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Giandalia et al.

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(54) **PLANAR TRANSFORMER ARRANGEMENT** JP 04-151810 5/1992

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(51) **Int. Cl.**
H01F 5/00 (2006.01)

(52) **U.S. Cl.** **336/200**

(58) **Field of Classification Search** 336/65, 336/83, 200, 206-208, 232; 257/531
See application file for complete search history.

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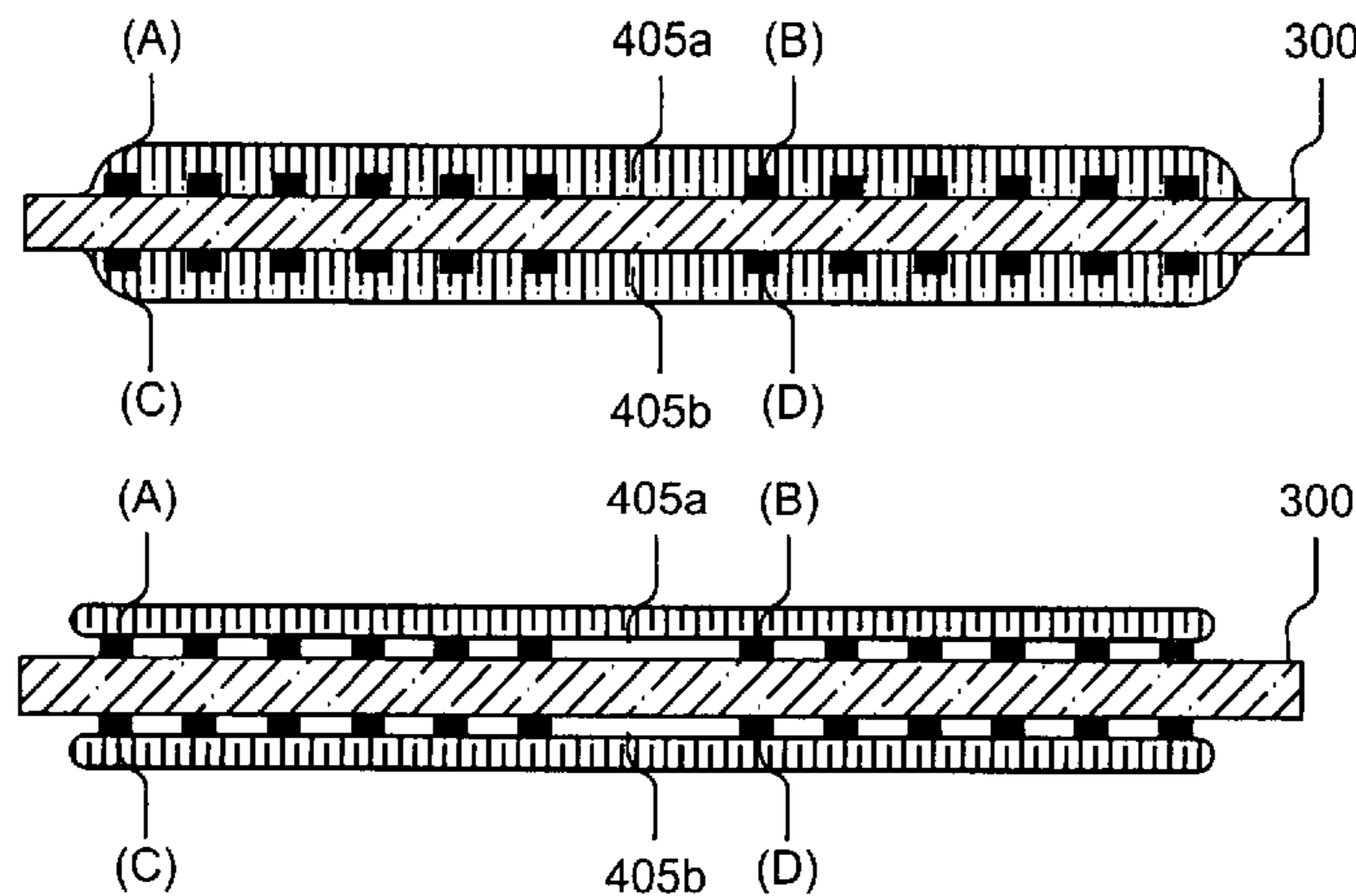
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(57) **ABSTRACT**

