

US007420733B1

(12) **United States Patent**
Natarajan et al.

(10) **Patent No.:** **US 7,420,733 B1**
(45) **Date of Patent:** **Sep. 2, 2008**

(54) **ELECTRICALLY SWITCHABLE
POLYMER-DISPERSED LIQUID CRYSTAL
MATERIALS INCLUDING SWITCHABLE
OPTICAL COUPLERS AND
RECONFIGURABLE OPTICAL
INTERCONNECTS**

(58) **Field of Classification Search** 359/1,
359/3, 15, 321, 566, 569; 349/1, 2, 20, 88,
349/201, 202; 252/299.01; 430/20; 385/36,
385/37
See application file for complete search history.

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(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 0 days.

(21) Appl. No.: **11/709,073**

(22) Filed: **Feb. 22, 2007**

Related U.S. Application Data

(63) Continuation of application No. 11/340,681, filed on
Jan. 27, 2006, now Pat. No. 7,198,737, which is a
continuation of application No. 10/916,430, filed on
Aug. 12, 2004, now Pat. No. 7,081,215, which is a
continuation of application No. 09/363,169, filed on
Jul. 29, 1999, now Pat. No. 6,821,457.

(60) Provisional application No. 60/094,578, filed on Jul.
29, 1998.

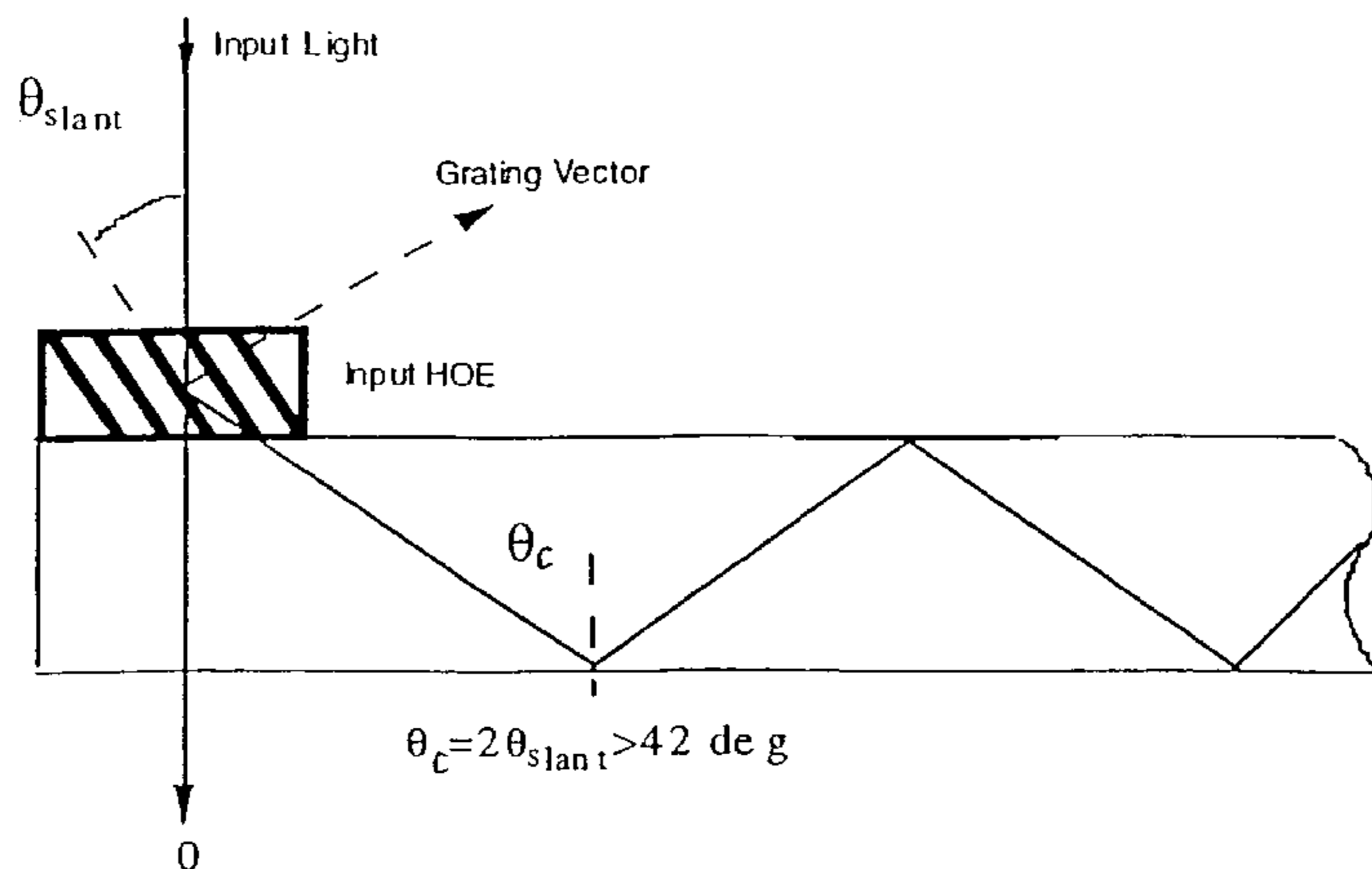
(51) **Int. Cl.**
G02B 5/18 (2006.01)
G02B 6/34 (2006.01)
G02F 1/133 (2006.01)

(52) **U.S. Cl.** **359/566**; 359/321; 359/569;
349/88; 349/201; 349/202; 385/36; 385/37

(57) **ABSTRACT**

A new photopolymerizable material allows single-step, fast recording of volume holograms with properties that can be electrically controlled. Polymer-dispersed liquid crystals (PDLCs) in accordance with the invention preferably comprise a homogeneous mixture of a nematic liquid crystal and a multifunctional pentaacrylate monomer in combination with photoinitiator, coinitiator and cross-linking agent. Optionally, a surfactant such as octanoic acid may also be added. The PDLC material is exposed to coherent light to produce an interference pattern inside the material. Photopolymerization of the new PDLC material produces a hologram of clearly separated liquid crystal domains and cured polymer domains.

