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(54) **STIMULATION/SENSING LEAD ADAPTED FOR PERCUTANEOUS INSERTION**

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**A61N 1/05** (2006.01)

(52) **U.S. Cl.** ..... **607/117**

(58) **Field of Classification Search** ..... **600/373,**  
**600/393; 607/117**

See application file for complete search history.

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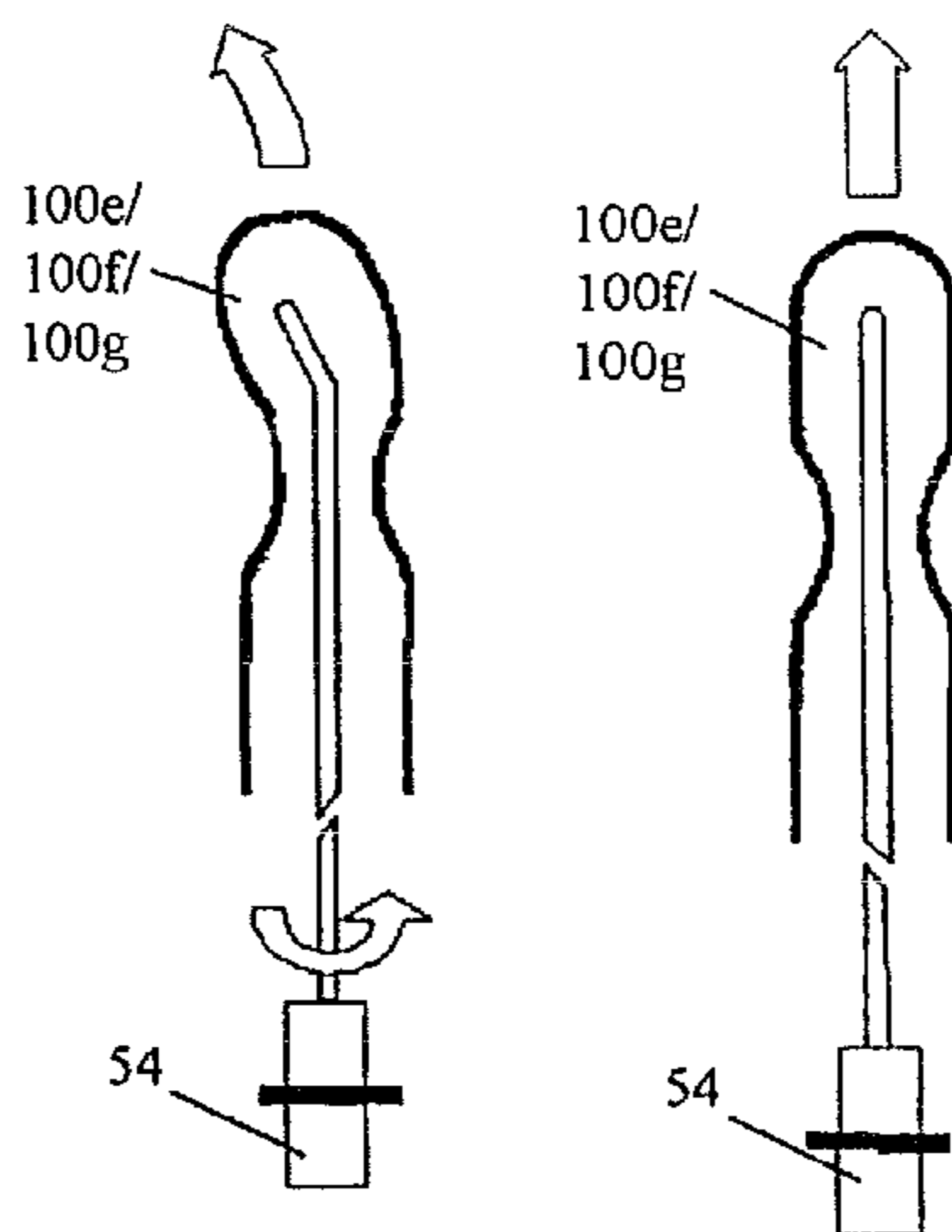
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(57) **ABSTRACT**

The present invention relates to a percutaneous insertion-capable lead, wherein insertion made through a percutaneous insertion structure. For one embodiment of such lead, the electrode-supporting stimulation portion of the lead includes at least one waisted region, relative to a transverse dimension of the lead, to facilitate lead steerability.

**3 Claims, 7 Drawing Sheets**



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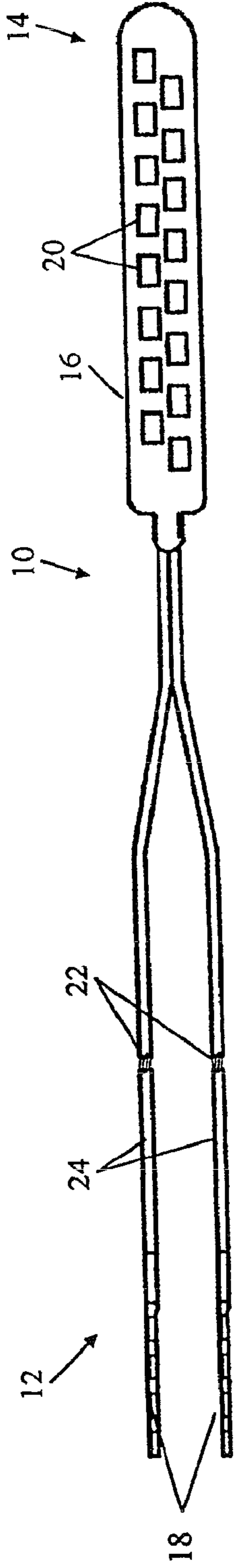
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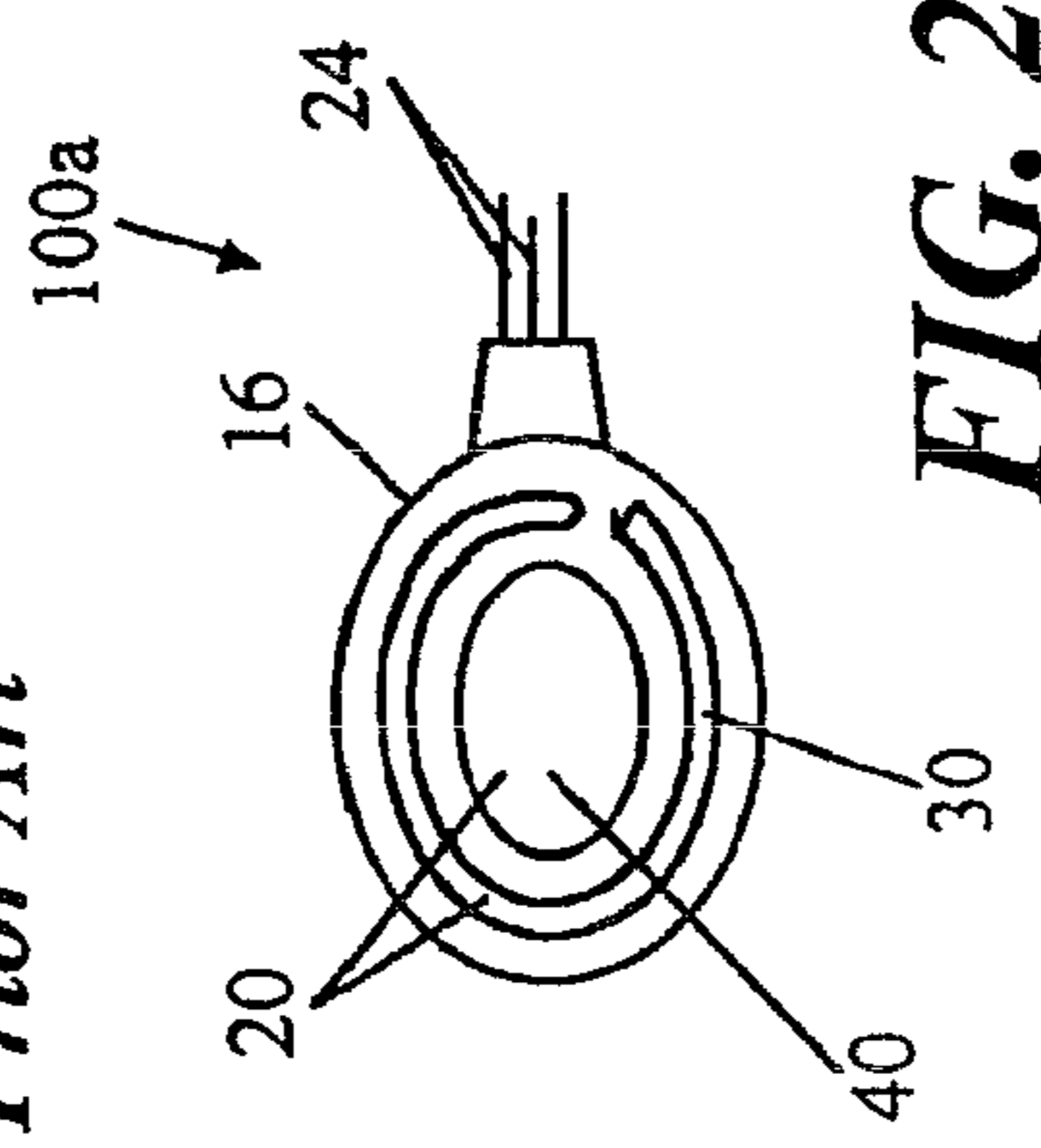
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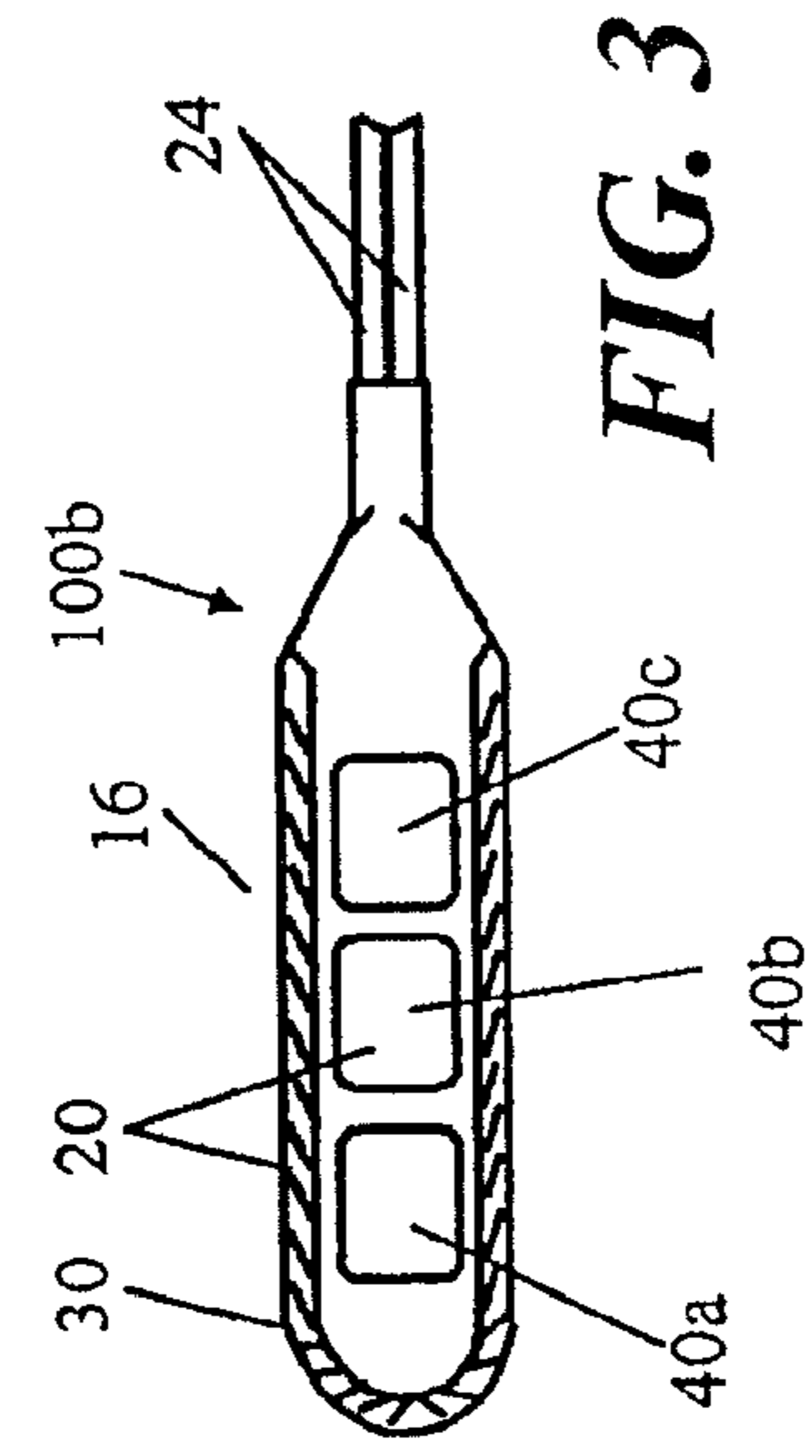
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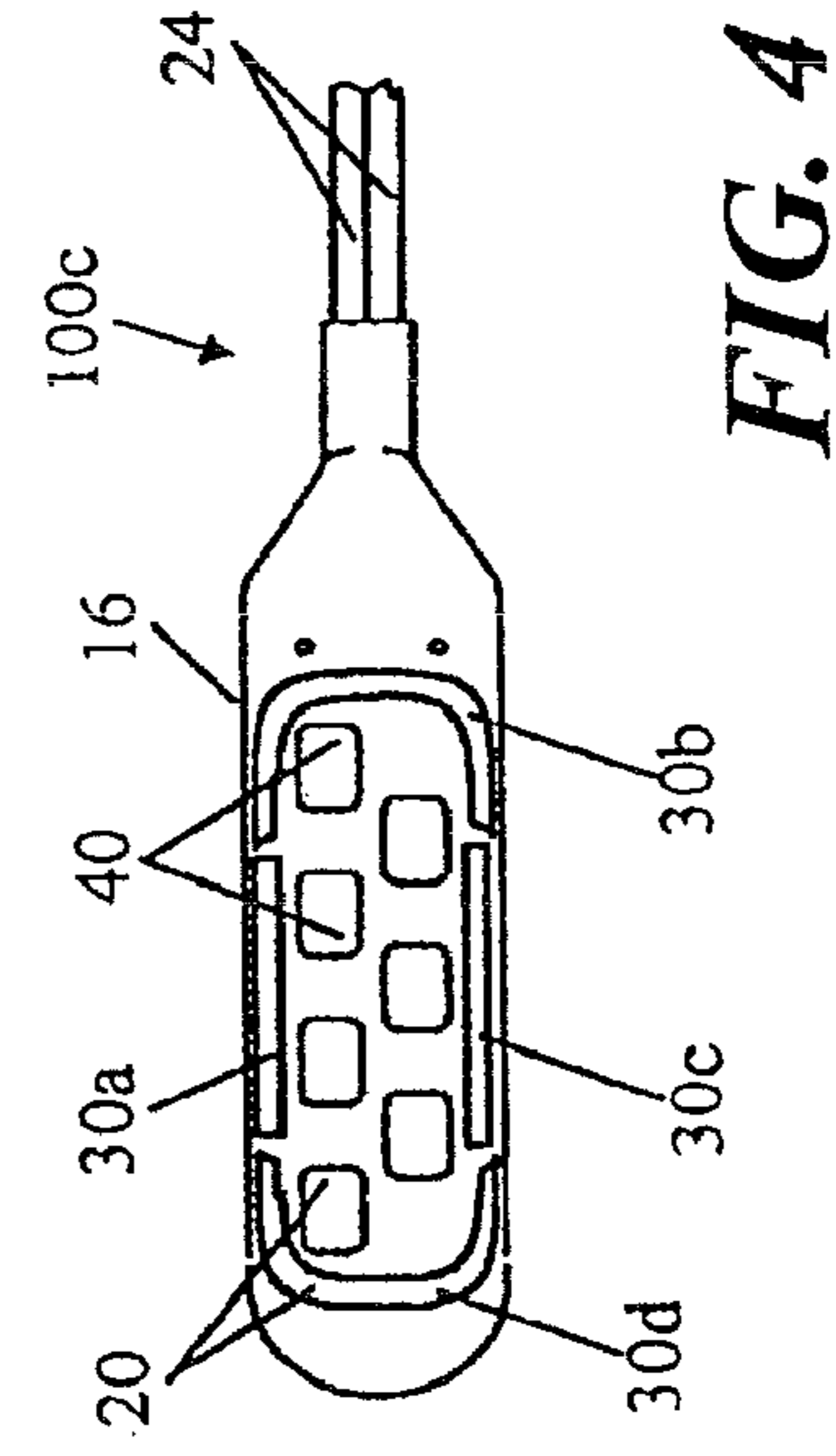
**FIG. 1**  
*Prior Art*