A planar transformer arrangement and method provide isolation between an input signal and an output signal. The planar transformer arrangement includes a planar medium having a first layer, a second layer, and a dielectric interlayer arranged between the first and second layers; at least one meandering primary winding arranged on the first layer of the planar medium, a current flow being induced within the primary winding in accordance with the input signal; at least one meandering secondary winding arranged on the second layer of the planar medium, the primary and secondary windings forming a planar transformer, whereby a voltage is induced across the secondary winding in accordance with the current flow within the primary winding; and a mode elimination arrangement configured to produce a compensated voltage by compensating for a common mode interference on the voltage induced across the secondary winding, the mode elimination arrangement being further configured to generate the output signal in accordance with the compensated voltage; wherein the dielectric interlayer of the planar medium provides a voltage isolation between the primary and secondary windings.

4 Claims, 7 Drawing Sheets



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Page 2

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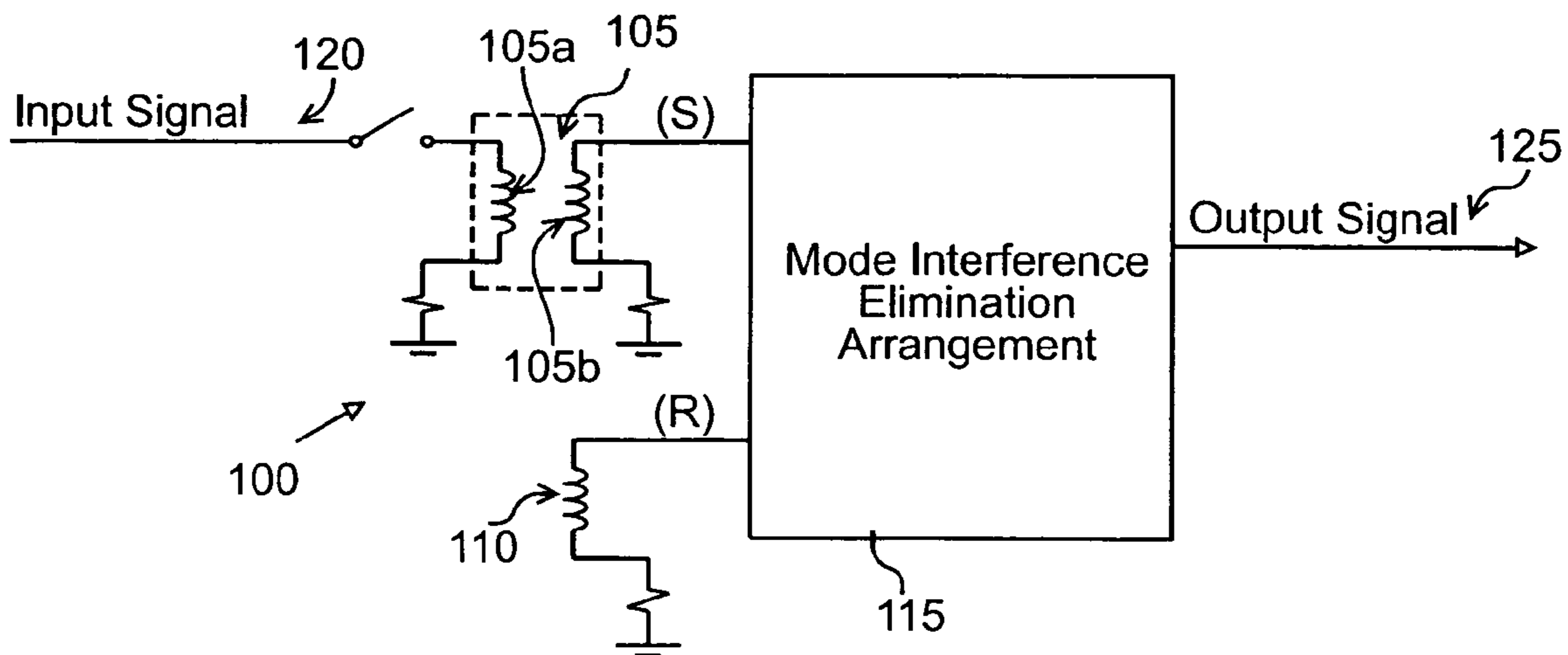


