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**Peng et al.**

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(54) **ZOOM LENS AND IMAGING DEVICE USING SAME**

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**G02B 15/14** (2006.01)

(52) **U.S. Cl.**  
USPC ..... **359/687**; 359/683; 359/684; 359/685;  
359/686; 359/740; 359/771; 359/774

(58) **Field of Classification Search**  
USPC ..... 359/683–687, 740, 771, 774  
See application file for complete search history.

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*Primary Examiner* — Evelyn A. Lester

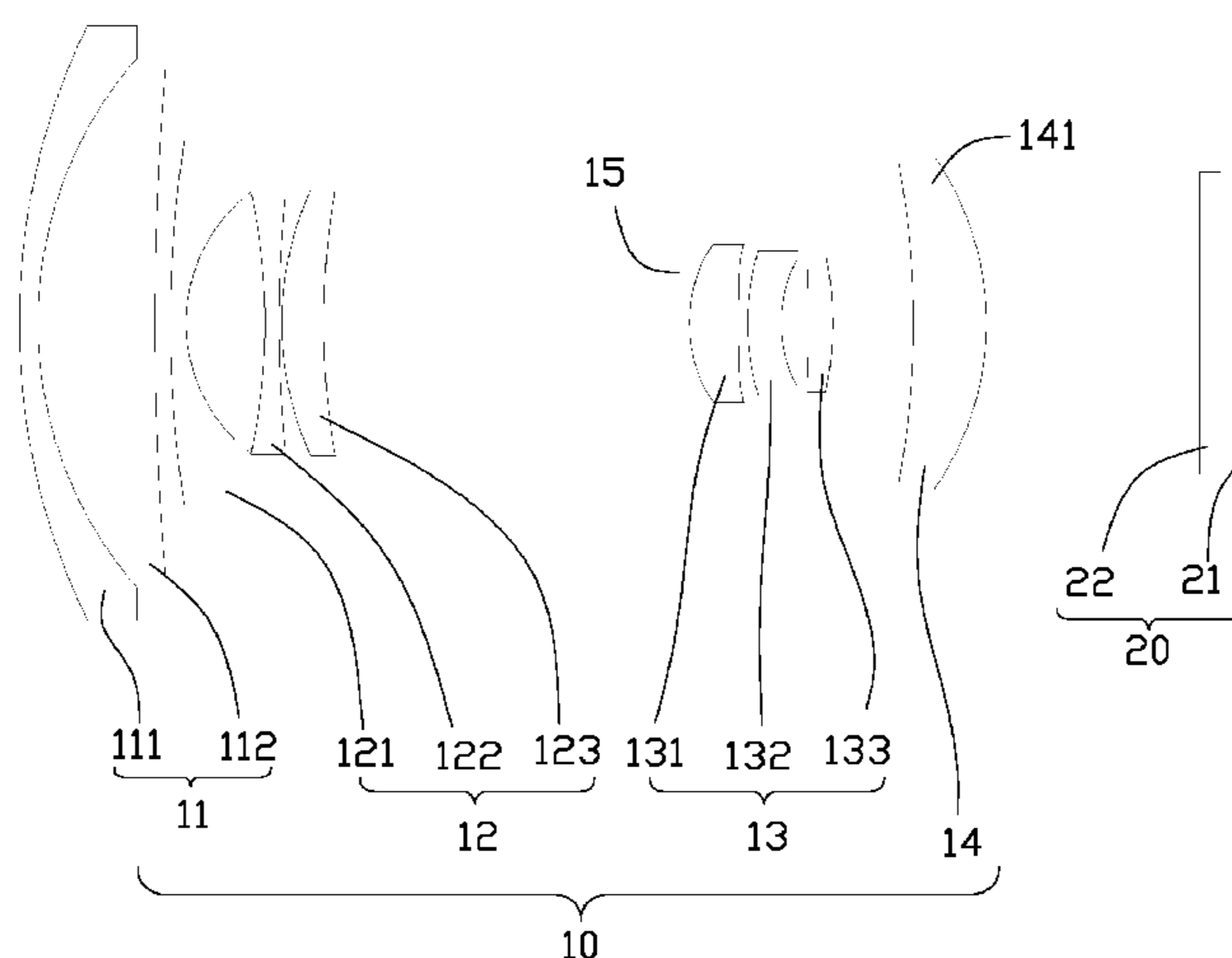
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(57) **ABSTRACT**

Provided is a zoom lens for imaging an object on an imaging surface. The zoom lens includes, in the order from an object side to an image side thereof, a first lens group with positive refraction power, a second lens group with negative refraction power, a third lens group with positive refraction power, and a fourth lens group with positive refraction power. The first lens group includes a first surface. The zoom lens satisfies the formula:  $0.15 < |L3|/Lt < 0.25$ , where L3 is a distance of the movement of the third lens group along an optical axis of the zoom lens when the zoom lens is switched between a wide-angle state and a telephoto state, and Lt is a distance from the first surface to the imaging surface.