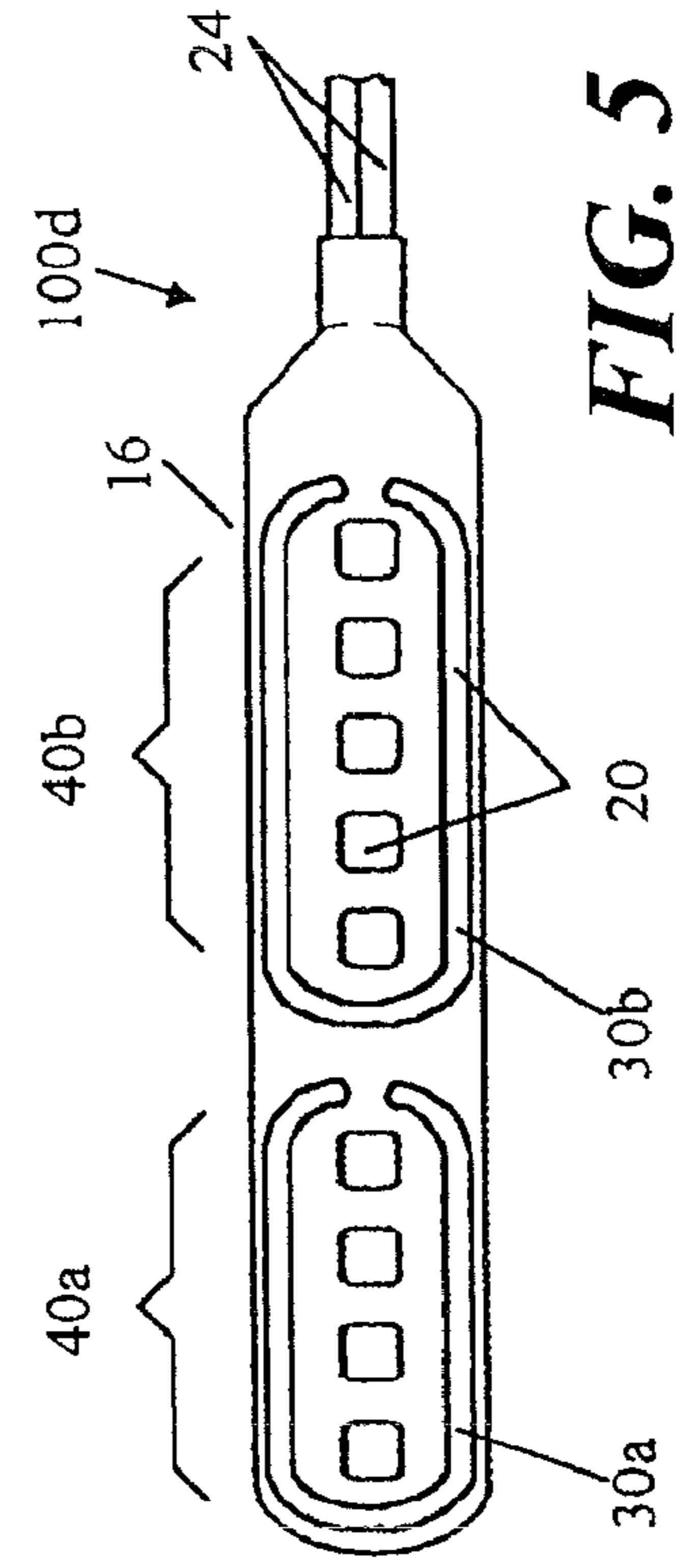
**FIG. 2**



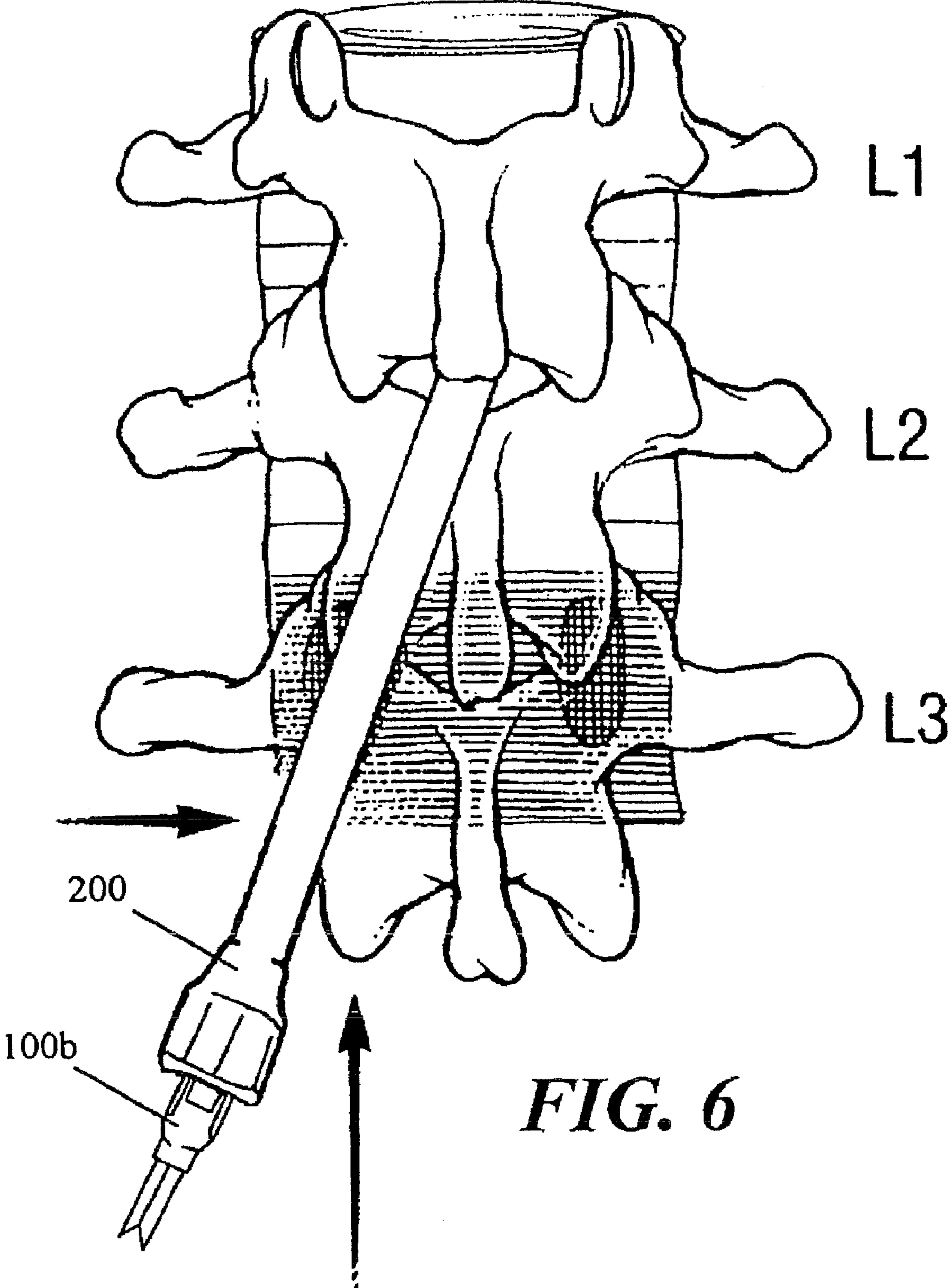
**FIG. 3**



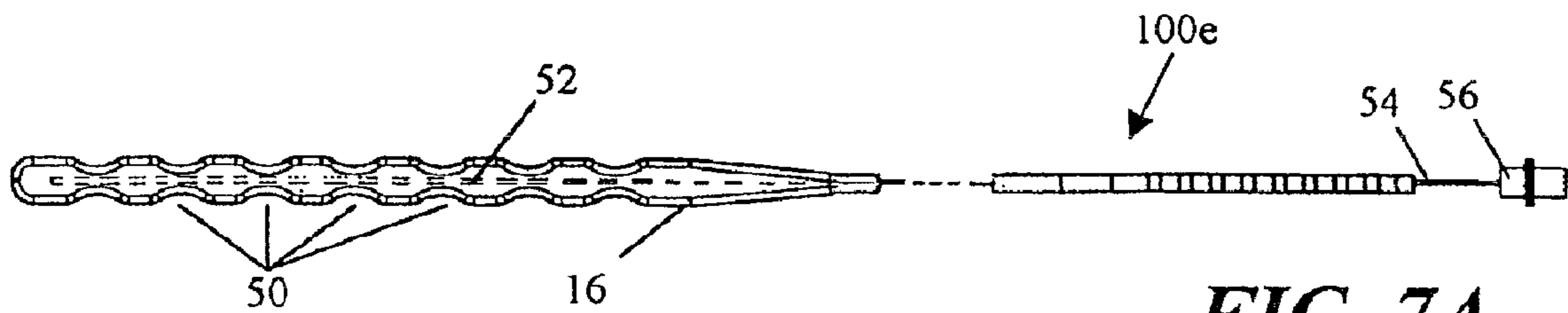
**FIG. 4**



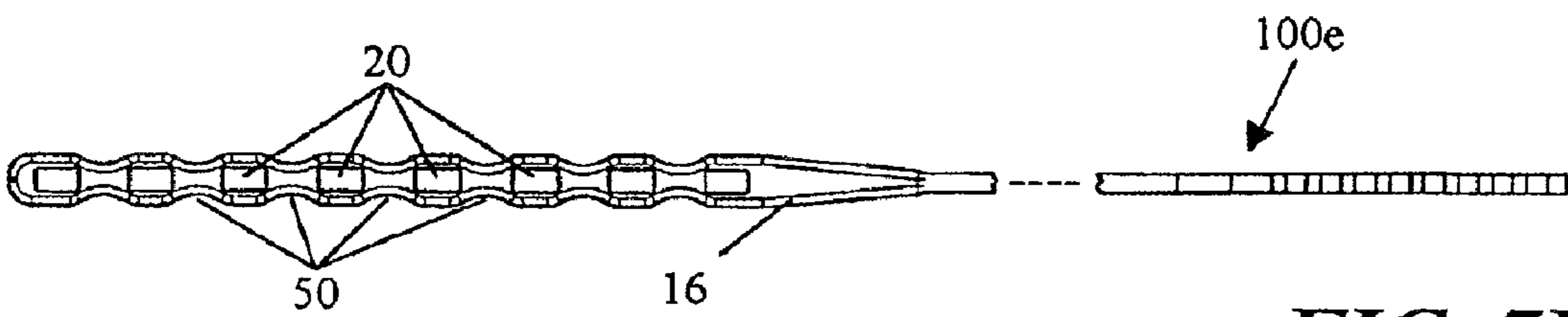
**FIG. 5**



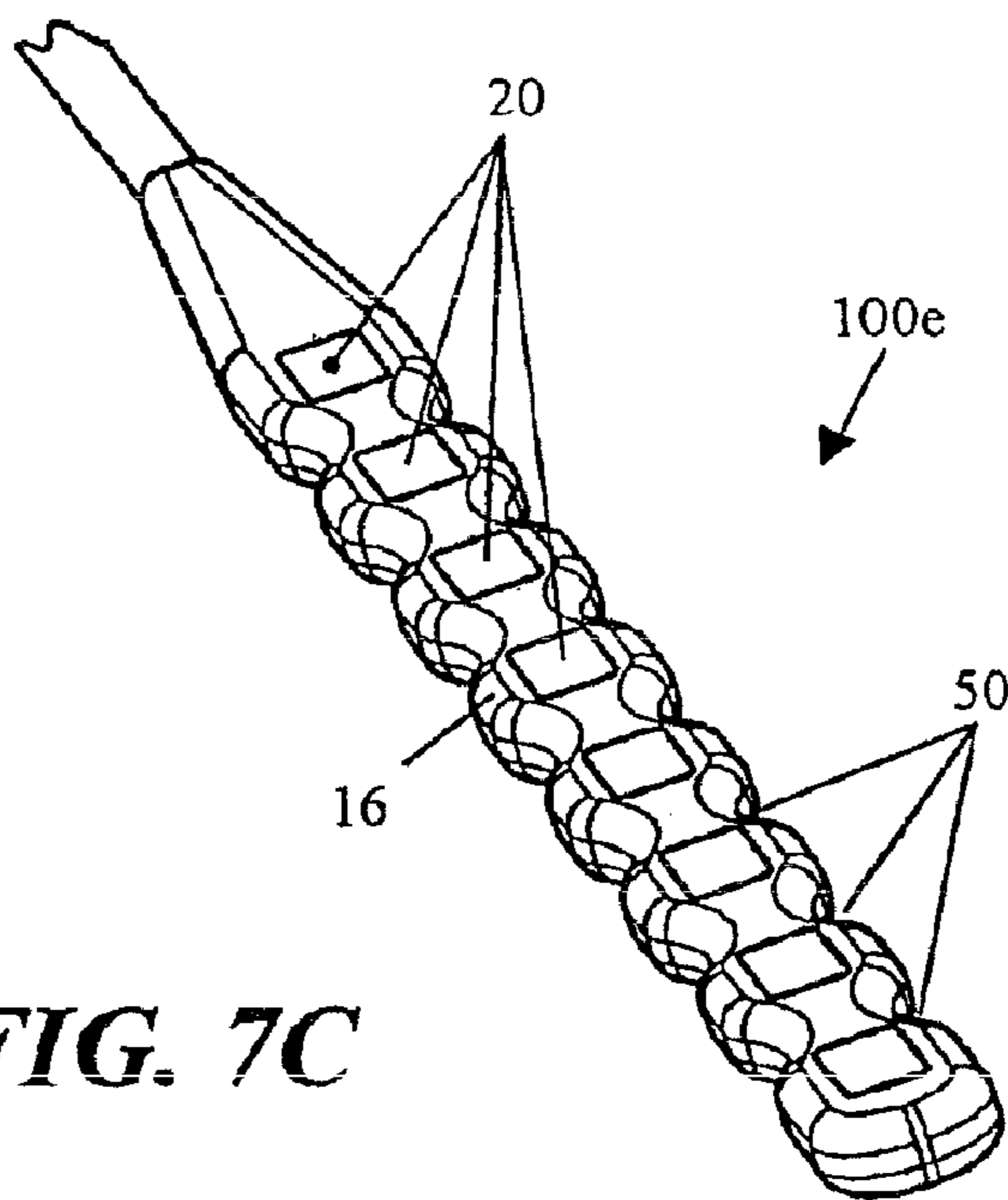