Figure 1

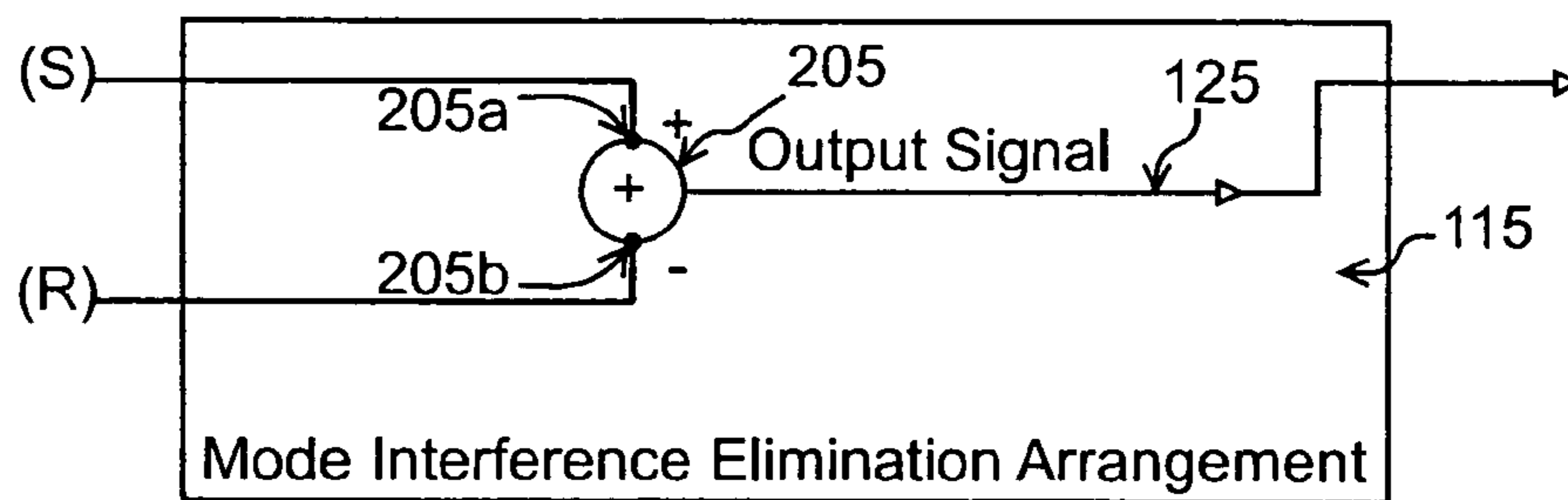


Figure 2

