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(54) **BATTERY STATE MONITORING CIRCUIT AND BATTERY APPARATUS**

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H01M 10/46 (2006.01)

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(58) **Field of Classification Search** 320/103,
320/114, 116, 117, 132, 134, 136, 149; 324/426,
324/427, 430, 433

See application file for complete search history.

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(57) **ABSTRACT**

Provided is a battery state monitoring circuit which is capable of preventing a discharge leak current from a battery so as to eliminate a load conventionally imposed on a user, including: a battery state detector circuit that detects a state of the battery based on a voltage of the battery; a transmitting terminal that transmits battery state information indicative of the state of the battery to an outside; a receiving terminal that receives battery state information of another battery from the outside; a transistor that is used for transmitting the battery state information, and has any one of two terminals except for a control terminal connected to the transmitting terminal; and a diode that is connected in a direction opposite to a direction of a parasitic diode disposed between the two terminals of the transistor, the diode being disposed between the transmitting terminal and one terminal of the transistor.

18 Claims, 15 Drawing Sheets

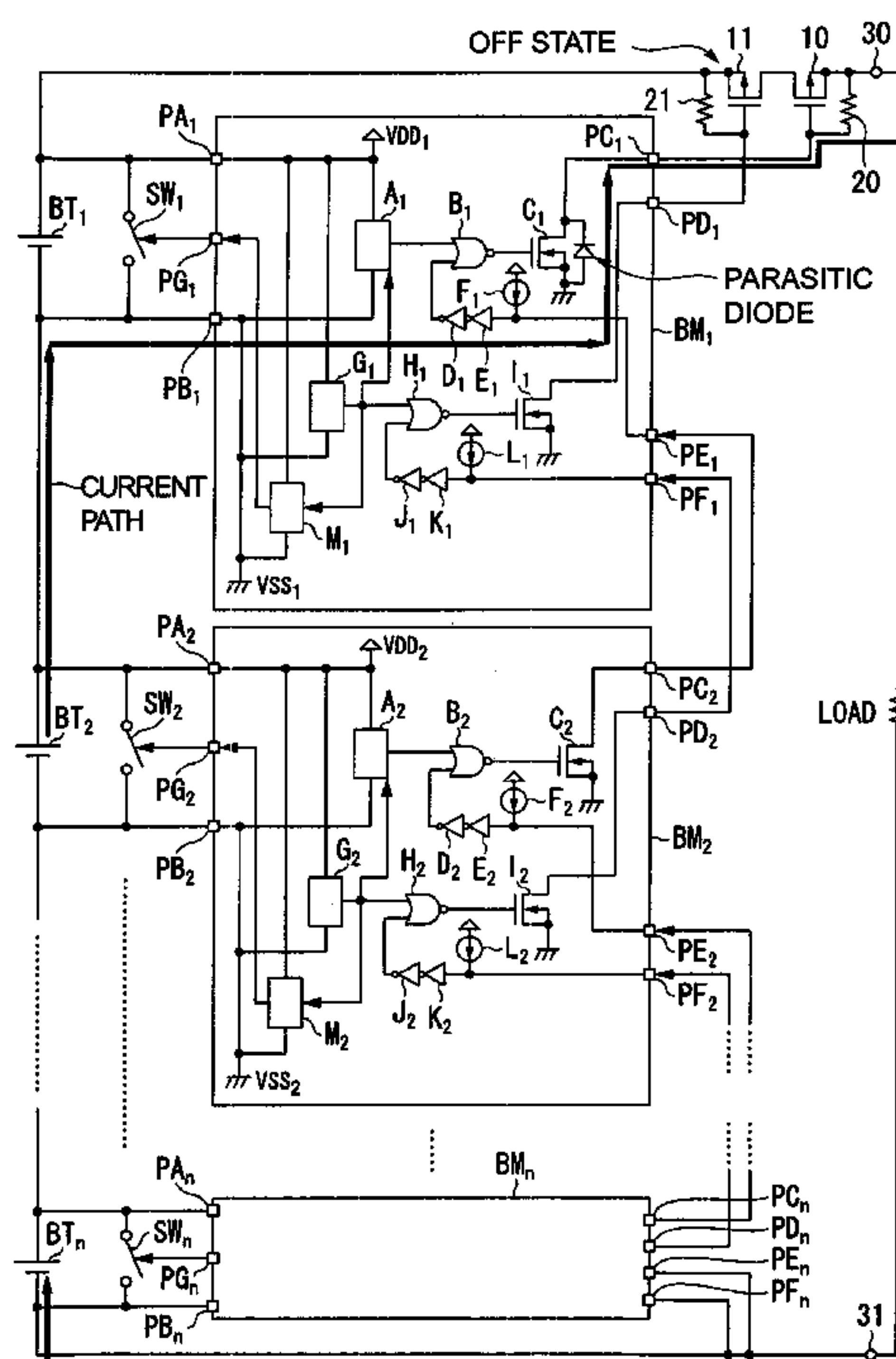


FIG. 1

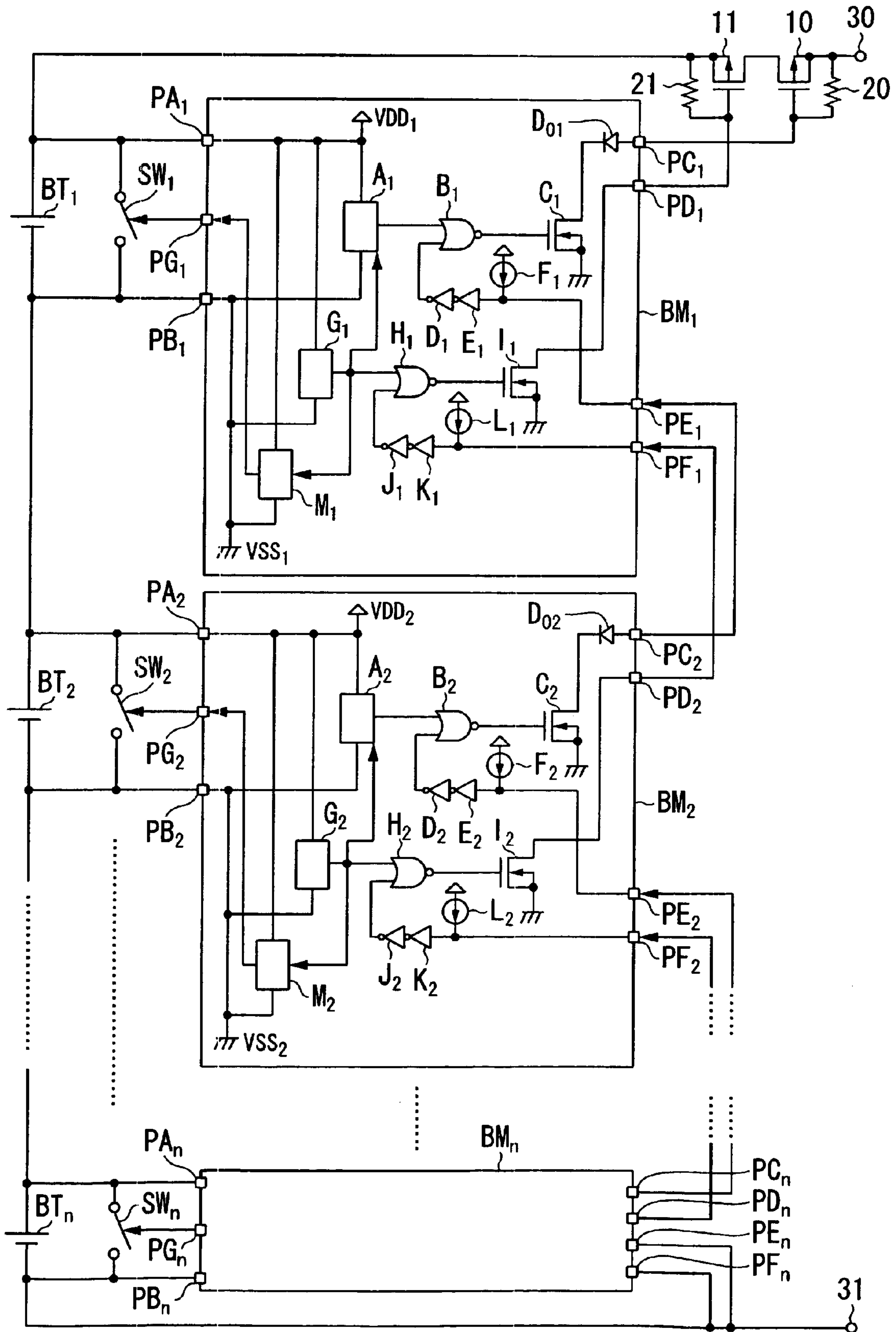


FIG. 2

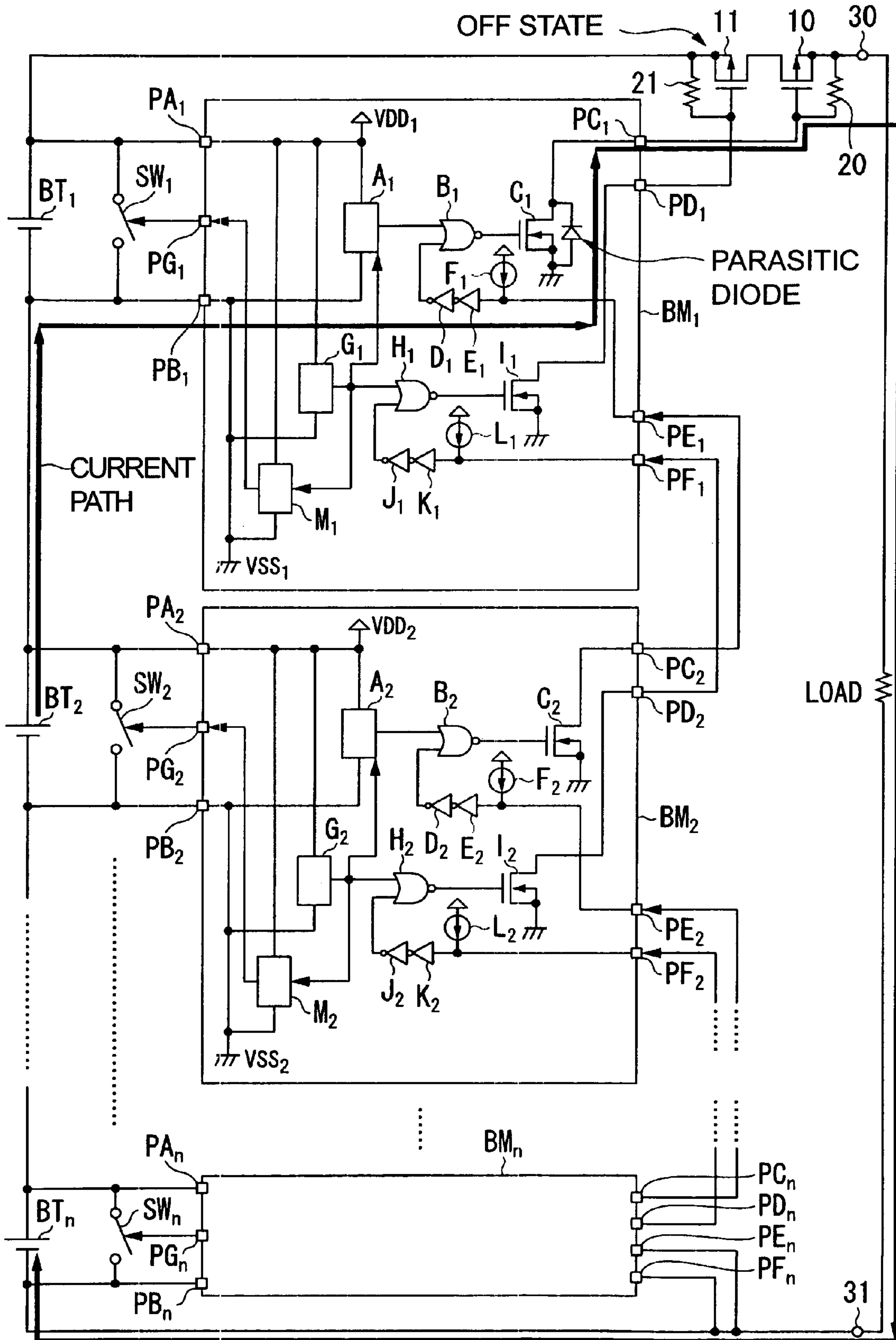


FIG. 3

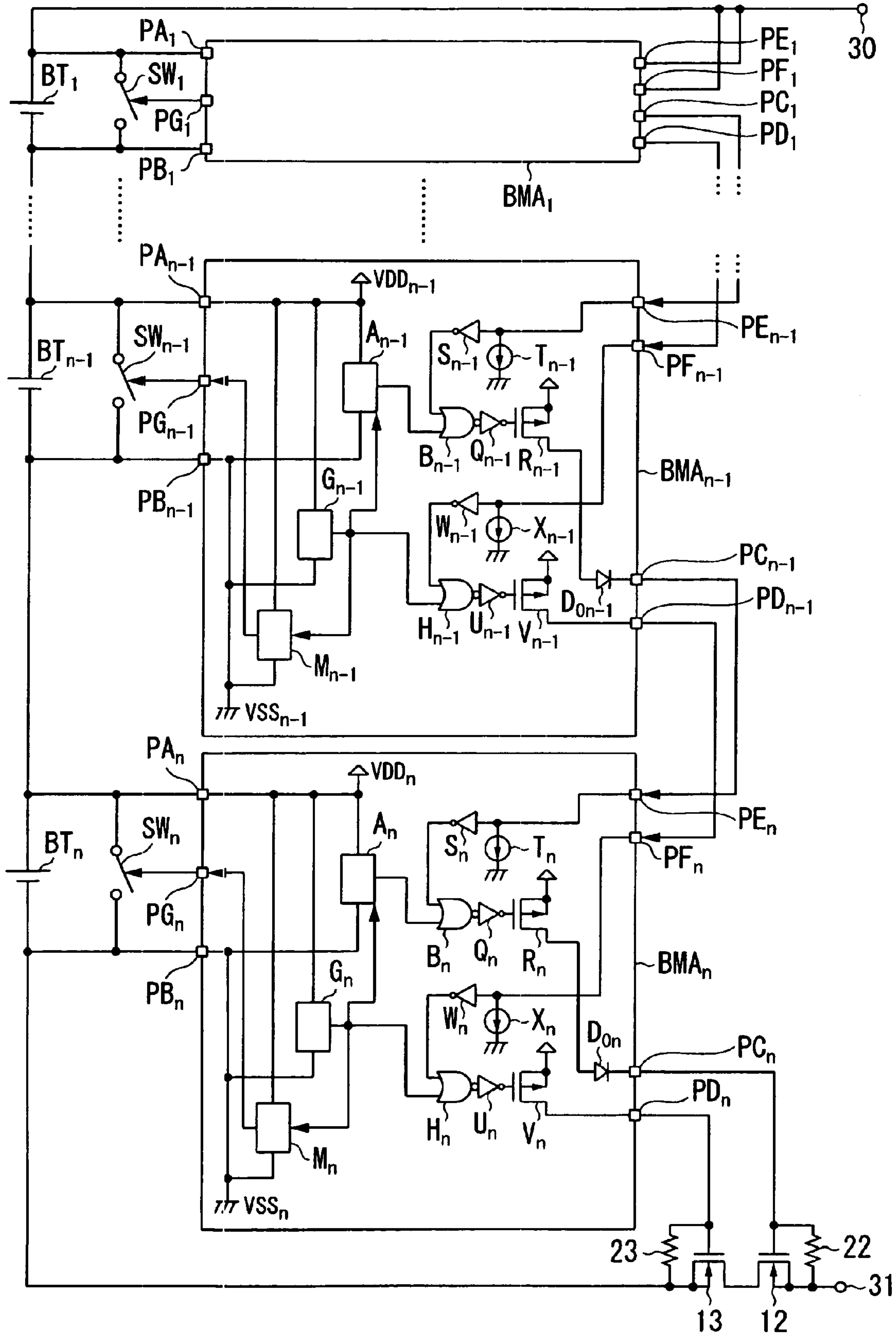


FIG. 4

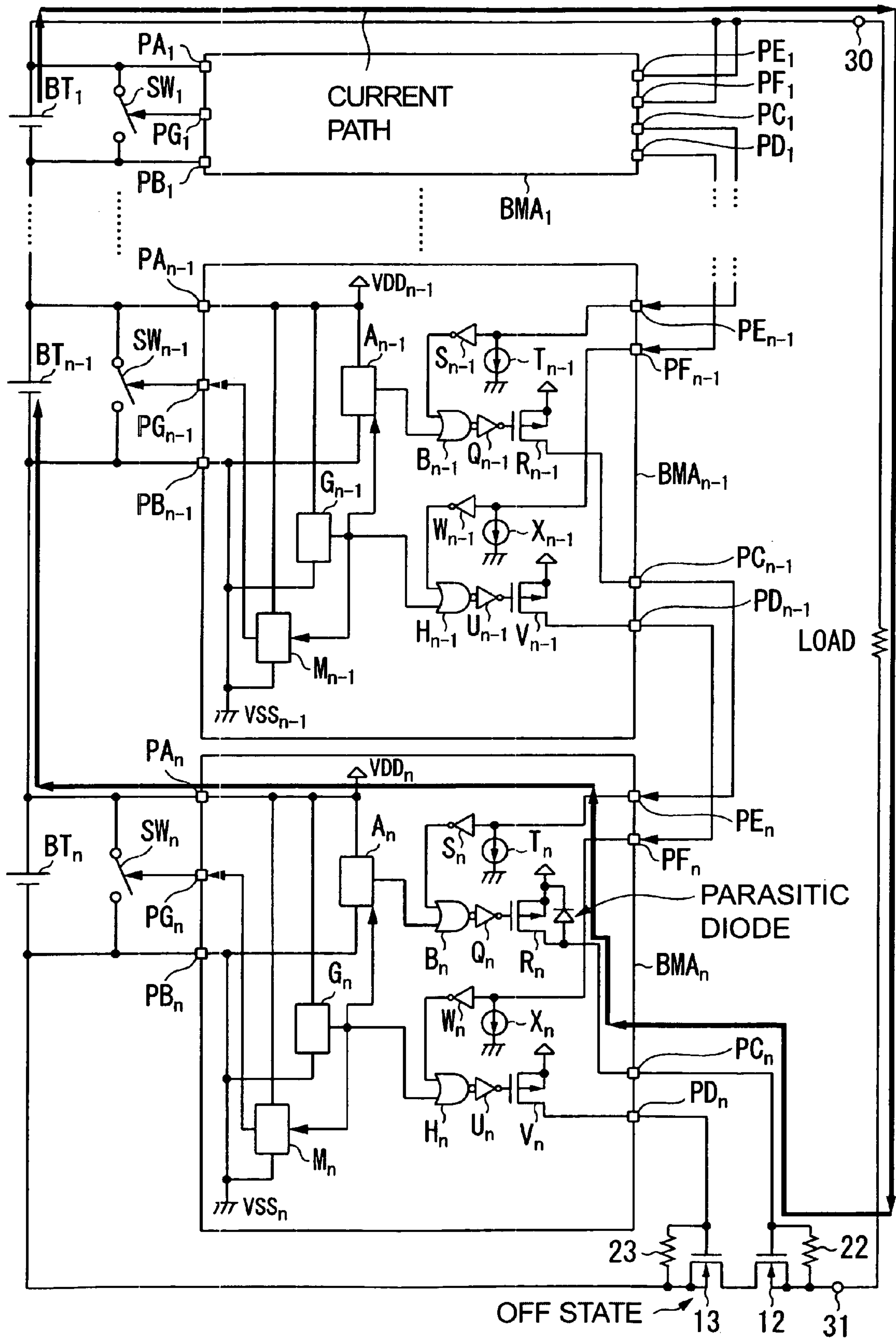


FIG. 5

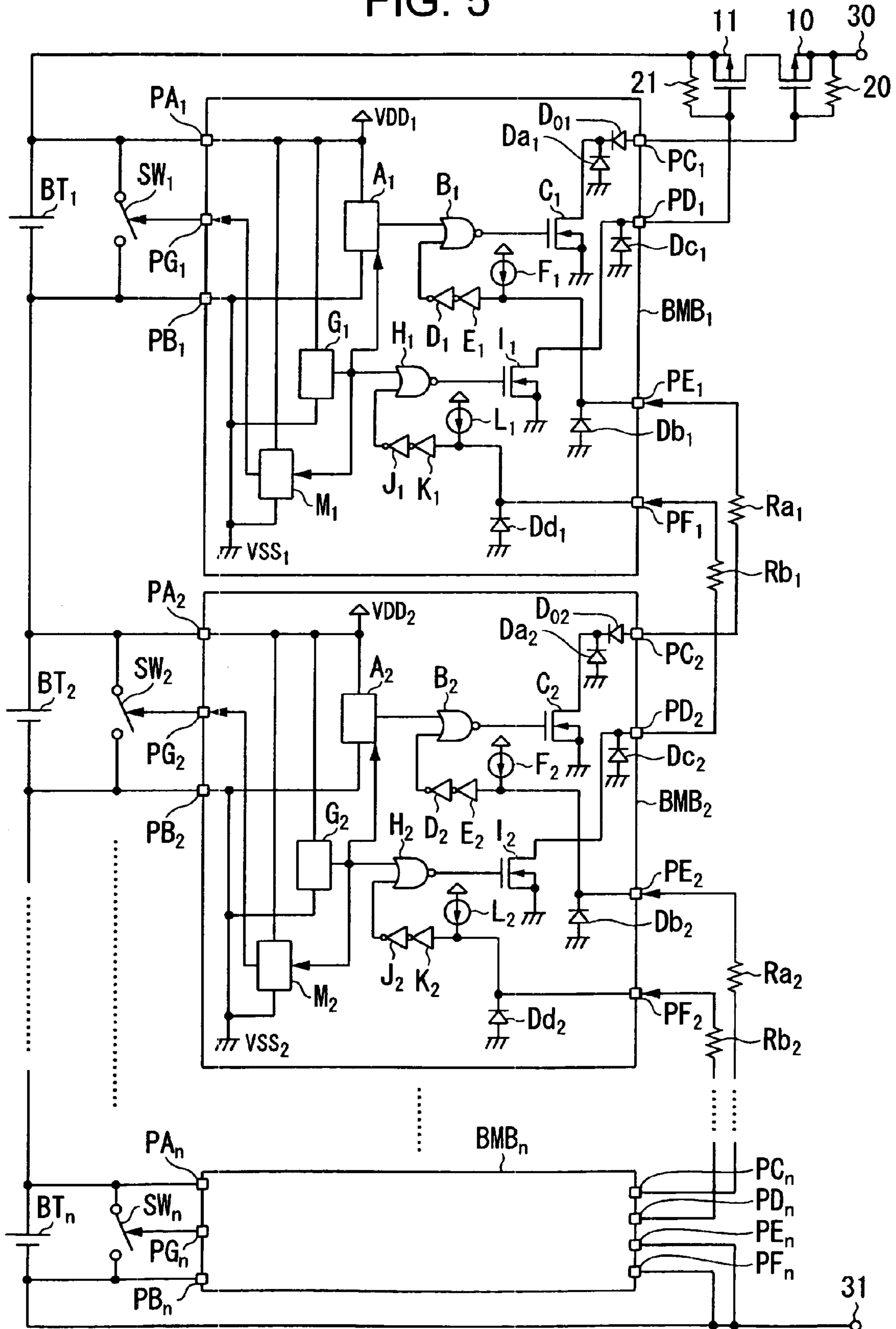


FIG. 6

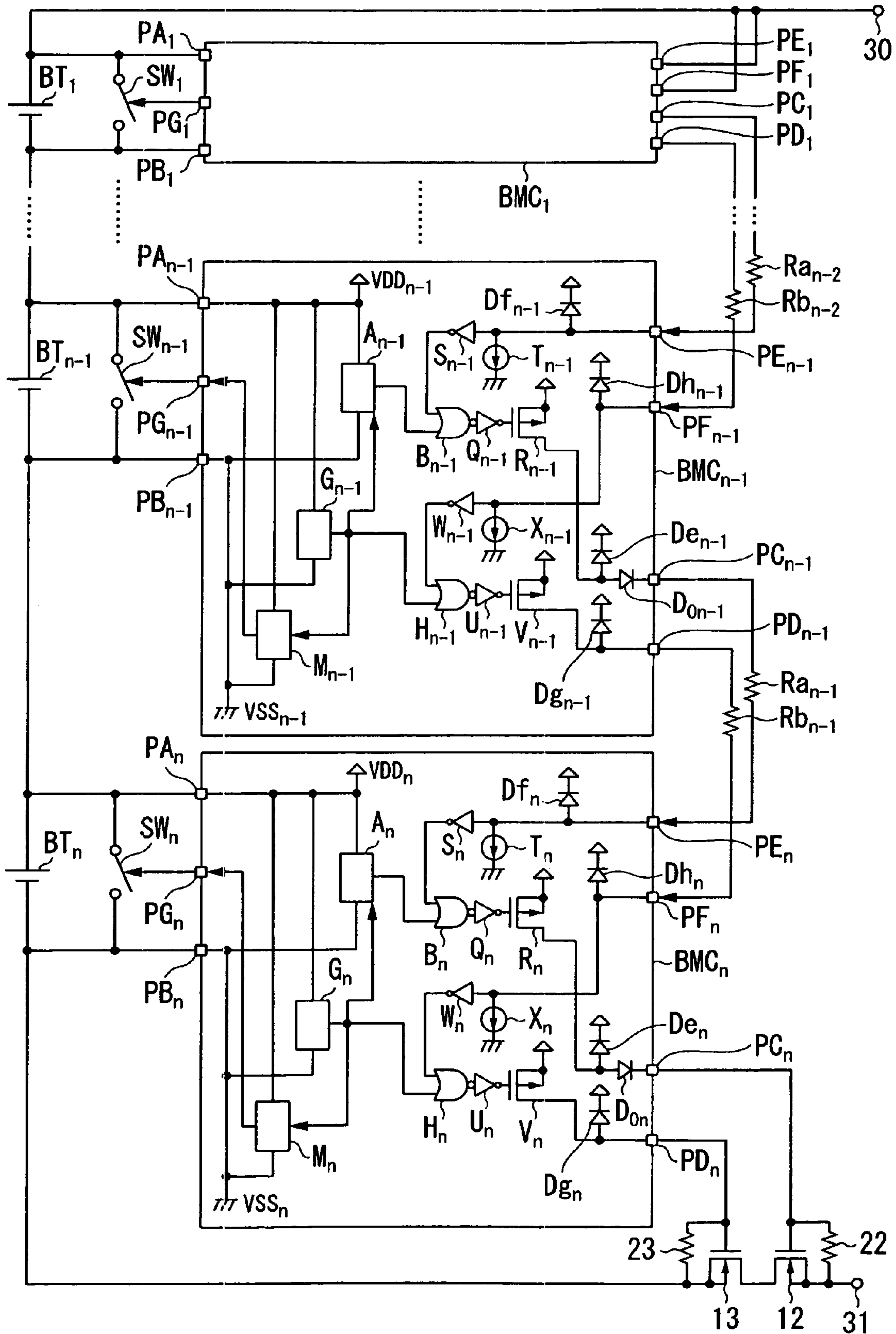


FIG. 7

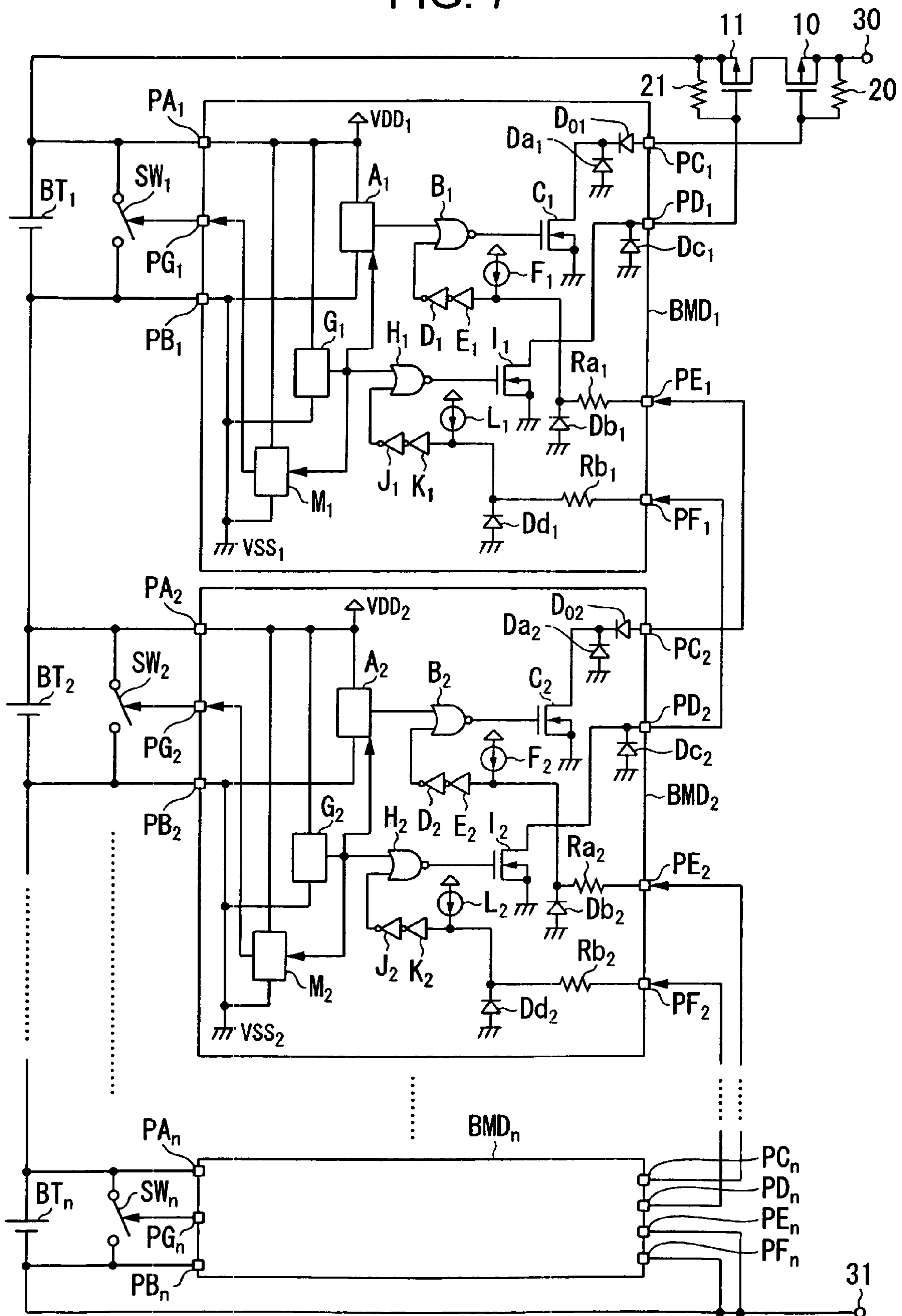


FIG. 9

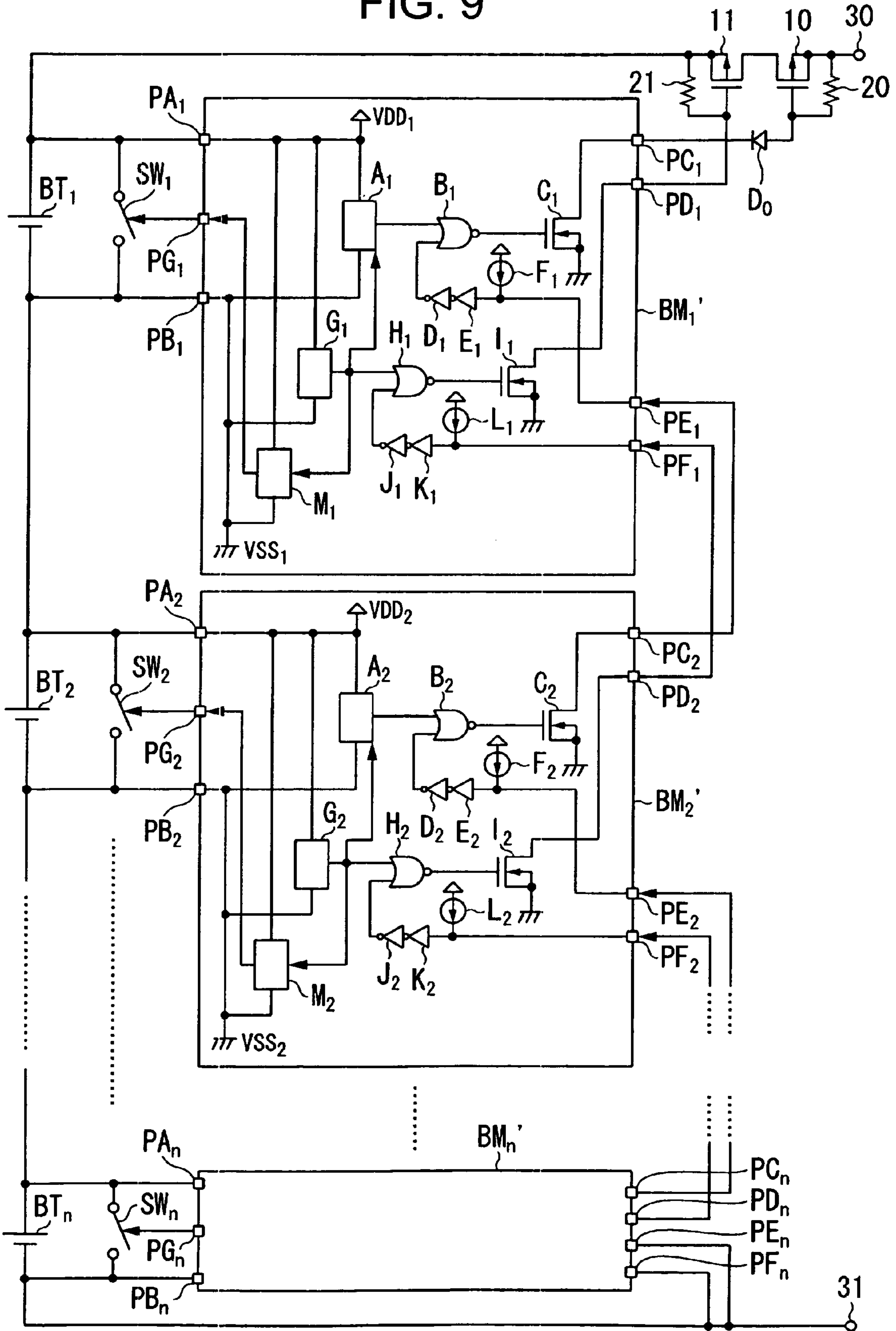


FIG. 10

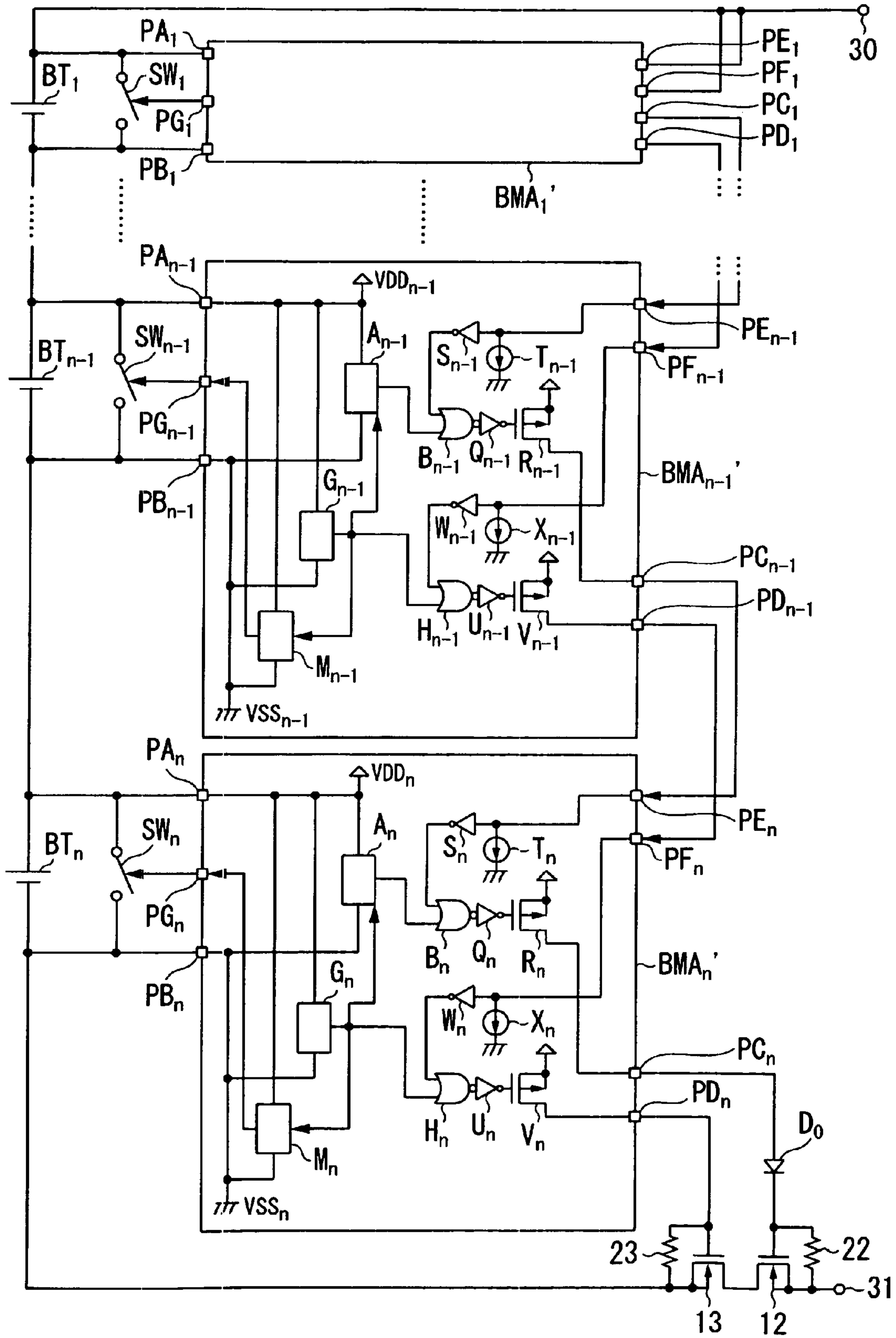


