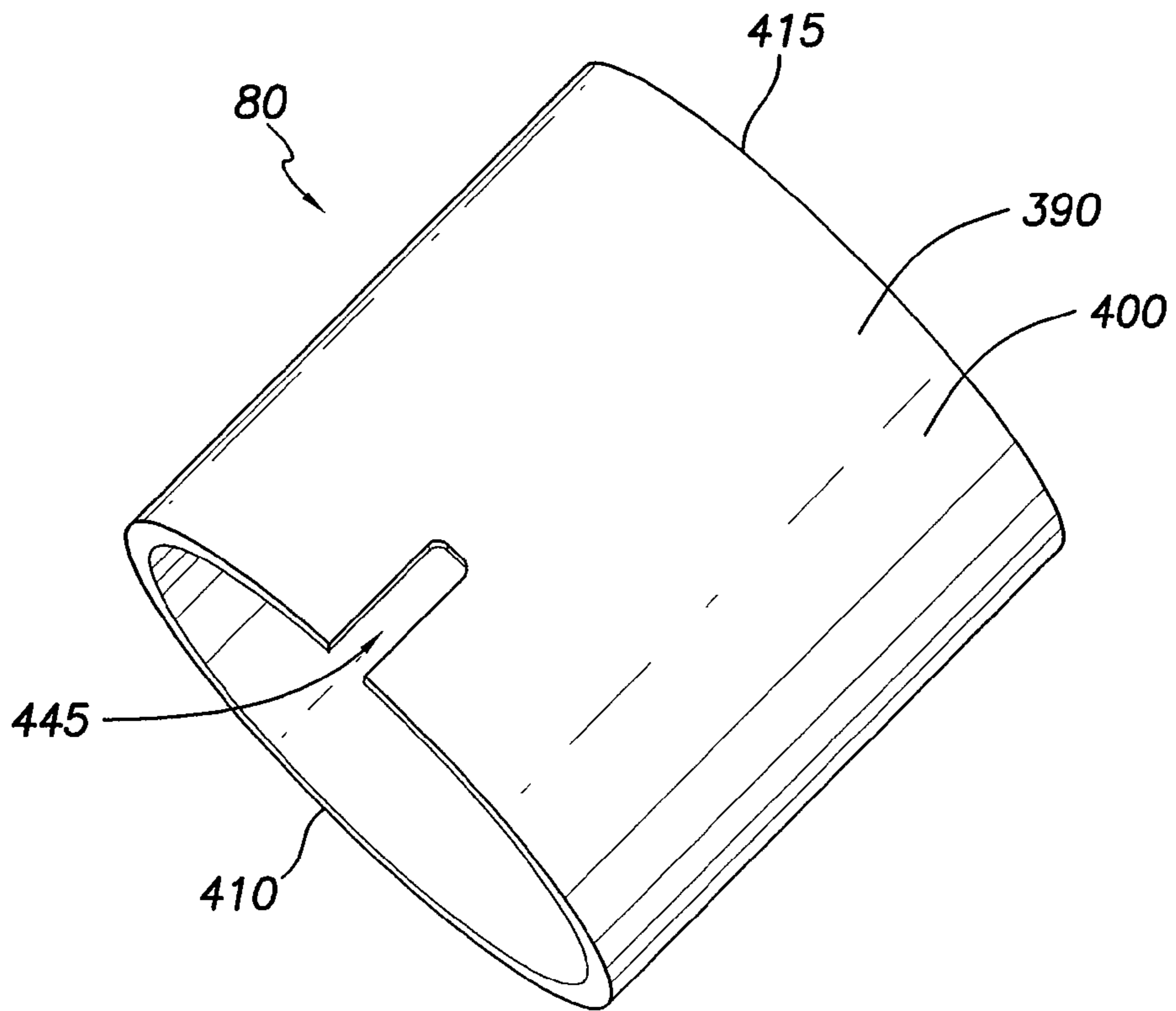


FIG. 15A

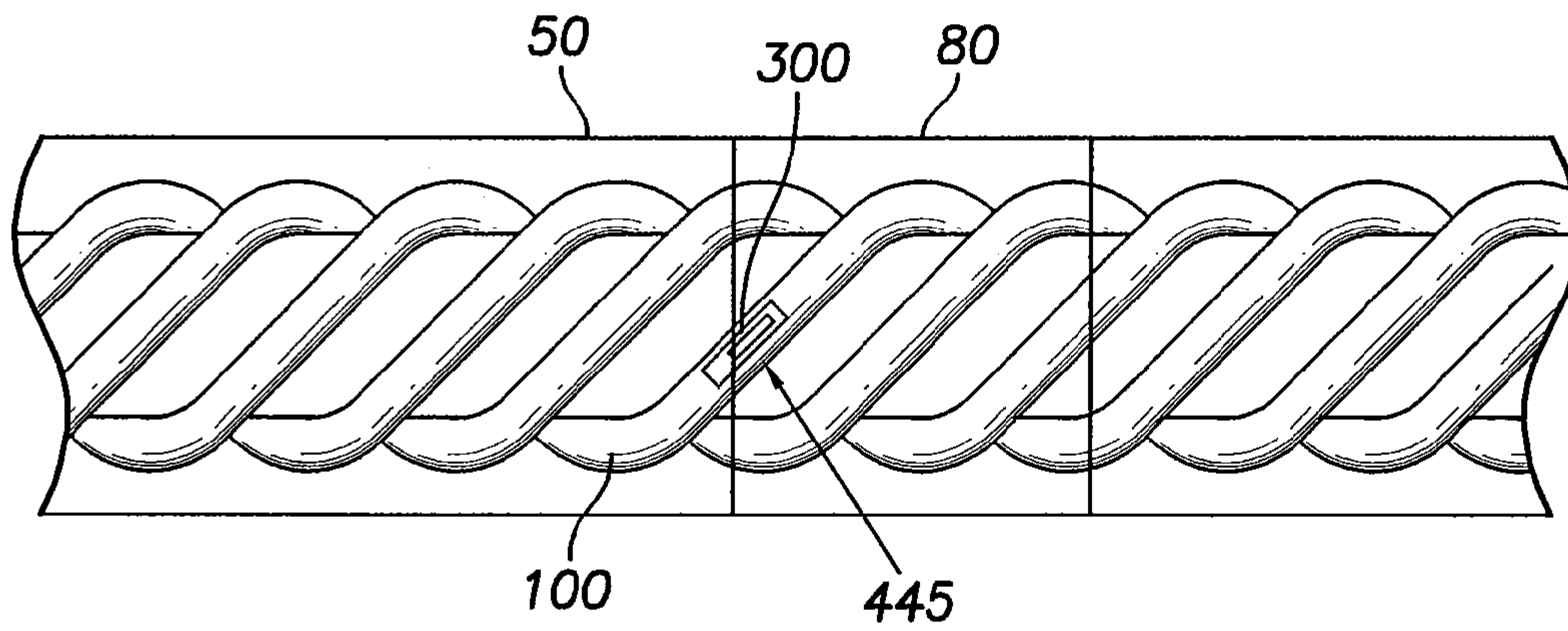
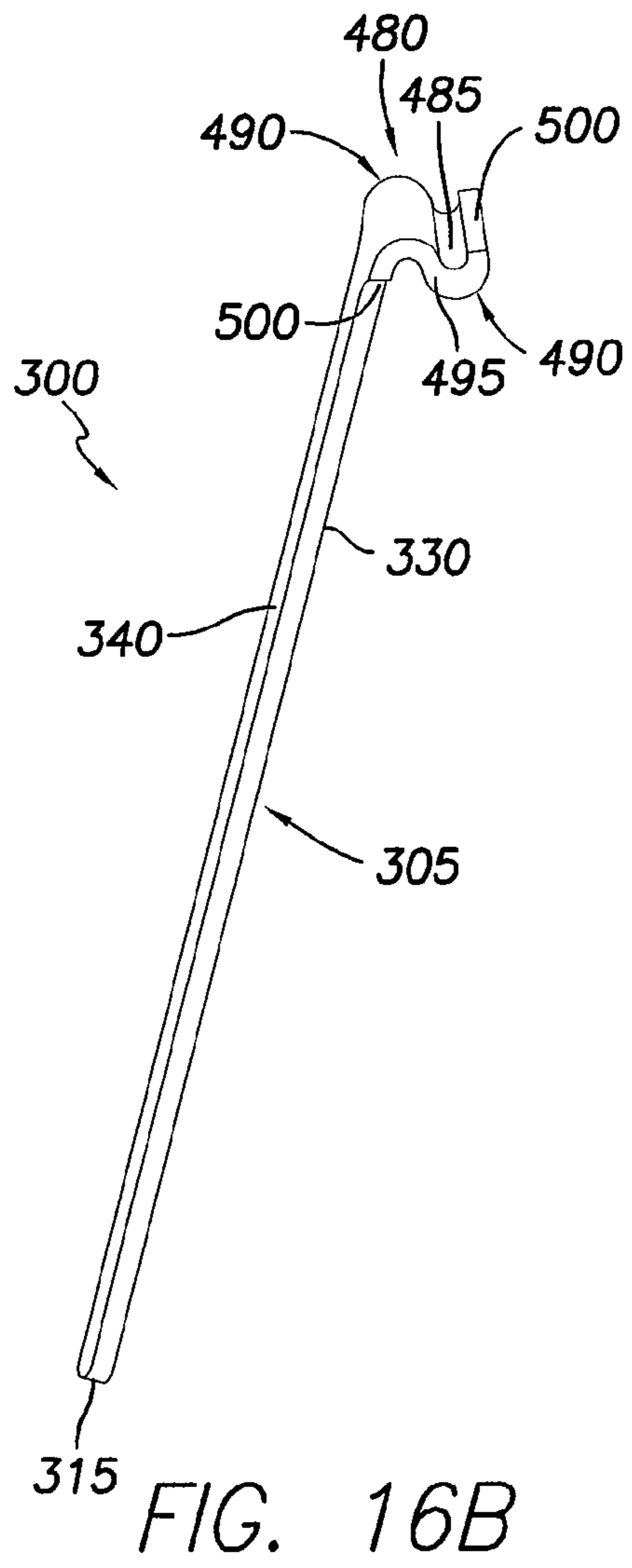
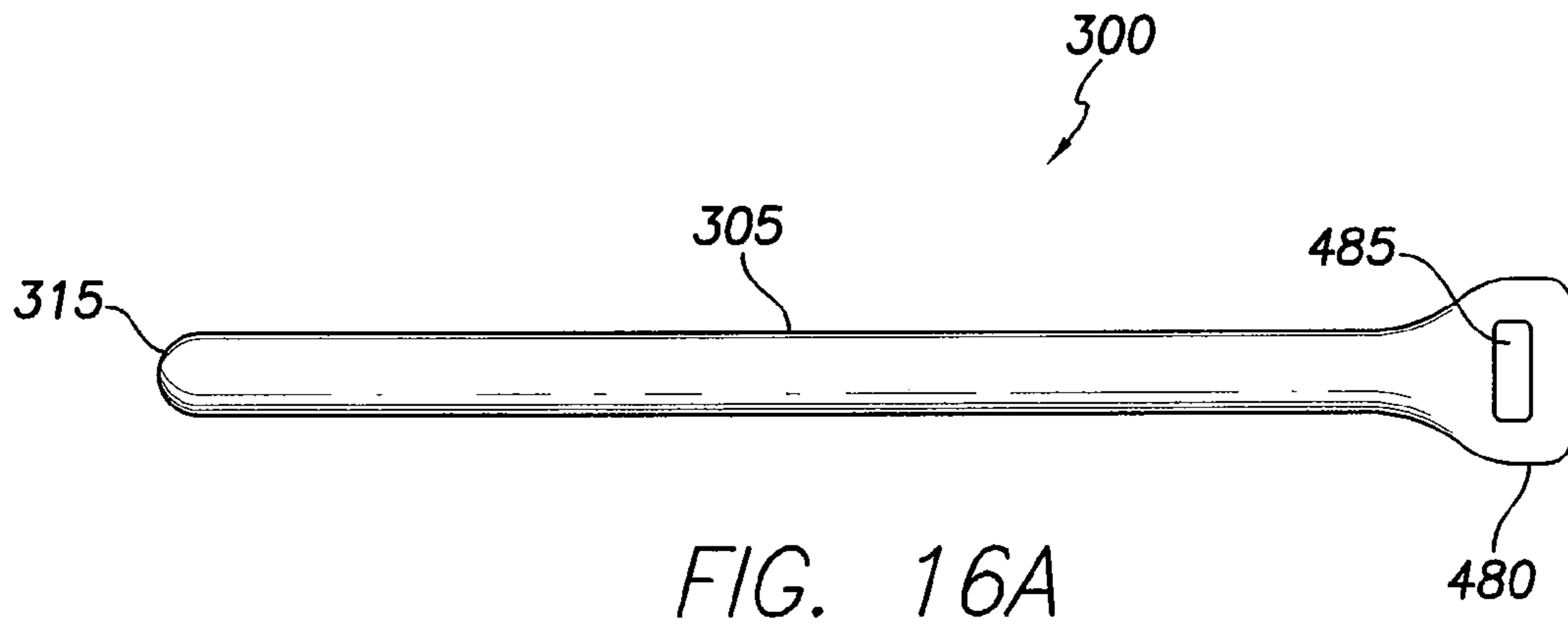