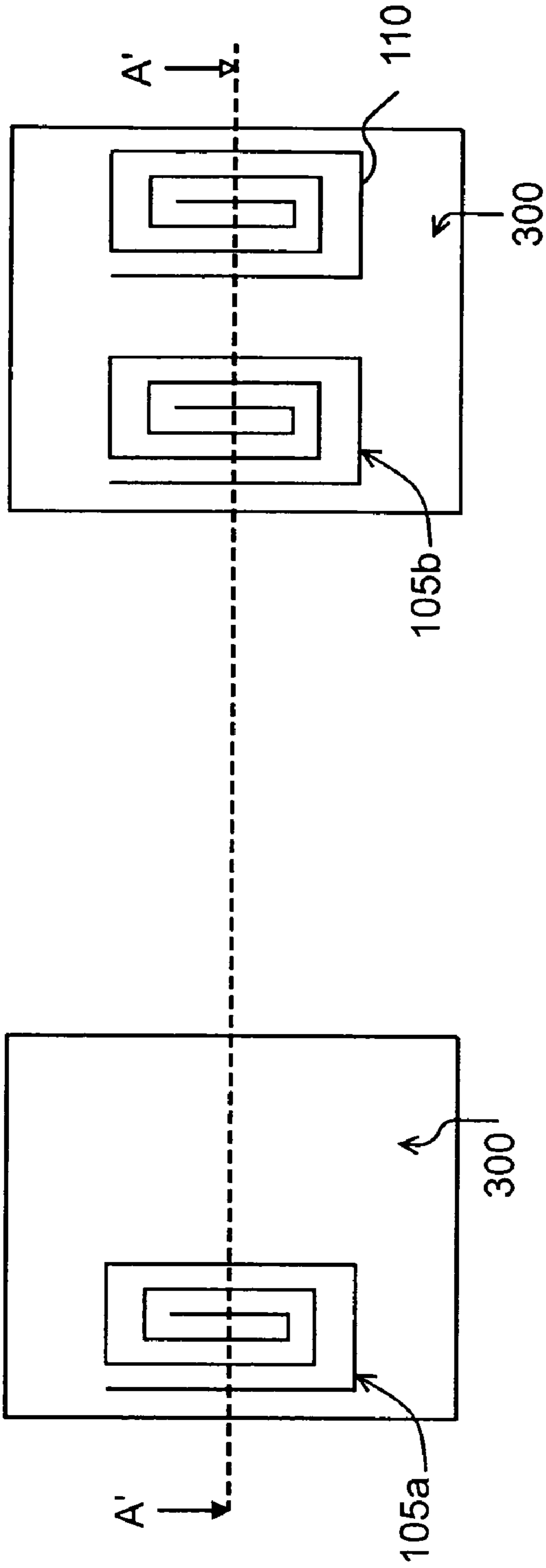


Figure 3a

Figure 3b

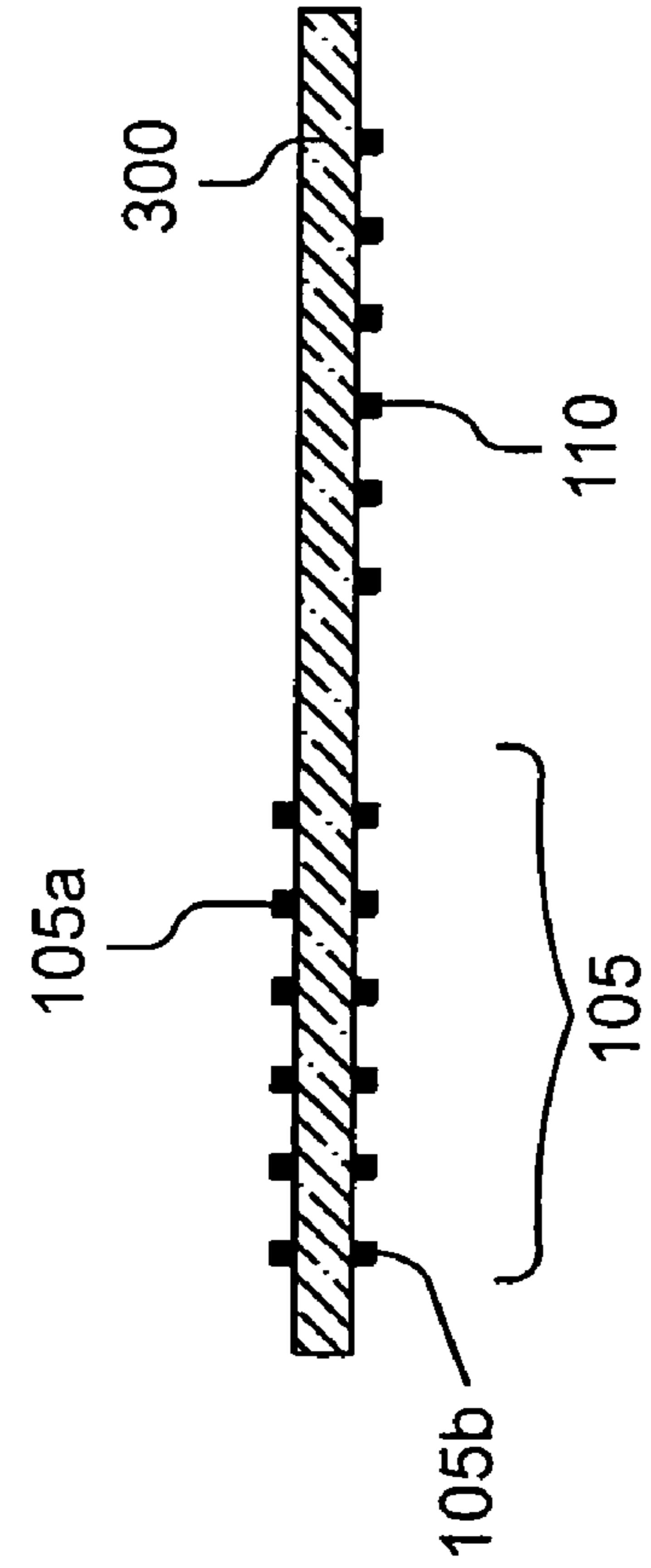