FIG. 11

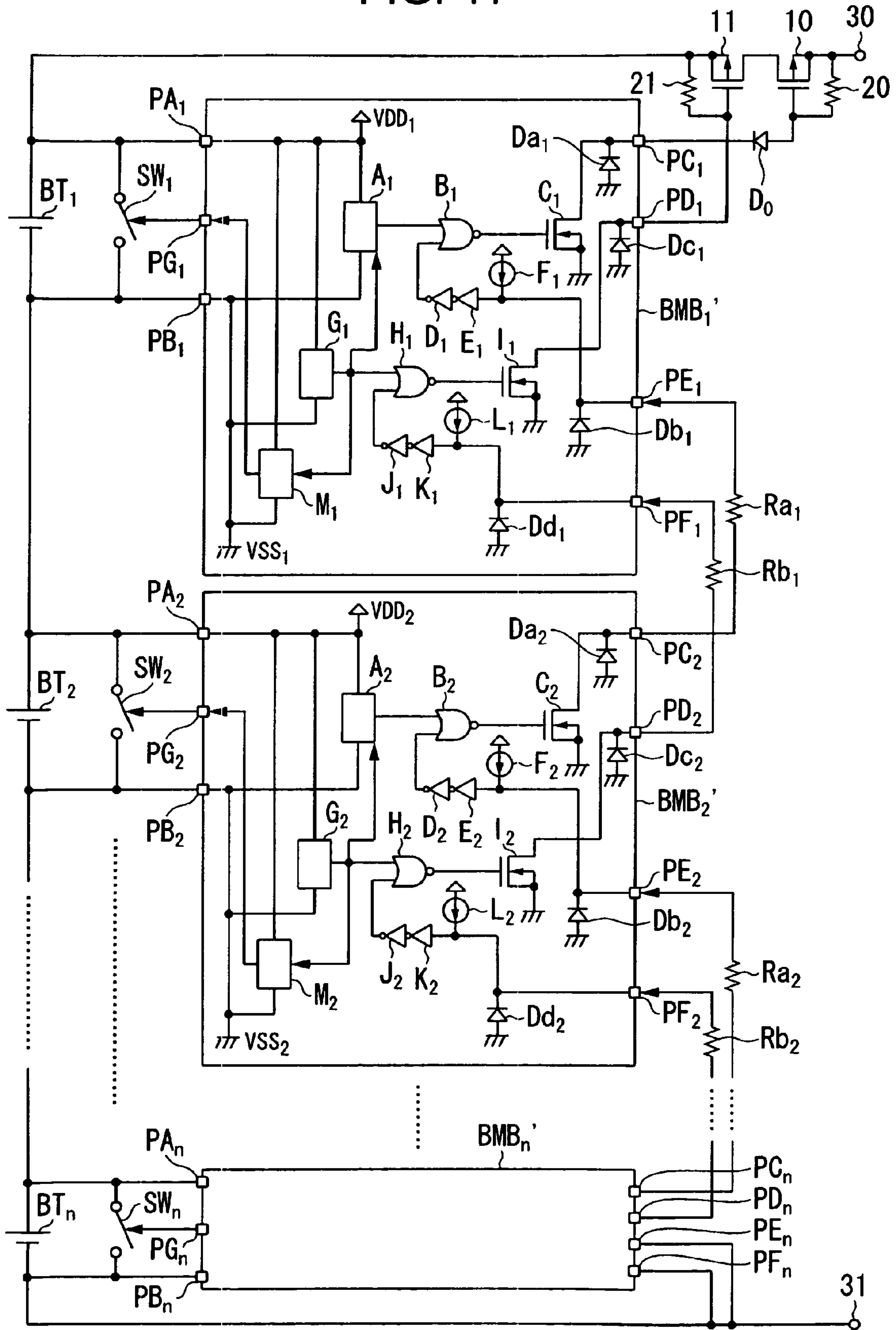


FIG. 12

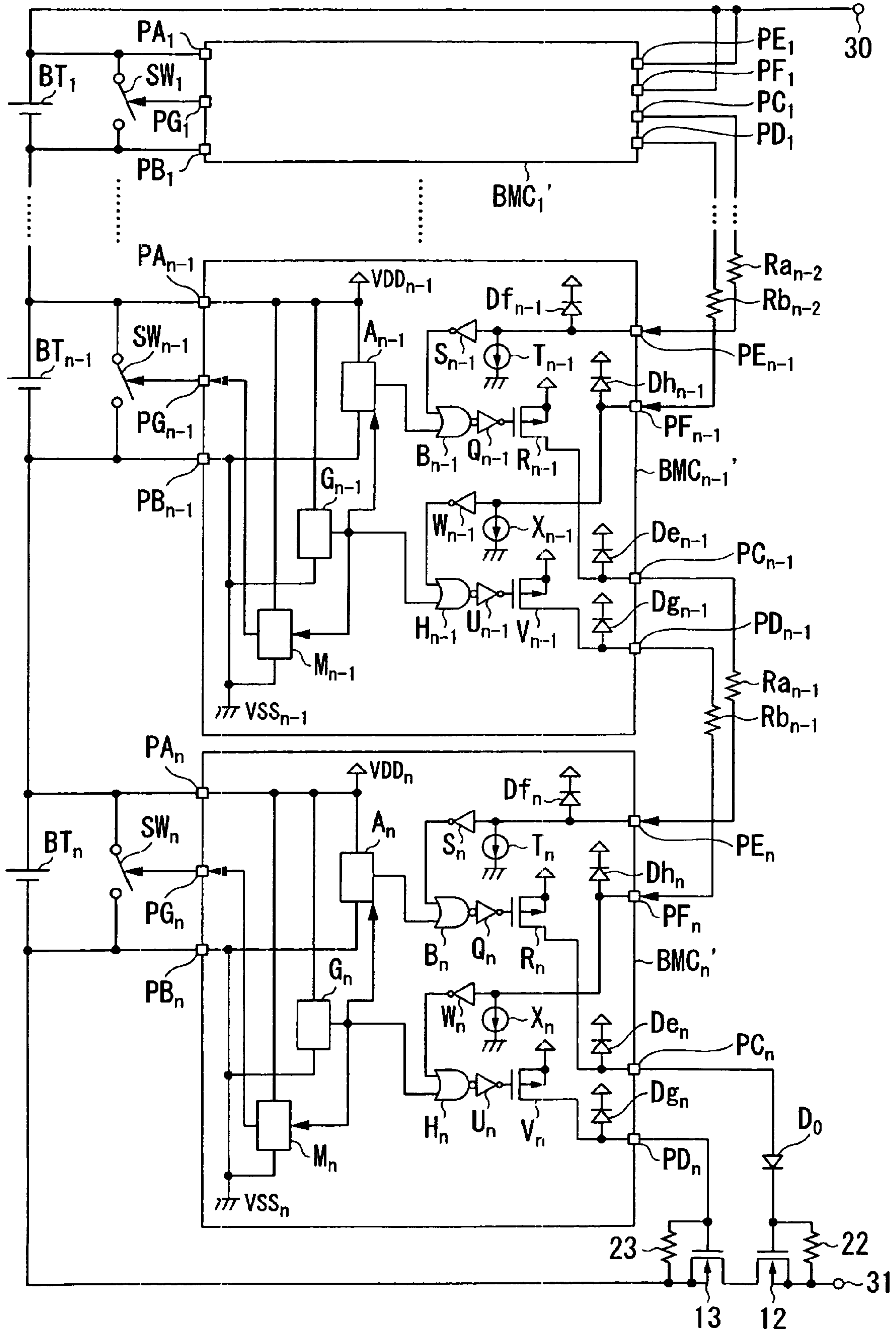


FIG. 14

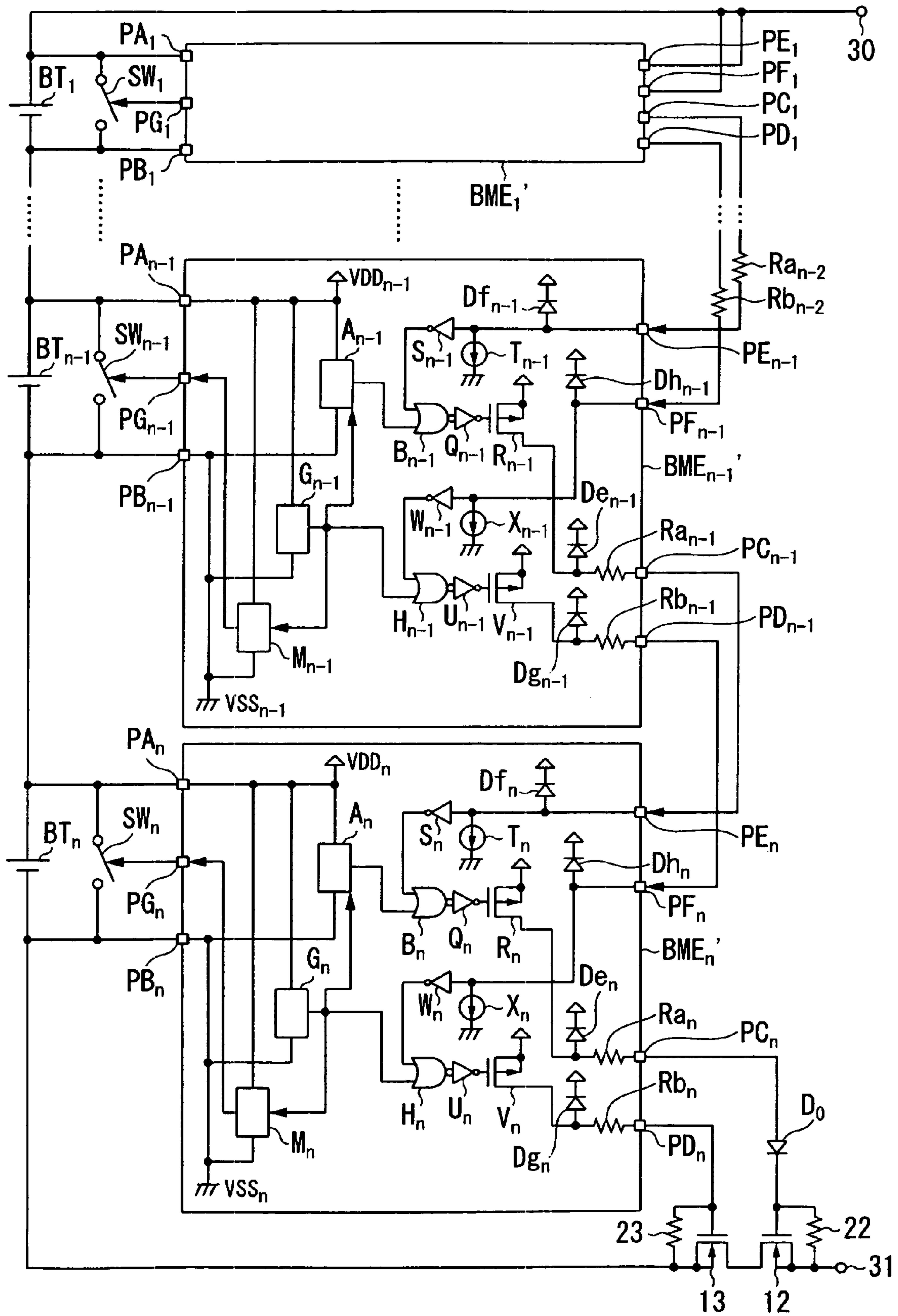


FIG. 15A PRIOR ART

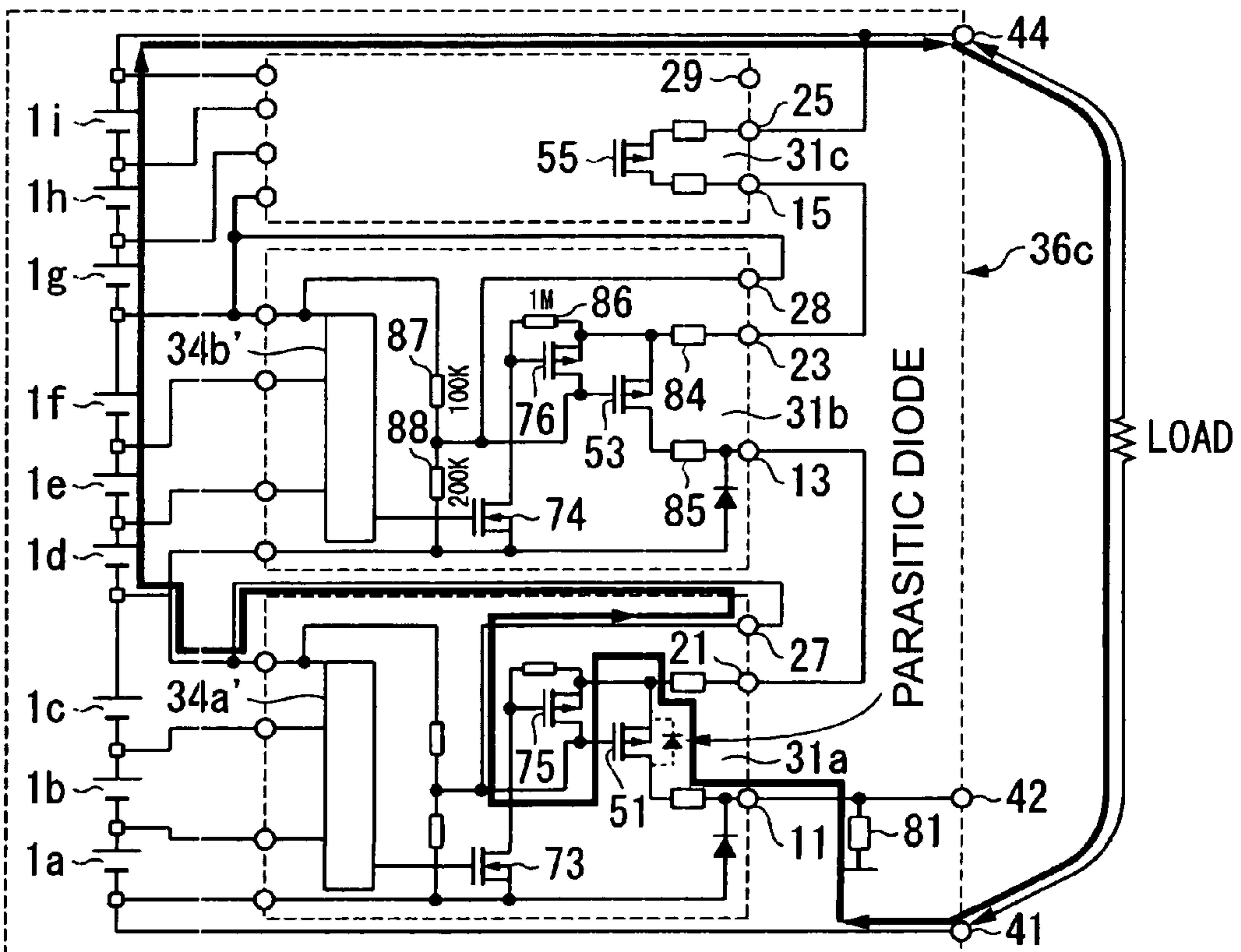
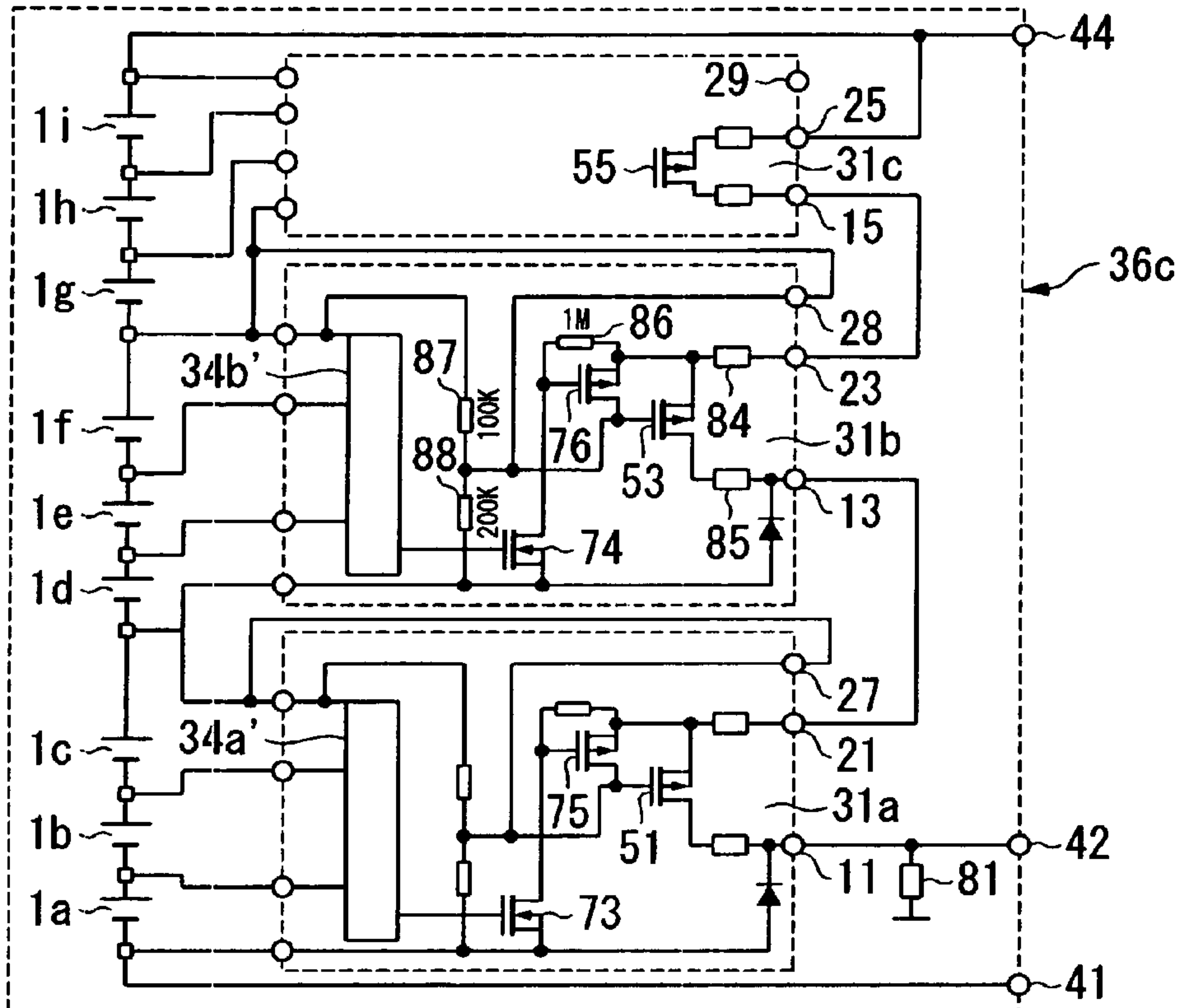


FIG. 15B PRIOR ART

BATTERY STATE MONITORING CIRCUIT AND BATTERY APPARATUS

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a battery state monitoring circuit that monitors a state of a battery, and a battery device that is equipped with a plurality of the battery state monitoring circuits.

2. Description of the Related Art

For example, JP 2005-117789 A discloses a protective IC that monitors voltages of a plurality of batteries that are connected in series with each other. FIG. 15A shows an example of the protective IC that is disclosed in JP 2005-117780 A. Referring to FIG. 15A, reference numbers **31a**, **31b**, and **31c** denote protective ICs, respectively. The protective IC **31a** monitors the voltages of batteries **1a** to **1c**, the protective IC **31b** monitors the voltages of batteries **1d** to **1f**, and the protective IC **31c** monitors the voltages of batteries **1g** to **1i**, respectively. In a normal state, that is, when the voltages of the batteries **1a** to **1i** are not abnormal, because all FETs **51**, **53**, and **55** of the respective protective ICs **31a**, **31b**, and **31c** are on, a current flows through a resistor **81**, and a monitor output terminal **42** becomes at high level. On the other hand, for example, when the voltage of any one of the batteries **1a** to **1c** becomes overvoltage (overcharged state), a signal of high level is output from an overvoltage detector circuit **34a'** that is disposed in the protective IC **31a** with the results that an FET **73** is turned on, and an FET **75** is turned on. In this situation, because the FET **51** is turned off, no current flows in the resistor **81**, and the monitor output terminal **42** becomes at low level. The same is applied to overdischarge detection.