FIG. 15B



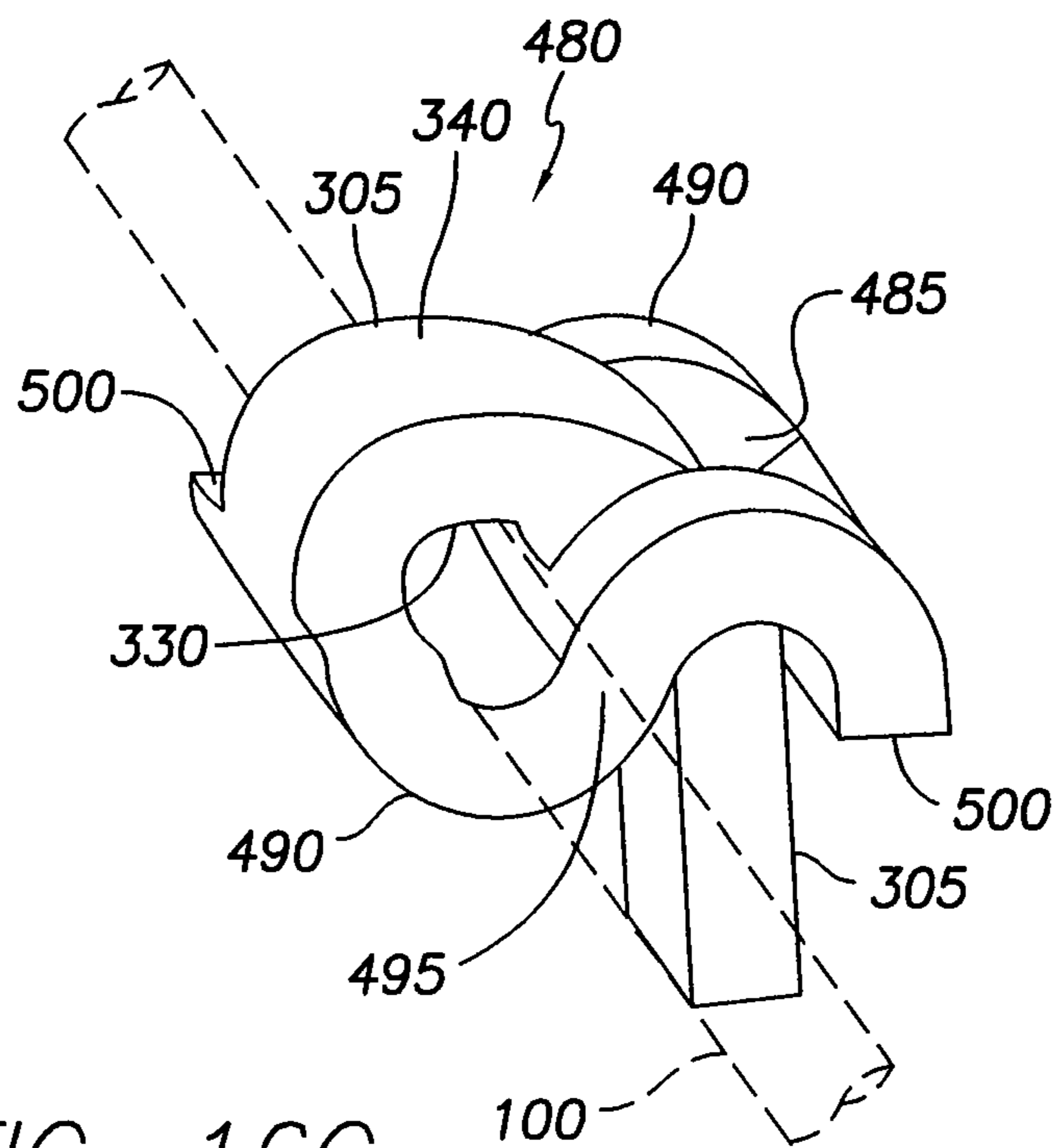


FIG. 16C

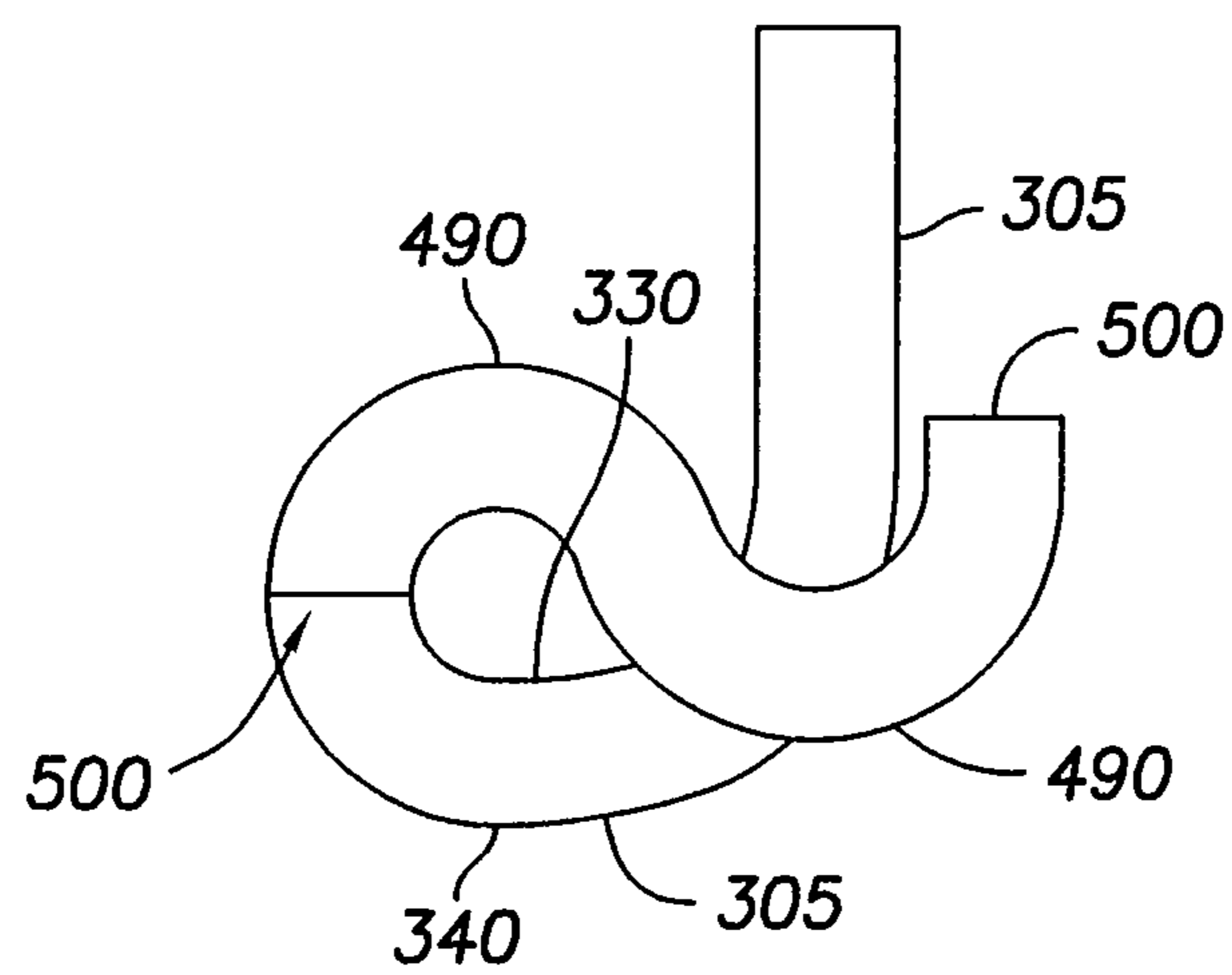


FIG. 16D

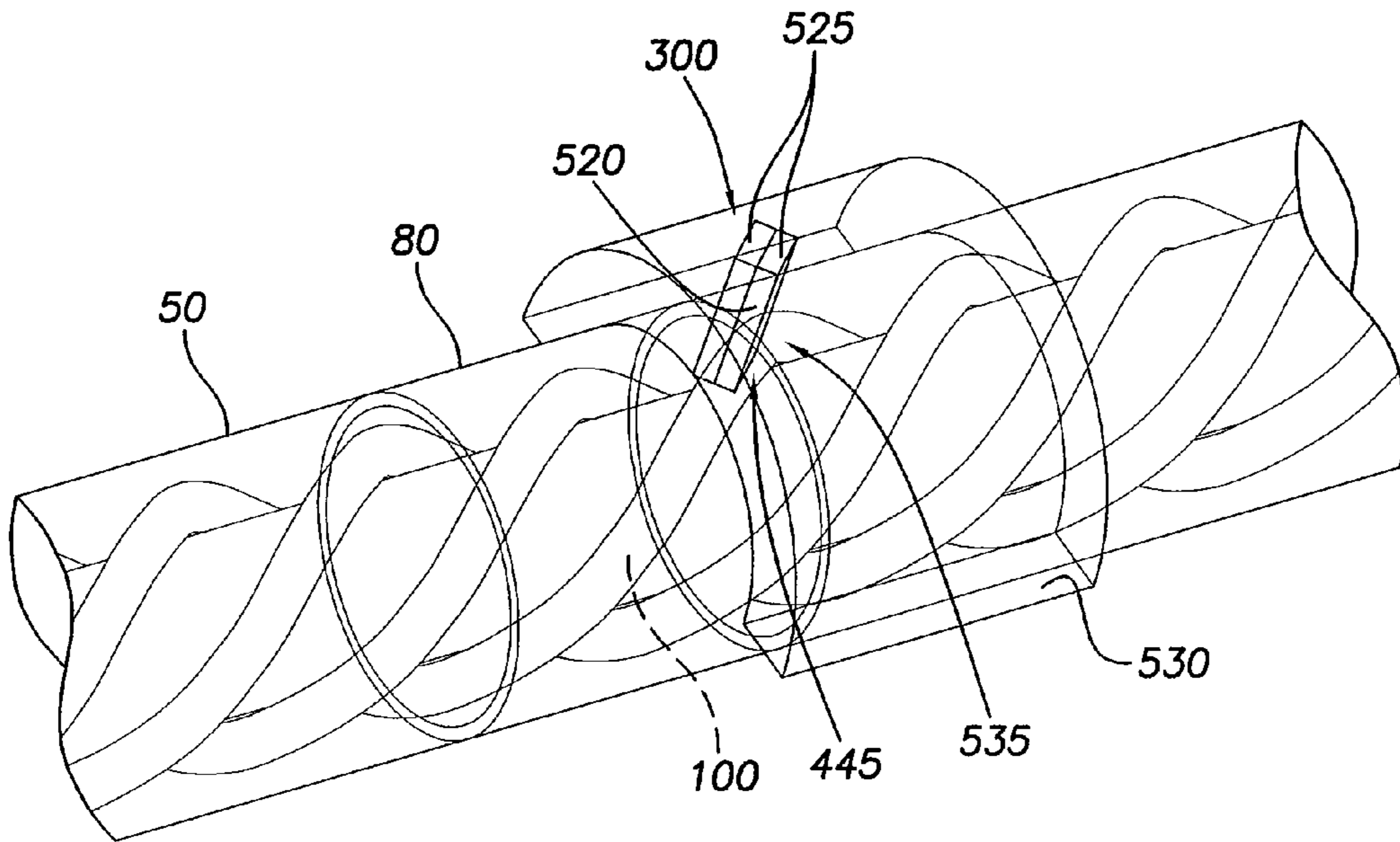


FIG. 17A

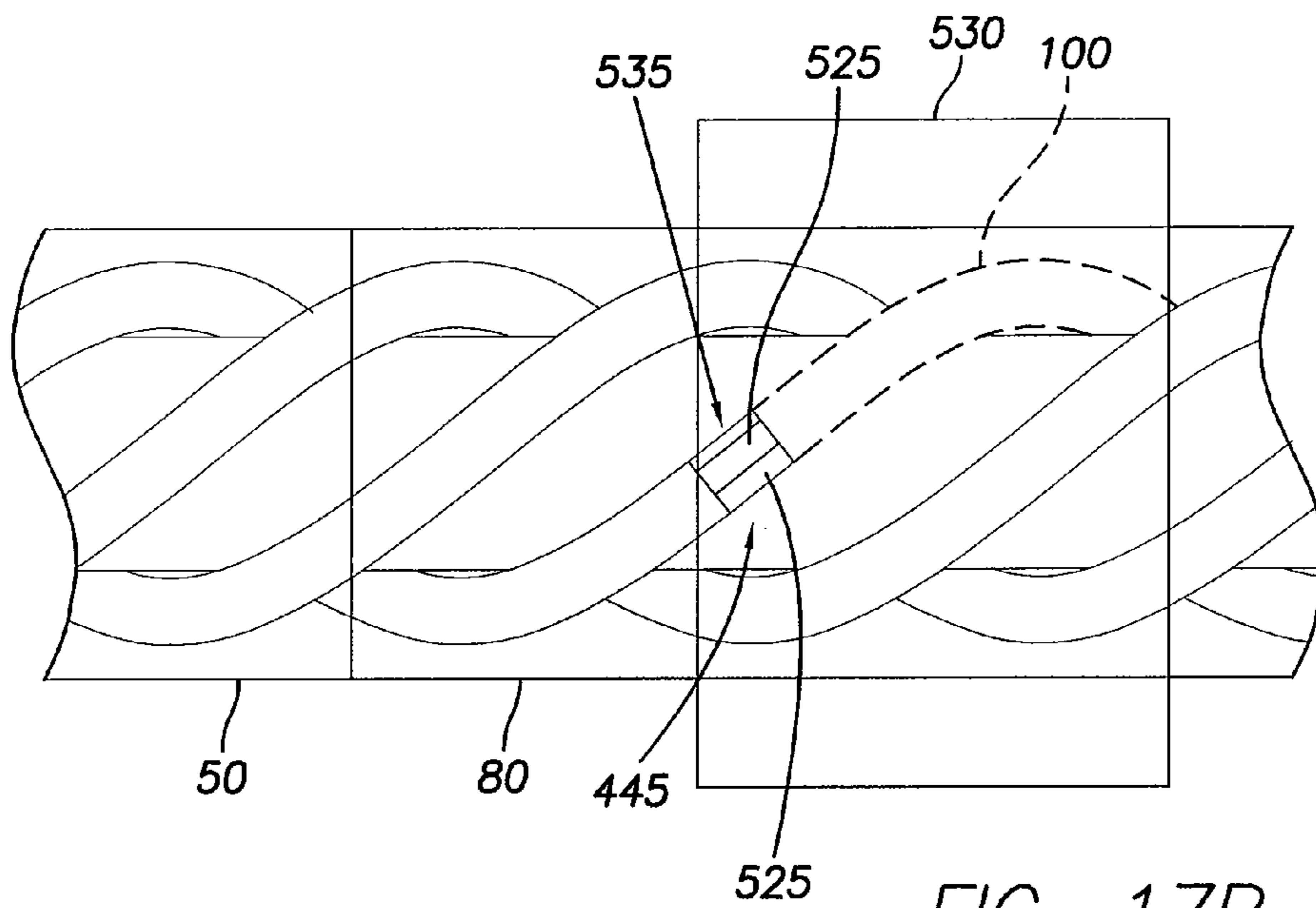


FIG. 17B



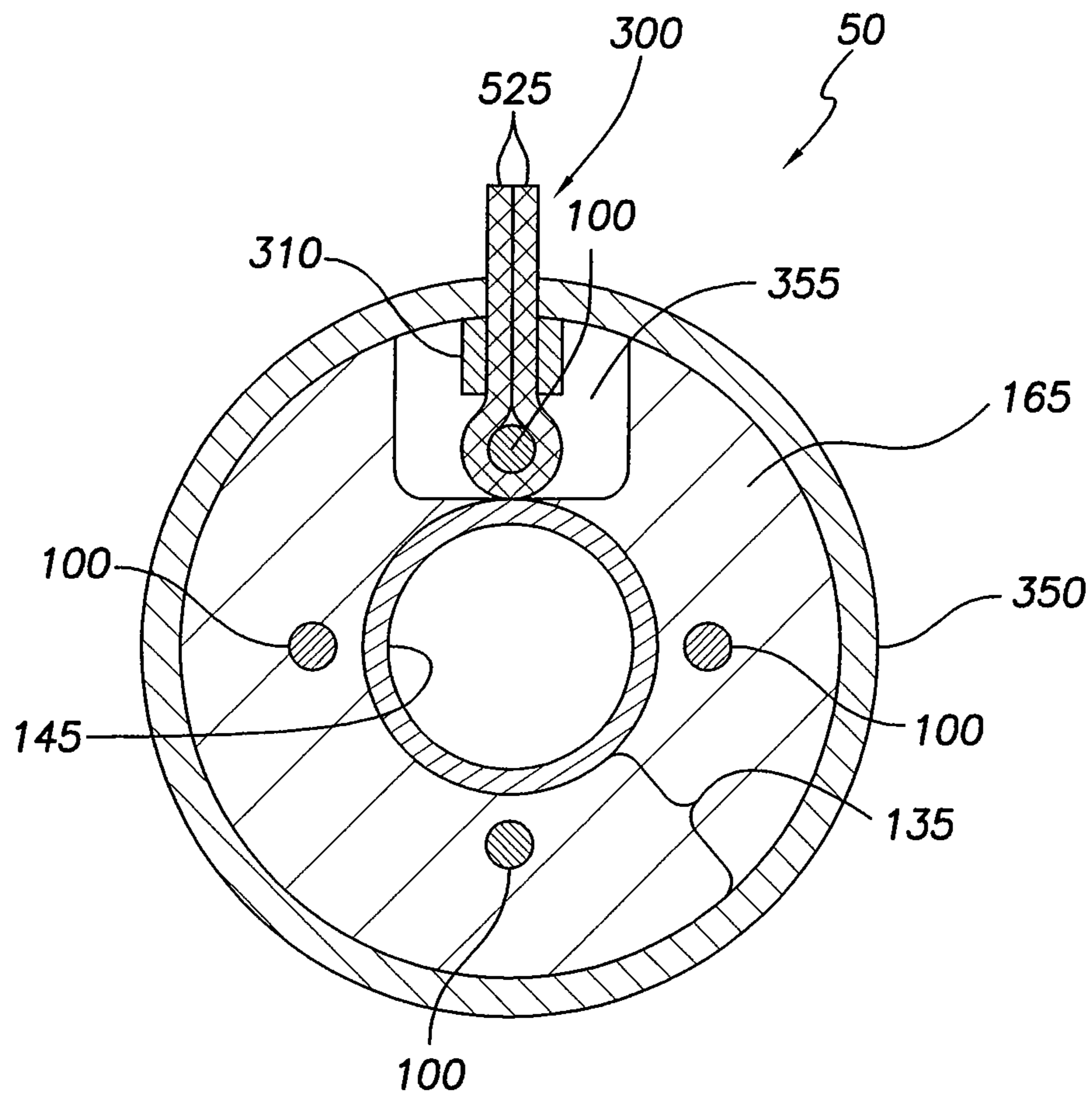


FIG. 17C

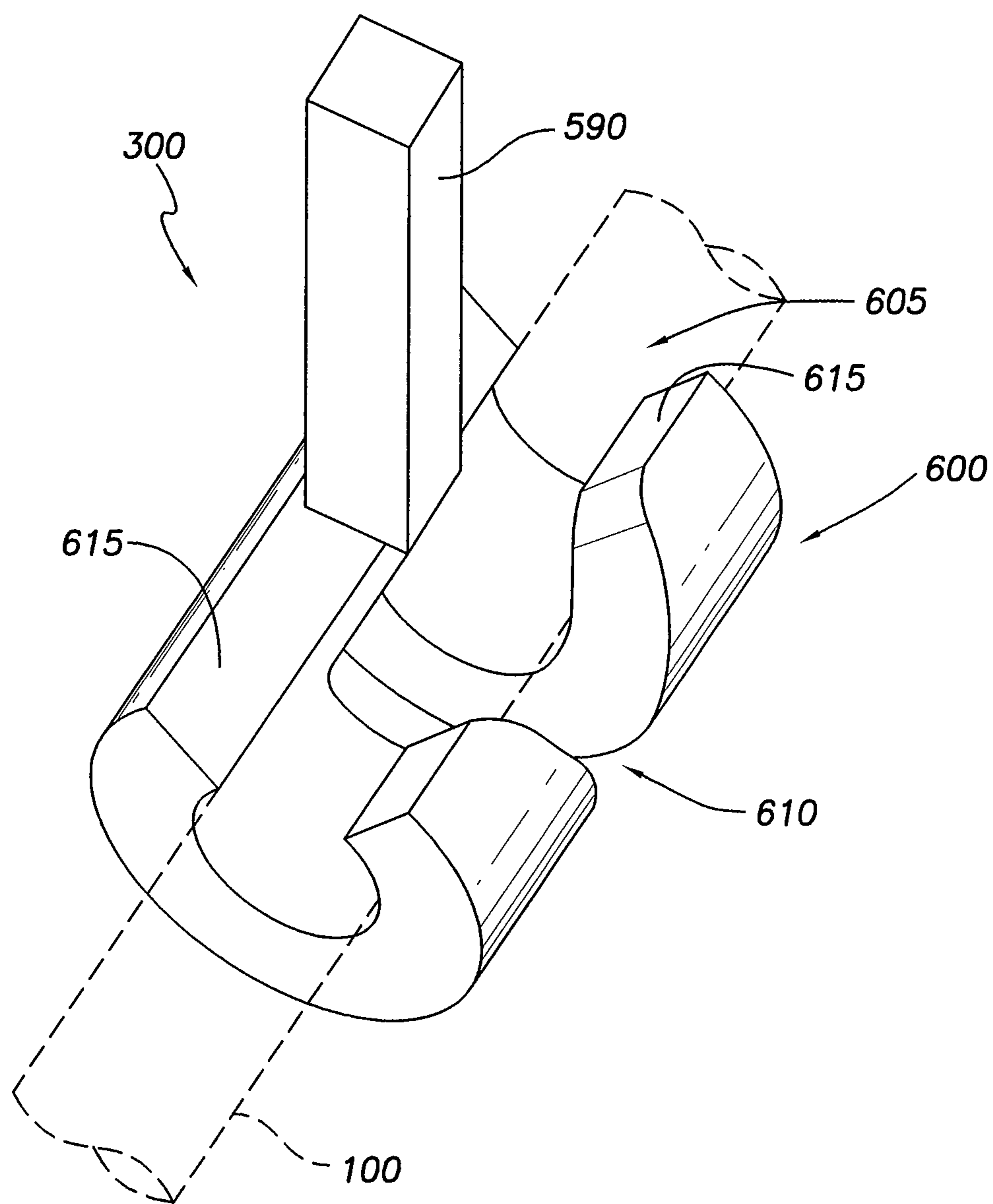


FIG. 18A

