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Rofougaran

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(54) **WIDE BANDWIDTH TRANSCEIVER**

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U.S.C. 154(b) by 25 days.

(57) **ABSTRACT**

(21) Appl. No.: **11/504,911**

The wide bandwidth transceiver includes a receiver section, a transmitter section, and a local oscillation module. The local oscillation module generates a first and a second local oscillation. The transmitter section converts an outbound baseband signal and/or a low intermediate frequency (IF) signal into a first outbound radio frequency (RF) signal based on the second local oscillation when the wide bandwidth transceiver is in a second wireless standard mode and converts the outbound baseband and/or the low IF signal into a second outbound RF signal based on the first and second local oscillations when the wide bandwidth transceiver is in a first wireless standard mode. The receiver section converts a first inbound RF signal into an inbound low IF signal and/or a baseband signal based on the first and second local oscillations when the wide bandwidth transceiver is in the first wireless standard mode and converts a second inbound RF signal into the inbound low IF signal and/or the baseband signal based on the second local oscillation when the wide bandwidth transceiver is in the second wireless standard mode.

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H03D 5/00 (2006.01)

(52) **U.S. Cl.** **455/168.1**; 455/142; 455/133;
455/150.1; 455/552.1

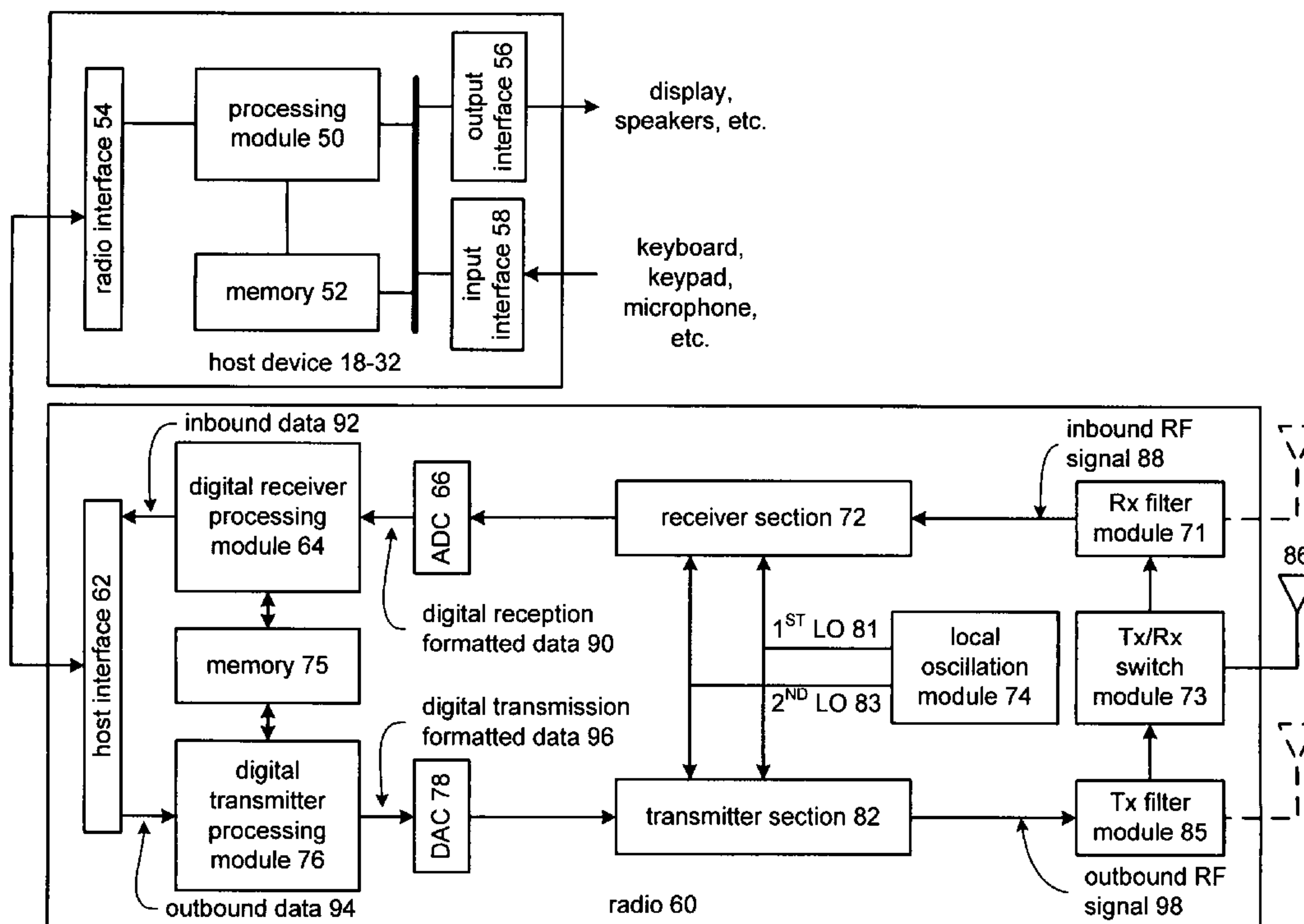
(58) **Field of Classification Search** 455/168.1,
455/142, 133, 150.1, 552.1, 73, 75, 78, 41.2
See application file for complete search history.

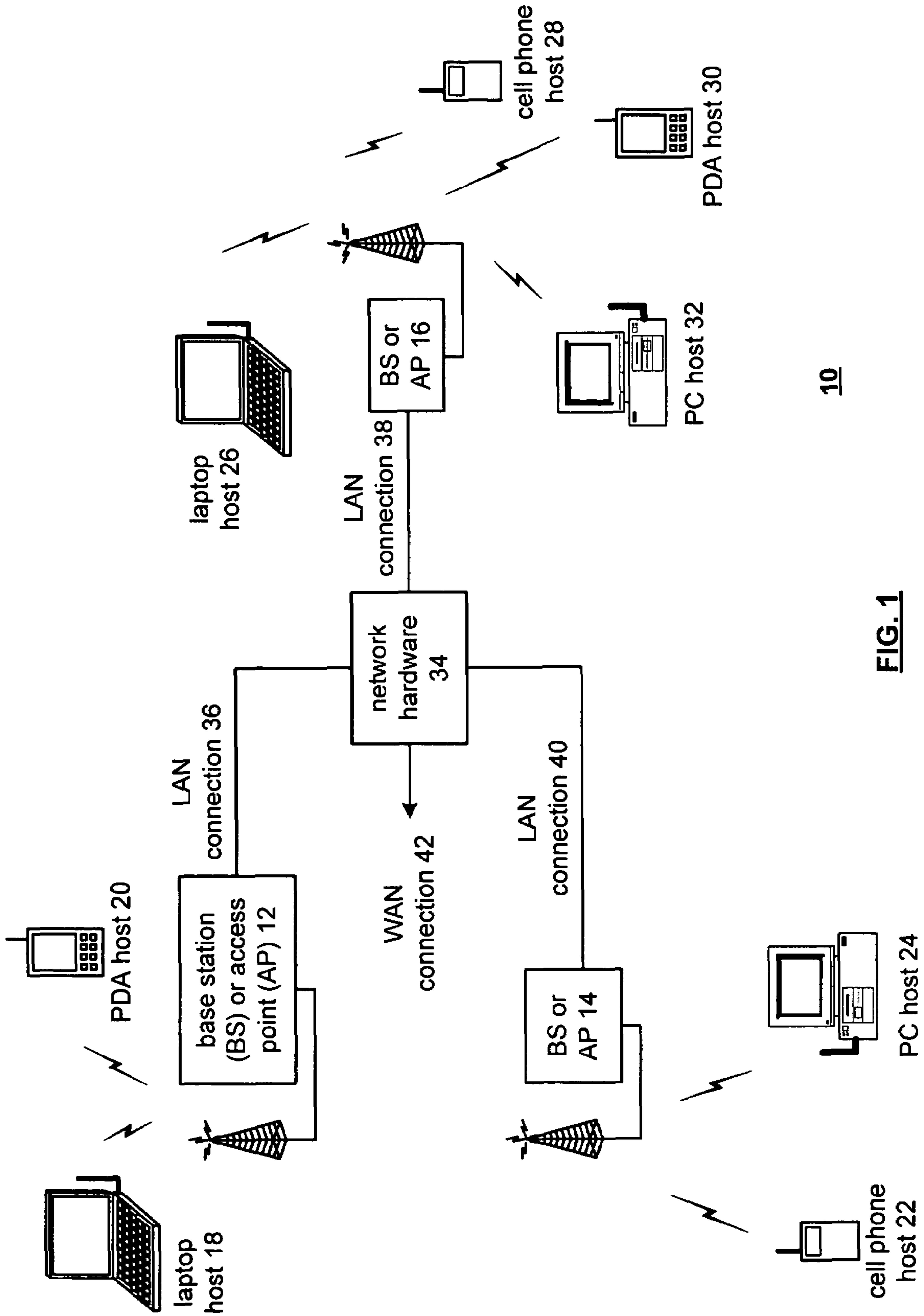
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5 Claims, 7 Drawing Sheets