52 Claims, 30 Drawing Sheets



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* cited by examiner

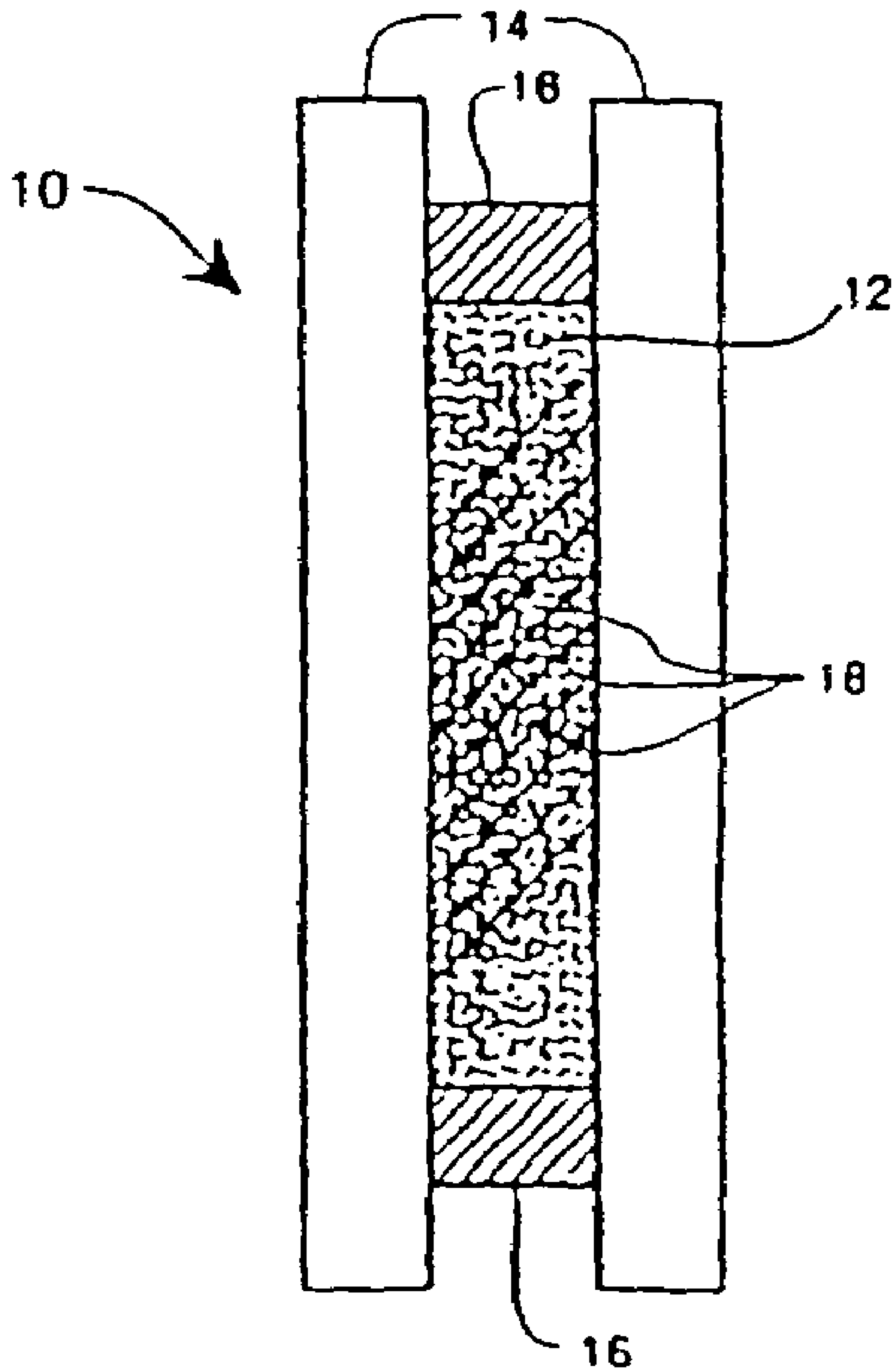


FIG. 1

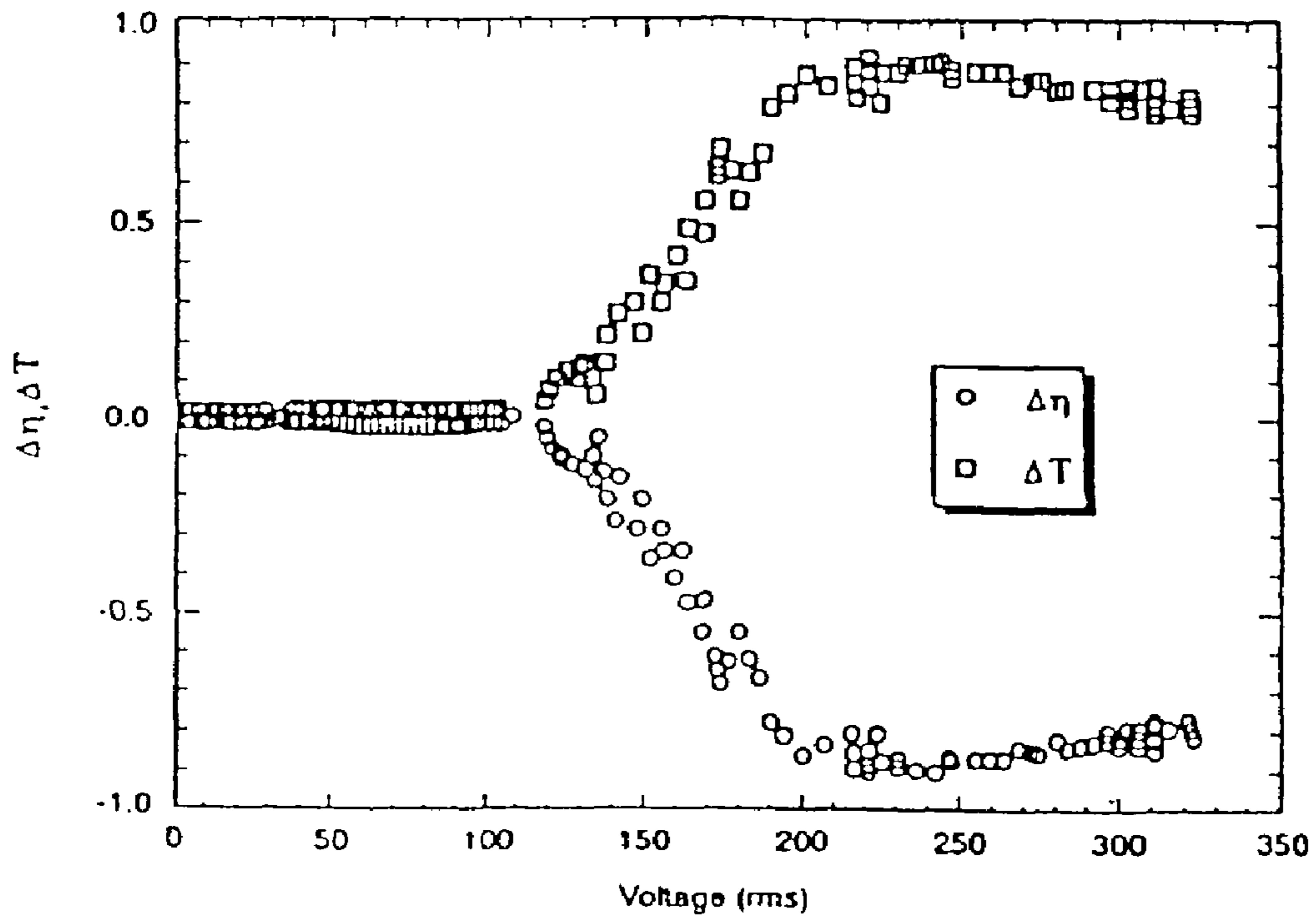


FIG. 2

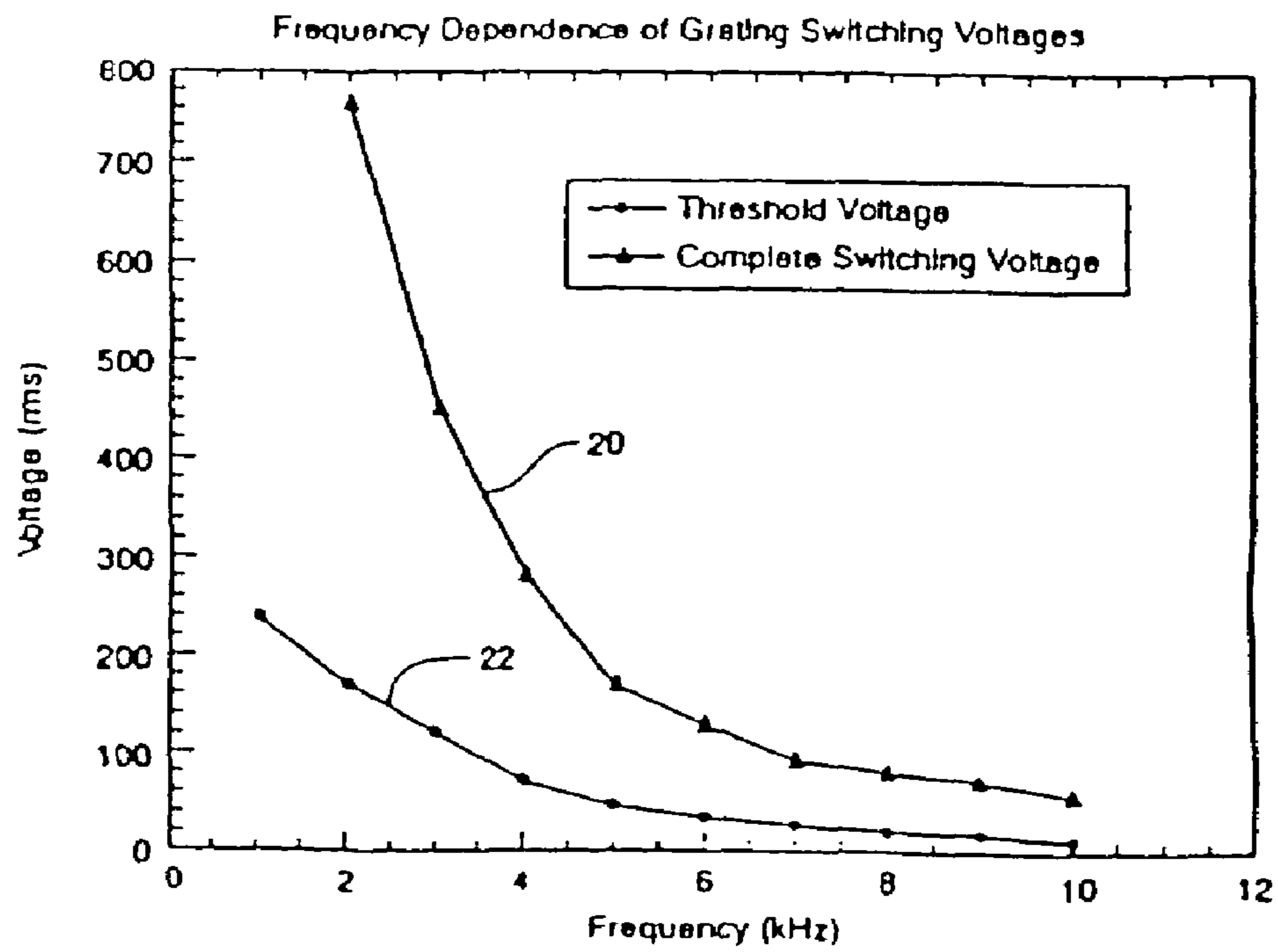


FIG. 3

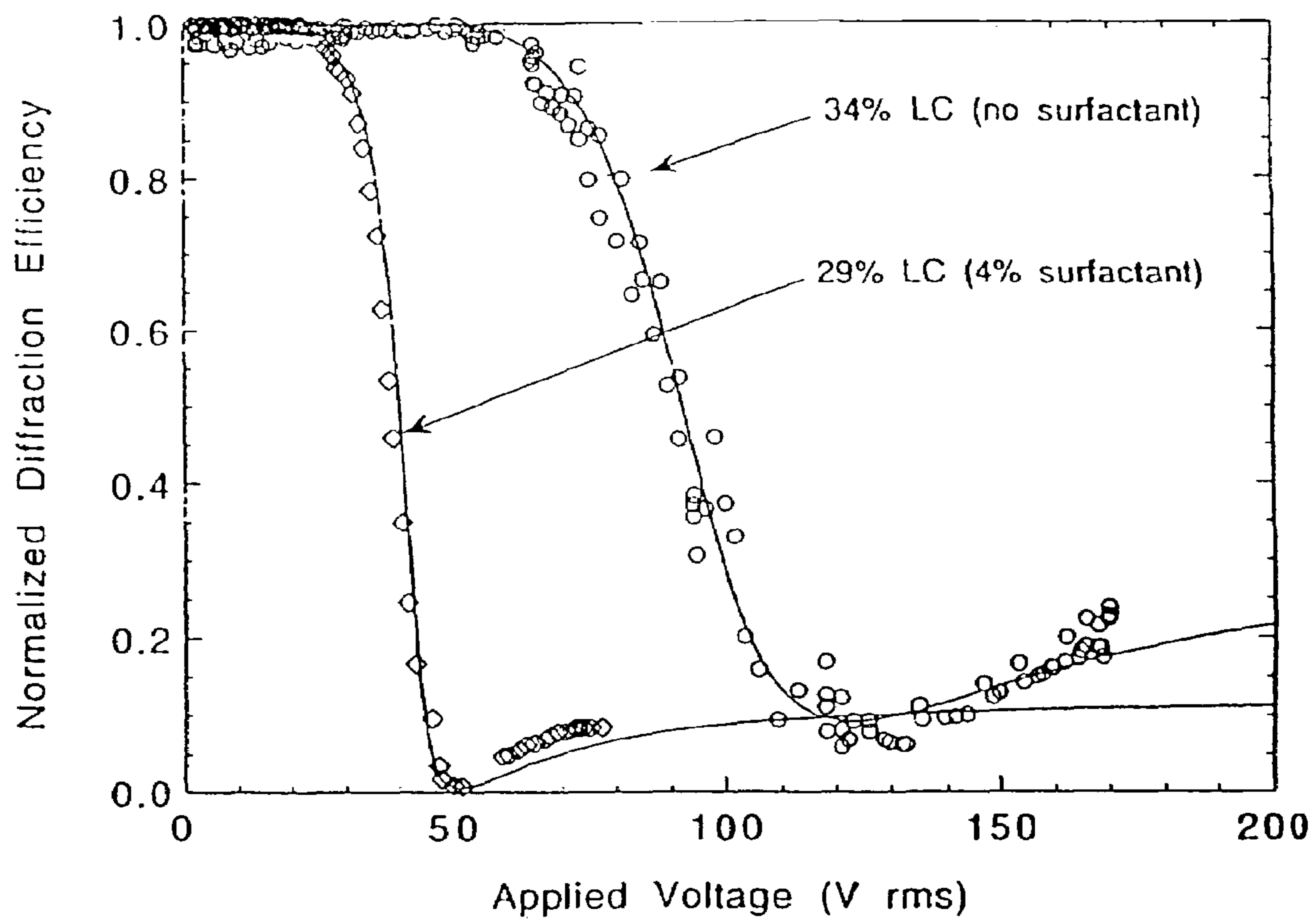


FIG. 4

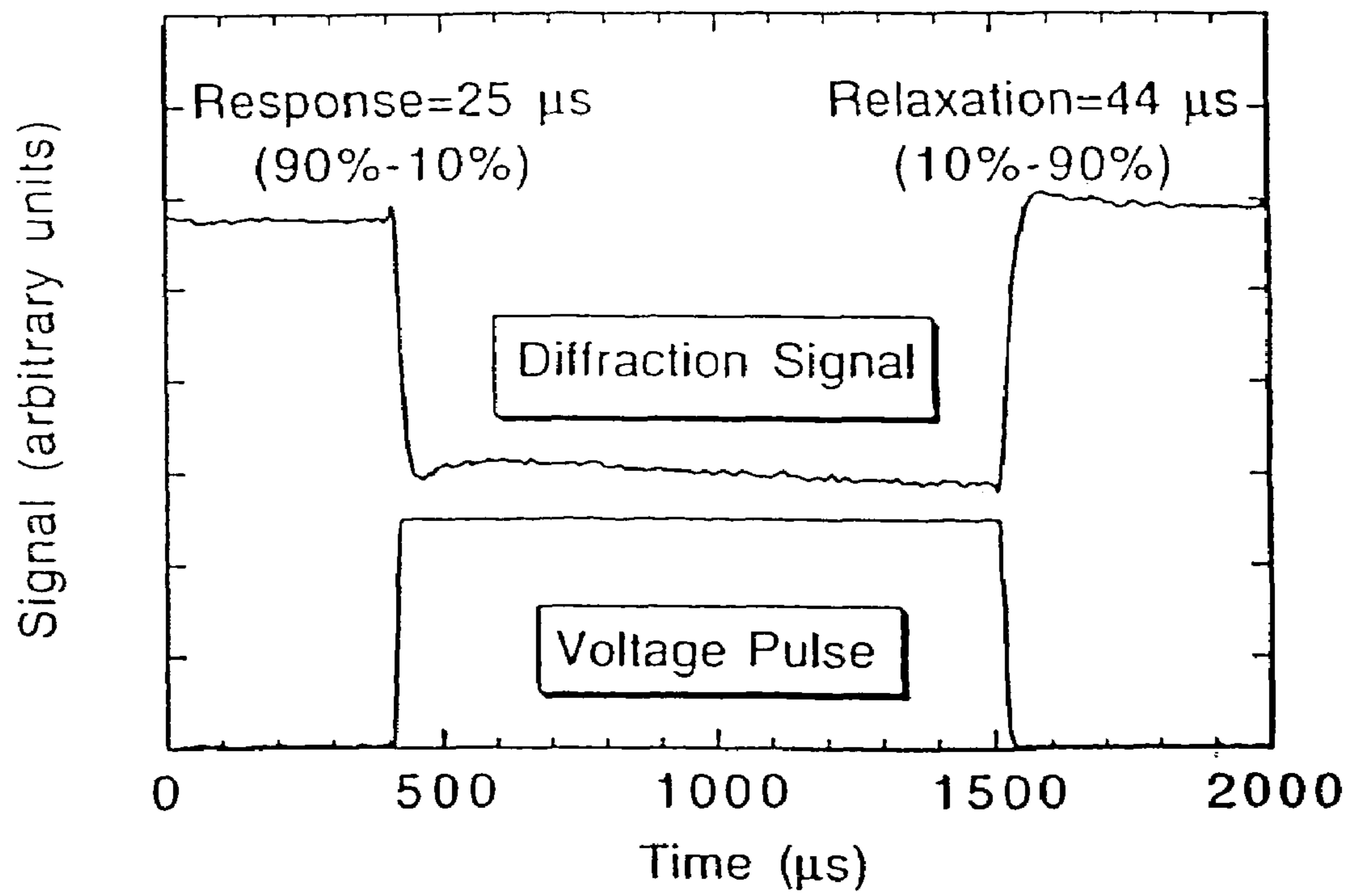


FIG. 5

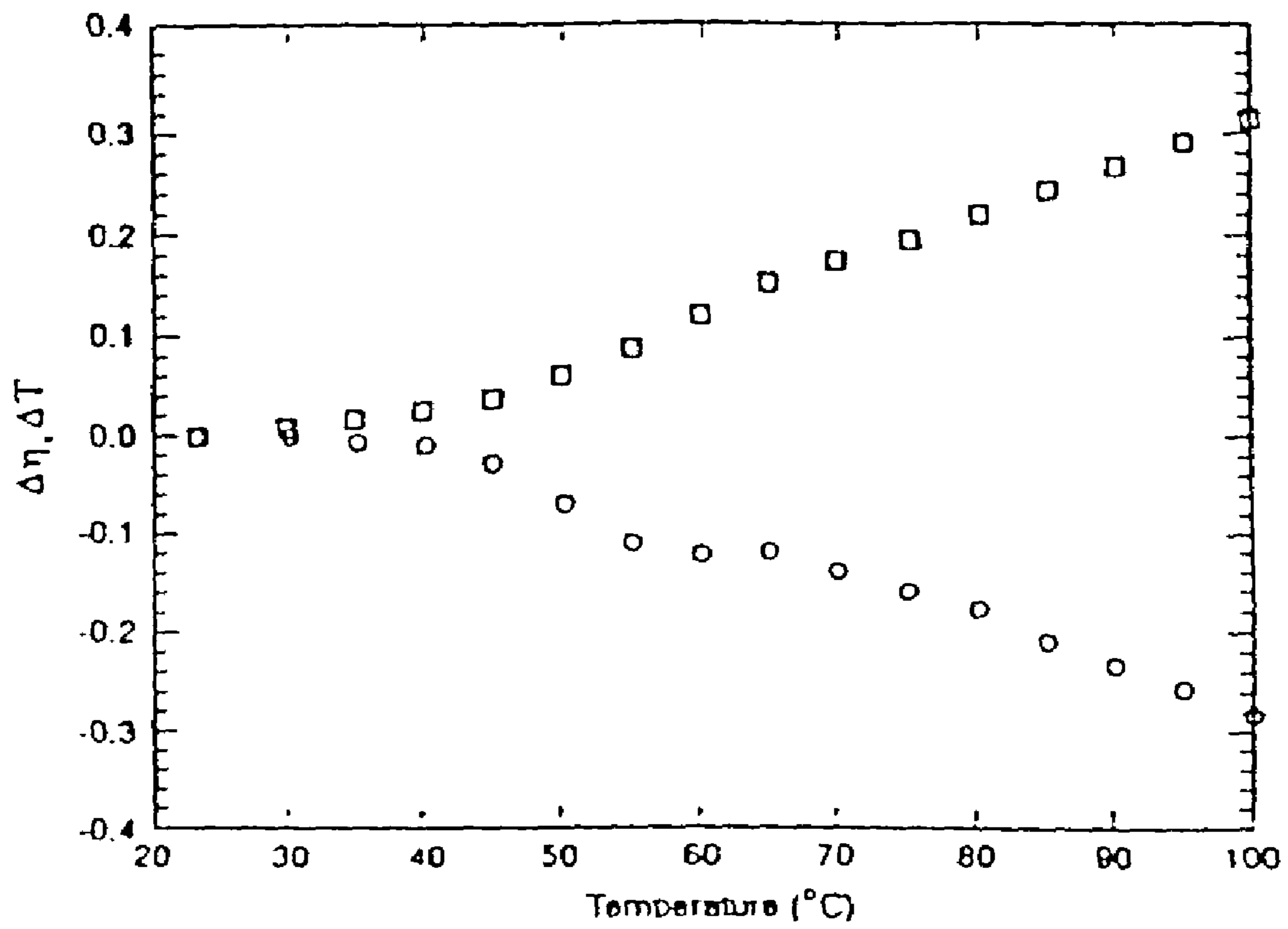


FIG. 6