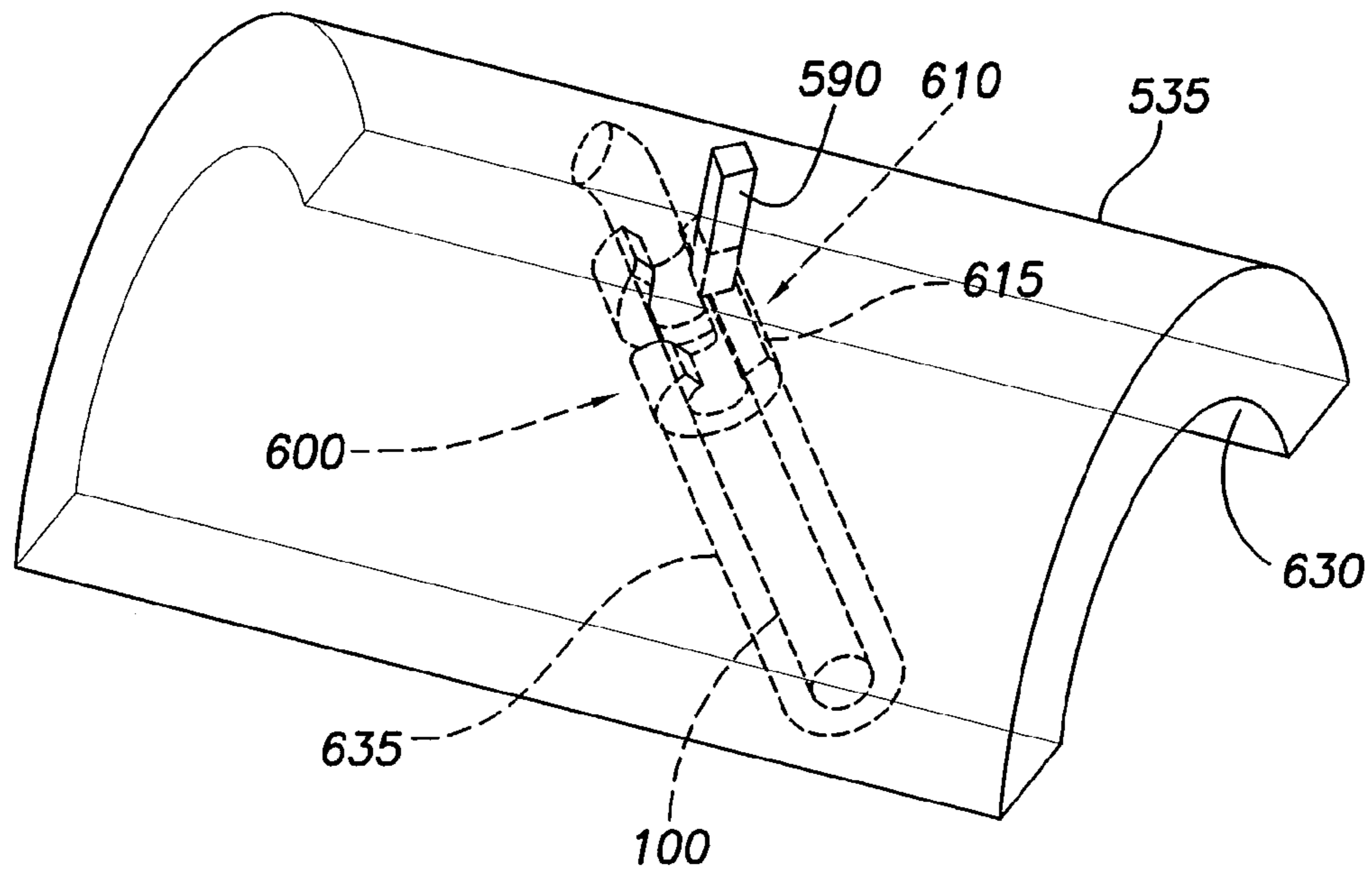


FIG. 18B

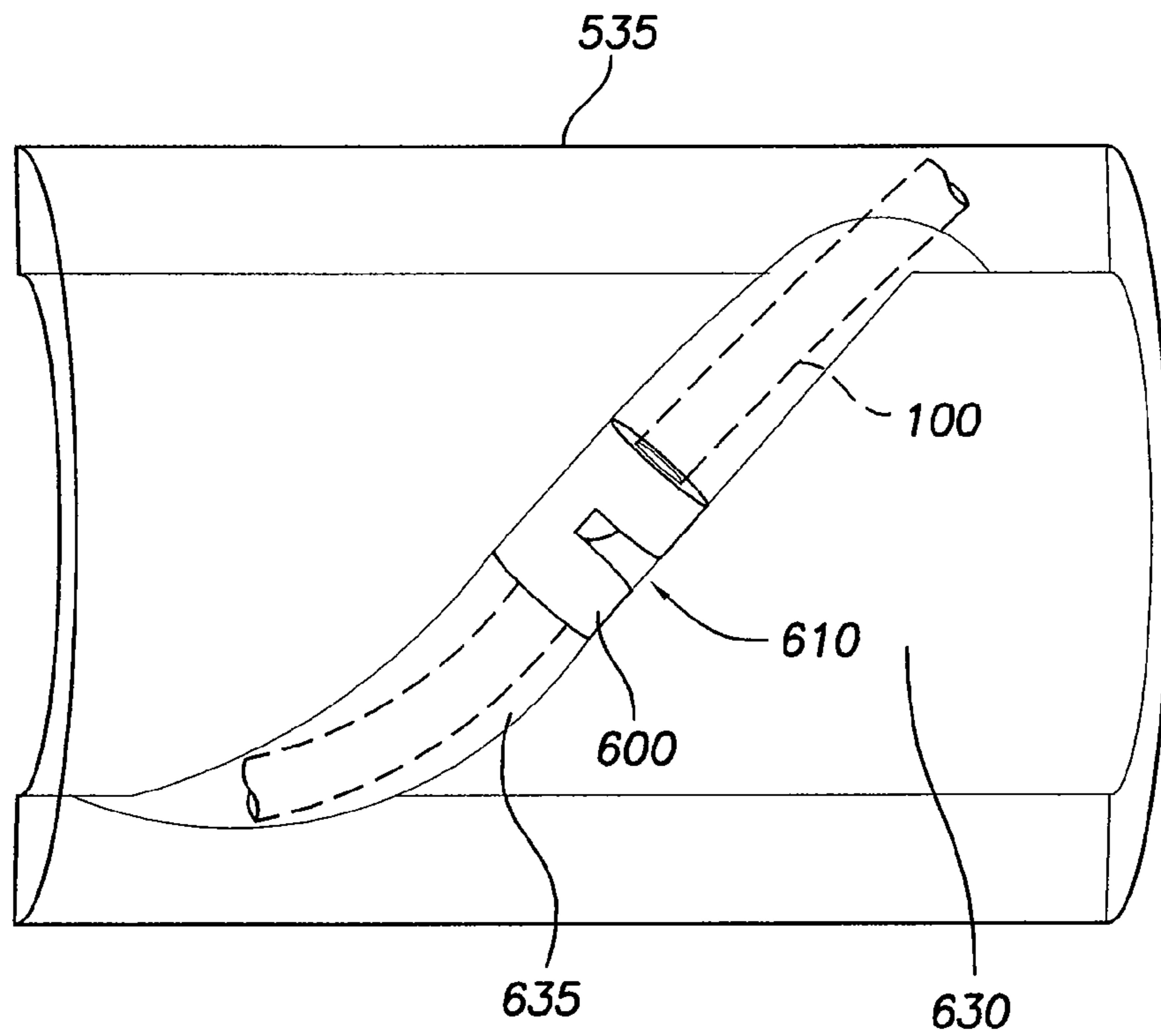


FIG. 18C

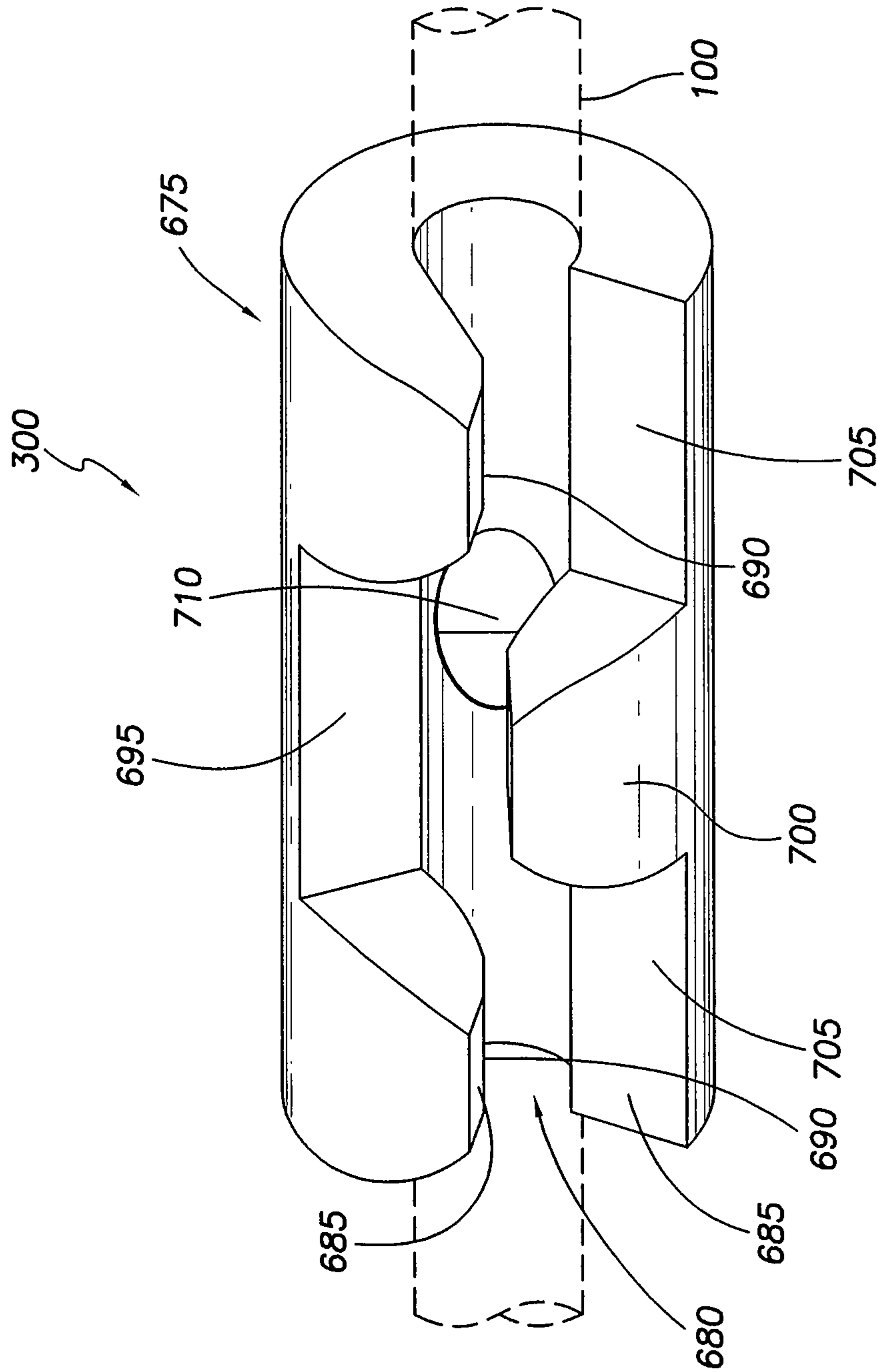
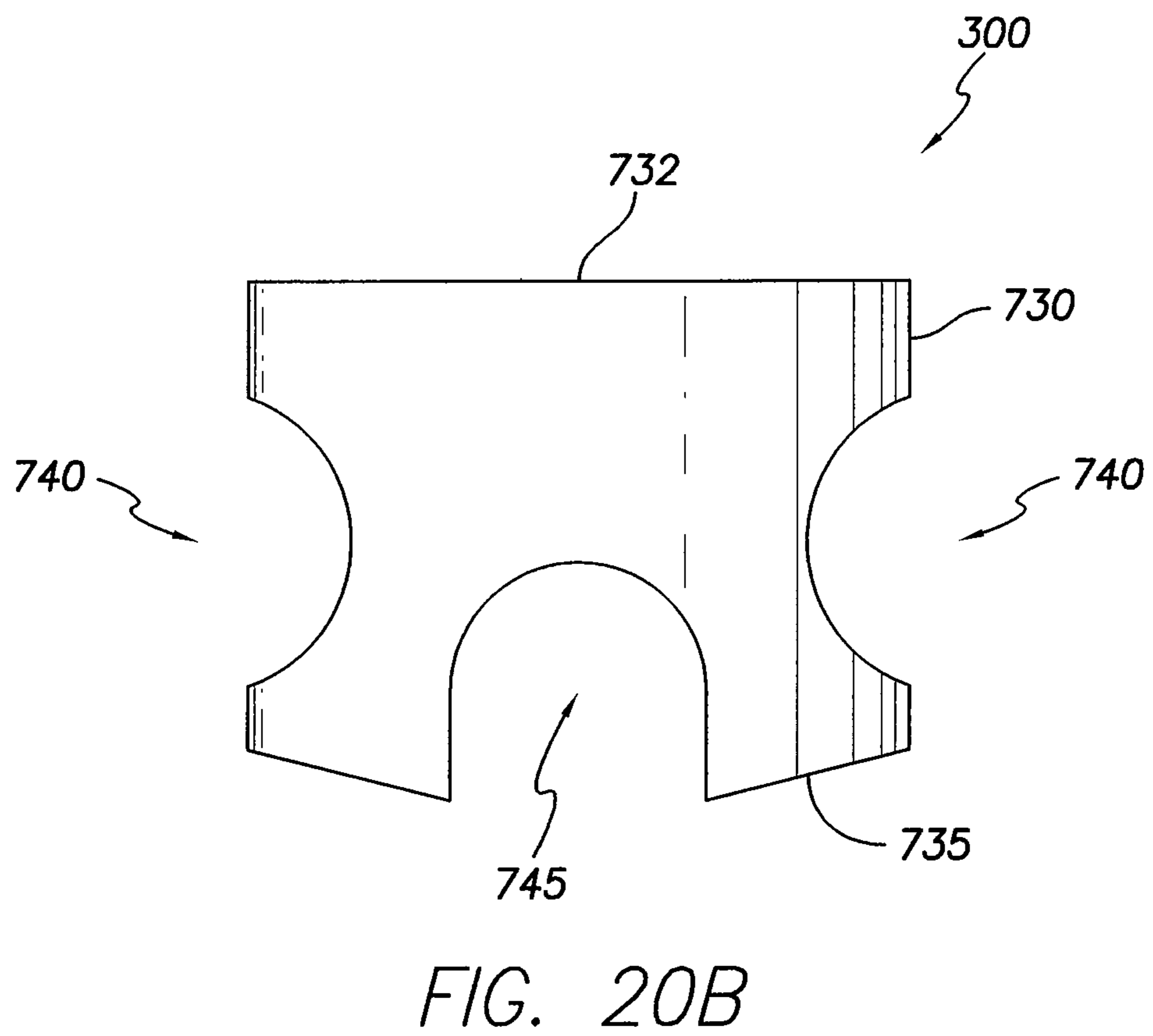
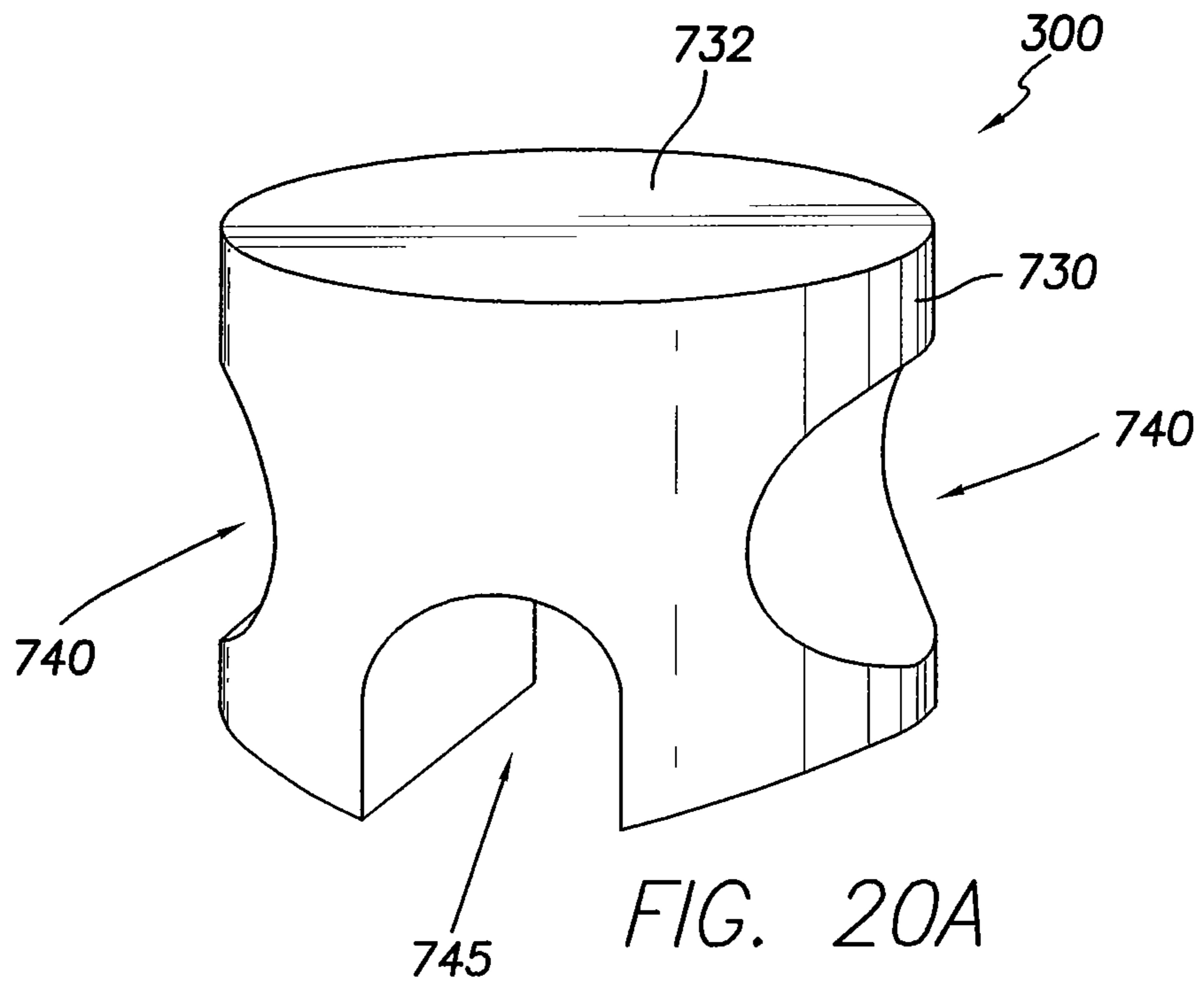


FIG. 19



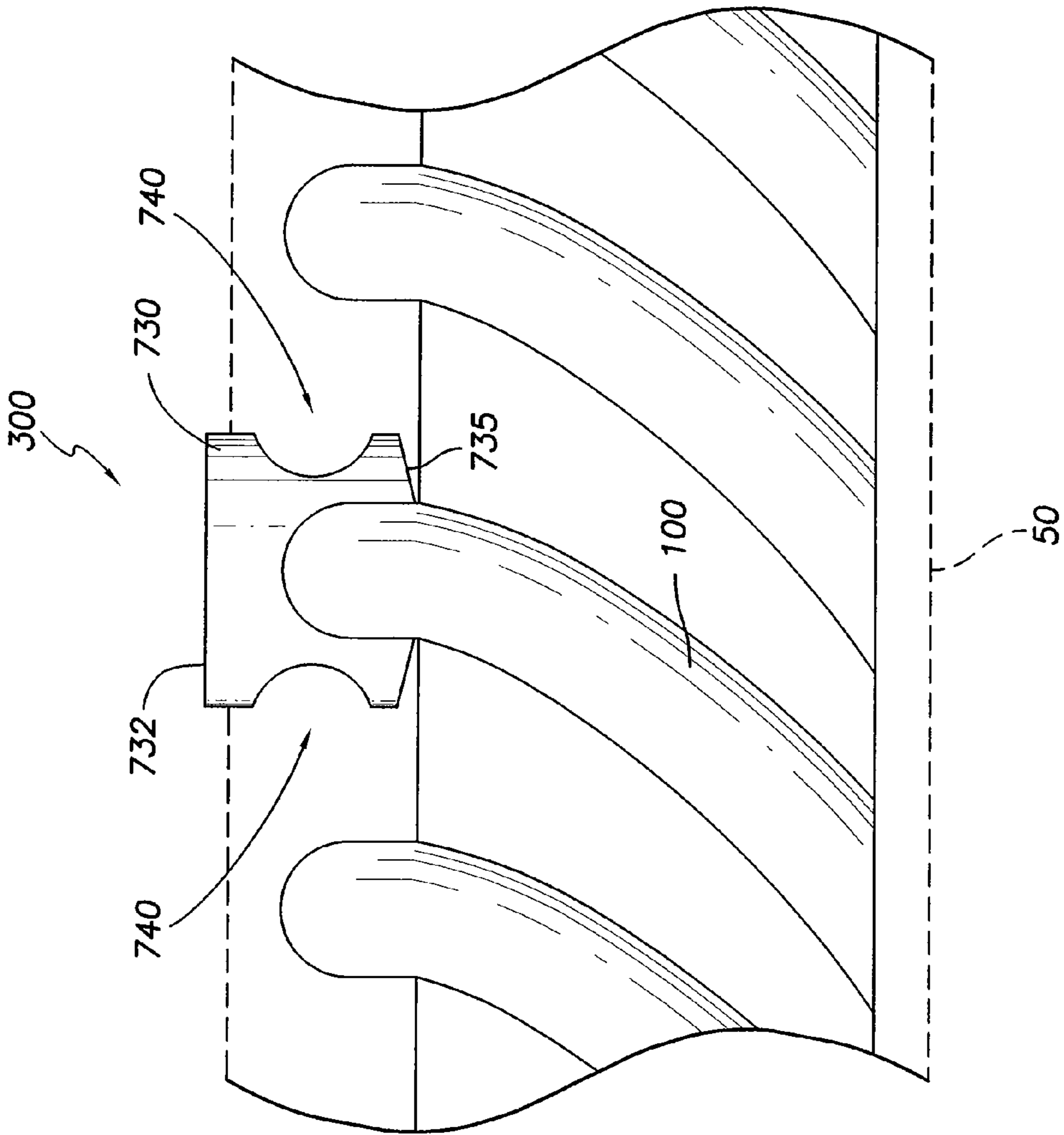
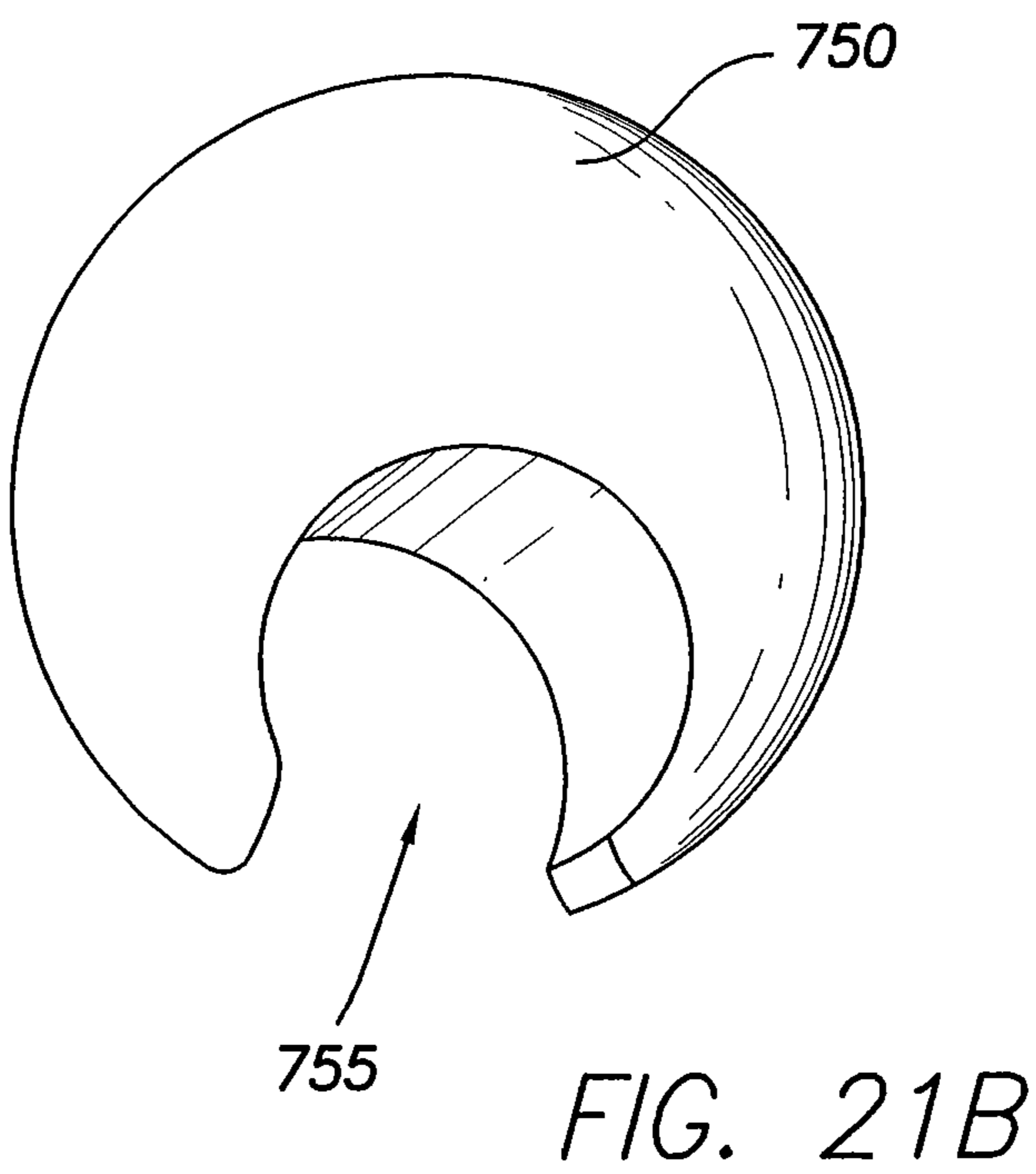
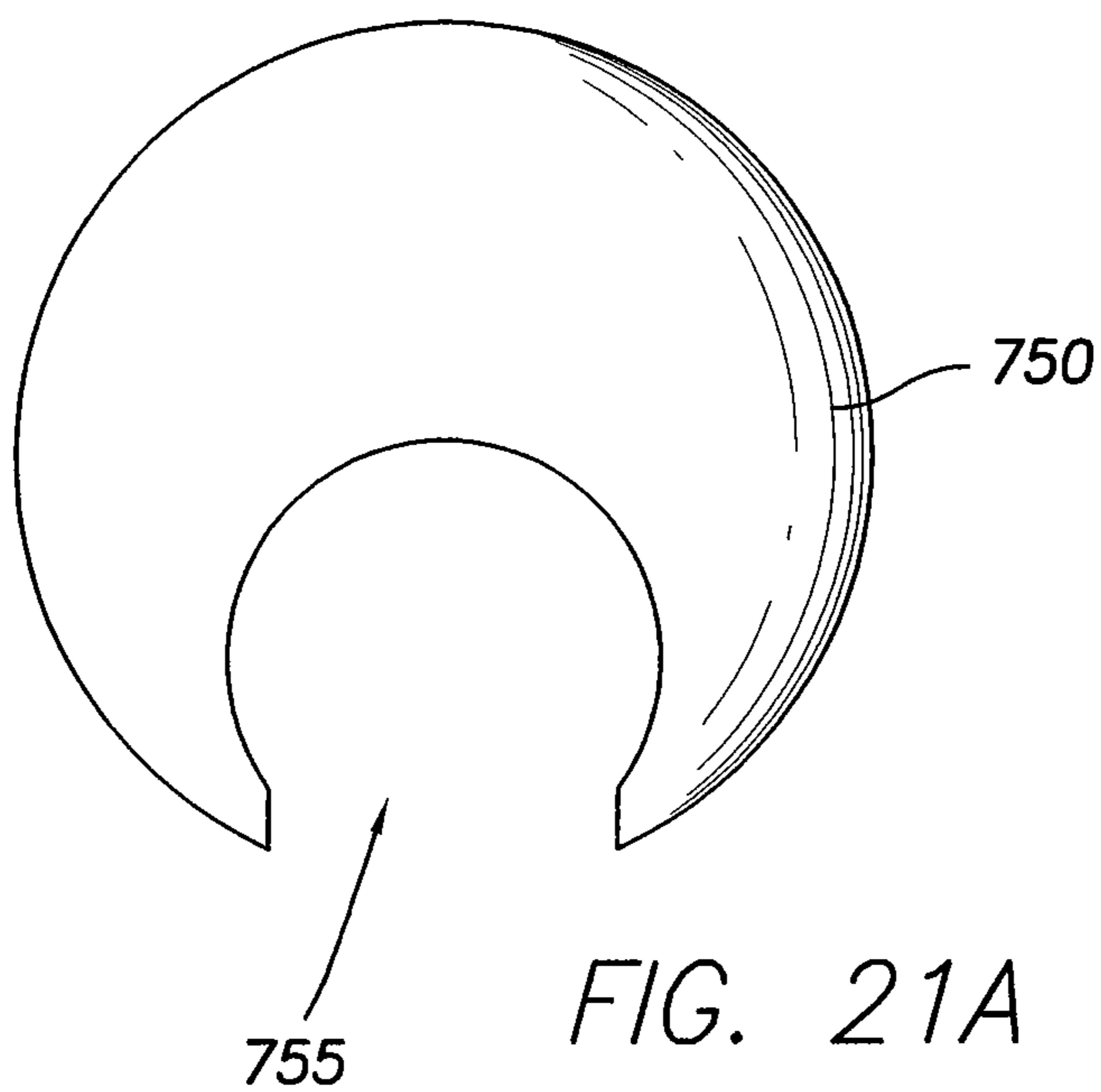