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FIG. 1

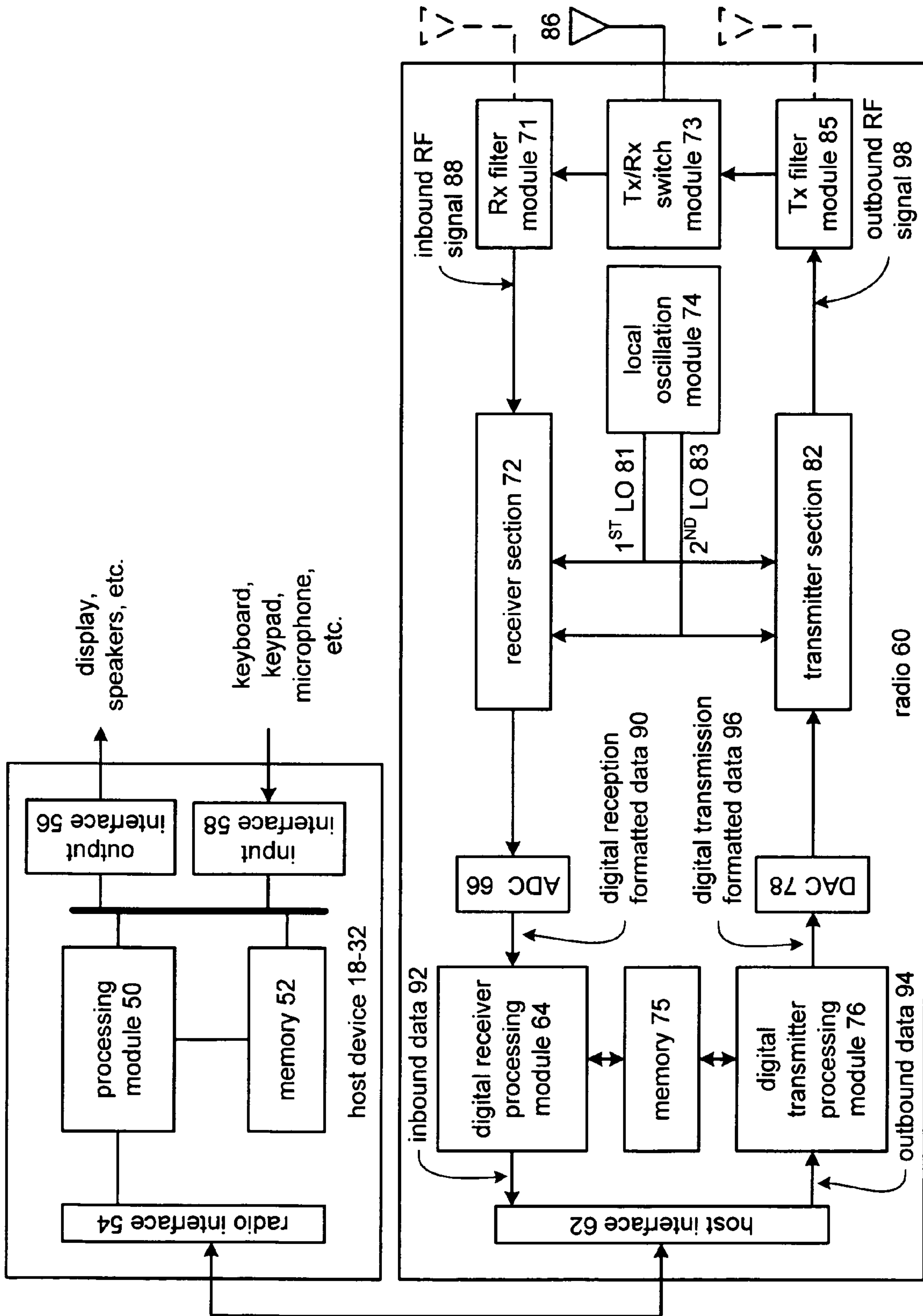


FIG. 2

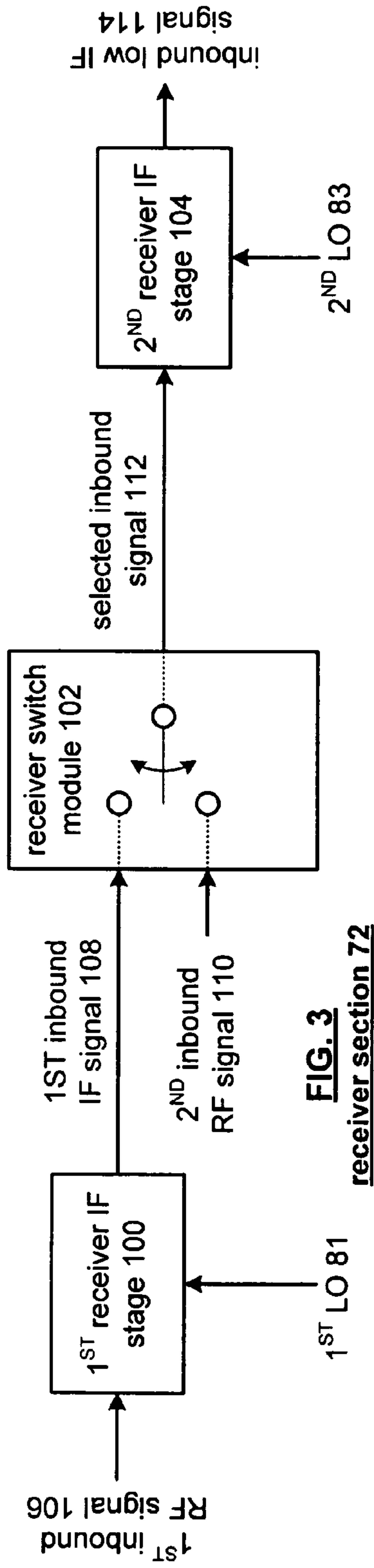


FIG. 3
receiver section 72

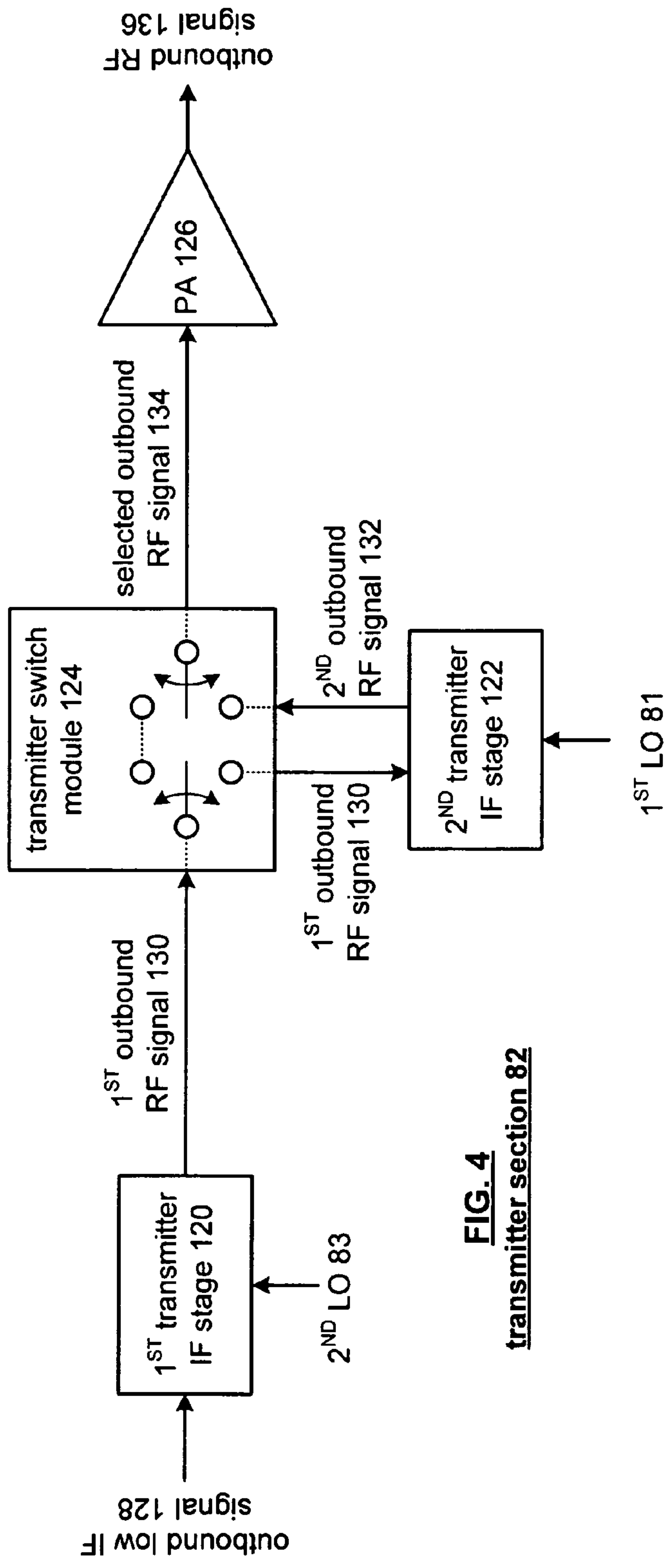


FIG. 4
transmitter section 82

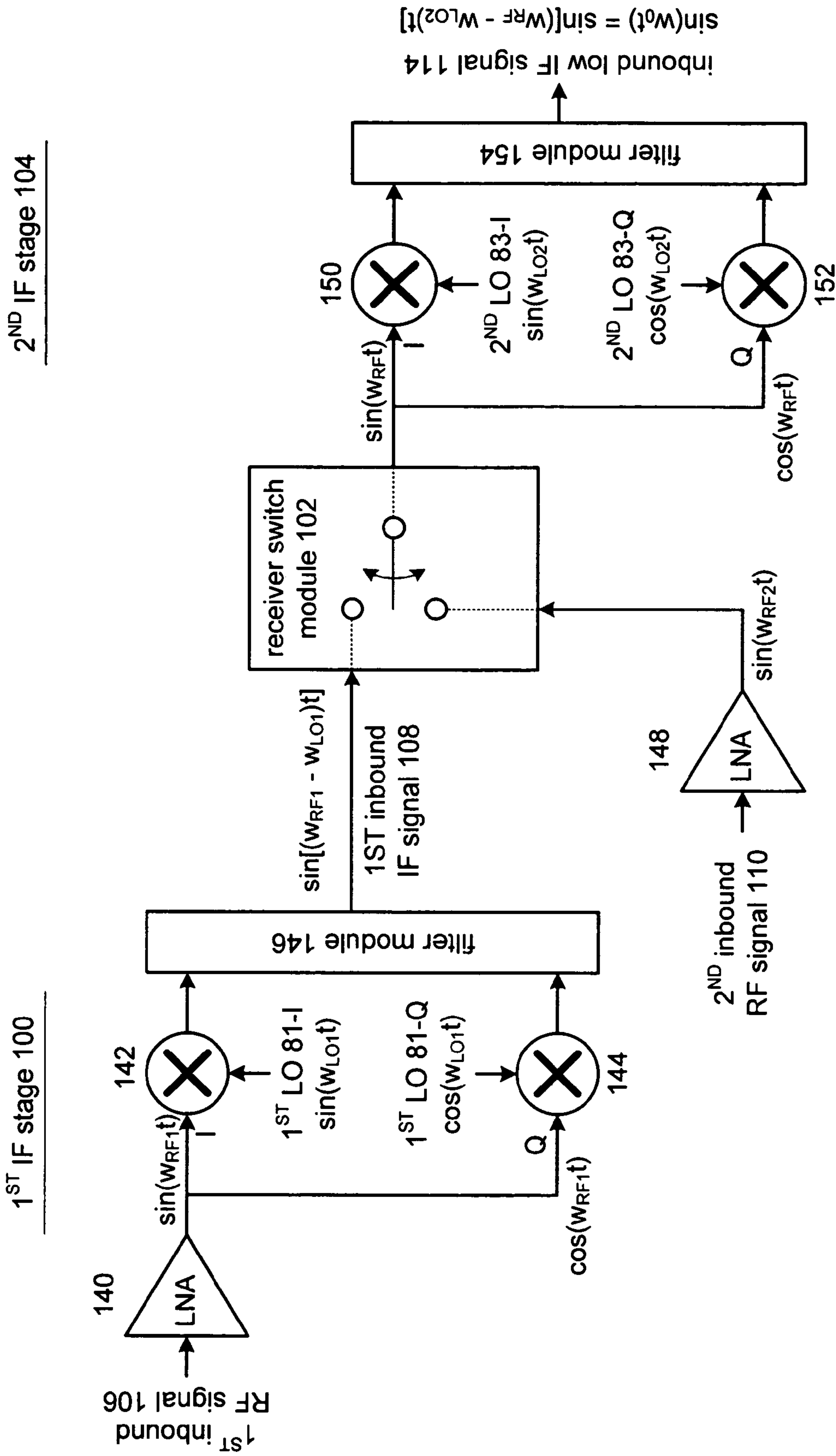


FIG. 5
receiver section 72

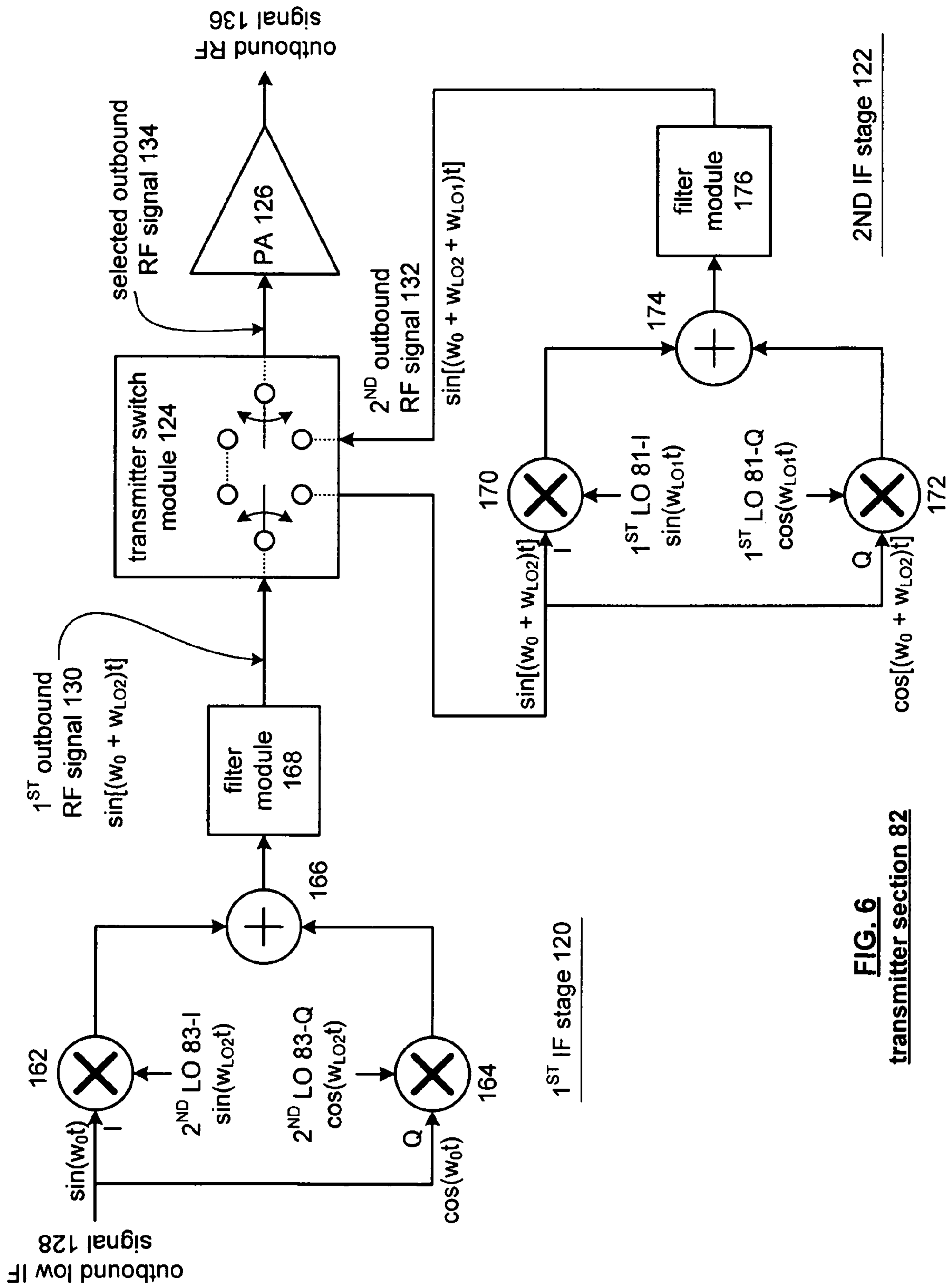


FIG. 6
transmitter section 82

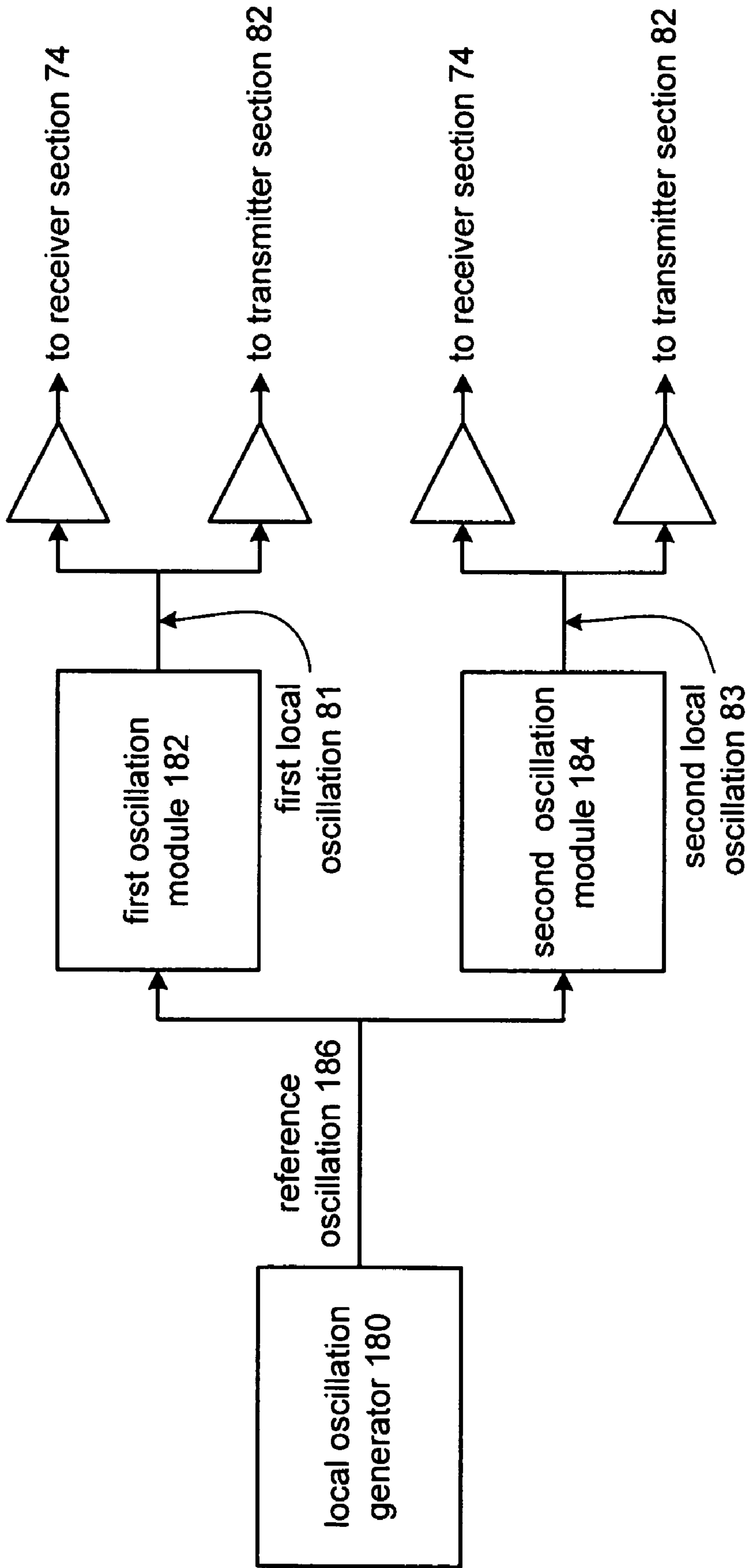


FIG. 7
local oscillation module 74

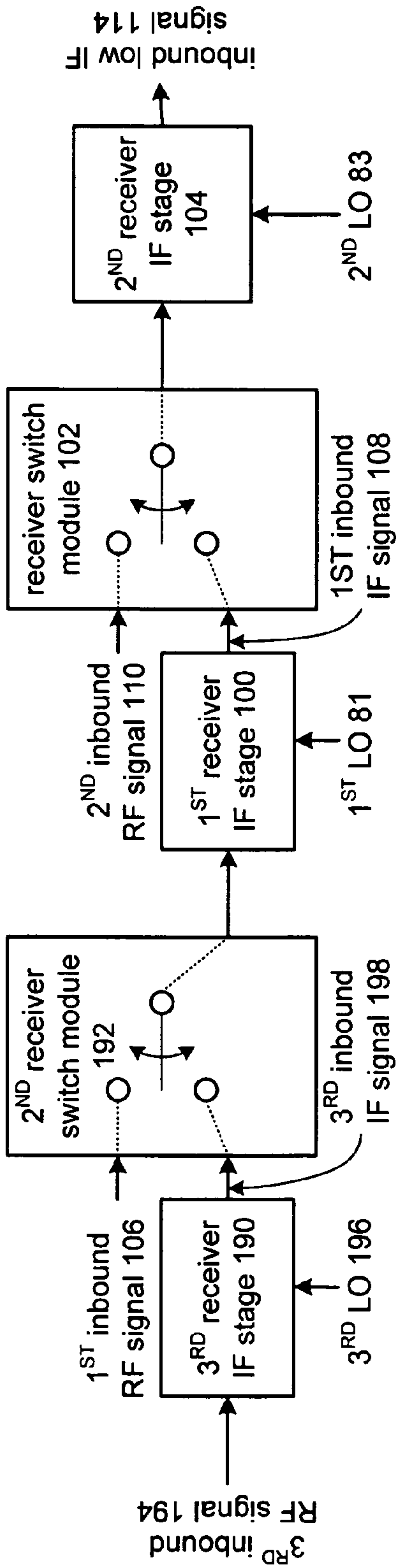


FIG. 8
receiver section 72

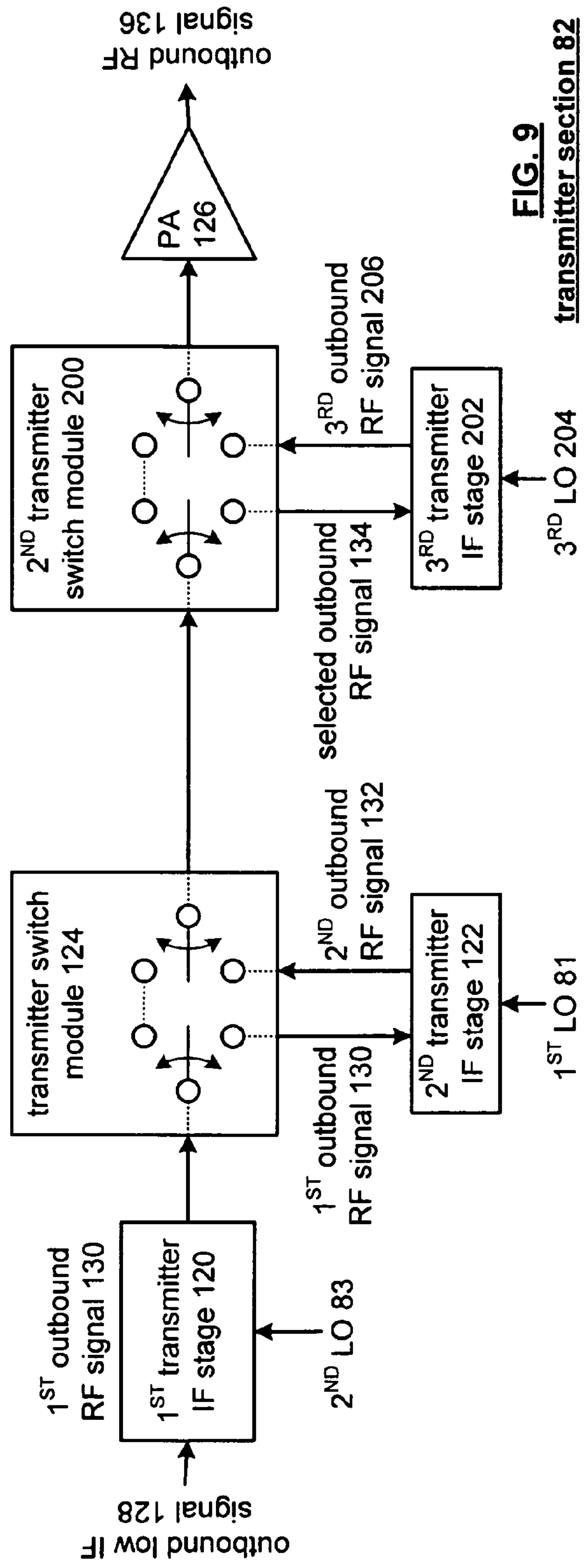


FIG. 9
transmitter section 82

WIDE BANDWIDTH TRANSCEIVER

This patent application is claiming priority under 35 USC § 120 as a continuing patent application of co-pending patent application entitled WIDE BANDWIDTH TRANSCEIVER, having a filing date of Nov. 27, 2002, and a Ser. No. 10/306,047.

BACKGROUND OF THE INVENTION**1. Technical Field of the Invention**

This invention relates generally to wireless communication systems and more particularly to transceivers used within such wireless communication systems.