**20 Claims, 16 Drawing Sheets**

100 →



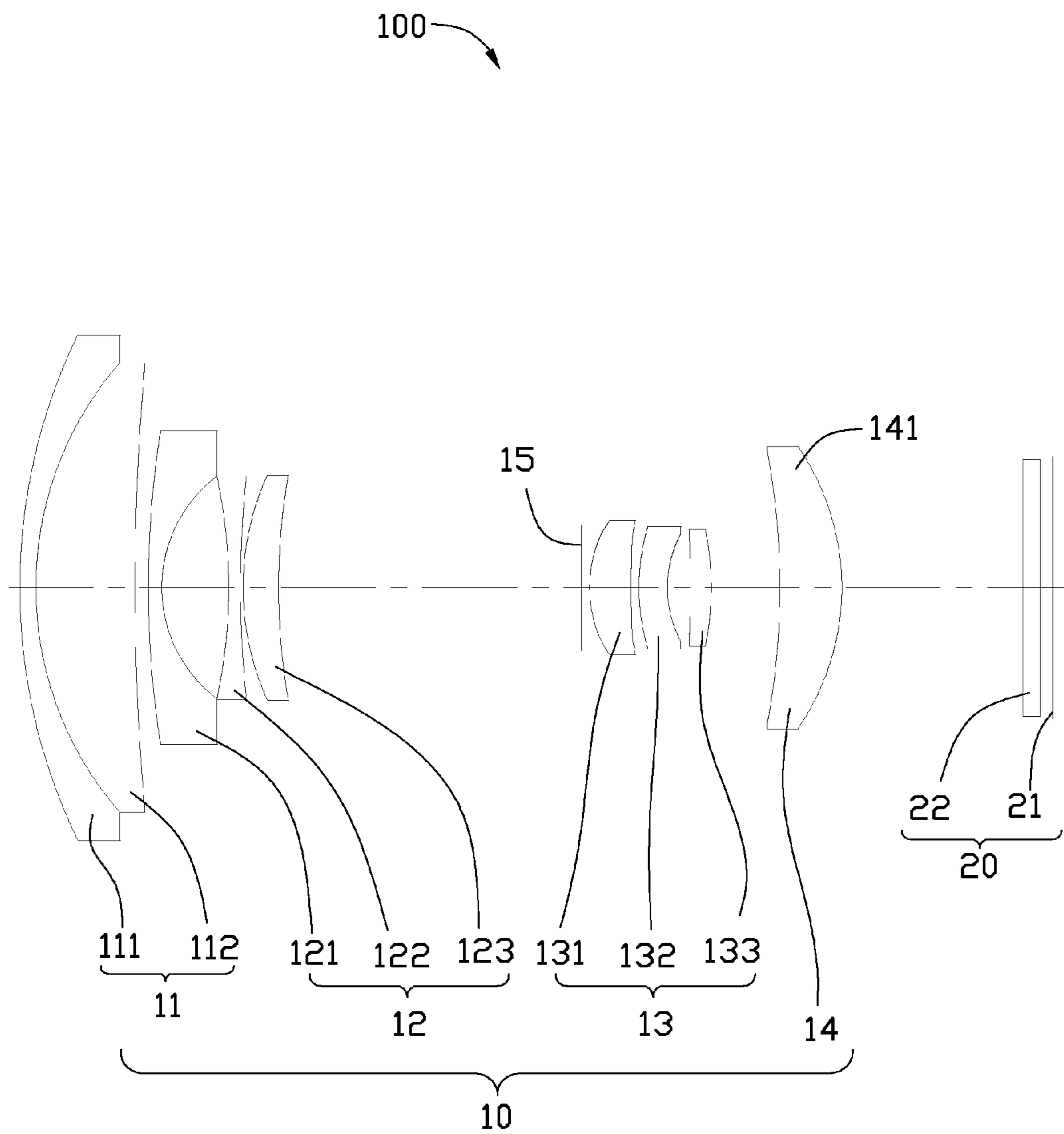


FIG. 1

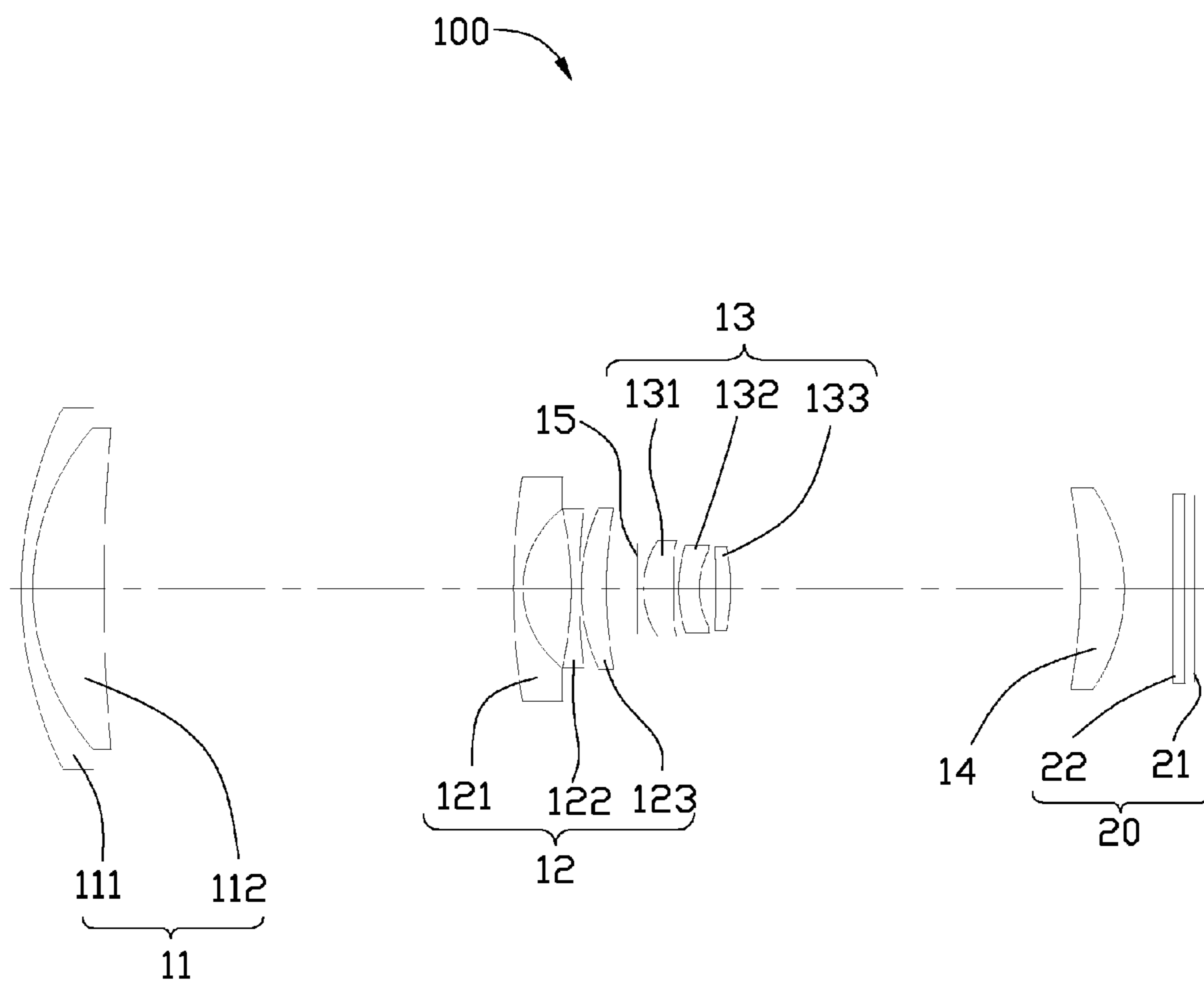


FIG. 2

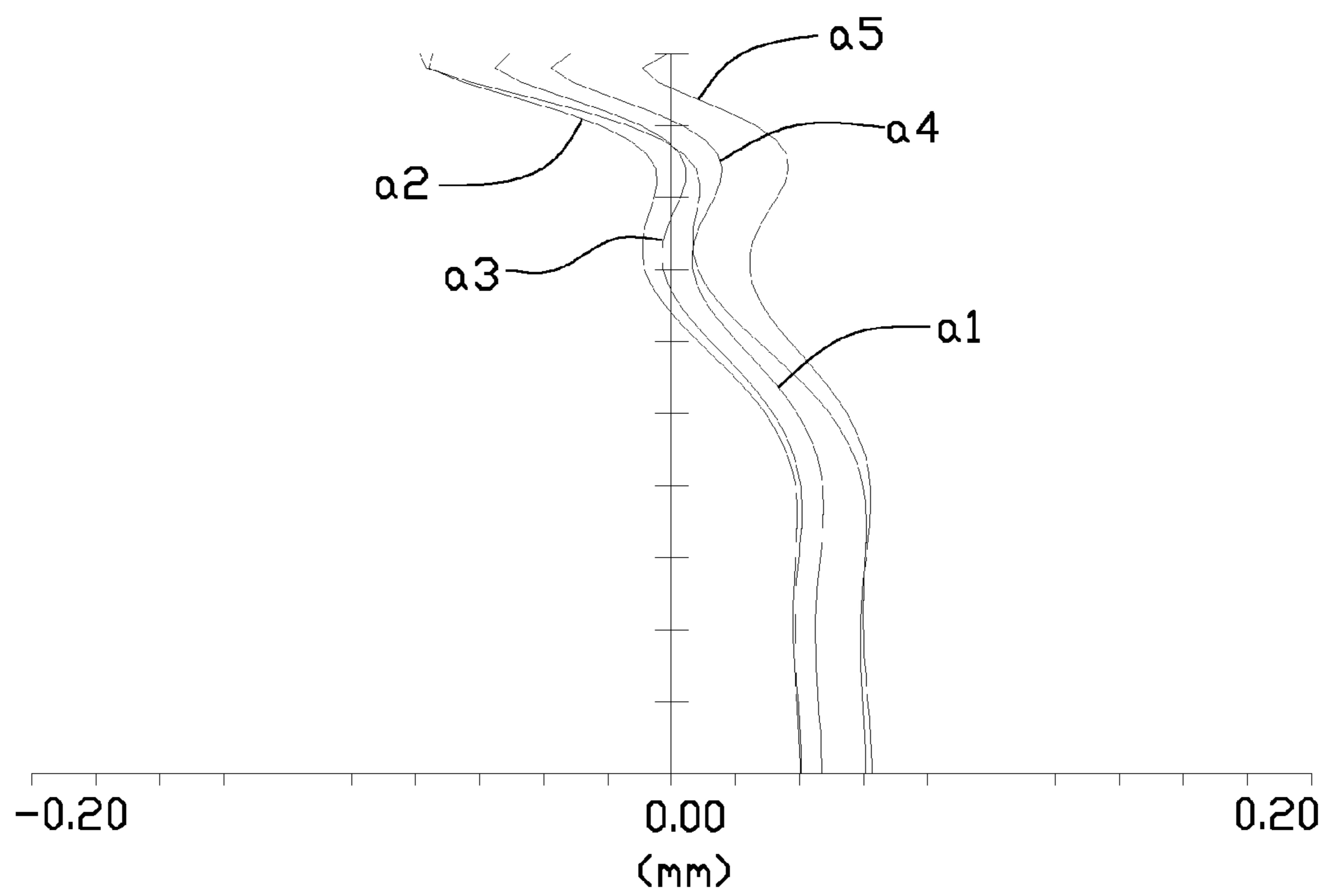


FIG. 3

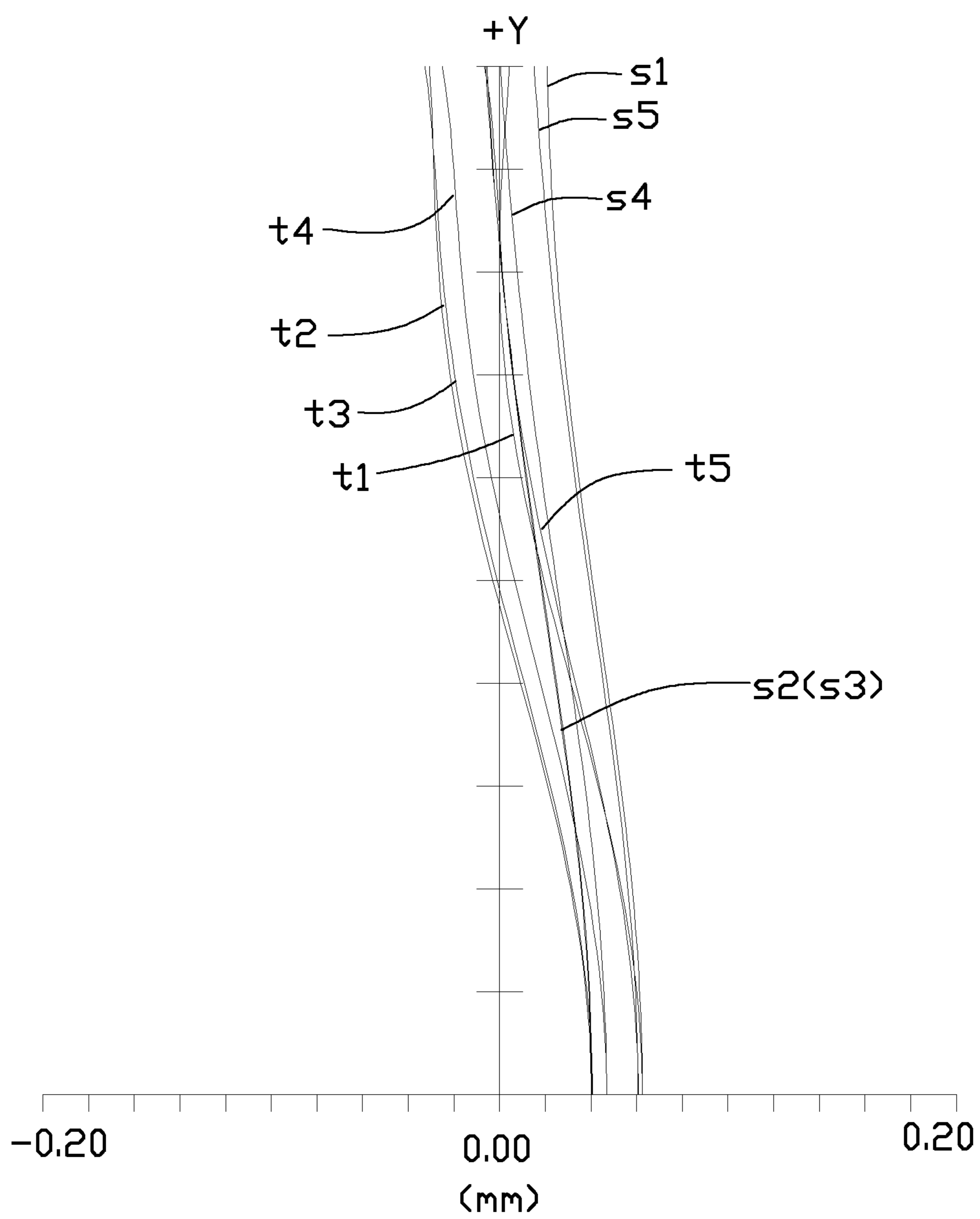


FIG. 4

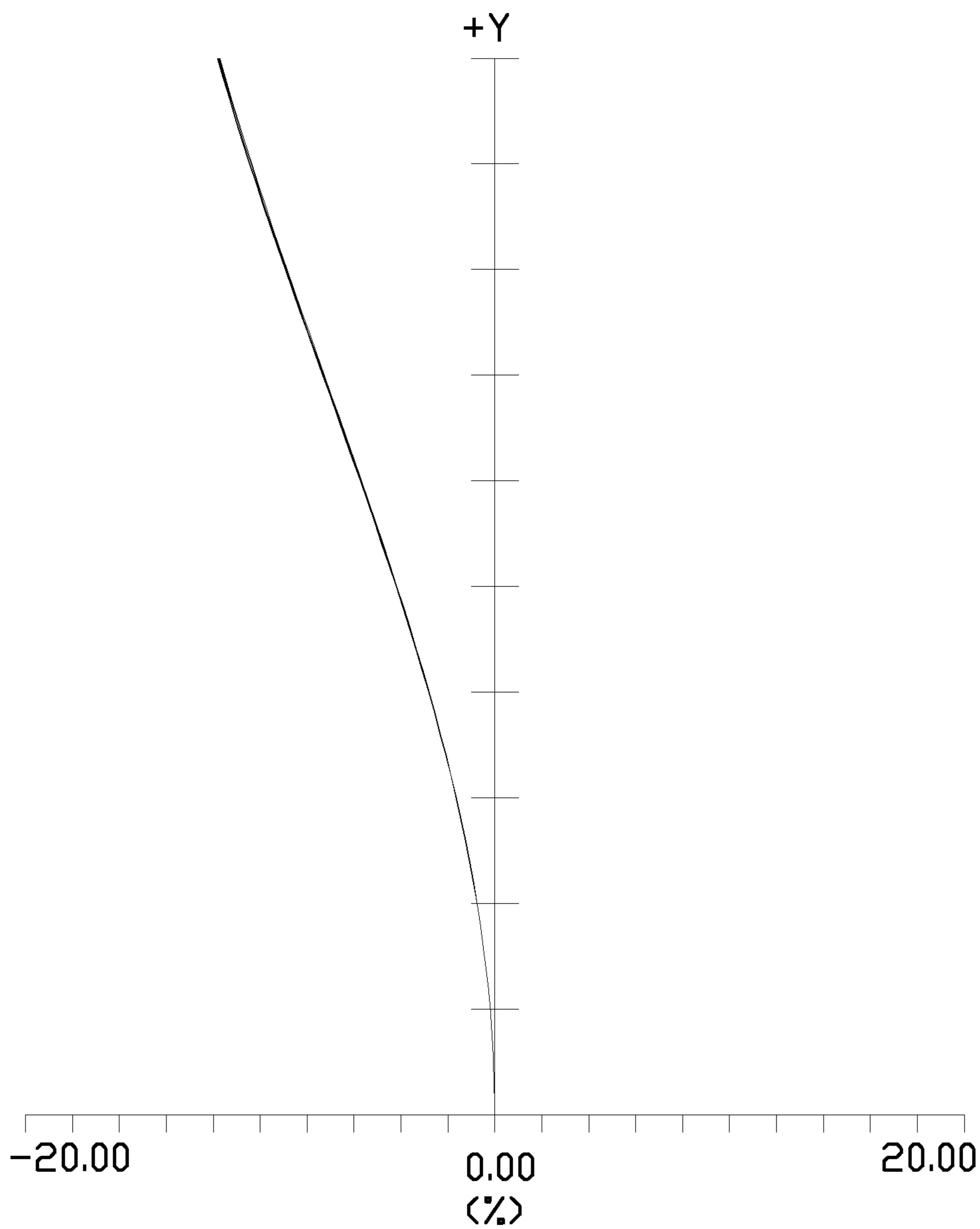


FIG. 5

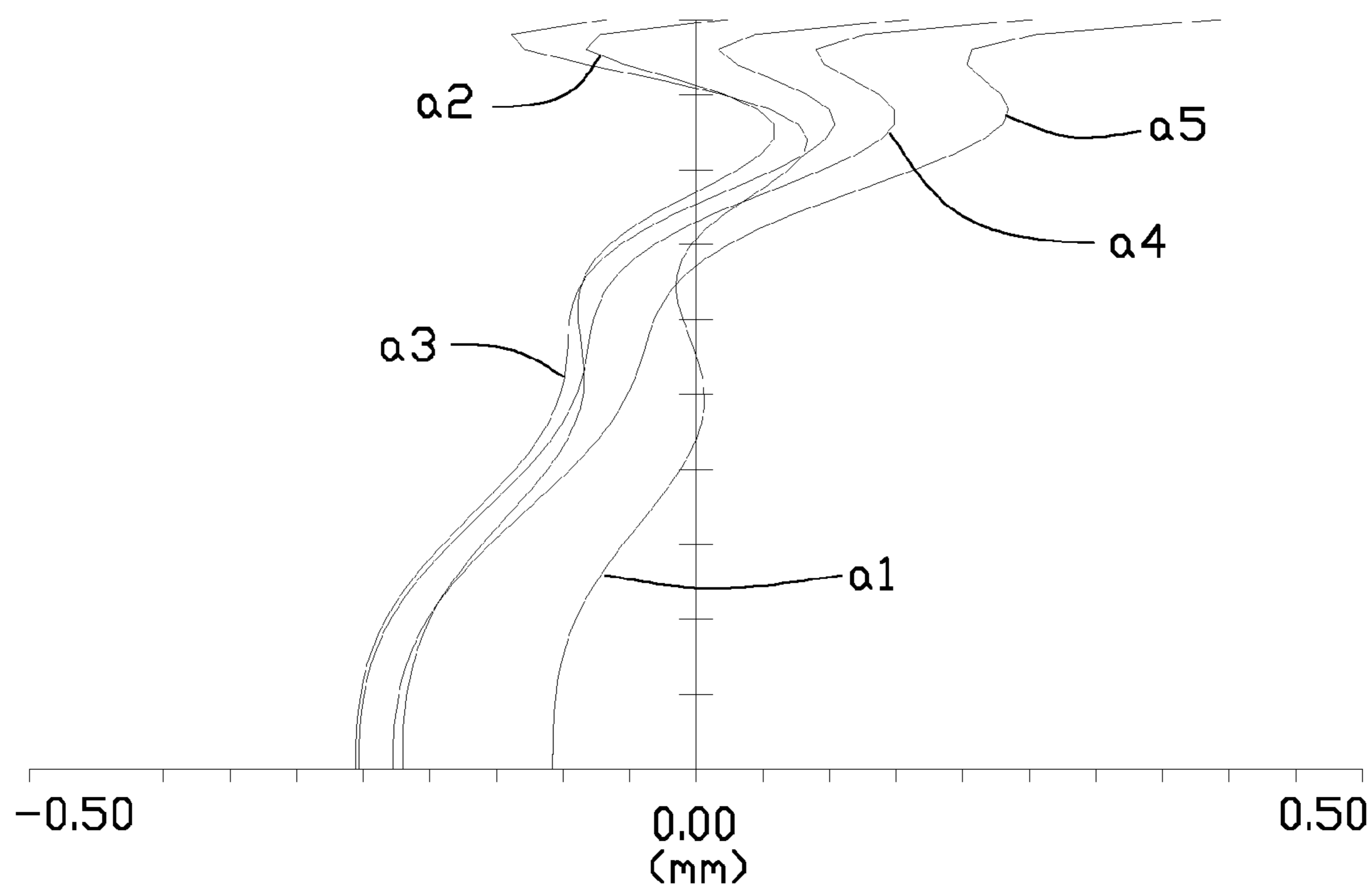


FIG. 6

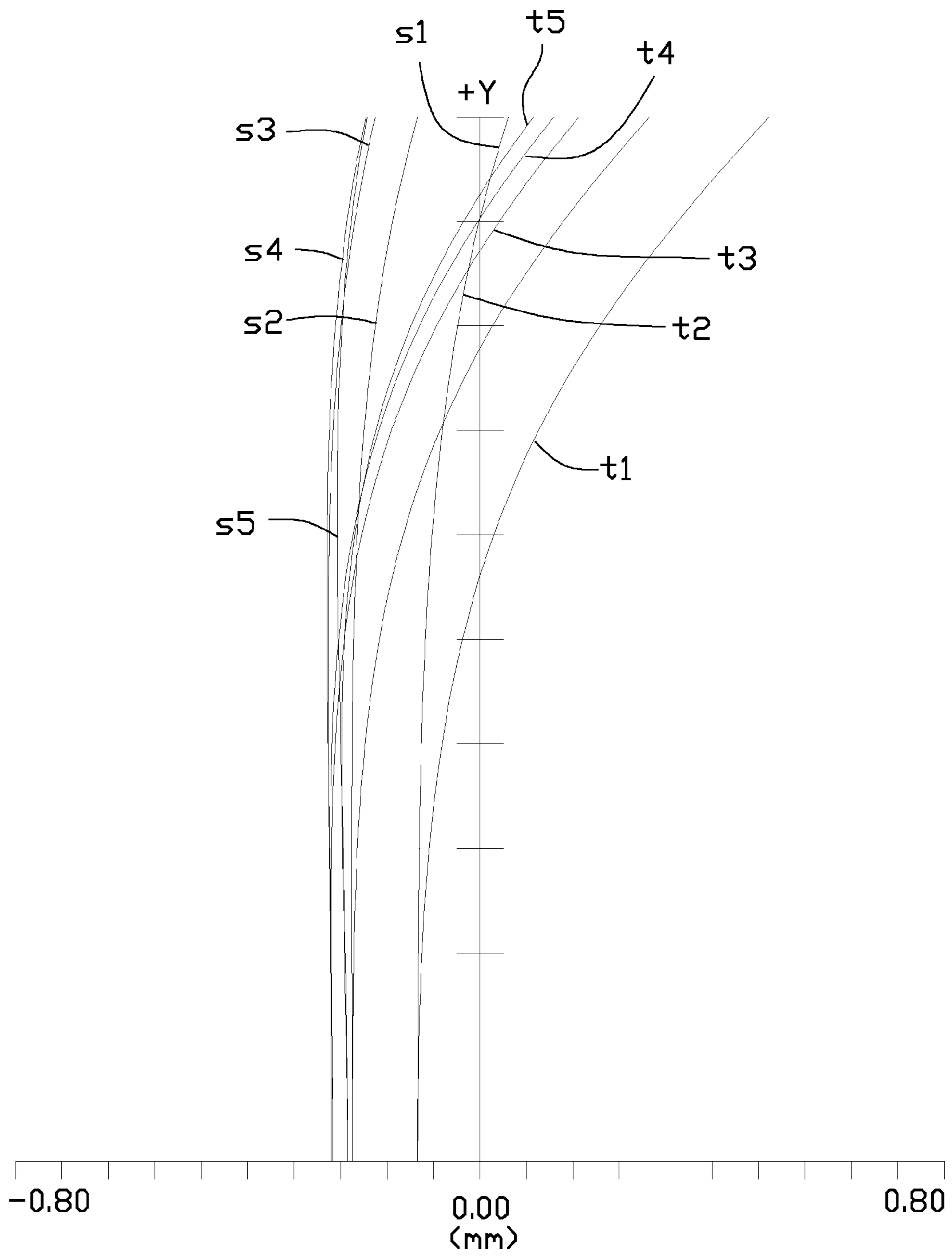


FIG. 7



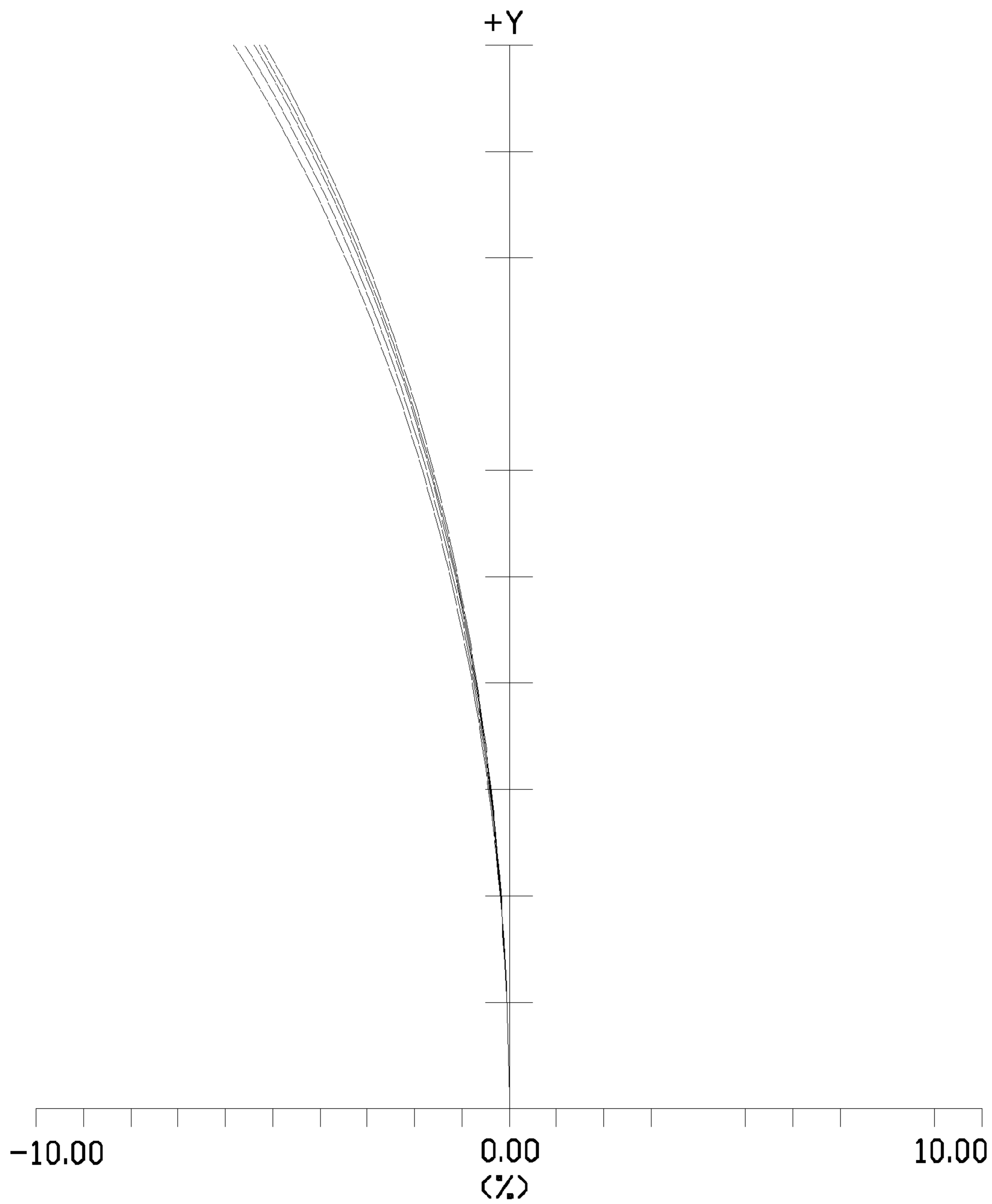


FIG. 8

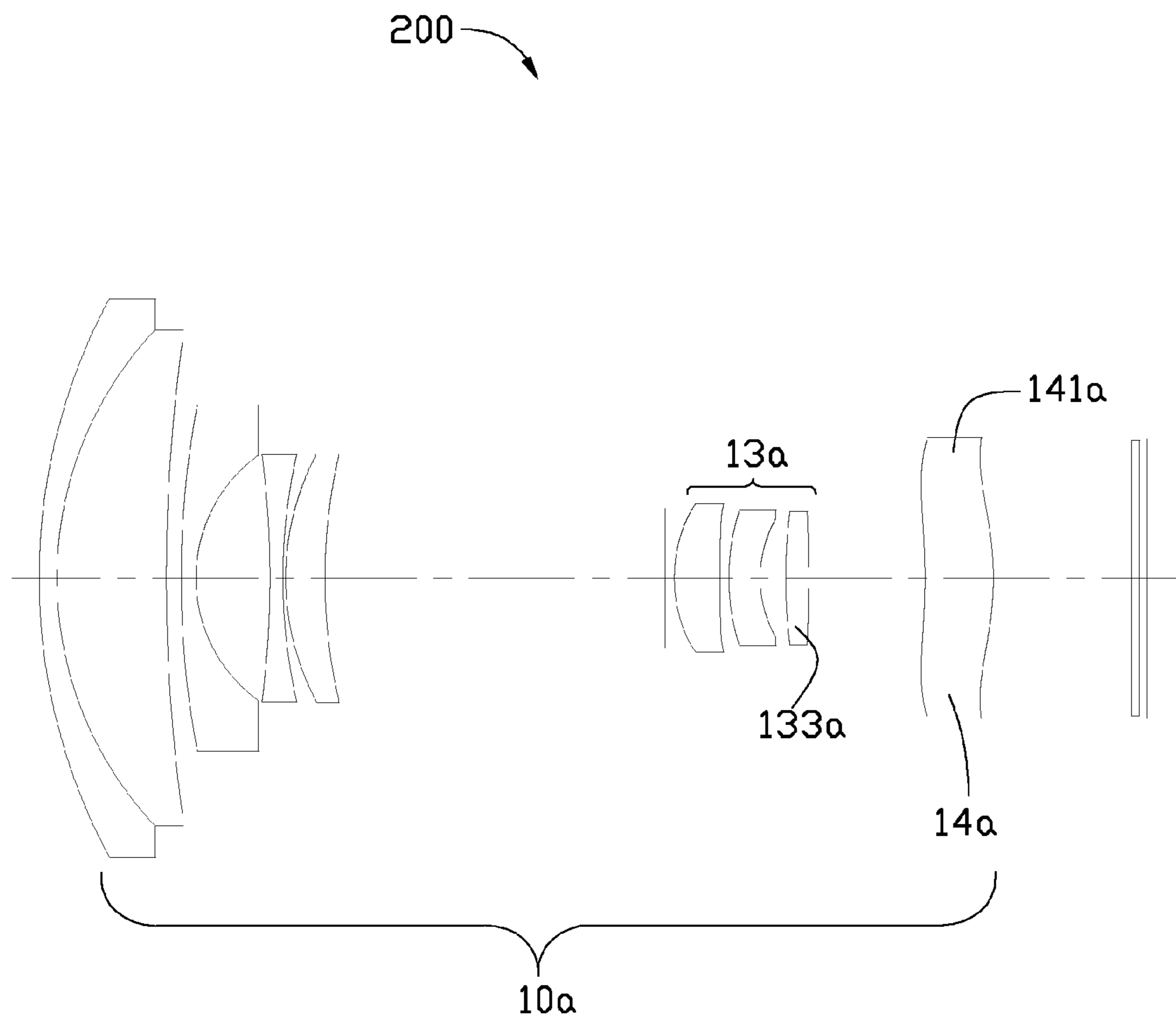


FIG. 9