**FIG. 6**



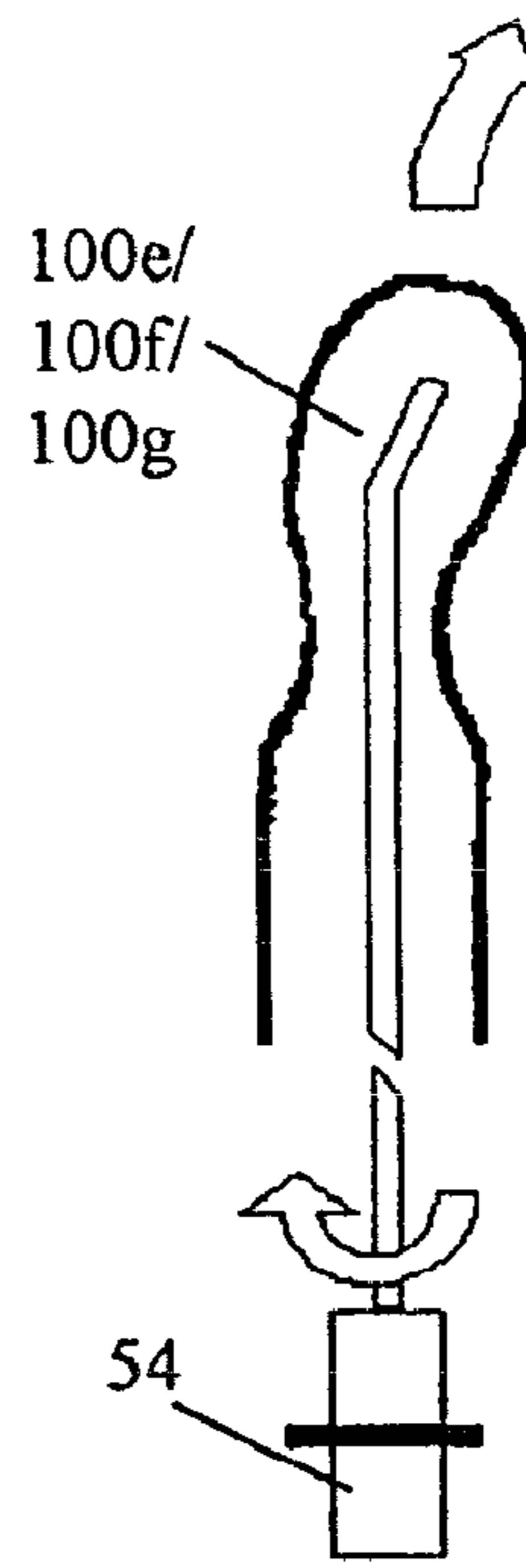
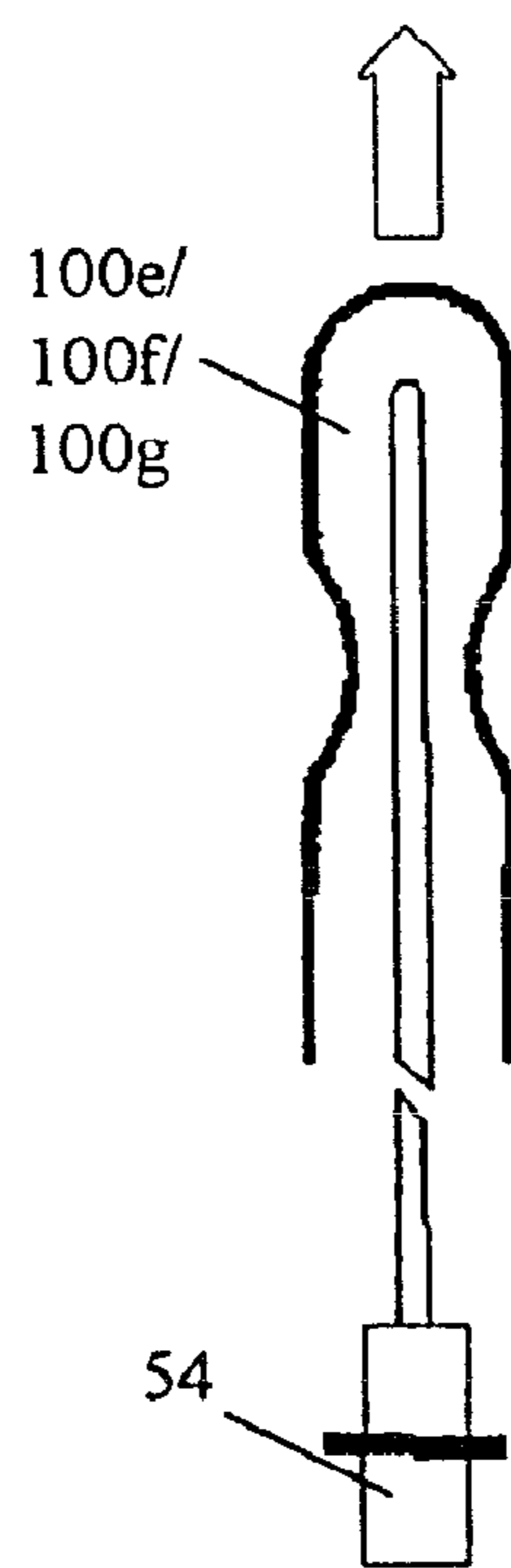
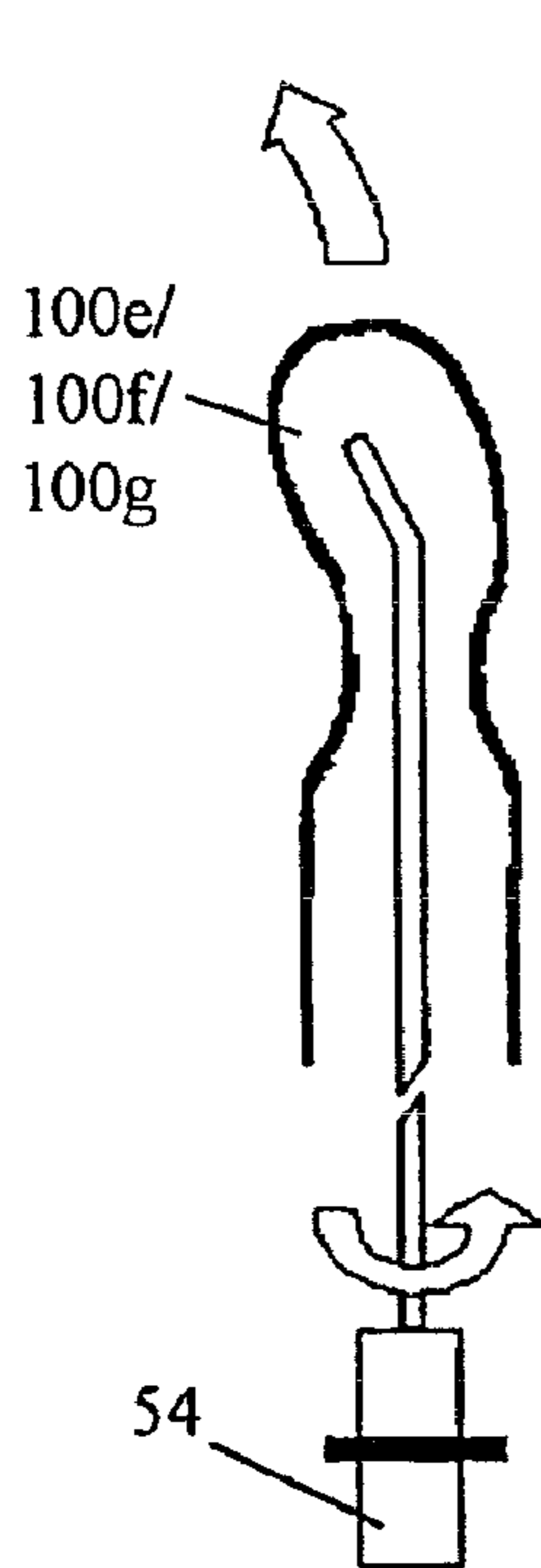
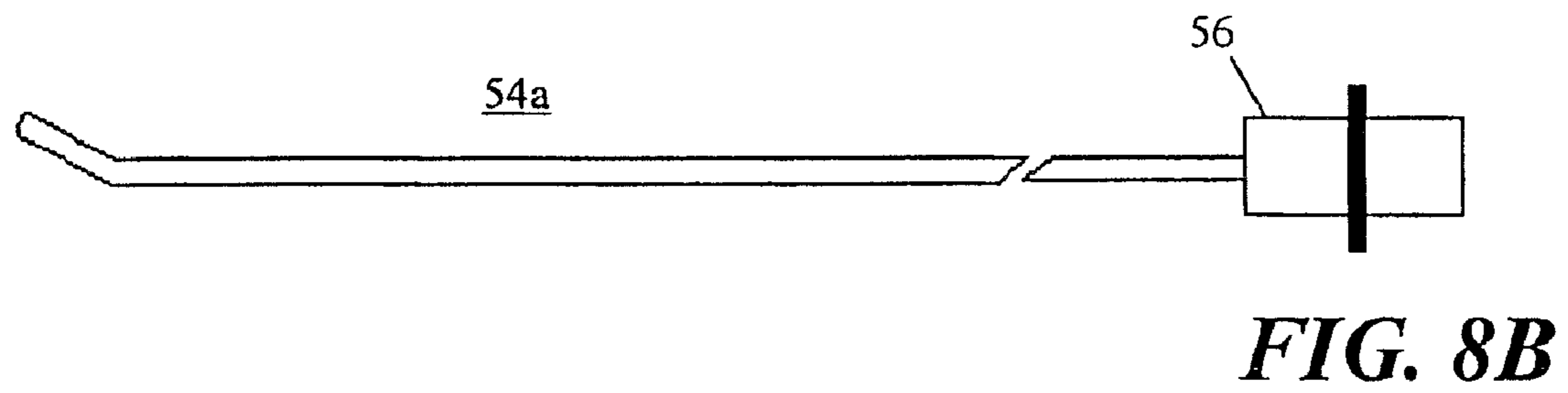
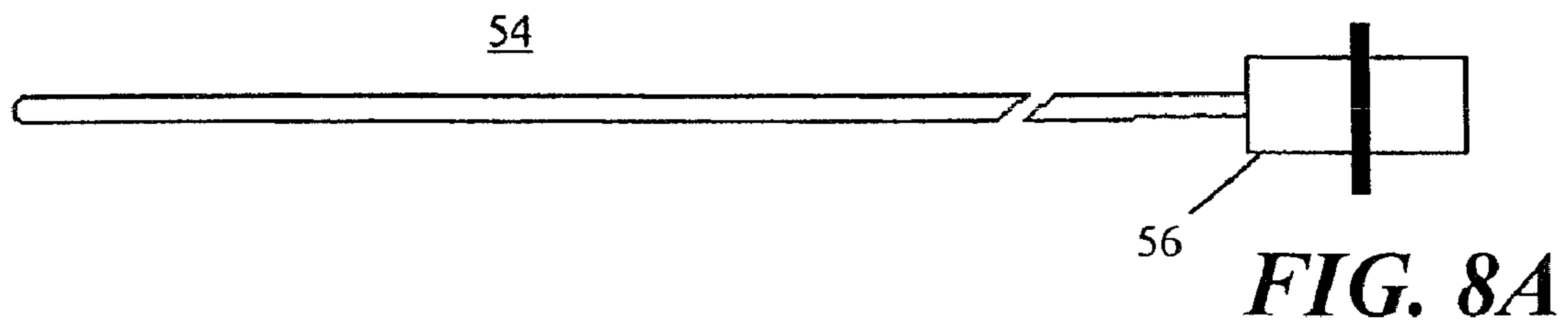
**FIG. 7A**