2. Description of Related Art

Communication systems are known to support wireless and wire lined communications between wireless and/or wire lined communication devices. Such communication systems range from national and/or international cellular telephone systems to the Internet to point-to-point in-home wireless networks. Each type of communication system is constructed, and hence operates, in accordance with one or more communication standards. For instance, wireless communication systems may operate in accordance with one or more standards including, but not limited to, IEEE 802.11, Bluetooth, advanced mobile phone services (AMPS), digital AMPS, global system for mobile communications (GSM), code division multiple access (CDMA), local multi-point distribution systems (LMDS), multi-channel-multi-point distribution systems (MMDS), and/or variations thereof.

Depending on the type of wireless communication system, a wireless communication device, such as a cellular telephone, two-way radio, personal digital assistant (PDA), personal computer (PC), laptop computer, home entertainment equipment, et cetera communicates directly or indirectly with other wireless communication devices. For direct communications (also known as point-to-point communications), the participating wireless communication devices tune their receivers and transmitters to the same channel or channels (e.g., one of the plurality of radio frequency (RF) carriers of the wireless communication system) and communicate over that channel(s). For indirect wireless communications, each wireless communication device communicates directly with an associated base station (e.g., for cellular services) and/or an associated access point (e.g., for an in-home or in-building wireless network) via an assigned channel. To complete a communication connection between the wireless communication devices, the associated base stations and/or associated access points communicate with each other directly, via a system controller, via the public switch telephone network, via the Internet, and/or via some other wide area network.