Figure 3c

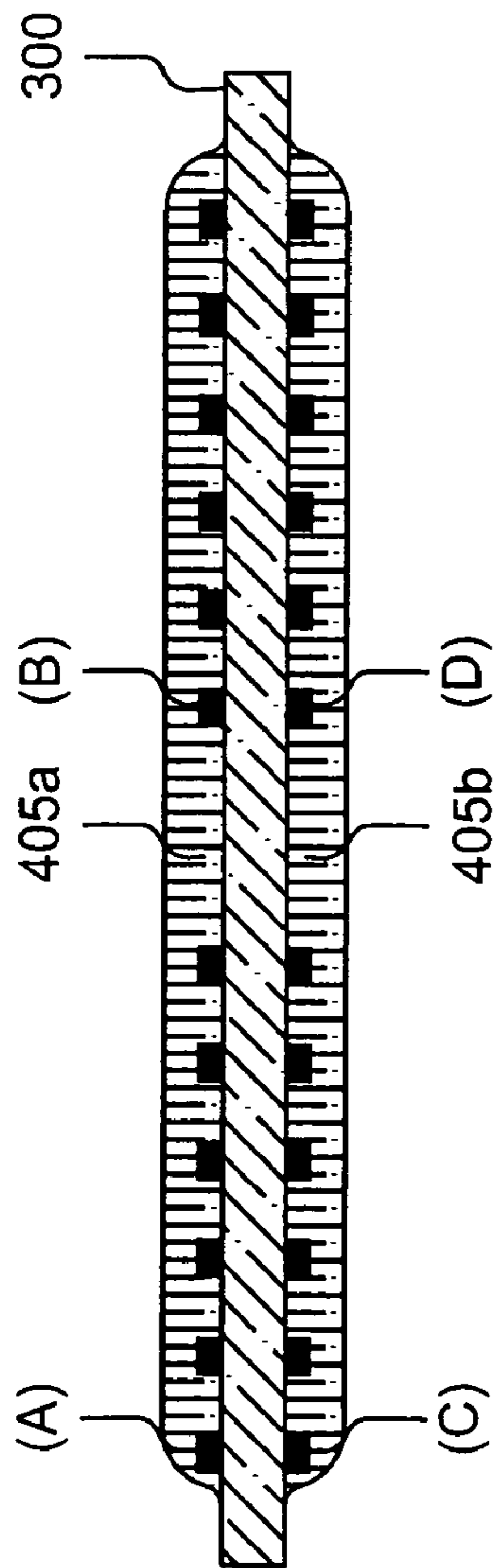