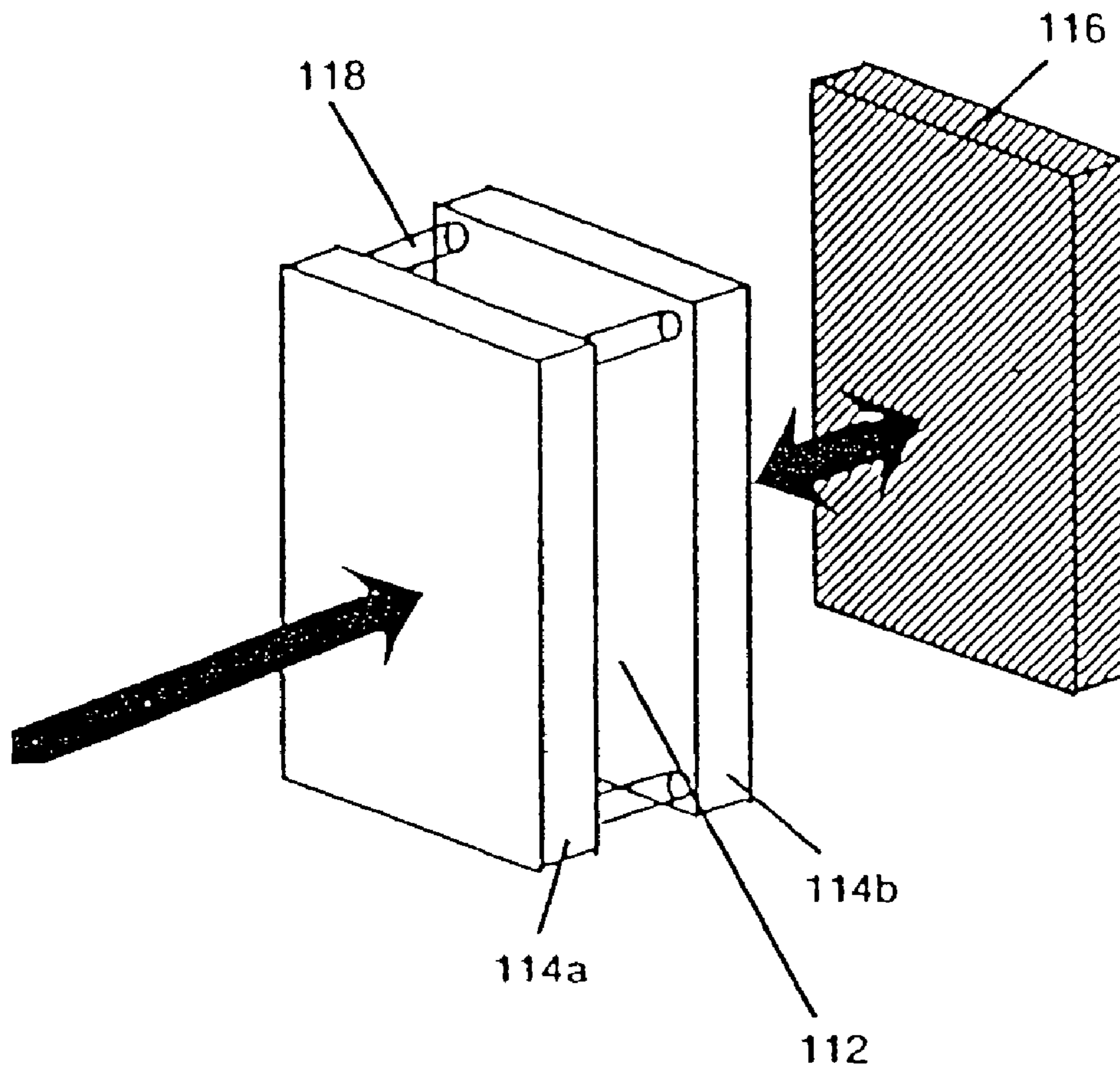


FIG. 7

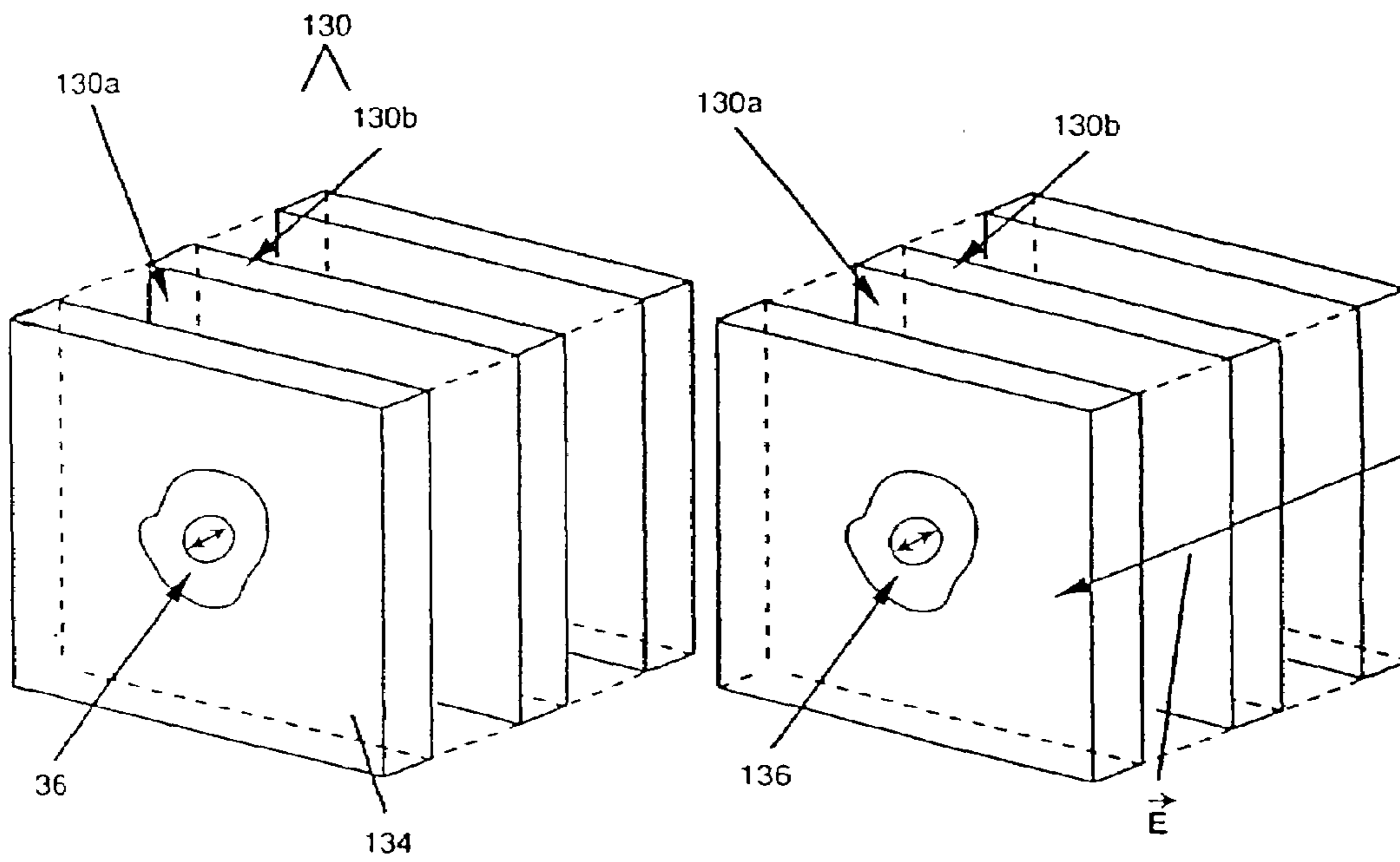


FIG. 8a

Reflection Grating

FIG. 8b

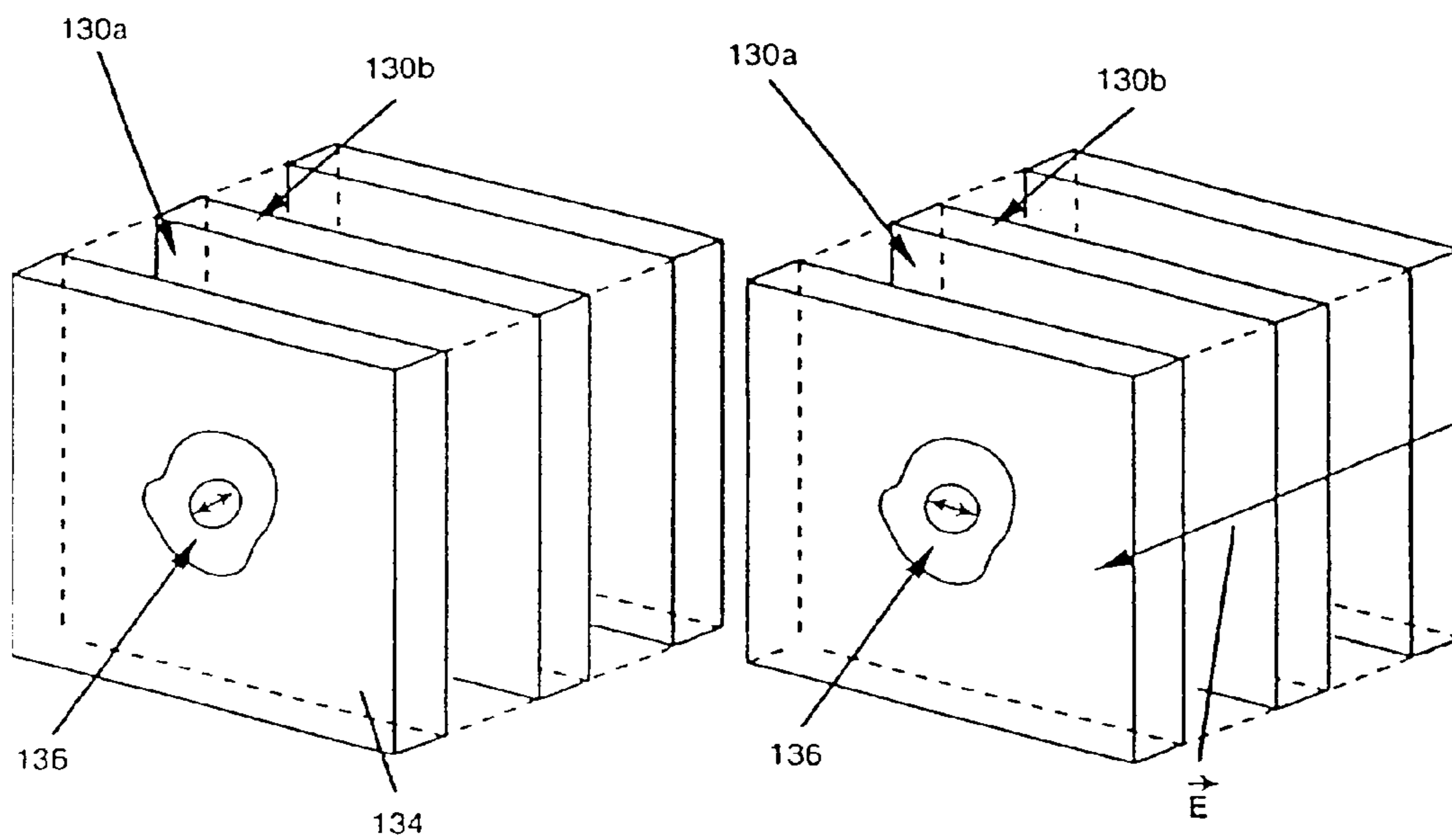


FIG. 9a

Reflection Grating

FIG. 9b

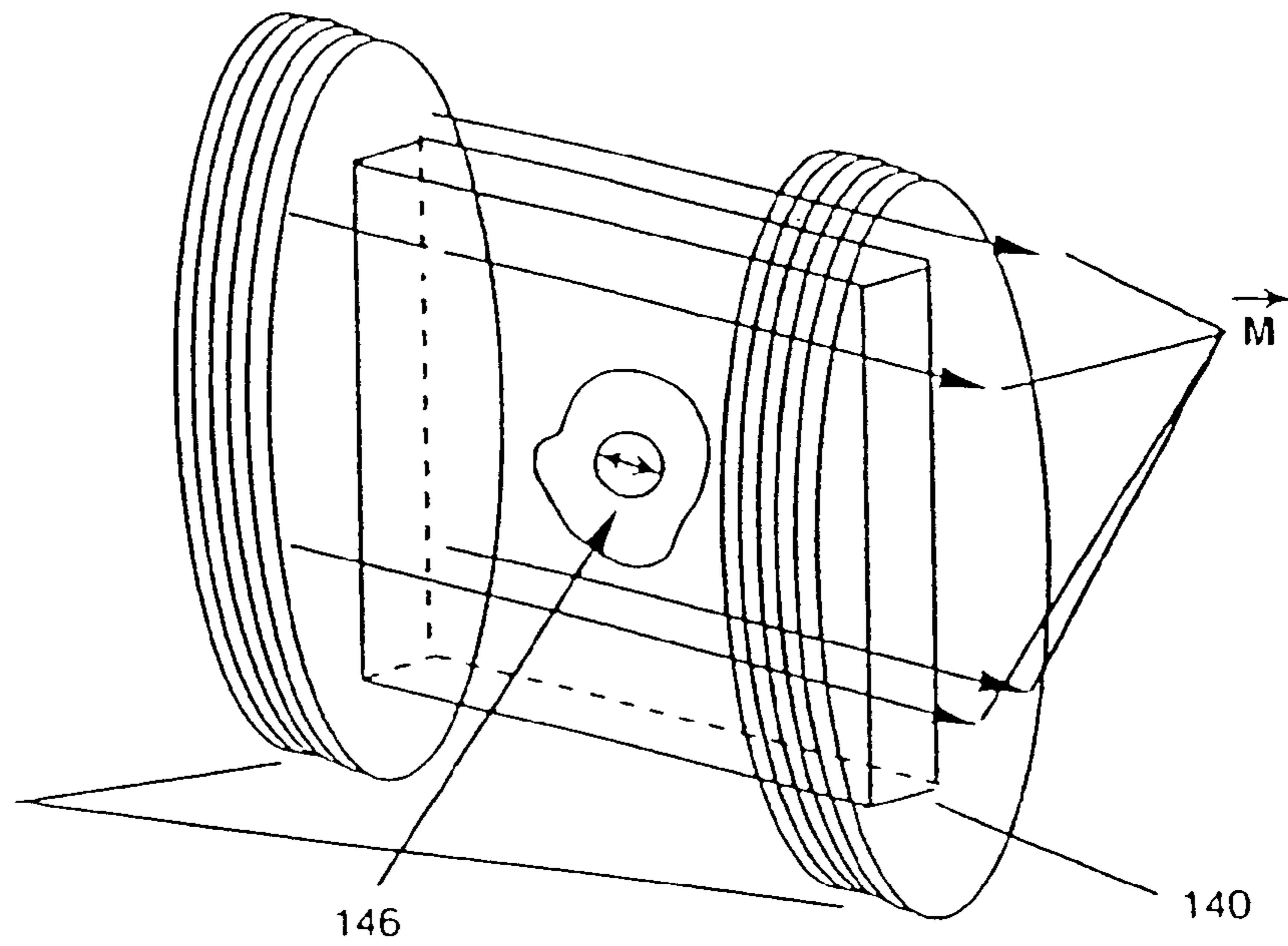


FIG. 10a

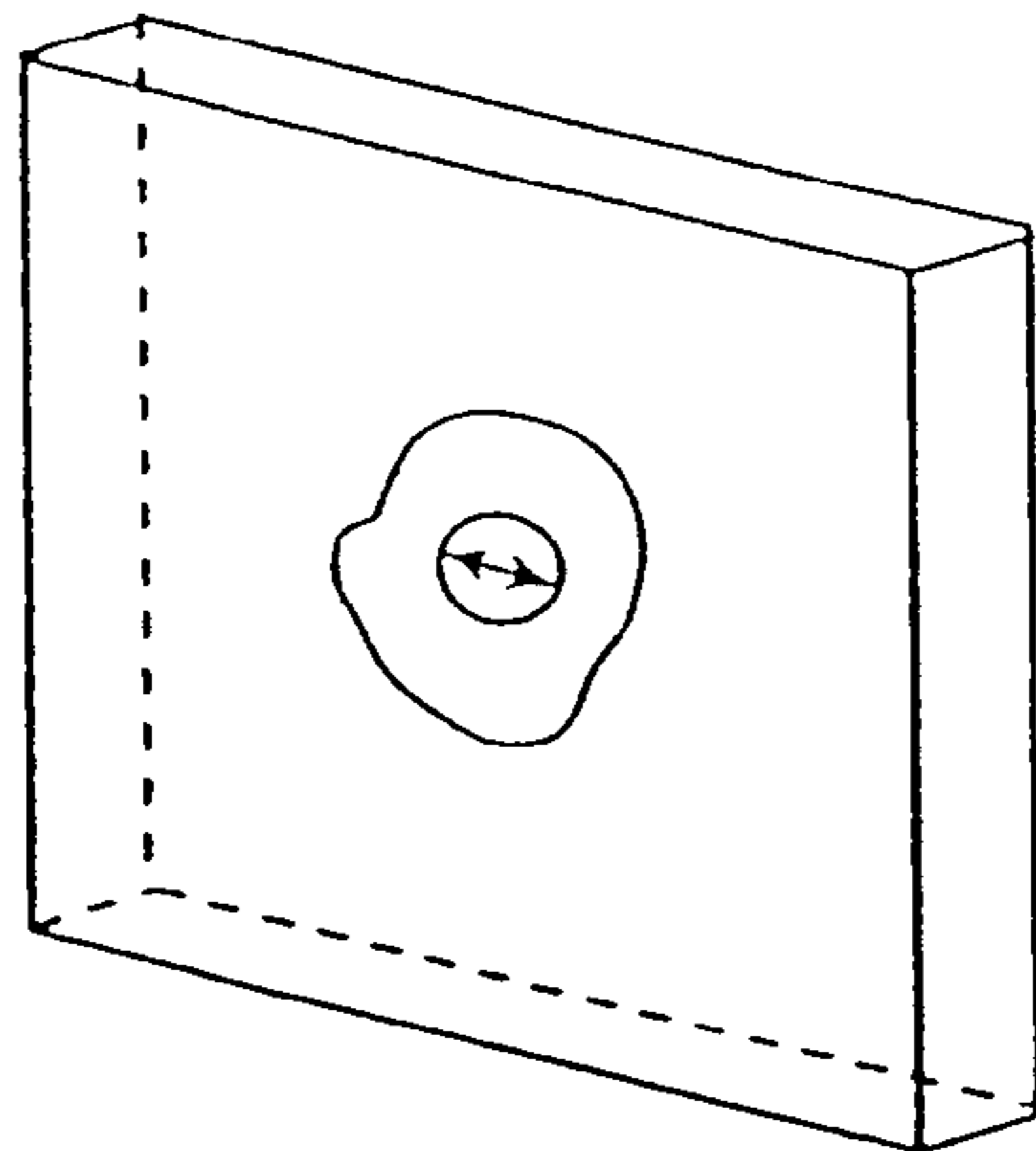


FIG. 10b

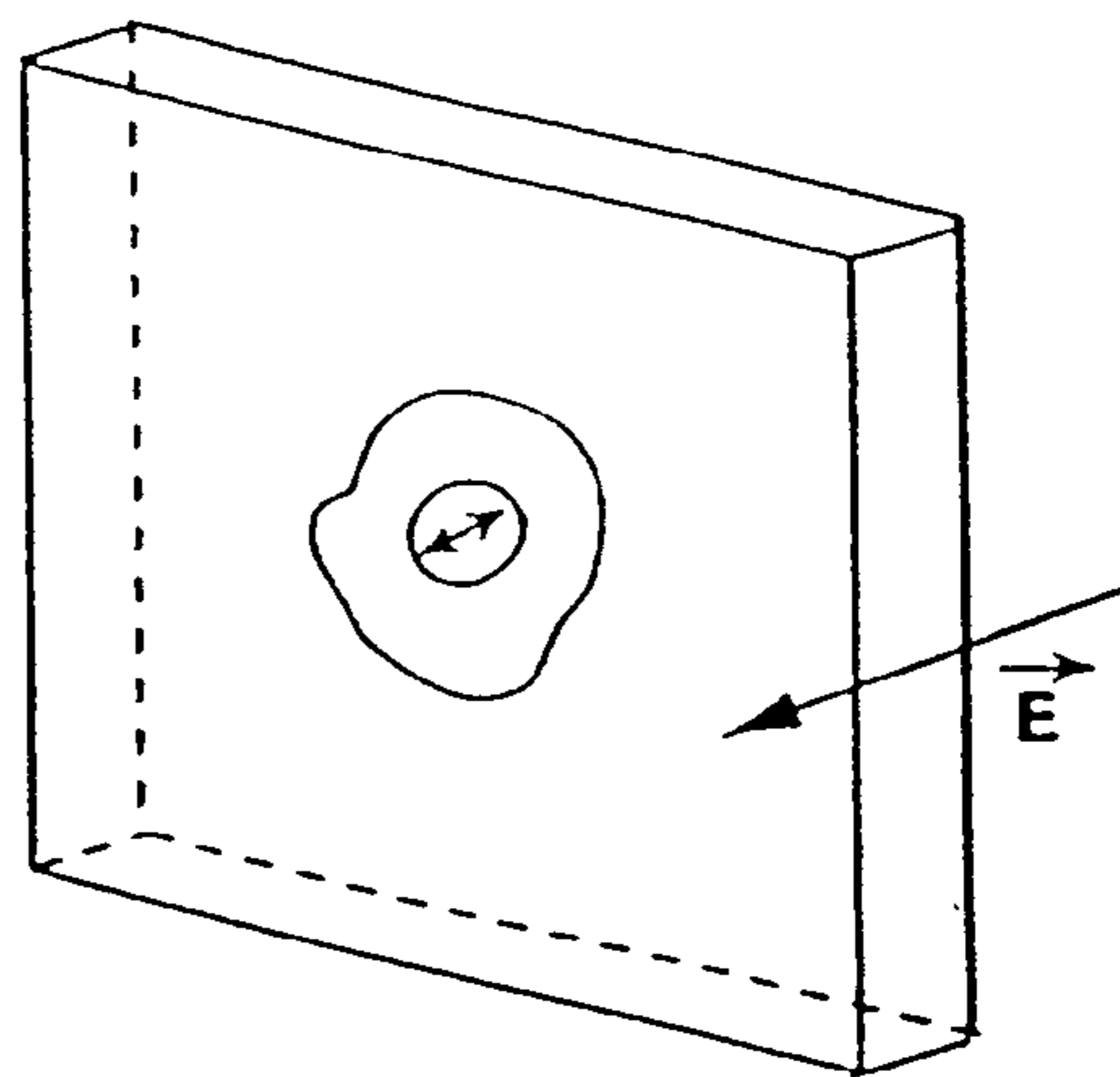
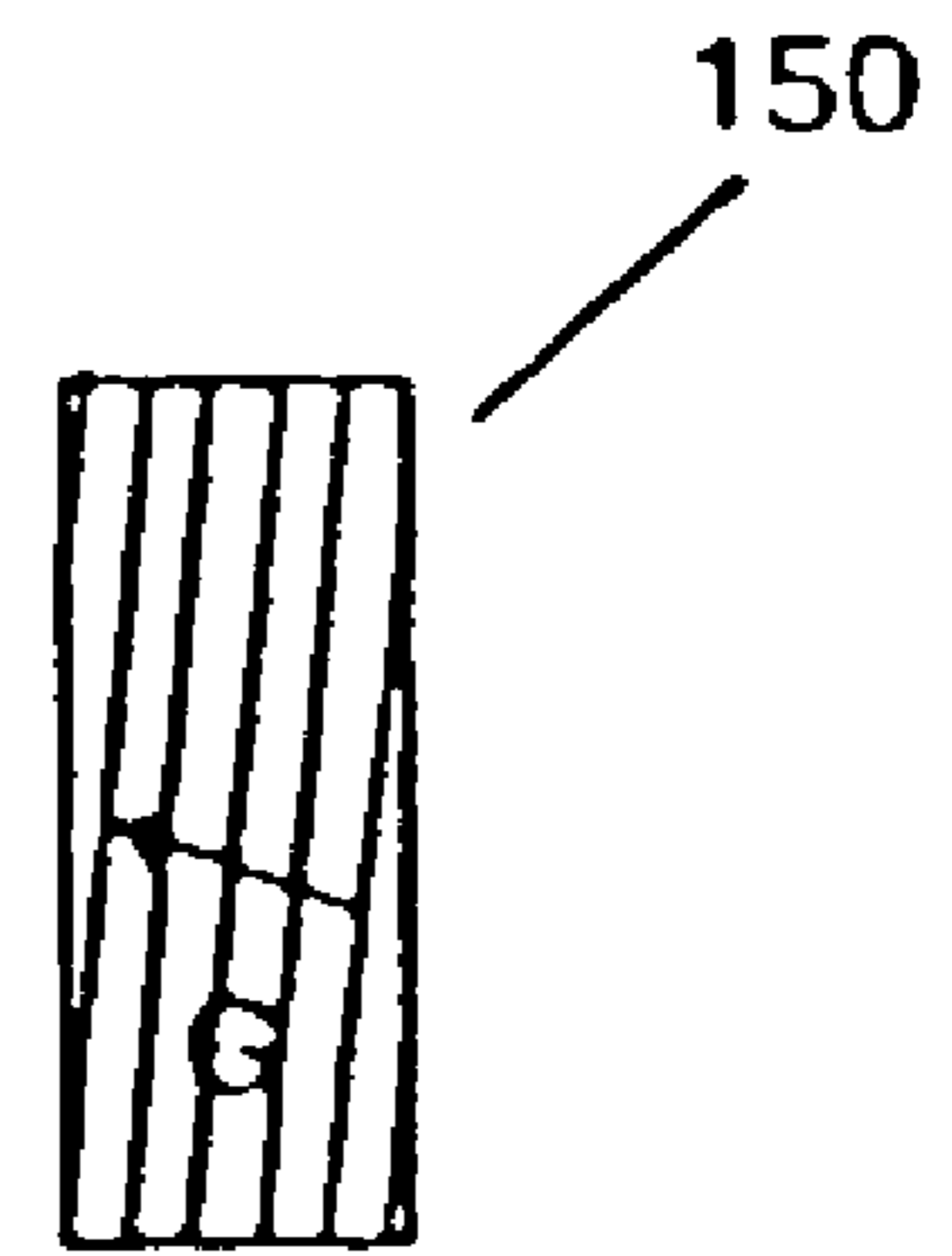
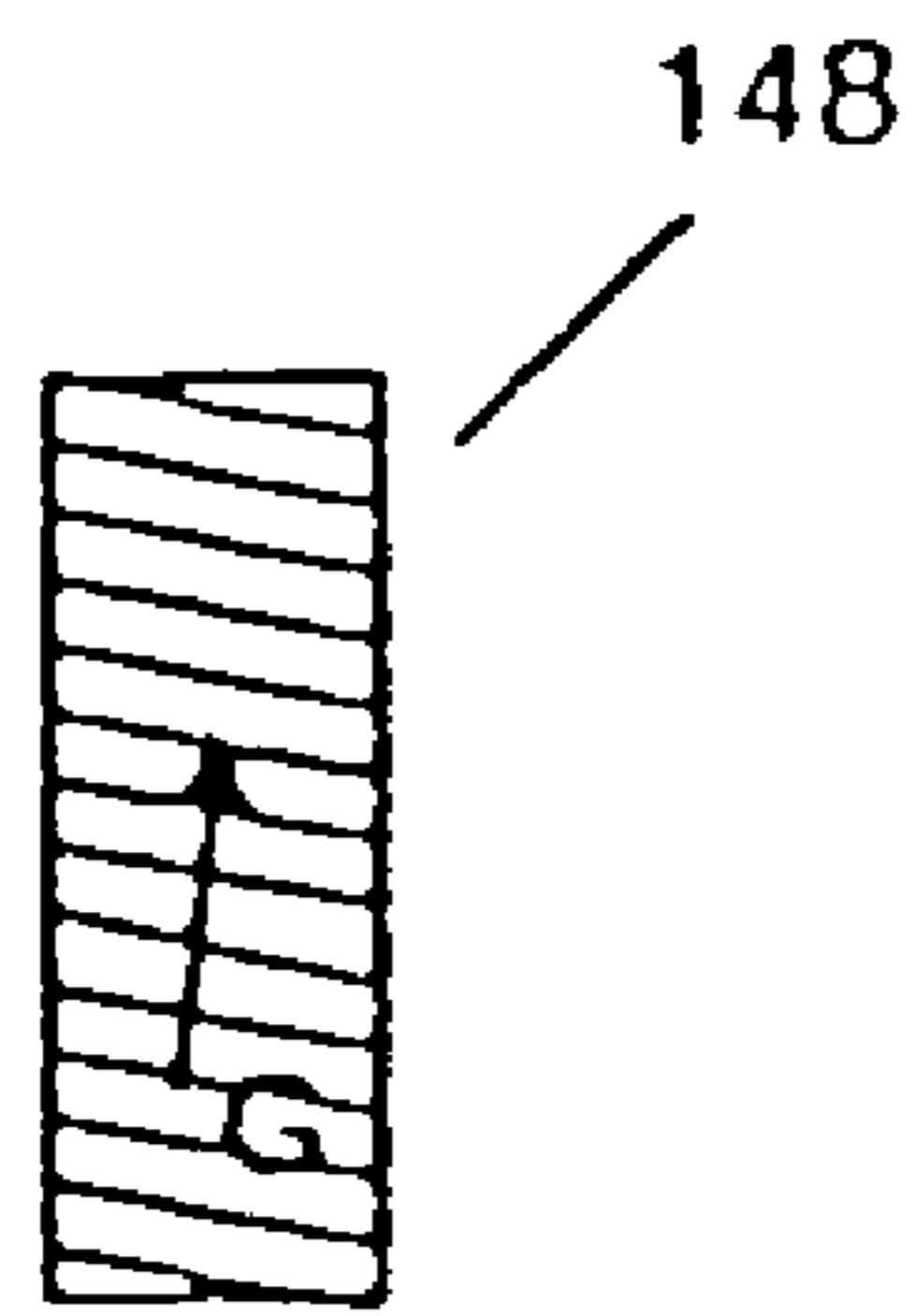