For each wireless communication device to participate in wireless communications, it includes a built-in radio transceiver (i.e., receiver and transmitter) or is coupled to an associated radio transceiver (e.g., a station for in-home and/or in-building wireless communication networks, RF modem, etc.). As is known, the receiver is coupled to the antenna and includes a low noise amplifier, one or more intermediate frequency stages, a filtering stage, and a data recovery stage. The low noise amplifier receives inbound RF signals via the antenna and amplifies them. The one or more intermediate frequency stages mix the amplified RF signals with one or more local oscillations to convert the amplified RF signal into baseband signals or intermediate frequency (IF) signals. The filtering stage filters the baseband signals or the IF signals to attenuate unwanted out of band signals to produce filtered

signals. The data recovery stage recovers raw data from the filtered signals in accordance with the particular wireless communication standard.

As is also known, the transmitter includes a data modulation stage, one or more intermediate frequency stages, and a power amplifier. The data modulation stage converts raw data into baseband signals in accordance with a particular wireless communication standard. The one or more intermediate frequency stages mix the baseband signals with one or more local oscillations to produce RF signals. The power amplifier amplifies the RF signals prior to transmission via an antenna.

As is further known, the many standards that govern wireless communication systems provide different operating frequency ranges. For example, IEEE802.11a operates in the 5.25 gigahertz and 5.75 gigahertz frequency ranges, IEEE802.11b and Bluetooth operate in the 2.4 gigahertz frequency range, and GSM operates in the 900 megahertz frequency range. Accordingly, the analog transmitter and receiver portions (e.g., the portions of a radio that convert between analog baseband signals and RF signals) are implemented differently for each different frequency range of the various standards. As such, if the analog transmitter and receiver portions are to be implemented on an integrated circuit, an integrated circuit manufacturer needs to produce separate integrated circuits for each different standard. Integrated circuit manufacturers are acutely aware of the added costs of developing, manufacturing, and supporting multiple integrated circuits of related technology.

Therefore, a need exists for a wide bandwidth transceiver that operates over a wide range of frequencies such that a single transceiver may support multiple wireless communication standards.

BRIEF SUMMARY OF THE INVENTION

The present invention is directed to apparatus and methods of operation that are further described in the following Brief Description of the Drawings, the Detailed Description of the Invention, and the claims. Other features and advantages of the present invention will become apparent from the following detailed description of the invention made with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

FIG. 1 is a schematic block diagram of a wireless communication system in accordance with the present invention;

FIG. 2 is a schematic block diagram of a wireless communication device in accordance with the present invention;

FIG. 3 is a schematic block diagram of a receiver section in accordance with the present invention;

FIG. 4 is a schematic block diagram of a transmitter section in accordance with the present invention;

FIG. 5 is a schematic block diagram of an alternate receiver section in accordance with the present invention;

FIG. 6 is a schematic block diagram of an alternate transmitter section in accordance with the present invention;

FIG. 7 is a schematic block diagram of a local oscillation module in accordance with the present invention;

FIG. 8 is a schematic block diagram of another embodiment of a receiver section in accordance with the present invention; and

FIG. 9 is a schematic block diagram of another embodiment of a transmitter section in accordance with the present invention.

DETAILED DESCRIPTION OF THE INVENTION

FIG. 1 is a schematic block diagram illustrating a communication system 10 that includes a plurality of base stations and/or access points 12-16, a plurality of wireless communication devices 18-32 and a network hardware component 34. The wireless communication devices 18-32 may be laptop host computers 18 and 26, personal digital assistant hosts 20 and 30, personal computer hosts 24 and 32 and/or cellular telephone hosts 22 and 28. The details of the wireless communication devices will be described in greater detail with reference to FIG. 2.

The base stations or access points 12-16 are operably coupled to the network hardware 34 via local area network connections 36, 38 and 40. The network hardware 34, which may be a router, switch, bridge, modem, system controller, et cetera provides a wide area network connection 42 for the communication system 10. Each of the base stations or access points 12-16 has an associated antenna or antenna array to communicate with the wireless communication devices in its area. Typically, the wireless communication devices register with a particular base station or access point 12-14 to receive services from the communication system 10. For direct connections (i.e., point-to-point communications), wireless communication devices communicate directly via an allocated channel.

Typically, base stations are used for cellular telephone systems and like-type systems, while access points are used for in-home or in-building wireless networks. Regardless of the particular type of communication system, each wireless communication device includes a built-in radio and/or is coupled to a radio. The radio includes a highly linear amplifier and/or programmable multi-stage amplifier as disclosed herein to enhance performance, reduce costs, reduce size, and/or enhance broadband applications.

FIG. 2 is a schematic block diagram illustrating a wireless communication device that includes the host device 18-32 and an associated radio 60. For cellular telephone hosts, the radio 60 is a built-in component. For personal digital assistants hosts, laptop hosts, and/or personal computer hosts, the radio 60 may be built-in or an externally coupled component.

As illustrated, the host device 18-32 includes a processing module 50, memory 52, radio interface 54, input interface 58 and output interface 56. The processing module 50 and memory 52 execute the corresponding instructions that are typically done by the host device. For example, for a cellular telephone host device, the processing module 50 performs the corresponding communication functions in accordance with a particular cellular telephone standard.

The radio interface 54 allows data to be received from and sent to the radio 60. For data received from the radio 60 (e.g., inbound data), the radio interface 54 provides the data to the processing module 50 for further processing and/or routing to the output interface 56. The output interface 56 provides connectivity to an output display device such as a display, monitor, speakers, et cetera such that the received data may be displayed. The radio interface 54 also provides data from the processing module 50 to the radio 60. The processing module 50 may receive the outbound data from an input device such as a keyboard, keypad, microphone, et cetera via the input interface 58 or generate the data itself. For data received via the input interface 58, the processing module 50 may perform a corresponding host function on the data and/or route it to the radio 60 via the radio interface 54.

Radio 60 includes a host interface 62, digital receiver processing module 64, an analog-to-digital converter 66, a receiver section 72, a receiver filter module 71, a transmitter/

receiver switch 73, a local oscillation module 74, memory 75, a digital transmitter processing module 76, a digital-to-analog converter 78, a transmitter section 82, a transmitter filter module 85, and an antenna 86. The antenna 86 may be a single antenna that is shared by the transmit and receive paths as regulated by the Tx/Rx switch 73, or may include separate antennas for the transmit path and receive path. The antenna implementation will depend on the particular standard to which the wireless communication device is compliant.

The digital receiver processing module 64 and the digital transmitter processing module 76, in combination with operational instructions stored in memory 75, execute digital receiver functions and digital transmitter functions, respectively. The digital receiver functions include, but are not limited to, digital intermediate frequency to baseband conversion, demodulation, constellation demapping, decoding, and/or descrambling. The digital transmitter functions include, but are not limited to, scrambling, encoding, constellation mapping, modulation, and/or digital baseband to IF conversion. The digital receiver and transmitter processing modules 64 and 76 may be implemented using a shared processing device, individual processing devices, or a plurality of processing devices. Such a processing device may be a micro-processor, micro-controller, digital signal processor, micro-computer, central processing unit, field programmable gate array, programmable logic device, state machine, logic circuitry, analog circuitry, digital circuitry, and/or any device that manipulates signals (analog and/or digital) based on operational instructions. The memory 75 may be a single memory device or a plurality of memory devices. Such a memory device may be a read-only memory, random access memory, volatile memory, non-volatile memory, static memory, dynamic memory, flash memory, and/or any device that stores digital information. Note that when the processing module 64 and/or 76 implements one or more of its functions via a state machine, analog circuitry, digital circuitry, and/or logic circuitry, the memory storing the corresponding operational instructions is embedded with the circuitry comprising the state machine, analog circuitry, digital circuitry, and/or logic circuitry.

In operation, the radio 60 receives outbound data 94 from the host device via the host interface 62. The host interface 62 routes the outbound data 94 to the digital transmitter processing module 76, which processes the outbound data 94 in accordance with a particular wireless communication standard (e.g., IEEE802.11a, IEEE 802.11b, Bluetooth, et cetera) to produce digital transmission formatted data 96. The digital transmission formatted data 96 will be a digital base-band signal or a digital low IF signal, where the low IF typically will be in the frequency range of one hundred kilohertz to a few megahertz.

The digital-to-analog converter 78 converts the digital transmission formatted data 96 from the digital domain to the analog domain. The transmitter section 82 converts the analog baseband or low IF signal into an outbound RF signal 98 based on a first and/or second local oscillation 81 and/or 83 provided by local oscillation module 74. The transmitter filter module 85, which may be a high frequency bandpass filter, filters the outbound RF signal 98 and provides the filtered RF signal to the Tx/Rx switch module 73 for subsequent transmission by the antenna 86 to a targeted device such as a base station, an access point and/or another wireless communication device.

The radio 60 also receives an inbound RF signal 88 via the antenna 86, which may have been transmitted by a base station, an access point, or another wireless communication device. The antenna 86 provides the inbound RF signal 88 to

5

the receiver filter module **71** via the Tx/Rx switch **73**, where the Rx filter **71**, which may be a high frequency bandpass filter, filters the inbound RF signal **88**. The Rx filter **71** provides the filtered RF signal to receiver section **72**, which converts the amplified inbound RF signal into an inbound low IF signal or baseband signal based on the first and/or second oscillation **81** and/or **83** provided by local oscillation module **74**. The receiver section **72** provides the inbound low IF signal or baseband signal to the ADC **66**.