Figure 4a

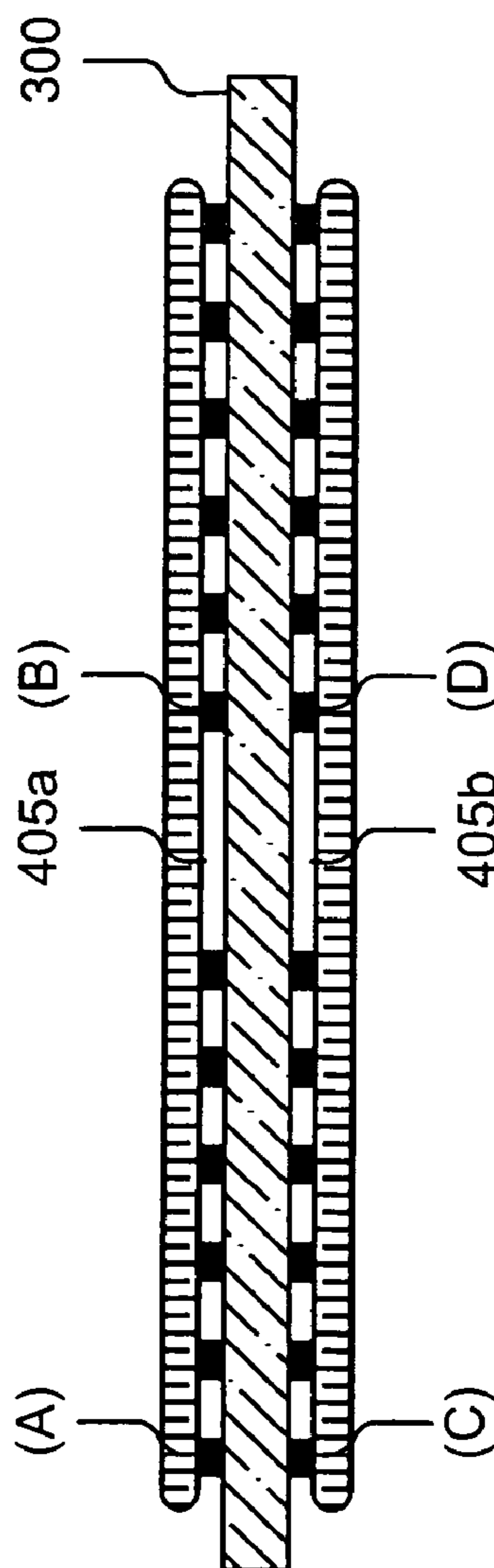


Figure 4b