FIG. 20C



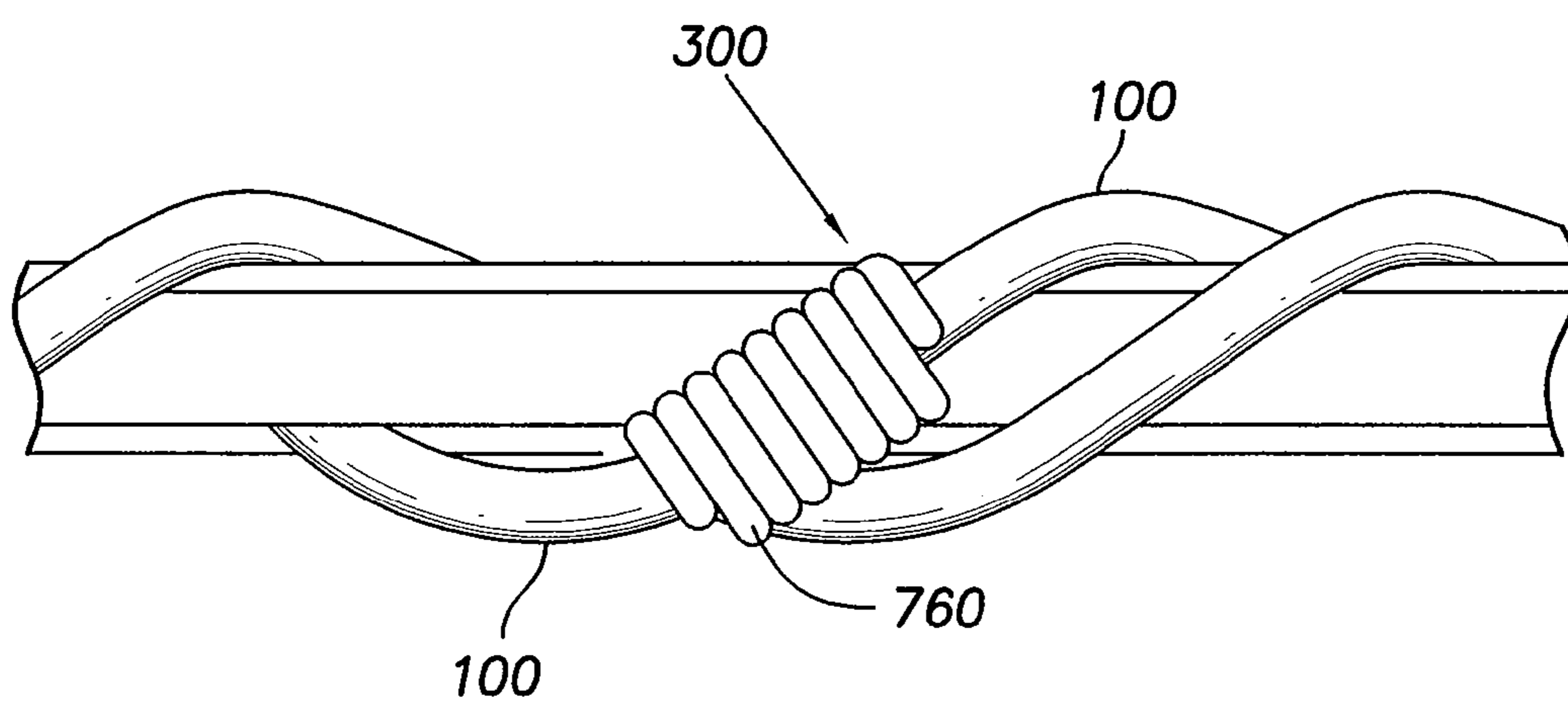


FIG. 22



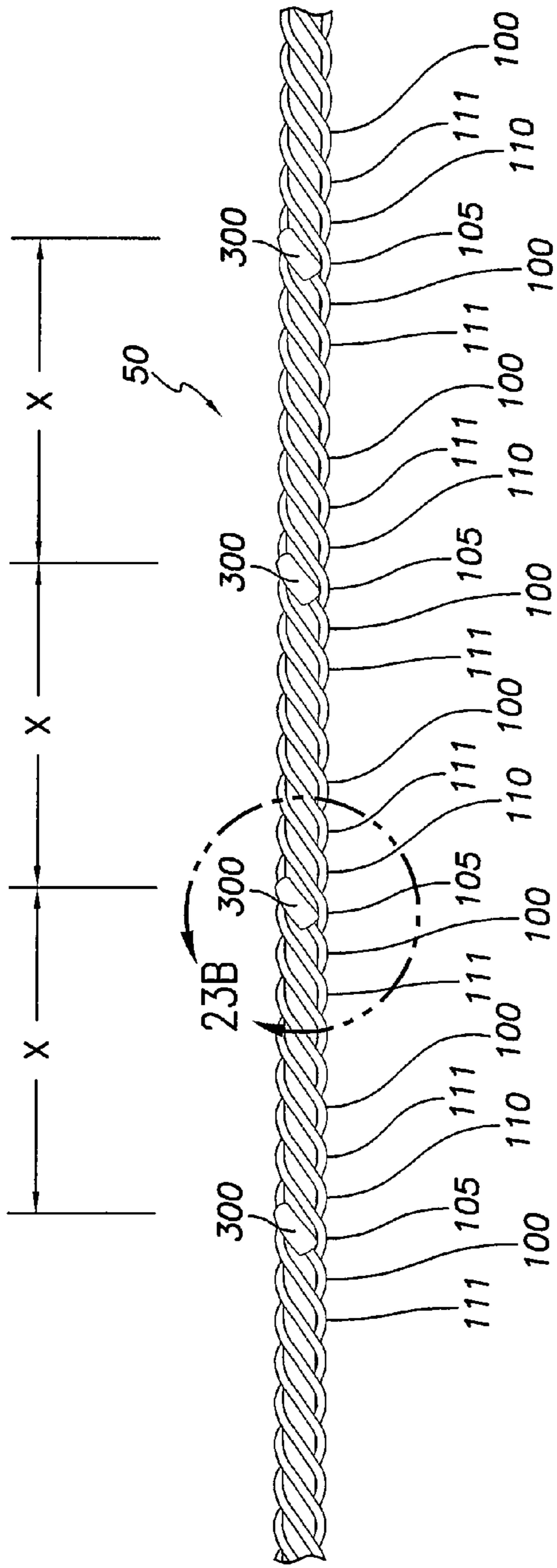


FIG. 23A

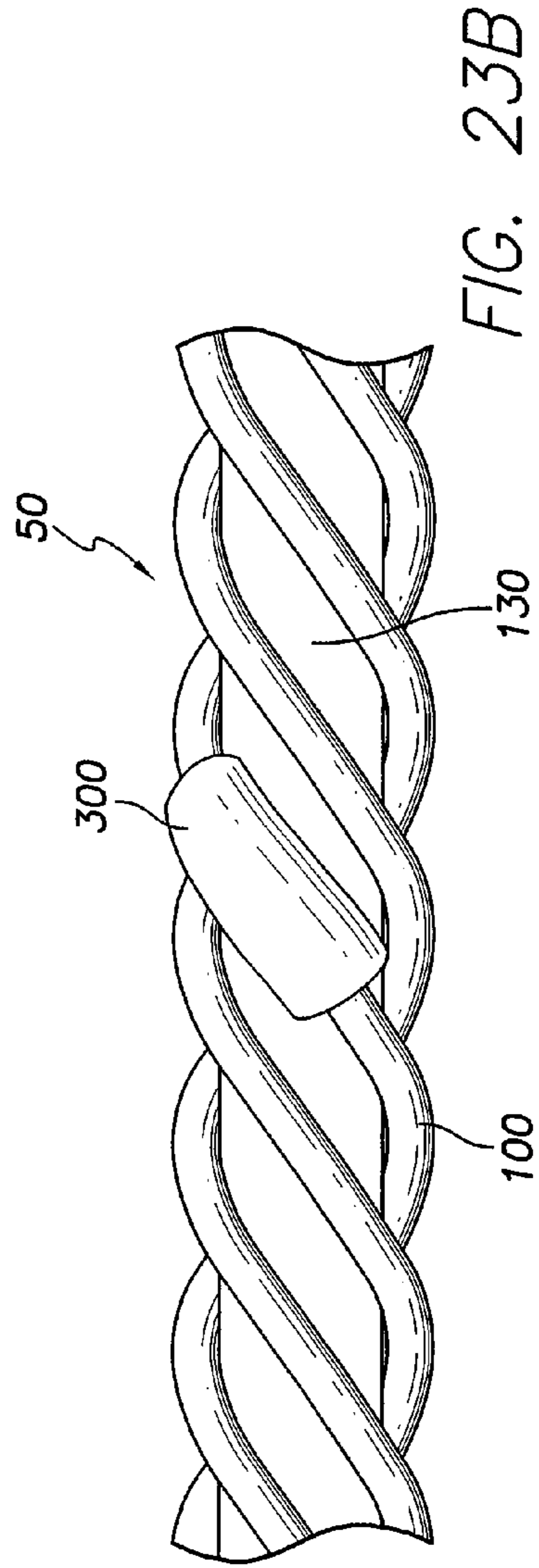


FIG. 23B

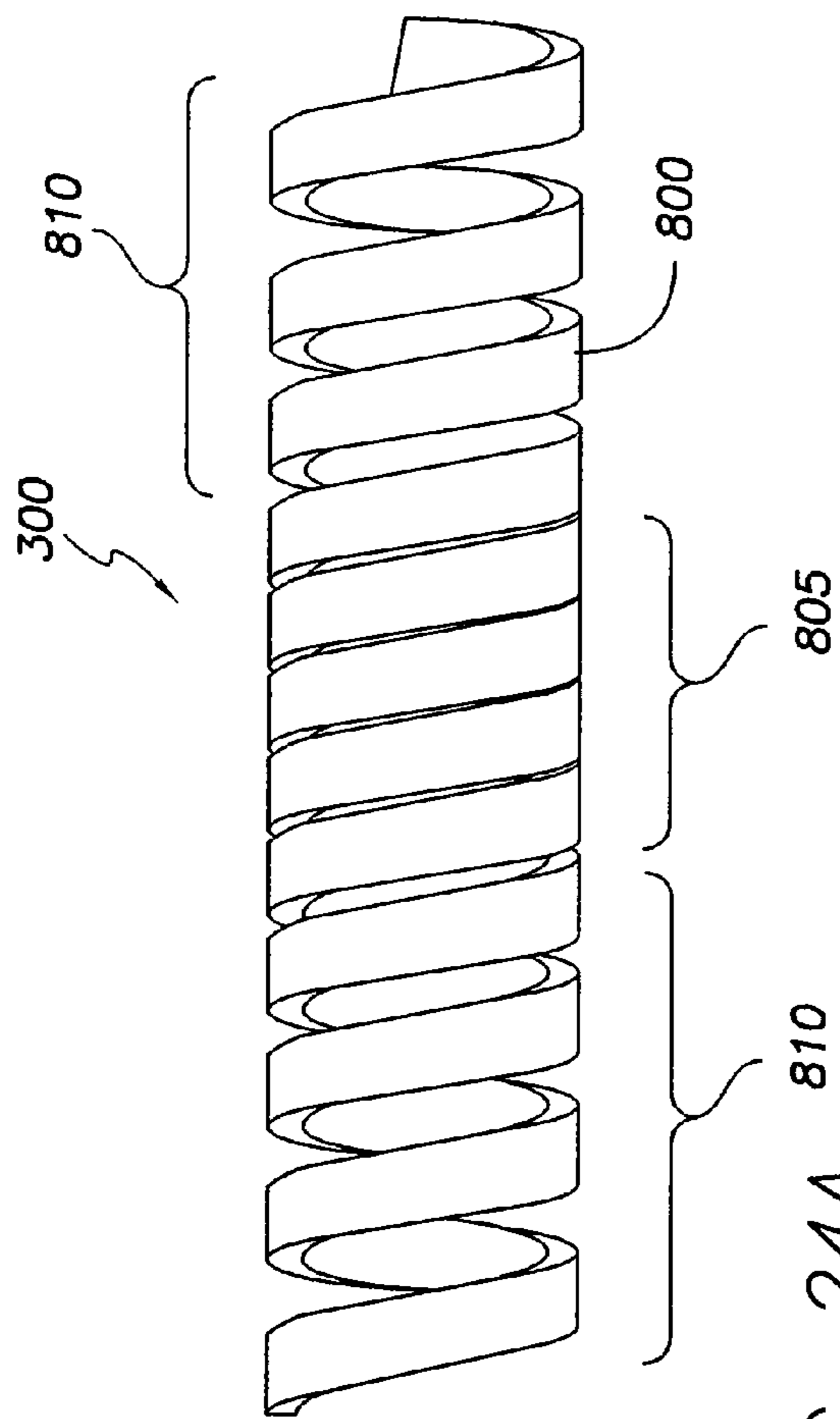


FIG. 24A

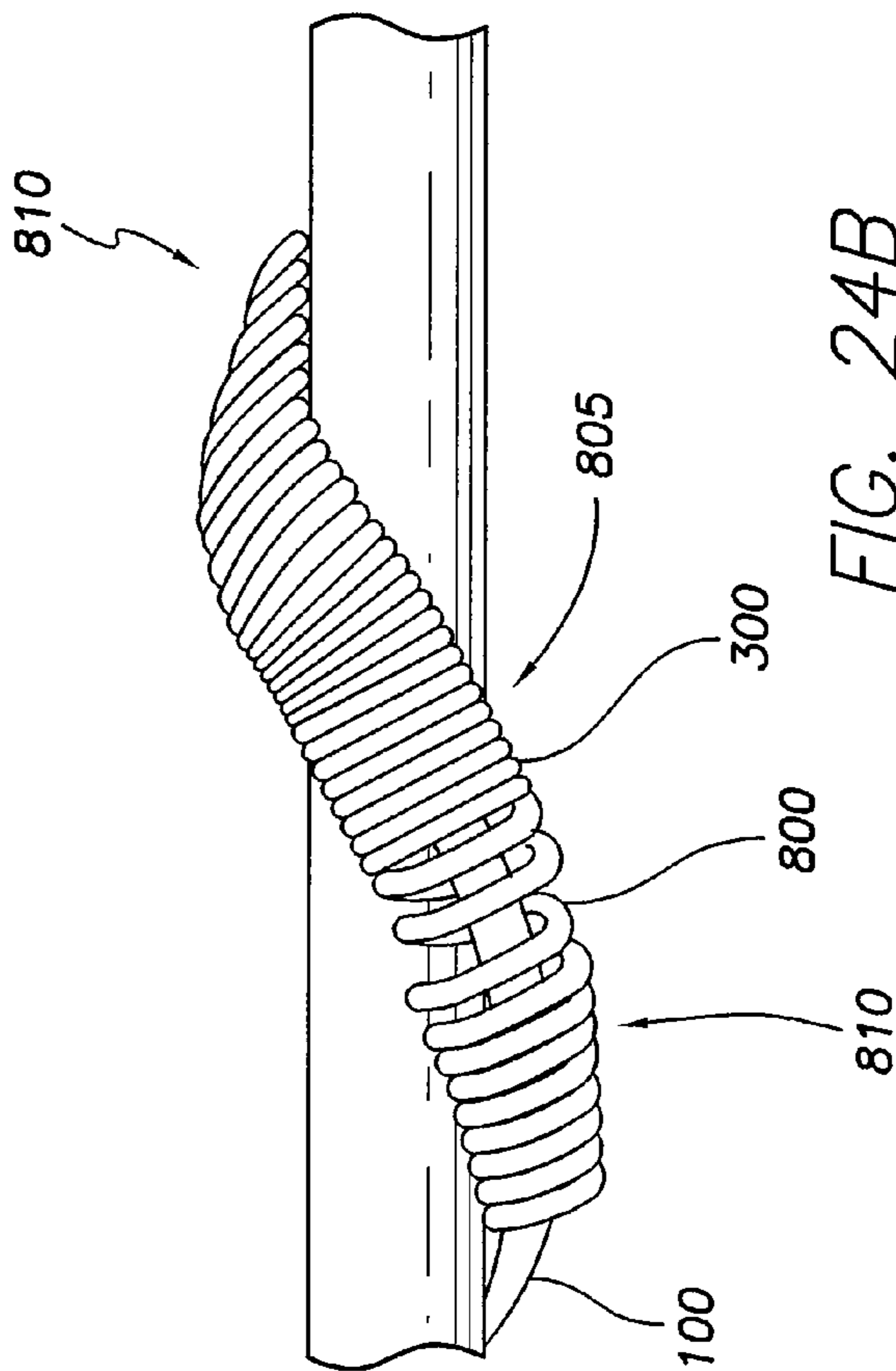


FIG. 24B

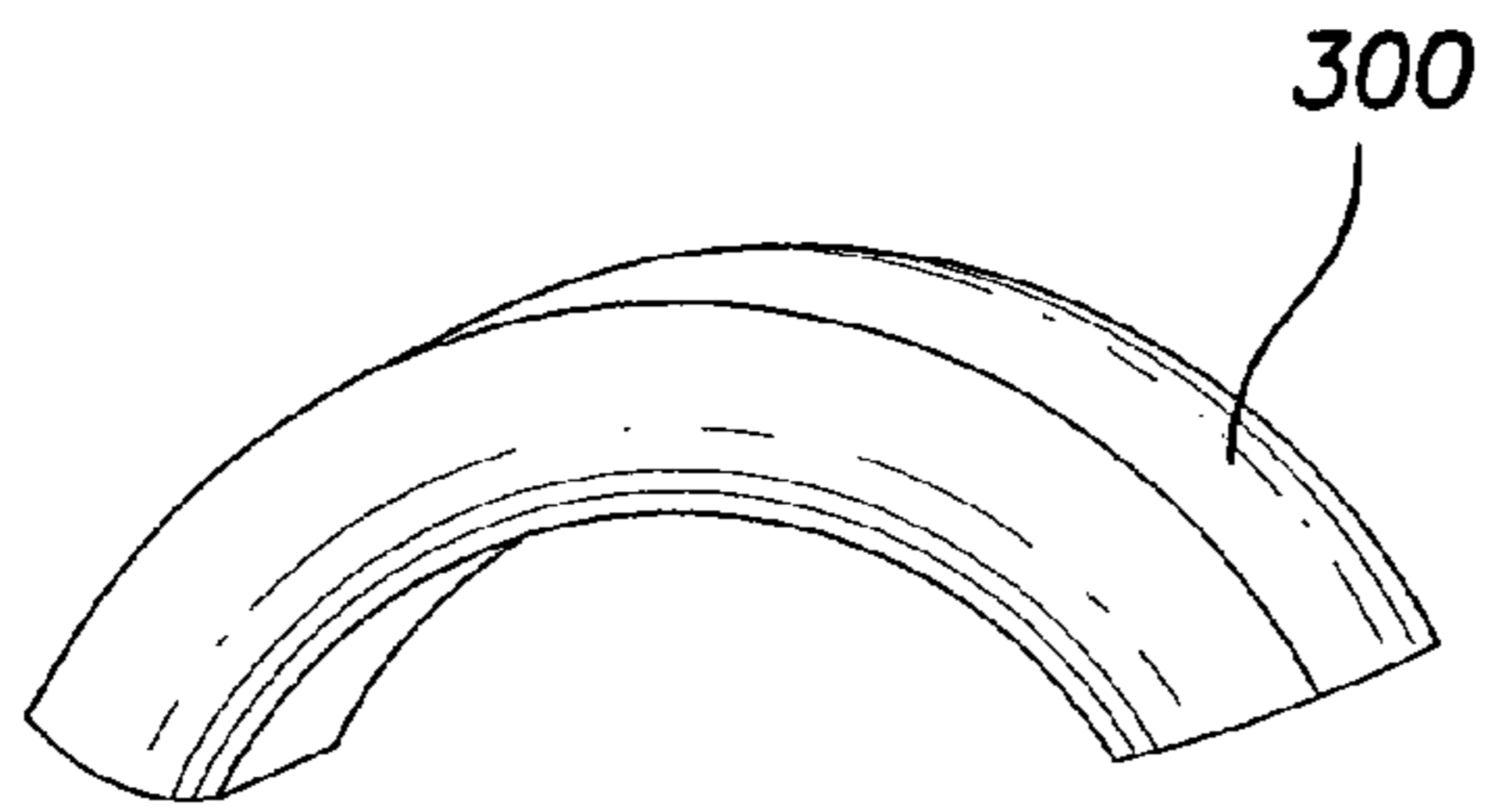


FIG. 25A

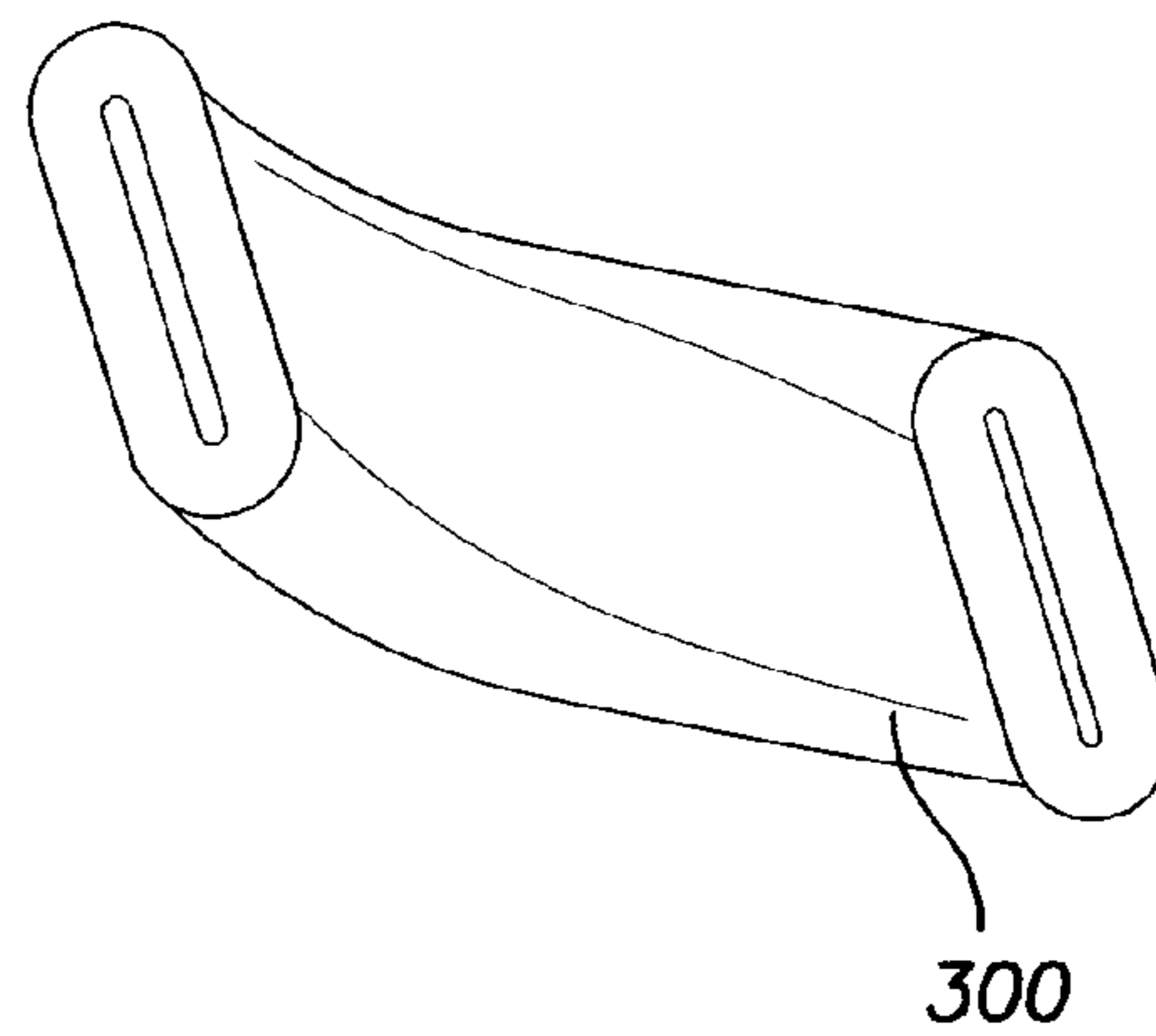


FIG. 25B

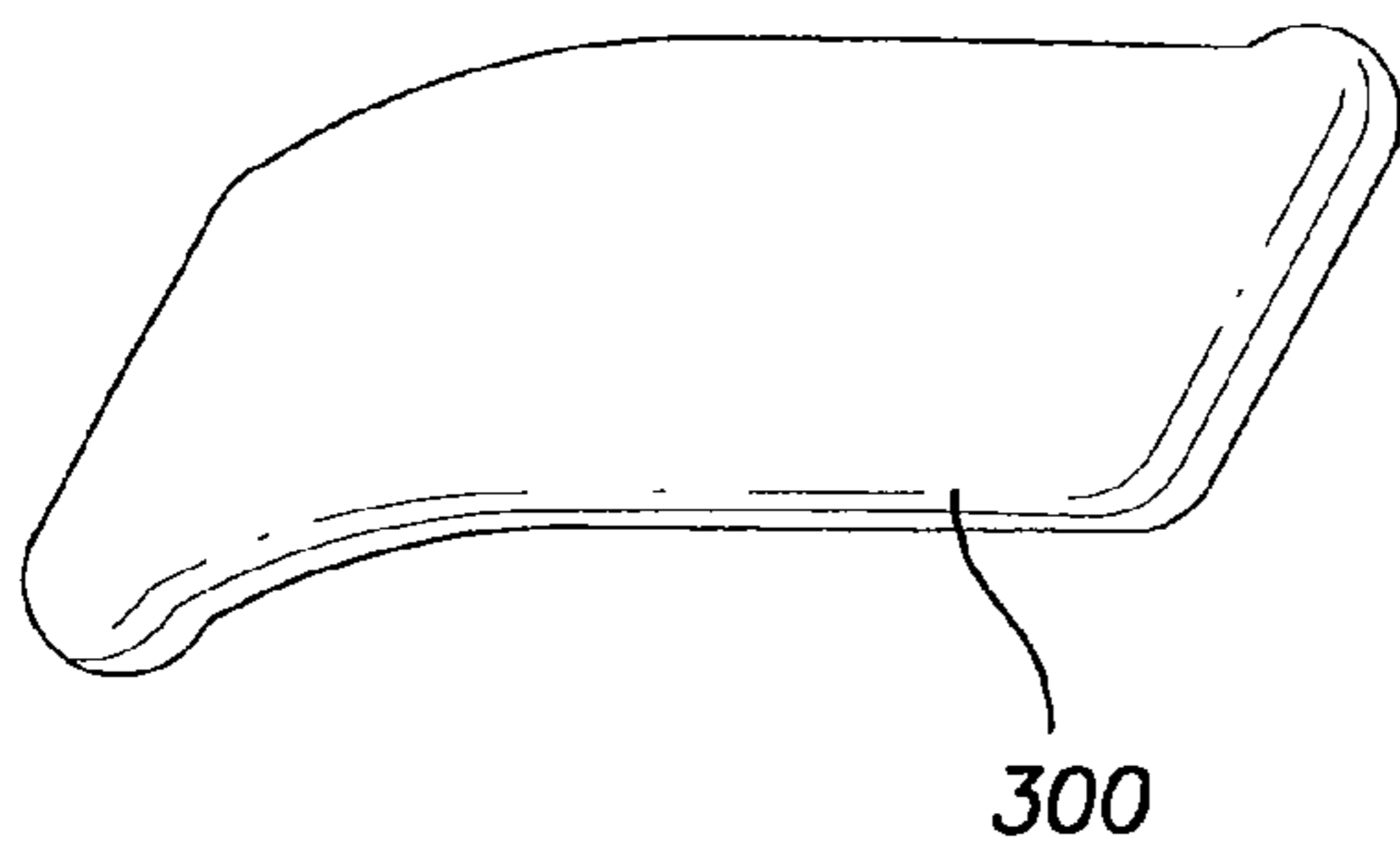


FIG. 25C

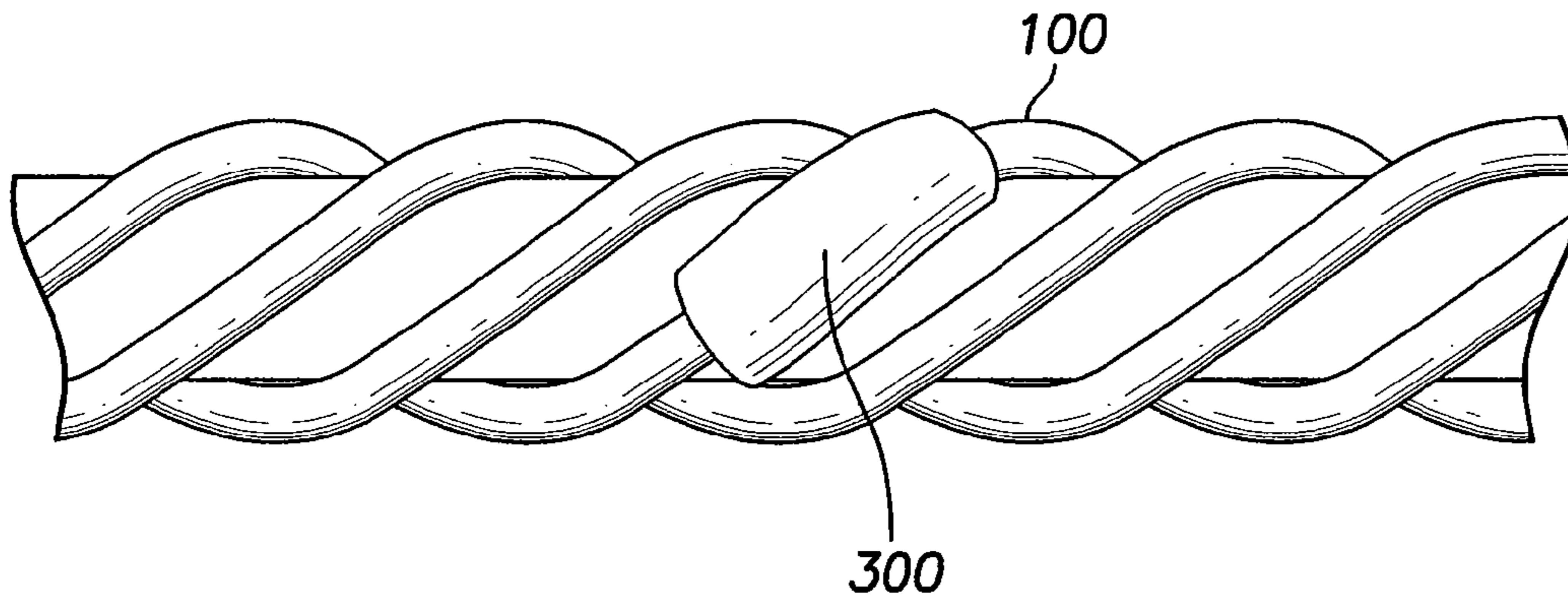


FIG. 25D

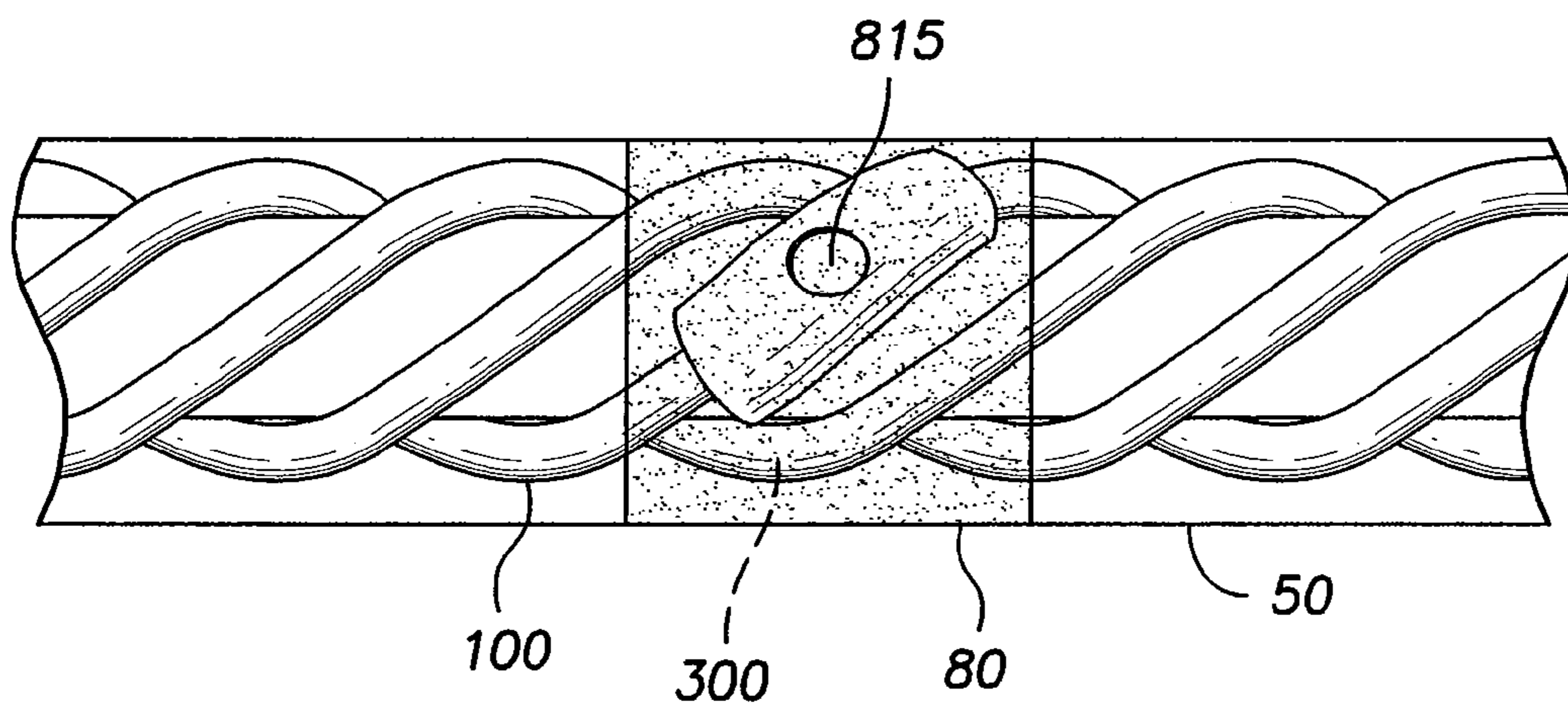


FIG. 25E

**CRIMP TERMINATIONS FOR CONDUCTORS  
IN IMPLANTABLE MEDICAL LEAD AND  
METHOD OF MAKING SAME**

CROSS REFERENCE TO RELATED  
APPLICATIONS

This application is a divisional of U.S. patent application Ser. No. 12/716,552, filed Mar. 3, 2010, now U.S. Pat. No. 8,594,761, and related to:

1) Ser. No. 14/051,764, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

2) Ser. No. 14/051,795, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

3) Ser. No. 14/051,829, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

5) Ser. No. 14/051,850, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

4) Ser. No. 14/051,976, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

6) Ser. No. 14/051,995, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

7) Ser. No. 14/052,020, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”;

8) Ser. No. 14/052,042, titled “Crimp Terminations for Conductors in Implantable Medical Lead and Method of Making Same”; all applications filed Oct. 11, 2014.

FIELD OF THE INVENTION

The present invention relates to medical apparatus and methods. More specifically, the present invention relates to implantable medical leads and methods of manufacturing such leads.

BACKGROUND OF THE INVENTION

Implantable pulse generators, such as pacemakers, defibrillators, implantable cardioverter defibrillators (“ICD”) and neurostimulators, provide electrotherapy via implantable medical leads to nerves, such as those nerves found in cardiac tissue, the spinal column, the brain, etc. Electrotherapy is provided in the form of electrical signals, which are generated in the pulse generator and travel via the lead’s conductors to the electrotherapy treatment site.

Patients may benefit from electrotherapy treatments to be proposed in the future. However, current conventional lead manufacturing technology has generally limited the extent to which leads can be reduced in size and the elements or features that can be carried on leads.

There is a need in the art for a lead having a configuration that allows the lead to have a reduced size and which is capable of supporting elements or features in a variety of configurations. There is also a need in the art for a method of manufacturing such a lead.

BRIEF SUMMARY OF THE INVENTION

Disclosed herein is an implantable medical lead. In one embodiment, the lead may include a longitudinally extending