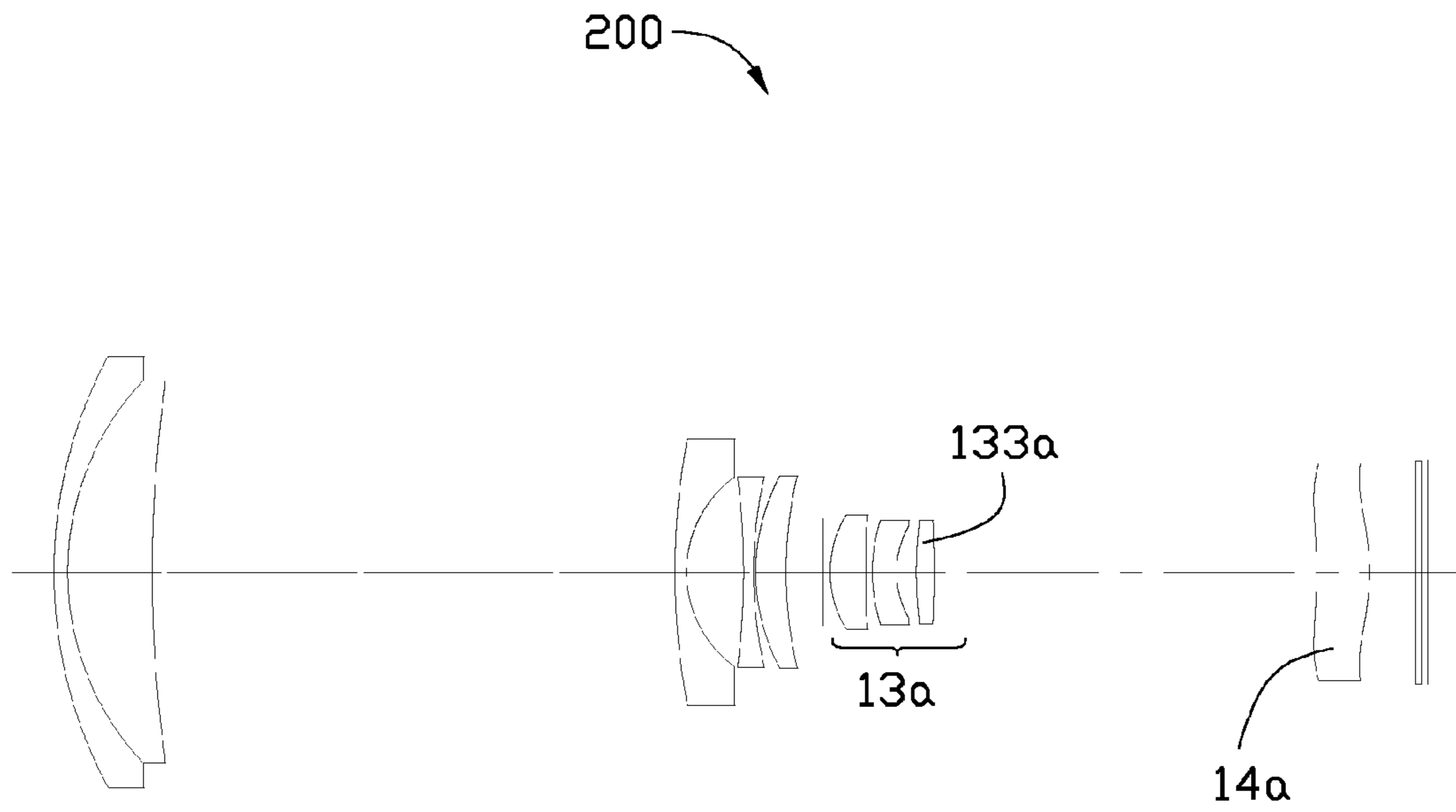


FIG. 10

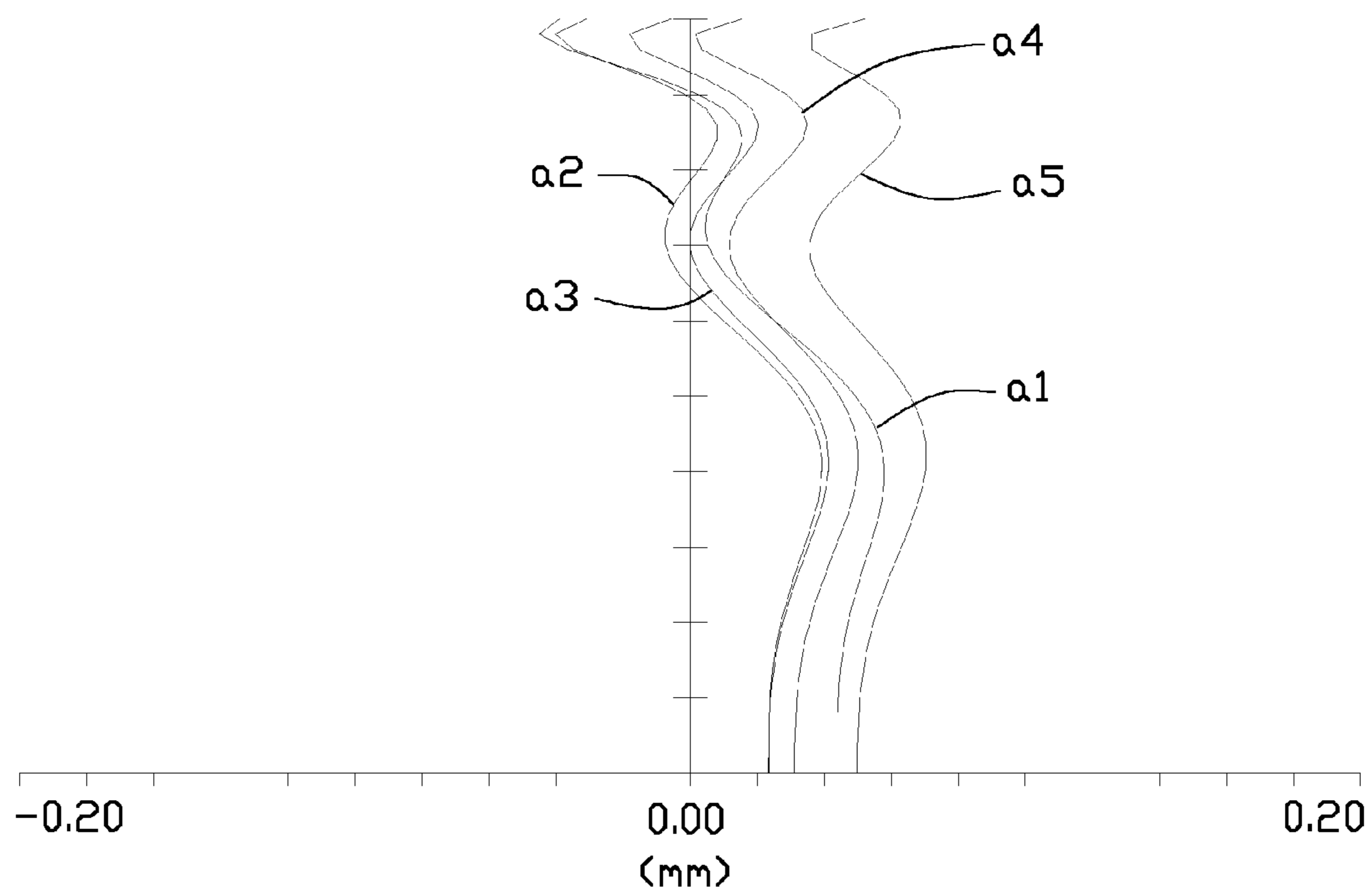


FIG. 11

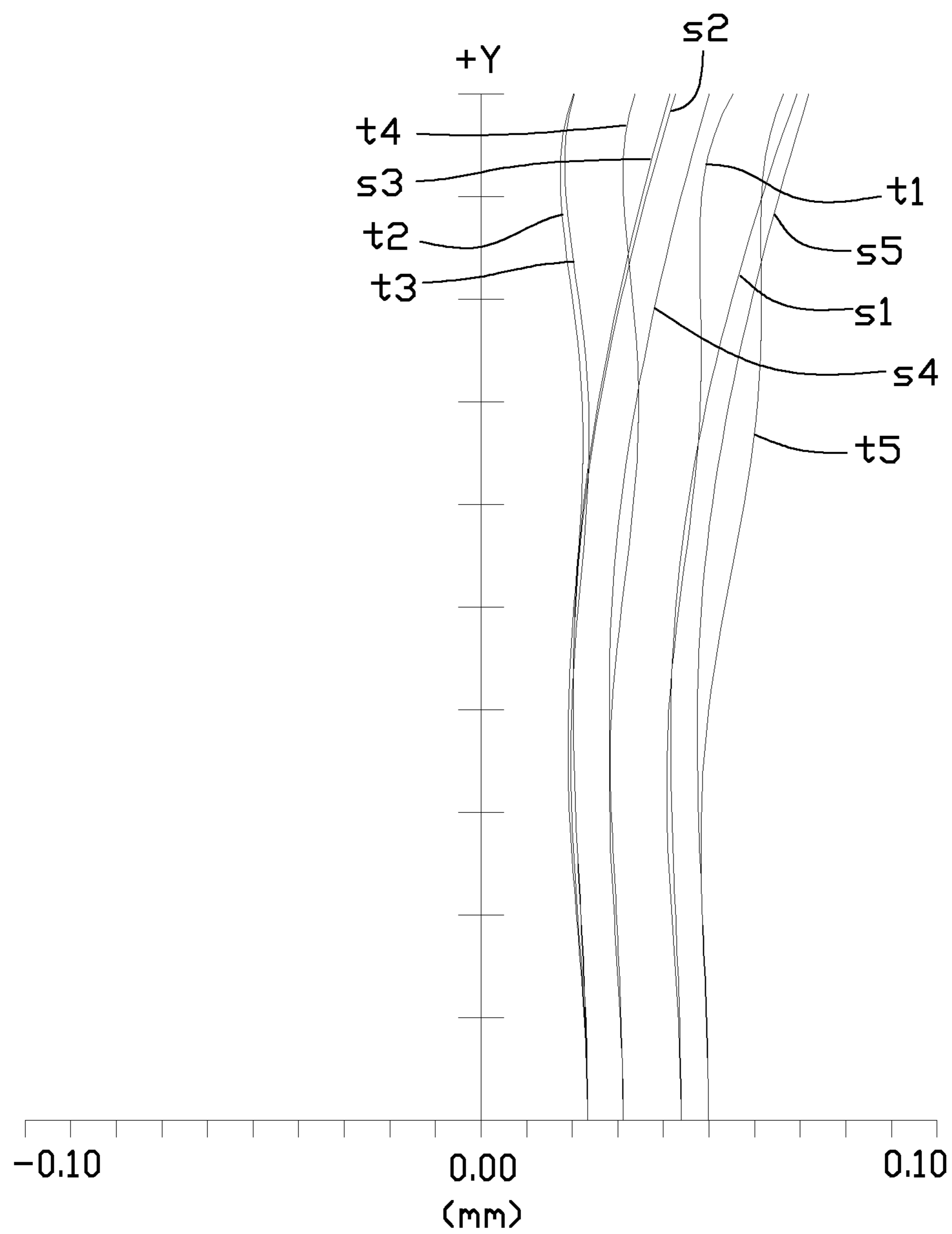


FIG. 12

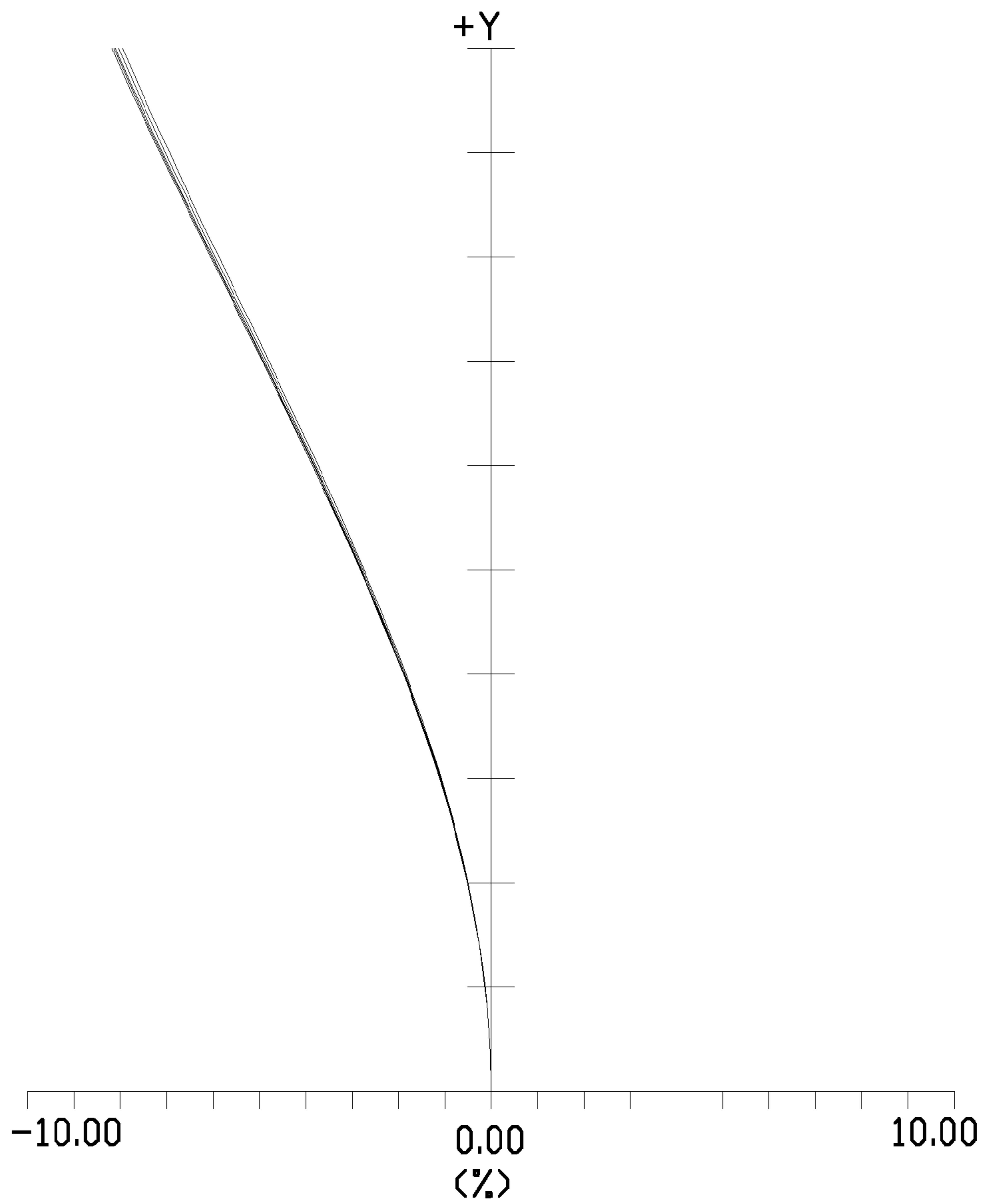


FIG. 13

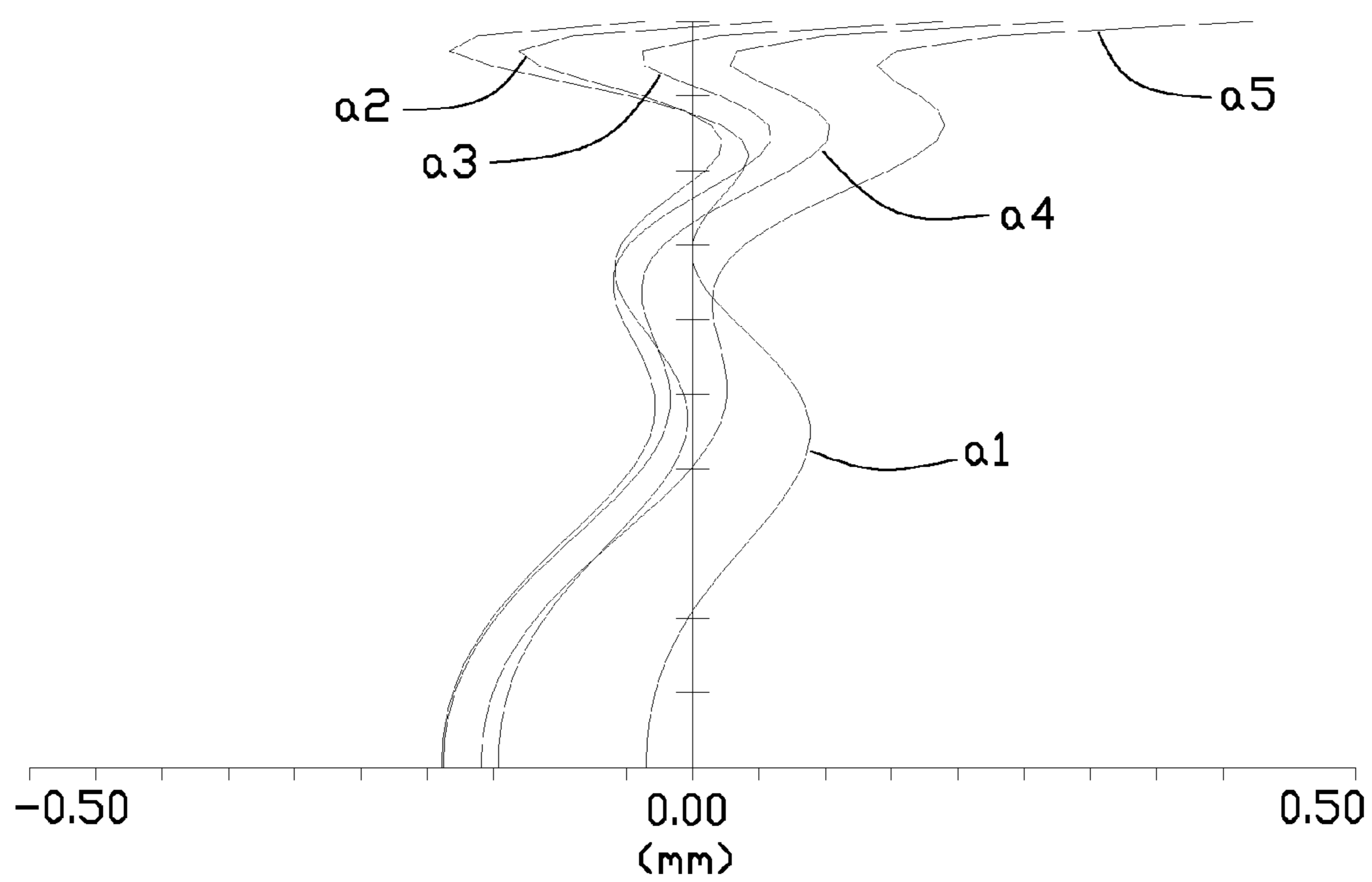


FIG. 14

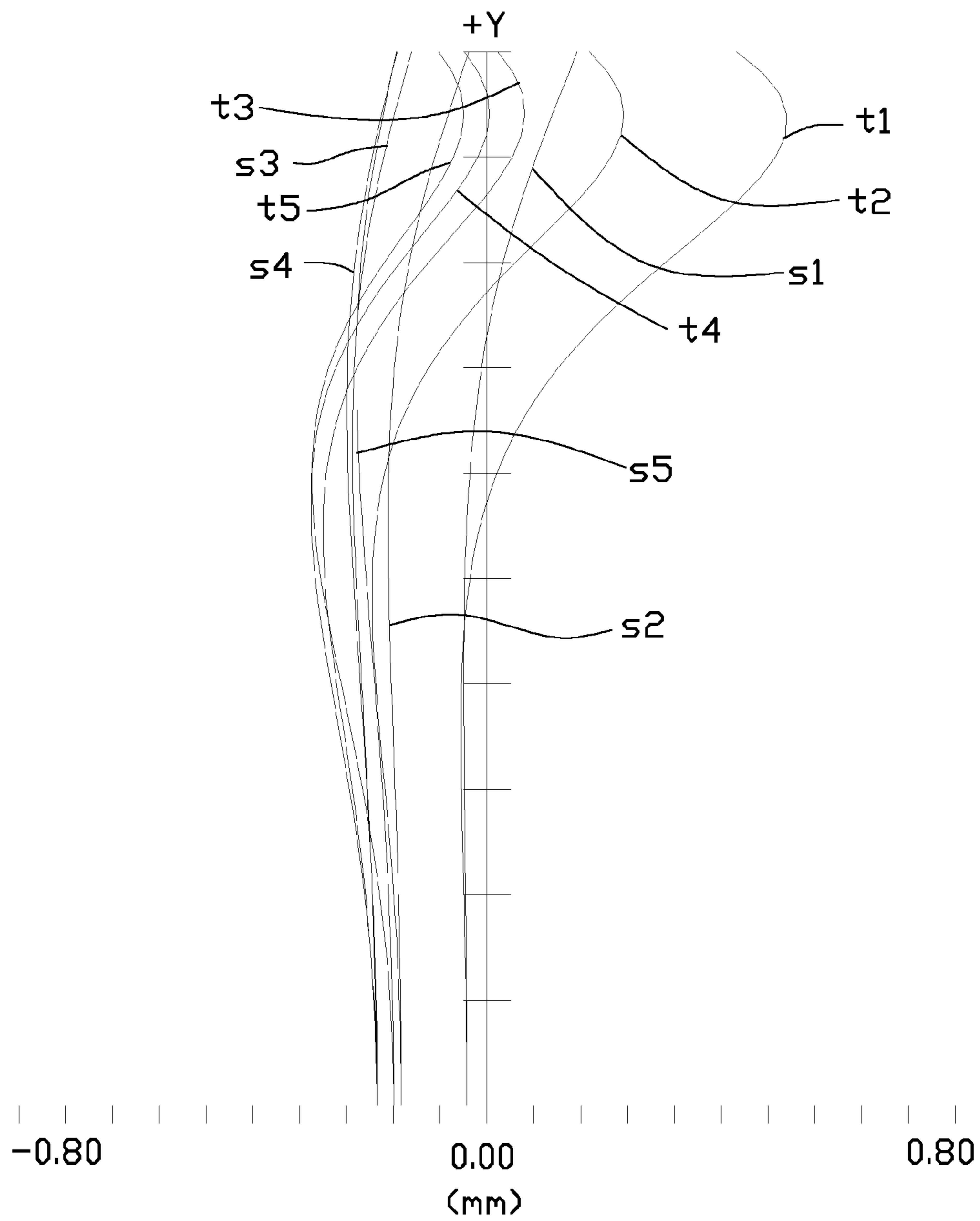


FIG. 15



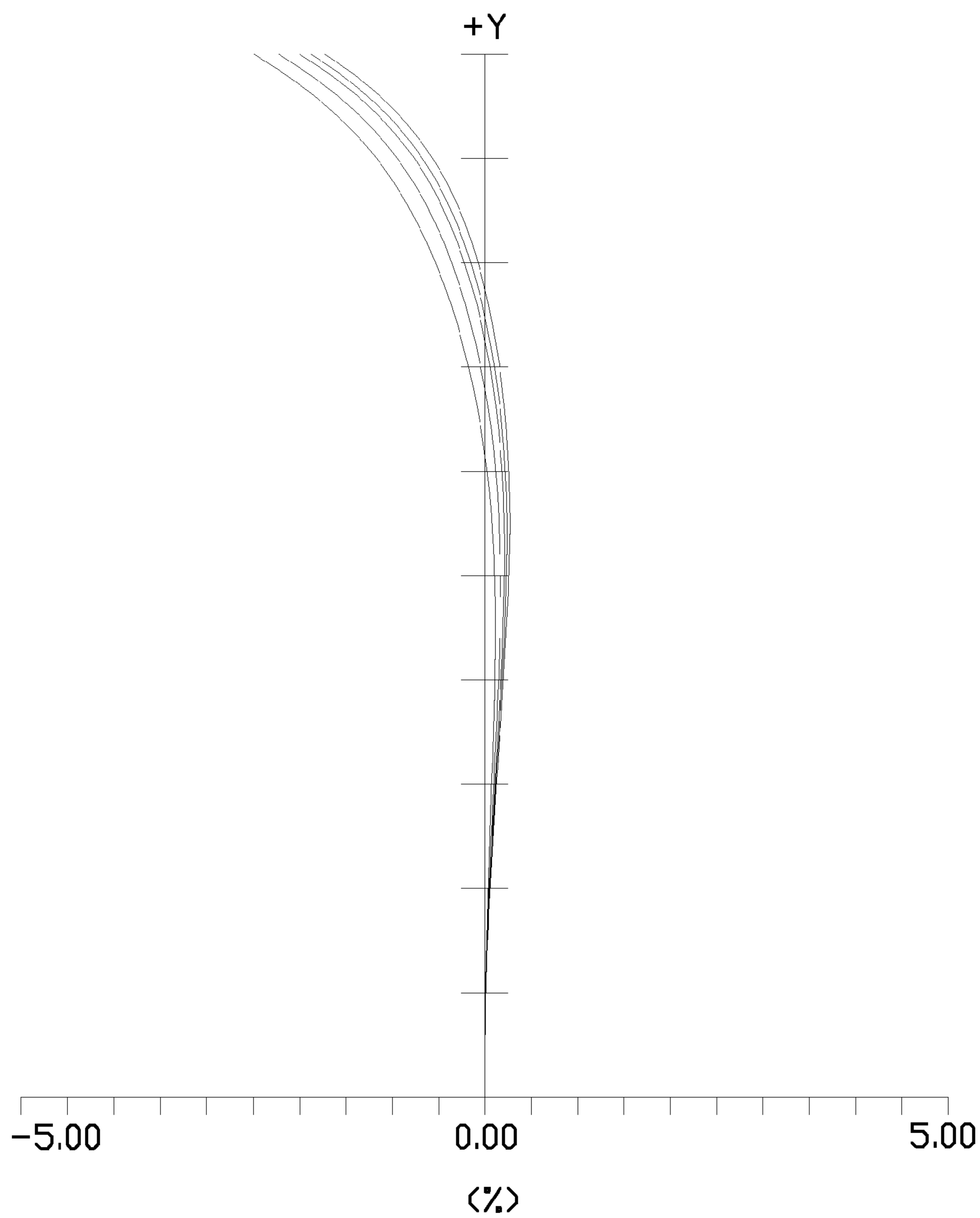


FIG. 16

## ZOOM LENS AND IMAGING DEVICE USING SAME

### BACKGROUND

#### 1. Technical Field

The present disclosure relates to a zoom lens and an imaging device using the zoom lens.