**FIG. 7B**



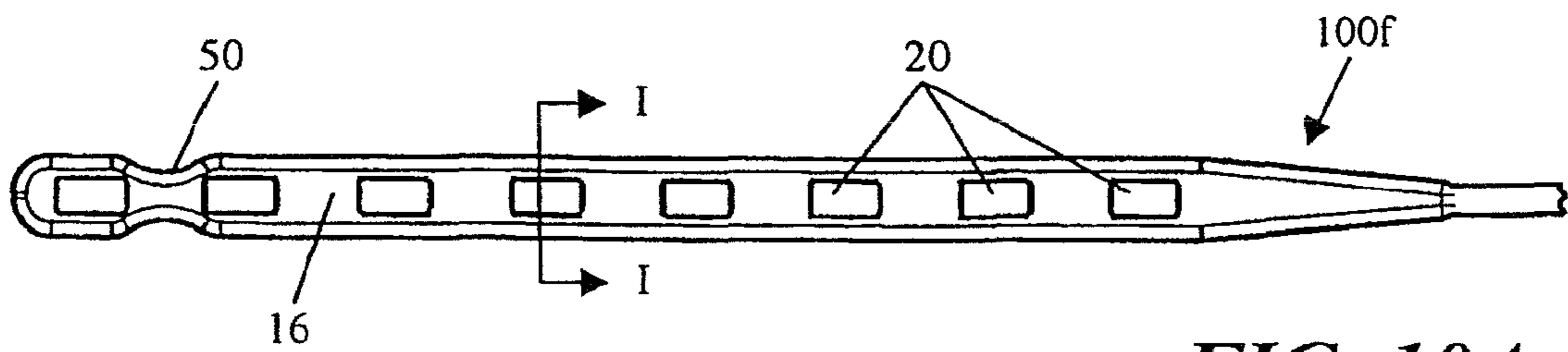
**FIG. 7C**



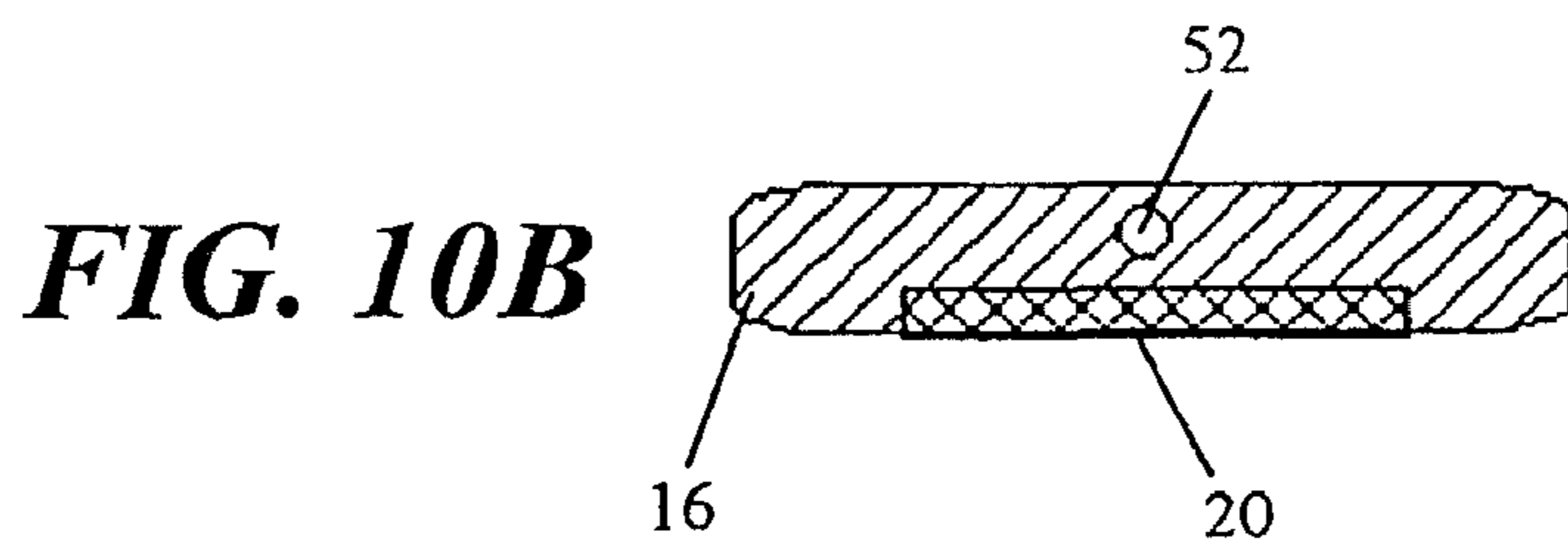
**FIG. 9A**

**FIG. 9B**

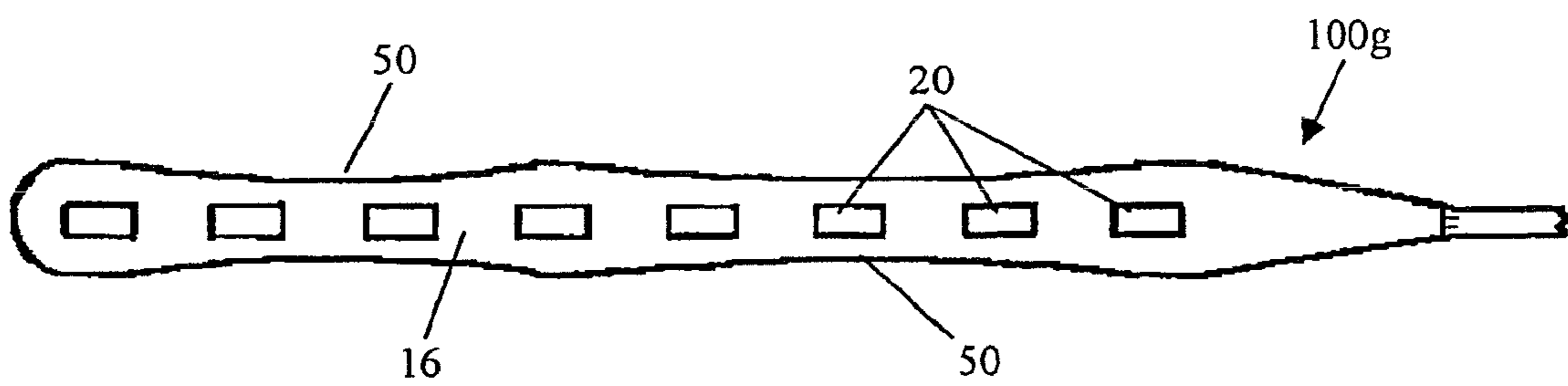
**FIG. 9C**



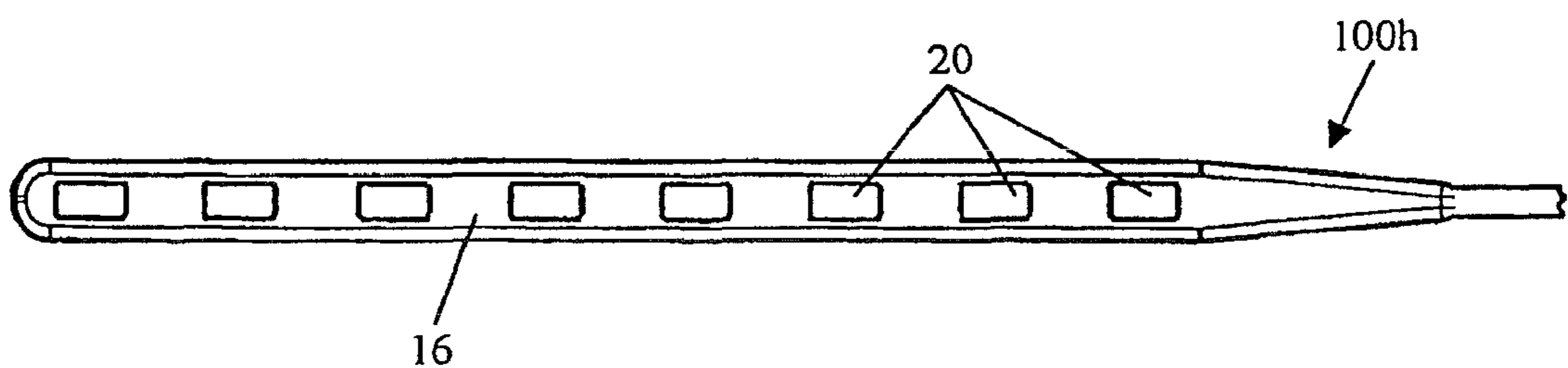
**FIG. 10A**



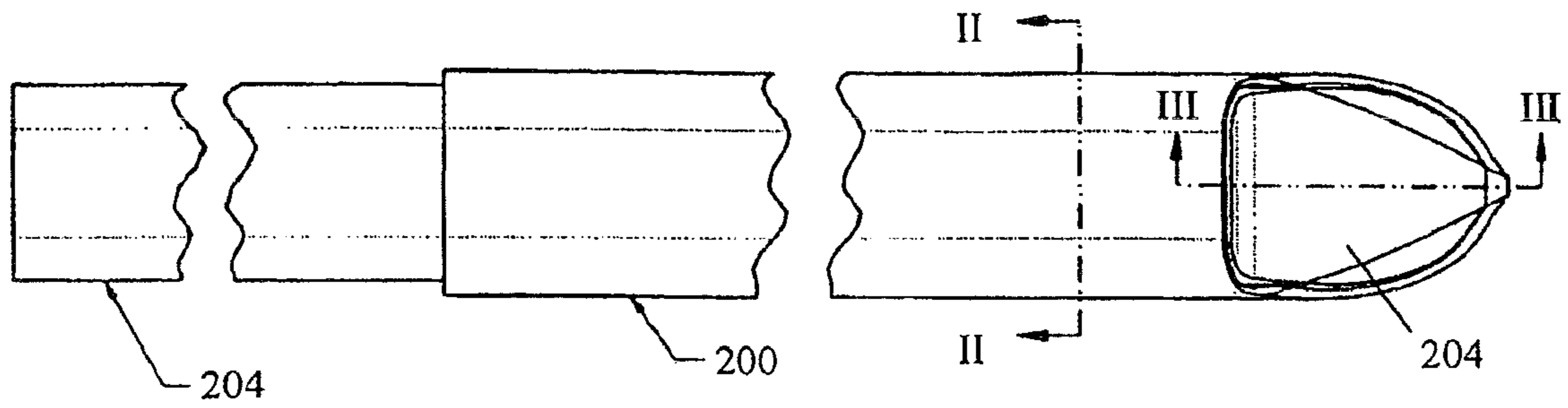
**FIG. 10B**



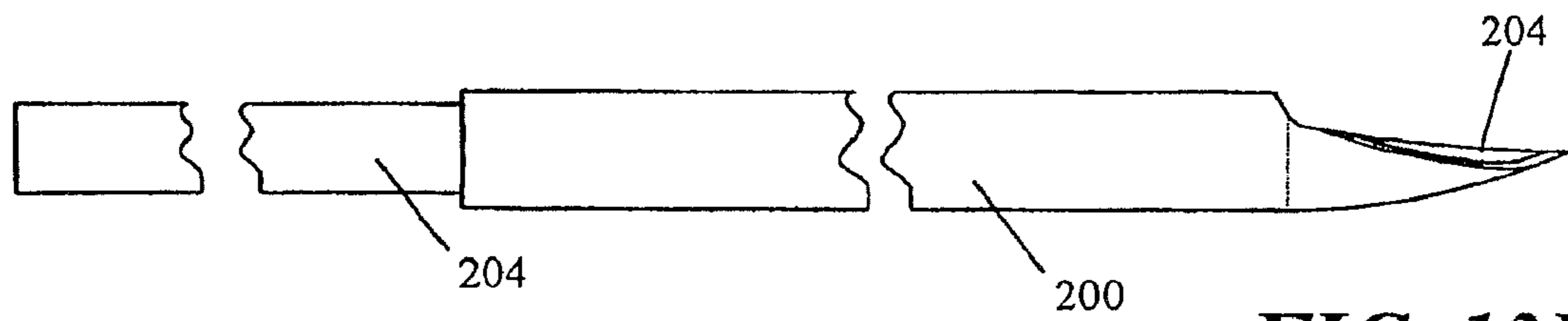
**FIG. 11**



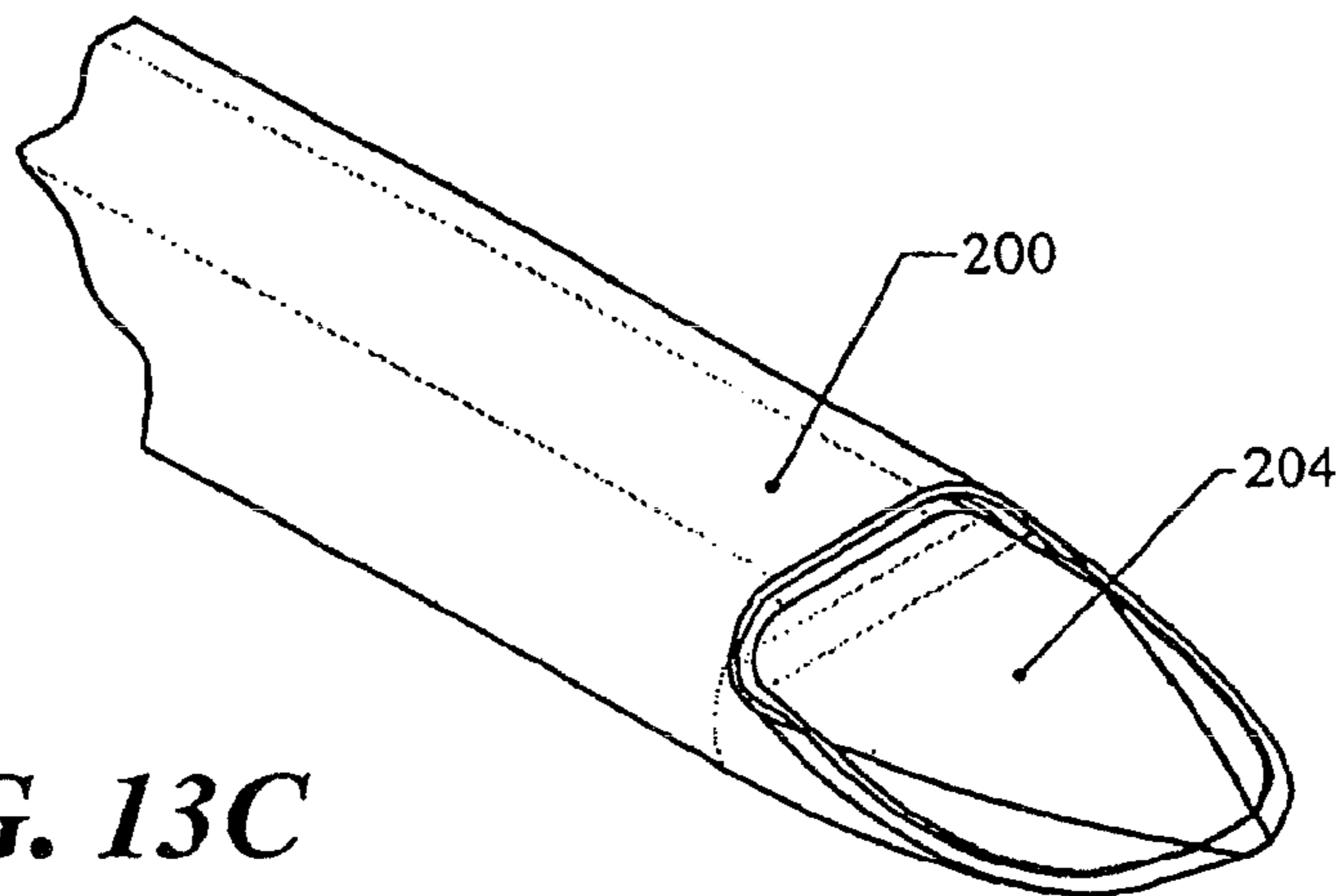
**FIG. 12**



**FIG. 13A**

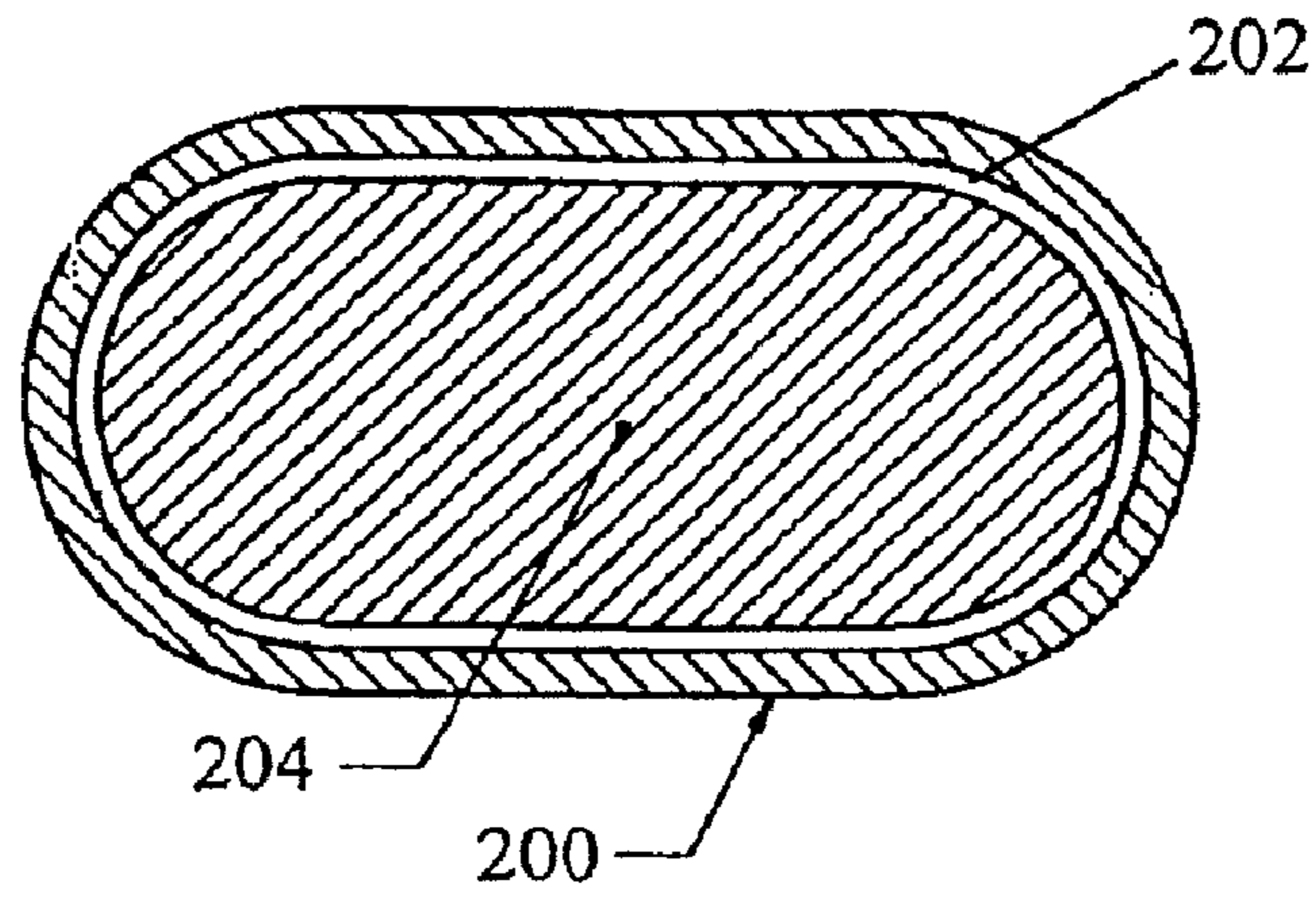


**FIG. 13B**

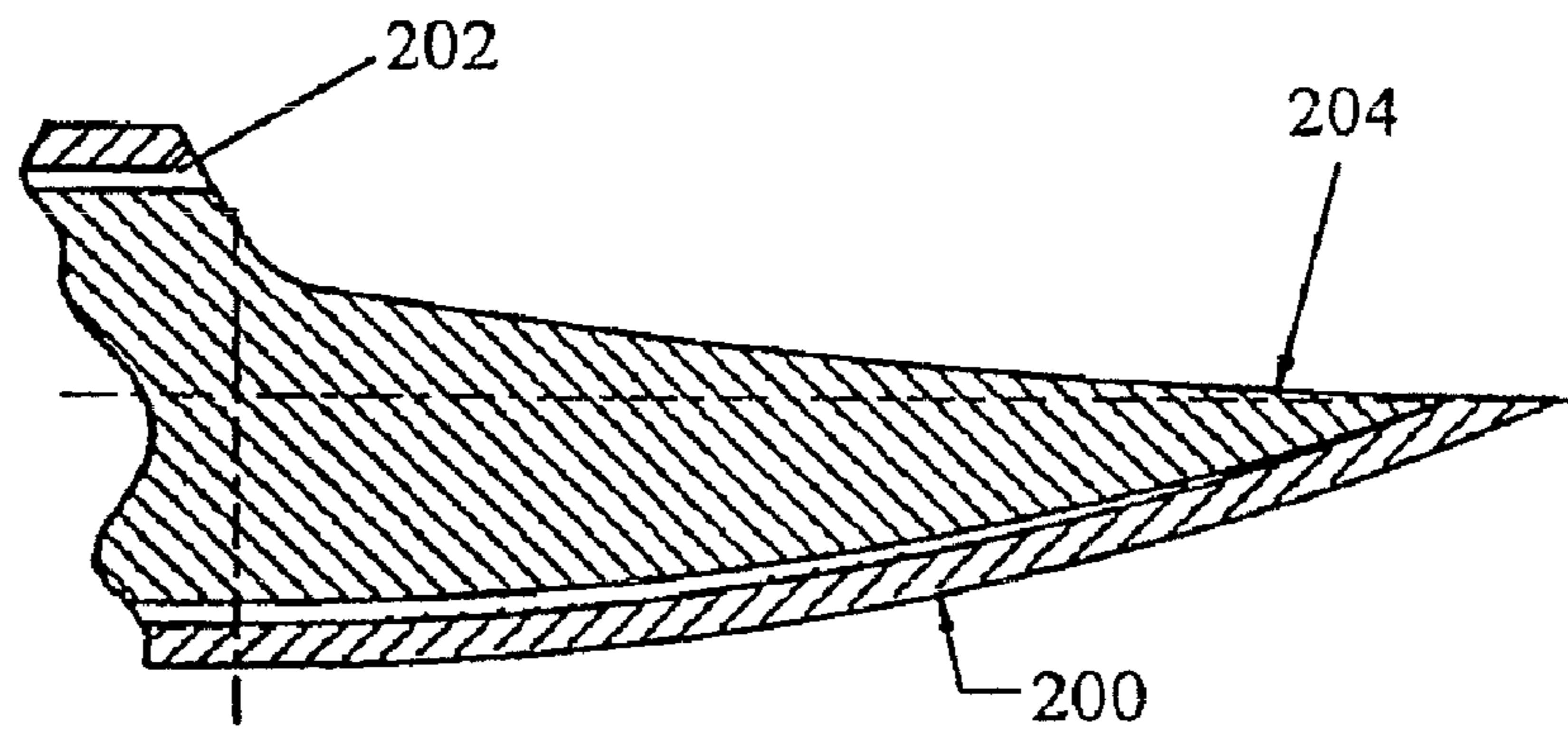


**FIG. 13C**

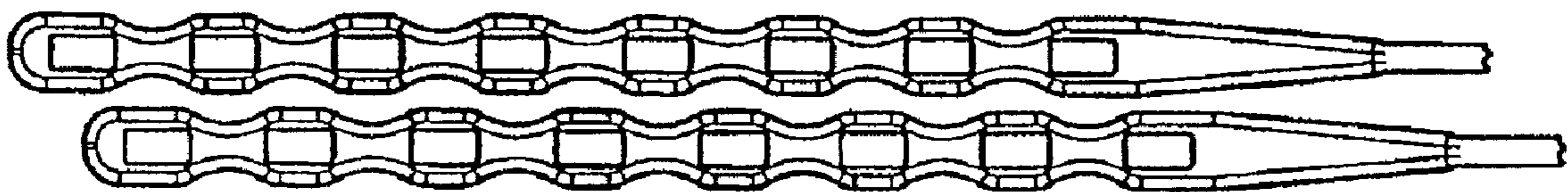




**FIG. 14**



**FIG. 15**



**FIG. 16**

## STIMULATION/SENSING LEAD ADAPTED FOR PERCUTANEOUS INSERTION

### CROSS-REFERENCE TO RELATED APPLICATIONS

This application is a continuation of U.S. application Ser. No. 11/130,000, filed May 16, 2005 now abandoned, which was a continuation of U.S. application Ser. No. 09/927,225, filed Aug. 10, 2001, now U.S. Pat. No. 6,895,283, which was a continuation-in-part of U.S. application Ser. No. 09/635,910, filed Aug. 10, 2000, now U.S. Pat. No. 6,754,539, the disclosures of which are fully incorporated herein by reference.

### TECHNICAL FIELD

The present invention relates to an epidural stimulation lead, and in particular, to an epidural stimulation lead adapted for percutaneous insertion.

### BACKGROUND

Application of specific electrical fields to spinal nerve roots, spinal cord, and other nerve bundles for the purpose of chronic pain control has been actively practiced since the 1960s. While a precise understanding of the interaction between the applied electrical energy and the nervous tissue is not fully appreciated, it is known that application of an electrical field to spinal nervous tissue (i.e., spinal nerve roots and spinal cord bundles) can effectively mask certain types of pain transmitted from regions of the body associated with the stimulated tissue. More specifically, applying particularized electrical energy to the spinal cord associated with regions of the body afflicted with chronic pain can induce paresthesia, or a subjective sensation of numbness or tingling, in the afflicted bodily regions. This paresthesia can effectively mask the transmission of non-acute pain sensations to the brain.

It is known that each exterior region, or each dermatome, of the human body is associated with a particular spinal nerve root at a particular longitudinal spinal position. The head and neck regions are associated with C2-C8, the back regions extend from C2-S3, the central diaphragm is associated with spinal nerve roots between C3 and C5, the upper extremities correspond to C5 and T1, the thoracic wall extends from T1 to T11, the peripheral diaphragm is between T6 and T11, the abdominal wall is associated with T6-L1, the lower extremities are located from L2 to S2, and the perineum from L4 to S4. By example, to address chronic pain sensations that commonly focus on the lower back and lower extremities, a specific energy field can usually be applied to a region between bony level T8 and T10. As should be understood, successful pain management and the avoidance of stimulation in unafflicted regions necessarily requires the applied electric field to be properly positioned longitudinally along the dorsal column.