FIG. 10c



Slanted

transmission

reflection

FIG. 11a

FIG. 11b

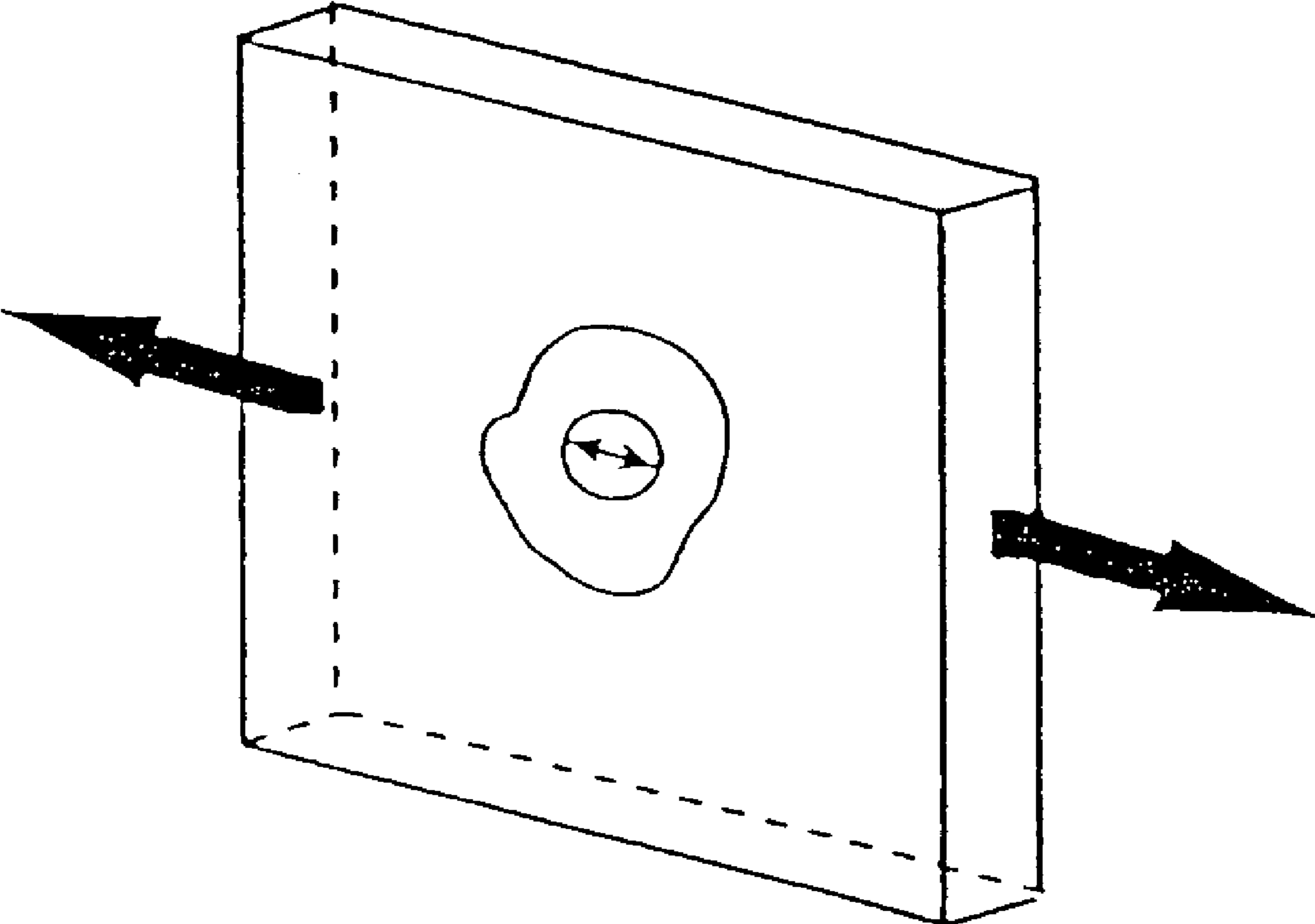


FIG. 12

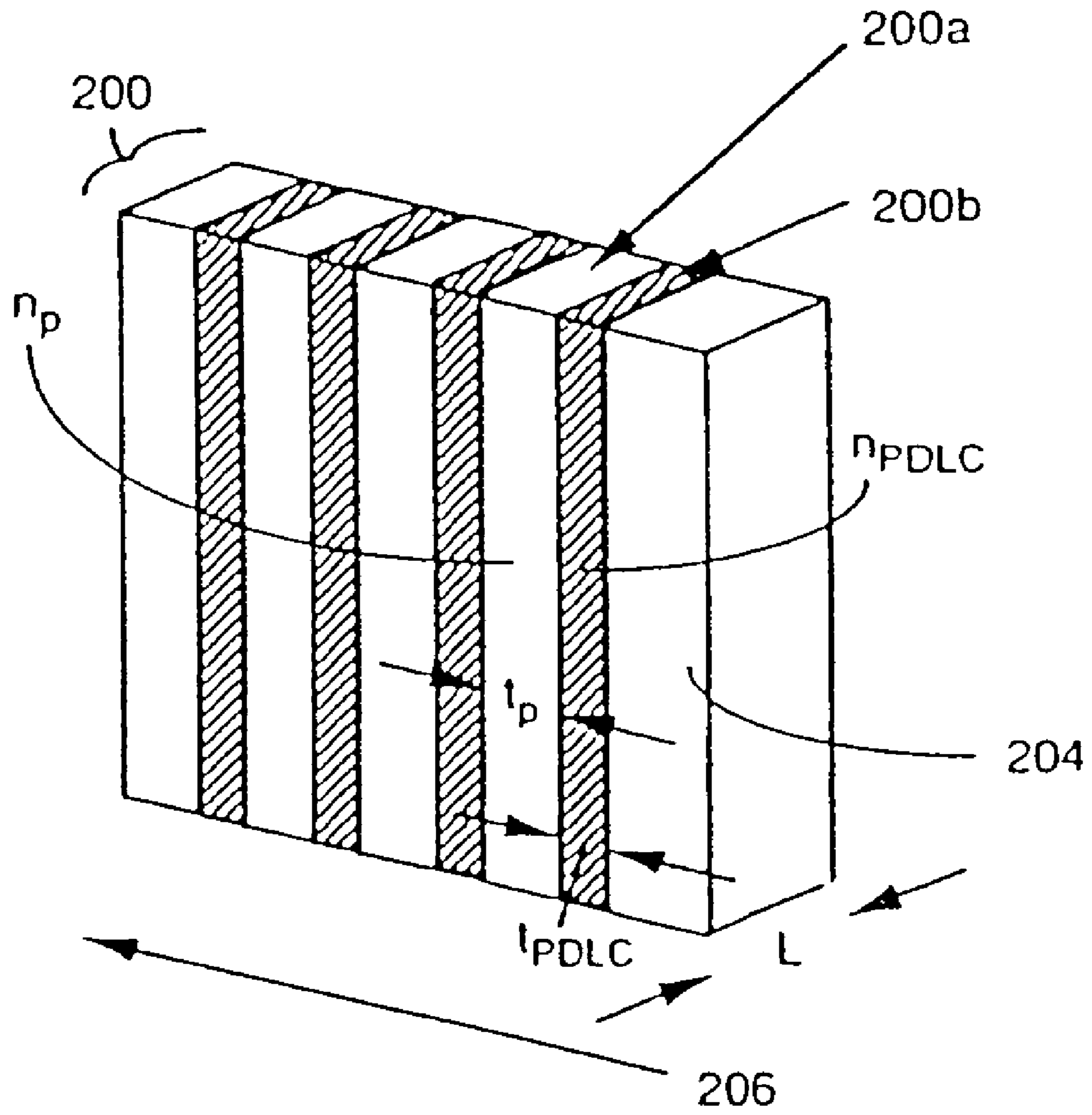


FIG. 13

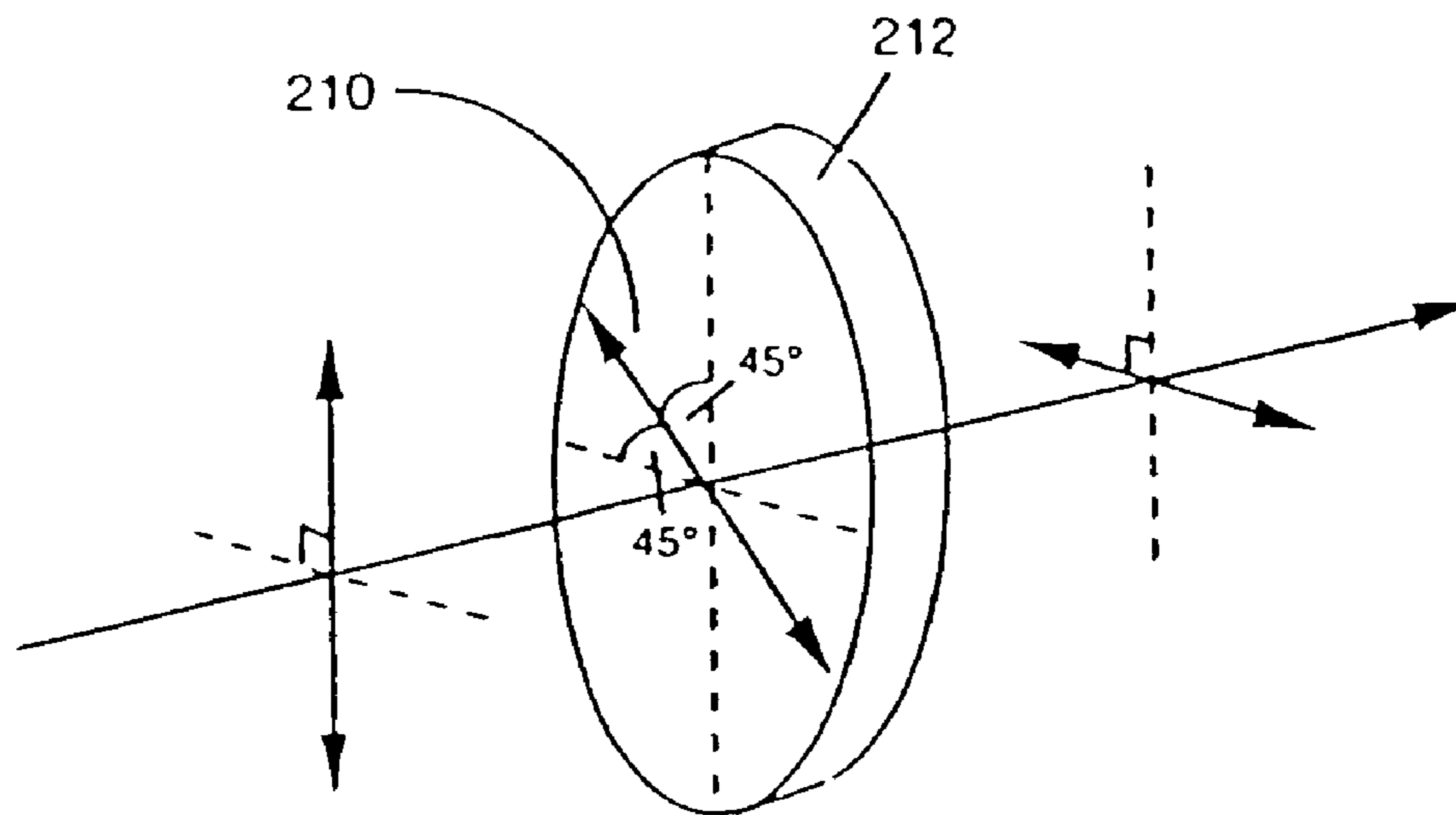


FIG. 14a

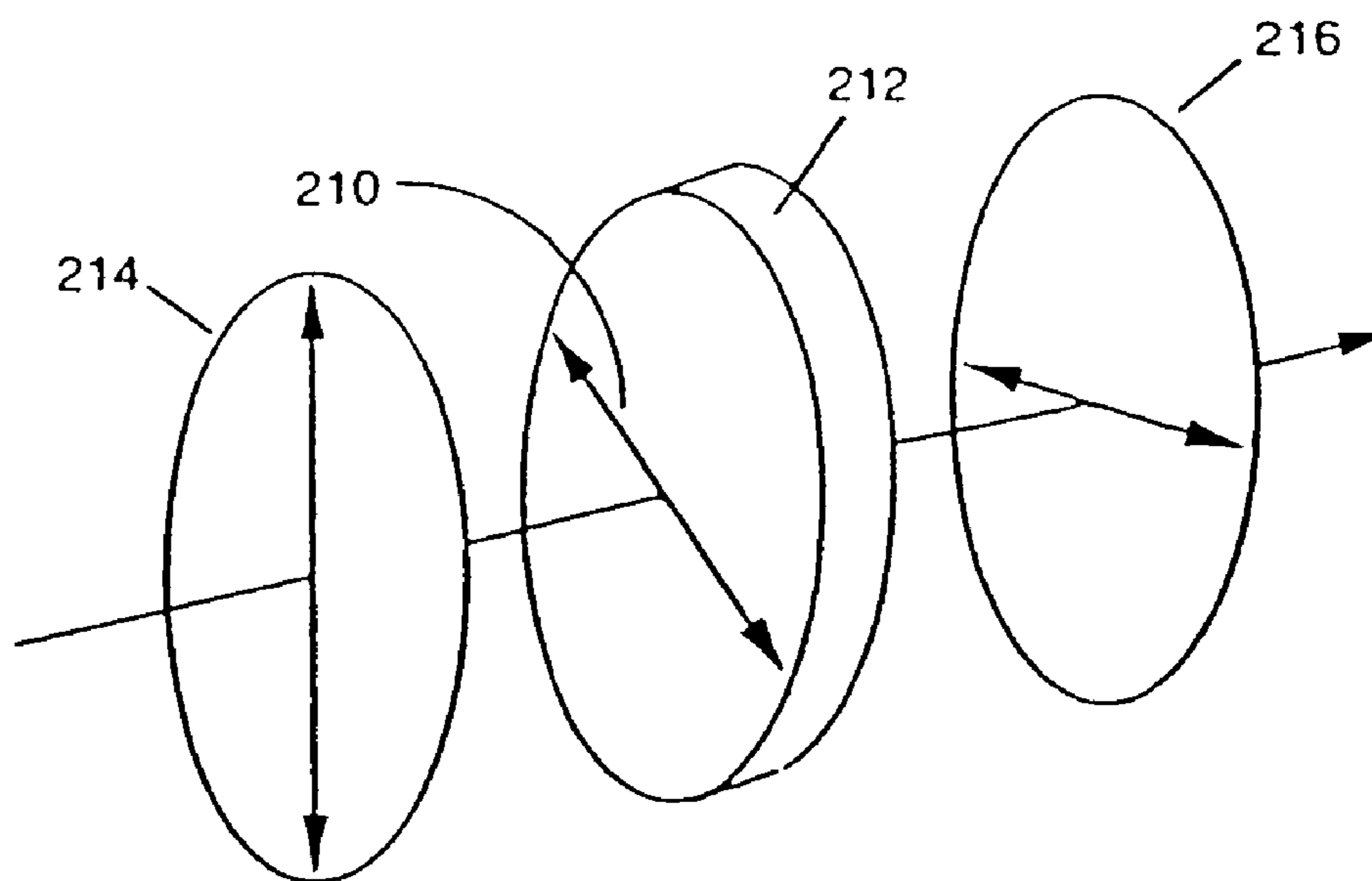


FIG. 14b

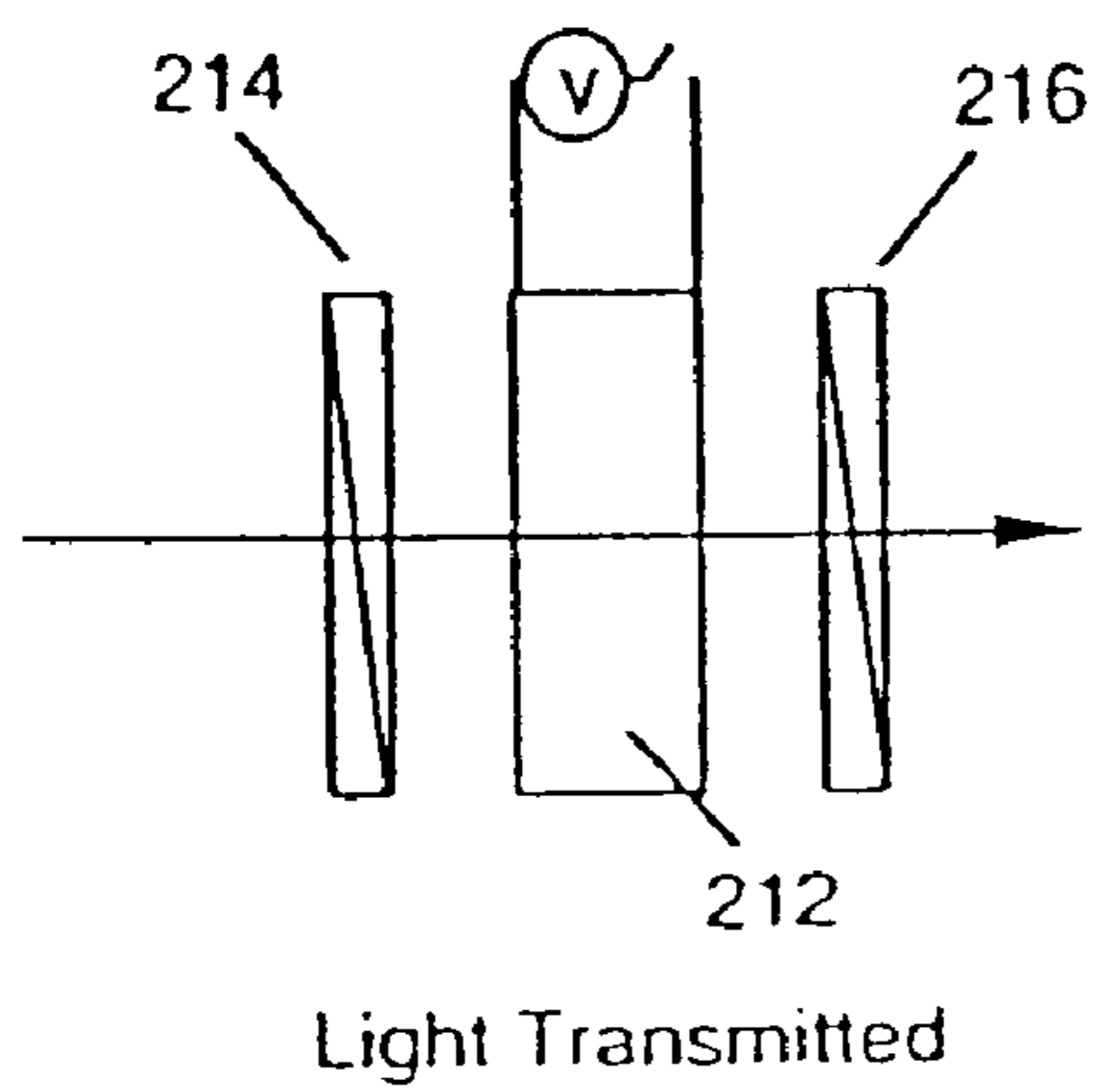


FIG. 14c

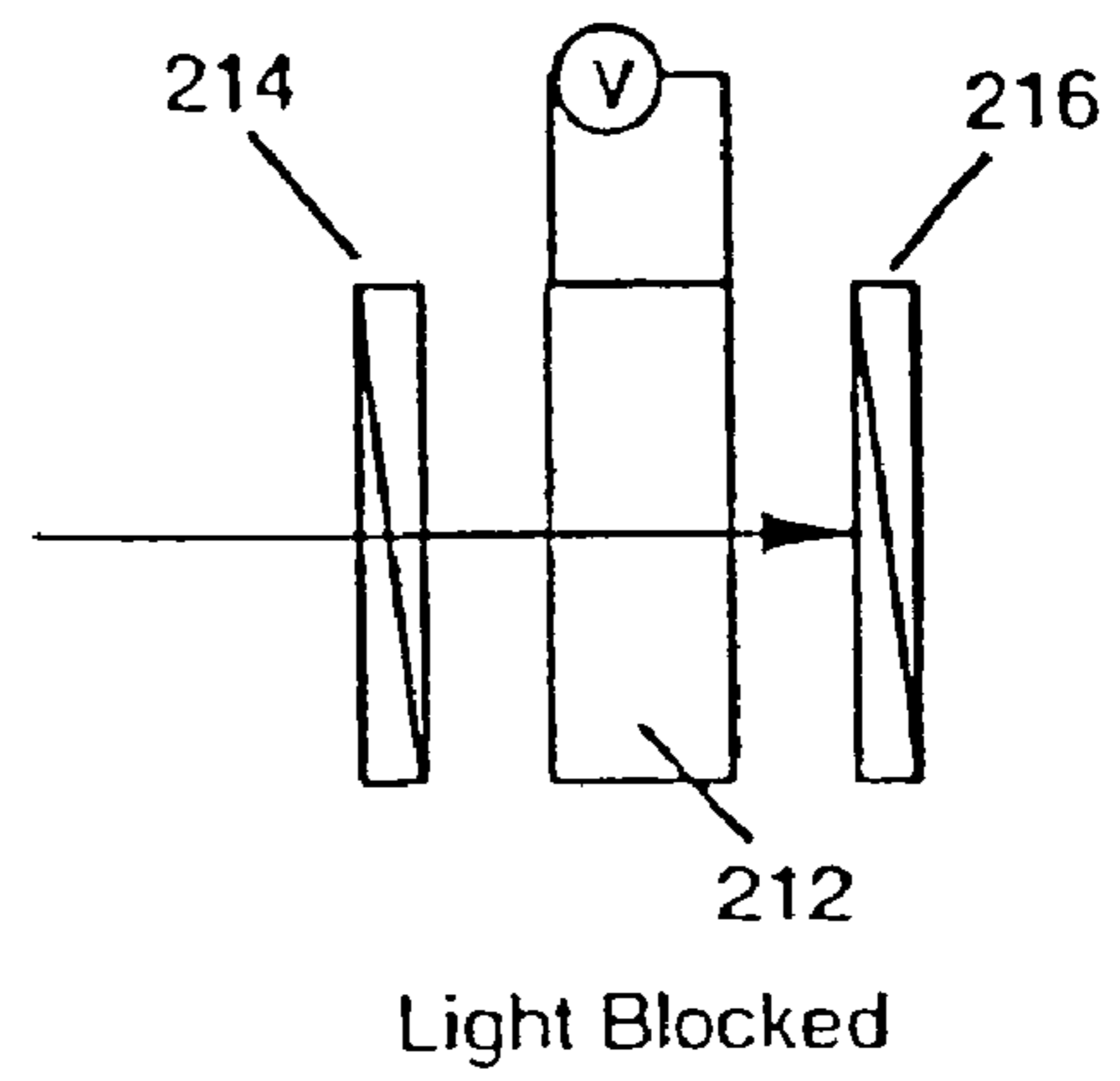


FIG. 14d

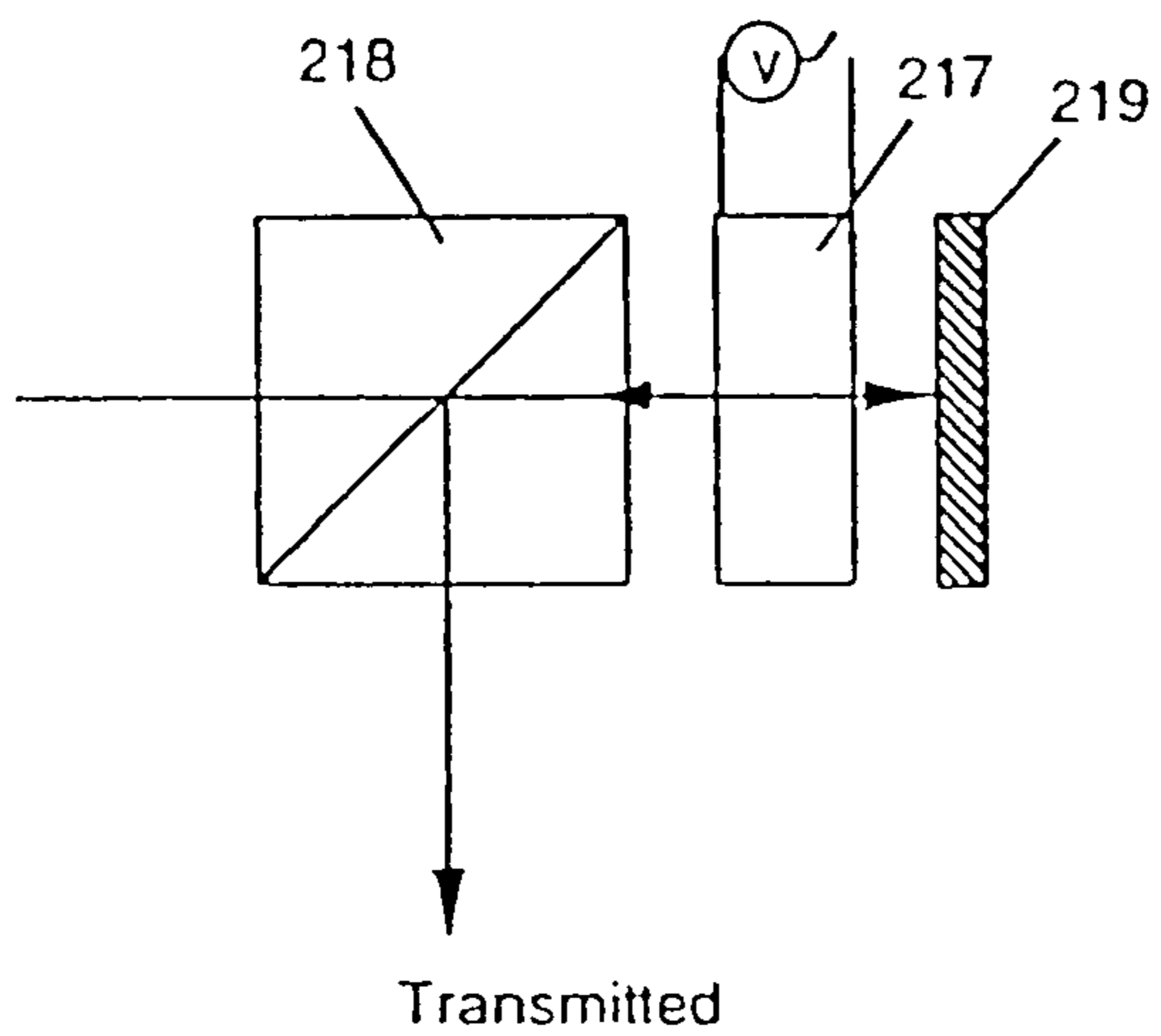


FIG. 15a

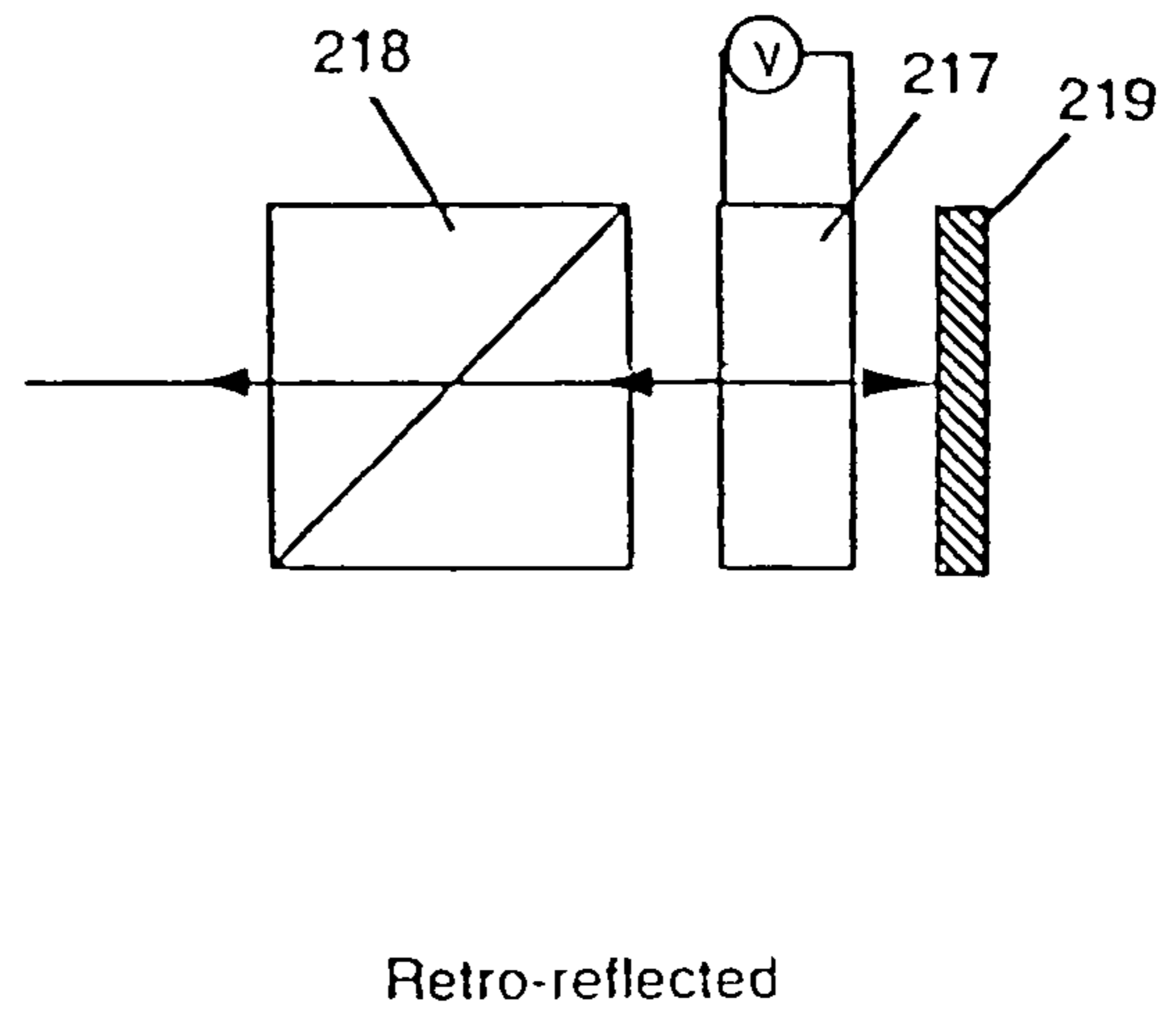
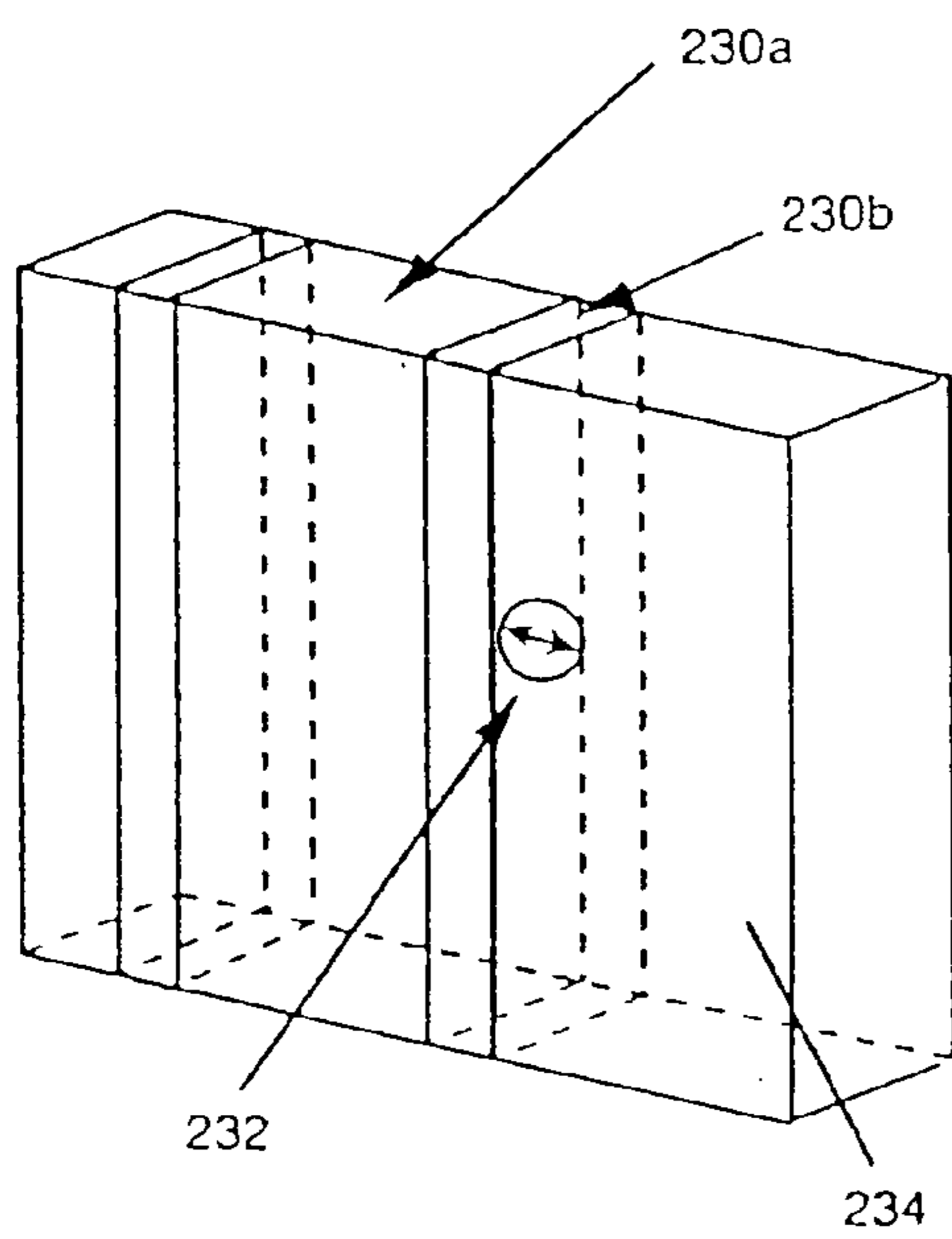
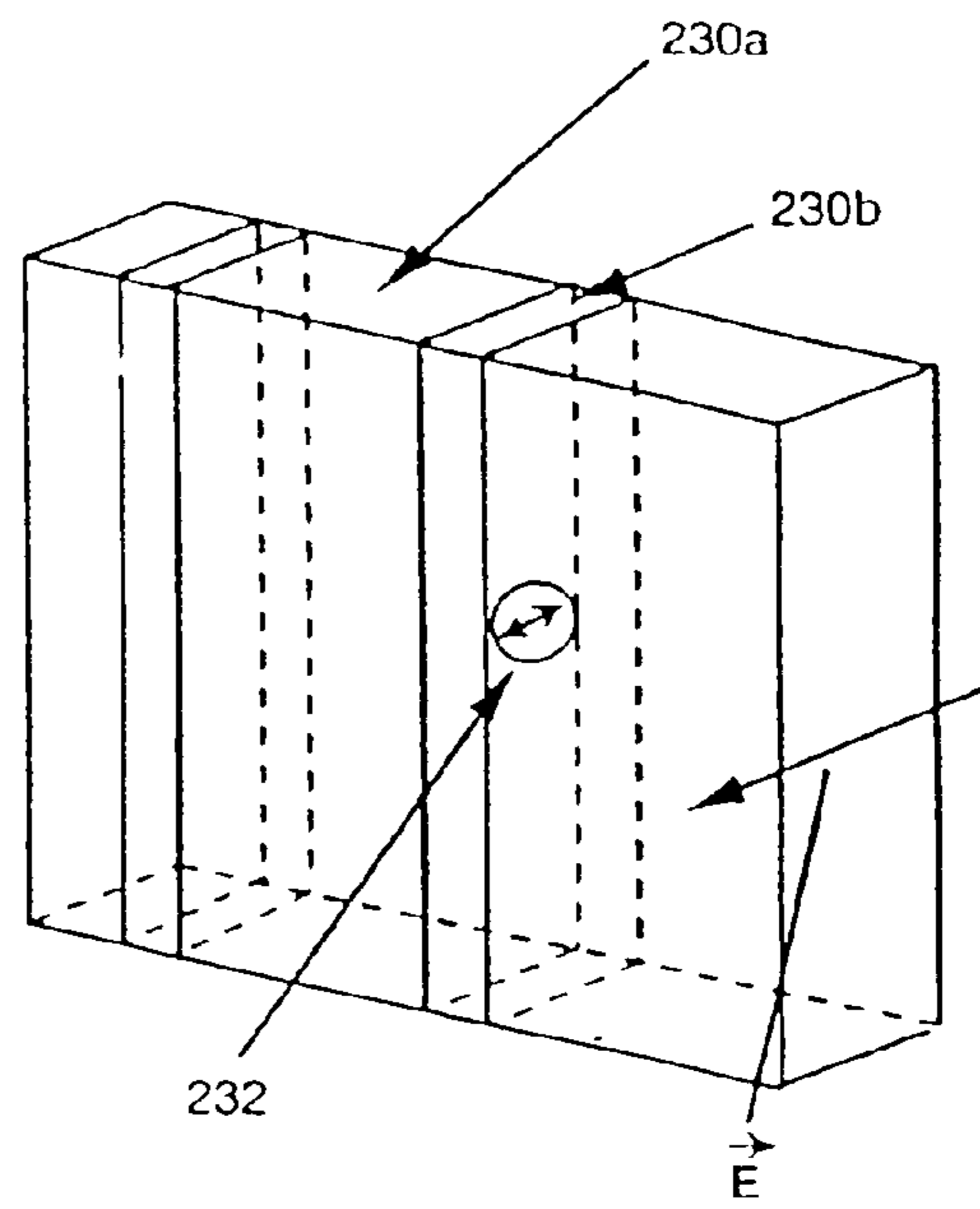