As described above, when the voltage of any one of the batteries **1a** to **1c** becomes overvoltage, the monitor output terminal **42** becomes at low level because the FET **73** is turned on, the FET **75** is turned on, and the FET **51** is turned off. However, a parasitic diode having an anode terminal connected to a drain terminal of the FET **51** and a cathode terminal connected to a source terminal of the FET **51** exists between the drain terminal and a gate terminal of the FET **51**. Therefore, when a load is connected between external terminals **41** and **44** in the above state, a current path is formed as shown in FIG. 15B, which leads to such a problem that electricity is discharged from the batteries **1d** to **1i** to generate discharge leak current.

The voltages of the batteries **1d** to **1i** are decreased due to an influence of the above discharge leak current, but the other batteries **1a** to **1c** have the high voltage close to the overvoltage. As a result, the voltage balance of the batteries **1a** to **1i** is disrupted. A state in which the voltage balance is disrupted is advanced so that the batteries **1a** to **1c** become voltages close to the overvoltage, and the batteries **1d** to **1i** become voltages close to overdischarge. As a result, because the overvoltage is detected by small charge, charging cannot be conducted. Also, because the overdischarge is detected by slightly using an application program, the batteries cannot be used. Such batteries are exchanged with fresh batteries. However, because the phenomenon of the discharge leak current is repeated so far as the conventional protective IC is used, the conventional protective IC not only causes inconvenience for a user, but also causes a large load such as costs and time required for battery replacement.