Positioning of an applied electrical field relative to a physiological midline is equally important. Nerve fibers relating to certain peripheral areas extend between the brain and a nerve root along the same relative side of the dorsal column as the corresponding peripheral areas. Pain that is concentrated on only one side of the body is "unilateral" in nature. To address unilateral pain, electrical energy is applied to neural structures on the side of a dorsal column that directly corresponds to a side of the body subject to pain. Pain that is present on both sides of a patient is "bilateral." Accordingly, bilateral pain is addressed through either an application of electrical

energy along a patient's physiological midline or an application of electrical energy that transverses the physiological midline.

Pain-managing electrical energy is commonly delivered through electrodes positioned external to the dura layer surrounding the spinal cord. The electrodes are carried by two primary vehicles: a percutaneous catheter and a laminotomy lead.

Percutaneous catheters, or percutaneous leads, commonly have a circular cross-section (about 0.05 inches) and three or more, equally-spaced ring electrodes. Percutaneous leads are placed above the dura layer of a patient using a Touhy-like needle. For insertion, the Touhy-like needle is passed through the skin, between desired vertebrae, to open above the dura layer. For unilateral pain, percutaneous leads are positioned on a side of a dorsal column corresponding to the "afflicted" side of the body, as discussed above, and for bilateral pain, a single percutaneous lead is positioned along the patient midline (or two or more leads are positioned on each side of the midline).

Laminotomy leads have a paddle configuration and typically possess a plurality of electrodes (for example, two, four, eight, or sixteen) arranged in one or more columns. An example of a sixteen-electrode laminotomy lead is shown in FIG. 1. Using the laminotomy lead of FIG. 1 as but one example, the paddle portion of the laminotomy lead is approximately 0.4 inches wide and a thickness of approximately 0.065 inches. Common to laminotomy leads, the exposed surface area of the plurality of electrodes is confined to only one surface of the laminotomy lead, thus facilitating a more focused application of electrical energy.

It is typical that implanted laminotomy leads are transversely centered over the physiological midline of a patient. In such position, multiple columns of electrodes are well suited to address both unilateral and bilateral pain, where electrical energy may be administered using either column independently (on either side of the midline) or administered using both columns to create an electric field which traverses the midline. A multi-column laminotomy lead enables reliable positioning of a plurality of electrodes, and in particular, a plurality of electrode columns that do not readily deviate from an initial implantation position.