#### 2. Description of Related Art

Nowadays, the demand for imaging devices, such as digital cameras, digital video cameras, and monitoring devices, to not only be smaller but also have excellent zoom ratio and imaging capabilities grows.

However, if the size of an imaging device is reduced, the zoom ratio and imaging capabilities of the imaging device may suffer, because the usual way to improve the zoom ratio and imaging capabilities of a lens system is to increase the total length and/or volume of the lens system of the imaging device. Therefore, it is difficult to obtain an imaging device having an excellent zoom ratio and imaging capabilities while at the same time making it smaller.

Therefore, it is desirable to provide a zoom lens and an imaging device which can overcome the limitations described above.

### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic view of an imaging device at a wide-angle state in accordance with a first exemplary embodiment.

FIG. 2 is a schematic view of the imaging device of FIG. 1 at a telephoto state.

FIGS. 3-5 are graphs respectively showing spherical aberration, field curvature and distortion of the imaging device of FIG. 1.

FIGS. 6-8 are graphs respectively showing spherical aberration, field curvature and distortion of the imaging device of FIG. 2.

FIG. 9 is a schematic view of an imaging device at a wide angle state in accordance with a second exemplary embodiment.

FIG. 10 is a schematic view of the imaging device of FIG. 9 at a telephoto state.