FIG. 15b



Unswitched State

FIG. 16a



Switched State

FIG. 16b

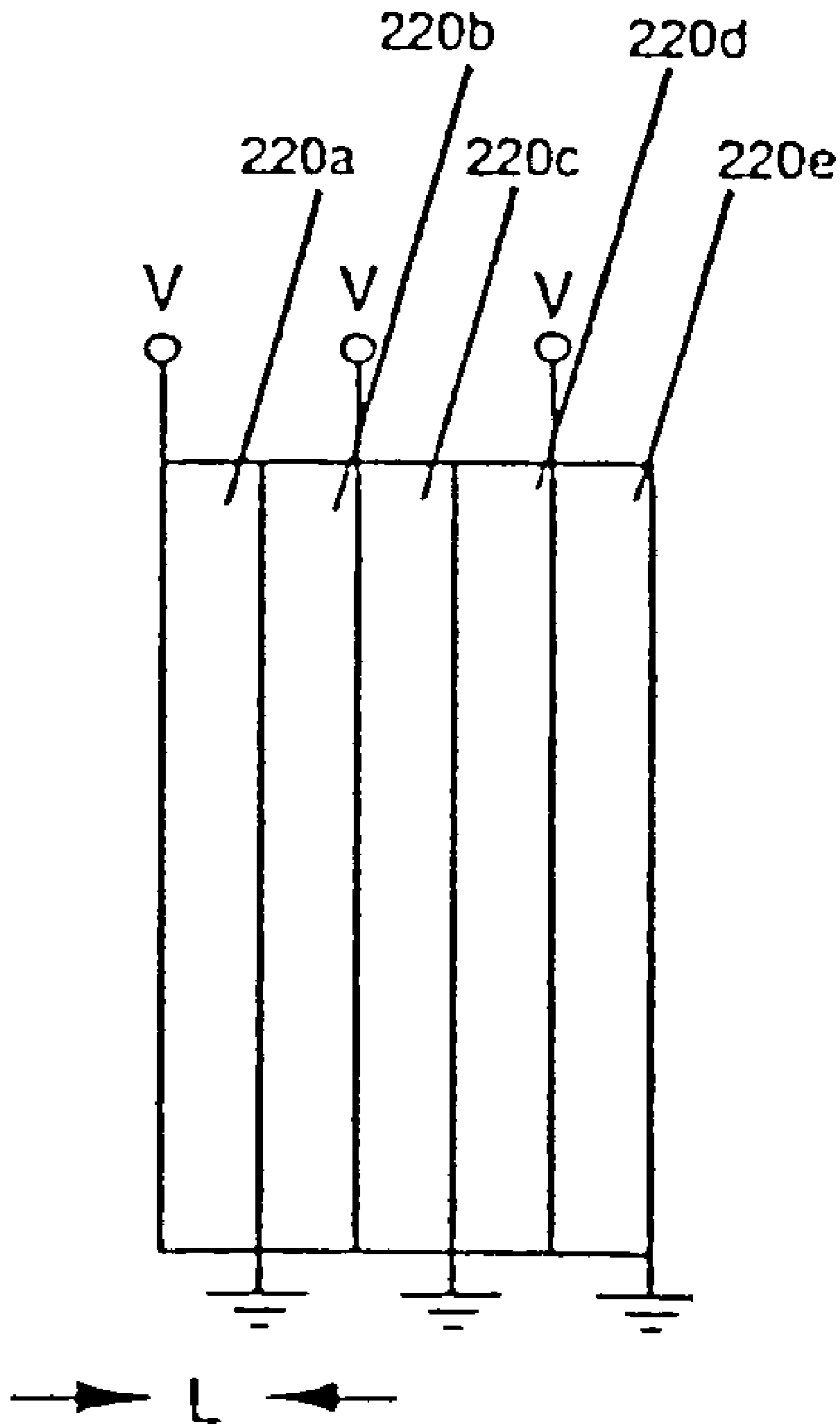


FIG. 17

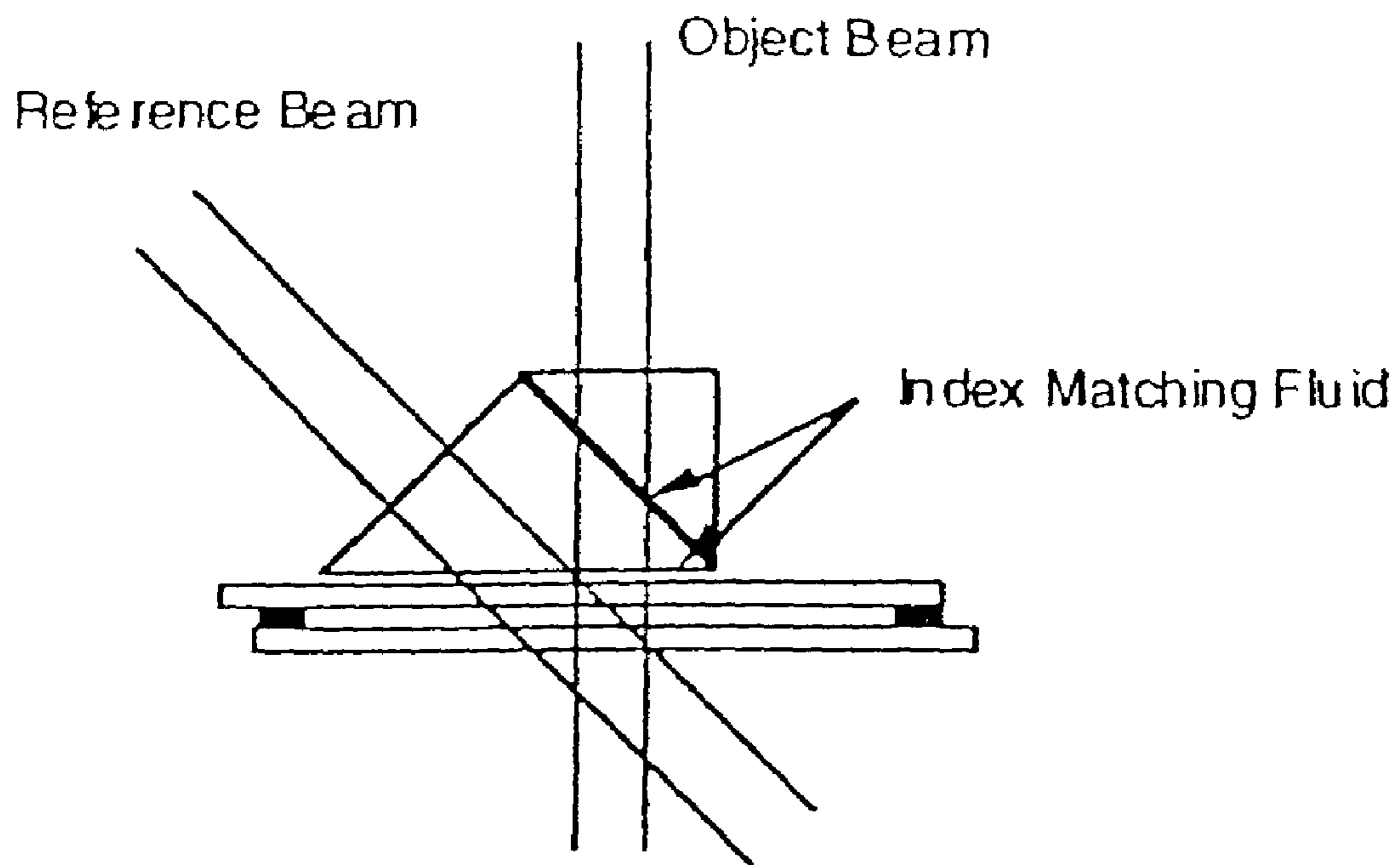


FIGURE 18

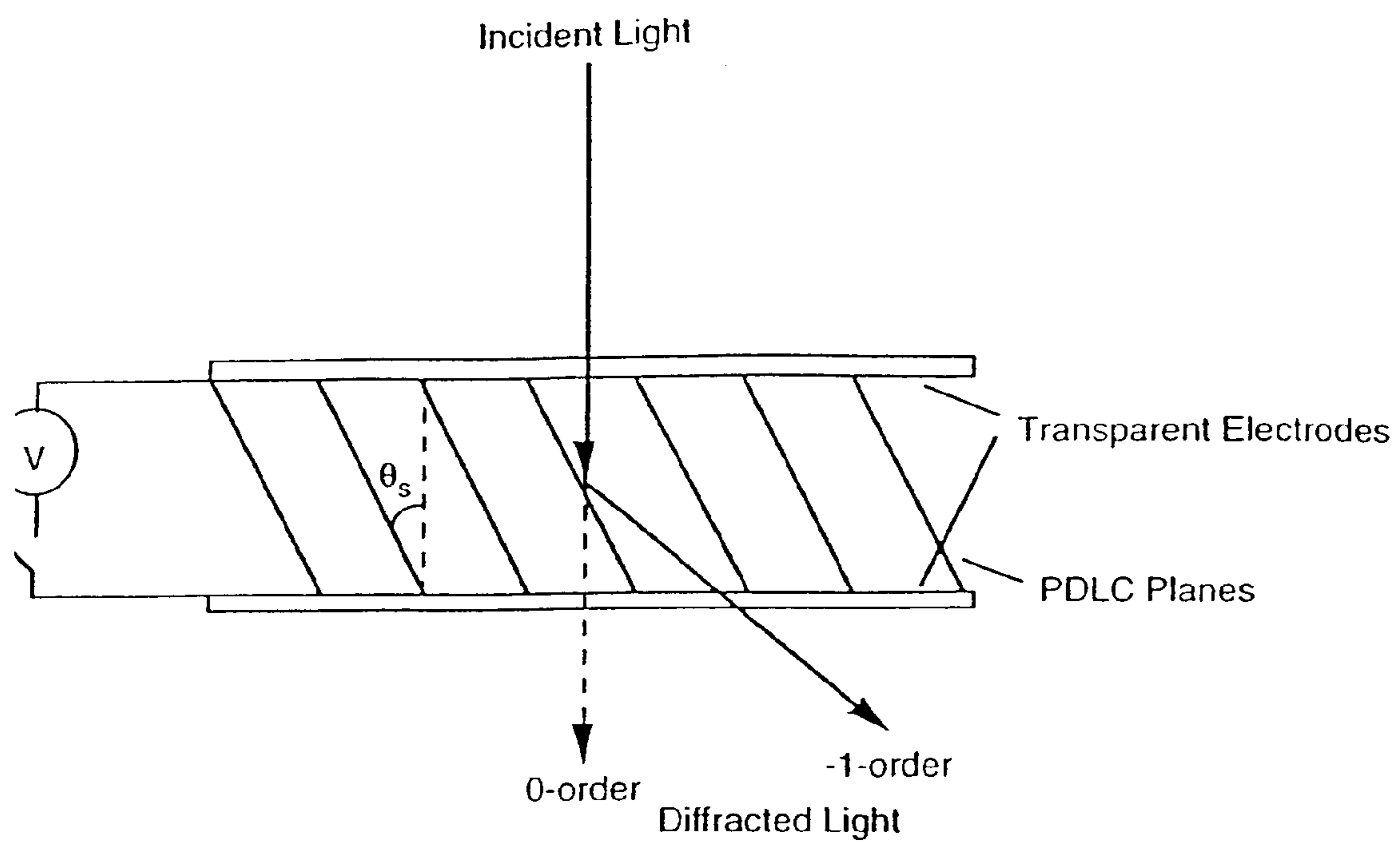


FIGURE 19

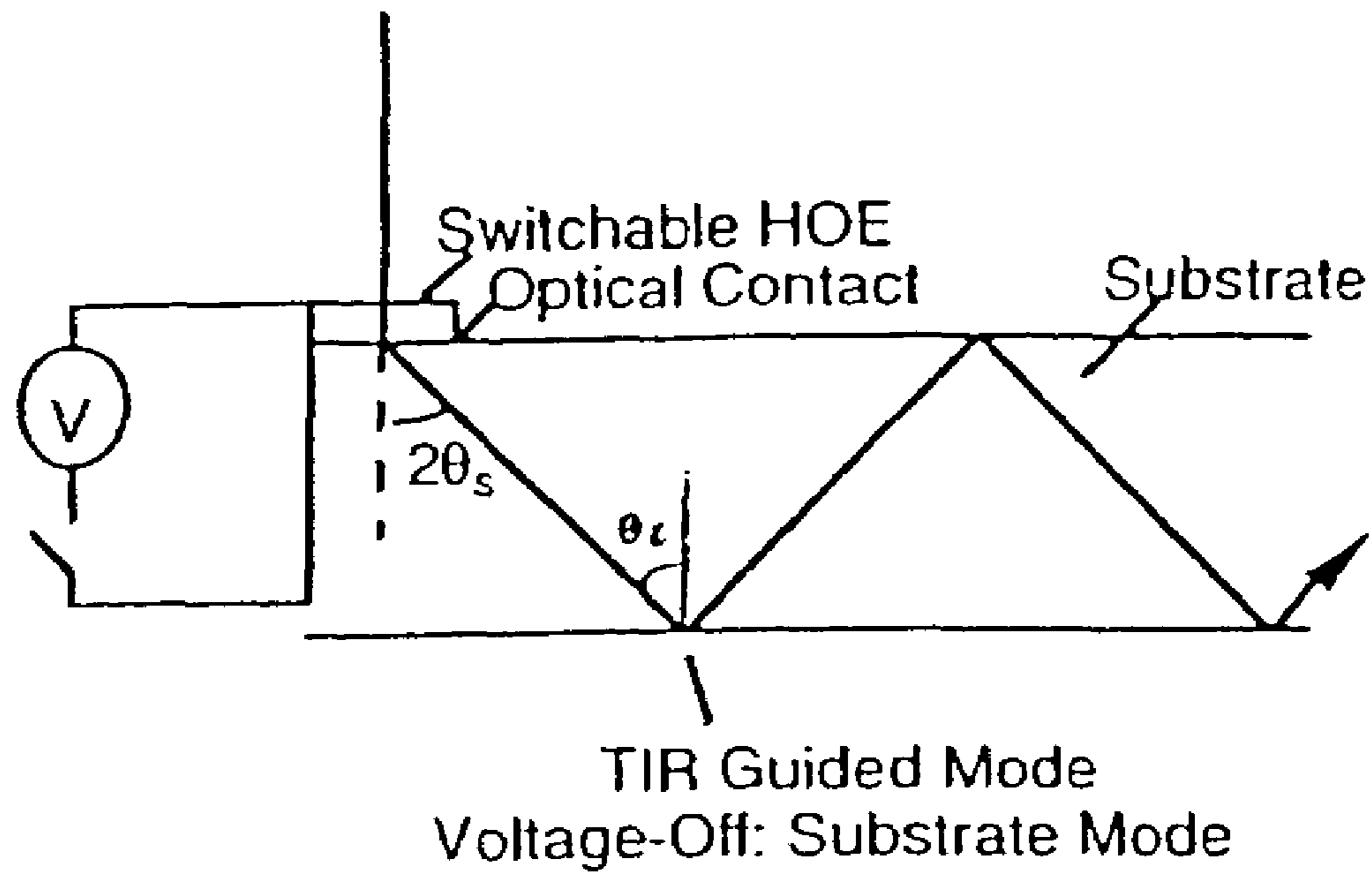


FIGURE 20

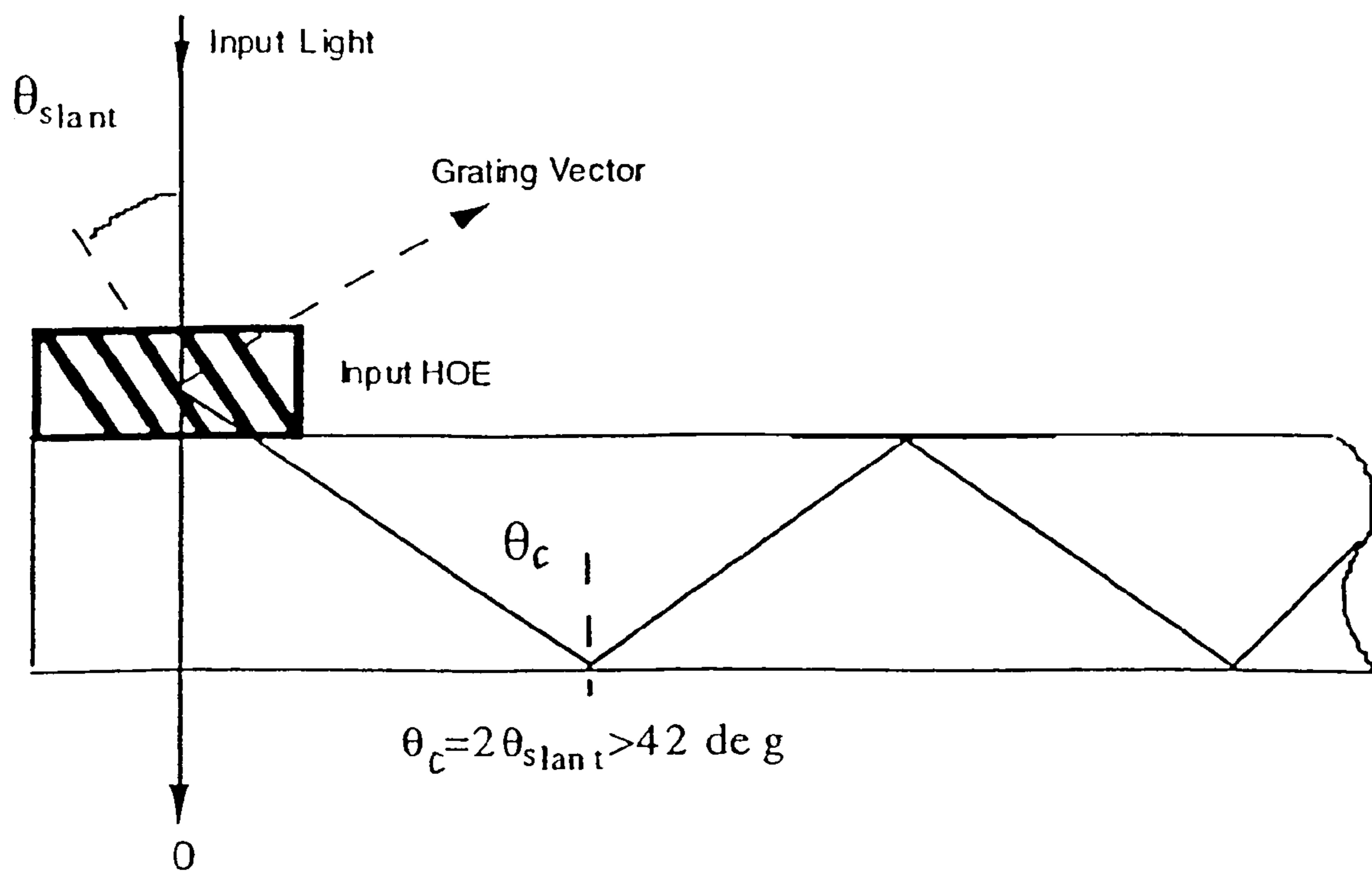
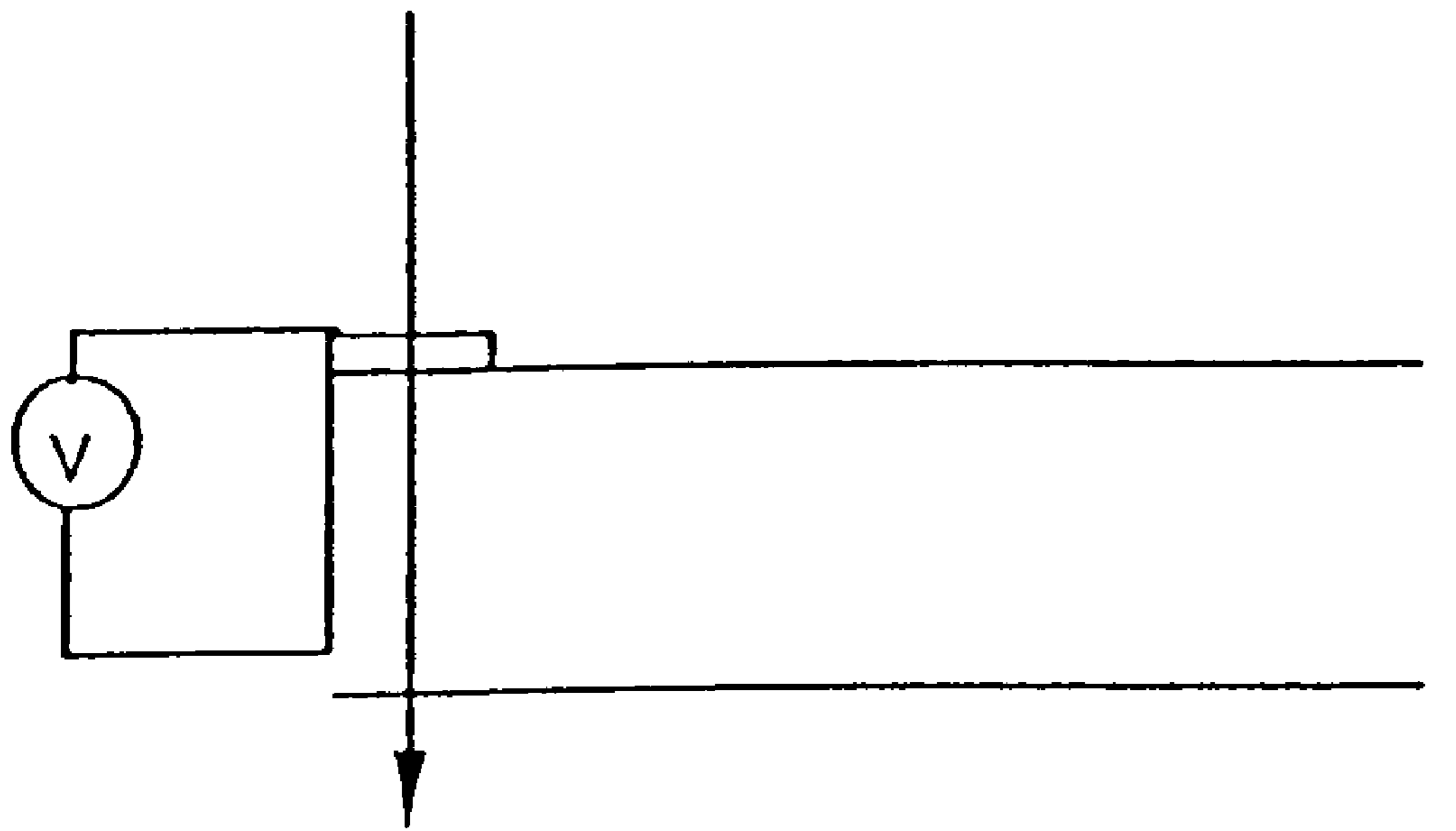
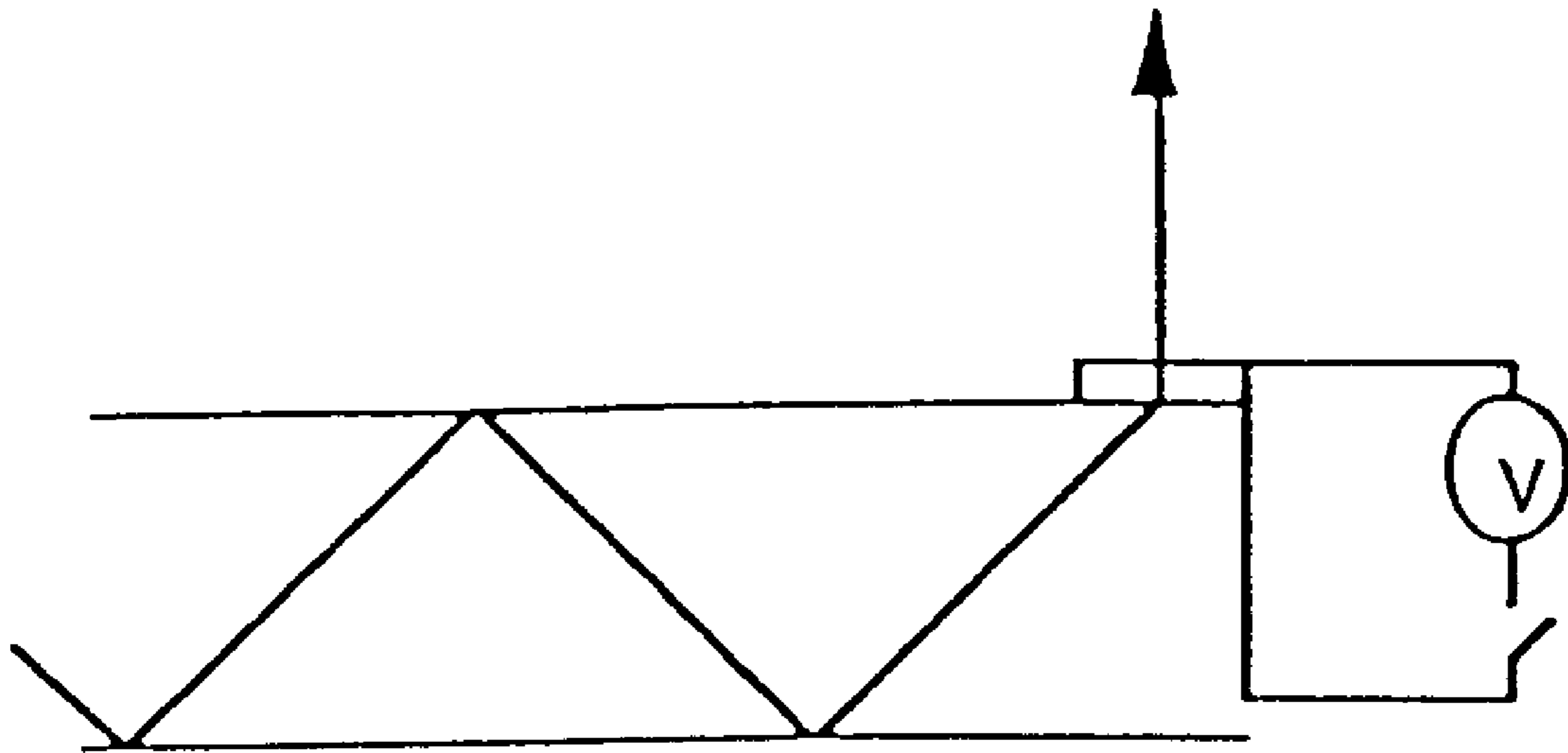