Given the relative dimensions of conventional laminotomy leads, a surgical procedure is necessary for implantation. The surgical procedure, or partial laminectomy, requires the resection and removal of certain vertebral tissue to allow both access to the dura and proper positioning of a laminotomy lead. The laminotomy lead offers a more stable platform, which is further capable of being sutured in place, that tends to migrate less in the operating environment of the human body.

Percutaneous leads require a less-invasive implantation method and, with a plurality of leads, provide a user the ability to create almost any electrode array. While laminotomy leads are likely more stable during use, these leads do not offer an opportunity for electrode array variance as the configuration of such arrays are fixed.

To supply suitable pain-managing electrical energy, stimulation leads are connected to multi-programmable stimulation systems, or energy sources (not shown). Typically, such systems enable each electrode of a connected stimulation lead to be set as an anode (+), a cathode (-), or in an OFF-state. As is well known, an electric current "flows" from an anode to a cathode. Consequently, using the laminotomy lead of FIG. 1 as an example, a range of very simple to very complex electric fields can be created by defining different electrodes in various combinations of (+), (-), and OFF. Of course, in any

instance, a functional combination must include at least one anode and at least one cathode.

Notwithstanding the range of electric fields that are possible with conventional stimulation leads, in certain instances it is necessary to concentrate electrical energy at a particular point, or over a small region. As an example of such occasion, assume pain-managing electrical energy is applied at or about T8 to address only localized lower back pain. At T8, however, spinal nervous tissue corresponding to the patient's lower extremities commingles with the specific spinal nervous tissue associated with the lower back. Moreover, it is common that the lower back-related spinal nervous tissue is deeply embedded within the combined spinal nervous tissue. It is thus desirable to focus applied electrical energy to the targeted nervous tissue to (i) reach the deeply situated target nervous tissue and (ii) avoid undesirable stimulation of unaffected regions.

Accordingly, a need exists for a percutaneously insertable stimulation lead that facilitates an application of delivered electrical energy in a manner consistent with that delivered through conventional laminotomy leads.

#### SUMMARY OF THE INVENTION

One aspect of certain embodiments of the present invention is drawn to a stimulation lead having a plurality of electrodes, a plurality of terminals, and a plurality of conductors, wherein a conductor of the plurality of conductors electrically couples one terminal of the plurality of terminals with at least one electrode of the plurality of electrodes. Although this lead is adapted to pass through a percutaneous introduction device for insertion into a human body, the lead includes a body defining a paddle structure that is substantially defined by two principal opposing planar surfaces. One of the two planar surfaces incorporate the plurality of electrodes; however, a greatest transverse dimension of the body is less than a corresponding interior dimension of a percutaneous introduction device used for insertion of the lead into a human body.