SUMMARY OF THE INVENTION

The present invention has been made in view of the above circumstances, and therefore an object of the present inven-

tion is to provide a battery state monitoring circuit and a battery device which are capable of preventing the discharge leak current from the battery so as to eliminate the load conventionally imposed on the user.

5 In order to achieve the above-mentioned object, as means for solving the above-mentioned problems, the present invention provides a battery state monitoring circuit, including: a battery state detector circuit that detects a state of a battery based on a voltage of the battery; a transmitting terminal that transmits battery state information indicative of the state of the battery to an outside; a receiving terminal that receives battery state information of another battery from the outside; a transistor that is used for transmitting the battery state information, and has any one of two terminals except for a control terminal connected to the transmitting terminal; and a diode that is connected in a direction opposite to a direction of a parasitic diode disposed between the two terminals of the transistor, the diode being disposed between the transmitting terminal and one terminal of the transistor.

BRIEF DESCRIPTION OF THE DRAWINGS

In the accompanying drawings:

FIG. 1 is a circuit configuration diagram showing a battery device according to a first embodiment of the present invention;

FIG. 2 is an explanatory diagram showing a discharge leak current preventing principle in the battery device according to the first embodiment of the present invention;

FIG. 3 is a circuit configuration diagram showing a battery device according to a second embodiment of the present invention;

FIG. 4 is an explanatory diagram showing a discharge leak current preventing principle in the battery device according to the second embodiment of the present invention;

FIG. 5 is a circuit configuration diagram showing a battery device according to a third embodiment of the present invention;

FIG. 6 is a circuit configuration diagram showing a battery device according to a fourth embodiment of the present invention;

FIG. 7 is a circuit configuration diagram showing a battery device according to a fifth embodiment of the present invention;

FIG. 8 is a circuit configuration diagram showing a battery device according to a sixth embodiment of the present invention;

FIG. 9 is a circuit configuration diagram showing a battery device according to a seventh embodiment of the present invention;

FIG. 10 is a circuit configuration diagram showing a battery device according to an eighth embodiment of the present invention;

FIG. 11 is a circuit configuration diagram showing a battery device according to a ninth embodiment of the present invention;

FIG. 12 is a circuit configuration diagram showing a battery device according to a tenth embodiment of the present invention;

FIG. 13 is a circuit configuration diagram showing a battery device according to an eleventh embodiment of the present invention;

FIG. 14 is a circuit configuration diagram showing a battery device according to a twelfth embodiment of the present invention; and

FIG. 15 is an explanatory diagram showing a conventional technology.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Hereinafter, a description will be given of embodiments of the present invention with reference to the accompanying drawings.

First Embodiment

FIG. 1 is a circuit configuration diagram showing a battery device according to a first embodiment. As shown in FIG. 1, the battery device according to the first embodiment includes n batteries BT_1 to BT_n , that are connected in series, n switches (cell balance switch circuits) SW_1 to SW_n which are connected in parallel with each of the batteries BT_1 to BT_n , n battery state monitoring circuits BM_1 to BM_n that are disposed in correspondence with the respective batteries BT_1 to BT_n , individually, a first transistor (charging p-channel transistor) 10, a second transistor (discharging p-channel transistor) 11, a first resistive element (first bias resistive element) 20, a second resistive element (second bias resistive element) 21, a first external terminal 30, and a second external terminal 31.

The battery state monitoring circuit BM_1 includes an overcharge detector circuit A_1 , a first NOR circuit B_1 , a first output transistor C_1 , a diode Do_1 , a first inverter D_1 , a second inverter E_1 , a first current source F_1 , an overdischarge detector circuit G_1 , a second NOR circuit H_1 , a second output transistor I_1 , a third inverter J_1 , a fourth inverter K_1 , a second current source L_1 , a cell balance circuit M_1 , a first voltage monitor terminal PA_1 , a second voltage monitor terminal PB_1 , a first transmitting terminal PC_1 , a second transmitting terminal PD_1 , a first receiving terminal PE_1 , a second receiving terminal PF_1 , and a control terminal PG_1 . The battery state monitoring circuit BM_1 having the above components is configured as an IC (semiconductor device) of one chip.

The other battery state monitoring circuits BM_2 to BM_n have the same components as those of the battery state monitoring circuit BM_1 , and therefore are shown with a change in only symbols. For example, the symbol of the overcharge detector circuit in the battery state monitoring circuit BM_2 is A_2 whereas the symbol of the overcharge detector circuit in the battery state monitoring circuit BM_n is A_n . The same is applied to other components.

Since all of the battery state monitoring circuits BM_1 to BM_n are identical in circuit configuration with each other as described above, the battery state monitoring circuit BM_1 corresponding to the battery BT_1 will be representatively described below.

In the battery state monitoring circuit BM_1 , the first voltage monitor terminal PA_1 is connected to a positive terminal of the battery BT_1 and one terminal of the switch SW_1 . Also, the first voltage monitor terminal PA_1 is connected to a positive side common power source wire within the battery state monitoring circuit BM_1 . The second voltage monitor terminal PB_1 is connected to a negative terminal of the battery BT_1 and another terminal of the switch SW_1 . Also, the second voltage monitor terminal PB_1 is connected to a negative side common power source wire within the battery state monitoring circuit BM_1 . In the following description, the positive side common power source wire is VDD_1 and the negative side common power source wire is VSS_1 within the battery state monitoring circuit BM_1 , and the positive side common power source wire is VDD_2 and the negative side common power source wire is

VSS_2 within the battery state monitoring circuit BM_2 . In the same manner, the positive side common power source wire is VDD_n and the negative side common power source wire is VSS_n within the battery state monitoring circuit BM_n .

The overcharge detector circuit A_1 has one end connected to the first voltage monitor terminal PA_1 , and another end connected to the second voltage monitor terminal PB_1 . The overcharge detector circuit A_1 detects a voltage between the first voltage monitor terminal PA_1 and the second voltage monitor terminal PB_1 (that is, voltage of battery BT_1). When the voltage of the battery BT_1 is equal to or higher than an overcharge voltage, the overcharge detector circuit A_1 outputs an overcharge detection signal of high level to one input terminal of the first NOR circuit B_1 . Also, when the voltage of the battery BT_1 is lower than the overcharge voltage, the overcharge detector circuit A_1 outputs an overcharge detection signal of low level to the first NOR circuit B_1 . Here, the overcharge voltage is an upper limit chargeable voltage. The overcharge detector circuit A_1 has a function of stopping the operation when the overdischarge detection signal of high level is input to the overcharge detector circuit A_1 from the overdischarge detector circuit G_1 .

To the first NOR circuit B_1 , the above overcharge detection signal and an output signal of the first inverter D_1 are input, and the first NOR circuit B_1 outputs a negative OR signal of both of those signals to a gate terminal of the first output transistor C_1 . The first output transistor C_1 is an n-channel type metal oxide semiconductor (MOS) transistor. The first output transistor C_1 has the gate terminal connected to an output terminal of the first NOR circuit B_1 , a drain terminal connected to a cathode terminal of the diode Do_1 , and a source terminal connected to the VSS_1 . The diode Do_1 is a discharge leak current prevention diode. The diode Do_1 has the cathode terminal connected to the drain terminal of the first output transistor C_1 , and an anode terminal connected to the first transmitting terminal PC_1 .

The first inverter D_1 outputs a logical inversion signal of an output signal from the second inverter E_1 to the first NOR circuit B_1 . The second inverter E_1 has an input terminal connected to the first receiving terminal PE_1 and an output terminal of the first current source F_1 , and outputs a logical inversion signal of an input signal to an input terminal to the first inverter D_1 . The first current source F_1 is a current source having an input terminal connected to the VDD_1 , and the output terminal connected to the input terminal of the second inverter E_1 and the first receiving terminal PE_1 .

The overdischarge detector circuit G_1 has one end connected to the first voltage monitor terminal PA_1 , and another end connected to the second voltage monitor terminal PB_1 . The overdischarge detector circuit G_1 detects a voltage between the first voltage monitor terminal PA_1 and the second voltage monitor terminal PB_1 (that is, voltage of battery BT_1). When the voltage of the battery BT_1 is lower than an overdischarge voltage, the overdischarge detector circuit G_1 outputs an overdischarge detection signal of high level to one input terminal of the second NOR circuit H_1 , the overcharge detector circuit A_1 , and the cell balance circuit M_1 . Also, when the voltage of the battery BT_1 is equal to or higher than the overdischarge voltage, the overdischarge detector circuit G_1 outputs an overdischarge detection signal of low level. Here, the overdischarge voltage is a lower limit dischargeable voltage.

To the second NOR circuit H_1 , the above overdischarge detection signal and an output signal of the third inverter J_1 are input, and the second NOR circuit H_1 outputs a negative OR signal of both of those signals to a gate terminal of the second output transistor I_1 . The second output transistor I_1 is an

n-channel type MOS transistor. The second output transistor I_1 has the gate terminal connected to an output terminal of the second NOR circuit H_1 , a drain terminal connected to the second transmitting terminal PD_1 , and a source terminal connected to the VSS_1 .

The third inverter J_1 outputs a logical inversion signal of an output signal from the fourth inverter K_1 to the second NOR circuit H_1 . The fourth inverter K_1 has an input terminal connected to the second receiving terminal PF_1 and an output terminal of the second current source L_1 , and outputs a logical inversion signal of an input signal to the input terminal of the fourth inverter K_1 . The second current source L_1 is a current source having an input terminal connected to the VDD_1 , and the output terminal connected to the input terminal of the fourth inverter L_1 and the second receiving terminal PF_1 .

The cell balance circuit M_1 has one end connected to the first voltage monitor terminal PA_1 , and another end connected to the second voltage monitor terminal PB_1 . The cell balance circuit M_1 detects a voltage between the first voltage monitor terminal PA_1 and the second voltage monitor terminal PB_1 (that is, voltage of battery BT_1). When the voltage of the battery BT_1 is equal to or higher than a cell balance voltage, the cell balance circuit M_1 outputs a cell balance signal to the switch SW_1 through the control terminal PG_1 . Also, when the voltage of the battery BT_1 is lower than the cell balance voltage, the cell balance circuit M_1 outputs a cell balance signal of low level to the switch SW_1 through the control terminal PG_1 . Here, the cell balance voltage is a voltage that is equal to or lower than the overcharge voltage in the case in which the battery BT_1 comes to a state close to the overcharged state (voltage in the case in which voltage of battery BT_1 is adjusted to voltages of other batteries to start to balance). The cell balance circuit M_1 has a function of stopping the operation when the overdischarge detection signal of high level is input to the cell balance circuit M_1 from the overdischarge detector circuit G_1 .

The first transmitting terminal PC_1 is connected to a gate terminal of the first transistor **10** and one end of the first resistive element **20**. The second transmitting terminal PD_1 is connected to a gate terminal of the second transistor **11** and one end of the second resistive element **21**. The first receiving terminal PE_1 is connected to a first transmitting terminal PC_2 of the battery state monitoring circuit BM_2 . The second receiving terminal PF_1 is connected to a second transmitting terminal PD_2 of the battery state monitoring circuit BM_2 .

Also, a first receiving terminal PE_2 of the battery state monitoring circuit BM_2 is connected to a first transmitting terminal PC_3 of the battery state monitoring circuit BM_3 , and a second receiving terminal PF_2 of the battery state monitoring circuit BM_2 is connected to a second transmitting terminal PD_3 of the battery state monitoring circuit BM_3 . The same is applied to the battery state monitoring circuits BM_3 to BM_n , and the first receiving terminal of the battery state monitoring circuit on an upstream side (battery BT_1 side) is connected to the first transmitting terminal of the battery state monitoring circuit on a downstream side (battery BT_n side). The second receiving terminal of the battery state monitoring circuit on the upstream side is connected to the second transmitting terminal of the battery state monitoring circuit on the downstream side. A first receiving terminal PE_n and a second receiving terminal PF_n of the battery state monitoring circuit BM_n which is the most downstream side are connected to a negative terminal of the battery BT_n .

The switch SW_1 is connected in parallel with the battery BT_1 , and changes over between the connection and the disconnection of the two terminals (that is, positive terminal and negative terminal of battery BT_1) according to the cell bal-

ance signal that is input to the switch SW_1 through the control terminal PG_1 . The switch SW_1 is turned on, that is, changes over the two terminals to the connection state when the cell balance signal is input. The same is applied to the other switches SW_2 to SW_n .

The first transistor **10** is a p-channel type MOS transistor. The first transistor **10** has the gate terminal connected to the first transmitting terminal PC_1 of the battery state monitoring circuit BM_1 and the one end of the first resistive element **20**. The first transistor **10** also has a drain terminal connected to a drain terminal of the second transistor **11**, and a source terminal connected to another terminal of the first resistive element **20** and the first external terminal **30**. The second transistor **11** is a p-channel type MOS transistor. The second transistor **11** has the gate terminal connected to the second transmitting terminal PD_1 of the battery state monitoring circuit BM_1 and the one end of the second resistive element **21**. The second transistor **11** also has the drain terminal connected to the drain terminal of the first transistor **10**, and a source terminal connected to another terminal of the second resistive element **21** and the positive terminal of the battery BT_1 . On the other hand, the second external terminal **31** is connected to the negative terminal of the battery BT_n on the most downstream side.

In the battery device configured as described above, a load or a charger is connected between the first external terminal **30** and the second external terminal **31** to conduct discharging or charging.

Subsequently, a description will be given of the operation of the battery device according to the first embodiment, which is configured as described above.

(Normal State)

First, a description will be given of a normal state, that is, a case in which all the voltages of the batteries BT_1 to BT_n are lower than the overcharge voltage, and equal to or higher than the overdischarge voltage. In the normal state thus defined, the overcharge detector circuit A_1 of the battery state monitoring circuit BM_1 outputs the overcharge detection signal of low level to the first NOR circuit B_1 .

In this situation, a first output transistor C_2 of the battery state monitoring circuit BM_2 is on (the reason will be described later). As a result, the input terminal of the second inverter E_1 of the battery state monitoring circuit BM_1 is at low level, and the output signal of low level is output from the first inverter D_1 to the first NOR circuit B_1 . Because, to the first NOR circuit B_1 , the overcharge detection signal of low level and the output signal of low level of the first inverter D_1 are input, the first NOR circuit B_1 outputs the negative OR signal of high level to the gate terminal of the first output transistor C_1 . As a result, because the first output transistor C_1 is turned on, the first transmitting terminal PC_1 becomes at low level, and the first transistor **10** is turned on.

Now, the reason why the first output transistor C_2 of the battery state monitoring circuit BM_2 is on will be described below. Because the first receiving terminal PE_n of the battery state monitoring circuit BM_n on the most downstream side is connected to the negative terminal of the battery BT_n , an input terminal of a second inverter E_n is always held at low level. Accordingly, a first inverter D_n always outputs the output signal of low level to a first NOR circuit B_n , and the overcharge detector circuit A_n outputs the overcharge detection signal of low level to the first NOR circuit B_n . With the above arrangement, the first NOR circuit B_n outputs the negative OR signal of high level to a gate terminal of a first output transistor C_n , and the first output transistor C_n of the battery state monitoring circuit BM_n is turned on.

As a result, an input terminal of a second inverter E_{n-1} in the battery state monitoring circuit BM_{n-1} becomes at low level, and the output signal of low level is output to a first NOR circuit B_{n-1} from a first inverter D_{n-1} . On the other hand, since an overcharge detector circuit A_{n-1} outputs the overcharge detection signal of low level to the first NOR circuit B_{n-1} , the first NOR circuit B_{n-1} outputs the negative OR signal of high level to a gate terminal of a first output transistor C_{n-1} . As a result, the first output transistor C_{n-1} of the battery state monitoring circuit BM_{n-1} is turned on.

The above operation is repeated in the upstream side battery state monitoring circuit and the downstream side battery state monitoring circuit, and the first output transistor C_2 of the battery state monitoring circuit BM_2 is turned on.

Also, in the above normal state, the overdischarge detector circuit G_1 of the battery state monitoring circuit BM_1 outputs the overdischarge detection signal of low level to the second NOR circuit H_1 . In this situation, because a second output transistor I_2 of the battery state monitoring circuit BM_2 is also on, the input terminal of the fourth inverter K_1 of the battery state monitoring circuit BM_1 becomes at low level, and the output signal of low level is output to the second NOR circuit H_1 from the third inverter J_1 . Because, to the second NOR circuit H_1 , the overdischarge detection signal of low level and the output signal of low level of the third inverter J_1 are input, the second NOR circuit H_1 outputs the negative OR signal of high level to the gate terminal of the second output transistor I_1 . As a result, because the second output transistor I_1 is turned on, the second transmitting terminal PD_1 becomes at low level, and the second transistor **11** is turned on.

As described above, in the normal state, because the first transistor **10** and the second transistor **11** are turned on, the battery device is chargeable and dischargeable.

(Overcharged State)

Subsequently, a description will be given of an overcharged state, that is, a case in which a charger is connected between the first external terminal **30** and the second external terminal **31** to charge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes equal to or higher than the overcharge voltage. In the following description, it is assumed that the voltage of the battery BT_2 is equal to or higher than the overcharge voltage.

In this case, the overcharge detector circuit A_2 of the battery state monitoring circuit BM_2 outputs the overcharge detection signal of high level to a first NOR circuit B_2 . In this situation, because the output signal of low level is output from a first inverter D_2 , the first NOR circuit B_2 outputs the negative OR signal of low level to a gate terminal of the first output transistor C_2 . As a result, the first output transistor C_2 is turned off.

That is, the input terminal of the second inverter E_1 is pulled up to high level by means of the first current source F_1 and the output signal of high level is output to the first NOR circuit B_1 from the first inverter D_1 . On the other hand, because the overcharge detector circuit A_1 outputs the overcharge detection signal of low level to the first NOR circuit B_1 , the first NOR circuit B_1 outputs the negative OR signal of low level to the gate terminal of the first output transistor C_1 . As a result, the first output transistor C_1 is turned off.

As described above, when the first output transistor C_1 is turned off, the gate terminal of the first transistor **10** becomes at high level by means of the first resistive element **20**, and the first transistor **10** is turned off. As a result, the charging from the charger is prohibited.

In the above description, it is assumed that the voltage of the battery BT_2 is equal to or higher than the overcharge voltage. The same is applied to a case in which the voltages of

the other batteries are equal to or higher than the overcharge voltage. That is, a fact that the overcharged state occurs is communicated from the battery state monitoring circuit corresponding to the battery that has become in the overcharged state to the upstream side battery state monitoring circuit, and the communication reaches the most upstream side battery state monitoring circuit BM_1 . As a result, the first transistor **10** is turned off to prohibit the charging from the charger.

(Overdischarged State)

Subsequently, a description will be given of an overdischarged state, that is, a case in which a load is connected between the first external terminal **30** and the second external terminal **31** to discharge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes lower than the overdischarge voltage. In the following description, it is assumed that the voltage of the battery BT_2 is lower than the overdischarge voltage.

In this case, an overdischarge detector circuit G_2 of the battery state monitoring circuit BM_2 outputs the overdischarge detection signal of high level to a second NOR circuit H_2 . In this situation, because the output signal of low level is output from a third inverter J_2 , the second NOR circuit H_2 outputs the negative OR signal of low level to a gate terminal of the second output transistor I_2 . As a result, the second output transistor I_2 is turned off.

That is, the input terminal of the fourth inverter K_1 is pulled up to high level by means of the second current source L_1 , and the output signal of high level is output to the second NOR circuit H_1 from the third inverter J_1 . On the other hand, because the overdischarge detector circuit G_1 outputs the overdischarge detection signal of low level to the second NOR circuit H_1 , the second NOR circuit H_1 outputs the negative OR signal of low level to the gate terminal of the second output transistor I_1 . As a result, the second output transistor I_1 is turned off.

As described above, when the second output transistor I_1 is turned off, the gate terminal of the second transistor **11** becomes at high level by means of the second resistive element **21**, and the second transistor **11** is turned off. As a result, the discharging to the load is prohibited.