The analog-to-digital converter **66** converts the filtered inbound low IF signal from the analog domain to the digital domain to produce digital reception formatted data **90**. The digital receiver processing module **64** decodes, descrambles, demaps, and/or demodulates the digital reception formatted data **90** to recapture inbound data **92** in accordance with the particular wireless communication standard being implemented by radio **60**. The host interface **62** provides the recaptured inbound data **92** to the host device **18-32** via the radio interface **54**.

As one of average skill in the art will appreciate, the wireless communication device of FIG. **2** may be implemented using one or more integrated circuits. For example, the host device may be implemented on one integrated circuit, the digital receiver processing module **64**, the digital transmitter processing module **76** and memory **75** may be implemented on a second integrated circuit, and the remaining components of the radio **60**, less the antenna **86**, may be implemented on a third integrated circuit. As an alternate example, the radio **60** may be implemented on a single integrated circuit. As yet another example, the processing module **50** of the host device and the digital receiver and transmitter processing modules **64** and **76** may be a common processing device implemented on a single integrated circuit. Further, the memory **52** and memory **75** may be implemented on a single integrated circuit and/or on the same integrated circuit as the common processing modules of processing module **50** and the digital receiver and transmitter processing module **64** and **76**.

FIG. **3** is a schematic block diagram of receiver section **72** that may be configured in one of two modes. As shown, the receiver section **72** includes a 1st receiver intermediate frequency (IF) stage **100**, a receiver switch module **102**, and a 2nd receiver IF stage **104**. In a 1st configuration of the receiver section **72**, the receiver section **72** receives a 1st inbound RF signal **106** via the 1st receiver IF stage **100**. The 1st receiver IF stage **100** converts the 1st inbound RF signal **106** into a 1st inbound IF signal **108** based on the 1st local oscillation **81**. For example, if the 1st inbound RF signal **106** corresponds to an IEEE802.11a signal, which has a carrier frequency of 5.25 gigahertz, the 1st local oscillation **81** may have a frequency of 2.85 gigahertz. Accordingly, the 1st inbound IF signal **108** has a carrier frequency of 2.4 gigahertz (e.g., 5.25 GHz-2.85 GHz). For this example, the frequency of the first local oscillation was selected such that the resulting 1st inbound IF signal has a carrier frequency of 2.4 GHz, which substantially equals the carrier frequency of Bluetooth based signals and/or IEEE802.11b signals. Accordingly, for this example, the receiver section **72** may be configured to process IEEE802.11a signals or Bluetooth/IEEE802.11b signals.

As an alternative example, the 1st local oscillation **81** may have a frequency of 4.35 gigahertz such that the 1st inbound IF signal **108** has a carrier frequency of 900 megahertz. In this example, the receiver section **72** would be configurable to process 1st inbound RF signal **106** that are compliant with IEEE802.11a, which has a carrier frequency of 5.25 gigahertz, or configured to process 2nd inbound RF signals **110** that are compliant with GSM, which has a carrier frequency of 900 megahertz.

6

As yet another alternate example, the 1st local oscillation **81** may have a frequency of 1.5 gigahertz and the 1st inbound RF signal **106** may have a carrier frequency of 2.4 gigahertz in accordance with 802.11b and/or Bluetooth. The resulting 1st inbound IF signal has a carrier frequency of 900 megahertz. According to this example, the receiver section **72** may be configured to process 1st inbound RF signals **106** that are compliant with 802.11b and/or Bluetooth or configured to process 2nd inbound RF signals **110** that are compliant with GSM or other standard that utilizes 900 megahertz transmissions.

Continuing with the 1st configuration of the receiver section **72**, the receiver switch module **102**, which may be a high frequency multiplexor, switching network, and/or tri-state input buffering network, couples the 1st inbound IF signal **108** to the 2nd receiver IF stage **104**. The 2nd receiver IF stage **104** converts the 1st inbound IF signal **108** into an inbound low IF signal **114** based on the 2nd local oscillation **83**. The inbound low IF signal **114** may have a carrier frequency in the range from baseband to a few megahertz. Continuing with the preceding examples, if the 1st inbound RF signal **106** has a carrier frequency of 5.25 gigahertz, the 1st local oscillation **81** has a frequency of 2.85 gigahertz such that the 1st inbound IF signal has a carrier frequency of 2.4 gigahertz, the 2nd local oscillation **83** may have a frequency of approximately 2.4 gigahertz such that the resulting inbound low IF signal has a zero to a few megahertz carrier frequency. In the 2nd example, if the 1st inbound RF signal has a 5.25 gigahertz carrier frequency and the 1st local oscillation **81** has a frequency of 4.35 gigahertz such that the 1st inbound IF signal **108** has a carrier frequency of 900 megahertz, the 2nd local oscillation **83** may have a frequency of approximately 900 megahertz. In the 3rd example, if the 1st inbound RF signal **106** has a carrier frequency of 2.4 gigahertz, the 1st local oscillation **81** may have a frequency of 1.5 gigahertz such that the 1st inbound IF signal **108** has a carrier frequency of 900 megahertz and the 2nd local oscillation **83** will have a frequency of 900 megahertz.

In a 2nd configuration of receiver section **72**, the receiver is coupled to receive the 2nd inbound RF signal **110**. In this configuration, the receiver switch module **102** passes the 2nd inbound RF signal **110** to the 2nd receiver IF stage **104**. The 2nd receiver IF stage **104** converts the 2nd inbound RF signal **110** into the inbound low IF signal **114** based on the 2nd local oscillation **83**. In this configuration, the 1st receiver IF stage **100** and the 1st local oscillation **81** may be disabled.

In general, for a dual mode receiver in accordance with the present invention, the 2nd inbound RF signal **110** corresponds to the mode having the lower carrier frequency, which for the preceding examples was either 2.4 gigahertz (GHz) or 900 megahertz and the 1st inbound RF signal **106** corresponds to the mode having the higher carrier frequency, which for the preceding examples was either 5.25 GHz or 2.4 GHz.

FIG. **4** is a schematic block diagram of transmitter section **82** that can be configured in one of two modes. The transmitter section **82** includes a 1st transmitter IF stage **120**, a transmitter switch module **124**, a 2nd transmitter IF stage **122**, and a power amplifier **126**. In a 1st mode, the transmitter section is operably coupled to convert an outbound low IF signal **128**, which has a carrier frequency in the range of baseband to a few megahertz, into an outbound RF signal **136** having a specified carrier frequency. For example, the outbound RF signal **136** may have a carrier frequency of 900 megahertz, 2.4 megahertz, or 5.25 megahertz. If the transmitter section **82** is to convert the low IF signal **128** into an output RF signal **136** having a 5.25 gigahertz carrier frequency, the transmitter switch module **124** is configured such that the outbound low IF signal **128** is up converted by both the 1st and 2nd transmit-

ter IF stages **120** and **122**. As one of average skill in the art will appreciate, the configuration of the transmitter section **82** corresponds to the configuration of the receiver section **72**. As such, if the receiver section is configured to receive 5.25 gigahertz carrier frequency signals, the transmitter section is configured to output radio frequency signals having a carrier frequency of 5.25 gigahertz.

In a 1st configuration of the transmitter section **82**, the transmitter switch module **124**, which may be a multiplexer, high frequency switching network, or tri-state buffering network, provides the 1st outbound RF signal **130** to the 2nd transmitter IF stage **122** and provides the output of the 2nd transmitter IF stage **122** to the power amplifier **126**. In a 2nd configuration of the transmitter section **82**, the transmitter switch module **124** bypasses the 2nd transmitter IF stage **122** and passes the 1st outbound RF signal **130** to the power amplifier **126**. Similarly to the receiver section **72**, the transmitter section **82** may have multiple configurations to provide multiple modes of operation.

As with the examples provided for the receiver section **72**, the transmitter section **82** may have a dual mode of up converting low IF signals to 900 megahertz and 2.4 gigahertz, to 2.4 gigahertz and 5.25 gigahertz, or to 900 megahertz and 5.25 gigahertz. For instance, if the transmitter section **82** is to up convert the outbound low IF signal **128** to 2.4 GHz or to 5.25 GHz, the first local oscillation would be 2.85 GHz and the second local oscillation would be 2.4 GHz. Thus, in the first mode, the 1st transmitter IF stage **120** up-converts the outbound low IF signal into the 1st outbound RF signal **130** having a carrier frequency of 2.4 GHz. The transmitter switching module **124** provides the 1st outbound RF signal **130** to the 2nd transmitter IF stage **122**. The 2nd transmitter IF stage **122** up-converts the 1st outbound RF signal **130** to the 2nd outbound RF signal **132** based on the 1st local oscillation **81**, which has a frequency of 2.85 GHz. As such, the 2nd outbound RF signal **132** has a carrier frequency of 5.35 GHz. In the 2nd configuration, the transmitter switch module **124** passes the 1st outbound RF signal **130** to the power amplifier **126**. In this mode, the resulting outbound RF signal **136** has a carrier frequency of 2.4 GHz.

FIG. **5** is a schematic block diagram of an alternate receiver section **72**. The receiver section **72** includes the 1st IF stage **100**, the receiver switch module **102**, and the 2nd IF stage **104**. The 1st IF stage **100** includes a low noise amplifier **140**, 1st and 2nd mixers **142** and **144**, and a filter module **146**. The 2nd IF stage **104** includes 1st and 2nd mixers **150** and **152** and filter module **154**. The receiver section **72** also includes a low noise amplifier **148**.