body, a helical anchor and a lead connector end. The longitudinally extending body may include a distal end, a proximal end, a braid-reinforced inner tubular layer extending between the proximal and distal ends, and an outer tubular layer extending between the proximal and distal ends. The braid-reinforced inner tubular layer may extend through the outer tubular layer in a coaxial arrangement. The helical anchor electrode may be operably coupled to a distal end of the braid-reinforced inner tubular layer. The lead connector end may be operably coupled to the proximal end of the body and include a pin contact operably coupled to a proximal end of the braid-reinforced tubular layer. Rotation of the pin contact relative to the lead connector end may cause rotation of the braid-reinforced inner tubular layer within the outer tubular layer, and the resulting rotation of the braid-reinforced inner tubular layer may cause rotation of the helical anchor electrode.

Another implantable medical lead is also disclosed herein. In one embodiment, the lead includes a longitudinally extending body having a distal end, a proximal end, and a braid-reinforced tubular layer extending between the proximal and distal ends. The braid-reinforced tubular layer may include a braid arrangement imbedded in a polymer wall material. The braid arrangement may include first and second conductors and first and second ribbons. The conductors and ribbons may be helically cross wound with each other such that the conductors do not cross each other and the ribbons do not cross each other.

Also disclosed herein is a method of assembling an implantable medical lead. In one embodiment, the method includes: providing a first longitudinally extending tubular liner including an outer circumferential surface; providing a first braid arrangement over the outer circumferential surface of the first longitudinally extending tubular liner, wherein the first braid arrangement includes first and second conductors and first and second ribbons, wherein the conductors and ribbons of the first braid arrangement are helically cross wound with each other such that the conductors do not cross each other and the ribbons do not cross each other; reflowing or molding (e.g., liquid injection mold (“LIM”)) a first polymer material over the first braid arrangement and outer circumferential surface of the first longitudinally extending tubular liner such that the braid arrangement is substantially imbedded in the polymer material and the polymer material substantially adheres to the outer circumferential surface, resulting in a first braid-reinforced tubular layer; and electrically connecting the first conductor to an electrode.

Another implantable medical lead is also disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp including a collar and a tail extending from the collar. The collar includes a hole. The tail extends around the electrical conductor and through the hole. The crimp is electrically and mechanically coupled to the electrode.

Yet another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp. The crimp includes opposed first and second portions that are each generally shaped like a half-cylinder. The portions are joined along a common lon-

gitudinal side. A tail extends from a free longitudinal side of the first portion. A hole is defined in the second portion. The tail extends around the electrical conductor and through the hole. The crimp is electrically and mechanically coupled to the electrode.

Yet another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp. The crimp includes a ribbon having a first end and a second end. The ribbon extends around the conductor. A first length of the ribbon near the first end is in contact with a second length of the ribbon near the second end. The crimp is electrically and mechanically coupled to the electrode.