FIGS. 11-13 are graphs respectively showing spherical aberration, field curvature and distortion of the imaging device of FIG. 9.

FIGS. 14-16 are graphs respectively showing spherical aberration, field curvature and distortion of the imaging device of FIG. 10.

### DETAILED DESCRIPTION

Embodiments of the disclosure will now be described in detail with reference to the accompanying drawings.

Referring to FIG. 1 and FIG. 2, an imaging device 100, according to a first exemplary embodiment, includes a zoom lens 10, and an image sensor 20 aligned with an optical axis of the zoom lens 10.

The zoom lens 10 includes, in the order from the object side to the image side thereof, a first lens group 11 with positive refraction power, a second lens group 12 with negative refraction power, a third lens group 13 with positive refraction power, and a fourth lens group 14 with positive refraction power. The zoom lens 10 further includes an aperture 15 positioned between the second lens group 12 and the third lens group 13. During focusing, the first lens group 11, the second lens group 12, the third lens group 13 and the fourth

lens group 14 are moved along the optical axis of the zoom lens 10. In addition, the fourth lens group 14 is also configured to compensate for image offset caused by focusing and/or changing of object distance. When in a wide-angle state, the zoom lens 10 has a minimal effective focal length, and when in a telephoto state, the lens 10 has a maximum effective focal length.

The first lens group 11 includes, in the order from the object side to the image side of the zoom lens 10, a first lens 111 with negative refraction power and a second lens 112 with positive refraction power. The first lens 111 and the second lens 112 are spherical lenses, and are combined using glue. The first lens 111 is meniscus shaped and includes a convex first surface facing the object side and a concave second surface facing the image side. The second lens 112 is meniscus shaped and includes a convex third surface facing the object side, and a concave fourth surface facing the image side.

The second lens group 12 includes, in the order from the object side to the image side of the zoom lens 10, a third lens 121 with negative refraction power, a fourth lens 122 with negative refraction power, and a fifth lens 123 with positive refraction power. The third lens 121, the fourth lens 122, and the fifth lens 123 are spherical lenses. The third lens 121 is meniscus shaped and includes a convex fifth surface facing the object side, and a concave sixth surface facing the image side. The fourth lens 122 is biconcave shaped and includes a concave seventh surface facing the object side, and a concave eighth surface facing the image side. The fifth lens 123 includes a convex ninth surface facing the object side, and a concave tenth surface facing the image side.

The third lens group 13 includes, in the order from the object side to the image side of the zoom lens 10, a sixth lens 131 with positive refraction power, a seventh lens 132 with negative refraction power, an eighth lens 133 with positive refraction power. The sixth lens 131 is an aspheric lens, and the seventh lens 132 and the eighth lens 133 are spherical lenses. The sixth lens 131 includes a convex eleventh surface facing the object side and a concave twelfth surface facing the image side. The seventh lens 132 includes a convex thirteenth surface facing the object side and a concave fourteenth surface facing the image side. The eighth lens 133 includes a concave fifteenth surface facing the object side and a convex sixteenth surface facing the image side.

The fourth lens group 14 includes a ninth lens 141 with positive refraction power. The ninth lens 141 is spherical lens. The ninth lens 141 includes a concave seventeenth surface facing the object side and a convex eighteenth surface facing the image side.

The image sensor 20 includes an imaging surface 21 and a filter 22 at the object side of the imaging surface 21. The filter 22 is configured for filtering incident light of a predetermined wavelength.

The zoom lens 10 satisfies the formulas:

$$0.15 < L3/Lt < 0.25; \quad (1)$$

wherein L3 is a distance of the movement of the third lens group 13 along the optical axis when the zoom lens is switched between the wide-angle state and the telephoto state, and Lt is a distance from the first surface to a surface which images are formed on (the imaging surface 21 of the image sensor 20), along the optical axis. In this embodiment, the L3 is positive when the third lens group 13 moves from the object side to the image side, and the L3 is negative when the third lens 12 moves from the image side to the object side.

Formula (1) is for balancing the total length of the zoom lens 10 and the imaging capability of the zoom lens 10.

## 3

Therefore, the zoom lens **10** has an excellent imaging capability and a compact size at the same time.

The zoom lens **10** further satisfies the formula:

$$0.045 < f_3 / (f_t \times f_w) < 0.055; \quad (2)$$

wherein  $f_3$  is an effective focal length of the third lens group **13**,  $f_t$  is an effective focal length of the zoom lens **10** at the telephoto state, and  $f_w$  is an effective focal length of the zoom lens **10** at the wide-angle state.

Formula (2) is for keeping a large zoom ratio and a super wide-angle of visual field of the zoom lens **10**. In addition, formula (2) correct for spherical aberration of the zoom lens **10**.

Furthermore, the zoom lens **10** can optically compensate for image offset caused by shaking of the imaging device **100** when handheld. The zoom lens **10** compensates by moving the third lens group **13**. The zoom lens **10** further satisfies the formula:

$$0.15 < f_3 / f_t < 0.25. \quad (3)$$

Formula (3) allows image offset with only a short distance of movement of the third lens group **13**, therefore, enhancing response speed of image offset by the zoom lens **10**.

The zoom lens **10** further satisfies the formula:

$$55 < |V_7 - V_8| < 70; \quad (4)$$

Wherein  $V_7$  is the Abbe number of the seventh lens **132**, and  $V_8$  is the Abbe number of the eighth lens **133**.

Formula (4) provides a large zooming ratio with excellent imaging capability to the zoom lens **10**.

In the first embodiment, the zoom lens **10** satisfies the parameters of Tables 1-3. Listed below are the symbols used in Tables 1-3:

R: radius of curvature,

D: distance between surfaces on the optical axis,

Nd: refractive index,

Vd: Abbe number,

f: effective focal length of the zoom lens **10**,

D4: distance between the fourth surface and the fifth surface on the optical axis,

D10: distance between the tenth surface and the eleventh surface on the optical axis,

D16: distance between the sixteenth surface and the seventeenth surface on the optical axis, and

D18: distance between the eighteenth surface and an object side surface of the filter on the optical axis.

TABLE 1

surface	type	R (mm)	D (mm)	Nd	Vd
first surface	spherical	17.22021	0.48	2.001003	29.134715
second/third surface	spherical	10.21879	2.955	1.804200	46.502535
fourth surface	spherical	73.91341	D4	—	—
fifth surface	spherical	30.21305	0.4	1.883000	40.805404
sixth surface	spherical	4.154824	2	—	—
seventh surface	spherical	-15.62686	0.35	1.729160	54.673513
eighth surface	spherical	31.40399	0.075	—	—
ninth surface	spherical	8.063187	1.062	2.002723	19.317191
tenth surface	spherical	19.60882	D10	—	—
aperture	—	infinity	0.25	—	—
eleventh surface	aspherical	3.904443	1.242	1.693500	53.200779
twelfth surface	aspherical	103.9837	0.232	—	—
thirteenth surface	spherical	6.443325	0.845	1.922860	18.896912

## 4

TABLE 1-continued

surface	type	R (mm)	D (mm)	Nd	Vd
5 fourteenth surface	spherical	3.393499	0.69	—	—
fifteenth surface	spherical	-33.9678	0.62	1.496997	81.608379
10 sixteenth surface	spherical	-8.734793	D16	—	—
seventeenth surface	spherical	-22.28714	1.85	1.496997	81.608379
15 eighteenth surface	spherical	-7.454892	D18	—	—
filter	flat	infinity	0.8	1.516	64.1
imaging surface	flat	infinity	—	—	—
20					

TABLE 2

state	F	D4	D10	D16	D18
wide-angle state	4.586	0.4	9.033	2.05	4.995
middle state	18.32	11.257	3.322	12.681	2
telephoto state	34.939	17.106	1.297	14.596	1.61

TABLE 3

aspherical coefficient	eleventh surface	twelfth surface
k	0.410787	665.2078
A4	-0.00011593348	0.0037053259
A6	0.000085725109	0.00075722376
A8	0.00020739289	-0.00036146427
A10	-0.000060320058	0.00030799676
A12	0.0000048226882	-0.00010332042
A14	0.0000017847423	0.000016711619
A16	-0.00000019630506	-0.00000068980054

The aspherical surfaces are shaped according to the formula:

$$x = \frac{ch^2}{1 + \sqrt{1 - (k+1)c^2h^2}} + \sum A_i h^i$$

wherein  $h$  is a height from the optical axis of the zoom lens **10** to the aspherical surface,  $c$  is a vertex curvature,  $k$  is a conic constant, and  $A_i$  are  $i$ -th order correction coefficients of the aspherical surfaces.

In the first embodiment, the zoom lens **10** satisfies the parameters of Table 4. Listed below are the symbols used in Table 4:  $2\omega$ : field angle;  $F_{No}$ : F number.

TABLE 4

State	$F_{No}$	$2\omega$ (degree)
wide-angle state	2.97	89
middle state	5.0	25.3
telephoto	5.5	13.5

## 5

From Table 1 and Table 2, the parameters for formulas (1)-(4) are listed in Table 5 as below.

TABLE 4

parameter	L3	Lt	f3	ft	fw	V7	V8
value	-9.16	48.97	8.04	34.94	4.59	18.9	81.6

Therefore, the value of  $|L3|/Lt$  is about 0.187, the value of  $f3/(ft \times fw)$  is about 0.05, the value of  $f3/ft$  is about 0.3, and the value of  $V7-V8$  is about -62.7.

The zoom lens **10** has a zooming ratio of eight, and was tested using the incident light at wavelengths of 436 nanometers, 486 nanometers, 546 nanometers, 588 nanometers, and 656 nanometers are sampled.

The spherical aberration graph, the field curvature graph, and the distortion graph of the zoom lens **10** in the wide angle state are respectively shown in FIGS. 3-5. In FIG. 3, a1-a5 are the field curvature curves of light with wavelength of 436 nanometers, 486 nanometers, 546 nanometers, 588 nanometers, and 656 nanometers respectively. In FIG. 4, t and s are the tangential field curvature curve and the sagittal field curvature curve respectively, t1-t5 are the tangential field curvature curves of light with wavelength of 436 nanometers, 486 nanometers, 546 nanometers, 588 nanometers, and 656 nanometers respectively, and s1-s5 are the sagittal field curvature curves of light with wavelength of 436 nanometers, 486 nanometers, 546 nanometers, 588 nanometers, and 656 nanometers respectively. Generally, spherical aberration of the zoom lens **10** is controlled within a range of -0.10 mm to 0.08 mm. The field curvature of the zoom lens **10** is kept within a range of -0.04 mm to 0.08 mm. The distortion of the zoom lens **10** falls within a range of -12% to 0%.

The spherical aberration graph, the field curvature graph, and the distortion graph of the zoom lens **10** in the telephoto state are respectively shown in FIGS. 6-8. Generally, spherical aberration of the zoom lens **10** is controlled within a range of -0.3 mm to 0.5 mm. The field curvature of the zoom lens **10** is kept within a range of -0.32 mm to 0.56 mm. The distortion of the zoom lens **10** falls within a range of -7% to 0%.

## 6

In the second exemplary embodiment, the zoom lens **10a** satisfies the parameters of Tables 6-8. The symbols used in the Table 5-7 have the same meaning as in the first exemplary embodiment.