Also, in the above overdischarge state, the overdischarge detector circuit G_2 that has detected the overdischarged state outputs the overdischarge detection signal of high level to the overcharge detector circuit A_2 and a cell balance circuit M_2 . With the above configuration, because the overcharge detector circuit A_2 and the cell balance circuit M_2 stop the operation, it is possible to reduce the power consumption. Also, a first voltage monitor terminal PA_2 also functions as a VDD power source terminal of the battery state monitoring circuit BM_2 , and the battery state monitoring circuit BM_2 receives a power from the battery BT_2 . As a result, the voltage of the overdischarged battery BT_2 becomes low, and the power consumption of the battery state monitoring circuit BM_2 is reduced as much.

In this example, when the characteristic variation occurs in the respective batteries to decrease the voltage of the battery BT_2 earlier than the voltages of the other batteries during discharging, the overdischarge detector circuit G_2 of the battery state monitoring circuit BM_2 outputs the overdischarge detection signal earlier than other battery state monitoring circuits. Then, the second transistor **11** is turned off to prohibit the discharging. In this situation, in the battery state monitoring circuit BM_2 , the power consumption is reduced more than those of the other battery state monitoring circuits. The battery BT_2 is lower than the other batteries in discharge speed as much as the power consumption is reduced, and the other batteries discharge electricity in the usual manner.

Therefore, since the discharge speed of the overdischarged battery BT_2 becomes low, the battery device is capable of conforming the voltages of the respective batteries to each other (taking cell balance).

In the above description, it is assumed that the voltage of the battery BT_2 is lower than the overdischarge voltage. The same is applied to a case in which the voltages of the other batteries are lower than the overdischarge voltage. That is, a fact that the overdischarged state occurs is communicated from the battery state monitoring circuit corresponding to the battery that has become in the overdischarged state to the upstream side battery state monitoring circuit, and the communication reaches the most upstream side battery state monitoring circuit BM_1 . As a result, the second transistor **11** is turned off to prohibit the discharging to the load.

(Cell Balance State)

Subsequently, a description will be given of a cell balance state, that is, a case in which a charger is connected between the first external terminal **30** and the second external terminal **31** to charge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes equal to or higher than the cell balance voltage. In the following description, it is assumed that the voltage of the battery BT_2 is equal to or higher than the cell balance voltage.

In this case, the cell balance circuit M_2 of the battery state monitoring circuit BM_2 outputs the cell balance signal to the switch SW_2 through a control terminal PG_2 . With the above configuration, the switch SW_2 is turned on, and the charged battery BT_2 discharges electricity through the switch SW_2 .

In this example, when the characteristic variation occurs in the respective batteries to increase the voltage of the battery BT_2 earlier than the voltages of the other batteries during charging, the battery state monitoring circuit BM_2 outputs the cell balance signal earlier than the other battery state monitoring circuits. Then, the switch SW_2 is turned on earlier than the other switches, and the battery BT_2 is different from the other batteries in change in amount of charge. For example, the battery BT_2 is lower in charging speed than the other batteries, and the other batteries are charged in the usual manner. Alternatively, the battery BT_2 is discharged, and the other batteries are charged in the usual manner. As a result, since the charging speed of the overcharged battery BT_2 becomes low, or since the overcharged battery BT_2 is discharged, the battery device is capable of taking the cell balance.

Hereinafter, a description will be given of the reason why the discharge leak current can be prevented with the provision of the diode Do_1 in the battery state monitoring circuit BM_1 on the premise of the above operation. FIG. 2 shows the circuit configuration of the battery device in which no diode Do_1 is provided. For example, in FIG. 2, it is assumed that the battery BT_1 is overdischarged during the discharging to the load, and the second transistor **11** is turned off. In this case, the first output transistor C_1 of the most upstream side battery state monitoring circuit BM_1 becomes off. However, because a parasitic diode having a cathode terminal on the drain side and an anode terminal on the source side exists between the drain terminal and the gate terminal of the first output transistor C_1 , a current path is formed as shown in FIG. 2. As a result, the electric discharge of the batteries BT_2 to BT_n does not stop, thereby causing the discharge leak current to occur. On the other hand, according to the battery state monitoring circuit BM_1 of the first embodiment, because the diode Do_1 of a direction opposite to the parasitic diode of the first output transistor C_1 is provided, it is possible to prevent the discharge leak current shown in FIG. 2 from occurring.

As described above, in the battery device according to the first embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user, such as the costs and time required for battery exchange.

Second Embodiment

Subsequently, a description will be given of a battery device according to a second embodiment. In the above first embodiment, the description is given of a case in which the n-channel type MOS transistors are used as the first output transistor and the second output transistor in the battery state monitoring circuit. In contrast, in the second embodiment, a description will be given of a battery device in the case where p-channel type MOS transistors are used as the first output transistor and the second output transistor.

FIG. 3 is a circuit configuration diagram showing the battery device according to the second embodiment. In FIG. 3, the same components as those of FIG. 1 are denoted by identical symbols, and their description will be omitted. In order to distinguish from FIG. 1, the symbols of the battery state monitoring circuits are BMA_1 to BMA_n , the symbol of the first transistor is **12**, the symbol of the second transistor is **13**, the symbol of the first resistive element is **22**, and the symbol of the second resistive element is **23**. Also, since the circuit configurations of those battery state monitoring circuits BMA_1 to BMA_n are identical with each other, the most downstream side battery state monitoring circuit BMA_n will be representatively described below.

The battery state monitoring circuit BMA_n according to the second embodiment includes the overcharge detector circuit A_n , the first NOR circuit B_n , a first inverter Q_n , a first output transistor R_n , a diode Do_n , a second inverter S_n , a first current source T_n , an overdischarge detector circuit G_n , a second NOR circuit H_n , a third inverter U_n , a second output transistor V_n , a fourth inverter W_n , a second current source X_n , a cell balance circuit M_n , a first voltage monitor terminal PA_n , a second voltage monitor terminal PB_n , a first transmitting terminal PC , a second transmitting terminal PD_n , a first receiving terminal PE_n , a second receiving terminal PF_n , and a control terminal PG_n . The battery state monitoring circuit BMA_n having the above components is configured as an IC of one chip.

To the first NOR circuit B_n , an overcharge detection signal that is output from the overcharge detector circuit A_n , and an output signal of the second inverter S_n are input, and the first NOR circuit B_n outputs a negative OR signal of those signals to the first inverter Q_n . The first inverter Q_n outputs the logical inversion signal of the negative OR signal that is input from the first NOR circuit B_n to a gate terminal of the first output transistor R_n . The first output transistor R_n is a p-channel type MOS transistor. The first output transistor R_n has the gate terminal connected to an output terminal of the first inverter Q_n , a drain terminal connected to an anode terminal of the diode Do_n , and a source terminal connected to the VDD_n . The diode Do_n is a discharge leak current prevention diode, and has the anode terminal connected to the drain terminal of the first output transistor R_n , and a cathode terminal connected to the first transmitting terminal PC_n .

The second inverter S_n has an input terminal connected to the first receiving terminal PE_n and an input terminal of the first current source T_n , and outputs the logical inversion signal of the input signal to the input terminal to the first NOR circuit B_n . The first current source T_n is a current source that has the input terminal connected to the first receiving terminal PE_n

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and the input terminal of the second inverter S_n , and an output terminal connected to the VSS_n .

To the second NOR circuit H_n , an overdischarge detection signal that is output from the overdischarge detector circuit G_n and the output signal of the fourth inverter W_n are input, and the second NOR circuit H_n outputs a negative OR signal of those signals to the third inverter U_n . The third inverter U_n outputs the logical inversion signal of the negative OR signal that is input from the second NOR circuit H_n to a gate terminal of the second output transistor V_n . The second output transistor V_n is a p-channel type MOS transistor, and has the gate terminal connected to an output terminal of the third inverter U_n , a drain terminal connected to the second transmitting terminal PD_n , and a source terminal connected to the VDD_n .

The fourth inverter W_n has an input terminal connected to the second receiving terminal PF_n , and an input terminal of the second current source X_n , and outputs the logical inversion signal of the input signal to the input terminal to the second NOR circuit H_n . The second current source X_n is a current source that has the input terminal connected to the second receiving terminal PF_n and the input terminal of the fourth inverter W_n , and an output terminal connected to the VSS_n .

The first transmitting terminal PC_n is connected to a gate terminal of the first transistor **12** and one end of the first resistive element **22**. The second transmitting terminal PD_n is connected to a gate terminal of the second transistor **13** and one end of the second resistive element **23**. The first receiving terminal PE_n is connected to a first transmitting terminal PC_{n-1} of the battery state monitoring circuit BMA_{n-1} . The second receiving terminal PF_n is connected to a second transmitting terminal PD_{n-1} of the battery state monitoring circuit BMA_{n-1} .

The same is applied to the other battery state monitoring circuits, and the first receiving terminal of the battery state monitoring circuit on the downstream side (battery BT_n side) is connected to the first transmitting terminal of the battery state monitoring circuit on the upstream side (battery BT_1 side). The second receiving terminal of the battery state monitoring circuit on the downstream side is connected to the second transmitting terminal of the battery state monitoring circuit on the upstream side. The first receiving terminal PE_1 and the second receiving terminal PF_1 of the battery state monitoring circuit BMA_1 which is the most upstream side are connected to the positive terminal of the battery BT_1 .

The first transistor **12** is an n-channel type MOS transistor. The first transistor **12** has the gate terminal connected to the first transmitting terminal PC_n of the battery state monitoring circuit BM_n and the one end of the first resistive element **22**. The first transistor **12** also has a drain terminal connected to a drain terminal of the second transistor **13**, and a source terminal connected to another terminal of the first resistive element **22** and the negative terminal of the battery BT_n . The second transistor **13** is an n-channel type MOS transistor. The second transistor **13** has the gate terminal connected to the second transmitting terminal PD_n of the battery state monitoring circuit BMA_n and the one end of the second resistive element **23**. The second transistor **13** also has the drain terminal connected to the drain terminal of the second transistor **12**, and a source terminal connected to another terminal of the second resistive element **23** and the second external terminal **31**. On the other hand, the first external terminal **30** is connected to the positive terminal of the battery BT_1 on the most upstream side.

Subsequently, a description will be given of the operation of the battery device according to the second embodiment, which is configured as described above. The operation in the

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cell balance state is identical with that in the first embodiment, and therefore its description will be omitted.

(Normal State)

First, a description will be given of a normal state, that is, a case in which the voltages of all the batteries BT_1 to BT_n are lower than the overcharge voltage, and equal to or higher than the overdischarge voltage. In the normal state thus defined, the overcharge detector circuit A_n of the battery state monitoring circuit BMA_n outputs the overcharge detection signal of low level to the first NOR circuit B_n .

In this situation, a first output transistor R_{n-1} of the battery state monitoring circuit BMA_{n-1} is on (the reason will be described later). As a result, the input terminal of the second inverter S_n of the battery state monitoring circuit BMA_n becomes at high level, and the output signal of low level is output from the second inverter S_n to the first NOR circuit B_n . The first NOR circuit B_n outputs the negative OR signal of high level to the first inverter Q_n , and the first inverter Q_n outputs the logical inversion signal of low level to the gate terminal of the first output transistor R_n . As a result, because the first output transistor R_n is turned on, the first transmitting terminal PC_n becomes at high level, and the first transistor **12** is turned on.

Now, the reason why the first output transistor R_{n-1} of the battery state monitoring circuit BMA_{n-1} is on will be described below. Because the first receiving terminal PE_1 of the battery state monitoring circuit BMA_1 on the most upstream side is connected to the positive terminal of the battery BT_1 , an input terminal of a second inverter S_1 is always held at high level. Accordingly, the second inverter S_1 always outputs the output signal of low level to the first NOR circuit B_1 , and the overcharge detector circuit A_1 outputs the overcharge detection signal of low level to the first NOR circuit B_1 . With the above arrangement, the first NOR circuit B_1 outputs the negative OR signal of high level to a first inverter Q_1 , and the first inverter Q_1 outputs the logical inversion signal of low level to a gate terminal of a first output transistor R_1 . As a result, the first output transistor R_1 of the battery state monitoring circuit BMA_1 is turned on.

In this situation, an input terminal of a second inverter S_2 in the battery state monitoring circuit BMA_2 that is the downstream side of the battery state monitoring circuit BMA_1 becomes at high level, and the output signal of low level is output from the second inverter S_2 to the first NOR circuit B_2 . Since the overcharge detector circuit A_2 outputs the overcharge detection signal of low level, the first NOR circuit B_2 outputs the negative OR signal of high level to a first inverter Q_2 , and the first inverter Q_2 outputs the logical inversion signal of low level to a gate terminal of a first output transistor R_2 . As a result, the first output transistor R_2 is turned on.

The above operation is repeated in the upstream side battery state monitoring circuit and the downstream side battery state monitoring circuit, and the first output transistor R_{n-1} of the battery state monitoring circuit BMA_{n-1} is turned on.

Also, in the above normal state, the overdischarge detector circuit G of the battery state monitoring circuit BM_n outputs the overdischarge detection signal of low level to the second NOR circuit H_n . In this situation, because a second output transistor V_{n-1} of the battery state monitoring circuit BM_{n-1} is also on, the input terminal of the fourth inverter W_n in the battery state monitoring circuit BMA_n becomes at high level, and the output signal of low level is output to the second NOR circuit H_n from the fourth inverter W_n . The second NOR circuit H_n outputs the negative OR signal of high level to the third inverter U_n , and the third inverter U_n outputs the logical inversion signal of low level to the gate terminal of the second output transistor V_n . As a result, because the second output

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transistor V_n is turned on, the second transmitting terminal PD_n becomes at high level, and the second transistor **13** is turned on.

As described above, in the normal state, because the first transistor **12** and the second transistor **13** are turned on, the battery device is chargeable and dischargeable.

(Overcharged State)

Subsequently, a description will be given of an overcharged state, that is, a case in which a charger is connected between the first external terminal **30** and the second external terminal **31** to charge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes equal to or higher than the overcharge voltage. In the following description, it is assumed that the voltage of the battery BT_{n-1} is equal to or higher than the overcharge voltage.

In this case, the overcharge detector circuit A_{n-1} of the battery state monitoring circuit BMA_{n-1} outputs the overcharge detection signal of high level to the first NOR circuit B_{n-1} . In this situation, because the output signal of low level is output from a second inverter S_{n-1} , the first NOR circuit B_{n-1} outputs the negative OR signal of low level to a first inverter Q_{n-1} , and the first inverter Q_{n-1} outputs the logical inversion signal of high level to a gate terminal of the first output transistor R_{n-1} . As a result, the first output transistor R_{n-1} is turned off.

That is, the input terminal of the second inverter S_n is pulled down to low level by means of the first current source T_n , and the output signal of high level is output to the first NOR circuit B_n from the second inverter S_n . On the other hand, because the overcharge detector circuit A_n outputs the overcharge detection signal of low level to the first NOR circuit B_n , the first NOR circuit B_n outputs the negative OR signal of low level to the first inverter Q_n , and the first inverter Q_n outputs the logical inversion signal of high level to the gate terminal of the first output transistor R_n . As a result, the first output transistor R_n is turned off.

As described above, when the first output transistor R_n is turned off, the gate terminal of the first transistor **12** becomes at low level by means of the first resistive element **22**, and the first transistor **12** is turned off. As a result, the charging from the charger is prohibited.

In the above description, it is assumed that the voltage of the battery BT_{n-1} is equal to or higher than the overcharge voltage. The same is applied to a case in which the voltages of the other batteries are equal to or higher than the overcharge voltage. That is, a fact that the overcharged state occurs is communicated from the battery state monitoring circuit corresponding to the battery that has become in the overcharged state to the downstream side battery state monitoring circuit, and the communication reaches the most downstream side battery state monitoring circuit BMA_n . As a result, the first transistor **12** is turned off to prohibit the charging from the charger.

(Overdischarged State)

Subsequently, a description will be given of an overdischarged state, that is, a case in which a load is connected between the first external terminal **30** and the second external terminal **31** to discharge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes lower than the overdischarge voltage. In the following description, it is assumed that the voltage of the battery BT_{n-1} is lower than the overdischarge voltage.

In this case, an overdischarge detector circuit G_{n-1} of the battery state monitoring circuit BMA_{n-1} outputs the overdischarge detection signal of high level to a second NOR circuit H_{n-1} . In this situation, because the output signal of low level is output from a fourth inverter W_{n-1} , the second NOR circuit

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H_{n-1} outputs the negative OR signal of low level to a third inverter U_{n-1} , and the third inverter U_{n-1} outputs the logical inversion signal of high level to a gate terminal of the second output transistor V_{n-1} . As a result, the second output transistor V_{n-1} is turned off.

That is, the input terminal of the fourth inverter W_n is pulled down to low level by means of the second current source X_n , and the output signal of high level is output to the second NOR circuit H_n from the fourth inverter W_n . On the other hand, because the overdischarge detector circuit G_n outputs the overdischarge detection signal of low level to the second NOR circuit H_n , the second NOR circuit H_n outputs the negative OR signal of low level to the third inverter U_n , and the third inverter U_n outputs the logical inversion signal of high level to the gate terminal of the second output transistor V_n . As a result, the second output transistor V_n is turned off.

As described above, when the second output transistor V_n is turned off, the gate of the second transistor **13** becomes at low level by means of the second resistive element **23**, and the second transistor **13** is turned off. As a result, the discharging to the load is prohibited.

In the above description, it is assumed that the voltage of the battery BT_{n-1} is lower than the overdischarge voltage. The same is applied to a case in which the voltages of the other batteries are lower than the overdischarge voltage. That is, a fact that the overdischarged state occurs is communicated from the battery state monitoring circuit corresponding to the battery that has become in the overdischarged state to the downstream side battery state monitoring circuit, and the communication reaches the most downstream side battery state monitoring circuit BMA_n . As a result, the second transistor **13** is turned off to prohibit the discharging to the load.

Hereinafter, a description will be given of the reason why the discharge leak current can be prevented with the provision of the diode Do_n in the battery state monitoring circuit BMA_n on the premise of the above operation. FIG. 4 shows the circuit configuration of the battery device in which no diode Do_n is provided. For example, in FIG. 4, it is assumed that the battery BT_n is overdischarged during the discharging to the load, and the second transistor **13** is turned off. In this case, the first output transistor R_n of the battery state monitoring circuit BMA_n becomes off. However, because a parasitic diode having a cathode terminal on the source side and an anode terminal on the drain side exists between the drain terminal and the gate terminal of the first output transistor R_n , a current path is formed as shown in FIG. 4. As a result, the electric discharge of the batteries BT_1 to BT_{n-1} does not stop, thereby causing the discharge leak current to occur. On the other hand, according to the battery state monitoring circuit BMA_n of the second embodiment, because the diode Do_n of a direction opposite to the parasitic diode of the first output transistor R_n is provided, it is possible to prevent the discharge leak current shown in FIG. 4 from occurring.

As described above, in the battery device according to the second embodiment, the occurrence of the discharge leak current can be prevented as in the first embodiment, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user, such as the costs and time required for battery exchange.

Third Embodiment

Subsequently, a description will be given of a battery device according to a third embodiment. FIG. 5 is a circuit configuration diagram showing the battery device according to the third embodiment. As shown in the figure, in the third

embodiment, two types of diodes are disposed in the battery state monitoring circuit of the first embodiment. That is, when it is assumed that the symbols of the battery state monitoring circuits are BMB_1 to BMB_n , the battery state monitoring circuit BMB_1 is newly equipped with a first diode (first clamp diode) Da_1 , a second diode (second clamp diode) Db_1 , a third diode (third clamp diode) Dc_1 , and a fourth diode (fourth clamp diode) Dd_1 in addition to the components of the first embodiment. The same is applied to the other battery state monitoring circuits. In the following description, the battery state monitoring circuit BMB_1 will be representatively described.

The first diode Da_1 has an anode terminal connected to the VSS_1 , and a cathode terminal connected to the drain terminal of the first output transistor C_1 . The first diode Da_1 has such a characteristic as to generate a reverse current when a reverse voltage corresponding to a voltage (for example, 4.5V) that exceeds the withstand voltage of the battery state monitoring circuit is applied between the anode terminal and the cathode terminal. The second diode Db_1 has an anode terminal connected to the VSS_1 , and a cathode terminal connected to the input terminal of the second inverter E_1 . It is assumed that the voltage drop of the second diode Db_1 is 0.7 V.