In a first mode of the receiver section **72**, the 1st IF stage **100** receives the 1st inbound IF signal **106** and amplifies it via the low noise amplifier **140**. The low noise amplifier **140** outputs an in-phase component and a quadrature component of the RF signal **106**. The in-phase component (I), which may be represented by $\sin(\omega_{RF1}t)$, is mixed via mixer **142** with an in-phase component of the 1st local oscillation **81**, which may be represented by $\sin(\omega_{LO1}t)$. The 2nd mixer **144** mixes the quadrature component (Q) of the RF signal, which may be represented by $\cos(\omega_{RF1}t)$, with the quadrature component of the 1st local oscillation **81**, which may be represented by $\cos(\omega_{LO1}t)$. The resulting mixed signals are then filtered by filter module **146**, which may be a bandpass filter, to produce the 1st inbound IF signal **108**, which may be represented by $\sin[(\omega_{RF1}-\omega_{LO1})t]$.

The receiver switch module **102** provides the 1st inbound IF signal **108** to the 2nd IF stage **104**. The 1st mixer **150** of the 2nd IF stage **104** mixes the in-phase component, e.g., $\sin(\omega_{RF1}t)$, of the 1st inbound IF signal **108** with the in-phase component,

e.g., $\sin(\omega_{LO2}t)$, of the 2nd local oscillation **83-I** to produce a first mixed signal. Note that, for this mode, ω_{RF} equals $\omega_{RF1}-\omega_{LO1}$. The 2nd mixer **152** of the 2nd IF stage **104** mixes the quadrature component of the 1st inbound IF signal **108**, e.g., $\cos(\omega_{RF1}t)$, with the in-phase component of the 2nd local oscillation i.e., $\cos(\omega_{LO2}t)$, to produce a second mixed signal. The first and second mixed signals are filtered via filter module **154**, which may be a bandpass filter, to produce the inbound low IF signal **114**, e.g., $\sin(\omega_0t)=\sin[(\omega_{RF}-\omega_{LO2})t]$.

In a second mode of the receiver section **72**, the receiver section **72** receives the 2nd inbound RF signal **110**, e.g., $\sin(\omega_{RF2}t)$, via the low noise amplifier **148**. In this mode, the receiver switch module **102** passes the output of low noise amplifier **148** to the mixers **150** and **152** of the 2nd IF stage **104**. The 1st mixer **150** mixes the in-phase component, e.g., $\sin(\omega_{RF2}t)$, of the 2nd inbound RF signal **110** with the in-phase component, e.g., $\sin(\omega_{LO2}t)$, of the 2nd local oscillation **83-I** to produce a first mixed signal. Note that, for this mode, ω_{RF} equals ω_{RF2} . The 2nd mixer **152** mixes the quadrature component of the 2nd inbound RF signal **110**, e.g., $\cos(\omega_{RF2}t)$, with the in-phase component of the 2nd local oscillation i.e., $\cos(\omega_{LO2}t)$, to produce a second mixed signal. The first and second mixed signals are filtered via filter module **154** to produce the inbound low IF signal **114**, e.g., $\sin(\omega_0t)=\sin[(\omega_{RF}-\omega_{LO2})t]$.

FIG. **6** is a schematic block diagram of an alternate transmitter section **82** that includes the 1st IF stage **120**, the transmitter switch **124**, the 2nd IF stage **122** and the power amplifier **126**. In this embodiment, the 1st IF stage **120** includes 1st and 2nd mixers **162** and **164**, a summation module **166**, and a filter module **168**. The 2nd IF stage **122** includes 1st and 2nd mixers **172**, summation module **174** and filter module **176**. When the transmitter section **82** is configured to up convert the outbound low IF signal **128** to the higher frequency range mode of operation, the transmitter switch module **124** couples the output of the 1st IF stage **120** to the 2nd IF stage **122** such that the outbound low IF signal **128** is up converted by the 1st and 2nd IF stages **120** and **122**. The 1st IF stage **120** up converts the outbound low IF signal **128** by mixing the in-phase component thereof, e.g., $\sin(\omega_0t)$, with the in-phase component of the 2nd local oscillation **83**, e.g., $\sin(\omega_{LO2}t)$ and by mixing the quadrature component thereof, e.g., $\cos(\omega_0t)$, with the quadrature component of the 2nd local oscillation **83**, e.g., $\cos(\omega_{LO2}t)$. The resulting mixed signals are summed via summation module **166** and then filtered via filter module **168**. The filter module **168**, which may be a bandpass filter, outputs the 1st outbound RF signal **130**, which may be represented by $\sin[(\omega_0+\omega_{LO2})t]$.

The transmit switch module **124** provides the 1st outbound RF signal **130** to the 2nd IF stage **122**. Mixing module **170** mixes the in-phase component of the 1st outbound RF signal **130**, e.g., $\sin[(\omega_0+\omega_{LO2})t]$, with the in-phase component of the 1st local oscillation **81**, e.g., $\sin(\omega_{LO1}t)$. Mixing module **172** mixes the quadrature component of the 1st outbound RF signal **130**, e.g., $\cos[(\omega_0+\omega_{LO2})t]$, with the quadrature component of the 1st local oscillation **81**, e.g., $\cos(\omega_{LO1}t)$. The resulting mixed signals are summed via summation module and filtered via filter module **176**. The filter module **176**, which may be a bandpass filter, outputs the 2nd outbound RF signal **132**, which may be represented by $\sin[(\omega_0+\omega_{LO2}+\omega_{LO1})t]$.

The transmit switch module **124** then provides the 2nd outbound RF signal **132**, as the selected outbound RF signal **134**, to power amplifier **126**, which produces the outbound RF signal **136**.

In the alternate configuration, the transmitter section **82** up converts the outbound low IF signal **128** to the lower of the

two frequency range modes. In this instance, the transmitter switch **124** bypasses the 2^{nd} IF stage **122** and provides the 1^{st} outbound RF signal **130** to the power amplifier **126**. The power amplifier **126** then produces the outbound RF signal **136** from the 1^{st} outbound RF signal **130**.

FIG. 7 is a schematic block diagram of a local oscillation module **74** that includes a local oscillation generator **180**, 1^{st} oscillation module **182** and 2^{nd} oscillation module **184**. The local oscillation generator **180** produces a reference oscillation **186**. The 1^{st} oscillation module **182** manipulates the reference oscillation **186** to produce the 1^{st} local oscillation **81**. The 1^{st} local oscillation **81** may be buffered and provided to the receiver section **72** and separately to the transmitter section **82**. Similarly, the 2^{nd} oscillation module **184** manipulates the reference oscillation **186** to produce the 2^{nd} local oscillation **83**. The 2^{nd} local oscillation **83** may be buffered and separately provided to the receiver section **72** and transmitter section **82**.

In one embodiment of the local oscillation module **74**, the local oscillation generator **180** is a crystal oscillator that produces a reference oscillation **186**. The 1^{st} and 2^{nd} oscillation modules **182** and **184** may be separate phase locked loops that produce the 1^{st} local oscillation **81** and 2^{nd} local oscillation **83**, respectively. For example, the crystal generator may generate a clock signal of approximately 20 megahertz while the 1^{st} local oscillation **81** may be 2.85 gigahertz and the 2^{nd} local oscillation may be 2.4 gigahertz.

In a 2^{nd} embodiment of the local oscillation module **74**, the local oscillation generator **180**, the 1^{st} oscillation module **182** and the 2^{nd} oscillation module **184** may each be phase locked loops producing their respective oscillations. In a 3^{rd} embodiment of the local oscillation module **74**, the local oscillation generator **180** may be a phase locked loop that produces a reference oscillation **186** at a frequency similar to the frequency of the 1^{st} local oscillation **81**. The 2^{nd} oscillation module **184** may be a phase locked loop or frequency adjust module to produce the 2^{nd} local oscillation **83** from the reference oscillation **186** or from the 1^{st} local oscillation **81**. In this example, the 1^{st} oscillation module **182** may be an additional buffer, or frequency adjust module.

FIG. 8 is a schematic block diagram of an alternate embodiment of receiver section **72**. In this embodiment, the receiver section **72** may be configured in one of three modes. For example, the receiver section **72** may be configured to receive 3^{rd} inbound RF signals **194**, 1^{st} inbound RF signals **106** or 2^{nd} inbound RF signals **110**. In one example, the 3^{rd} inbound RF signals **194** have a carrier frequency of 5.25 gigahertz, the 1^{st} inbound RF signals **106** have a carrier frequency of 2.4 gigahertz and the 2^{nd} inbound RF signals **110** have a carrier frequency of 900 megahertz.

When the receiver section **72** is configured to process the 2^{nd} inbound RF signals **110**, which for example may have a carrier frequency of 900 megahertz, the 2^{nd} receiver switch module **192**, the 1^{st} receiver IF stage **100** and the 3^{rd} receiver IF stage **190** may be disabled. Accordingly, the receiver switch module **102** provides the 2^{nd} inbound RF signals **110** to the 2^{nd} receiver IF stage **104**. The 2^{nd} receiver IF stage **104** converts the 2^{nd} inbound RF signals **110** into the inbound low IF signals **114** based on the 2^{nd} local oscillation **83**. For example, if the 2^{nd} inbound RF signal **110** has a carrier frequency of 900 megahertz, the 2^{nd} local oscillation **83** has a frequency of 900 megahertz such that the inbound low IF signal **114** has a carrier frequency of zero to a few megahertz.