TABLE 6

Surface	type	D		Nd	Vd
		R (mm)	(mm)		
first surface	spherical	15.90384	0.48	2.001003	29.134715
second/third surface	spherical	9.777388	2.955	1.804200	46.502535
fourth surface	spherical	46.94601	D4	—	—
fifth surface	spherical	25.18727	0.4	1.883000	40.805404
sixth surface	spherical	4.086963	2	—	—
seventh surface	spherical	-26.08895	0.35	1.729160	54.673513
eighth surface	spherical	15.03196	0.075	—	—
ninth surface	spherical	7.094077	1.062	2.002723	19.317191
tenth surface	spherical	14.75046	D10	—	—
aperture	—	infinity	0.25	—	—
eleventh surface	aspherical	3.994934	1.242	1.693500	53.200779
twelfth surface	aspherical	-218.5659	0.232	—	—
thirteenth surface	spherical	6.057806	0.845	1.922860	18.896912
fourteenth surface	spherical	3.250027	0.69	—	—
fifteenth surface	spherical	14.11827	0.62	1.496997	81.608379
sixteenth surface	spherical	-39.91605	D16	—	—
seventeenth surface	aspherical	-17.63791	1.85	1.531131	55.753858
eighteenth surface	aspherical	-8.030745	D18	—	—
filter	flat	infinity	0.8	1.516	64.1
imaging surface	flat	infinity	—	—	—

TABLE 7

state	f	D4	D10	D16	D18
wide-angle state	4.59	0.4	9.194	3.144	3.74
middle state	18.32	10627	2.84	12.635	2
telephoto state	34.94	18.304	1.297	13.398	1.61

TABLE 8

aspherical coefficient	eleventh surface	twelfth surface	seventeenth surface	eighteenth surface
k	0.4224068	665.2078	0	0
A4	$-1.9103235 \times 10^{-4}$	$3.4826645 \times 10^{-3}$	$1.2500546 \times 10^{-3}$	$1.9397925 \times 10^{-3}$
A6	$-8.8052476 \times 10^{-5}$	$3.2837747 \times 10^{-4}$	$1.9121893 \times 10^{-4}$	$1.4044656 \times 10^{-4}$
A8	$2.232613 \times 10^{-4}$	$-3.0253524 \times 10^{-4}$	$-1.3631872 \times 10^{-5}$	$-3.2052117 \times 10^{-6}$
A10	$-5.5652128 \times 10^{-5}$	0.00032280731	$3.715308 \times 10^{-7}$	$-7.2218202 \times 10^{-7}$
A12	$4.080371 \times 10^{-6}$	$-1.077947 \times 10^{-4}$	$8.0259183 \times 10^{-9}$	$8.7218075 \times 10^{-8}$
A14	$1.3592509 \times 10^{-6}$	$1.5561491 \times 10^{-5}$	$1.1934615 \times 10^{-10}$	$-2.9079321 \times 10^{-9}$
A16	$-1.3754611 \times 10^{-7}$	$-5.0671169 \times 10^{-7}$	$-4.0113779 \times 10^{-11}$	$-7.8706165 \times 10^{-12}$

Obviously, the spherical aberration, field curvature, and distortion are well controlled in the zoom lens **10** although the zoom lens **10** is compact.

Referring to FIGS. 9-10, an imaging device **200** according to a second exemplary embodiment is shown. The difference between the imaging device **200** and the imaging device **100** of the first exemplary embodiment is: the eighth lens **133a** of the third lens group **13a** includes a convex fifteenth surface facing the object side, and the ninth lens **141a** of the fourth lens group **14a** is an aspherical lens.

In this embodiment, the zoom lens **10a** also satisfies the formulas (1)-(4) in the first exemplary embodiment.

The aspherical surfaces are shaped according to the formula:

$$x = \frac{ch^2}{1 + \sqrt{1 - (k+1)c^2h^2}} + \sum A_i h^i$$

wherein  $h$  is a height from the optical axis of the zoom lens **10a** to the aspherical surface,  $c$  is a vertex curvature,  $k$  is a conic constant, and  $A_i$  are  $i$ -th order correction coefficients of the aspherical surfaces.

In the second exemplary embodiment, the zoom lens **10a** satisfies the parameters of Table 9. Listed below are the symbols used in Table 9:  $2\omega$ : field angle;  $F_{No}$ : F number.

TABLE 9

state	$F_{No}$	$2\omega$ (degree)
wide-angle state	3.1	86
middle state	5	24.26
telephoto state	5.5	13

From Tables 6 and Table 7, the parameters for formulas (1)-(4) are listed in Table 10 below.

TABLE 10

parameter	L3	Lt	f3	ft	fw	V7	V8
value	8.124	48.97	7.46	34.94	4.59	18.9	81.6

Therefore, the value of  $|L3|/Lt$  is about 0.166, the value of  $f3/(ft \times fw)$  is about 0.047, the value of  $f3/ft$  is about 0.21, and the value of  $V7-V8$  is about -62.7.

The zoom lens **10a** has a zooming ratio of eight, and was tested using incident light at wavelengths of 436 nanometers, 486 nanometers, 546 nanometers, 588 nanometers, and 656 nanometers.

The spherical aberration graph, the field curvature graph, and the distortion graph of the zoom lens **10a** in the wide angle state are respectively shown in FIGS. 11-13. Generally, spherical aberration of the zoom lens **10a** is controlled within a range of -0.06 mm to 0.08 mm. The field curvature of the zoom lens **10a** is kept within a range of 0.01 mm to 0.08 mm. The distortion of the zoom lens **10a** falls within a range of -10% to 0%.

The spherical aberration graph, the field curvature graph, and the distortion graph of the zoom lens **10a** in the telephoto state are respectively shown in FIGS. 14-16. Generally, spherical aberration of the zoom lens **10a** is controlled within a range of -0.2 mm to 0.5 mm. The field curvature of the zoom lens **10a** is kept within a range of -0.24 mm to 0.56 mm. The distortion of the zoom lens **10a** falls within a range of -3% to 0%.

Obviously, the spherical aberration, field curvature, and distortion are well controlled in the zoom lens **10a** although the zoom lens **10a** is compact.

Particular embodiments are shown and described by way of illustration only. The principles and the features of the present disclosure may be employed in various and numerous embodiments thereof without departing from the scope of the disclosure as claimed. The above-described embodiments illustrate the scope of the disclosure but do not restrict the scope of the disclosure.

What is claimed is:

**1.** A zoom lens for imaging an object on an imaging surface, in the order from an object side to an image side thereof, comprising:

- a first lens group with positive refraction power, the first lens group having a first surface facing the object side;
- a second lens group with negative refraction power;
- a third lens group with positive refraction power; and

a fourth lens group with positive refraction power; wherein the zoom lens satisfies the formulas:

$$0.15 < |L3|/Lt < 0.25;$$

where  $L3$  is a distance of the movement of the third lens group along an optical axis of the zoom lens when the zoom lens is switched between a wide-angle state and a telephoto state, and  $Lt$  is a distance from the first surface to the imaging surface.

**2.** The zoom lens as claimed in claim **1**, wherein the zoom lens satisfies the formulas:

$$0.045 < f3/(ft \times fw) < 0.055;$$

wherein  $f3$  an effective focal length of the third lens group,  $ft$  is an effective focal length of the zoom lens at the telephoto state, and  $fw$  is an effective focal length of the zoom lens at the wide-angle state.

**3.** The zoom lens as claimed in claim **2**, wherein the zoom lens satisfies the formulas:

$$0.15 < f3/ft < 0.25.$$

**4.** The zoom lens as claimed in claim **1**, wherein the first lens group comprises, in the order from the object side to the image side of the zoom lens, a first lens with negative refraction power and a second lens with positive refraction power, the first lens and the second lens are spherical lenses, the first lens comprises the first surface.

**5.** The zoom lens as claimed in claim **1**, wherein the second lens group comprises, in the order from the object side to the image side of the zoom lens, a third lens with negative refraction power, a fourth lens with negative refraction power, and a fifth lens with positive refraction power.

**6.** The zoom lens as claimed in claim **1**, wherein the third lens group comprises, in the order from the object side to the image side of the zoom lens, a sixth lens with positive refraction power, a seventh lens with negative refraction power, and an eighth lens with positive refraction power.

**7.** The zoom lens as claimed in claim **6**, wherein the sixth lens is an aspherical lens, and the seventh lens and the eighth lens are spherical lenses.

**8.** The zoom lens as claimed in claim **6**, wherein the zoom lens satisfies the formulas:

$$55 < |V7 - V8| < 70;$$

wherein  $V7$  is the Abbe number of the seventh lens, and  $V8$  is the Abbe number of the eighth lens.

**9.** The zoom lens as claimed in claim **1**, wherein the fourth lens group comprises a ninth lens with positive refraction power.

**10.** The zoom lens as claimed in claim **9**, wherein the ninth lens is a spherical lens.

**11.** The zoom lens as claimed in claim **9**, wherein the ninth lens is an aspherical lens.

**12.** An imaging device comprising:

a zoom lens, in the order from an object side to an image side thereof, comprising:

- a first lens group with positive refraction power, the first lens group comprising a first surface facing the object side;

- a second lens group with negative refraction power;

- a third lens group with positive refraction power; and

- a fourth lens group with positive refraction power; and

an image sensor aligned with an optical axis of the zoom lens, the image sensor comprising an imaging surface facing the object side;

wherein the zoom lens satisfies the formulas:

$$0.15 < |L3|/Lt < 0.25;$$

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where L3 is a distance of the movement of the third lens group along the optical axis when the zoom lens is switched between a wide-angle state and a telephoto state, and Lt is a distance from the first surface to the imaging surface.

13. The imaging device as claimed in claim 12, wherein the zoom lens satisfies the formulas:

$$0.045 < f_3 / (f_t \times f_w) < 0.055;$$

wherein f3 an effective focal length of the third lens group, ft is an effective focal length of the zoom lens at the telephoto state, and fw is an effective focal length of the zoom lens at the wide-angle state.

14. The imaging device as claimed in claim 13, wherein the zoom lens satisfies the formulas:

$$0.15 < f_3 / f_t < 0.25.$$

15. The imaging device as claimed in claim 12, wherein the first lens group comprises, in the order from the object side to the image side of the zoom lens, a first lens with negative refraction power and a second lens with positive refraction power, the first lens and the second lens are spherical lenses, the first lens comprises the first surface.

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16. The imaging device as claimed in claim 12, wherein the second lens group comprises, in the order from the object side to the image side of the zoom lens, a third lens with negative refraction power, a fourth lens with negative refraction power, and a fifth lens with positive refraction power.

17. The imaging device as claimed in claim 12, wherein the third lens group comprises, in the order from the object side to the image side of the zoom lens, a sixth lens with positive refraction power, a seventh lens with negative refraction power, and an eighth lens with positive refraction power.

18. The imaging device as claimed in claim 17, wherein the sixth lens is an aspherical lens, and the seventh lens and the eighth lens are spherical lenses.

19. The imaging device as claimed in claim 17, wherein the zoom lens satisfies the formulas:

$$55 < |V_7 - V_8| < 70;$$

wherein V7 is the Abbe number of the seventh lens, and V8 is the Abbe number of the eighth lens.

20. The imaging device as claimed in claim 12, wherein the fourth lens group comprises a ninth lens with positive refraction power.

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