The third diode Dc_1 has an anode terminal connected to the VSS_1 , and a cathode terminal connected to the drain terminal of the second output transistor I_1 . The third diode Dc_1 has such a characteristic as to generate a reverse current when a reverse voltage corresponding to a voltage that exceeds the withstand voltage of the battery state monitoring circuit is applied between the anode terminal and the cathode terminal. The fourth diode Dd_1 has an anode terminal connected to the VSS_1 , and a cathode terminal connected to the input terminal of the fourth inverter K_1 . It is assumed that the voltage drop of the fourth diode Dd_1 is 0.7 V.

Also, resistive elements are connected between the first transmitting terminal of the downstream side battery state monitoring circuit and the first receiving terminal of the upstream side battery state monitoring circuit, and between the second transmitting terminal of the downstream side battery state monitoring circuit and the second receiving terminal of the upstream side battery state monitoring circuit, respectively. Specifically, a resistive element Ra_1 is connected between the first transmitting terminal PC_2 of the battery state monitoring circuit BMB_2 and the first receiving terminal PE_1 of the battery state monitoring circuit BMB_1 , and a resistive element Rb_1 is connected between the second transmitting terminal PD_2 of the battery state monitoring circuit BMB_2 and the second receiving terminal PF_1 of the battery state monitoring circuit BMB_1 , respectively.

Subsequently, a description will be given of the operation of the battery device according to the third embodiment, which is configured as described above. The operation in the cell balance state is identical with that in the first embodiment, and therefore its description will be omitted.

(Normal State)

First, a description will be given of a normal state, that is, a case in which all the voltages of the batteries BT_1 to BT_n are lower than the overcharge voltage, and equal to or higher than the overdischarge voltage. In the normal state thus defined, the overcharge detector circuit A_1 of the battery state monitoring circuit BMB_1 outputs the overcharge detection signal of low level to the first NOR circuit B_1 .

In this situation, the first output transistor C_2 of the battery state monitoring circuit BMB_2 is on. As a result, the input terminal of the second inverter E_1 of the battery state monitoring circuit BMB_1 becomes at low level, and the output signal of low level is output from the first inverter D_1 to the

first NOR circuit B_1 . The first NOR circuit B_1 outputs the negative OR signal of high level to the gate terminal of the first output transistor C_1 . As a result, because the first output transistor C_1 is turned on, the first transmitting terminal PC_1 becomes at low level, and the first transistor **10** is turned on.

In this situation, when the first output transistor C_2 of the battery state monitoring circuit BMB_2 is on, the first receiving terminal PE_1 of the battery state monitoring circuit BMB_1 is connected to the VSS_2 through the resistive element Ra_1 . However, since the first receiving terminal PE_1 is equipped with the second diode Db_1 , the voltage is clamped to $VSS_1 - 0.7$ V, and does not decrease lower than that value.

Also, in the above normal state, the overdischarge detector circuit G_1 of the battery state monitoring circuit BMB_1 outputs the overdischarge detection signal of low level to the second NOR circuit H_1 . In this situation, the second output transistor I_2 of the battery state monitoring circuit BMB_2 is also on. Therefore, the input terminal of the fourth inverter K_1 in the battery state monitoring circuit BMB_1 becomes at low level, and the output signal of low level is output to the second NOR circuit H_1 from the third inverter J_1 . The second NOR circuit H_1 outputs the negative OR signal of high level to the gate terminal of the second output transistor I_1 . As a result, because the second output transistor I_1 is turned on, the second transmitting terminal PD_1 becomes at low level, and the second transistor **11** is turned on.

Similarly, the voltage of the second receiving terminal PF_1 of the battery state monitoring circuit BMB_1 is clamped to $VSS_1 - 0.7$ V.

As described above, in the normal state, because the first transistor **10** and the second transistor **11** are turned on, the battery device is chargeable and dischargeable.

(Overcharged State)

Subsequently, a description will be given of an overcharged state, that is, a case in which a charger is connected between the first external terminal **30** and the second external terminal **31** to charge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes equal to or higher than the overcharge voltage. In the following description, it is assumed that the voltage of the battery BT_2 is equal to or higher than the overcharge voltage.

In this case, the overcharge detector circuit A_2 of the battery state monitoring circuit BMB_2 outputs the overcharge detection signal of high level to the first NOR circuit B_2 . In this situation, because the output signal of low level is output from the first inverter D_2 , the first NOR circuit B_2 outputs the negative OR signal of low level to the gate terminal of the first output transistor C_2 . As a result, the first output transistor C_2 is turned off.

That is, the input terminal of the second inverter E_1 is pulled up to high level by means of the first current source F_1 . As a result, a voltage recognized as high level is applied to the input terminal of the second inverter E_1 , and the output signal of high level is output to the first NOR circuit B_1 from the first inverter D_1 . On the other hand, because the overcharge detector circuit A_1 outputs the overcharge detection signal of low level to the first NOR circuit B_1 , the first NOR circuit B_1 outputs the negative OR signal of low level to the gate terminal of the first output transistor C_1 . As a result, the first output transistor C_1 is turned off.

In this situation, the first transmitting terminal PC_2 of the battery state monitoring circuit BMB_2 is pulled up to VDD_1 through the resistive element Ra_1 . However, since the first transmitting terminal PC_2 is equipped with a first diode Da_2 , the terminal voltage is clamped to $VSS_2 + 4.5$ V by a voltage (4.5 V) that causes the reverse current of the first diode Da_2 to be generated. Also, the resistance of the resistive element Ra_1

is set to a value that allows the voltage of the input terminal of the second inverter E_1 to be pulled up to high level by the first current source F_1 .

As described above, when the first output transistor C_1 is turned off, the gate terminal of the first transistor **10** becomes at high level by means of the first resistive element **20**, and the first transistor **10** is turned off. As a result, the charging from the charger is prohibited.

(Overdischarged State)

Subsequently, a description will be given of an overdischarged state, that is, a case in which a load is connected between the first external terminal **30** and the second external terminal **31** to discharge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes lower than the overdischarge voltage. In the following description, it is assumed that the voltage of the battery BT_2 is lower than the overdischarge voltage.

In this case, the overdischarge detector circuit G_2 of the battery state monitoring circuit BMB_2 outputs the overdischarge detection signal of high level to the second NOR circuit H_2 . In this situation, because the output signal of low level is output from the third inverter J_2 , the second NOR circuit H_2 outputs the negative OR signal of low level to the gate terminal of the second output transistor I_2 . As a result, the second output transistor I_2 is turned off.

That is, the input terminal of the fourth inverter K_1 is pulled up to high level by means of the second current source L_1 . As a result, a voltage is recognized as high level is applied to the input terminal of the fourth inverter K_1 , and the output signal of high level is output to the second NOR circuit H_1 from the third inverter J_1 . On the other hand, because the overdischarge detector circuit G_1 outputs the overdischarge detection signal of low level to the second NOR circuit H_1 , the second NOR circuit H_1 outputs the negative OR signal of low level to the gate terminal of the second output transistor I_1 . As a result, the second output transistor I_1 is turned off.

In this situation, the second transmitting terminal PD_2 of the battery state monitoring circuit BMB_2 is pulled up to VDD_1 through the resistive element Rb_1 . However, since the second transmitting terminal PD_2 is equipped with a third diode Dc_2 , the terminal voltage is clamped to $VSS_2+4.5$ V by a voltage (4.5 V) that causes the reverse current of the third diode Dc_2 to be generated. Also, the resistance of the resistive element Rb_1 is set to a value that allows the voltage of the input terminal of the fourth inverter K_1 to be pulled up to high level by the second current source L_1 .

As described above, when the second output transistor I_1 is turned off, the gate terminal of the second transistor **11** becomes at high level, and the second transistor **11** is turned off. As a result, the discharging to the load is prohibited.

In the first embodiment, in the battery state monitoring circuit that has detected the overcharged state or the overdischarged state, the first output transistor or the second output transistor are turned off, and a voltage for two cells (two batteries) is applied to the downstream side first output transistor or second output transistor which has been turned off by the pull-up operation in the upstream side battery state monitoring circuit. That is, the withstand voltage of one battery state monitoring circuit needs to be equal to or higher than the voltage for at least two cells. In contrast, in the third embodiment, in the battery state monitoring circuit that has detected the overcharged state or the overdischarged state, the first output transistor or the second output transistor are turned off, and a voltage for one cell (one battery) is applied to the downstream side first output transistor or second output transistor which has been turned off by the pull-up operation in the upstream side battery state monitoring circuit. That is, the

withstand voltage of one battery state monitoring circuit needs to be equal to or higher than the voltage for at least one cell. As a result, according to the third embodiment, the battery state monitoring circuit that is lower in withstand voltage than that of the first embodiment can be fabricated, and a range of the available manufacturing process is further broadened. As in the first embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange.

Fourth Embodiment

Subsequently, a description will be given of a battery device according to a fourth embodiment. FIG. 6 is a circuit configuration diagram showing the battery device according to the fourth embodiment. As shown in the figure, in the fourth embodiment, two types of diodes are disposed in the battery state monitoring circuit of the second embodiment. That is, when it is assumed that the symbols of the battery state monitoring circuits are BMC_1 to BMC_n , the battery state monitoring circuit BMC_n is newly equipped with a first diode De_n , a second diode Df_n , a third diode Dg_n , and a fourth diode Dh_n in addition to the components of the second embodiment. The same is applied to the other battery state monitoring circuits. In the following description, the battery state monitoring circuit BMC_n will be representatively described.

The first diode De_n has an anode terminal connected to the drain terminal of the first output transistor R_n , and a cathode terminal connected to the VDD_n . The first diode De_n has such a characteristic as to generate a reverse current when a reverse voltage corresponding to a voltage (for example, 4.5 V) that exceeds the withstand voltage of the battery state monitoring circuit is applied between the anode terminal and the cathode terminal. The second diode Df_n has an anode terminal connected to the input terminal of the second inverter S_n , and a cathode terminal connected to the VDD_n . It is assumed that the voltage drop of the second diode Df_n is 0.7 V.

The third diode Dg_n has an anode terminal connected to the drain terminal of the second output transistor V_n , and a cathode terminal connected to the VDD_n . The third diode Dg_n has such a characteristic as to generate a reverse current when a reverse voltage corresponding to a voltage (for example, 4.5 V) that exceeds the withstand voltage of the battery state monitoring circuit is applied between the anode terminal and the cathode terminal. The fourth diode Dh_n has an anode terminal connected to the input terminal of the fourth inverter W_n , and a cathode terminal connected to the VDD_n . It is assumed that the voltage drop of the fourth diode Dh_n is 0.7 V.

Also, resistive elements are connected between the first transmitting terminal of the upstream side battery state monitoring circuit and the first receiving terminal of the downstream side battery state monitoring circuit, and between the second transmitting terminal of the upstream side battery state monitoring circuit and the second receiving terminal of the downstream side battery state monitoring circuit, respectively. Specifically, a resistive element Ra_{n-1} is connected between the first transmitting terminal PC_{n-1} of the battery state monitoring circuit BMC_{n-1} and the first receiving terminal PE_n of the battery state monitoring circuit BMC_n , and a resistive element Rb_{n-1} is connected between the second transmitting terminal PD_{n-1} of the battery state monitoring circuit BMC_{n-1} and the second receiving terminal PF_{n-1} of the battery state monitoring circuit BMC_n , respectively.

Subsequently, a description will be given of the operation of the battery device according to the fourth embodiment, which is configured as described above. The operation in the cell balance state is identical with that in the first embodiment, and therefore its description will be omitted.

(Normal State)

First, a description will be given of a normal state, that is, a case in which all the voltages of the batteries BT_1 to BT_n are lower than the overcharge voltage, and equal to or higher than the overdischarge voltage. In the normal state thus defined, the overcharge detector circuit A_n of the battery state monitoring circuit BMC_n outputs the overcharge detection signal of low level to the first NOR circuit B_n .

In this situation, the first output transistor R_{n-1} of the battery state monitoring circuit BMC_{n-1} is on. As a result, the input terminal of the second inverter S_n of the battery state monitoring circuit BMC_n becomes at high level, and the output signal of low level is output from the second inverter S_n to the first NOR circuit B_n . The first NOR circuit B_n outputs the negative OR signal of high level to the first inverter Q_n , and the first inverter Q_n outputs the logical inversion signal of low level to the gate terminal of the first output transistor R_n . As a result, because the first output transistor R_n is turned on, the first transmitting terminal PC_n becomes at high level, and the first transistor **12** is turned on.

Also, in the above normal state, the overdischarge detector circuit G_n of the battery state monitoring circuit BMC_n outputs the overdischarge detection signal of low level to the second NOR circuit H_n . In this situation, the second output transistor V_{n-1} of the battery state monitoring circuit BMC_{n-1} is on. Therefore, the input terminal of the fourth inverter W_n in the battery state monitoring circuit BMC_n becomes at high level, and the output signal of low level is output to the second NOR circuit H_n from the fourth inverter W_n . The second NOR circuit H_n outputs the negative OR signal of high level to the third inverter U_n , and the third inverter U_n outputs the logical inversion signal of low level to the gate terminal of the second output transistor V_n . As a result, because the second output transistor V_n is turned on, the second transmitting terminal PD_n becomes at high level, and the second transistor **13** is turned on.

As described above, in the normal state, because the first transistor **12** and the second transistor **13** are turned on, the battery device is chargeable and dischargeable.

(Overcharged State)

Subsequently, a description will be given of an overcharged state, that is, a case in which a charger is connected between the first external terminal **30** and the second external terminal **31** to charge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes equal to or higher than the overcharge voltage. In the following description, it is assumed that the voltage of the battery BT_{n-1} is equal to or higher than the overcharge voltage.

In this case, the overcharge detector circuit A_{n-1} of the battery state monitoring circuit BMC_{n-1} outputs the overcharge detection signal of high level to the first NOR circuit B_{n-1} . In this situation, because the output signal of low level is output from the second inverter S_{n-1} , the first NOR circuit B_{n-1} outputs the negative OR signal of low level to the first inverter Q_{n-1} , and the first inverter Q_{n-1} outputs the logical inversion signal of high level to the gate terminal of the first output transistor R_{n-1} . As a result, the first output transistor R_{n-1} is turned off.

That is, the input terminal of the second inverter S_n is pulled down to low level by means of the first current source T_n . When the pull-down voltage becomes equal to or lower than $VDD_n-4.5$ V, a current flows in the VSS_n through a first diode

De_{n-1} of the battery state monitoring circuit BMC_{n-1} . That is, the input terminal of the second inverter S_n is clamped to $VDD_n-4.5$ V, and in that condition, the voltage does not satisfy the operating voltage (voltage that is recognized as low level) of the second inverter S_n . Therefore, the resistance of the resistive element Ra_{n-1} is set so that the voltage of the input terminal of the second inverter S_n reaches the operating voltage.

With the above arrangement, a voltage recognized as low level is applied to the input terminal of the second inverter S_n , and the output signal of high level is output to the first NOR circuit B_n from the second inverter S_n . On the other hand, because the overcharge detector circuit A_n outputs the overcharge detection signal of low level to the first NOR circuit B_n , the first NOR circuit B_n outputs the negative OR signal of low level to the first inverter Q_n , and the first inverter Q_n outputs the logical inversion signal of high level to the gate terminal of the first output transistor R_n . As a result, the first output transistor R_n is turned off.

As described above, when the first output transistor R_n is turned off, the gate terminal of the first transistor **12** becomes at low level, and the first transistor **12** is turned off. As a result, the charging from the charger is prohibited.

(Overdischarged State)

Subsequently, a description will be given of an overdischarged state, that is, a case in which a load is connected between the first external terminal **30** and the second external terminal **31** to discharge the batteries BT_1 to BT_n , and at least one voltage of those batteries BT_1 to BT_n becomes lower than the overdischarge voltage. In the following description, it is assumed that the voltage of the battery BT_{n-1} is lower than the overdischarge voltage.

In this case, the overdischarge detector circuit G_{n-1} of the battery state monitoring circuit BMC_{n-1} outputs the overdischarge detection signal of high level to the second NOR circuit H_{n-1} . In this situation, because the output signal of low level is output from the fourth inverter W_{n-1} , the second NOR circuit H_{n-1} outputs the negative OR signal of low level to the third inverter U_{n-1} , and the third inverter U_{n-1} outputs the logical inversion signal of high level to the gate terminal of the second output transistor V_{n-1} . As a result, the second output transistor V_{n-1} is turned off.

That is, the input terminal of the fourth inverter W_n is pulled down to low level by means of the second current source X_n . When the pull-down voltage becomes equal to or lower than $VDD_n-4.5$ V, a current flows in the VSS_n through a third diode Dg_{n-1} of the battery state monitoring circuit BMC_{n-1} . That is, the input terminal of the fourth inverter W_n is clamped to $VDD_n-4.5$ V, and in that condition, the voltage does not satisfy the operating voltage (voltage that is recognized as low level) of the fourth inverter W_n . Therefore, the resistance of the resistive element Rb_{n-1} is set so that the voltage of the input terminal of the fourth inverter W_n reaches the operating voltage.

With the above arrangement, a voltage recognized as low level is applied to the input terminal of the fourth inverter W_n , and the output signal of high level is output to the second NOR circuit H_n from the fourth inverter W_n . On the other hand, because the overdischarge detector circuit G_n outputs the overdischarge detection signal of low level to the second NOR circuit H_n , the second NOR circuit H_n outputs the negative OR signal of low level to the third inverter U_n , and the third inverter U_n outputs the logical inversion signal of high level to the gate terminal of the second output transistor V_n . As a result, the second output transistor V_n is turned off.

As described above, when the second output transistor V_n is turned off, the gate terminal of the second transistor **13**

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becomes at low level, and the second transistor 13 is turned off. As a result, the discharging to the load is prohibited.

As described above, according to the fourth embodiment, the withstand voltage of one battery state monitoring circuit needs to be equal to or higher than the voltage for at least one cell as in the third embodiment. As a result, according to the fourth embodiment, the battery state monitoring circuit that is further lower in withstand voltage than that of the second embodiment can be fabricated, and a range of the available manufacturing process is further broadened. As in the second embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange.

Fifth Embodiment

Subsequently, a description will be given of a battery device according to a fifth embodiment. FIG. 7 is a circuit configuration diagram showing the battery device according to the fifth embodiment. As shown in the figure, in the fifth embodiment, the resistive elements that are disposed in the exterior of the battery state monitoring circuit in the third embodiment are disposed in the interior of the battery state monitoring circuit.

A battery state monitoring circuit BMD_1 will be representatively described. The resistive element Ra_1 is connected between the first receiving terminal PE_1 and the cathode terminal of the second diode Db_1 in the battery state monitoring circuit BMD_1 . Also, the resistive element Rb_1 is connected between the second receiving terminal PF_1 and the cathode terminal of the fourth diode Dd_1 .

The operation is identical with that in the third embodiment, and therefore its description will be omitted.

With the above configuration, a manufacturer of the battery device may merely prepare the battery state monitoring circuits BMD_1 of the same number as the number of batteries, and connect the upstream side and downstream side battery state monitoring circuits through no resistive element, thereby contributing to a reduction in manufacturing process. The provision of the resistive elements in the interior of the battery state monitoring circuit causes an increase in sizes of the battery state monitoring circuit and an increase in costs. In order to prevent this drawback, there can be applied the third embodiment.

Sixth Embodiment

Subsequently, a description will be given of a battery device according to a sixth embodiment. FIG. 8 is a circuit configuration diagram showing the battery device according to the sixth embodiment. As shown in the figure, in the sixth embodiment, the resistive elements that are disposed in the exterior of the battery state monitoring circuit in the fourth embodiment are disposed in the interior of the battery state monitoring circuit.

A battery state monitoring circuit BME_n will be representatively described. A resistive element Ra_n is connected between the anode terminal of the diode Do_n and the anode terminal of the first diode De_n in the battery state monitoring circuit BME_n . Also, a resistive element Rb_n is connected between the anode terminal of the third diode Dg_n and the second transmitting terminal PD_n .