Another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp. The crimp includes a portion and a tail extending from the portion, the portion having a generally half-cylinder shape that defines a trough. The conductor is received in the trough. The tail is electrically and mechanically coupled to the electrode.

Another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp. The crimp includes a generally cylindrical shape, a split extending generally longitudinally along the generally cylindrical shape, a hole in the generally cylindrical shape opposite the split, and a trough in which the conductor is received. The crimp is electrically and mechanically coupled to the electrode.

Yet another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp. The crimp includes a spherical outer surface and a recess formed in the spherical outer surface. The conductor is received in the recess, the crimp electrically and mechanically coupled to the electrode.

Yet another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp. The crimp includes a cylindrical outer surface, a pair of recesses formed in the cylindrical outer surface, and another recess formed in an end of the crimp. The conductor is received in the another recess, and the crimp is electrically and mechanically coupled to the electrode.

Another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, an electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the

electrode, and a crimp. The crimp includes a helical shaped outer surface and a helically shaped opening extending through the length of the crimp. The conductor extends through the helically shaped opening. The crimp is electrically and mechanically coupled to the electrode.

Yet another implantable medical lead is disclosed herein. In one embodiment, the lead includes a longitudinally extending body including a distal end and a proximal end, a ring electrode on the body near the distal end, a lead connector end operably coupled to the proximal end of the body, an electrical conductor extending between the lead connector end and the electrode, and a crimp electrically and mechanically coupled to the electrode. The ring electrode includes a cylindrical wall and a seam extending proximal to distal along the wall. The seam is formed by a first wall edge extending proximal to distal and a second wall edge extending proximal to distal. The wall edges are opposed and brought together to form the seam. Each wall edge includes a notch such that, when the wall edges are brought together to form the seam, the notches form a window extending through the wall.

A method of manufacturing an implantable medical lead is also disclosed herein. In one embodiment the method includes: providing a lead body including a proximal end, a distal end, and an electrode near the distal end; provide a conductor extending between the proximal and distal ends; providing a crimp including a ribbon-like member and extending the ribbon-like member around the conductor; and mechanically and electrically connecting the ribbon-like member to the electrode.

Yet another method of manufacturing an implantable medical lead is disclosed herein. In one embodiment the method includes: providing a lead body including a proximal end and a distal end; providing a conductor extending between the proximal and distal ends; ablating a ringed recess in an outer surface of the lead body; providing a split ring electrode; threading the lead body through the split ring electrode when the split ring electrode is expanded; positioning the split ring electrode in the ringed recess; and mechanically and electrically connecting the ring electrode to the conductor.

A method of manufacturing an implantable medical lead is also disclosed herein. In one embodiment the method includes: providing a lead body including a proximal end, a distal end, and an electrode near the distal end; provide a conductor extending between the proximal and distal ends, the conductor including a helical crimp mounted on the conductor, the conductor extending through the helical crimp; and mechanically and electrically connecting the helical crimp to the electrode.

While multiple embodiments are disclosed, still other embodiments of the present invention will become apparent to those skilled in the art from the following Detailed Description, which shows and describes illustrative embodiments of the invention. As will be realized, the invention is capable of modifications in various aspects, all without departing from the spirit and scope of the present invention. Accordingly, the drawings and detailed description are to be regarded as illustrative in nature and not restrictive.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is an isometric view of an implantable medical lead and a pulse generator for connection thereto.

FIG. 2 is an isometric view of a distal portion of a tubular body of a medical lead similar to the lead depicted in FIG. 1, except the lead having an active fixation helical anchor at the lead distal end.

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FIG. 3 is an enlarged isometric view of the distal portion of the tubular body of the medical lead of FIG. 2, except the shock coil is hidden and the outer circumferential surface of the outer tubular layer of the lead body is shown in phantom line for clarity purposes.

FIG. 4 is a transverse cross section of the tubular body of the medical lead as taken along section line 4-4 in FIG. 3.

FIG. 5 is a side view of an example conductor/fiber braid arrangement that may be in at least one of the tubular layers or walls forming the tubular body of FIG. 3.

FIG. 6 is an isometric view of the conductor/fiber braid arrangement of FIG. 5.

FIG. 7 is the same view as FIG. 5, except the conductor/fiber braid arrangement has been reflowed or molded with SPC to form a braided tubular wall or layer of the tubular body depicted in FIGS. 3 and 4.

FIG. 8 is an enlarged partial transverse cross section through a window formed in the outer tubular wall or layer at arrow A and as taken along section line 8-8 in FIG. 3.

FIG. 9 is the same view of the tubular body of the medical lead depicted in FIG. 3, except depicting only the inner tubular wall or layer and helical anchor extending therefrom.

FIG. 10 is a longitudinal cross section of the inner tubular wall or layer as taken along section line 10-10 in FIG. 9.

FIG. 11 is the same view as depicted in FIG. 10, except showing both layer assemblies.

FIG. 11A is an isometric view of a zip tie type crimp slug.

FIGS. 11B and 11C are, respectively, plan and side views of the crimp slug of FIG. 11A.

FIG. 12A is a plan view of a portion of a lead tubular body with a conductor helically routed about a liner layer and imbedded in the polymer material, the helically routed conductor and polymer material forming the reinforced layer.

FIGS. 12B and 12C are, respectively, cross sections of the lead tubular body as taken along section line 12B-12B and section line 12C-12C in FIG. 12A.

FIG. 13A is a view of the tubular body similar to the view depicted in FIG. 12A.

FIG. 13B is generally the same view of the tubular body depicted in FIG. 13A.

FIG. 13C is a side view of the lead body with the crimp fully cinched down on the conductor.

FIG. 13D is an isometric view of the crimp fully cinched down on the conductor, which is shown in phantom lines.

FIG. 13E is another isometric view of the crimp fully cinched down on the conductor, which is shown in phantom lines.

FIG. 14A is an isometric view of a split ring electrode in an expanded or split condition.

FIG. 14B is a view of a tubular body with the split ring electrode depicted in FIG. 14A in a non-expanded condition.

FIG. 14C is a view of the tubular body with a weld formed at a crimp of the split ring electrode depicted in FIG. 14A.

FIG. 15A is an isometric of a notched ring electrode.

FIG. 15B is a view of the tubular body similar to that of FIG. 14B.

FIG. 16A is a plan view of another zip tie type crimp slug in a flat pattern condition.

FIG. 16B is an isometric view of the zip tie type crimp slug of FIG. 16A in a formed state.

FIGS. 16C and 16D are, respectively, isometric and side views of the crimp slug of FIG. 16B in a looped condition.

FIGS. 17A and 17B are, respectively, isometric and plan views of a lead body.

FIG. 17C is a transverse cross section of the lead body at a location of an alternative version of the ribbon equipped crimp of FIGS. 17A-17B.

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FIG. 18A is an isometric view of another embodiment of the crimp slug.

FIGS. 18B and 18C are, respectively, top and bottom isometric views of a half-cylinder shaped tool for use in crimping the crimp on an exposed conductor.

FIG. 19 is an isometric view of a side loader crimp slug.

FIGS. 20A and 20B are, respectively, isometric and side views of a

FIG. 20C is a side view of a portion of a lead, wherein the crimp slug of FIGS. 20A and 20B is coupled to a conductor.

FIGS. 21A and 21B, which are, respectively, isometric and side views of a notched spherical crimp slug.

FIG. 22 is a plan view of a twisted micro wire crimp on a conductor.

FIGS. 23A and 23B are respectively, a side view of a lead body and an enlarged side view of the same lead body at a location of a crimp.

FIGS. 24A and 24B are, respectively, a plan view of a helical wound crimp and a plan view of the same crimp mounted on a conductor.

FIGS. 25A-25C are, respectively, side, inner and outer views of a helically shaped crimp.

FIGS. 25D-25E are, respectively, the crimp on a conductor and a crimp-equipped conductor assembled into a lead body, the conductor would be fed through the helical crimp.

## DETAILED DESCRIPTION

An implantable medical lead 10 is disclosed herein. In one embodiment, the implantable medical lead 10 includes a tubular body 50 having one, two or more tubular layers 125, 135 each reinforced with a conductor/fiber braid arrangement 115 imbedded in the polymer material 162 forming the walls of the tubular layers 125, 135. The conductor/fiber braid arrangement 115 may be one, two or more helically wound conductors 100, 105, 110 woven with one, two or more helically wound fiber strips 165. In one embodiment, the braid arrangement 115 is such each conductor crosses the strips or ribbon 165, but does not cross itself or any other conductor. Similarly, each strip or ribbon 165 crosses the conductors, but does not cross itself or any of the strip or ribbon.

Such braid-reinforced layers 125, 135 offer the ability to manufacture lead bodies 50 have substantially reduced diameters, substantial improvement with respect to torque and flexibility consistency and capabilities, reduced manufacturing costs, and the ability to support a large number of electrodes and sensors in a large variety of configurations. Also, such braid-reinforced layers 135 may be used to replace the common helically wound central coil as a mechanism for extending/retracting a helical anchor electrode 85 and, in doing so, offer an anchor extension/retraction mechanism that provides one-to-one torque.

For a general discussion of an embodiment of a lead 10 including a body having at least one tubular layer reinforced with the conductor/fiber braid arrangement, reference is made to FIG. 1, which is an isometric view of the implantable medical lead 10 and a pulse generator 15 for connection thereto. The pulse generator 15 may be a pacemaker, defibrillator, ICD or neurostimulator. As indicated in FIG. 1, the pulse generator 15 may include a can 20, which may house the electrical components of the pulse generator 15, and a header 25. The header may be mounted on the can 20 and may be configured to receive a lead connector end 35 in a lead receiving receptacle 30.

As shown in FIG. 1, in one embodiment, the lead 10 may include a proximal end 40, a distal end 45 and a tubular body 50 extending between the proximal and distal ends. The

proximal end **40** may include a lead connector end **35** including a pin contact **55**, a first ring contact **60**, a second ring contact **61**, which is optional, and sets of spaced-apart radially projecting seals **65**. In some embodiments, the lead connector end **35** may include the same or different seals and may include a greater or lesser number of contacts. For example, the lead connector end **35** may be in the form of an IS-1, IS-4, DF-1, etc. configuration. The lead connector end **35** may be received in a lead receiving receptacle **30** of the pulse generator **15** such that the seals **65** prevent the ingress of bodily fluids into the respective receptacle **30** and the contacts **55**, **60**, **61** electrically contact corresponding electrical terminals within the respective receptacle **30**.

As illustrated in FIG. 1, in one embodiment, the lead distal end **45** may include a distal tip **70**, a tip electrode **75** and a ring electrode **80**. In some embodiments, as indicated in FIG. 2, which is an isometric view the distal end **45** of an alternative embodiment of the lead **10**, the lead distal end **45** may include a helical anchor **85** that is extendable from within the distal tip **70** for active fixation and may or may not act as an electrode. In other embodiments, the lead distal end **45** may include features or a configuration that facilitates passive fixation.

As shown in FIGS. 1 and 2, in some embodiments, the distal end **45** may include a defibrillation coil **82** about the outer circumference of the lead body **50**. The defibrillation coil **82** may be located proximal of the ring electrode **80**.

As illustrated in FIG. 1 where the lead **10** is configured for passive fixation, the tip electrode **75** may form the distal tip **70** of the lead body **50**. The ring electrode **80** may extend about the outer circumference of the lead body **50**, proximal of the distal tip **70**. In other embodiments, the distal end **45** may include a greater or lesser number of electrodes **75**, **80** in different or similar configurations.

As indicated in FIG. 2 where the lead **10** is configured for active fixation, an atraumatic tip **90** may form the distal tip **70** of the lead body **50**, and the helical anchor electrode **85** may be extendable/retractable relative to the distal tip **70** through an opening **95** in the distal tip **70**. The ring electrode **80** may extend about the outer circumference of the lead body **50**, proximal of the distal tip **70**. In other embodiments, the distal end **45** may include a greater or lesser number of electrodes in different or similar configurations.

In one embodiment, the tip electrode **75** or helical anchor electrode **85** may be in electrical communication with the pin contact **55** via a first helically routed electrical conductor **100** (see FIGS. 9 and 10) and the ring electrode **80** may be in electrical communication with the first ring contact **60** via a second helically routed electrical conductor or pair of helically routed electrical conductors **105** (see FIGS. 2 and 3). In some embodiments, the defibrillation coil **82** may be in electrical communication with the second ring contact **61** via a third helically routed electrical conductor or pair of helically routed electrical conductors **110** (see FIGS. 2, 3 and 8). In yet other embodiments, other lead components (e.g., additional ring electrodes, various types of sensors, etc.) mounted on the lead body distal region **45** or other locations on the lead body **50** may be in electrical communication with a third ring contact (not shown) similar to the second ring contact **61** via a fourth helically routed electrical conductor or pair of helically routed electrical conductors. Of course, if needed, helically routed electrical conductors in addition to those already mentioned may be routed through the lead body in a manner similar to that depicted in FIGS. 2, 3, 9 and 10. Any of the helically routed conductors may be routed singly, in pairs, groups of three, groups of four, etc. Depending on the embodiment, any of the helically routed electrical conductors may be in the form of a multi-strand or filar cable or a solid

wire conductor. Depending on the embodiment, any of the helically routed conductors may have a dedicated electrical insulation jacket or be jacketless such that the electrical conductor is reliant upon the material forming the tubular liner for electrical insulation.

For a detailed discussion regarding a lead body **50** employing the conductor/fiber braid arrangement **115** disclosed herein, reference is made to FIGS. 3 and 4. FIG. 3 is an enlarged isometric view of the distal end **45** of the tubular body **50** of the medical lead **10** of FIG. 2, except the shock coil **82** is hidden and the outer circumferential surface **120** of the outer tubular layer **125** of the lead body **50** is shown in phantom line for clarity purposes. FIG. 4 is a transverse cross section of the lead body **50** as taken along section line 4-4 in FIG. 3.

As shown in FIG. 4, in one embodiment, the tubular body **50** of the medical lead **10** may include an innermost tubular liner layer **130**, an innermost tubular braid-reinforced layer **135**, an outermost tubular liner layer **140** and an outermost tubular braid-reinforced layer **125**. An inner circumferential surface **145** of the innermost liner layer **130** may define a central lumen **150** extending longitudinally through the tubular lead body **50**. An outer circumferential surface of the innermost liner layer **130** may abut against the inner circumferential surface of the innermost braid-reinforced layer **135**. An outer circumferential surface of the innermost braid-reinforced layer **135** may displaceably abut against the inner circumferential surface of the outermost liner layer **140** such that the innermost layer assembly **155** (i.e., the innermost liner layer **130** and the innermost braid-reinforced layer **135**) may be caused to rotationally displace within the outermost layer assembly **160** (i.e., the outermost liner layer **140** and the outermost braid-reinforced layer **125**). An outer circumferential surface of the outermost liner layer **140** may abut against the inner circumferential surface of the outermost braid-reinforced layer **125**. The outer circumferential surface **120** of the outermost braid-reinforced layer **125** may form the outer circumferential surface of the tubular lead body **120**.

In one embodiment, the liner layers **130** and **140** may be formed of polytetrafluoroethylene PTFE or another polymer material having similar properties. Each liner layer **130** and **140** may have a wall thickness of between approximately 0.001" and approximately 0.005". In one embodiment, the braid-reinforced layers **125** and **135** may each be formed of a conductor/fiber braid arrangement **115** (see FIGS. 3-10) imbedded in a wall material **162** of silicone rubber—polyurethane—copolymer ("SPC"), silicone rubber, polyurethane or another polymer material having similar properties. Each layer **125** and **135** may have a wall thickness of between approximately 0.004" and approximately 0.02".

In some embodiments, the layers **125** and **135** may both be braid-reinforced with the braid arrangement **115**. However, in other embodiments, only one of the layers **125** and **135** may be braid-reinforced with the braid arrangement **115**, the other non-braid-reinforced layer being simply a layer of SPC or other similar polymer material. For example, in one embodiment, the innermost layer **135** may be braid-reinforced with the braid arrangement **115** and the outermost layer **125** may not employ the braid arrangement **115**. Conversely, in another embodiment, the outermost layer **125** may be braid-reinforced with the braid arrangement **115** and the innermost layer **135** may not employ the braid arrangement **115**.

For a discussion of an example braid arrangement **115**, reference is now made to FIGS. 5 and 6. FIG. 5 is a side view of the example conductor/fiber braid arrangement **115** that may be in at least one of the tubular layers or walls **125** and



**135** forming the tubular body **50** of FIG. 3. FIG. 6 is an isometric view of the conductor/fiber braid arrangement **115** of FIG. 5.

As can be understood from FIGS. 5 and 6, the braid arrangement **115** may be formed by braiding one, two or more single electrical conductors **100** with one, two or more ribbons **165**. In one embodiment, a ribbon **165** may in the form of a fibrous polyester material. In other embodiments, a ribbon **165** may be in the form of a non-fibrous polymer material. In one embodiment, the ribbon **165** may be formed of polyester, nylon, KEVLAR™, expanded polytetrafluoroethylene (“ePTFE”) or etc. The ribbon **165** may have a thickness of less than approximately 0.0005 inch.

As can be understood from FIGS. 5 and 6, the braid arrangement **115** may be wound in such a way that all the conductors **100** are spatially separated from each other via the ribbon **165** and form a helical coil pattern in the braid arrangement **115**. The braid pattern as depicted in FIGS. 3, 5 and 6 may be such that each conductor **100**, **105**, **110** only crosses over ribbons **165** and not other conductors, and each ribbon **165** only crosses over the conductors, not other ribbons; thus, this braid pattern advantageously reduces the diameter of the braid arrangement **115** as compared to braid patterns where each conductor crosses over other conductors. The reduced diameter of the braid arrangement **115** disclosed herein saves space in the lead body **50**.

Since the ribbon **165** acts as a spacer between the conductors **100**, conductors **100** with or without individual electrical insulation jackets may be employed in the braid arrangement **115**. As can be understood from FIG. 7, which is the same view as FIG. 5, except the conductor/fiber braid arrangement has been reflowed or molded (e.g., liquid injection mold (“LIM”)) with SPC wall material **162** to form a braided tubular wall or layer **125** and **135** similar to those depicted in FIGS. 3, 4, 9 and 10.

As can be understood from FIGS. 3, 5 and 6, the braid pattern results in conductors **100**, **105**, **110** that are wound in an open pitch coil. Therefore, the conductors cannot touch each other and the resulting lead body **50** has improved balance with respect to stresses in the lead body, reducing the likelihood of waviness in the lead body surface subsequent to manufacture. The braid arrangement **115** acts as a structural member for the final lead body construction. The braid arrangement **115** imparts to the lead body **50** many improved mechanical characteristics, including improved torqueability, pushability, flex fatigue resistance, and kink resistance.

As can be understood from FIGS. 4-7, 9 and 10, in some embodiments, the braid arrangement **115** may have one or any multiple number of electrical conductors **100**, and these conductors **100** may be routed singly through the braid arrangement **115**. In other embodiments, as can be understood from FIGS. 3 and 4, the braid arrangement **115** may have one or any multiple number of electrical conductors **105** and **110**, and these conductors **105** and **110** may be routed in pairs (as shown in FIGS. 3 and 4), in groups of three, groups of four, or etc. through the braid arrangement **115**.

The configuration of the braid-reinforced layers **125** and **135** readily lends itself to the efficient coupling of the electrical conductors **105** and **110** to their respective electrodes **80** and **82**. For example, as can be understood from FIG. 3 at arrow A, in one embodiment, the wall material **162** of the outer reinforced layer **125** may be removed via laser ablation, mechanical cutting or other methods to form a window **170** through the wall material **162** that exposes the appropriate conductors **110**.

As can be understood from FIG. 8, which is an enlarged partial transverse cross section through the window **170**

formed in the wall material **162** of the outer tubular wall or layer **125** at arrow A and as taken along section line 8-8 in FIG. 3, a crimp slug **175** may extend through the window **170** between an electrode (e.g., the shock coil **82** in this example) and the respective conductor pair **110**. The bottom portion **180** of the crimp slug **175** may be crimped to the conductors **110** and the top portion **185** of the crimp slug **175** may be welded to the electrode **82**.

As indicated in FIG. 8, the inner circumferential surface **190** of the outermost reinforced layer **125** abuts against the outer circumferential surface **195** of the outermost liner layer **140**. As the outermost reinforced layer **125** may be assembled on the outermost liner layer **140**, the two layers **125** and **140** may be considered to be a single outermost assembly layer **160**. The inner circumferential surface **200** of the outermost liner layer **140** may displaceably abut against the outermost circumferential surface **205** of the innermost braid-reinforced layer **135** such that the innermost assembly layer **155** and outermost assembly layer **160** may coaxially displace relative to each other once assembled into the lead tubular body **50** and the outermost assembly layer **160** may be pulled over the innermost assembly layer **155** during the assembly of the lead tubular body **50**.