FIGURE 21



Voltage-On: Transmission Mode

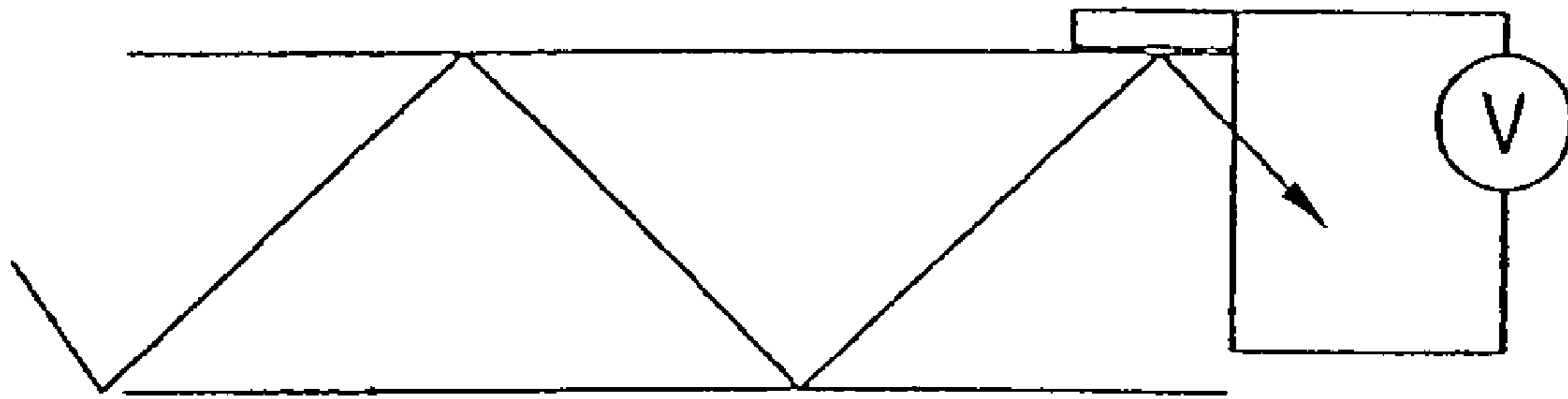
FIGURE 22



Voltage-Off: Switch-Out Mode

FIGURE 23

FIG. 24



VOLTAGE-ON: SUBSTRATE MODE

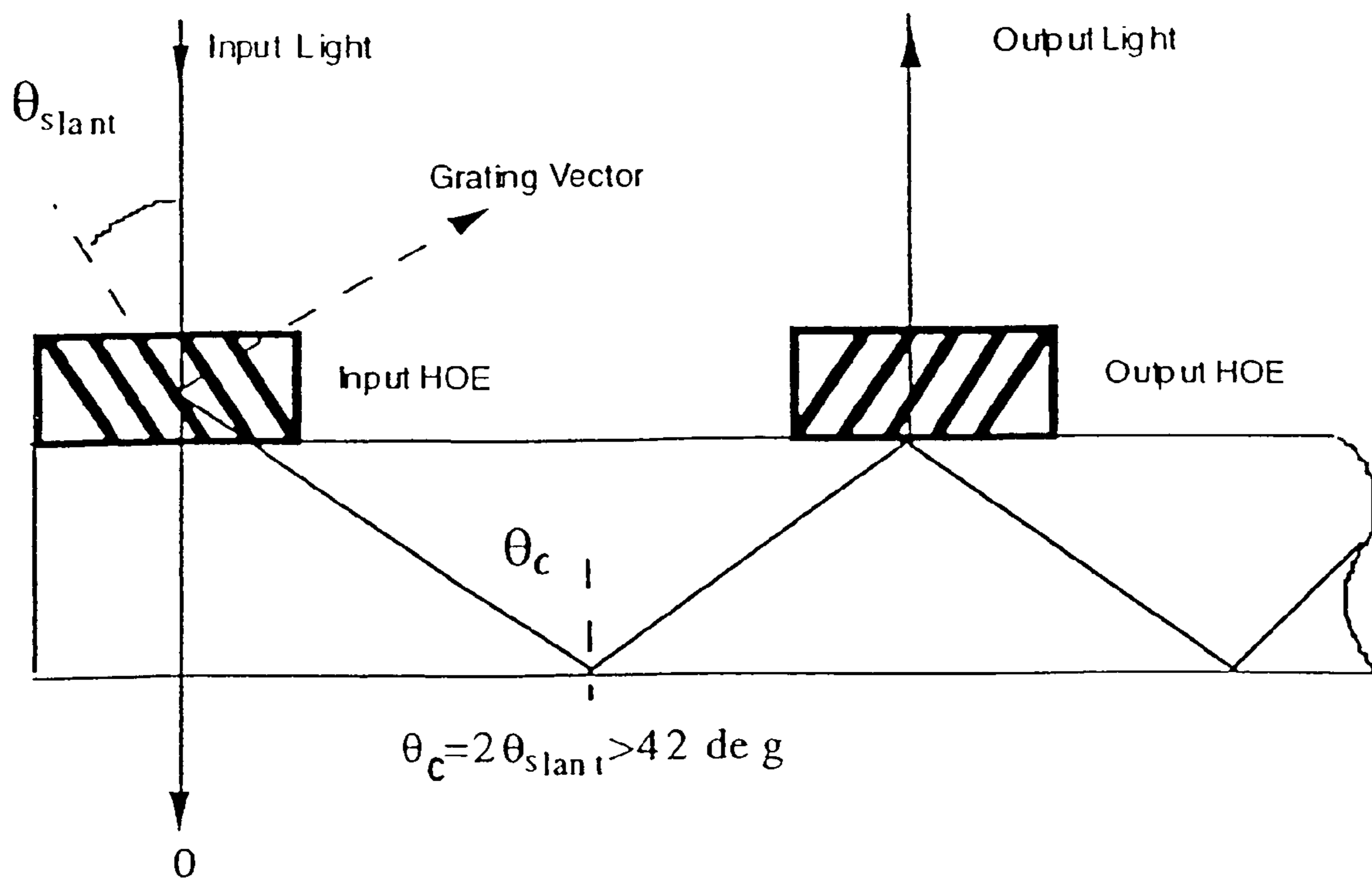


FIGURE 25

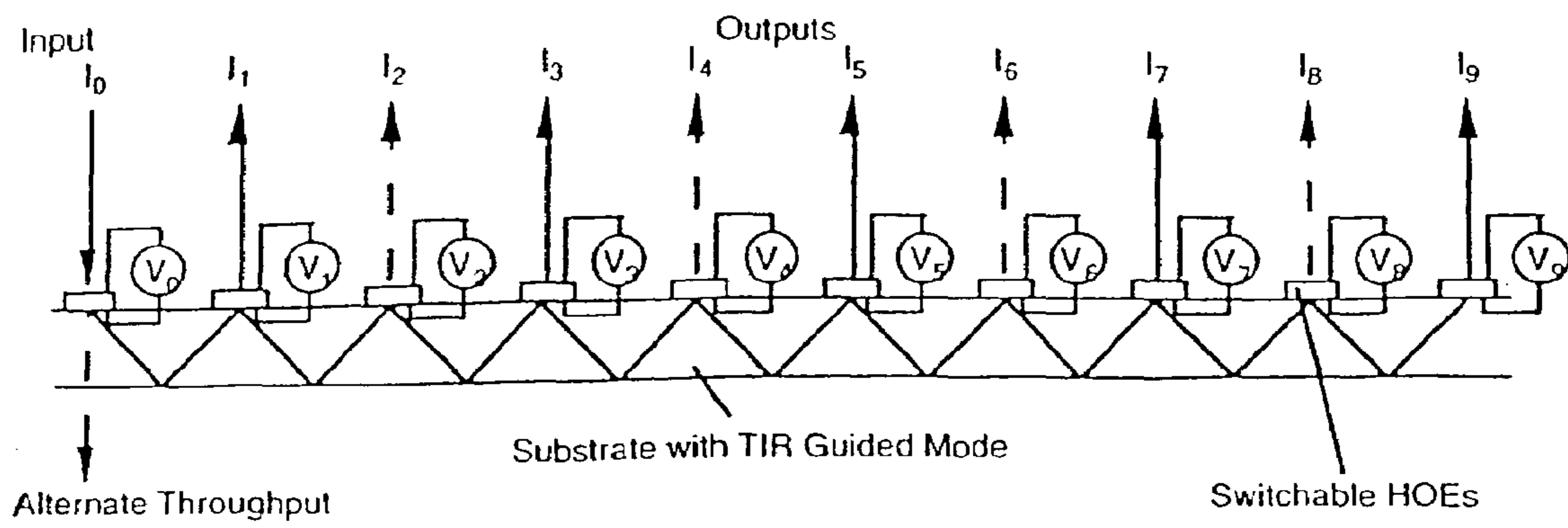


FIGURE 26

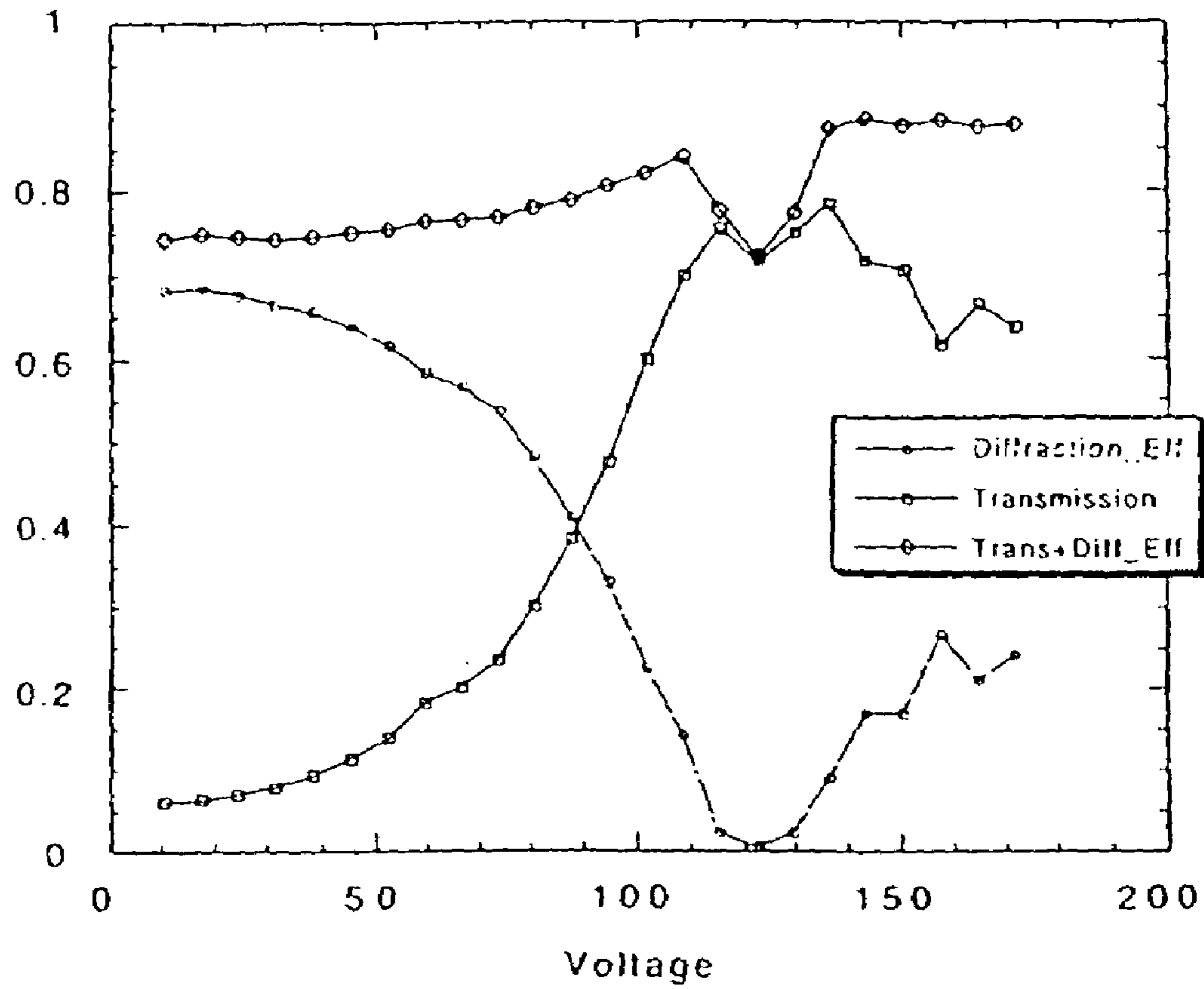


FIGURE 27

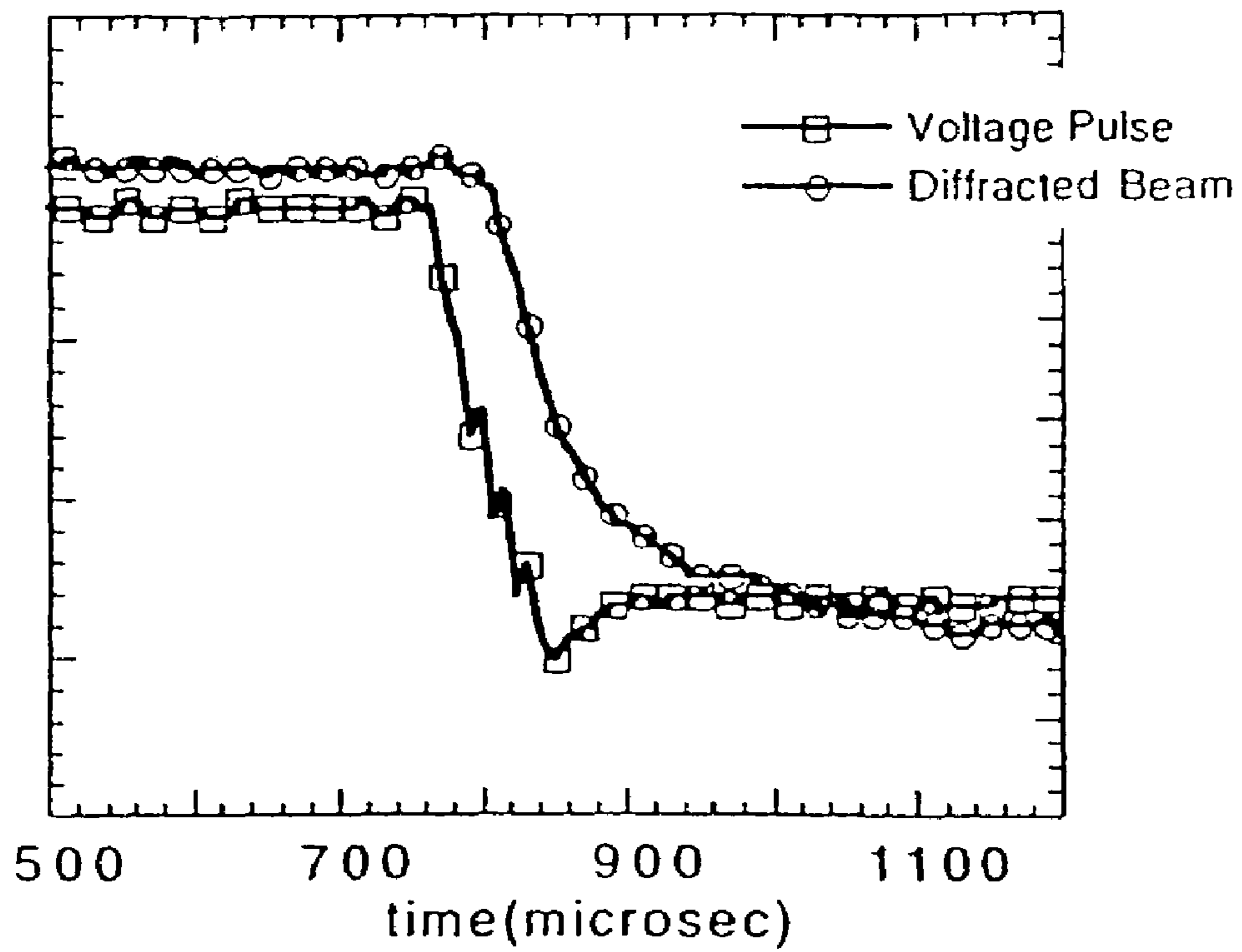


FIGURE 28

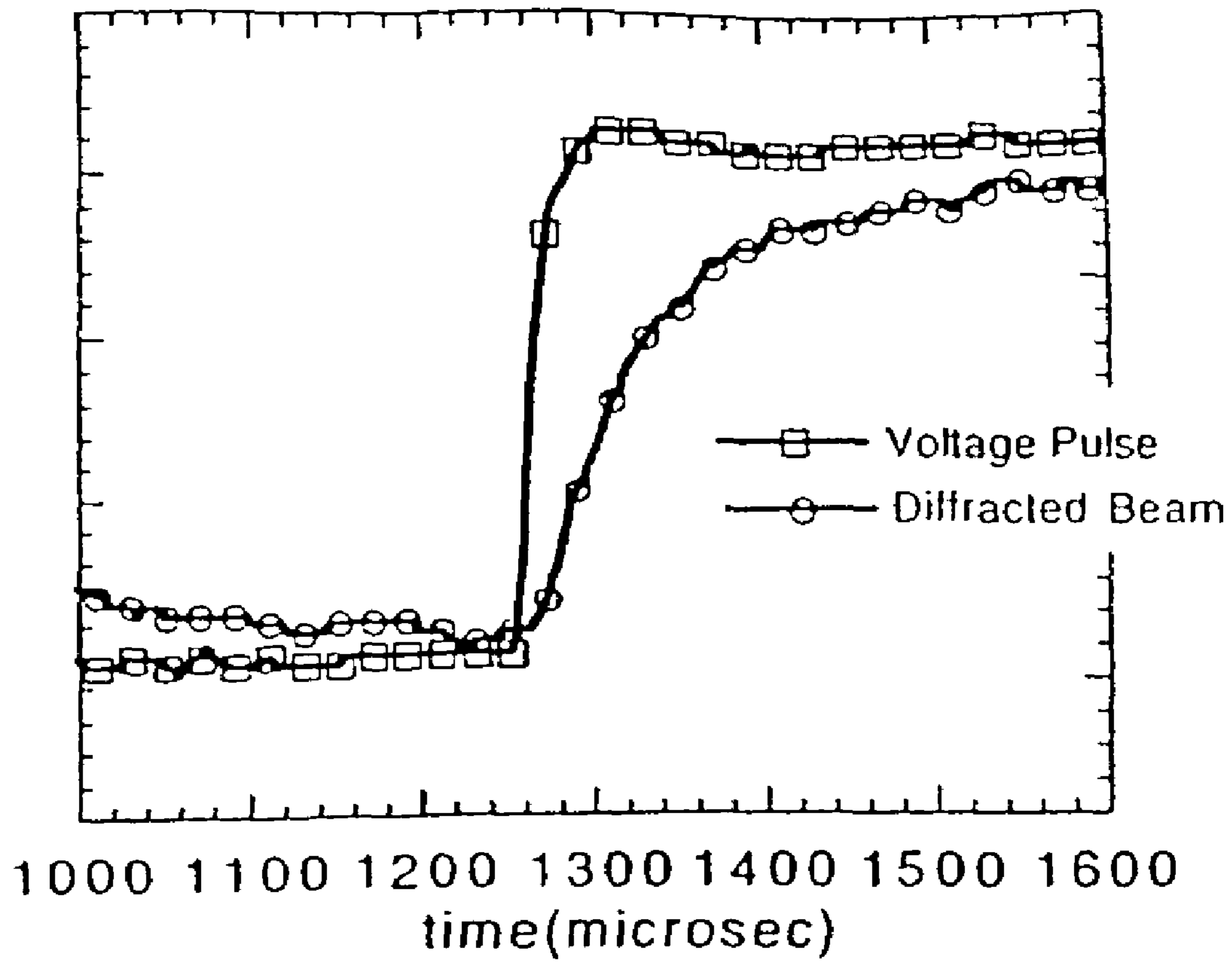


FIGURE 29

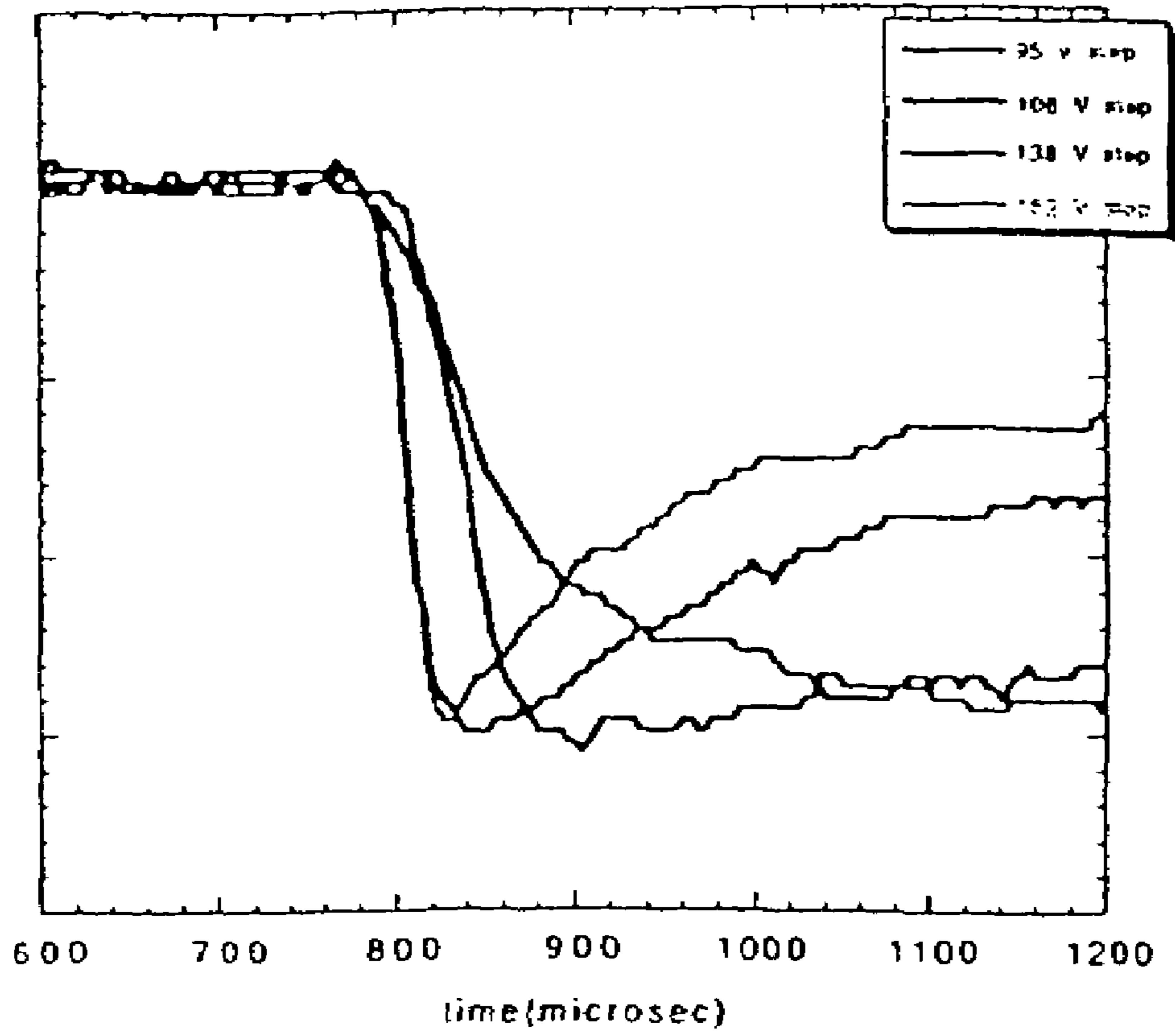


FIGURE 30

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**ELECTRICALLY SWITCHABLE
POLYMER-DISPERSED LIQUID CRYSTAL
MATERIALS INCLUDING SWITCHABLE
OPTICAL COUPLERS AND
RECONFIGURABLE OPTICAL
INTERCONNECTS**

CROSS-REFERENCE TO RELATED
APPLICATIONS

This application is a continuation of U.S. patent application Ser. No. 11/340,681, filed Jan. 27, 2006 now U.S. Pat. No. 7,198,737, which is a continuation of U.S. patent application Ser. No. 10/916,430, filed Aug. 12, 2004, issued as U.S. Pat. No. 7,081,215, which is a continuation of U.S. patent application Ser. No. 09/363,169, filed Jul. 29, 1999, issued as U.S. Pat. No. 6,821,457, which claims the benefit of U.S. Provisional Application 60/094,578, filed Jul. 29, 1998. Each of the above-identified applications is incorporated herein by reference in its entirety.

BACKGROUND OF THE INVENTION

1. Field of Invention

The present invention relates generally to electrically switchable polymer-dispersed liquid crystal holographic materials, and more specifically to switchable polymer-dispersed liquid crystal materials suitable for switchable optical coupling and reconfigurable optical interconnects.

2. Description of Related Art

Typical state-of-the-art holographic materials do not have an electro-optical nature which can be exploited for real time control of their optical properties. That is, once the hologram is fixed, its optical characteristics cannot be changed. Thus, it is seen that there is a need for materials that can record volume holograms with properties that can be electrically controlled.

Liquid crystals have long been utilized in the prior art for their ability to change their optical orientation in the presence of an electric field. Additionally, liquid crystals can dramatically increase the diffraction efficiency of a volume hologram of which they are a part. Together, these properties offer the very desirable possibility of electrically switching the diffraction efficiency of volume holograms for use in a wide variety of optical information processing and display applications.

The prior art has attempted to combine the properties of liquid crystals with holograms by a variety of methods. Unfortunately, most of these prior art devices are complex to manufacture and are not successful at offering all the advantages of volume holographic gratings.

One approach for combining the advantages of liquid crystals with volume holographic gratings has been to first make a holographic transmission grating by exposing a photopolymerizable material with a conventional two-beam apparatus for forming interference patterns inside the material. After exposure, the material is processed to produce voids where the greatest amount of exposure occurred, that is, along the grating lines, and then, in a further step, the pores are infused with liquid crystals. Unfortunately, these materials are complex to manufacture and do not offer flexibility for in situ control over liquid crystal domain size, shape, density, or ordering.

Polymer-dispersed liquid crystals (PDLCs) are formed from a homogeneous mixture of prepolymer and liquid crystals. As the polymer cures, the liquid crystals separate out as a distinct microdroplet phase. If the polymer is a photopolymer, this phase separation occurs as the prepolymer is irradiated with light. If a photopolymerizable polymer-dispersed

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liquid crystal material is irradiated with light in a suitable pattern, a holographic transmission grating can be made inside the cured polymer comprising gratings of cured polymer separated by phase-separated liquid crystals. The prior art has attempted to employ polymer-dispersed liquid crystal materials for writing volume gratings, but, despite a variety of approaches, has not been able to achieve high efficiency in the Bragg regime, high density (small grating spacing) capability, or low voltage (<100 Vrms) switching for films in the range of 15 microns thickness. The inability to make an electrically switchable volume hologram that can be switched at voltages less than 100 volts has been a particular deficiency in the prior art in that lower voltages are necessary to be compatible with conventional display and information processing technology.

It is, therefore, a principal object of the present invention to provide an improved polymer-dispersed liquid crystal system suitable for recording volume holograms.

It is a particular object of the present invention to provide a polymer-dispersed liquid crystal system that has a fast curing rate to produce small liquid crystal droplets, particularly in the range of 0.01-0.05 microns, for greater clarity of any resulting film and for writing finer gratings.

It is another object of the present invention to provide a single-step, fast holographic recording material.

It is a further object of the present invention to provide electrically switchable volume holograms that can be switched at voltages less than 100 volts.

It is also an object of the present invention to provide an improved polymer-dispersed liquid crystal system suitable for recording reflection gratings, including, in particular, switchable reflection gratings.

It is also an object of the present invention to provide an improved polymer-dispersed liquid crystal system suitable for recording subwavelength gratings, including, in particular, switchable subwavelength gratings.

These and other objects of the present invention will become apparent as the description of certain representative embodiments proceeds.

BRIEF SUMMARY OF THE INVENTION

The present invention provides a novel photopolymerizable material for single-step, fast recording of volume holograms with properties that can be electrically controlled. The unique discovery of the present invention is a new homogeneous mixture of a nematic liquid crystal and a multifunctional pentaacrylate monomer, with a photoinitiator, a coinitiator and a cross-linking agent, that accomplishes the objects of the invention, particularly the object of fast curing speed and small liquid crystal droplet size.

Accordingly, the present invention is directed to a polymer-dispersed liquid crystal ("PDLC") material, comprising the monomer dipentaerythritol hydroxypentaacrylate, a liquid crystal, a cross-linking monomer, a coinitiator and a photoinitiator dye. The polymer-dispersed liquid crystal material may optionally further comprise a surfactant. The PDLC material may be approximately 10-40 wt % of the liquid crystal. The PDLC material may be approximately 5-15 wt % of the cross-linking monomer. The amount of the coinitiator may be 10^{-3} to 10^{-4} gram moles and the amount of the photoinitiator dye may be 10^{-5} to 10^{-6} gram moles. The surfactant, when present, may be up to approximately 6 wt % of the PDLC material.

The present invention is also directed to an electrically switchable hologram, comprising a pair of transparent plates, and sandwiched between the transparent plates, a volume

hologram made by exposing an interference pattern inside a polymer-dispersed liquid crystal material, the polymer-dispersed liquid crystal material comprising, before exposure, the monomer dipentaerythritol hydroxypentaacrylate, a liquid crystal, a cross-linking monomer, a coinitiator and a photoinitiator dye. The electrically switchable hologram may optionally further comprise a surfactant.

The present invention is additionally directed to a method for reducing the switching voltage needed to switch the optical orientation of liquid crystals in a polymer-dispersed liquid crystal material, comprising the step of using alternating current switching voltage frequencies greater than 1000 Hz.

The present invention is additionally directed to a switchable slanted transmission grating comprising a polymer-dispersed liquid crystal material disposed between at least two optically transparent electrode plates, wherein the polymer-dispersed liquid crystal material is constructed by exposing to light in an interference pattern a mixture comprising, before exposure: (a) a polymerizable monomer comprising at least one acrylate; (b) at least one liquid crystal; (c) a chain-extending monomer; (d) a coinitiator; and (e) a photoinitiator.

The present invention is additionally directed to an optical coupling device comprising: at least one switchable slanted transmission grating and at least one voltage source associated with said switchable slanted transmission grating.

The present invention is additionally directed to a method for preparing a switchable slanted transmission grating, comprising: disposing between at least two optically transparent electrode plates a mixture that comprises, before exposure: (a) a polymerizable monomer comprising at least one acrylate; (b) a liquid crystal; (c) a chain-extending monomer; (d) a coinitiator; and (e) a photoinitiator; and exposing this mixture to light in an interference pattern.

The present invention is additionally directed to a method for preparing an optical coupling device comprising constructing a switchable slanted transmission grating, and electrically connecting said optically transparent electrodes to a voltage source.

It is a feature of the present invention that a very clear and orderly separation of liquid crystal from cured polymer results, so as to produce high quality holographic transmission gratings. The prior art has achieved generally only a distribution of large and small liquid crystal domains and not the clear, orderly separation made possible by the present invention.

It is also a feature of the present invention that volume Bragg gratings with small grating spacings (approximately 4,000 lines per mm) can be recorded.

It is another feature of the present invention that in situ control of domain size, shape, density, and ordering is allowed.

It is yet another feature of the present invention that holograms can be recorded using conventional optical equipment and techniques.

It is a further feature of the present invention that a unique photopolymerizable prepolymer material is employed. This unique material can be used to record holograms in a single step.

It is also a feature of the present invention that the PDLC material has an anisotropic spatial distribution of phase-separated liquid crystal droplets within a photochemically-cured polymer matrix.

It is an advantage of the present invention that single-step recording is nearly immediate and requires no later development or further processing.

It is another advantage of the present invention that uses thereof are not limited to transmission gratings, but can be

extended to other holograms such as optical storage devices and reflection and transmission pictorial holograms.

It is also an advantage that, unlike holograms made with conventional photograph-type films or dichromated gels, holograms in accordance with the present invention can be exposed in a one-step process that requires little or no further processing.

It is a further advantage of the present invention that reflection, transmission and pictorial holograms made using the teachings provided herein can be switched on and off.

It is also an advantage of the present invention that switchable reflection gratings can be formed using positive and negative dielectric anisotropy liquid crystals.

These and other features and advantages of the present invention will become apparent as the description of certain representative embodiments proceeds.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWINGS

The present invention will be more clearly understood from a reading of the following detailed description in conjunction with the accompanying figures wherein:

FIG. 1 is a cross-sectional view of an electrically switchable hologram made of an exposed polymer-dispersed liquid crystal material according to the teachings of the present invention;

FIG. 2 is a graph of the normalized net transmittance and normalized net diffraction efficiency of a hologram made according to the teachings of the present invention (without the addition of a surfactant) versus the rms voltage applied across the hologram;

FIG. 3 is a graph of both the threshold and complete switching rms voltages needed for switching a hologram made according to the teachings of the present invention to minimum diffraction efficiency versus the frequency of the rms voltage;

FIG. 4 is a graph of the normalized diffraction efficiency as a function of the applied electric field for a PDLC material formed with 34% by weight liquid crystal surfactant present and a PDLC material formed with 29% by weight liquid crystal and 4% by weight surfactant;

FIG. 5 is a graph showing the switching response time data for the diffracted beam in the surfactant-containing PDLC material in FIG. 5;

FIG. 6 is a graph of the normalized net transmittance and the normalized net diffraction efficiency of a hologram made according to the teachings of the present invention versus temperature;

FIG. 7 is an elevational view of a typical experimental arrangement for recording reflection gratings;

FIGS. 8a and 8b are elevational views of a reflection grating in accordance with the present invention having periodic planes of polymer channels and PDLC channels disposed parallel to the front surface in the absence of a field (FIG. 8a) and with an electric field applied (FIG. 8b) wherein the liquid crystal utilized in the formation of the grating has a positive dielectric anisotropy;

FIGS. 9a and 9b are elevational views of a reflection grating in accordance with the invention having periodic planes of polymer channels and PDLC channels disposed parallel to the front surface of the grating in the absence of an electric field (FIG. 9a) and with an electric field applied (FIG. 9b) wherein the liquid crystal utilized in the formation of the grating has a negative dielectric anisotropy;

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FIG. 10a is an elevational view of a reflection grating in accordance with the invention disposed within a magnetic field generated by Helmholtz coils;

FIGS. 10b and 10c are elevational views of the reflection grating of FIG. 10a in the absence of an electric field (FIG. 10b) and with an electric field applied (FIG. 10c);

FIGS. 11a and 11b are representative side views of a slanted transmission grating (FIG. 11a) and a slanted reflection grating (FIG. 11b) showing the orientation of the grating vector G of the periodic planes of polymer channels and PDLC channels;

FIG. 12 is an elevational view of a reflection grating formed in accordance with the invention while a shear stress field is applied;

FIG. 13 is an elevational view of a subwavelength grating in accordance with the present invention having periodic planes of polymer channels and PDLC channels disposed perpendicular to the front surface of the grating;

FIG. 14a is an elevational view of a switchable subwavelength grating in accordance with the present invention wherein the subwavelength grating functions as a half wave plate whereby the polarization of the incident radiation is rotated by 90° ;

FIG. 14b is an elevational view of the switchable half wave plate shown in FIG. 14a disposed between crossed polarizers whereby the incident light is transmitted;

FIGS. 14c and 14d are side views of the switchable half wave plate and crossed polarizers shown in FIG. 14b showing the effect of the application of a voltage to the plate whereby the polarization of the light is no longer rotated and thus blocked by the second polarizer;

FIG. 15a is a side view of a switchable subwavelength grating in accordance with the invention wherein the subwavelength grating functions as a quarter wave plate whereby plane polarized light is transmitted through the subwavelength grating, retroreflected by a mirror and reflected by the beam splitter;

FIG. 15b is a side view of the switchable subwavelength grating of FIG. 15a showing the effect of the application of a voltage to the plate whereby the polarization of the light is no longer modified, thereby permitting the reflected light to pass through the beam splitter;

FIGS. 16a and 16b are elevational views of a subwavelength grating in accordance with the present invention having periodic planes of polymer channels and PDLC channels disposed perpendicular to the front face of the grating in the absence of an electrical field (FIG. 16a) and with an electric field applied (FIG. 16b) wherein the liquid crystal utilized in formation of the grating has a positive dielectric anisotropy;

FIG. 17 is a side view of five subwavelength gratings wherein the gratings are stacked and connected electrically in parallel thereby reducing the switching voltage of the subwavelength grating;

FIG. 18 is a cross sectional view of the prism system and geometric arrangement for forming highly slanted transmission gratings in accordance with the present invention;

FIG. 19 is a cross sectional view of a switchable highly slanted transmission grating in accordance with the present invention;

FIG. 20 is a representative side view of a switchable highly slanted transmission grating coupled to a substrate in the absence of an applied field;

FIG. 21 is a representative side view of a switchable highly slanted transmission grating coupled as an input to a substrate;

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FIG. 22 is a representative side view of a switchable highly slanted transmission grating coupled as an input to a substrate in the presence of an applied field;

FIG. 23 is a representative side view of a switchable highly slanted transmission grating coupled as an output to a substrate in the absence of an applied field;

FIG. 24 is a representative side view of a highly slanted transmission grating coupled as an output to a substrate in the presence of an applied field;

FIG. 25 is a representative side view of a first highly slanted transmission grating coupled as an input to a substrate and a second highly slanted transmission grating coupled as an output to a substrate;

FIG. 26 is a representative side view of a selectively adjustable and reconfigurable one-to-many fan-out optical interconnect in accordance with the present invention;

FIG. 27 is a graph of the electrical switching of a highly slanted transmission grating;

FIG. 28 is a graph of the electrical switching time response of a highly slanted grating for a 97V step voltage;

FIG. 29 is a graph of the relaxation of a slanted grating when a switching field of 97 V step voltage was turned off; and

FIG. 30 is a graph of the time response of a slanted grating with higher switching voltages.

DETAILED DESCRIPTION OF THE INVENTION

In accordance with the present invention there is provided a polymer-dispersed liquid crystal ("PDLC") material comprising a monomer, a dispersed liquid crystal, a cross-linking monomer, a coinitiator and a photoinitiator dye. These PDLC materials exhibit clear and orderly separation of the liquid crystal and cured polymer, whereby the PDLC material advantageously provides high quality holographic gratings. The PDLC materials of the present invention are also advantageously formed in a single step. The present invention also utilizes a unique photopolymerizable prepolymer material that permits in situ control over characteristics of the resulting gratings, such as domain size, shape, density, ordering, and the like. Furthermore, methods and materials of the present invention can be used to prepare PDLC materials that function as switchable transmission or reflection gratings.

Polymer-dispersed liquid crystal materials, methods, and devices contemplated for use in the practice of the present invention are also described in R. L. Sutherland et al., "Bragg Gratings in an Acrylate Polymer Consisting of Periodic Polymer-Dispersed Liquid-Crystal Planes," *Chemistry of Materials*, No. 5, pp. 1533-1538 (1993); in R. L. Sutherland et al., "Electrically switchable volume gratings in polymer-dispersed liquid crystals," *Applied Physics Letters*, Vol. 64, No. 9, pp. 1074-1076 (1994); and T. J. Bunning et al., "The Morphology and Performance of Holographic Transmission Gratings Recorded in Polymer-Dispersed Liquid Crystals," *Polymer*, Vol. 36, No. 14, pp. 2699-2708 (1995), G. S. Iannacchino, et al., *Europhys. Lett.* 36, 425 (1996); and V. P. Tondiglia, et al. *Opt. Lett.* 20, pp. 1325-1327 (1995) all of which are fully incorporated by reference into this Detailed Description of the Invention. Copending patent application Ser. Nos. 08/273,436 and 08/273,437, Sutherland et al., titled "Switchable Volume Hologram Materials and Devices," and "Laser Wavelength Detection and Energy Dosimetry Badge," respectively, include background material on the formation of transmission gratings inside volume holograms. Reference is also made to copending application Ser. Nos. 09/033,513, 09/033,512, 09/033,514 and 09/034,014, also incorporated herein.

The process by which a hologram is formed according to the invention is controlled primarily by the choice of components used to prepare the homogeneous starting mixture, and to a lesser extent by the intensity of the incident light pattern. The preferred polymer-dispersed liquid crystal ("PDLC") material employed in the practice of the present invention creates a switchable hologram in a single step. A new feature of the preferred PDLC material is that illumination by an inhomogeneous, coherent light pattern initiates a patterned, anisotropic diffusion (or counter diffusion) of polymerizable monomer and second phase material, particularly liquid crystal ("LC") for this application. Thus, alternating well-defined channels of second phase-rich material, separated by well-defined channels of nearly pure polymer, are produced in a single-step process.

The resulting preferred PDLC material has an anisotropic spatial distribution of phase-separated LC droplets within the photochemically cured polymer matrix. Prior art PDLC materials made by a single-step process can achieve at best only regions of larger LC bubbles and smaller LC bubbles in a polymer matrix. The large bubble sizes are highly scattering which produces a hazy appearance and multiple order diffractions, in contrast to the well-defined first order diffraction and zero order diffraction made possible by the small LC bubbles of the preferred PDLC material in well-defined channels of LC-rich material. Reasonably well-defined alternately LC-rich channels and nearly pure polymer channels in a PDLC material are possible by multi-step processes, but such processes do not achieve the precise morphology control over LC droplet size and distribution of sizes and widths of the polymer and LC-rich channels made possible by the preferred PDLC material.

The sample is prepared by coating the mixture between two indium-tin-oxide (ITO) coated glass slides separated by spacers of nominally 10-20 μm thickness. The sample is placed in a conventional holographic recording setup. Gratings are typically recorded using the 488 nm line of an argon ion laser with intensities of between about 0.1-100 mW/cm^2 and typical exposure times of 30-120 seconds. The angle between the two beams is varied to vary the spacing of the intensity peaks, and hence the resulting grating spacing of the hologram. Photopolymerization is induced by the optical intensity pattern. A more detailed discussion of an exemplary recording apparatus can be found in R. L. Sutherland, et al., "Switchable Holograms in New Photopolymer-Liquid Crystal Composite Materials," Society of Photo-Optical Instrumentation Engineers (SPIE), Proceedings Reprint, Volume 2404, reprinted from *Diffraction and Holographic Optics Technology II* (1995), incorporated herein by reference.

The features of the PDLC material are influenced by the components used in the preparation of the homogeneous starting mixture and, to a lesser extent, by the intensity of the incident light pattern. In a preferred embodiment, the prepolymer material comprises a mixture of a photopolymerizable monomer, a second phase material, a photoinitiator dye, a coinitiator, a chain extender (or cross-linker), and, optionally, a surfactant.

In the preferred embodiment, the two major components of the prepolymer mixture are the polymerizable monomer and the second phase material, which are preferably completely miscible. Highly functionalized monomers are preferred because they form densely cross-linked networks which shrink to some extent and tend to squeeze out the second phase material. As a result, the second phase material is moved anisotropically out of the polymer region and, thereby, separated into well-defined polymer-poor, second phase-rich regions or domains. Highly functionalized monomers are also

preferred because the extensive cross-linking associated with such monomers yields fast kinetics, allowing the hologram to form relatively quickly, whereby the second phase material will exist in domains of less than approximately 0.1 μm .

Highly functionalized monomers, however, are relatively viscous. As a result, these monomers do not tend to mix well with other materials, and they are difficult to spread into thin films. Accordingly, it is preferable to utilize a mixture of pentaacrylates in combination with di-, tri-, and/or tetra-acrylates in order to optimize both the functionality and viscosity of the prepolymer material. Suitable acrylates, such as triethyleneglycol diacrylate, trimethylolpropane triacrylate, pentaerythritol triacrylate, pentaerythritol tetraacrylate, pentaerythritol pentaacrylate, and the like can be used in accordance with the present invention. In the preferred embodiment, it has been found that an approximately 1:4 mixture of tri- to pentaacrylate facilitates homogeneous mixing while providing a favorable mixture for forming 10-20 μm films on the optical plates.