The operation is identical with that in the fourth embodiment, and therefore its description will be omitted.

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With the above configuration, a manufacturer of the battery device may merely prepare the battery state monitoring circuits BME_n of the same number as the number of batteries, and connect the upstream side and downstream side battery state monitoring circuits through no resistive element, thereby contributing to a reduction in manufacturing process. The provision of the resistive elements in the interior of the battery state monitoring circuit causes an increase in sizes of the battery state monitoring circuit and an increase in costs. In order to prevent this drawback, there can be applied the fourth embodiment.

Alternatively, the resistive element Ra_n may be connected between the input terminal of the second inverter S_n and the first receiving terminal PE_n , and the resistive element Rb_n may be connected between the input terminal of the fourth inverter W_n and the second receiving terminal PF_n . Also, the resistive element Ra_n may be connected between the anode terminal of the second diode Df_n and the first receiving terminal PE_n , and the resistive element Rb_n may be connected between the cathode terminal of the fourth diode Dh_n and the second receiving terminal PF_n .

Seventh Embodiment

Subsequently, a description will be given of a battery device according to a seventh embodiment. FIG. 9 is a circuit configuration diagram showing the battery device according to the seventh embodiment. As shown in the figure, the seventh embodiment is directed to the battery device in which the discharge leak current prevention diodes Do_1 to Do_n are not disposed in the respective battery state monitoring circuits BM_1 to BM_n of the first embodiment. In order to distinguish from the first embodiment, the symbols of the battery state monitoring circuits in the seventh embodiment are denoted by BM_1' to BM_n' . In the seventh embodiment, a discharge leak current prevention diode Do is disposed in the exterior of the battery state monitoring circuits BM_1' to BM_n' . Specifically, an anode terminal of the diode Do is connected to the gate terminal of the first transistor 10, and a cathode terminal of the diode Do is connected to the first transmitting terminal PC_1 of the battery state monitoring circuit BM_1 .

With the battery device configured as described above, as in the first embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange. Also, because it is unnecessary to provide the discharge leak current prevention diode within the battery state monitoring circuit, it is possible to reduce the costs and downsize the circuit.

Eighth Embodiment

Subsequently, a description will be given of a battery device according to an eighth embodiment. FIG. 10 is a circuit configuration diagram showing the battery device according to the eighth embodiment. As shown in the figure, the eighth embodiment is directed to the battery device in which the discharge leak current prevention diodes Do_1 to Do_n are not disposed in the respective battery state monitoring circuits BMA_1 to BMA_n of the second embodiment. In order to distinguish from the second embodiment, the symbols of the battery state monitoring circuits in the eighth embodiment are denoted by BMA_1' to BMA_n' . In the eighth embodiment, the discharge leak current prevention diode Do is disposed in the exterior of the battery state monitoring circuits BMA_1' to

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BMA_n'. Specifically, the cathode terminal of the diode Do is connected to the gate terminal of the first transistor 12, and the anode terminal of the diode Do is connected to the first transmitting terminal PC_n of the battery state monitoring circuit BMA_n.

With the battery device configured as described above, as in the second embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange. Also, because it is unnecessary to provide the discharge leak current prevention diode within the battery state monitoring circuit, it is possible to reduce the costs and downsize the circuit.

Ninth Embodiment

Subsequently, a description will be given of a battery device according to a ninth embodiment. FIG. 11 is a circuit configuration diagram showing the battery device according to the ninth embodiment. As shown in the figure, the ninth embodiment is directed to the battery device in which the discharge leak current prevention diodes Do₁ to Do_n are not disposed in the respective battery state monitoring circuits BMB₁ to BMB_n of the third embodiment. In order to distinguish from the third embodiment, the symbols of the battery state monitoring circuits in the ninth embodiment are denoted by BMB₁' to BMB_n'. In the ninth embodiment, the discharge leak current prevention diode Do is disposed in the exterior of the battery state monitoring circuits BMB₁' to BMB_n'. Specifically, the anode terminal of the diode Do is connected to the gate terminal of the first transistor 10, and the cathode terminal of the diode Do is connected to the first transmitting terminal PC₁ of the battery state monitoring circuit BMB₁.

With the battery device configured as described above, as in the third embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange. Also, because it is unnecessary to provide the discharge leak current prevention diode within the battery state monitoring circuit, it is possible to reduce the costs and downsize the circuit.

Tenth Embodiment

Subsequently, a description will be given of a battery device according to a tenth embodiment. FIG. 12 is a circuit configuration diagram showing the battery device according to the tenth embodiment. As shown in the figure, the tenth embodiment is directed to the battery device in which the discharge leak current prevention diodes Do₁ to Do_n are not disposed in the respective battery state monitoring circuits BMC₁ to BMC_n of the fourth embodiment. In order to distinguish from the fourth embodiment, the symbols of the battery state monitoring circuits in the tenth embodiment are denoted by BMC₁' to BMC_n'. In the tenth embodiment, the discharge leak current prevention diode Do is disposed in the exterior of the battery state monitoring circuits BMC₁' to BMC_n'. Specifically, the cathode terminal of the diode Do is connected to the gate terminal of the first transistor 12, and the anode terminal of the diode Do is connected to the first transmitting terminal PC_n of the battery state monitoring circuit BMC_n.

With the battery device configured as described above, as in the fourth embodiment, the occurrence of the discharge

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leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange. Also, because it is unnecessary to provide the discharge leak current prevention diode within the battery state monitoring circuit, it is possible to reduce the costs and downsize the circuit.

Eleventh Embodiment

Subsequently, a description will be given of a battery device according to an eleventh embodiment. FIG. 13 is a circuit configuration diagram showing the battery device according to the eleventh embodiment. As shown in the figure, the eleventh embodiment is directed to the battery device in which the discharge leak current prevention diodes Do₁ to Do_n are not disposed in the respective battery state monitoring circuits BMD₁ to BMD_n of the fifth embodiment. In order to distinguish from the fifth embodiment, the symbols of the battery state monitoring circuits in the eleventh embodiment are denoted by BMD₁' to BMD_n'. In the eleventh embodiment, the discharge leak current prevention diode Do is disposed in the exterior of the battery state monitoring circuits BMD₁' to BMD_n'. Specifically, the anode terminal of the diode Do is connected to the gate terminal of the first transistor 10, and the cathode terminal of the diode Do is connected to the first transmitting terminal PC₁ of the battery state monitoring circuit BMD₁.

With the battery device configured as described above, as in the fifth embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange. Also, because it is unnecessary to provide the discharge leak current prevention diode within the battery state monitoring circuit, it is possible to reduce the costs and downsize the circuit.

Twelfth Embodiment

Subsequently, a description will be given of a battery device according to a twelfth embodiment. FIG. 14 is a circuit configuration diagram showing the battery device according to the twelfth embodiment. As shown in the figure, the twelfth embodiment is directed to the battery device in which the discharge leak current prevention diodes Do₁ to Do_n are not disposed in the respective battery state monitoring circuits BME₁ to BME_n of the sixth embodiment. In order to distinguish from the sixth embodiment, the symbols of the battery state monitoring circuits in the twelfth embodiment are denoted by BME₁' to BME_n'. In the twelfth embodiment, the discharge leak current prevention diode Do is disposed in the exterior of the battery state monitoring circuits BME₁' to BAE_n'. Specifically, the cathode terminal of the diode Do is connected to the gate terminal of the first transistor 12, and the anode terminal of the diode Do is connected to the first transmitting terminal PC_n of the battery state monitoring circuit BME_n.

With the battery device configured as described above, as in the sixth embodiment, the occurrence of the discharge leak current can be prevented, and the disruption of the voltage balance between the batteries as in the conventional technology does not occur. As a result, it is possible to eliminate the load on the user such as the costs and time required for battery exchange. Also, because it is unnecessary to provide the

discharge leak current prevention diode within the battery state monitoring circuit, it is possible to reduce the costs and downsize the circuit.

What is claimed is:

1. A battery state monitoring circuit, comprising:
 - a battery state detector circuit that detects a state of a battery based on a voltage of the battery;
 - a transmitting terminal that transmits battery state information indicative of the state of the battery to an outside;
 - a receiving terminal that receives battery state information of another battery from the outside;
 - a transistor that is used for transmitting the battery state information, and has any one of two terminals except for a control terminal connected to the transmitting terminal; and
 - a diode that is connected in a direction opposite to a direction of a parasitic diode disposed between the two terminals of the transistor, the diode being disposed between the transmitting terminal and one terminal of the transistor.
2. A battery state monitoring circuit according to claim 1, further comprising:
 - a first voltage monitor terminal that is used for connection with a positive terminal of the battery and connected to an internal positive side common power source wire;
 - a second voltage monitor terminal that is used for connection with a negative terminal of the battery and connected to an internal negative side common power source wire;
 - a first transmitting terminal;
 - a second transmitting terminal;
 - a first receiving terminal;
 - a second receiving terminal;
 - a cell balance control terminal;
 - an overcharge detector circuit that detects whether or not the battery is overcharged based on a voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overcharge detection signal indicative of a detection result in question as the battery state detector circuit;
 - an overdischarge detector circuit that detects whether or not the battery is overdischarged based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overdischarge detection signal indicative of a detection result in question as the battery state detector circuit;
 - a cell balance circuit that detects whether or not the battery needs to be subjected to cell balance control based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs a cell balance signal indicative of a detection result in question to the cell balance control terminal as the battery state detector circuit;
 - a first logical inversion circuit;
 - a second logical inversion circuit having an output terminal connected to an input terminal of the first logical inversion circuit, and an input terminal connected to the first receiving terminal;
 - a first current source having an input terminal connected to the internal positive side common power source wire, and an output terminal connected to the first receiving terminal;
 - a first negative OR circuit that receives the overcharge detection signal and an output signal of the first logical inversion circuit, and outputs a negative OR signal of the overcharge detection signal and the output signal of the first logical inversion circuit;

- a first n-channel type transistor having a gate terminal receiving the negative OR signal of the overdischarge detection signal and the output signal of the first logical inversion circuit, a drain terminal connected to a cathode terminal of the diode, and a source terminal connected to the internal negative side common power source wire;
 - a third logical inversion circuit;
 - a fourth logical inversion circuit having an output terminal connected to an input terminal of the third logical inversion circuit, and an input terminal connected to the second receiving terminal;
 - a second current source having an input terminal connected to the internal positive side common power source wire, and an output terminal connected to the second receiving terminal;
 - a second negative OR circuit that receives the overdischarge detection signal and an output signal of the third logical inversion circuit, and outputs a negative OR signal of the overcharge detection signal and the output signal of the third logical inversion circuit; and
 - a second n-channel type transistor having a gate terminal receiving the negative OR signal the overdischarge detection signal and the output signal of the third logical inversion circuit, a drain terminal connected to the second transmitting terminal, and a source terminal connected to the internal negative side common power source wire, wherein the diode has an anode terminal connected to the first transmitting terminal, and wherein the battery state monitoring circuit is constituted as one semiconductor device.
3. A battery state monitoring circuit according to claim 1, further comprising:
 - a first voltage monitor terminal that is used for connection with a positive terminal of the battery and connected to an internal positive side common power source wire;
 - a second voltage monitor terminal that is used for connection with a negative terminal of the battery and connected to an internal negative side common power source wire;
 - a first transmitting terminal;
 - a second transmitting terminal;
 - a first receiving terminal;
 - a second receiving terminal;
 - a cell balance control terminal;
 - an overcharge detector circuit that detects whether or not the battery is overcharged based on a voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overcharge detection signal indicative of a detection result in question as the battery state detector circuit;
 - an overdischarge detector circuit that detects whether or not the battery is overdischarged based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overdischarge detection signal indicative of a detection result in question as the battery state detector circuit;
 - a cell balance circuit that detects whether or not the battery needs to be subjected to cell balance control based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs a cell balance signal indicative of a detection result in question to the cell balance control terminal as the battery state detector circuit;
 - a first logical inversion circuit;
 - a first p-channel type transistor having a gate terminal receiving an output signal of the first logical inversion

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circuit, a drain terminal connected to an anode terminal of the diode, and a source terminal connected to the internal positive side common power source wire;

a first current source having an input terminal connected to the first receiving terminal, and an output terminal connected to the internal negative side common power source wire;

a second logical inversion circuit having an input terminal connected to the first receiving terminal;

a first negative OR circuit that receives the overcharge detection signal and an output signal of the second logical inversion circuit, and outputs a negative OR signal of the overcharge detection signal and the output signal of the second logical inversion circuit to the first logical inversion circuit;

a third logical inversion circuit;

a second p-channel type transistor having a gate terminal receiving an output signal of the third logical inversion circuit, a drain terminal connected to the second transmitting terminal, and a source terminal connected to the internal positive side common power source wire;

a second current source having an input terminal connected to the second receiving terminal, and an output terminal connected to the internal negative side common power source wire;

a fourth logical inversion circuit having an input terminal connected to the second receiving terminal; and

a second negative OR circuit that receives the overdischarge detection signal and an output signal of the fourth logical inversion circuit, and outputs a negative OR signal of the overdischarge detection signal and the output signal of the fourth logical inversion circuit to the third logical inversion circuit,

wherein the diode has a cathode terminal connected to the first transmitting terminal, and

wherein the battery state monitoring circuit is constituted as one semiconductor device.

4. A battery state monitoring circuit according to claim 2, further comprising:

a first clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the drain terminal of the first n-channel type transistor, and has a characteristic that allows a reverse current to flow in the first clamp diode when a reverse voltage corresponding to a voltage which exceeds a withstand voltage of the battery state monitoring circuit is applied to the first clamp diode;

a second clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the output terminal of the first current source;

a third clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the drain terminal of the second n-channel type transistor, and has a characteristic that allows the reverse current to flow in the third clamp diode when the reverse voltage corresponding to the voltage which exceeds the withstand voltage of the battery state monitoring circuit is applied to the third clamp diode; and

a fourth clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the output terminal of the second current source.

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5. A battery state monitoring circuit according to claim 3, further comprising:

a first clamp diode that has an anode terminal connected to the drain terminal of the first p-channel type transistor, and a cathode terminal connected to the internal positive side common power source wire, and has a characteristic that allows a reverse current to flow in the first clamp diode when a reverse voltage corresponding to a voltage which exceeds a withstand voltage of the battery state monitoring circuit is applied to the first clamp diode;

a second clamp diode that has an anode terminal connected to the input terminal of the first current source, and a cathode terminal connected to the internal positive side common power source wire;

a third clamp diode that has an anode terminal connected to the drain terminal of the second p-channel type transistor, and a cathode terminal connected to the internal positive side common power source wire, and has a characteristic that allows the reverse current to flow in the third clamp diode when the reverse voltage corresponding to the voltage which exceeds the withstand voltage of the battery state monitoring circuit is applied to the third clamp diode; and

a fourth clamp diode that has an anode terminal connected to the input terminal of the second current source, and a cathode terminal connected to the internal positive side common power source wire.

6. A battery state monitoring circuit according to claim 4, further comprising:

a first resistive element that is connected between the cathode terminal of the second clamp diode and the first receiving terminal; and

a second resistive element that is connected between the cathode terminal of the fourth clamp diode and the second receiving terminal.

7. A battery state monitoring circuit according to claim 5, further comprising:

a first resistive element that is connected between the anode terminal of the first clamp diode and the first transmitting terminal; and

a second resistive element that is connected between the anode terminal of the third clamp diode and the second transmitting terminal.

8. A battery device, comprising:

a plurality of batteries that are connected in series;

the battery state monitoring circuit according to claim 1, which is disposed in correspondence with each of the plurality of batteries; and

a switch circuit that switches between permission and prohibition of charging and discharging of the plurality of batteries,

wherein the transmitting terminal of the battery state monitoring circuit is connected to the receiving terminal of one of the adjacent battery state monitoring circuits, and the receiving terminal of the battery state monitoring circuit is connected to the transmitting terminal of another one of the adjacent battery state monitoring circuits, and

wherein the switch circuit switches between the permission and the prohibition of the charging and the discharging based on the battery state information that is transmitted from the transmitting terminal of the battery state monitoring circuit corresponding to a battery at one end of the plurality of batteries that are connected in series.

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9. A battery device, comprising:
 a plurality of batteries that are connected in series;
 the battery state monitoring circuit according to claim 2 or
 6, which is disposed in correspondence with each of the
 plurality of batteries; 5
 a cell balance switch circuit that is connected in parallel
 with the each of the plurality of batteries, and switches
 between connection and disconnection of two terminals
 according to the cell balance signal that is output from
 the cell balance control terminal of the battery state 10
 monitoring circuit which corresponds to the each of the
 plurality of batteries;
 a first external terminal;
 a second external terminal;
 a charging p-channel type transistor; 15
 a discharging p-channel type transistor;
 a first bias resistive element having one end connected to a
 gate terminal of the charging p-channel type transistor,
 and another end connected to a source terminal of the
 charging p-channel type transistor; and 20
 a second bias resistive element having one end connected
 to a gate terminal of the discharging p-channel type
 transistor, and another end connected to a source termi-
 nal of the discharging p-channel type transistor,
 wherein the battery state monitoring circuit has the first 25
 voltage monitor terminal connected to the positive ter-
 minal of a corresponding battery, respectively, the sec-
 ond voltage monitor terminal connected to the negative
 terminal of the corresponding battery, respectively, the
 first transmitting terminal connected to the first receiv- 30
 ing terminal of one of the adjacent battery state moni-
 toring circuits, the second transmitting terminal con-
 nected to the second receiving terminal of the one of the
 adjacent battery state monitoring circuits, the first
 receiving terminal connected to the first transmitting 35
 terminal of another one of the adjacent battery state
 monitoring circuits, and the second receiving terminal
 connected to the second transmitting terminal of the
 another one of the adjacent battery state monitoring
 circuits, 40
 wherein the battery state monitoring circuit corresponding
 to a battery at one end of the plurality of batteries that are
 connected in series has the first transmitting terminal
 connected to the gate terminal of the charging p-channel
 type transistor, and the second transmitting terminal 45
 connected to the gate terminal of the discharging p-chan-
 nel type transistor,
 wherein the discharging p-channel type transistor has the
 source terminal connected to the positive terminal of the
 battery at the one end, and a drain terminal connected to 50
 a drain terminal of the charging p-channel type transis-
 tor, and the charging p-channel type transistor has the
 source terminal connected to the first external terminal,
 wherein a battery at another end of the plurality of batteries
 that are connected in series has the negative terminal 55
 connected to the second external terminal, and
 wherein the battery state monitoring circuit corresponding
 to the battery at the another end has the first receiving
 terminal and the second receiving terminal connected to
 the negative terminal of the battery at the another end. 60

10. A battery device, comprising:
 a plurality of batteries that are connected in series;
 the battery state monitoring circuit according to claim 3 or
 7, which is disposed in correspondence with each of the
 plurality of batteries; 65
 a cell balance switch circuit that is connected in parallel
 with the each of the plurality of batteries, and switches

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between connection and disconnection of two terminals
 according to the cell balance signal that is output from
 the cell balance control terminal of the battery state
 monitoring circuit which corresponds to the each of the
 plurality of batteries;
 a first external terminal;
 a second external terminal;
 a charging n-channel type transistor;
 a discharging n-channel type transistor;
 a first bias resistive element having one end connected to a
 gate terminal of the charging n-channel type transistor,
 and another end connected to a source terminal of the
 charging n-channel type transistor; and
 a second bias resistive element having one end connected
 to a gate terminal of the discharging n-channel type
 transistor, and another end connected to a source termi-
 nal of the discharging n-channel type transistor,
 wherein the battery state monitoring circuit has the first
 voltage monitor terminal connected to the positive ter-
 minal of a corresponding battery, respectively, the sec-
 ond voltage monitor terminal connected to the negative
 terminal of the corresponding battery, respectively, the
 first transmitting terminal connected to the first receiv-
 ing terminal of one of the adjacent battery state moni-
 toring circuits, the second transmitting terminal con-
 nected to the second receiving terminal of the one of the
 adjacent battery state monitoring circuits, the first
 receiving terminal connected to the first transmitting
 terminal of another one of the adjacent battery state
 monitoring circuits, and the second receiving terminal
 connected to the second transmitting terminal of the
 another one of the adjacent battery state monitoring
 circuits,
 wherein a battery at one end of the plurality of batteries that
 are connected in series has the positive terminal con-
 nected to the first external terminal,
 wherein the battery state monitoring circuit corresponding
 to the battery at the one end has the first receiving ter-
 minal and the second receiving terminal connected to the
 positive terminal of the battery at the one end,
 wherein the battery state monitoring circuit corresponding
 to a battery at another end of the plurality of batteries that
 are connected in series has the first transmitting terminal
 connected to the gate terminal of the charging n-channel
 type transistor, and the second transmitting terminal
 connected to the gate terminal of the discharging n-chan-
 nel type transistor, and
 wherein the discharging n-channel type transistor has the
 source terminal connected to the negative terminal of the
 battery at the another end, and a drain terminal con-
 nected to a drain terminal of the charging n-channel type
 transistor, and the charging n-channel type transistor has
 the source terminal connected to the second external
 terminal.