Due to the innermost assembly layer **155** and outermost assembly layer **160** being coaxially rotatably relative to each other, in some embodiments, the innermost assembly layer **155** may serve in place of the helically coiled central conductor commonly found in active fixation leads and which are commonly used to extend/retract the helical active fixation anchors of such leads. The configuration of the innermost assembly layer **155** offers several advantages over the traditional helically coiled central conductor. For example, unlike the traditional helically coiled central conductor, the innermost assembly layer **155**, due to its configuration/construction, offers a one-to-one torque transfer when used as the mechanism for extending/retracting the helical anchor **85**.

A discussion of an embodiment of the lead tubular body **50** employing the innermost assembly layer **155** as the mechanism for rotatably extending/retracting the helical active fixation anchor **85** will now be given with respect to FIGS. 9 and 10. FIG. 9 is the same view of the tubular body **50** of the medical lead **10** depicted in FIG. 3, except depicting only the inner tubular wall or layer assembly **155** and helical anchor **85** extending therefrom. FIG. 10 is a longitudinal cross section of the inner tubular wall or layer assembly **155** as taken along section line 10-10 in FIG. 9. As shown in FIGS. 9 and 10, wherein the wall material **162** is shown in phantom line, the braid arrangement **115** may be generally identical to that depicted in FIGS. 5-7.

As can be understood from FIG. 10, the inner circumferential surface **210** of the innermost reinforced layer **135** abuts against the outer circumferential surface **215** of the innermost liner layer **130**. As the innermost reinforced layer **135** may be assembled on the innermost liner layer **130**, the two layers **135** and **130** may be considered to be a single innermost assembly layer **155**. As discussed above, the outer circumferential surface **205** of the innermost braid-reinforced layer **135** may displaceably abut against the innermost circumferential surface **200** of the outermost liner layer **140** such that the innermost assembly layer **155** and outermost assembly layer **160** may coaxially displace relative to each other once assembled into the lead tubular body **50** and the outermost assembly layer **160** may be pulled over the innermost assembly layer **155** during the assembly of the lead tubular body **50**.

As indicated in FIG. 10, a proximal end **220** of a metal helix shank **225** may be received within the distal end of the innermost liner layer **130** and coupled to the inner circumferential

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surface **155** of the layer **130**. A distal end **230** of the shank **225** may be received within and coupled to the proximal end of the helical active fixation anchor **85**. In a manner similar to that depicted in FIG. **8**, the conductor **100** of the innermost reinforced layer **135** may be electrically coupled to the electrically conductive shank **225**, which is electrically coupled to the helical anchor **85**. Alternatively, in a manner similar to that depicted in FIG. **8**, the conductor **100** may be electrically coupled to the proximal end of the helical anchor **85**.

As can be understood FIGS. **3**, **9**, **10**, and **11**, which is the same view as depicted in FIG. **10**, except showing both layer assemblies **155** and **160**, because the helical anchor **85** is fixedly coupled to the distal end of the inner layer assembly **155** and the inner layer assembly **155** is capable of being displaced within the outer layer assembly **160**, the helical anchor can be caused to extend/retract relative to the lead distal tip **70**. More specifically, the extreme proximal end of the inner layer assembly **155** may be coupled to the pin contact **55** (see FIG. **1**), which may be rotatable relative to the rest of the lead connector end **35** (see FIG. **1**). Rotation of the pin contact **55** in a first direction may cause the inner layer assembly **155** to axially rotate within the outer layer assembly **160** and longitudinally displace within the outer layer assembly **160** such that the helical anchor **85** may be caused to extend distally from the opening **95** in the distal tip **70**. Rotation in an opposite direction may cause the helical anchor **85** to retract back into the opening **95**.

In one embodiment, the coupling of the shank **225** to the innermost liner layer **130** in combination with the configuration of the header assembly **235** (see FIG. **3**) may be such that the helical anchor **85** is caused to extend/retract via rotation of the pin contact **55** despite the inner layer assembly **155** being limited to axial rotation relative to the outer layer assembly **160** and not being allowed to longitudinally displace within the outer layer assembly **160**.

A variety of implantable medical leads **10** may be configured as described herein. For example, the lead **10** may be a cardiac lead (both high and low voltage), a multi-polar lead (both cardiac and neurologic), an MRI compatible lead, and an "intelligent" lead such as those intelligent leads that incorporate active components, such as sensors, integrated circuits, MEMS devices or drug delivery mechanisms.

The construction of a lead body **50** may be done on an individual basis or on a continuous basis. When the lead body **50** is manufactured on an individual basis, the conductors **100**, **105**, **110** and ribbon **165** may be braided together on a standard braiding machine to assemble the braid arrangement **115**, which can then be stored on a spool until it is ready to be pulled as a whole or completed braid arrangement **115** onto a liner layer **130**, **140** of the lead body **50** during the assembly process.

Prior to winding the braid assembly **115**, the braid pattern, inside diameter and pitch may be determined according to the type of lead **10** being constructed, such as LV, high or low voltage. In some embodiments, the pitch may be varied at certain points along the length of the lead body **50** to impart different flexibility and torque characteristics at the certain points along the lead body **50**.

Once the braid assembly **115** is braided, the braid assembly **115** may be stored on a large spool. When it is time to assemble a specific lead tubular body **50**, the specific length of braid assembly **115** may be removed from the spool as needed for the specific length of the lead tubular body **50** being assembled. This specific length of braid assembly **115** may then be pulled over an innermost liner layer **130**, which, as discussed above, may be PTFE or other applicable polymer materials. Once the braid assembly **115** extends about the

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outer circumferential surface **215** of the innermost liner layer **130**, SPC (which is also known as OPTIM™ and will act as the wall material **162**) may be reflowed or molded (e.g., LIM) about the braid assembly **115** and innermost liner layer **130** enclosed within the braid assembly **115**. Specifically, in one embodiment employing reflowing, a SPC tube **162** may be pulled over the combined braid assembly **115** and liner layer **130**. A fluorinated ethylene propylene ("FEP") jacket is then pulled over the SPC tube **162**, the braid **115**, and liner **130** and then subjected to reflow conditions to form the inner layer assembly **155**. The FEP jacket is then removed from the resulting inner layer assembly **155**.

In some embodiments, a mandrel is used to dip or extrude the PTFE liner **130** onto the mandrel outer circumferential surface. The PTFE innermost liner layer **130** is left on the mandrel as the braid **115** is braided over the outer circumferential surface **215** of the innermost liner layer **130**. The SPC wall material **162** is then reflowed or molded over the PTFE liner layer **130** and braid **115**, imbedding the braid **115** in the wall material **162**. The mandrel can then be pulled from the completed assembly or left in the completed assembly for the addition of additional elements of the lead. The completed assembly can be stored on a spool in lengths of, for example, 500' or discrete lengths.

In multi-layer leads, the inner layer may be built as described above with respect to the mandrel process and stored on a spool or in discrete lengths, the mandrel for the inner layer being of a small diameter. A second or outer layer may then be assembled as described above with respect to the mandrel process, except the second mandrel is of a larger diameter as compared to the first mandrel. Once the second layer (i.e., outer layer) is completed, it may be pulled over the first layer (i.e., inner layer).

In some embodiments, the inner layer is assembled via any of the above described methods, and the outer layer assembly takes place by first pulling an outer PTFE layer over the assembled inner layer. The outer braid is then braided over the outer PTFE layer. The SPC wall material for the outer layer is then reflowed or molded over the outer braid and outer PTFE layer.

In one embodiment, the inner layer is a standard inner lead layer having, for example, a helical inner conductor coil surrounded by a PTFE liner. An outer layer with the imbedded braid, as described herein, could be pulled over the standard inner layer or assembled over the standard inner layer via any of the above-described methods.

At this point in the process, the conductor **100** may be laser ablated to expose the conductor **100** through the conductor insulation, if any, and the reflowed SPC wall material **162** to create a pathway that may be used to electrically couple the conductor **100** to the anchor electrode **85**. A crimp slug may be applied to the exposed conductor **100** in preparation for electrically connecting the conductor **100** and electrode **85**.

The shank **225** and its connected helical anchor electrode **85** may be inserted into the distal end of the inner layer assembly **155** and connected thereto. The crimp slug may then be laser welded to the helical anchor electrode **85** or the shank **225**, which is electrically connected to the helical anchor electrode **85**.

Generally speaking, a crimp slug may be attached to a conductor before or after the conductor insulation, if any, is removed. The form of a crimp slug may be open or closed, tubular or coiled, and/or circular. A conductor may be cut or left intact depending on the type of crimp slug used. This process may be repeated as many times as needed to attach the appropriate number of electrodes. Depending on where the electrode is located, the electrode may be a platinum band/

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ring, a half ring, a quarter ring, a coil, a helical active fixation anchor, and/or a sensor. The electrode may be attached to the crimp slug via laser welding.

After the electrode **85** has been attached to the crimp slug, any gaps around and under the electrode **85** are filled in with the appropriate material such as, OPTIM™, MedA, epoxy, etc. The proximal end of the conductor **100** and inner layer assembly **155** may then be coupled to respectively to the pin contact **55** and lead connector end **35**.

Once the inner layer assembly **155** is completed, the construction of the outer layer assembly **160** may be begun. As with the inner layer assembly **155**, the specific length of braid assembly **115** may be removed from the spool. This specific length of braid assembly **115** may then be pulled over an outermost liner layer **140**, which, as discussed above, may be PTFE or other applicable polymer materials. Once the braid assembly **115** extends about the outer circumferential surface **195** of the outermost liner layer **140**, SPC (which is also known as OPTIM™ and will act as the wall material **162**) may be reflowed or molded (e.g., LIM) about the braid assembly **115** and outermost liner layer **140** enclosed within the braid assembly **115**. Specifically, in one embodiment employing reflow, a SPC tube **162** may be pulled over the combined braid assembly **115** and liner layer **140**. A FEP jacket is then pulled over the SPC tube **162**, the braid **115**, and liner **140** and then subjected to reflow conditions to form the outer layer assembly **160**. The FEP jacket is then removed from the resulting outer layer assembly **160**.

At this point in the process, the conductors **105**, **110** may be laser ablated to expose the conductors **105**, **110** through the conductor insulation, if any, and the reflowed SPC wall material **162** to create a pathway that may be used to electrically couple the conductors **105**, **110** to the respective electrodes **80**, **82**. Crimp slugs may be applied to the exposed conductors **105**, **110** in preparation for electrically connecting the conductors **105**, **110** to their respective electrodes **80**, **82**.

As can be understood from FIGS. **3** and **8**, where the lead employs a shock coil **82** and may be a high voltage lead, the conductive path to the shock coil **82** may include multiple conductors **110** that, when combined, meet the electrical requirements for shocking while the lead body **50** still offers a reduced diameter on account of the configuration of the braid assembly **115** employed in the outer layer assembly **160**. Silicone, SPC or other materials may be added to the coil **82** to stabilize the coil **82** and create a non-tissue in-growth (“NTI”) surface on the coil **82**. The area adjacent the electrodes **80**, **82** may be filled in with a reflowed or molded SPC or other material to create an iso-diametric lead body **50**.

In some embodiments, once the entire lead body is constructed via any of the above described methods, the entire lead body or portions thereof may be heat-set to assume a desired configuration that may, for example, allow passive fixation features to bias within a vein for LV implantation in the case of a CRT lead. Also, such heat-setting may be used for strain relief.

At this point, in one embodiment, the outer layer assembly **160** is pulled over the completed inner layer assembly **155** such that the outer circumferential surface **205** of the inner layer assembly **155** abuts against the inner circumferential surface **200** of the outer layer assembly **160**. The crimp slugs of the respective conductors **105**, **110** may then be laser welded to the respective electrodes **80**, **82**. After the electrodes **80**, **82** have been attached to the crimp slugs, any gaps around and under the electrodes **80**, **82** are filled in with the appropriate material such as, OPTIM™, MedA, epoxy, etc. The proximal end of the conductors **105**, **110** and outer layer assembly **160** may then be coupled respectively to the ring

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contacts **60**, **61** and lead connector end **35**. In one embodiment, the resulting completed lead **10** may have a tubular body **50** with an braid-reinforced inner layer assembly **155** that is axially rotatable relative to an braid-reinforced outer layer assembly **160**, thereby allowing the inner layer assembly **155** to be rotated via the pin contact **55** to cause the helical anchor electrode **85** to extend or retract at the lead distal end **70**.

When the lead body **50** is manufactured on a continuous basis, the appropriate length of inner liner **130** may be selected depending on the type of lead **10** being constructed. The braid assembly **115** may then be braided over the outer circumferential surface **215** of the inner liner **130** in a continuous manner. If beneficial to the lead configuration and function, a variable pitch may be braided into the braid assembly **115** where desired during the braiding process. Once the braid assembly **115** is braided over the inner liner **130**, the SPC wall material **162**, crimp slugs, shank **225**, anchor **85** and electrical connections may be completed as discussed above with respect to the individual basis discussion, thereby forming the inner layer assembly **155**.

A braid assembly **115** is then braided onto the outer circumferential surface **195** of the outer liner layer **140**. Once the braid assembly **115** is braided over the outer liner **140**, the SPC wall material **162**, crimp slugs, shank **225**, anchor **85** and electrical connections may be completed as discussed above with respect to the individual basis discussion, thereby forming the outer layer assembly **160**. The inner layer assembly **155** is then placed within the outer layer assembly **160** as discussed above with respect to the individual basis discussion, thereby forming the complete lead body **50**. In one embodiment, the resulting lead body **50** has an inner braid-reinforced layer assembly **155** that is axially rotatable within an outer braid-reinforced layer assembly **160** to cause a helical anchor electrode **85** to extend/retract from the lead distal tip.

In some embodiments, the braid assembly **115** of the outer layer assembly **160** may be left exposed in certain selected discrete areas along the length of the lead body **50**. These discrete areas of exposed braid assembly **115** may function as tissue in-growth locations where tissue may in-grow into the exposed braid assembly to facilitate chronic anchoring of the lead body **50** at the location of the implantation of the lead **10**.

In some embodiments, one or more of the conductors **105** may instead be a tubular lumen extending distally from the lead proximal end. Such a lumen or lumens **105**, although forming a portion of the braid assembly **115**, may be used to transfer something other than current through the lead body **50**. For example, such a lumen **105** of the braid assembly **115** may be used to deliver air, liquid, drugs, etc. from a proximal end of the lead to a location on the lead near the lead distal end.

In some embodiments, the helix anchor **85** at the lead distal end is not extendable/retractable relative to the lead distal end. Instead, the helix anchor **85** is fixed in an extended configuration and the entire lead body is rotated to imbedded the helix anchor **85** in cardiac tissue. Thus, in such fixed helix anchor embodiments, the inner layer of the lead body is not configured to rotate within the outer layer of the lead body or, alternatively, the lead body has a single layer.

The braid-reinforced layer assemblies **155**, **160** used to form the lead tubular body **50** offer a number of advantages over known lead body configurations. For example, in some embodiments, the such braid-reinforced layer assemblies **155** may be substituted for helically wound central coils that are employed to extend/retract helical anchors; providing one-to-one torqueability, reduced manufacturing costs, and

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improved and more consistent flexibility as compared to leads employing the helically wound central coils known in the art.

The braid-reinforced layer assemblies **155**, **160** allow greater flexibility in positioning an electrode along the lead body as the conductors of the assemblies **155**, **160** are more readily located and accessible, as compared to lead configurations known in the art. As a result, the manufacturing of multi-electrode leads having, for example, 1-32 or more electrodes is made more feasible.

Since the conductors are imbedded in the material of the tubular wall, the French size made possible via the braid-reinforced layer assemblies **155**, **160** may be substantially less than other leads commonly known in the art.

The leads disclosed herein are applicable to both cardiology applications and other medical areas, including neurological.

For a discussion regarding crimp slug configurations that can securely coupled to a variety of types of electrical conductors used in leads, including the helically wound conductors **100**, **105**, **110** of the above-described braided layers, reference is first made to FIGS. **11A-11C**. FIG. **11A** is an isometric view of a zip tie type crimp slug **300**. FIGS. **11B** and **11C** are, respectively, plan and side views of the crimp slug **300** of FIG. **11A**.

As shown in FIGS. **11A-11C**, in one embodiment, the crimp slug **300** includes a ribbon or tail **305** and a collar **310**. The tail **305** has a substantial length as compared to the size of the collar **310**, extends from the collar **310** on one end, and terminates on the other end in the form of a tip or free end **315**. The collar **310** includes a hole **320** defined therein and extends relative to the tail **305** such that the faces **325** of the collar **310** are generally transverse to the tail **310**.

In one embodiment, the tail **305** includes an inner face **330** that is a generally flush extension of the arcuate inner surface **335** of the hole **320** and is similarly arcuate. The tail **305** includes an outer face **340** that is a generally flush extension of the arcuate outer surface **345** of the collar **310** and is similarly arcuate.

In one embodiment, the tail **305** extends between approximately 0.05" and approximately 0.5" from the adjacent collar face **325**. The tail **305** has a transverse width of between approximately 0.005" and approximately 0.02". The tail **305** has a thickness of between approximately 0.001" and approximately 0.008". The collar **310** has an outer diameter of between approximately 0.01" and approximately 0.04". The collar **310** has a face to face thickness of between approximately 0.002" and approximately 0.01". The hole **320** has a diameter of between approximately 0.005" and approximately 0.02". The crimp slug **300** is formed of an electrically conductive material, such as, for example, platinum-iridium alloy, platinum, MP35N, or etc.

The crimp slug **300** depicted in FIGS. **11A-11C** is advantageously configured such that it may be attached to a cable or a solid filament routed in either a wound or straight configuration. Even more advantageously, the crimp slug **300** can be coupled to such a cable or solid filament imbedded in a polymer (e.g., SPC) and only exposed in a specific region, as may be the case with conductors **100**, **105**, **110** of the embodiments of the lead body described above with respect to FIGS. **1-10**.

For a discussion of a method of preparing the lead body **50** for the coupling of the crimp slug **300** of FIGS. **11A-11C** to a conductor **100** in the lead body, reference is made to FIGS. **12A-12C**. FIG. **12A** is a plan view of a portion of a lead tubular body **50** with a conductor **100** helically routed about a liner layer **130** and imbedded in the polymer material **162**, the helically routed conductor **100** and polymer material **162**

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forming the reinforced layer **135**. FIGS. **12B** and **12C** are, respectively, cross sections of the lead tubular body **50** as taken along section line **12B-12B** and section line **12C-12C** in FIG. **12A**.

As shown in FIGS. **12A-12C**, the polymer material **162** of the reinforced layer **135** is removed in the vicinity of a desired conductor access location to form a recessed ring **350** about the outer circumference of the tubular body **50** and a window **355** in the recessed ring **350** that extends in general alignment with the helically wound conductor **100** revealed by the window **355**. The removal of the polymer material **162** may be accomplished via a variety of methods, including, for example, laser ablation. The ablation or other removal method may also be used to remove any electrical jacket that may be present about the conductor **100**, thereby reveal the electrically conductive core of the conductor **100**, as shown in FIGS. **12A-12C**.

In one embodiment, the polymer material **162** may be masked during reflow to result in voids or openings that may be used to access the conductors or allow for the addition of conductive elements to the conductors.

FIG. **13A** is a view of the tubular body **50** similar to the view depicted in FIG. **12A** and illustrating the beginning of the process of coupling the crimp slug **300** to the conductor **100** exposed in the window **355**. Specifically, as shown in FIG. **13A**, the tail **305** of the crimp **300** is inserted under the exposed conductor **100** by working the tip **315** of the crimp tail **305** under the conductor **100** and then further sliding the crimp tail **305** under the conductor **100** to cause the crimp collar **310** to move towards the conductor **100**. As shown in FIG. **13B**, which is generally the same view of the tubular body **50** depicted in FIG. **13A**, the crimp tail tip **315**, which is wrapped around the exposed conductor **100**, is inserted through the crimp collar hole **320**. The crimp **300** now forms a loop **360** about the exposed conductor **100**. The crimp tail tip **315** is grasped (e.g., via a crimp tool) and pulled as the crimp collar **310** pushed down against the cable, cinching the crimp tail **305** down tight on the conductor **100**. The crimp collar **310** can then be crimped down on the cinched tight tail **305** to hold the tail **305** tightly cinched about the conductor **100**, as shown in FIG. **13C-13E**. A final crimp of the collar may be applied to further lock the collar in position about the tightly cinched tail.

Once the crimp **300** is fully cinched down on the conductor **100** and fully crimped to lock the crimp **300** in place, a ring electrode **80** may be positioned on the lead body and coupled to the crimp **300**. For example, as depicted in FIG. **14A**, which is an isometric of a split ring electrode **80**, an electrode **80** configured to be coupled to the crimp **300** may have an overall ring shape that includes a cylindrical wall **390** with an outer circumferential surface **400**, an inner circumferential surface **405**, a first end edge **410**, a second end edge **415**, and a slot, cut or split **420** extending through the wall **390** generally parallel to the axis of the electrode **80**. The slot **420** is defined by opposed edges **425**. Each opposed edge **425** includes a notch **430**.