The second phase material of choice for use in the practice of the present invention is a liquid crystal. This also allows an electro-optical response for the resulting hologram. The concentration of LC employed should be large enough to allow a significant phase separation to occur in the cured sample, but not so large as to make the sample opaque or very hazy. Below about 20% by weight very little phase separation occurs and diffraction efficiencies are low. Above about 35% by weight, the sample becomes highly scattering, reducing both diffraction efficiency and transmission. Samples fabricated approximately 25% by weight typically yield good diffraction efficiency and optical clarity. In prepolymer mixtures utilizing a surfactant, the concentration of LC may be increased to 35% by weight without loss in optical performance by adjusting the quantity of surfactant. Suitable liquid crystals contemplated for use in the practice of the present invention include the mixture of cyanobiphenyls marketed as E7 by Merck, 4'-n-pentyl-4-cyanobiphenyl, 4'-n-heptyl-4-cyanobiphenyl, 4'-octaoxy-4-cyanobiphenyl, 4'-pentyl-4-cyanoterphenyl, 4-methoxybenzylidene-4'-butylaniline, and the like. Other second phase components are also possible.

The preferred polymer-dispersed liquid crystal material employed in the practice of the present invention is formed from a prepolymer material that is a homogeneous mixture of a polymerizable monomer comprising dipentaerythritol hydroxypentaacrylate (available, for example, from Polysciences, Inc., Warrington, Pa.), approximately 10-40 wt % of the liquid crystal E7 (which is a mixture of cyanobiphenyls marketed as E7 by Merck and also available from BDH Chemicals, Ltd., London, England), the chain-extending monomer N-vinylpyrrolidone ("NVP") (available from the Aldrich Chemical Company, Milwaukee, Wis.), coinitiator N-phenylglycine ("NPG") (also available from the Aldrich Chemical Company, Milwaukee, Wis.), and the photoinitiator dye rose bengal ester; (2,4,5,7-tetraiodo-3',4',5',6'-tetrachlorofluorescein-6-acetate ester) marketed as RBAX by Spectra-graph, Ltd., Maumee, Ohio). Rose bengal is also available as rose bengal sodium salt (which must be esterified for solubility) from the Aldrich Chemical Company. This system has a very fast curing speed which results in the formation of small liquid crystal micro-droplets.

The mixture of liquid crystal and prepolymer material are homogenized to a viscous solution by suitable means (e.g., ultrasonification) and spread between indium-tin-oxide ("ITO") coated glass slides with spacers of nominally 15-100 μm thickness and, preferably, 10-20 μm thickness. The ITO is electrically conductive and serves as an optically transparent electrode. Preparation, mixing and transfer of the prepolymer

Thus, it is believed that semifluorinated acrylate monomers which are bifunctional and liquid crystalline will find suitable application in the present invention.

Referring now to FIG. 1 of the drawings, there is shown a cross-sectional view of an electrically switchable hologram 10 made of an exposed polymer-dispersed liquid crystal material according to the teachings of the present invention. A layer 12 of the polymer-dispersed liquid crystal material is sandwiched between a pair of indium-tin-oxide (ITO) coated glass slides 14 and spacers 16. The interior of hologram 10 shows the Bragg transmission gratings 18 formed when layer 12 was exposed to an interference pattern from two intersecting beams of coherent laser light. The exposure times and intensities can be varied depending on the diffraction efficiency and liquid crystal domain size desired. Liquid crystal domain size can be controlled by varying the concentrations of photoinitiator, cointiator and chain-extending (or cross-linking) agent. The orientation of the nematic directors can be controlled while the gratings are being recorded by application of an external electric field across the ITO electrodes.

The scanning electron micrograph shown in FIG. 2 of the referenced *Applied Physics Letters* article and incorporated herein by reference is of the surface of a grating which was recorded in a sample with a 36 wt % loading of liquid crystal using the 488 nm line of an argon ion laser at an intensity of 95 mW/cm². The size of the liquid crystal domains is about 0.2 μm and the grating spacing is about 0.54 μm. This sample, which is approximately 20 μm thick, diffracts light in the Bragg regime.

FIG. 2 is a graph of the normalized net transmittance and normalized net diffraction efficiency of a hologram made according to the teachings of the present invention versus the root mean square voltage ("V_{rms}") applied across the hologram. Δη₁ is the change in first order Bragg diffraction efficiency. ΔT is the change in zero order transmittance. FIG. 2 shows that energy is transferred from the first order beam to the zero-order beam as the voltage is increased. There is a true minimum of the diffraction efficiency at approximately 225 V_{rms}. The peak diffraction efficiency can approach 100%, depending on the wavelength and polarization of the probe beam, by appropriate adjustment of the sample thickness. The minimum diffraction efficiency can be made to approach 0% by slight adjustment of the parameters of the PDLC material to force the refractive index of the cured polymer to be equal to the ordinary refractive index of the liquid crystal.

By increasing the frequency of the applied voltage, the switching voltage for minimum diffraction efficiency can be decreased significantly. This is illustrated in FIG. 3, which is a graph of both the threshold rms voltage 20 and the complete switching rms voltage 22 needed for switching a hologram made according to the teachings of the present invention to minimum diffraction efficiency versus the frequency of the rms voltage. The threshold and complete switching rms voltages are reduced to 20 V_{rms} and 60 V_{rms}, respectively, at 10 kHz. Lower values are expected at even higher frequencies.

Smaller liquid crystal droplet sizes have the problem that it takes high switching voltages to switch their orientation. As described in the previous paragraph, using alternating current switching voltages at high frequencies helps reduce the needed switching voltage. As demonstrated in FIG. 4, another unique discovery of the present invention is that adding a surfactant (e.g., octanoic acid) to the prepolymer material in amounts of about 4%-6% by weight of the total mixture resulted in sample holograms with switching voltages near 50 V_{rms} at lower frequencies of 1-2 kHz. As shown in FIG. 5, it has also been found that the use of the surfactant with the associated reduction in droplet size, reduces the switching

time of the PDLC materials. Thus, samples made with surfactant can be switched on the order of 25-44 microseconds. Without wishing to be bound by any theory, the surfactant is believed to reduce switching voltages by reducing the anchoring of the liquid crystals at the interface between liquid crystal and cured polymer.

Thermal control of diffraction efficiency is illustrated in FIG. 6. FIG. 6 is a graph of the normalized net transmittance and normalized net diffraction efficiency of a hologram made according to the teachings of the present invention versus temperature.

The polymer-dispersed liquid crystal materials described herein successfully demonstrate the utility for recording volume holograms of a particular composition for such polymer-dispersed liquid crystal systems. Although the disclosed polymer-dispersed liquid crystal systems are specialized, the present invention will find application in other areas where a fast curing polymer and a material that can be phase-separated from the polymer will find use.

As shown in FIG. 7, a PDLC reflection grating is prepared by placing several drops of the mixture of prepolymer material 112 on an indium-tin oxide ("ITO") coated glass slide 114a. A second indium-tin oxide ("ITO") coated slide 114b is then pressed against the first, thereby causing the prepolymer material 112 to fill the region between the slides 114a and 114b. Preferably, the separation of the slides is maintained at approximately 20 μm by utilizing uniform spacers 118. Preparation, mixing and transfer of the prepolymer material is preferably done in the dark. Once assembled, a mirror 116 is placed directly behind the glass plate 114b. The distance of the mirror from the sample is preferably substantially shorter than the coherence length of the laser. The PDLC material is preferably exposed to the 488 nm line of an argon ion laser, expanded to fill the entire plane of the glass plate, with an intensity of approximately 0.1-100 mWatts/cm² with typical exposure times of 30-120 seconds. Constructive and destructive interference within the expanded beam establishes a periodic intensity profile through the thickness of the film.

In the preferred embodiment, the prepolymer material utilized to make a reflection grating comprises a monomer, a liquid crystal, a cross-linking monomer, a cointiator, and a photoinitiator dye. In the preferred embodiment, the reflection grating is formed from prepolymer material comprising by total weight of the monomer dipentaerythritol hydroxypentaacrylate ("DPHA"), 34% by total weight of a liquid crystal comprising a mixture of cyanobiphenyls (known commercially as "E7"), 10% by total weight of a cross-linking monomer comprising N-vinylpyrrolidone ("NVP"), 2.5% by weight of the cointiator N-phenylglycine ("NPG"), and 10⁻⁵ to 10⁻⁶ gram moles of a photoinitiator dye comprising rose bengal ester. Further, as with transmission gratings, the addition of surfactants is expected to facilitate the same advantageous properties discussed above in connection with transmission gratings. It is also expected that similar ranges and variation of prepolymer starting materials will find ready application in the formation of suitable reflection gratings.

It has been determined by low voltage, high resolution scanning electron microscopy ("LVHRSEM") that the resulting material comprises a fine grating with a periodicity of 165 nm with the grating vector perpendicular to the plane of the surface. Thus, as shown schematically in FIG. 8a, grating 130 includes periodic planes of polymer channels 130a and PDLC channels 130b which run parallel to the front surface 134. The grating spacing associated with these periodic planes remains relatively constant throughout the full thickness of the sample from the air/film to the film/substrate interface.

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Although interference is used to prepare both transmission and reflection gratings, the morphology of the reflection grating differs significantly. In particular, it has been determined that, unlike transmission gratings with similar liquid crystal concentrations, very little coalescence of individual droplets was evident. Furthermore, the droplets that were present in the material were significantly smaller, having diameters between 50 and 100 nm. Furthermore, unlike transmission gratings where the liquid crystal-rich regions typically comprise less than 40% of the grating, the liquid crystal-rich component of a reflection grating is significantly larger. Due to the much smaller periodicity associated with reflection gratings, i.e., a narrower grating spacing (~ 0.2 microns), it is believed that the time difference between completion of curing in high intensity versus low intensity regions is much smaller. Thus, gelation occurs more quickly and droplet growth is minimized. It is also believed that the fast polymerization, as evidenced by small droplet diameters, traps a significant percentage of the liquid crystal in the matrix during gelation and precludes any substantial growth of large droplets or diffusion of small droplets into larger domains.

Analysis of the reflection notch in the absorbance spectrum supports the conclusion that a periodic refractive index modulation is disposed through the thickness of the film. In PDLC materials that are formed with the 488 nm line of an argon ion laser, the reflection notch typically has a reflection wavelength at approximately 472 nm for normal incidence and a relatively narrow bandwidth. The small difference between the writing wavelength and the reflection wavelength (approximately 5%) indicates that shrinkage of the film is not a significant problem. Moreover, it has been found that the performance of such gratings is stable over periods of many months.

In addition to the materials utilized in the preferred embodiment described above, it is believed that suitable PDLC materials could be prepared utilizing monomers such as triethyleneglycol diacrylate, trimethylolpropanetriacrylate, pentaerythritol triacrylate, pentaerythritol tetraacrylate, pentaerythritol pentaacrylate, and the like. Similarly, other coinitiators such as triethylamine, triethanolamine, N,N-dimethyl-2,6-diisopropylaniline, and the like could be used instead of N-phenyl glycine. Where it is desirable to use the 458 nm, 476 nm, 488 nm or 514 nm lines of an argon ion laser, the photoinitiator dyes rose bengal sodium salt, eosin, eosin sodium salt, fluorescein sodium salt and the like will give favorable results. Where the 633 nm line is utilized, methylene blue will find ready application. Finally, it is believed that other liquid crystals, such as 4'-pentyl-4-cyanobiphenyl or 4'-heptyl-4-cyanobiphenyl, can be utilized in accordance with the invention.

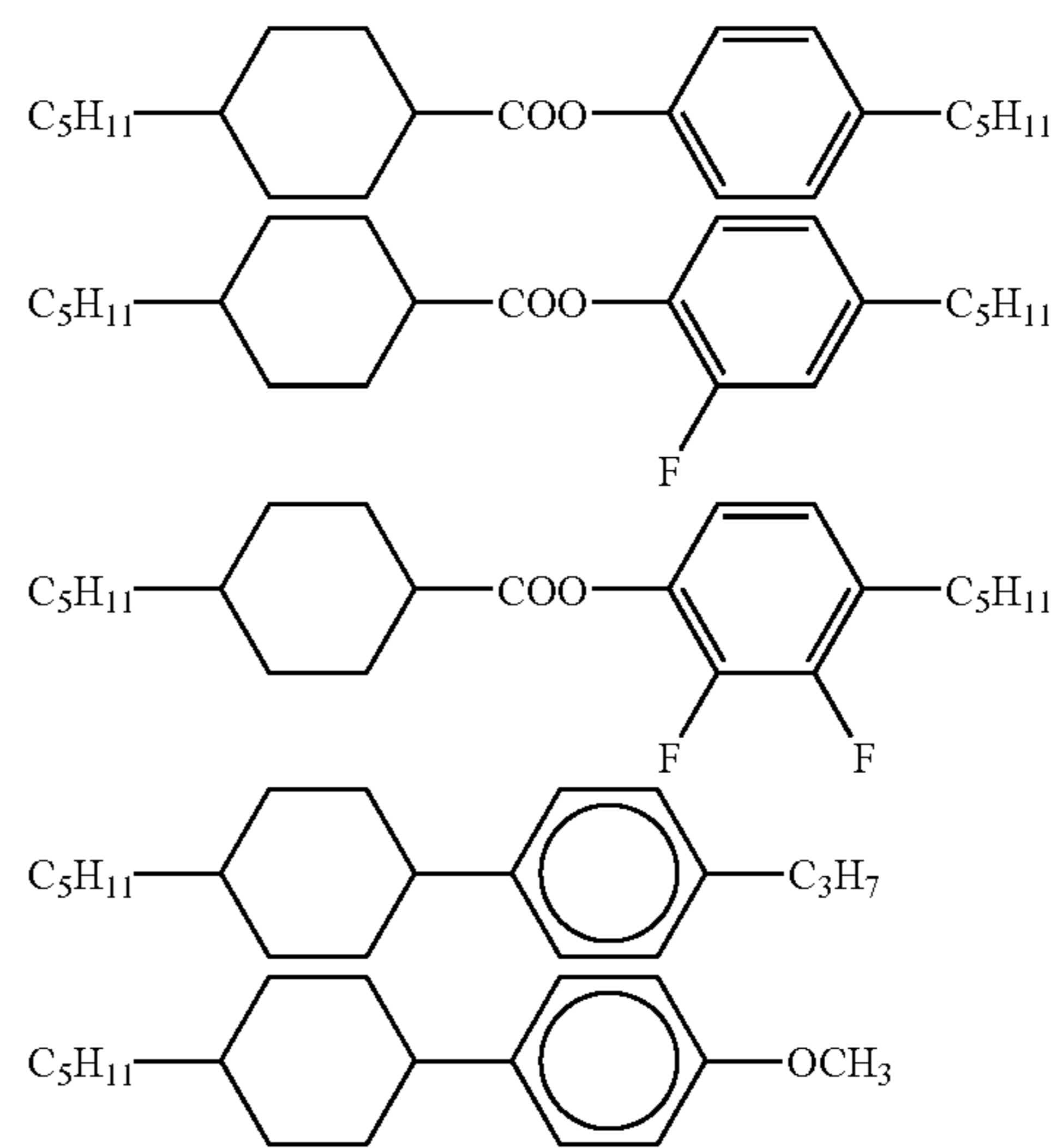
Referring again to FIG. 8a, there is shown an elevational view of a reflection grating 130 in accordance with the invention having periodic planes of polymer channels 130a and PDLC channels 130b disposed parallel to the front surface 134 of the grating 130. The symmetry axis 136 of the liquid crystal domains is formed in a direction perpendicular to the periodic channels 130a and 130b of the grating 130 and perpendicular to the front surface 134 of the grating 130. Thus, when an electric field E is applied, as shown in FIG. 8b, the symmetry axis 136 is already in a low energy state in alignment with the field E and will not reorient. Thus, reflec-

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tion gratings formed in accordance with the procedure described above will not normally be switchable.

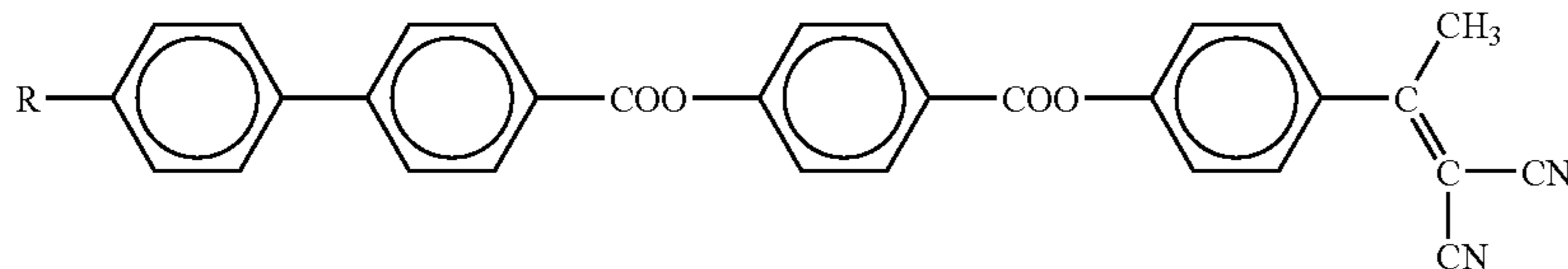
In general, a reflection grating tends to reflect a narrow wavelength band, such that the grating can be used as a reflection filter. In the preferred embodiment, however, the reflection grating is formed so that it will be switchable. In accordance with the present invention, switchable reflection gratings can be made utilizing negative dielectric anisotropy LCs (or LCs with a low cross-over frequency), an applied magnetic field, an applied shear stress field, or slanted gratings.

It is known that liquid crystals having a negative dielectric anisotropy ($\Delta\epsilon$) will rotate in a direction perpendicular to an applied field. As shown in FIG. 9a, the symmetry axis 136 of the liquid crystal domains formed with liquid crystal having a negative $\Delta\epsilon$ will also be disposed in a direction perpendicular to the periodic channels 130a and 130b of the grating 130 and to the front surface 134 of the grating. However, when an electric field E is applied across such gratings, as shown in FIG. 9b, the symmetry axis of the negative $\Delta\epsilon$ liquid crystal will distort and reorient in a direction perpendicular to the field E, which is perpendicular to the film and the periodic planes of the grating. As a result, the reflection grating can be switched between a state where it is reflective and a state where it is transmissive. The following negative $\Delta\epsilon$ liquid crystals and others are expected to find ready application in the methods and devices of the present invention:

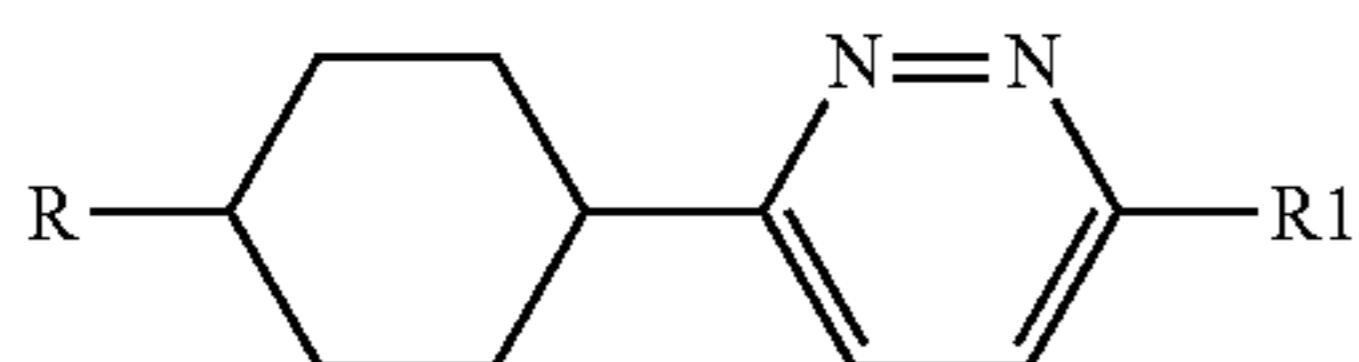


Liquid crystals can be found in nature (or synthesized) with either positive or negative $\Delta\epsilon$. Thus, in more detailed aspects of the invention, it is possible to use a LC which has a positive $\Delta\epsilon$ at low frequencies, but becomes negative at high frequencies. The frequency (of the applied voltage) at which $\Delta\epsilon$ changes sign is called the cross-over frequency. The cross-over frequency will vary with LC composition, and typical values range from 1-10 kHz. Thus, by operating at the proper frequency, the reflection grating may be switched. In accordance with the invention, it is expected that low crossover frequency materials can be prepared from a combination of positive and negative dielectric anisotropy liquid crystals. A suitable positive dielectric liquid crystal for use in such a combination contains four ring esters as shown below:

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A strongly negative dielectric liquid crystal suitable for use in such a combination is made up of pyridazines as shown below:



Both liquid crystal materials are available from LaRoche & Co., Switzerland. By varying the proportion of the positive and negative liquid crystals in the combination, crossover frequencies from 1.4-2.3 kHz are obtained at room temperature. Another combination suitable for use in the present embodiment is a combination of the following: p-pentylphenyl-2-chloro-4-(p-pentylbenzoyloxy)benzoate and benzoate. These materials are available from Kodak Company.

In still more detailed aspects of the invention, switchable reflection gratings can be formed using positive $\Delta\epsilon$ liquid crystals. As shown in FIG. 10a, such gratings are formed by exposing the PDLC starting material to a magnetic field during the curing FIG. 10a), the use of a permanent magnet, or other suitable means. Preferably, the magnetic field M is oriented parallel to the front surface of the glass plates (not shown) that are used to form the grating 140. As a result, the symmetry axis 146 of the liquid crystals will orient along the field while the mixture is fluid. When polymerization is complete, the field may be removed and the alignment of the symmetry axis of the liquid crystals will remain unchanged. (See FIG. 10b.) When an electric field is applied, as shown in FIG. 10c, the positive $\Delta\epsilon$ liquid crystal will reorient in the direction of the field, which is perpendicular to the front surface of grating and to the periodic channels of the grating.

FIG. 11a depicts a slanted transmission grating 148 and FIG. 11b depicts a slanted reflection grating 150. A holographic transmission grating is considered slanted if the direction of the grating vector G is not parallel to the grating surface. In a holographic reflection grating, the grating is said to be slanted if the grating vector G is not perpendicular to the grating surface. Slanted gratings have many of the same uses as non-slanted gratings such as visual displays, mirrors, line filters, optical switches, and the like.

Primarily, slanted holographic gratings are used to control the direction of a diffracted beam. For example, in reflection holograms a slanted grating is used to separate the specular reflection of the film from the diffracted beam. In a PDLC holographic grating, a slanted grating has an even more useful advantage. The slant allows the modulation depth of the grating to be controlled by an electric field when using either tangential or homeotropic aligned liquid crystals. This is because the slant provides components of the electric field in the directions both tangential and perpendicular to the grating vector. In particular, for the reflection grating, the LC domain symmetry axis will be oriented along the grating vector G and can be switched to a direction perpendicular to the film plane

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by a longitudinally applied field E. This is the typical geometry for switching of the diffraction efficiency of a slanted reflection grating.

When recording slanted reflection gratings, it is desirable to place the sample between the hypotenuses of two right-angle glass prisms. Neutral density filters can then be placed in optical contact with the back faces of the prisms using index matching fluids so as to frustrate back reflections which would cause spurious gratings to also be recorded. The incident laser beam is split by a conventional beam splitter into two beams which are then directed to the front faces of the prisms, and then overlapped in the sample at the desired angle. The beams thus enter the sample from opposite sides. This prism coupling technique permits the light to enter the sample at greater angles. The slant of the resulting grating is determined by the angle at which the prism assembly is rotated (i.e., the angle between the direction of one incident beam and the normal to the prism front face at which that beam enters the prism).

As shown in FIG. 12, switchable reflection gratings may be formed in the presence of an applied shear stress field. In this method, a shear stress would be applied along the direction of a magnetic field M. This could be accomplished, for example, by applying equal and opposite tensions to the two ITO coated glass plates which sandwich the prepolymer mixture while the polymer is still soft. This shear stress would distort the LC domains in the direction of the stress, and the resultant LC domain symmetry axis will be preferentially along the direction of the stress, parallel to the PDLC planes and perpendicular to the direction of the applied electric field for switching.

Reflection gratings prepared in accordance with the teachings of the present invention will find application in color reflective displays, switchable wavelength filters for laser projection, and the like.

As described herein, a holographic grating may be formed by overlapping two interfering incident beams in a sample. Similarly, a slanted grating can be prepared by overlapping the beams so that the angle of incidence of the first beam with respect to a normal from the sample is different from the angle of incidence of the second beam. In recording a slanted reflection grating the beams preferably enter the sample from opposite sides. In recording a slanted transmission grating, however, the beams enter the sample from the same side. The resulting slant of the grating, $\frac{1}{2}(\theta_{ref} - \theta_{obj})$, will be related to the angle between the incident beams. In certain applications, it may be desirable to prepare slanted gratings in which the grating vector G is disposed at a large angle to the grating surface. Such gratings are referred to as highly slanted gratings.

In preparing highly slanted gratings, it is desirable to dispose the first incident beam at a large angle of incidence with respect to the second beam, which is directed along a normal to the sample. However, this arrangement may result in undesirable reflection losses in the first beam, which may affect the balance between the intensity of the incident beams and the resulting index modulation. Therefore, it may be desirable to

reduce these reflection losses by directing the incident beam through a prism assembly as shown in FIG. 18.

In the particular arrangement shown in FIG. 18, two right angle prisms are combined into an assembly that is adapted to reduce reflection losses. This assembly is disposed on the surface of the sample. It is desirable to utilize an index matching fluid between the prisms and between the prism assembly and the sample in order to minimize reflections. The prisms are advantageously selected so that the first, object beam may be directed at a normal to one of the prisms (corresponding to a normal to the sample) and the second, reference beam can be directed at a normal to the other prism (corresponding to the desired angle to the sample). Neutral density filters can then be placed in optical contact with the back faces of the prisms using index matching fluids so as to frustrate back reflections which would cause spurious gratings to also be recorded. The incident laser beam is split by a conventional beam splitter into two beams which are then directed to the front faces of the prisms, and then overlapped in the sample at the desired angle. The beams thus enter the sample from the same side and the prism assembly advantageously reduces spurious reflections.

A switchable slanted transmission grating made in accordance with the present invention is shown in FIG. 19. Light of a wavelength that is matched to the Bragg condition will be diffracted into the -1 -order by the grating and deflected by an angle $2\theta_s$, where θ_s or θ_{slant} is the slant angle of the grating. When a voltage is applied, the index modulation of the grating is reduced and the incident radiation can pass through the grating.

As shown in FIGS. 20-22, switchable slanted transmission gratings in accordance with the present invention can be utilized as holographic optical elements (HOEs), and, more particularly, as switchable optical coupling devices. In the system shown in FIGS. 20-22, a switchable slanted transmission grating is placed in optical contact with a transparent substrate. The substrate is preferably a thick transparent medium, such as glass, so that the light guided by total internal reflection (TIR) follows a path determined primarily by geometric optics rather than in a waveguide mode (which would occur for a thin film of thickness comparable to the optical wavelength). In the system shown in FIGS. 20-22, the grating has a slant angle, θ_s or θ_{slant} , and the substrate has a critical angle, θ_c , for total internal reflection. If, as shown in FIGS. 20-21, the condition $2\theta_{slant} > \theta_c$, is satisfied, then the input light will be diffracted into the substrate where it will be subjected to total internal reflection. Moreover, if a voltage is applied to the switchable slanted transmission grating, as shown in FIG. 22, the diffraction efficiency of the grating can be modified so that the incident light will be transmitted through the grating. Thus, by applying a voltage, the system shown in FIGS. 20-21 can be selectively switched out of the TIR substrate mode. In addition, by varying the applied voltage and the corresponding diffraction efficiency of the grating, the amount of light diffracted into the substrate can be selectively controlled.