11. A battery device, comprising:
 a plurality of batteries that are connected in series;
 the battery state monitoring circuit according to claim 4,
 which is disposed in correspondence with each of the
 plurality of batteries;
 a cell balance switch circuit that is connected in parallel
 with the each of the plurality of batteries, and switches
 between connection and disconnection of two terminals
 according to the cell balance signal that is output from
 the cell balance control terminal of the battery state
 monitoring circuit which corresponds to the each of the
 plurality of batteries;
 a first external terminal;

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a second external terminal;
 a charging p-channel type transistor;
 a discharging p-channel type transistor;
 a first bias resistive element having one end connected to a
 gate terminal of the charging p-channel type transistor, 5
 and another end connected to a source terminal of the
 charging p-channel type transistor; and
 a second bias resistive element having one end connected
 to a gate terminal of the discharging p-channel type
 transistor, and another end connected to a source terminal 10
 of the discharging p-channel type transistor,
 wherein the battery state monitoring circuit has the first
 voltage monitor terminal connected to the positive ter-
 minal of a corresponding battery, respectively, the sec- 15
 ond voltage monitor terminal connected to the negative
 terminal of the corresponding battery, respectively, the
 first transmitting terminal connected to the first receiv-
 ing terminal of one of the adjacent battery state moni-
 toring circuits through a resistive element, the second
 transmitting terminal connected to the second receiving 20
 terminal of the one of the adjacent battery state moni-
 toring circuits through the resistive element, the first
 receiving terminal connected to the first transmitting
 terminal of another one of the adjacent battery state
 monitoring circuits through the resistive element, and 25
 the second receiving terminal connected to the second
 transmitting terminal of the another one of the adjacent
 battery state monitoring circuits through the resistive
 element,
 wherein the battery state monitoring circuit corresponding 30
 to a battery at one end of the plurality of batteries that are
 connected in series has the first transmitting terminal
 connected to the gate terminal of the charging p-channel
 type transistor, and the second transmitting terminal
 connected to the gate terminal of the discharging p-chan- 35
 nel type transistor,
 wherein the discharging p-channel type transistor has the
 source terminal connected to the positive terminal of the
 battery at the one end, and a drain terminal connected to
 a drain terminal of the charging p-channel type transis- 40
 tor, the charging p-channel type transistor has the source
 terminal connected to the first external terminal, and a
 battery at another end of the plurality of batteries that are
 connected in series has the negative terminal connected
 to the second external terminal, and 45
 wherein the battery state monitoring circuit corresponding
 to the battery at the another end has the first receiving
 terminal and the second receiving terminal connected to
 the negative terminal of the battery at the another end.

12. A battery device, comprising: 50
 a plurality of batteries that are connected in series;
 the battery state monitoring circuit according to claim 5,
 which is disposed in correspondence with each of the
 plurality of batteries;
 a cell balance switch circuit that is connected in parallel 55
 with the each of the plurality of batteries, and switches
 between connection and disconnection of two terminals
 according to the cell balance signal that is output from
 the cell balance control terminal of the battery state
 monitoring circuit which corresponds to the each of the 60
 plurality of batteries;
 a first external terminal;
 a second external terminal;
 a charging n-channel type transistor;
 a discharging n-channel type transistor; 65
 a first bias resistive element having one end connected to a
 gate terminal of the charging n-channel type transistor,

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and another end connected to a source terminal of the
 charging n-channel type transistor; and
 a second bias resistive element having one end connected
 to a gate terminal of the discharging n-channel type
 transistor, and another end connected to a source termi-
 nal of the discharging n-channel type transistor,
 wherein the battery state monitoring circuit has the first
 voltage monitor terminal connected to the positive ter-
 minal of a corresponding battery, respectively, the sec-
 ond voltage monitor terminal connected to the negative
 terminal of the corresponding battery, respectively, the
 first transmitting terminal connected to the first receiv-
 ing terminal of one of the adjacent battery state moni-
 toring circuits through a resistive element, the second
 transmitting terminal connected to the second receiving
 terminal of the one of the adjacent battery state moni-
 toring circuits through the resistive element, the first
 receiving terminal connected to the first transmitting
 terminal of another one of the adjacent battery state
 monitoring circuits through the resistive element, and
 the second receiving terminal connected to the second
 transmitting terminal of the another one of the adjacent
 battery state monitoring circuits through the resistive
 element,
 wherein a battery at one end of the plurality of batteries that
 are connected in series has the positive terminal con-
 nected to the first external terminal,
 wherein the battery state monitoring circuit corresponding
 to the battery at the one end has the first receiving ter-
 minal and the second receiving terminal connected to the
 positive terminal of the battery at the one end,
 wherein the battery state monitoring circuit corresponding
 to a battery at another end of the plurality of batteries that
 are connected in series has the first transmitting terminal
 connected to the gate terminal of the charging n-channel
 type transistor, and the second transmitting terminal
 connected to the gate terminal of the discharging n-chan-
 nel type transistor, and
 wherein the discharging n-channel type transistor has the
 source terminal connected to the negative terminal of the
 battery at the another end, and a drain terminal con-
 nected to a drain terminal of the charging n-channel type
 transistor, and the charging n-channel type transistor has
 the source terminal connected to the second external
 terminal.

13. A battery device, comprising:
 a plurality of batteries that are connected in series;
 a battery state monitoring circuit that is disposed in corre-
 spondence with each of the plurality of batteries, the
 battery state monitoring circuit comprising:
 a first voltage monitor terminal that is used for connec-
 tion with a positive terminal of one of the plurality of
 batteries and connected to an internal positive side
 common power source wire;
 a second voltage monitor terminal that is used for con-
 nection with a negative terminal of the one of the
 plurality of batteries and connected to an internal
 negative side common power source wire;
 a first transmitting terminal;
 a second transmitting terminal;
 a first receiving terminal;
 a second receiving terminal;
 a cell balance control terminal;
 an overcharge detector circuit that detects whether or not
 the one of the plurality of batteries is overcharged
 based on a voltage between the first voltage monitor
 terminal and the second voltage monitor terminal, and

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outputs an overcharge detection signal indicative of a detection result in question;
 an overdischarge detector circuit that detects whether or not the one of the plurality of batteries is overdischarged based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overdischarge detection signal indicative of a detection result in question;
 a cell balance circuit that detects whether or not the one of the plurality of batteries needs to be subjected to cell balance control based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs a cell balance signal indicative of a detection result in question to the cell balance control terminal;
 a first logical inversion circuit;
 a second logical inversion circuit having an output terminal connected to an input terminal of the first logical inversion circuit, and an input terminal connected to the first receiving terminal;
 a first current source having an input terminal connected to the internal positive side common power source wire, and an output terminal connected to the first receiving terminal;
 a first negative OR circuit that receives the overcharge detection signal and an output signal of the first logical inversion circuit, and outputs a negative OR signal of the overcharge detection signal and the output signal of the first logical inversion circuit;
 a first n-channel type transistor having a gate terminal receiving the negative OR signal of the overcharge detection signal and the output signal of the first logical inversion circuit, a drain terminal connected to the first transmitting terminal, and a source terminal connected to the internal negative side common power source wire;
 a third logical inversion circuit;
 a fourth logical inversion circuit having an output terminal connected to an input terminal of the third logical inversion circuit, and an input terminal connected to the second receiving terminal;
 a second current source having an input terminal connected to the internal positive side common power source wire, and an output terminal connected to the second receiving terminal;
 a second negative OR circuit that receives the overdischarge detection signal and an output signal of the third logical inversion circuit, and outputs a negative OR signal of the overdischarge detection signal and the output signal of the third logical inversion circuit;
 and
 a second n-channel type transistor having a gate terminal receiving the negative OR signal of the overdischarge detection signal and the output signal of the third logical inversion circuit, a drain terminal connected to the second transmitting terminal, and a source terminal connected to the internal negative side common power source wire;
 a cell balance switch circuit that is connected in parallel with the each of the plurality of batteries, and switches between connection and disconnection of two terminals according to the cell balance signal that is output from the cell balance control terminal of the battery state monitoring circuit corresponding to the each of the plurality of batteries;
 a first external terminal;
 a second external terminal;

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a charging p-channel type transistor;
 a discharging p-channel type transistor;
 a first bias resistive element having one end connected to a gate terminal of the charging p-channel type transistor, and another end connected to a source terminal of the charging p-channel type transistor;
 a second bias resistive element having one end connected to a gate terminal of the discharging p-channel type transistor, and another end connected to a source terminal of the discharging p-channel type transistor; and
 a diode having an anode terminal connected to the gate terminal of the charging p-channel type transistor, wherein the battery state monitoring circuit has the first voltage monitor terminal connected to the positive terminal of a corresponding battery, respectively, the second voltage monitor terminal connected to the negative terminal of the corresponding battery, respectively, the first transmitting terminal connected to the first receiving terminal of one of the adjacent battery state monitoring circuits, the second transmitting terminal connected to the second receiving terminal of the one of the adjacent battery state monitoring circuits, the first receiving terminal connected to the first transmitting terminal of another one of the adjacent battery state monitoring circuits, and the second receiving terminal connected to the second transmitting terminal of the another one of the adjacent battery state monitoring circuits,
 wherein the battery state monitoring circuit corresponding to a battery at one end of the plurality of batteries that are connected in series has the first transmitting terminal connected to a cathode terminal of the diode, and the second transmitting terminal connected to the gate terminal of the discharging p-channel type transistor,
 wherein the discharging p-channel type transistor has the source terminal connected to the positive terminal of the battery at the one end, and a drain terminal connected to a drain terminal of the charging p-channel type transistor, the charging p-channel type transistor has the source terminal connected to the first external terminal, and a battery at another end of the plurality of batteries that are connected in series has the negative terminal connected to the second external terminal, and
 wherein the battery state monitoring circuit corresponding to the battery at the another end has the first receiving terminal and the second receiving terminal connected to the negative terminal of the battery at the another end.

14. A battery device, comprising:
 a plurality of batteries that are connected in series;
 a battery state monitoring circuit that is disposed in correspondence with each of the plurality of batteries, the battery state monitoring circuit comprising:
 a first voltage monitor terminal that is used for connection with a positive terminal of one of the plurality of batteries and connected to an internal positive side common power source wire;
 a second voltage monitor terminal that is used for connection with a negative terminal of the one of the plurality of batteries and connected to an internal negative side common power source wire;
 a first transmitting terminal;
 a second transmitting terminal;
 a first receiving terminal;
 a second receiving terminal;
 a cell balance control terminal;
 an overcharge detector circuit that detects whether or not the one of the plurality of batteries is overcharged

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based on a voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overcharge detection signal indicative of a detection result in question;

an overdischarge detector circuit that detects whether or not the one of the plurality of batteries is overdischarged based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs an overdischarge detection signal indicative of a detection result in question;

a cell balance circuit that detects whether or not the one of the plurality of batteries needs to be subjected to cell balance control based on the voltage between the first voltage monitor terminal and the second voltage monitor terminal, and outputs a cell balance signal indicative of a detection result in question to the cell balance control terminal;

a first logical inversion circuit;

a first p-channel type transistor having a gate terminal receiving an output signal of the first logical inversion circuit, a drain terminal connected to the first transmitting terminal, and a source terminal connected to the internal positive side common power source wire;

a first current source having an input terminal connected to the first receiving terminal, and an output terminal connected to the internal negative side common power source wire;

a second logical inversion circuit having an input terminal connected to the first receiving terminal;

a first negative OR circuit that receives the overcharge detection signal and an output signal of the second logical inversion circuit, and outputs a negative OR signal of the overcharge detection signal and the output signal of the second logical inversion circuit to the first logical inversion circuit;

a third logical inversion circuit;

a second p-channel type transistor having a gate terminal receiving an output signal of the third logical inversion circuit, a drain terminal connected to the second transmitting terminal, and a source terminal connected to the internal positive side common power source wire;

a second current source having an input terminal connected to the second receiving terminal, and an output terminal connected to the internal negative side common power source wire;

a fourth logical inversion circuit having an input terminal connected to the second receiving terminal; and

a second negative OR circuit that receives the overdischarge detection signal and an output signal of the fourth logical inversion circuit, and outputs a negative OR signal of the overdischarge detection signal and the output signal of the fourth logical inversion circuit to the third logical inversion circuit;

a cell balance switch circuit that is connected in parallel with the each of the plurality of batteries, and switches between connection and disconnection of two terminals according to the cell balance signal that is output from the cell balance control terminal of the battery state monitoring circuit corresponding to the each of the plurality of batteries;

a first external terminal;

a second external terminal;

a charging n-channel type transistor;

a discharging n-channel type transistor;

a first bias resistive element having one end connected to a gate terminal of the charging n-channel type transistor,

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and another end connected to a source terminal of the charging n-channel type transistor;

a second bias resistive element having one end connected to a gate terminal of the discharging n-channel type transistor, and another end connected to a source terminal of the discharging n-channel type transistor; and

a diode having a cathode terminal connected to the gate terminal of the charging n-channel type transistor, wherein the battery state monitoring circuit has the first voltage monitor terminal connected to the positive terminal of a corresponding battery, respectively, the second voltage monitor terminal connected to the negative terminal of the corresponding battery, respectively, the first transmitting terminal connected to the first receiving terminal of one of the adjacent battery state monitoring circuits, the second transmitting terminal connected to the second receiving terminal of the one of the adjacent battery state monitoring circuits, the first receiving terminal connected to the first transmitting terminal of another one of the adjacent battery state monitoring circuits, and the second receiving terminal connected to the second transmitting terminal of the another one of the adjacent battery state monitoring circuits,

wherein the positive terminal of a battery at one end of the plurality of batteries that are connected in series is connected to the first external terminal,

wherein the first receiving terminal and the second receiving terminal of the battery state monitoring circuit corresponding to the battery at the one end are connected to the positive terminal of the battery at the one end,

wherein the battery state monitoring circuit corresponding to a battery at another end of the plurality of batteries that are connected in series has the first transmitting terminal connected to an anode terminal of the diode, and the second transmitting terminal connected to the gate terminal of the discharging n-channel type transistor, and wherein the discharging n-channel type transistor has the source terminal connected to the negative terminal of the battery at the another end, and a drain terminal connected to a drain terminal of the charging n-channel type transistor, and the source terminal of the charging n-channel type transistor is connected to the second external terminal.

15. A battery device according to claim **13**, wherein the battery state monitoring circuit further comprises:

a first clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the drain terminal of the first n-channel type transistor, and has a characteristic that allows a reverse current to flow in the first clamp diode when a reverse voltage corresponding to a voltage which exceeds a withstand voltage of the battery state monitoring circuit is applied to the first clamp diode;

a second clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the output terminal of the first current source;

a third clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the drain terminal of the second n-channel type transistor, and has a characteristic that allows the reverse current to flow in the third clamp diode when the reverse voltage corresponding to the voltage which exceeds the withstand voltage of the battery state monitoring circuit is applied to the third clamp diode; and

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a fourth clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the output terminal of the second current source,

wherein the battery state monitoring circuit has the first transmitting terminal connected to the first receiving terminal of one of the adjacent battery state monitoring circuits through a resistive element, the second transmitting terminal connected to the second receiving terminal of the one of the adjacent battery state monitoring circuits through the resistive element, the first receiving terminal connected to the first transmitting terminal of another one of the adjacent battery state monitoring circuits through the resistive element, and the second receiving terminal connected to the second transmitting terminal of the another one of the adjacent battery state monitoring circuits through the resistive element.

16. A battery device according to claim **14**, wherein the battery state monitoring circuit further comprises:

a first clamp diode that has an anode terminal connected to the drain terminal of the first p-channel type transistor, and a cathode terminal connected to the internal positive side common power source wire, and has a characteristic that allows a reverse current to flow in the first clamp diode when a reverse voltage corresponding to a voltage which exceeds a withstand voltage of the battery state monitoring circuit is applied to the first clamp diode;

a second clamp diode that has an anode terminal connected to the input terminal of the first current source, and a cathode terminal connected to the internal positive side common power source wire;

a third clamp diode that has an anode terminal connected to the drain terminal of the second p-channel type transistor, and a cathode terminal connected to the internal positive side common power source wire, and has a characteristic that allows the reverse current to flow in the third clamp diode when the reverse voltage corresponding to the voltage which exceeds the withstand voltage of the battery state monitoring circuit is applied to the third clamp diode; and

a fourth clamp diode that has an anode terminal connected to the input terminal of the second current source, and a cathode terminal connected to the internal positive side common power source wire,

wherein the battery state monitoring circuit has the first transmitting terminal connected to the first receiving terminal of one of the adjacent battery state monitoring circuits through a resistive element, the second transmitting terminal connected to the second receiving terminal of the one of the adjacent battery state monitoring circuits through the resistive element, the first receiving terminal connected to the first transmitting terminal of another one of the adjacent battery state monitoring circuits through the resistive element, and the second receiving terminal connected to the second transmitting terminal of the another one of the adjacent battery state monitoring circuits through the resistive element.

17. A battery device according to claim **13**, wherein the battery state monitoring circuit further comprises:

a first clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the drain terminal of

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the first n-channel type transistor, and has a characteristic that allows a reverse current to flow in the first clamp diode when a reverse voltage corresponding to a voltage which exceeds a withstand voltage of the battery state monitoring circuit is applied to the first clamp diode;

a second clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the output terminal of the first current source;

a third clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the drain terminal of the second n-channel type transistor, and has a characteristic that allows the reverse current to flow in the third clamp diode when the reverse voltage corresponding to the voltage which exceeds the withstand voltage of the battery state monitoring circuit is applied to the third clamp diode;

a fourth clamp diode that has an anode terminal connected to the internal negative side common power source wire, and a cathode terminal connected to the output terminal of the second current source;

a first resistive element that is connected between the cathode terminal of the second clamp diode and the first receiving terminal; and

a second resistive element that is connected between the cathode terminal of the fourth clamp diode and the second receiving terminal.

18. A battery device according to claim **14**, wherein the battery state monitoring circuit further comprises:

a first clamp diode that has an anode terminal connected to the drain terminal of the first p-channel type transistor, and a cathode terminal connected to the internal positive side common power source wire, and has a characteristic that allows a reverse current to flow in the first clamp diode when a reverse voltage corresponding to a voltage which exceeds a withstand voltage of the battery state monitoring circuit is applied to the first clamp diode;

a second clamp diode that has an anode terminal connected to the input terminal of the first current source, and a cathode terminal connected to the internal positive side common power source wire;

a third clamp diode that has an anode terminal connected to the drain terminal of the second p-channel type transistor, and a cathode terminal connected to the internal positive side common power source wire, and has a characteristic that allows the reverse current to flow in the third clamp diode when the reverse voltage corresponding to the voltage which exceeds the withstand voltage of the battery state monitoring circuit is applied to the third clamp diode;

a fourth clamp diode that has an anode terminal connected to the input terminal of the second current source, and a cathode terminal connected to the internal positive side common power source wire;

a first resistive element that is connected between the anode terminal of the first clamp diode and the first transmitting terminal; and

a second resistive element that is connected between the anode terminal of the third clamp diode and the second transmitting terminal.

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