The ring electrode **80**, when in an expanded or split condition as shown in FIG. **14A** with the opposed edges **425** spaced apart from each other, has an inner diameter that is greater than the outer diameter of the lead body **50**. Thus, when the ring electrode **80** is in the split condition shown in FIG. **14A**, the lead tubular body **50** can be threaded through the ring electrode to cause the ring electrode to be positioned over the recessed ring **350** formed in the lead body (see FIG. **13C**), the notches **430** being positioned on each side of the crimp **300**. As shown in FIG. **14B**, which is a view of the lead tubular body similar to that of FIG. **13B**, the ring electrode **80**

can then be transitioned to a contracted or non-split condition by pressing the opposed edges 425 of the ring electrode together such that the inner diameter of the ring electrode matches the outer diameter of the lead tubular body 50 at the recessed ring 350 and the outer diameter of the ring electrode 80 matches the outer diameter of the lead tubular body proximal and distal of the recessed ring 350. Thus, the ring electrode 80 in the non-split condition resides with the recessed ring 350 in the tubular body 50 and the outer circumferential surface 400 of the ring electrode 80 is generally flush with the outer circumferential surface of the lead body 50.

As indicated in FIG. 14B, when the ring electrode is positioned in the recessed ring 350 in a non-expanded condition with the opposed edges 425 abutting or nearly abutting each other and the crimp 300 is located between the notches 430, the notches 430 form a window or opening 435 in the wall of the ring electrode 80 through which the crimp 300 extends. As illustrated in FIG. 14C, a weld 440 can be formed at the location of the crimp and window to mechanically and electrically couple the crimp to the ring electrode and maintain the ring electrode in the non-expanded condition. Additional welds can be formed along the opposed edges 425 if it is desired to close off the seam formed by the opposed edges 425. It should be noted that although in some embodiments the crimp 300 projects into the window 435, in other embodiments this may not be the case, the window simply serving for visualization during welding, the crimp simply being located below the window, but not projecting into the window.

The split ring electrode 80 of FIGS. 14A-14C combined with an ablated recessed ring in the lead body provides a novel way of creating an isodiametric lead body. While the split ring electrode works well with the ribbon type crimps discussed above, the split ring electrode can be used to attach to an assortment of more traditional crimps. The preferred configuration is to have a ribbon/post come through the split crimp window. However, the window can also just be used for visualization during welding, allowing the concept to be used in conjunction with almost any crimp currently used in the industry.

Other ring electrode configurations may be employed with the crimp 300. For example, as depicted in FIG. 15A, which is an isometric view of a notched ring electrode 80, an electrode 80 configured to be coupled to the crimp 300 may have an overall ring shape that includes a cylindrical wall 390 with an outer circumferential surface 400, an inner circumferential surface 405, a first end edge 410, a second end edge 415, and a notch 445 extending through the wall 390 oblique to the axis of the electrode 80. The notch 445 is defined in one of the end edges 410 and extends in the direction of the opposite edge for a portion of the length of the ring electrode.

As shown in FIG. 15B, which is a view of the tubular body 50 similar to that of FIG. 14B, the ring electrode of FIG. 15A may be supported on the tubular body with the notch 445 positioned such that the crimp 300 is located within the notch 445. The notch 445 and crimp 300 can be welded together to form a weld similar to that discussed above with respect to FIG. 14C.

For a discussion regarding another crimp slug configuration, reference is now made to FIGS. 16A-16D. FIG. 16A is a plan view of another zip tie type crimp slug 300 in a flat pattern state. FIG. 16B is an isometric view of the zip tie type crimp slug 300 of FIG. 16A in a formed condition. FIGS. 16C and 16D are, respectively, isometric and side views of the crimp slug 300 of FIG. 16B in a looped state.

As shown in FIGS. 16A-16B, in one embodiment, the crimp slug 300 includes a ribbon or tail 305 and a slot head 480. The tail 305 has a substantial length as compared to the

size of the slot head 480, extends from the slot head 480 on one end, and terminates on the other end in the form of a tip or free end 315. The slot head includes a slot 485 defined therein, the slot 485 extending transverse to the tail 310.

As shown in FIGS. 16B-16D, the slot head 480 includes two opposed half-cylinder portions 490, each half-cylinder portion 490 sharing a common longitudinal merged or joined wall portion 495 and each having a free longitudinal wall edge 500. The tail 305 extends from free wall edge 500 of one of the half-cylinder portions 490, and the slot 485 is defined in the center of the trough of the other half-cylinder portion 490. The slot 485 extends generally parallel to the longitudinal axis of the half-cylinder portion 490 in which the slot is defined. Since the half-cylinder portions 490 are opposed and share a common wall portion 495, the slot head 480 has a s-shaped side edges, as can be understood from FIGS. 16B-16D.

In one embodiment, the tail 305 includes an inner face 330 that is a generally flush extension of the arcuate inner surface of the trough of the half-cylindrical portion 490 from which the tail extends. The tail 305 includes an outer face 340 that is a generally flush extension of the arcuate outer surface of the half-cylindrical portion 490 from which the tail extends.

In one embodiment, the tail 305 extends between approximately 0.1" and approximately 0.5" from the free wall edge 500 from which the tail extends. The tail 305 has a transverse width of between approximately 0.005" and approximately 0.02". The tail 305 has a thickness of between approximately 0.002" and approximately 0.01". Each half-cylinder portion 490 has an outer diameter of between approximately 0.01" and approximately 0.04". Each half-cylinder portion 490 has an inner diameter of between approximately 0.003" and approximately 0.02". The slot head 480 has a length of between approximately 0.01" and approximately 0.1". The slot 485 has a width of between approximately 0.002" and approximately 0.012" and a length of between approximately 0.005" and approximately 0.025". The crimp slug 300 is formed of an electrically conductive material, such as, for example, platinum-iridium alloy, platinum, MP35N, or etc.

The crimp slug 300 depicted in FIGS. 16A-16D offers the same advantages of the crimp 300 depicted in FIGS. 11A-11C. Also, as can be understood from a comparison of the FIG. 16C to FIG. 13C, the crimp slug 300 of FIGS. 16A-16D may be secured to the conductor 100 and a ring electrode 80 in the same manner as the crimp slug 300 in FIGS. 11A-15B. Specifically, the tail 305 is looped around the conductor 100, threaded through the slot 485, and then cinched tight about the conductor 100. The slot head 480 is then crimped down on the tail to maintain the crimp slug 300 tightly cinched down on the conductor. The ring electrode can then be placed about the lead tubular body and welded to the crimp slug.

In one embodiment, as shown in FIGS. 17A and 17B, which are, respectively, isometric and plan views of a lead body, the crimp slug 300 is in the form of a ribbon or strip 520 that is inserted under the exposed conductor 100, the free ends 525 of the ribbon 520 being brought together and pulled such that the ribbon 520 is wrapped tightly about the exposed conductor 100. Specifically, the ribbon doubles back on itself and slides in to a slot 445 in the notched ring electrode 80 of FIG. 15A or a window 435 of the split ring electrode 80 of FIG. 14A. A half-cylinder shaped tool 535 having an arcuate inner surface that has a diameter that generally matches the outer diameter of the lead body may be employed to crimp the ribbon about the conductor 100. The tool 535 may have a slot or notch 535 similar, but opposite to the slot or notch 445 in the ring electrode 80. Pulling on the ribbon free ends 525 and pushing with the tool 535 can cinch and crimp the ribbon 520

tightly down on the conductor **100**. The ribbon can then be spot welded within the ring electrode notch **445**.

The ribbon is formed of an electrically conductive material similar to that discussed above with respect to FIGS. **11A-11C** and **16A-16D** and may have dimensions similar to those discussed above with respect to the tail **305**.

The embodiments of the crimp **300** discussed above with respect to FIGS. **11A-17B** may be considered to have a tail portion (alternatively referred to as a ribbon portion) that can be slid under a conductor **100** imbedded in a layer of the lead body. These crimps can be constructed from a flat pattern or a tube and can take on many different configurations while still achieving the same general crimp concept. Also, any of these tail or ribbon equipped crimps **300** of FIGS. **11A-17B** can be attached to two or more conductors **100** running next to each other (e.g., for the purposes of redundancy).

In one embodiment, as depicted in FIG. **17C**, which is a transverse cross section of the lead body **50** at a location of an alternative version of the ribbon equipped crimp **300** of FIGS. **17A-17B**, the crimp **300** may include a collar **310** that is separate from the ribbon portion **525** of the crimp **300**. Once the ribbon portion **525** is tightly wrapped about the conductor **100**, the collar **310** can be slid down over the ribbon portion **525** and then crimped down on the ribbon portion **525**. The ring electrode **350** can then be placed over the collar **310** such that the ribbon portion **525** extends from opening (e.g., slot) in the ring electrode and the collar **310** is in intimate contact with the inner surface of the ring electrode. The ribbon portion and collar can then be welded to the ring electrode.

The process of wrapping the ribbon portion around the conductor **100**, cinching the crimp tight, and crimping, results in mechanical deformation between the crimp and the conductor. This ensures a reliable electrical and mechanical connection between the conductor and the crimp, which is then welded or otherwise mechanically and electrically coupled to the ring electrode.

These crimps **300** may be employed to couple conductors **100** to ring electrodes **80** that are in the form of split-ring electrodes, solid ring electrodes, half-ring electrodes, etc. These crimps **300** can also be used to couple the conductors **100** to shock coils **82** in the form of spot end or solid ring end shock coils. Finally, these crimps **300** can be used to couple conductors **100** to additional features, such as, for example, sensors or chips.

These crimps **300** are particularly useful when attaching to a straight or wound conductor **100** when the ends of the conductor are constrained or locked into a polymer matrix of a lead body. The ribbon equipped crimps **300** are particularly well suited for attachment to a wound conductor **100** because only a narrow ribbon **305** can be slid under the imbedded conductor **100**. Also, the ribbon **305** facilitates the easy and secure coupling of the crimp to a helically routed conductor.

FIG. **18A** is an isometric view of another embodiment of the crimp slug **30**. As shown in FIG. **18A**, the crimp **300** includes a tail **590** extending from a cylindrical head **600**. The cylindrical head **600** includes a longitudinal slot **605** and a transverse slot **610**. The longitudinal slot **605** is generally parallel to the longitudinal axis of the cylindrical head **600** and defines two longitudinal edges **615** in the wall of the head **600**. The tail **590** extends from one of the edges **615**, and the transverse slot **610** begins at the other edge **615**. The tail **590** and transverse slot **610** are centered on the head **600** with respect to the length of the head.

As illustrated in FIG. **18A**, the exposed conductor **100** is received in the trough of the cylindrical head **600**. Specifically, the edge **615** in which the transverse slot **610** is defined

is inserted under the exposed conductor **100** to cause the conductor to be received in the trough of the head **600**.

As indicated in FIGS. **18B** and **18C**, which are, respectively, top and bottom isometric views of a half-cylinder shaped tool **535** for use in crimping the crimp **300** on an exposed conductor **100**, the tool **535** has an arcuate inner surface **630** that has diameter that generally matches the outer diameter of the lead body. A helically routed groove or recess **635** is defined in the arcuate inner surface **630**. An opening **640** extends through the wall **645** of the tool **535** from the recess **635**. The tail **590** of the crimp **300** extends through the opening **640** when the cylindrical head **600** of the crimp **300** is received in the opening **640**.

Pulling on the tail and pushing with the tool **530** can cinch and crimp the ribbon cylindrical head **600** tightly down on the conductor **100**. The tail **590** can then be spot welded within the ring electrode notch **445** or window **435**.

In one embodiment, the tail **590** extends between approximately 0.01" and approximately 0.2" from the edge **615** from which the tail extends. The tail **590** has a transverse width of between approximately 0.002" and approximately 0.02". The tail **590** has a thickness of between approximately 0.002" and approximately 0.01". The cylinder head **600** has an outer diameter of between approximately 0.012" and approximately 0.03". The cylinder head **600** has an inner diameter of between approximately 0.004" and approximately 0.015". The cylinder head **600** has a length of between approximately 0.02" and approximately 0.1". The longitudinal slot **605** has a width of between approximately 0.003" and approximately 0.02" and a length of between approximately 0.02" and approximately 0.1". The transverse slot **610** has a width of between approximately 0.003" and approximately 0.022" and a length of between approximately 0.01" and approximately 0.04". The crimp slug **300** is formed of an electrically conductive material, such as, for example, platinum-iridium alloy, platinum, MP35N, or etc.

FIG. **19** is an isometric view of a side loader crimp slug **300**. As depicted in FIG. **19**, the crimp **300** includes a cylindrical head **675** with a longitudinal slot **680** that defines two opposed edges **685**. One edge **685** includes two end projections **690** separated by a single central recess **695**. The other edge **685** includes a single centered projection **700**. The two edges complement each other in that when the edges **685** are forced together when the crimp **300** is crimped down on an exposed conductor **100** extending through the cylindrical head **675**, the single centered projection **700** is received in the single central recess **695**, and the end projections **690** are received in the open spaces **705** adjacent the centered projection **700**.

As illustrated in FIG. **19**, the exposed conductor **100** is received in the trough of the cylindrical head **675**. Specifically, one of the edges **685** is inserted under the exposed conductor **100** to cause the conductor to be received in the trough of the head **675**.

The crimp **300** could be added to the conductor before the conductor is wound into the lead body as described above with respect to FIGS. **1-10**. A hole **710** in the crimp **300** could then be used to add a post to the crimp. The post could be added by stamping a flat pattern and welding the post into the hole.

Alternatively, the crimp **300** could be made as shown and then crimped onto the conductor subsequent to the conductor being wound into the body as described above with respect to FIGS. **1-10**. After crimping a post could be placed in the hole and welded on. This post, similar to the tails described above, would be used to aid in welding and alignment to a slot or window in the ring electrode.

In other embodiments, the crimp **300** will not have the hole **710** depicted in FIG. **19**. The crimp is instead welded to the ring electrode via welding and direct intimate contact between the outer surface of the crimp and the interior of the ring electrode.

FIGS. **20A** and **20B**, which are, respectively, isometric and side views of another crimp slug **300**. As shown in FIGS. **20A** and **20B**, the crimp slug **300** includes a generally cylindrical side surface **730**, a planar upper surface **732**, and a semi-sloped bottom surface **735**. A pair of notches or recesses **740** are defined in opposite sides of the cylindrical side surface **730**, the recesses being configured to be engaged by a crimping tool. A notch or recess **745** is defined in the bottom surface **735**, the recess being configured to receive a conductor **100**.

FIG. **20C** is a side view of a portion of a lead body **50**, wherein the crimp slug **300** of FIGS. **20A** and **20B** is coupled to a conductor **100**. As depicted in FIG. **20C**, the conductor **100** is received in the bottom recess **745**, and a crimp tool is applied to the side recesses **740** to crimp the bottom recess **745**, causing the crimp slug **300** to be coupled to the conductor **100**. The crimp slug **300** can be attached to a pre-wound conductor, access to the conductor **100** being achieved by ablating a window. Alternatively, the crimp slug **300** can be added to the conductor **100** prior to the addition of the polymer layer in which the conductor ends up being imbedded. Regardless of when the crimp slug **300** is attached to the conductor, the crimp can then be welded to a split ring electrode or a slotted ring electrode.

FIGS. **21A** and **21B**, which are, respectively, isometric and side views of another crimp slug **300**. As illustrated in FIGS. **21A** and **21B**, the crimp slug **300** includes a generally spherical outer surface **750** and a notch or recess **755** defined in the spherical outer surface **750**, the recess being configured to receive a conductor **100**.

Similar to the crimp **300** of FIGS. **20A-20C**, the crimp **300** of FIGS. **21A-21B** can be coupled to a conductor **100**. Specifically, the conductor **100** is received in the recess **755**, and a crimp tool is applied to the outer spherical surface **750** to crimp the recess **755**, causing the crimp slug **300** to be coupled to the conductor **100**. The crimp slug **300** can be attached to a pre-wound conductor, access to the conductor **100** being achieved by ablating a window. Alternatively, the crimp slug **300** can be added to the conductor **100** prior to the addition of the polymer layer in which the conductor ends up being imbedded. Regardless of when the crimp slug **300** is attached to the conductor, the crimp can then be welded to a split ring electrode or a slotted ring electrode.

As indicated in FIG. **22**, which is a plan view of a twisted crimp **300** on a conductor **100**, the crimp slug **300** may be in the form of a micro wire or coil **760** twisted onto the conductor **100** and then crimped flat on the conductor. The twisted crimp **300** can then be welded to a ring electrode **80**.

Most, if not all, of the above-described crimp slugs **300** can be added to the conductor **100** subsequent to the assembly of the conductor into the lead body **50**. Also, most, if not all, of the above-described crimp slugs **300** can be added to the conductor **100** prior to the conductor **100** being assembled into the lead body **10**, for example, where the crimp slugs **300** are applied to the conductor **100** and the crimp slug equipped conductor is stored in discrete lengths or in bulk on a spool until needed for assembly into the lead body **50**. Also, in another embodiment, the crimp slugs **300** may be added to the conductor **100** during the manufacture of the lead body **50** immediately before the conductor **100** is wound into the lead body.

The following crimp slugs **300** are especially useful in the context of applying the crimp slugs **300** to a conductor **100**

prior to the conductor **100** being assembled into the lead body **50**. Specifically, the crimps **300** discussed below are attached to the conductor **100** and the crimp equipped conductor **100** is stored in discrete lengths or in bulk on spools until needed for assembly into a lead body. For example, when assembling the lead body **50** depicted in FIG. **4**, a conductor **100** with crimps **300** already mounted along the length of the conductor **100** is removed from a spool and wound about the inner liner **130**.

As can be understood from FIGS. **23A** and **23B**, which are, respectively, a side view of a lead body **50** and an enlarged side view of the same lead body at a location of a crimp **300**, in the context of preassembling the crimps **300** onto the conductor **100** and storing the conductor in discrete lengths or on a spool, the crimps **300** can be added at an evenly spaced defined distance on a conductor **100**. The spacing of the crimps **300** on the conductors **100** could be such that when multiple conductors are wound onto the liner **130**, the crimp patterns are appropriately offset to create a specified spacing between the crimps. For example, as indicated in FIG. **23A**, four conductors **100**, **105**, **110**, **111** are wound about the liner **130** and the crimps **300** on the conductors are spaced such that the spacing **X** between adjacent crimps **300** is approximately 15 mm apart, the pattern repeating approximately every 90 cm.

FIGS. **24A** and **24B** are, respectively, a plan view of a helical wound crimp **300** and a plan view of the same crimp **300** mounted on a conductor **100**. As indicated in FIGS. **24A** and **24B**, such a helical wound crimp **300** may have coils **800** with a variable pitch. Specifically, part of the crimp **300** has a tight pitch region **805** that can act as a strong location for welding to a ring electrode and an open pitch region **810** that can act as a conformal strain relief. In one embodiment, the coils **800** of the tight pitch region **805** is welded to the ring electrode **80**. In another embodiment, a portion of the crimp **300** is welded to the ring electrode **80**, wherein the portion of the crimp **300** is a coil **800** that is pulled outward to form a tab to be welded to the electrode or an end of the wire forming the coils **80** is pulled outward to form a tab to be welded to the electrode. The resulting tab could be welded to the slot in the ring electrode, similar to methods described above.

To mount the helical crimp **300** on the conductor **100**, the conductor is threaded through the helical crimp **300** when the helical crimp is in a cylindrical shape. Once positioned as desired, the helical crimp **300** is crimped onto the conductor **100** to cause the crimp to conform to the conductor.

FIGS. **25A-25C** illustrate, respectively, side, inner and outer views of a helically shaped crimp **300**. As can be understood from FIGS. **25A-25C**, the crimp **300** is a solid tube that is helically shaped. The helical crimp **300** of FIGS. **25A-25C** would work similar to the helical spring crimp **300** of FIGS. **24A-24B**. Specifically, as can be understood from FIGS. **25D-25E**, which are, respectively, the crimp **300** on a conductor and a crimp-equipped conductor assembled into a lead body, the conductor **100** would be fed through the helical crimp **300**. The crimp **300** would then be crimped onto the conductor **100** such that the crimp **100** would match the natural pitch of the final wound cable. The helical crimp outside diameter would match the inside diameter of the ring electrode **80**, creating a large surface for welding. The crimp **300** would be welded to a ring electrode **80** through a hole **815** for visualization in the crimp **300**.

All crimp concepts disclosed herein apply to conductors that are solid wire or multi-filar conductors and conductors that are wound or braided.

Although the present invention has been described with reference to preferred embodiments, persons skilled in the art

will recognize that changes may be made in form and detail without departing from the spirit and scope of the invention.

What is claimed is:

1. An implantable medical lead comprising:

a longitudinally extending body having a distal end and a proximal end; 5

an electrode on the body near the distal end;

a lead connector end operably coupled to the proximal end of the body;

a tubular braid arrangement having an electrical conductor braided with an electrical nonconductor; 10

a crimp slug comprising a spherical outer surface and a recess formed in the spherical outer surface, the conductor received in the recess, a crimp tool applied to the spherical outer surface to crimp the recess and causing the crimp slug to be electrically and mechanically coupled to the electrode. 15

2. The lead of claim 1, wherein the crimp slug is welded to the electrode to be electrically and mechanically coupled to the electrode. 20

3. The lead of claim 1, wherein the electrode is a ring electrode.

4. The lead of claim 3, wherein the ring electrode is a split ring electrode.

5. The lead of claim 3, wherein the ring electrode is a slotted ring electrode. 25

6. The lead of claim 1, wherein the electrode is a shock electrode.

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