Another aspect of certain embodiments of the present invention includes providing the body of the lead with at least one waisted region that effectively increases the flexibility of the body.

Another aspect of certain embodiments of the present invention is drawn to a method of placing a lead in a human patient. This method concerns providing a lead, percutaneously accessing a site proximate to a desired lead placement site through formation of an access passage, and directing the lead through the access passage to the desired lead placement site. The lead includes a body having two principal surfaces arranged opposite to one another, each of such surfaces being substantially planar, and at least one waisted region; a plurality of terminals; a plurality of electrodes positioned relative to one principal surface of the body; and a plurality of conductors. A conductor electrically couples one terminal of the plurality of terminals with at least one electrode.

An object of certain embodiments of the present invention is to provide a paddle-type lead, capable of either delivering stimulation or sensing electrical activity, which includes a plurality of electrodes but is adapted to be inserted and positioned within a human body via percutaneous access.

Another object of certain embodiments of the present invention is to provide a paddle-type lead that includes certain features to increase the flexibility of such lead, thus enhancing the steerability of such lead.

Other objects and advantages of certain embodiments of the present invention will be apparent to those of ordinary skill in the art having reference to the following specification together with the drawings.

#### BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings, like reference numerals and letters indicate corresponding parts throughout the several views:

FIG. 1 is a plan view of a conventional laminotomy spinal cord stimulation lead;

FIG. 2 is a plan view of a laminotomy spinal cord stimulation lead that illustrates the fundamental principle of construction of one aspect of certain embodiments of the present invention;

FIG. 3 is a plan view of a first embodiment of a laminotomy spinal cord stimulation lead in accordance with one aspect of certain embodiments of the present invention;

FIG. 4 is a plan view of a second embodiment of a laminotomy spinal cord stimulation lead in accordance with one aspect of certain embodiments of the present invention;

FIG. 5 is a plan view of a third embodiment of a laminotomy spinal cord stimulation lead in accordance with one aspect of certain embodiments of the present invention;

FIG. 6 illustrates a percutaneous implantation of the laminotomy spinal cord stimulation lead of FIG. 3;

FIG. 7A illustrates a lower surface of another embodiment of a percutaneous laminotomy lead in accordance with certain embodiments of the present invention, FIG. 7B is a plan view of the percutaneous laminotomy lead of FIG. 7A, and FIG. 7C is a perspective view of the percutaneous laminotomy lead of FIGS. 7A and 7B;

FIG. 8A illustrates a straight stylet for placement within a passage formed within the percutaneous laminotomy leads of certain embodiments of the present invention, and FIG. 8B illustrates a bent stylet also for placement within a passage formed within the percutaneous laminotomy leads of certain embodiments of the present invention;

FIGS. 9A, 9B, and 9C illustrate a functional relationship between the bent stylet of FIG. 8A and the percutaneous laminotomy leads of at least one of FIGS. 7B, 10A, and 11;

FIG. 10A is a plan view of another embodiment of a percutaneous laminotomy lead in accordance with certain embodiments of the present invention, and FIG. 10B is a cross-sectional view of the percutaneous laminotomy lead of FIG. 10A as taken along line I-I;

FIG. 11 is a plan view of another embodiment of a percutaneous laminotomy lead in accordance with certain embodiments of the present invention;

FIG. 12 is a plan view of another embodiment of a percutaneous laminotomy lead in accordance with certain embodiments of the present invention;

FIG. 13A is a plan view of an insertion needle-insertion stylet combination for facilitating the implantation of a percutaneous laminotomy lead, FIG. 13B illustrates a side view of the insertion needle-stylet of FIG. 13A, and FIG. 13C is a partial perspective view of the insertion needle-stylet combination of FIGS. 13A and 13B;

FIG. 14 is a cross-sectional view of the insertion needle-stylet combination of FIG. 13A as taken along line II-II;

FIG. 15 is a cross-sectional view of the insertion needle-stylet combination of FIG. 13A as taken along line III-III; and

FIG. 16 illustrates a potential placement relationship using multiple percutaneous laminotomy leads, wherein the illustrated leads are of the form illustrated in FIG. 7A.

DETAILED DESCRIPTION OF THE PREFERRED  
EMBODIMENTS

Various embodiments, including preferred embodiments, will now be described in detail below with reference to the drawings.

In reference to FIG. 1, the illustrated laminotomy lead **10** includes a proximal end **12** and a distal end **14**. The proximal end **12** includes a plurality of electrically conductive terminals **18**, and the distal end **14** includes a plurality of electrically conductive electrodes **20** arranged within a flat, thin paddle-like structure **16**. Typically, each terminal **18** is electrically connected to a single electrode **20** via a conductor **22**; however, a terminal **18** can be connected to two or more electrodes **20**.

Terminals **18** and electrodes **20** are preferably formed of a non-corrosive, highly conductive material. Examples of such material include stainless steel, MP35N, platinum, and platinum alloys. In a preferred embodiment, terminals **18** and electrodes **20** are formed of a platinum-iridium alloy.

The sheaths **24** and the paddle structure **16** are formed from a medical grade, substantially inert material, for example, polyurethane, silicone, or the like. Importantly, such material must be non-reactive to the environment of the human body, provide a flexible and durable (i.e., fatigue resistant) exterior structure for the components of lead **10**, and insulate adjacent terminals **18** and/or electrodes **20**. Additional structure (e.g., a nylon mesh, a fiberglass substrate) (not shown) can be internalized within the paddle structure **16** to increase its overall rigidity and/or to cause the paddle structure **16** to assume a prescribed cross-sectional form (e.g., a prescribed arc along a transverse direction of the paddle structure **16**) (not shown).

The conductors **22** are carried in sheaths **24**. In the illustrated example, each sheath **24** carries eight (8) conductors **22**. Given the number of conductors **22** that are typically carried within each sheath **24**, the cross-sectional area of each conductor **22** is restricted. As but one example, for a sheath **24** in accordance with certain embodiments of the present invention, having an outer diameter of approximately 0.055 inches, each conductor **22** would be approximately 0.0065 inches in diameter.

Each conductor **22** is formed of a conductive material that exhibits desired mechanical properties of low resistance, corrosion resistance, flexibility, and strength. While conventional stranded bundles of stainless steel, MP35N, platinum, platinum-iridium alloy, drawn-brazed silver (DBS) or the like can be used, a preferred embodiment of the present invention uses conductors **22** formed of multi-strands of drawn-filled tubes (DFT). Each strand is formed of a low resistance material and is encased in a high strength material (preferably, metal). A selected number of “sub-strands” are wound and coated with an insulative material. With regard to the operating environment of certain embodiments of the present invention, such insulative material would protect each individual conductor **22** if its respective sheath **24** were to be breached during use. Wire formed of multi-strands of drawn-filled tubes to form conductors **22**, as discussed here, is available from Temp-Flex Cable, Inc.

In addition to providing the requisite strength, flexibility, and resistance to fatigue, conductors **22** formed of multi-strands of drawn-filled tubes, in accordance with the above description, provide a low resistance alternative to other conventional materials. Specifically, a stranded wire, or even a coiled wire, having a length of approximately 60 cm and formed of MP35N or stainless steel or the like would have a measured resistance in excess of 30 ohms. In contrast, for the

same length, a wire formed of multi-strands of drawn-filled tubes could have a resistance less than 4 ohms. Accordingly, in a preferred embodiment, each conductor **22**, having a length equal to or less than 60 cm, has a resistance of less than 25 ohms. In a more preferred embodiment, each conductor **20**, having a length equal to or less than 60 cm, has a resistance equal to or less than 10 ohms. In a most preferred embodiment, each conductor **20**, having a length equal to or less than 60 cm, has a resistance of less than 4 ohms.

While a number of material and construction options have been discussed above, it should be noted that neither the materials selected nor a construction methodology is critical to the present invention.

The following discussion is directed to a number of examples illustrated in FIGS. 2-5. While the examples set forth a variety of variations of the present invention, it may be readily appreciated that the present invention could take any of a variety of forms and include any number of electrodes. Importantly, however, certain embodiments of the present invention are characterized by a first electrode, or a first electrode array, that substantially encompasses or circumscribes at least one independently controlled electrode. The first electrode (or first electrode array) can operatively form an “anode guard” relative to the substantially surrounded independently controlled electrode(s). To clarify such structure, the following examples are provided.

FIG. 2 illustrates a laminotomy lead **100a** featuring the fundamental principle of construction of certain embodiments of the present invention. Specifically, the paddle structure **16** includes a plurality of electrodes **20**, wherein one electrode **30** substantially surrounds another electrode **40**. For this embodiment, each electrode is electrically coupled to an independent terminal (not shown), which is connectable to a programmable energy source, for example, a pulse generator (not shown). The construction and arrangement of the terminals (and related conductors, which establish the desired electrical coupling) are not in themselves unique but are consistent with that described hereinabove.

Depending upon a configuration/programmability of the energy source connected to the laminotomy lead **100a**, either the electrode **30** or the electrode **40** could operatively assume a positive polarity (with the remaining electrode assuming a negative polarity) during active delivery of electrical energy therefrom. For purposes of focusing applied electrical energy, however, the electrode **30** assumes a positive polarity, whereby in such a condition the electrode **30** forms an “anode guard” relative to the encompassed electrode **40**.

The electrode **30** can be constructed in a manner and from a material consistent with that used to form electrode **40**. Alternatively, as longitudinal and transverse flexibility of the paddle structure **16** are desirable, it is preferred that the electrode(s) **30** be formed so as to not otherwise significantly impair the inherent flexibility of the paddle structure **16**. Accordingly, the electrode **30** can be constructed using less material—in a thickness direction—than an electrode **40**, formed from a conductive film/foil applied to the surface of the paddle structure **16**, formed through deposition of a conductive material, constructed using a coil (FIG. 3), or formed using other like processes/techniques that are well known in the art.

An anode guard functions, in part, to laterally limit an applied electrical field, which assists in reducing extraneous stimulation of surrounding neural tissue. In this regard, neural tissue at or immediately about the cathode electrode(s) is depolarized, while neural tissue relative to the anode guard is subject to hyperpolarization. Further, an anode guard in accordance with that illustrated in FIG. 2 focuses an applied

electrical field from practically every direction to any cathode-electrode(s) positioned therein. Thus, for any given drive signal from a coupled energy source, the stimulation lead of certain embodiments of the present invention can effect a deeper application of applied energy than stimulation leads of a conventional nature.

FIG. 3 illustrates a four-channel (a “channel” represents a controllable electrical output) laminotomy stimulation lead **100b** in accordance with certain embodiments of the present invention. The stimulation lead **100b** is shown having a plurality of electrodes **20**, which includes an electrode **30**, formed from a coil, that substantially circumscribes an electrode array formed of three electrodes **40a**, **40b**, and **40c**.

Again, while each of the plurality of electrodes **20** could individually function as a cathode or an anode, or be placed in an OFF-state, it is intended that the electrode **30**, as an anode guard, assume a positive polarity. To this end, the form of an electric field generated using the electrode **30** is altered/controlled through setting each of the electrodes **40a**, **40b**, and **40c** as a cathode, an anode, or in an OFF-state. Such control over the electrodes **40a**, **40b**, and **40c** enables formation of a focused electrical field with a single electrode **40** as a cathode or a more diverse electrical field spread over two or more electrodes **40**, whereas each electrode **40** of such plurality functions as a cathode.

Furthermore, to the extent that the benefits of an anode guard are not required, the electrode **30** may be placed in an OFF-state. In such operative configuration, the laminotomy lead **100b** then functions in a manner consistent with conventional laminotomy stimulation leads.

The configuration illustrated in at least FIG. 3 enables the delivery of electrical energy to targeted nervous tissue with fewer required electrodes. Moreover, it should be noted that the compact structure (i.e., narrow transverse dimension) of the laminotomy lead **100b** enables such laminotomy lead to be implanted percutaneously, if so desired, using a special insertion needle **200** (FIG. 6) that accommodates the larger dimensions (relative to a conventional percutaneous lead) of the laminotomy lead **100b**. Of note, additional embodiments of this variation are described below in cooperation with FIGS. 7 and 10-12.

FIG. 4 illustrates a laminotomy stimulation lead **100c** in accordance with certain embodiments of the present invention. The stimulation lead **100c** includes a plurality of electrodes **20**, which includes a first electrode array having a plurality of electrodes **30a-30d** that substantially surrounds a second electrode array having a plurality of electrodes **40**.