When the receiver section **72** is configured to receive 1^{st} inbound RF signals **106**, which may have a carrier frequency of 2.4 gigahertz, the 3^{rd} receiver IF stage **190** may be deactivated. In this mode, the 2^{nd} receiver switch module **192** pro-

vides the 1^{st} inbound RF signals **106** to the 1^{st} receiver IF stage **100**. The 1^{st} receiver IF stage **100** converts the 1^{st} inbound RF signals **106** into 1^{st} inbound IF signals **108** based on the 1^{st} local oscillation **81**, which may have a frequency of 1.5 gigahertz. The receiver switch module **102** passes the 1^{st} inbound IF signals **108** to the 2^{nd} receiver IF stage **104**. The 2^{nd} receiver IF stage **104** converts the 1^{st} inbound IF signal **108** into the inbound low IF signal based on the 2^{nd} local oscillation **83**, which may have a frequency of 900 megahertz.

In a 3^{rd} configuration, the receiver section **72** is operably coupled to receive the 3^{rd} inbound RF signals **194**. The 3^{rd} receiver IF stage **190** converts the 3^{rd} inbound RF signals **194** into 3^{rd} inbound IF signals **198** based on a 3^{rd} local oscillation **196**. The 3^{rd} local oscillation **196** may have a frequency of 2.85 gigahertz when the 3^{rd} inbound RF signals **194** have a carrier frequency of 5.25 gigahertz. The 2^{nd} switch module **192** provides the 3^{rd} inbound IF signals **198** to the 1^{st} receiver IF stage **100**. The 1^{st} receiver IF stage **100** converts the 3^{rd} inbound IF signals **198** into the 1^{st} inbound IF signals **100** based on the 1^{st} local oscillation **81**, which may have a frequency of 1.5 gigahertz.

The receiver switch module **102** provides the 1^{st} inbound IF signals **108** to the 2^{nd} IF stage **104**. The 2^{nd} receiver IF stage **104** converts the 1^{st} inbound IF signal **108** into the inbound low IF signal **114** based on the 2^{nd} local oscillation **83** which may have a frequency of 900 megahertz.

FIG. 9 is a schematic block diagram of another embodiment of transmitter section **82** that includes the 1^{st} transmitter IF stage **120**, the 2^{nd} transmitter IF stage **122**, the transmitter switch module **124**, a 2^{nd} transmitter switch module **200**, a 3^{rd} transmitter IF stage **202** and the power amplifier **126**. As illustrated, the transmitter section **82** may be configured to up convert the outbound low IF signal **128** to an output RF signal **136** having a 1^{st} , 2^{nd} or 3^{rd} carrier frequency. For example, the 1^{st} carrier frequency may correspond to 900 megahertz, the 2^{nd} carrier frequency to 2.4 gigahertz and the 3^{rd} carrier frequency to 5.25 gigahertz.

When the transmitter section **82** is configured to up convert the outbound low IF signal **128** to the outbound RF signal **136** having a carrier frequency of 900 megahertz, the 2^{nd} local oscillation **83** has a frequency of 900 megahertz. Accordingly, the 1^{st} transmitter IF stage **120** up converts the outbound low IF signal **128** to the 1^{st} outbound RF signal **130** having a carrier frequency of 900 megahertz. The transmitter switch module **124** and 2^{nd} transmitter switch module **200** are configured to pass the 1^{st} outbound RF signal **130** to the power amplifier **126**.

In a 2^{nd} configuration, the transmitter section **82** may be configured to up convert the outbound low IF signal **128** to the outbound RF signal **136** having a carrier frequency of 2.4 gigahertz. In this configuration, the 1^{st} transmitter IF stage **120** produces the 1^{st} outbound RF signal **130** having a carrier frequency of 900 megahertz. Transmitter switch module **124** provides the 1^{st} outbound RF signal **130** to the 2^{nd} transmitter IF stage **122**. The 2^{nd} transmitter IF stage **122** up converts the 1^{st} outbound RF signal **130** to the 2^{nd} outbound RF signal **132** having a carrier frequency of 2.4 gigahertz based on the 1^{st} local oscillation **81** having a frequency of 1.5 gigahertz. The 2^{nd} transmitter switch module **200** is configured to pass the 2^{nd} outbound RF signal **132** to the power amplifier.

In the 3^{rd} configuration, where the transmitter section **82** is configured to convert the outbound low IF signal **128** into the outbound RF signal **136** having a carrier frequency of 5.25 gigahertz, the 1^{st} transmitter IF stage **120**, transmitter switch module **124** and 2^{nd} transmitter IF stage **122** are active to produce the 2^{nd} outbound RF signal **132** having a carrier frequency of 2.4 gigahertz.

11

The 2nd transmitter switch module **200**, in this configuration, provides the 2nd outbound RF signal **132** to the 3rd transmitter IF stage **202**. The 3rd transmitter IF stage **202** up converts the 2nd outbound RF signal **132** based on the 3rd local oscillation **204**, which may have a frequency of 2.85 gigahertz, to produce the 3rd outbound RF signal **206**. The 2nd transmitter switch module **200** provides the 3rd outbound RF signal **206** to the power amplifier **126**, which outputs the outbound RF signal **136** having a carrier frequency of 5.25 gigahertz.

The preceding discussion has presented a wide bandwidth transceiver that is capable of supporting multiple wireless communication standards. As one of average skill in the art will appreciate, other embodiments may be derived from the teaching of the present invention, without deviating from the scope of the claims.

What is claimed is:

1. A wide bandwidth transceiver comprises:

local oscillation module coupled to generate a first local oscillation and a second local oscillation;

a transmitter section coupled to convert at least one of an outbound baseband signal and a low intermediate frequency (IF) signal into a first outbound radio frequency (RF) signal based on the second local oscillation when the wide bandwidth transceiver is in a second wireless standard mode and coupled to convert the at least one of the outbound baseband and the low IF signal into a second outbound RF signal based on the first and second local oscillations when the wide bandwidth transceiver is in a first wireless standard mode; and

a receiver section coupled to convert a first inbound RF signal into at least one of an inbound low IF signal and a baseband signal based on the first and second local oscillations when the wide bandwidth transceiver is in the first wireless standard mode and coupled to convert a second inbound RF signal into the at least one of the inbound low IF signal and the baseband signal based on the second local oscillation when the wide bandwidth transceiver is in the second wireless standard mode.

2. The wide bandwidth transceiver of claim **1** comprises: the first wireless standard mode including at least one of: IEEE 802.11, Bluetooth, advanced mobile phone services (AMPS), digital AMPS, global system for mobile communications (GSM), code division multiple access (CDMA), local multi-point distribution systems (LMDS), multi-channel-multi-point distribution systems (MMDS), and variations thereof; and

the second wireless standard mode including at least one of: IEEE 802.11, Bluetooth, advanced mobile phone services (AMPS), digital AMPS, global system for mobile communications (GSM), code division multiple

12

access (CDMA), local multi-point distribution systems (LMDS), multi-channel-multi-point distribution systems (MMDS), and variations thereof.

3. The wide bandwidth transceiver of claim **1** comprises: the local oscillation module coupled to generate a third local oscillation;

the transmitter section coupled to convert the at least one of the outbound baseband and the low IF signal into a third outbound RF signal based on the first, second, and third local oscillations when the wide bandwidth transceiver is in a third wireless standard mode; and

the receiver section coupled to convert a third inbound RF signal into the at least one of the inbound low IF signal and the baseband signal based on the first, second, and third local oscillation when the wide bandwidth transceiver is in the third wireless standard mode.

4. The wide bandwidth transceiver of claim **1**, wherein the receiver section comprises:

a first low noise amplifier coupled to amplify the first inbound RF signal to produce an amplified first inbound RF signal;

a second low noise amplifier coupled to amplify the second inbound RF signal to produce an amplified second inbound RF signal;

a first receiver IF stage, when enabled, converts the amplified first inbound RF signal into a first inbound IF signal based on the first local oscillation;

receiver switching module coupled to pass one of the first inbound IF signal and the second inbound RF signal to produce a selected inbound signal; and

second receiver IF stage coupled to convert the selected inbound signal into the at least one of the inbound low IF signal and the baseband signal based on the second local oscillation.

5. The wide bandwidth transceiver of claim **1**, wherein transmitter section comprises:

a first transmitter IF stage coupled to convert the at least one of the outbound baseband and a low IF signal into the first outbound RF signal based on the second local oscillation;

a second transmitter IF stage, when enabled, converts the first outbound RF signal into the second outbound RF signal based on the first local oscillation;

a power amplifier operably coupled to amplify a selected outbound RF signal; and

a transmitter switching module operably coupled to provide one of the first outbound RF signal and the second outbound RF signal to the power amplifier as the selected outbound RF signal.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

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INVENTOR(S) : Ahmadreza Reza Rofougaran

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Title Page, after Item (65): "Prior Publication Data US 2006/0276222 A1 Dec. 7, 2006"
insert --Related U.S. Application Data (63) Continuation of application No. 10/306,047,
filed on Nov. 27, 2002, now Pat. No. 7,120,405.--

Signed and Sealed this

Thirteenth Day of October, 2009



David J. Kappos
Director of the United States Patent and Trademark Office