Referring now to FIGS. 23 and 24, a switchable slanted transmission grating may similarly be utilized as an output coupling device. As shown in FIG. 23, a switchable slanted transmission grating may be placed in optical contact with a transparent substrate at a point where light is totally internally reflected within the substrate, so that the light will be diffracted out of the substrate. Where a voltage is applied to the switchable slanted transmission grating, as shown in FIG. 24, the diffraction efficiency of the grating can be modified so that the incident light will not be diffracted through the grating.

More detailed aspects of such output coupling devices are discussed in connection with the discussion of FIGS. 25 and 26.

Where a slanted grating is to be used for optical coupling to a substrate, it is often desirable to select the angle of the slant and to match the index of the grating to that of the substrate. Moreover, it will be appreciated that the application of an anti-reflective coating to the grating will advantageously reduce spurious reflections. It will also be appreciated that the polymer-dispersed liquid crystal material may be selected so that the diffraction efficiency of the grating can be conveniently adjusted from 0 to 100% by the application of an electric field.

An example of a static one-to-many fan-out optical interconnect is given in an article entitled "Cross-link Optimized Cascaded Volume Hologram Array with Energy-equalized One-to-many Surface-normal Fan-outs," by J. Liu, C. Zhao, R. Lee, and R. T. Chen, *Optics Letters*, 22, pp. 1024-26 (1997), incorporated herein by reference.

As shown in FIGS. 25 and 26, however, switchable slanted transmission gratings can be used as optical couplers to form devices such as a selectively adjustable and reconfigurable one-to-many fan-out optical interconnect. A first input slanted transmission grating, such as the grating shown in FIG. 19, is disposed in optical contact with the substrate. At several points along the substrate where light reflects internally, transmission grating, such as the grating shown in FIG. 19, is disposed in optical contact with the substrate. At several points along the substrate where light reflects internally, additional output slanted transmission gratings, such as those shown in FIGS. 23-24, may be deposited with good optical contact so that the light may be diffracted out of the substrate. It will be appreciated that the slant angle, θ_s or θ_{slant} , of the output gratings is advantageously oriented at the opposite angle of the input grating. Individual voltage sources are preferably connected to the input and each of the output gratings.

As shown in the particular example in FIG. 25, the slant angle of the grating should exceed 23° so that the diffracted angle is 46° and greater than the 41.3° critical angle for the total internal reflection for the BK-7 glass substrate (having a refractive index of 1.52). This large slant allows light, normally incident on the waveguide, to be diffracted at such a large angle that the light becomes trapped inside the glass slab due to total internal reflection.

For a one-to-many fan-out optical interconnect having a total of N outputs of equal optical power, the diffraction efficiencies of each successive HOE is given by:

$$\eta_j = \frac{1}{N - j + 1}, (j = 1^KN)$$

Thus, light may be coupled into the substrate by a diffraction grating which deflects the light at an angle greater than the critical angle for TIR. The coupled light is guided along the substrate by TIR. At each output node some light is coupled out of the substrate by diffraction while the remainder continues to propagate down the substrate. Eventually all of the light may be coupled out of the substrate and sent to N other inputs, such as detectors, nodes of other switches, or the like. In such devices, it is desirable to control the diffraction efficiency to equalize the output power in each channel of the fan-out from the required values result in either poor performance or rejection of the element and re-manufacture of the part. In particular, it is difficult to achieve a uniform fan-out

energy distribution in such substrate guided-wave interconnects. In the present invention, the holographic optical elements can be manufactured with the same diffraction efficiency (~100%) and voltage-tuned in real-time to achieve the desired diffraction efficiency. As a result, the yield and quality of such elements can be increased and the ease of use is dramatically improved. Moreover, in devices incorporating static HOEs, it is difficult to adjust individual outputs and the configuration of the device. Typically such changes must be made mechanically by alteration of the existing HOEs or substitution of HOEs within the system. In particular, the same HOEs could not be used in a general reconfiguration of a substrate guided-wave interconnect since the diffraction efficiencies would not be correct for equal power fan-out. Finally, it is desirable to incorporate an input HOE having a high diffraction efficiency, such as the switchable gratings of the present invention, into such devices.

Switchable polymer-dispersed liquid crystal materials in accordance with the invention have been advantageously utilized to provide electrically switchable substrate guidedwave optical interconnects. Advantageously, the diffraction efficiency of each HOE can be tuned electrically to achieve equal-power fan-out. This feature eases manufacturing tolerances. In addition, by adjusting the output of the HOEs, the system can be reconfigured to display different fan-out, different outputs, different modules, or other configurational changes. Moreover, when a system is reconfigured, the diffraction efficiencies can be voltage-tuned to equalize the fan-out energy distribution, if desired.

In the example of a reconfigurable interconnect incorporating switchable HOEs in accordance with the present invention shown in FIG. 26, each HOE is preferably fabricated with a nominal diffraction efficiency $\eta \sim 100\%$. Each HOE may then be individually voltage-tuned to a value $\eta_j = (N-j+1)^{-1}$, where, for example, $N=9$. If $V_o = V_{sw}$ (where V_{sw} is the 100%-switching voltage), the fan-out is 1-to-0, i.e., no fan-out. If $V_o = 0$ such that $\eta_0 = 100\%$, the fan-out is 1-to-N. Examples of reconfigurable voltage/fan-out schemes corresponding to the reconfigurable substrate mode optical interconnect shown in FIG. 26 are set forth in the following table.

Reconfigurable Fan-Out Scheme	
1-to-9 Fan-Out	1-to-5 Fan-Out
V_1 $\eta = 11\%$	$V_{1'}$ $\eta = 20\%$
V_2 $\eta = 12\%$	V_{sw} $\eta = 0\%$
V_3 $\eta = 14\%$	$V_{3'}$ $\eta = 25\%$
V_4 $\eta = 16\%$	V_{sw} $\eta = 0\%$
V_5 $\eta = 20\%$	$V_{5'}$ $\eta = 33\%$
V_6 $\eta = 25\%$	V_{sw} $\eta = 0\%$
V_7 $\eta = 33\%$	$V_{7'}$ $\eta = 50\%$
V_8 $\eta = 50\%$	V_{sw} $\eta = 0\%$
V_9 $\eta = 100\%$	$V_{9'}$ $\eta = 100\%$
with each output $I_j = I_0/9$	with each output $I_j = I_0/5$

In the 1-9 Fan-Out Configuration, the voltages V_j are adjusted to yield diffraction efficiencies such that the outputs will have equal output intensities. In the 1-5 Fan-Out Configuration, four of the HOE outputs are set to yield zero diffraction efficiency, i.e., no output, and the remaining five voltages are adjusted to yield equal output intensities of the five active channels. It will be appreciated that a variety of configurations are possible, such as a 1-to-5 fan-out involving just the first five channels, or a 1-to-3 fan-out involving the first, sixth, and ninth channel. Moreover, it will be appreciated that the relative intensities of the outputs can be advantageously

adjusted by adjusting the switching voltages. In addition, for any system including N channels, the outputs can be matched by adjusting the voltage of each HOE to $V_j(N)$ to keep $\eta_j = (N-j+1)^{-1}$ for each value of N.

It will be appreciated that such systems can include a plurality of inputs and that these inputs may be disposed on either side of the substrate. Similarly, such systems could advantageously include one or a plurality of outputs and that these outputs may be disposed on either side of the substrate. It will be further appreciated that a static input could be combined with switchable outputs and that static outputs could be substituted for one or all of the switchable outputs. Moreover, as noted above, the ability to switch the PDLC grating allows for selected control of the intensity and position of light coupled into or out of the substrate and has more potential for use as reconfigurable optical interconnects.

It will be appreciated that prepolymer mixtures for the preparation of switchable slanted gratings have been described herein. In the preparation of switchable slanted gratings for use as optical coupling devices, it is desirable to select the prepolymer mixture so that the average refractive index of the resulting grating is similar to the refractive index of the substrate. In the preferred embodiment in which the grating is coupled to a glass substrate, it has been found that a combination of the following prepolymer components will yield a grating having a desirable average index of refraction: dipentaerythritol pentaacrylate, the chain extender N-vinyl pyrrolidinone (NVP), the liquid crystal E7, the photoinitiator rose bengal and a co-initiator N-phenyl glycine as described previously herein.

Highly slanted gratings in accordance with the invention can be prepared by disposing the prepolymer mixture between ITO coated glass slides using spacers of thickness 15-20 μm . The gratings were recorded using the 488 nm line of an argon-ion laser. The geometry for writing the gratings is shown in FIG. 18. Reading of the gratings was carried out using a He-Ne(633 nm) laser beam.

Electrical switching of the gratings can be accomplished by monitoring the change in the diffraction efficiency (DE) and transmission as the strength of the electric field is increased. The electric field was produced by applying an amplified 2 kHz square wave from a function generator to the ITO electrodes on the sample. Using square wave pulse, the time responses of the gratings for electrical switching were also measured. Both field on and off times were measured.

Low voltage, high resolution scanning electron microscopy (SEM) can be used to obtain film thickness and morphology. Samples for SEM can be prepared by removing the films from the glass slides and fracturing in liquid nitrogen. The liquid crystal in the sample can be removed by soaking in methanol, and the films coated with 2-3 nm tungsten.

FIG. 27 shows the electrical switching curve for a switchable guided substrate-mode coupler. The curve is very similar to non-slanted grating curves with a critical switching field of about 7.5 V/ μm . The best dynamic range measured was 17.8 dB in the transmitted beam and 20.6 dB in the diffracted beam. The switching times of the slanted gratings were also measured as shown in FIGS. 28 and 29. The measured on time was 197 μs and the off time 168 μs for an applied 95 V step voltage. Higher driving voltages appear to lead to the unusual response shown in FIG. 30 where the diffracted beam quickly reaches a minimum and then increases again to a constant. It is believed that this effect is due to the rotation of the LC symmetry axis far past the angle for best index matching, a situation which is difficult to obtain in a non-slanted grating but not in a highly slanted grating.

An experimental demonstration of the coupling of the diffracted light from the slanted grating on to a glass slab and the electrical switching is shown in FIGS. 7 and 8 of an article entitled "Electrically Switchable Holograms Containing Novel PDLC Structures," L. V. Natarajan, R. L. Sutherland, V. P. Tondiglia, T. J. Bunning, and R. M. Neal, Vol. 3143, Liquid Crystals, SPE (1997), incorporated herein by reference. Similarly, an SEM image, which clearly shows the slanted nature of the grating, is shown in FIG. 9 of this article. According to the SEM image, the grating spacing was found to be 0.35 μm and the slant angle of the grating calculated from the SEM image was found to be 26°, which was in agreement with the theoretical expectation. It is also seen from the SEM image that the grating consists of periodic planes of phase separated liquid crystals and polymer.

In another embodiment of the present invention, PDLC materials can be made that exhibit a property known as form birefringence whereby polarized light that is transmitted through the grating will have its polarization modified. Such gratings are known as subwavelength gratings, and they behave like a negative uniaxial crystal, such as calcite, potassium dihydrogen phosphate, or lithium niobate, with an optic axis perpendicular to the PDLC planes. Referring now to FIG. 13, there is shown an elevational view of a transmission grating 200 in accordance with the present invention having periodic planes of polymer planes 200a and PDLC planes 200b disposed perpendicular to the front surface 204 of the grating 200. The optic axis 206 is disposed perpendicular to polymer planes 200a and the PDLC planes 200b. Each polymer plane 200a has a thickness t_p , and refractive index n_p , and each PDLC plane 200b has a thickness t_{PDLC} and refractive index N_{PDLC} .

Where the combined thickness of the PDLC plane and the polymer plane is substantially less than an optical wavelength (i.e. $(t_{PDLC}+t_p) \ll \lambda$), the grating will exhibit form birefringence. As discussed below, the magnitude of the shift in polarization is proportional to the length of the grating. Thus, by carefully selecting the length, L, of the subwavelength grating for a given wavelength of light, one can rotate the plane of polarization or create circularly polarized light. Consequently, such subwavelength gratings can be designed to act as a half-wave or quarter-wave plate, respectively. Thus, an advantage of this process is that the birefringence of the material may be controlled by simple design parameters and optimized to a particular wavelength, rather than relying on the given birefringence of any material at that wavelength.

To form a half-wave plate, the retardance of the subwavelength grating must be equal to one-half of a wavelength, i.e., retardance= $\lambda/2$, and to form a quarter-wave plate, the retardance must be equal to one-quarter of a wavelength, i.e., retardance= $\lambda/4$. It is known that the retardance is related to the net birefringence, $|\Delta n|$, which is the difference between the ordinary index of refraction, n_o , and the extraordinary index of refraction n_e , of the sub-wavelength grating by the following relation:

$$\text{Retardance} = |\Delta n|L = n_e - n_o |L$$

Thus, for a half-wave plate, i.e., a retardance equal to one-half of a wavelength, the length of the subwavelength grating should be selected so that:

$$L = \lambda / (2|\Delta n|)$$

Similarly, for a quarter-wave plate, i.e., a retardance equal to one-quarter of a wavelength, the length of the subwavelength grating should be selected so that:

$$L = \lambda / (4|\Delta n|)$$

If, for example, the polarization of the incident light is at an angle of 45° with respect to the optic axis 210 of a half-wave plate 212, as shown in FIG. 14a, the plane polarization will be preserved, but the polarization of the wave exiting the plate will be shifted by 90°. Thus, referring now to FIGS. 14b and 14c, where the half-wave plate 212 is placed between cross polarizers 214 and 216, the incident light will be transmitted. If an appropriate switching voltage is applied, as shown in FIG. 14d, the polarization of the light is not rotated and the light will be blocked by the second polarizer.

For a quarter-wave plate plane polarized light is converted to circularly polarized light. Thus, referring now to FIG. 15a, where quarter wave plate 217 is placed between a polarizing beam splitter 218 and a mirror 219, the reflected light will be reflected by the beam splitter 218. If an appropriate switching voltage is applied, as shown in FIG. 15b, the reflected light will pass through the beam splitter and be retroreflected on the incident beam.

Referring now to FIG. 16a, there is shown an elevational view of a subwavelength grating 230 recorded in accordance with the above-described methods and having periodic planes of polymer channels 230a and PDLC channels 230b disposed perpendicular to the front surface 234 of grating 230. As shown FIG. 16a, the symmetry axis 232 of the liquid crystal domains is disposed in a direction parallel to the front surface 234 of the grating and perpendicular to the periodic channels 230a and b of the grating 230. Thus, when an electric field E is applied across the grating, as shown in FIG. 15b, the symmetry axis 232 distorts and reorients in a direction along the field E, which is perpendicular to the front surface 234 of the grating and parallel to the periodic channels 230a and 230b of the grating 230. As a result, subwavelength grating 230 can be switched between a state where it changes the polarization of the incident radiation and a state in which it does not. Without wishing to be bound by any theory, it is currently believed that the direction of the liquid crystal domain symmetry 232 is due to a surface tension gradient which occurs as a result of the anisotropic diffusion of monomer and liquid crystal during recording of the grating and that this gradient causes the liquid crystal domain symmetry to orient in a direction perpendicular to the periodic planes.

As discussed in Born and Wolf, Principles of Optics, 5th Ed., New York (1975) and incorporated herein by reference, the birefringence of a subwavelength grating is given by the following relation:

$$n_e^2 - n_o^2 = \frac{-(f_{PDLC})(f_p)(n_{PDLC}^2 - n_p^2)}{[f_{PDLC}n_{PDLC}^2 + f_p n_p^2]}$$

where

n_o = the ordinary index of refraction of the subwavelength grating;

$$n_e^2 - n_o^2 = \frac{-(f_{PDLC})(f_p)(n_{PDLC}^2 - n_p^2)}{[f_{PDLC}n_{PDLC}^2 + f_p n_p^2]}$$

where

n_o = the ordinary index of refraction of the subwavelength grating;

n_e = the extraordinary index of refraction;

n_{PDLC} = the refractive index of the PDLC plane;

n_p = the refractive index of the polymer plane;

n_{LC} = the effective refractive index of the liquid crystal seen by an incident optical wave;

$$f_{PDLC} = t_{PDLC} / (t_{PDLC} + t_p)$$

$$f_p = t_p / (t_{PDLC} + t_p)$$

Thus, the net birefringence of the subwavelength grating will be zero if $n_{PDLC} = n_p$.

It is known that the effective refractive index of the liquid crystal, n_{LC} , is a function of the applied electric field, having a maximum when the field is zero and a value equal to that of the polymer, n_p , at some value of the electric field, E_{MAX} . Thus, by application of an electric field, the refractive index of the liquid crystal, n_{LC} , and, hence, the refractive index of the PDLC plane can be altered. Using the relationship set forth above, the net birefringence of a subwavelength grating will be a minimum when n_{PDLC} is equal to n_p , i.e., when $n_{LC} = n_p$. Therefore, if the refractive index of the PDLC plane can be matched to the refractive index of the polymer plane, i.e., $n_{PDLC} = n_p$, by the application of an electric field, the birefringence of the subwavelength grating can be switched off.

The following equation for net birefringence, i.e., $|\Delta n| = |n_e - n_o|$, follows from the equation given in Born and Wolf (reproduced above):

Furthermore, it is known that the refractive index of the PDLC plane n_{PDLC} is related to the effective refractive index of the liquid crystal seen by an incident optical wave, n_{LC} , and the refractive index of the surrounding polymer plane, n_p , by the following relation:

$$n_{PDLC} = n_p + f_{LC}(n_{LC} - n_p)$$

where f_{LC} is the volume fraction of liquid crystal dispersed in the polymer within the PDLC plane, $f_{LC} = [V_{LC} / (V_{LC} + V_P)]$.

By way of example, a typical value for the effective refractive index for the liquid crystal in the absence of an electric field is $n_{LC} = 1.7$, and for the polymer layer $n_p = 1.5$. For a grating where the thickness of the PDLC planes and the polymer planes are equal (i.e., $t_{PDLC} = t_p$, $f_{PDLC} = 0.5 = f_p$) and $f_{LC} = 0.35$, the net birefringence, Δn , of the subwavelength grating is approximately 0.008. Thus, where the incident light has a wavelength of 0.8 μm , the length of the subwavelength grating should be 50 μm for a half-wave plate and 25 μm for a quarter-wave plate. Furthermore, by application of an electric field of approximately 5 V/ μm , the refractive index of the liquid crystal can be matched to the refractive index of the polymer and the birefringence of the subwavelength grating turned off. Thus, the switching voltage, V_n , for a halfwave plate is on the order of 250 volts, and for a quarterwave plate approximately 125 volts.

By applying such voltages, the plates can be switched between the on and off (zero retardance) states on the order of microseconds. As a means of comparison, current Pockels cell technology can be switched in nanoseconds with voltages of approximately 1000-2000 volts, and bulk nematic liquid crystals can be switched on the order of milliseconds with voltages of approximately 5 volts.

In an alternative embodiment of the invention shown in FIG. 17, the switching voltage of the subwavelength grating can be reduced by stacking several subwavelength gratings 220a-e together, and connecting them electrically in parallel. By way of example, it has been found that a stack of five gratings each with a length of 10 μm yields the thickness required for a half-wave plate. It should be noted that the length of the sample is somewhat greater than 50 μm , because each grating includes an indium-tin-oxide coating which acts as a transparent electrode. The switching voltage for such a stack of plates, however, is only 50 volts.

Subwavelength gratings in accordance with the present invention are expected to find suitable application in the areas of polarization optics and optical switches for displays and laser optics, as well as tunable filters for telecommunications, colorimetry, spectroscopy, laser protection, and the like. Similarly, electrically switchable transmission gratings have many applications for which beams of light must be deflected or holographic images switched. Among these applications are: fiber optic switches, reprogrammable N×N optical interconnects for optical computing, beam steering for laser surgery, beam steering for laser radar, holographic image storage and retrieval, digital zoom optics (switchable holographic lenses), graphic arts and entertainment, and the like.

A switchable hologram is one for which the diffraction efficiency of the hologram may be modulated by the application of an electric field, and can be switched from a fully on state (high diffraction efficiency) to a fully off state (low or zero diffraction efficiency). A static hologram is one whose properties remain fixed independent of an applied field. In accordance with the present invention, a high contrast static hologram can also be created. In this variation of the present invention, the holograms are recorded as described previously. The cured polymer film is then soaked in a suitable solvent at room temperature for a short duration and finally dried. For the liquid crystal E7, methanol has shown satisfactory application. Other potential solvents include alcohols such as ethanol, hydrocarbons such as hexane and heptane, and the like. When the material is dried, a high contrast static hologram with high diffraction efficiency results. The high diffraction efficiency is a consequence of the large index modulation in the film ($\Delta n \sim 0.5$) because the second phase domains are replaced with empty (air) voids ($n \sim 1$).

Similarly, in accordance with the present invention, a high birefringence static sub-wavelength wave-plate can also be formed. Due to the fact that the refractive index for air is significantly lower than for most liquid crystals, the corresponding thickness of the half-wave plate would be reduced accordingly. Synthesized waveplates in accordance with the present invention can be used in many applications employing polarization optics, particularly where a material of the appropriate birefringence at the appropriate wavelength is unavailable, too costly, or too bulky.

In the claims, the term polymer-dispersed liquid crystals and polymer-dispersed liquid crystal material includes, as may be appropriate, solutions in which none of the monomers have yet polymerized or cured, solutions in which some polymerization has occurred, and solutions which have undergone complete polymerization. Those of skill in the art in the field of the invention will clearly understand that the use herein of the standard term used in the art, polymer-dispersed liquid crystals (which grammatically refers to liquid crystals dispersed in a fully polymerized matrix) is meant to include all or part of a more grammatically correct prepolymer-dispersed liquid crystal material or a more grammatically correct starting material for a polymer-dispersed liquid crystal material.

It will be seen that modifications to the invention as described may be made, as might occur to one with skill in the field of the invention, within the intended scope of the claims. Therefore, all embodiments contemplated have not been shown in complete detail. Other embodiments may be developed without departing from the spirit of the invention or from the scope of the claims.

What is claimed is:

1. A system for forming a slanted grating comprising: a sample comprising a polymerizable monomer, a liquid crystal, a chain-extending monomer, a co-initiator, and a photoinitiator; and

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a first incident beam and a second incident beam entering the sample forming the slanted grating therein, wherein an angle of incidence of the first incident beam with respect to a normal from the sample is different from an angle of incidence of the second incident beam; a transparent substrate placed in optical contact with the formed slanted grating; and an at least one additional slanted grating placed in optical contact with the transparent substrate.

2. The system according to claim 1, wherein the first incident beam and the second incident beam enter the sample from opposite sides of the sample.

3. The system according to claim 1, wherein the first incident beam and the second incident beam enter the sample from a same side of the sample.

4. The system according to claim 1, further comprising a prism assembly, wherein the first and second incident beams are directed through the prism assembly.

5. The system according to claim 4, wherein the prism assembly comprises a first right angle prism comprising a front face and a back face; and a second right angle prism comprising a front face and a back face.

6. The system according to claim 4, wherein the prism assembly is disposed on the surface of the sample.

7. The system according to claim 5, further comprising an index matching fluid between the two right angle prisms.

8. The system according to claim 4, further comprising an index matching fluid between the prism assembly and the sample.

9. The system according to claim 5, wherein the first incident beam is directed at a normal to the first right angle prism.

10. The system according to claim 5, wherein the second incident beam is directed at a normal to the second right angle prism.

11. The system according to claim 5, further comprising at least one neutral density filter placed in optical contact with the back face of the first right angle prism and the back face of the second right angle prism.

12. The system according to claim 5, further comprising a beam splitter, wherein the beam splitter splits a beam into the first incident beam and the second incident beam.

13. The system according to claim 1, wherein the transparent substrate comprises glass.

14. The system according to claim 1, wherein the transparent substrate is located at a point where the first and second incident beams are totally internally reflected within the transparent substrate so that the first and second incident beams will be diffracted out of the transparent substrate.

15. The system according to claim 1, wherein the transparent substrate has the same refractive index as the formed slanted grating.

16. The system according to claim 1, further comprising an anti-reflective coating.

17. The system according to claim 1, wherein a slant angle of the formed slanted grating is greater than about 23 degrees.

18. The system according to claim 1, wherein a slant angle of the formed slanted grating is greater than a critical angle for the total internal reflection of the transparent substrate.

19. The system according to claim 13, wherein the sample comprises dipentaerythritol pentaacrylate, N-vinyl pyrrolidone, a mixture of cyanobiphenyls, rose bengal, and N-phenyl glycine.

20. The system according to claim 1, further comprising two glass slides, wherein the sample is disposed between the glass slides.

21. The system according to claim 20, further comprising at least one spacer.

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22. The system according to claim 21, wherein the at least one spacer have a thickness of about 15 to 20 μm .

23. The system according to claim 21, wherein the at least one spacer have a thickness of about 15 to 100 μm .

24. The system according to claim 1, further comprising an argon-ion laser for recording the gratings.

25. The system according to claim 24, wherein the argon-ion laser is about 488 nm.

26. The system according to claim 1, further comprising a He—Ne laser beam for reading the formed slanted grating.

27. A system for forming a slanted grating comprising: a sample comprising a polymerizable monomer, a liquid crystal, a chain-extending monomer, a co-initiator, and a photoinitiator; and

a first incident beam and a second incident beam entering the sample forming the slanted grating therein,

wherein an angle of incidence of the first incident beam with respect to a normal from the sample is different from an angle of incidence of the second incident beam;

a transparent substrate placed in optical contact with the formed slanted grating; and

individual voltage sources connected to the slanted grating and the at least one additional slanted grating.

28. The system according to claim 27, wherein the first incident beam and the second incident beam enter the sample from opposite sides of the sample.

29. The system according to claim 27, wherein the first incident beam and the second incident beam enter the sample from a same side of the sample.

30. The system according to claim 27, further comprising a prism assembly, wherein the first and second incident beams are directed through the prism assembly.

31. The system according to claim 30, wherein the prism assembly comprises a first right angle prism comprising a front face and a back face; and a second right angle prism comprising a front face and a back face.

32. The system according to claim 30, wherein the prism assembly is disposed on the surface of the sample.

33. The system according to claim 31, further comprising an index matching fluid between the two right angle prisms.

34. The system according to claim 30, further comprising an index matching fluid between the prism assembly and the sample.

35. The system according to claim 31, wherein the first incident beam is directed at a normal to the first right angle prism.

36. The system according to claim 31, wherein the second incident beam is directed at a normal to the second right angle prism.

37. The system according to claim 31, further comprising at least one neutral density filter placed in optical contact with the back face of the first right angle prism and the back face of the second right angle prism.

38. The system according to claim 31, further comprising a beam splitter, wherein the beam splitter splits a beam into the first incident beam and the second incident beam.

39. The system according to claim 27, wherein the transparent substrate comprises glass.

40. The system according to claim 27, wherein the transparent substrate is located at a point where the first and second incident beams are totally internally reflected within the transparent substrate so that the first and second incident beams will be diffracted out of the transparent substrate.

41. The system according to claim 27, wherein the transparent substrate has the same refractive index as the formed slanted grating.

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42. The system according to claim 27, further comprising an anti-reflective coating.

43. The system according to claim 27, wherein a slant angle of the formed slanted grating is greater than about 23 degrees.

44. The system according to claim 27, wherein a slant angle 5 of the formed slanted grating is greater than a critical angle for the total internal reflection of the transparent substrate.

45. The system according to claim 39, wherein the sample comprises dipentaerythritol pentaacrylate, N-vinyl pyrrolidone, a mixture of cyanobiphenyls, rose bengal, and N-phenyl glycine. 10

46. The system according to claim 27, further comprising two glass slides, wherein the sample is disposed between the glass slides.

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47. The system according to claim 46, further comprising at least one spacer.

48. The system according to claim 47, wherein the at least one spacer have a thickness of about 15 to 20 μm .

49. The system according to claim 47, wherein the at least one spacer have a thickness of about 15 to 100 μm .

50. The system according to claim 27, further comprising an argon-ion laser for recording the gratings.

51. The system according to claim 50, wherein the argon-ion laser is about 488 nm.

52. The system according to claim 27, further comprising a He—Ne laser beam for reading the formed slanted grating.

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