Similar to the stimulation lead **100b**, the second electrode array of the stimulation lead **100c** is formed of a group of individual electrodes that can respectively be set as an anode, a cathode, or in an OFF-state. Although the electrodes **40** of the stimulation lead **100c** are shown in two, staggered columns, the arrangement of the electrodes **40** of the second electrode array is not critical to the present invention—the electrodes **40** of the second electrode array may assume any multiple-column arrangement.

Unlike the other embodiments illustrated, the anode guard is constructed of a first electrode array that includes electrodes **30a-30d**. In a preferred embodiment, each electrode of the first electrode array extends for a length substantially equivalent to a comparable dimension of at least two of electrodes **40** of the second electrode array. Further, and generally consistent with the structures of FIGS. 2, 3, and 5, the collection of electrodes **30a-30d** forms an effectively continuous ring that substantially extends about the second electrode array.

Although each of the electrodes **30a-30d** may be electrically independent (i.e., coupled to respective conductors/terminals), allowing each respective electrode to be an anode, a cathode, or set to an OFF-state, in consideration of practical space limitations, it may be advisable to electrically couple two or more of electrodes **30a-30d**. In a simplest form, electrodes **30a-30d** are electrically linked so as to maintain the same electrical state during operation and minimize the number of conductors necessary to couple the first electrode array to an energy source.

Depending upon the form/construction of the electrodes **30a-30d**, the segmented nature of the illustrated first electrode array of this embodiment would improve longitudinal flexibility of the paddle structure **16**. As additional segmentation of electrodes **30b** and **30d** would likewise improve transverse flexibility of the paddle structure **16**, such modification is within the scope of this embodiment of the present invention.

To maintain a generally uniform electrical field between an anode guard and one or more cathode-electrodes, the distance between the one or more cathode-electrodes and the anode guard should be largely equidistant. Achieving this optimum arrangement is typically hindered by both a need that the platform structure **16** fit easily within the narrow confines of the human epidural space and a desire that the provided electrode array(s) span a significant vertebral range of spinal nervous tissue.

While a long electrode array substantially surrounded by a single anode guard electrode (or a composite anode guard) would not be operatively ineffective, an alternative to such structure is illustrated by the stimulation lead **100d** of FIG. 5. Specifically, the electrodes **40** can be divided into groups **40a** and **40b**, and each electrode group **40a** and **40b** is encompassed by its own independently controlled anode guard electrode **30a** and **30b**.

In furtherance of the percutaneous implantation method illustrated in FIG. 6, another embodiment of a percutaneous lead **100e** is illustrated in FIGS. 7a-7c. The percutaneous lead **100e** is a “laminotomy” lead which can have the anode guard construction or it can be a non-anode guard-bearing percutaneous lead. Consistent with conventional laminotomy leads, the stimulation lead **100e** includes two principal, substantially planar surfaces, one of which carries the plurality of electrodes **20**. Unique to the percutaneous insertion-capable lead of certain embodiments of the present invention, the greatest transverse dimension (i.e., the width dimension) of the stimulation lead **100e** is preferably about 75% of a width dimension of a conventional laminotomy lead, more preferably about 50% of a width dimension of a conventional laminotomy lead, and most preferably about 40% of a width dimension of a conventional laminotomy lead. Notwithstanding these preferences, the greatest width dimension of the percutaneous laminotomy lead of certain embodiments of the present invention can be between about 20% and 40% of a conventional laminotomy lead. Further yet, it is preferable that the greatest transverse dimension of the platform structure **16** is substantially equivalent to two times (2 times) the thickness of the same.

The limiting factor for a minimum width dimension of the percutaneous laminotomy lead of certain embodiments of this invention is a maximum transverse dimension of any given electrode **20**, wherein each electrode must possess adequate surface area to effectively deliver sufficient electrical energy or sense environmental conditions.

The stimulation lead **100e** includes necked portions **50**, or “waisted” regions, wherein a transverse dimension at the necked portions **50** is less than an adjacent (e.g., maximum)

transverse dimension of the platform structure **16**. This structural configuration creates a stimulation lead having a varying cross-sectional moment of inertia, which enables a predetermined flexibility in a plane substantially parallel to the principal planar surfaces of the platform structure **16**. Improving the flexibility of the stimulation leads in this matter enhances the steerability of such stimulation leads.

As shown in FIGS. **7A** and **10B**, a channel **52** longitudinally extends through stimulation lead **100e** (FIGS. **7A** and **10B**). The channel **52** is adapted to receive a stylet **54**.

FIGS. **8A** and **8B** illustrate two configurations for a stylet. FIG. **8A** illustrates a stylet **54** having a straight distal end. If used with the stimulation lead **100e**, this stylet **54** would enable forward driving of the stimulation lead/stylet combination but would not offer an optimum structure to readily alter a course of (i.e., steer) the stimulation lead **100e** from a particular course. Conversely, FIG. **8B** illustrates a stylet **54a** having a bent (i.e., contoured) distal end. If used with the stimulation lead **100e**, this stylet **54a** would enable forward driving of the stimulation lead/stylet combination (FIG. **9B**, when the contoured end of the stylet **54a** is oriented substantially perpendicular to the principal planar surfaces of the stimulation lead **100e**) as well as directional steering. In reference to FIGS. **9A** and **9C**, when the contoured end of the stylet **54a** is oriented substantially parallel to the principal planar surfaces of the stimulation lead **100e**, the stimulation lead **100e** deforms in a direction consistent with a predetermined direction of the bent end of the stylet **54a**. Accordingly, through rotation of a bent stylet **54a**, a practitioner can purposely control and direct the stimulation lead being implanted to a desired site. Thus the combination of the curved stylet **54a** and the stimulation lead **100e** provides a stylet steerable, electric field directional, percutaneous stimulation lead. With either the straight stylet **54** or the curved stylet **54a**, the insertion of the stylet into the inner lumen the entire length of the lead provides a stiffening member for handling and placing the lead.

While the bent stylet **54** of FIG. **8B** is illustrated in one particular form, it should be readily appreciated that the contour could take any of a number of forms. In particular, the distal end of the illustrated stylet **54** could be formed so as to have a gentle bow (not shown) or include additional angles (not shown) that could heighten the nature of the deflection of the platform structure **16** when the stylet **54** is properly oriented.

It is anticipated that the handle **56** of the stylet **54** would include a marking or the like (not shown) to indicate to the user a contour direction, if any, of the stylet **54**.

For this embodiment, the stimulation lead **100e** includes a serial arrangement of waisted regions **50** that repeat along substantially an entire length of the platform structure **16** so as to maximize the flexibility of the stimulation lead **100e**. In addition to adding flexibility to the platform structure **16**, the scalloped edge of at least the stimulation lead **100e** enables multiple stimulation leads to be operatively positioned relative to one another (FIG. **16**) in close proximity. In this instance, multiple stimulation leads can be combined to effectively produce a structure akin to a conventional, non-percutaneous laminotomy lead like that illustrated in FIG. **1**.

FIG. **10A** illustrates a stimulation lead **100f** that includes a single waisted region **50**. The stimulation lead **100f** would operatively exhibit performance characteristics like the stimulation lead **100e**; however, the overall flexibility of the platform structure **16** would be arguably less. Depending upon the nature of the procedure to be performed or the environment to which a percutaneous laminotomy stimulation lead is to be inserted, it may be that the stimulation lead

**100f** may be more suitable than the stimulation lead **100e**. Moreover, while the stimulation leads **100e** and **100f** represent two extremes of this design, it is contemplated that any number of waisted regions **50** can be used for a stimulation lead depending upon a desired level of planar flexibility. To this end, an alternative design **100g** is further illustrated in FIG. **11**.

FIG. **12** illustrates a percutaneous laminotomy lead that is formed of suitable flexible material without any waisted regions **50**. Although material selection for or construction of the platform structure **16** could be used to emulate the flexibility characteristics otherwise attainable through the use of the waisted regions **50**, it may be desirable to provide a less flexible structure that simply exploits the valuable attribute of a percutaneously insertable "laminotomy" lead.

While not shown, it is contemplated that a waisted region(s) **50** could be formed in the principal planar surfaces of a platform structure of a laminotomy lead between two or more electrodes **20** so as to form thinner regions in a thickness direction. Functionally, when the contoured end of the stylet **54** of Figure **BB** is then oriented substantially perpendicular to the principal planar surfaces of a stimulation lead, at least a portion of the platform structure **16** would be caused to deform outside a non-deflected plane otherwise defined by the platform structure **16**. Accordingly, a stimulation lead having this feature would facilitate relative upward and downward movement of the platform structure **16** during insertion. While the environment of an epidural space may not require such feature, other regions of the human body or other environments may benefit from such feature. Further yet, this feature could be combined with the earlier-described, transversely oriented waisted regions **50** to enable such a lead to be steered in two dimensions. Steering control could be accomplished with multiple stylets, each stylet including a unique contour to address a corresponding waisted region, or a single stylet "keyed" to corresponding waisted regions.

Notwithstanding the plurality of configurations of the percutaneous insertion-capable stimulation leads of the present invention, FIGS. **13A** and **13B** illustrate one embodiment of the insertion needle **200** (FIG. **6**) usable to insert and place anyone of the above-discussed stimulation leads. The needle **200** defines an interior path **202** that ultimately receives and guides a stimulation lead **100** times into an epidural space. However, at least initially, the path **202** receives a stylet **204**, wherein the needle **200** and the stylet **204** combination facilitates penetration through human tissue into the patient's epidural space.

As but one example of an implantable procedure, a small incision is first made in a patient's skin using a scalpel at the desired site of insertion. Making an initial incision prevents the application of excess force to the tip of the needle **200** and further avoids the undesirable introduction of dermal matter into the epidural space. The needle **200** and the stylet **204** combination is introduced through the incision at an angle that allows passage of the needle **200** between vertebral bodies. Once the distal end of the needle **200** is positioned within and opens into the epidural space, the stylet **204** is removed to allow insertion of the platform structure **16** of a stimulation lead **100** times.

Given the increased surface area of the cross-section of the needle **200** and the stylet **204** combination (FIG. **14**), it is important that the stylet **204** efficiently integrate with the needle **200** (FIG. **15**) to provide a largely "unitary" surface that facilitates penetration through the tissue that encompasses an epidural space.

A lamitrode epidural needle having a generally rectangular passageway can be employed for the insertion of the percu-

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taneous stimulation lead, as an example, the generally rectangular passageway can have a height in the range of one to two millimeters and a width in the range of two to four millimeters, with the width to height ratio being approximate 2:1. While a needle is one type of percutaneous introduction device, there are other known percutaneous introduction devices and methods available, e.g., a dilating catheter can be employed in the form of a silicone sleeve surrounding a needle for the initial insertion through the skin, with removal of the needle after the insertion of the sleeve through the skin, followed by insertion of a dilator into the hollow sleeve to expand the sleeve. The dilator can have a hollow passage for the insertion of the stimulation lead of certain embodiments of the present invention.

While the invention has been described herein relative to a number of particularized embodiments, it is understood that modifications of, and alternatives to, these embodiments, such modifications and alternatives realizing the advantages and benefits of this invention, will be apparent to those of ordinary skill in the art having reference to this specification and its drawings. It is contemplated that such modifications and alternatives are within the scope of this invention as subsequently claimed herein, and it is intended that the scope of this invention claimed herein be limited only by the broadest interpretation of the appended claims to which the inventors are legally entitled.

What is claimed is:

1. A method for implanting a stimulation lead into the epidural space of a patient, the method comprising:  
 inserting a needle through tissue of the patient until a tip of the needle is disposed within the epidural space of the patient;

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inserting a stiffening stylet into a stimulation lead through an internal stylet guide of the stimulation lead, wherein the stimulation lead further comprises a plurality of terminals at a proximal end of the stimulation lead, the stimulation lead comprises a body at a distal end of the stimulation lead, the body including two principal opposing planar surfaces with electrodes arranged on one of the planar surfaces, and the body having a first portion at a distal end of the body, the first portion of the body being flexible in a plane substantially parallel to the planar surfaces, and the stylet guide extends the proximal end to the distal end, and wherein after the inserting is performed, an end of the stylet is disposed at a distal end of the body of the stimulation lead;  
 advancing the stimulation lead with the stiffening stylet through the needle and into the epidural space of the patient; and  
 removing the needle from the epidural space of the patient.

2. The method of claim 1 wherein the electrodes are arranged in a linear column along the body of the stimulation lead.

3. The method of claim 1 further comprising:  
 steering the body of the stimulation lead within the epidural space in a direction transverse to the spinal cord of the patient by manipulating an orientation of a bent distal end of the stylet causing the first portion of the body to flex in a plane substantially parallel to the planar surfaces.

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