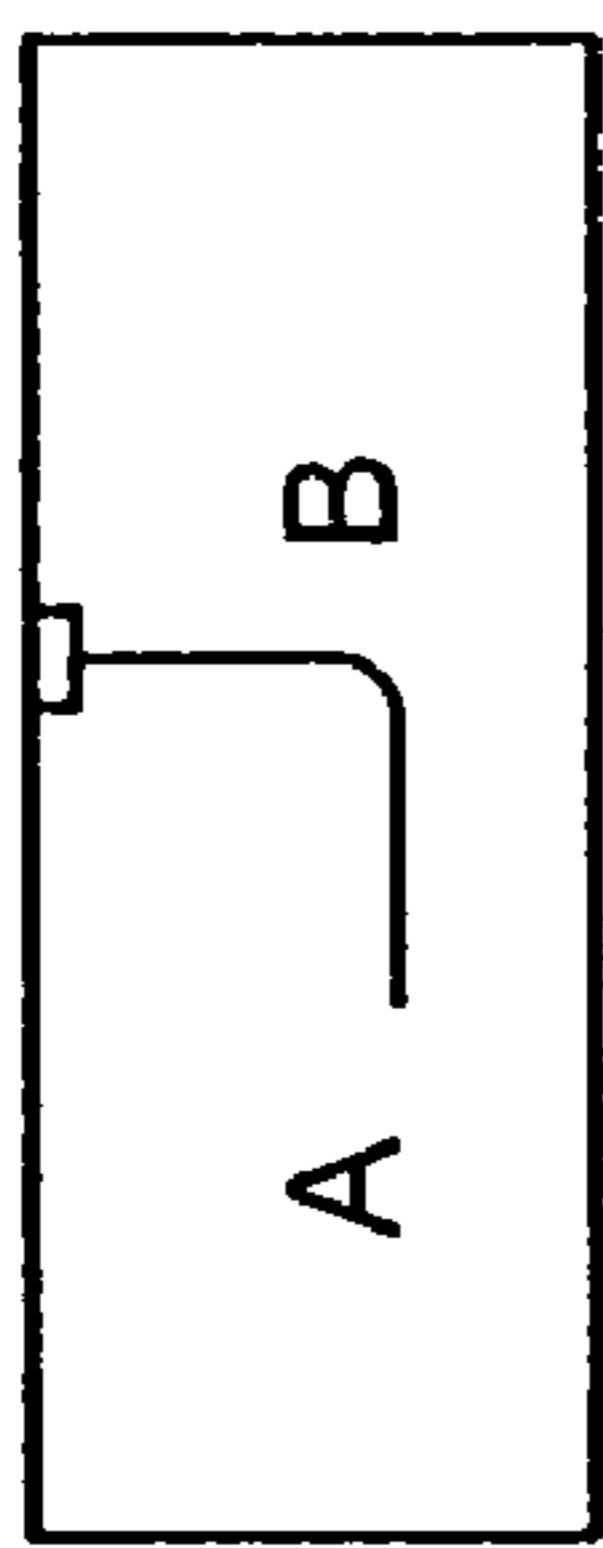
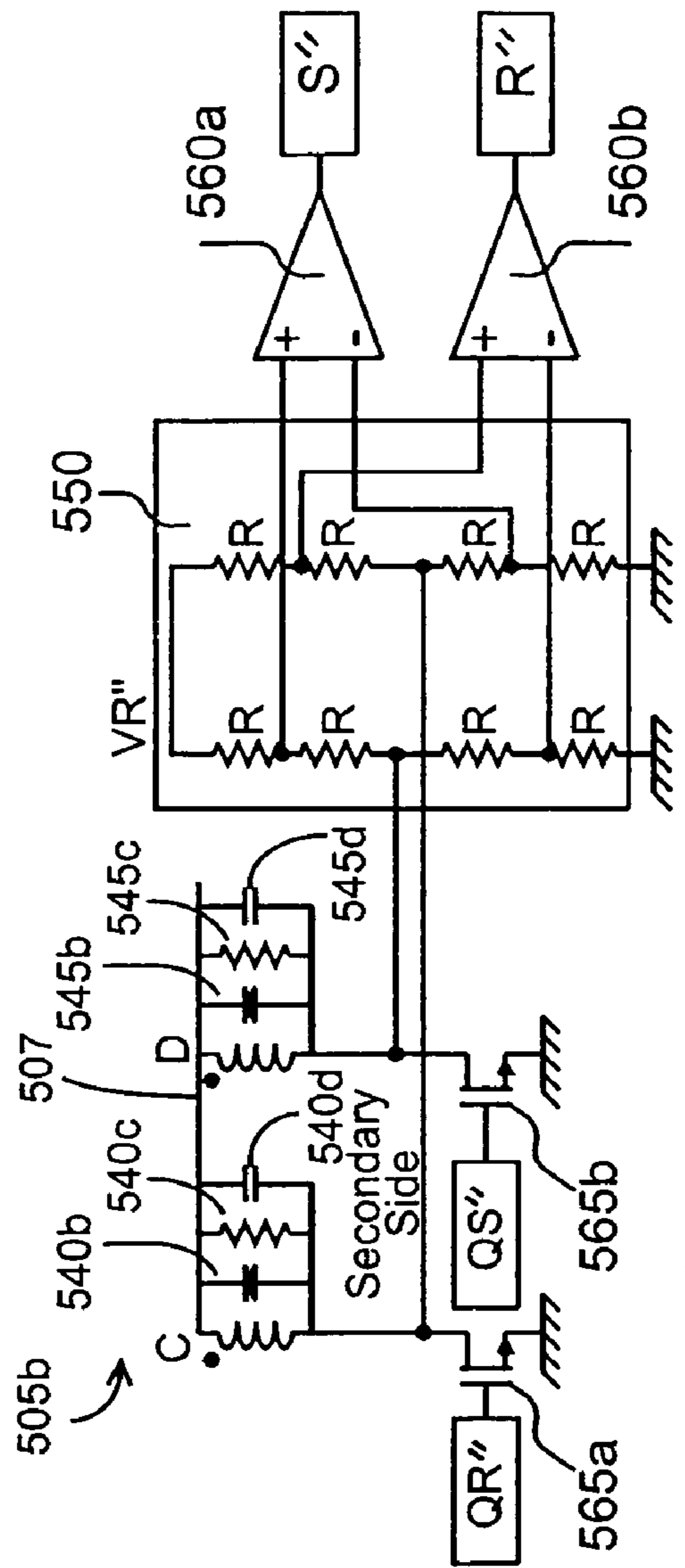
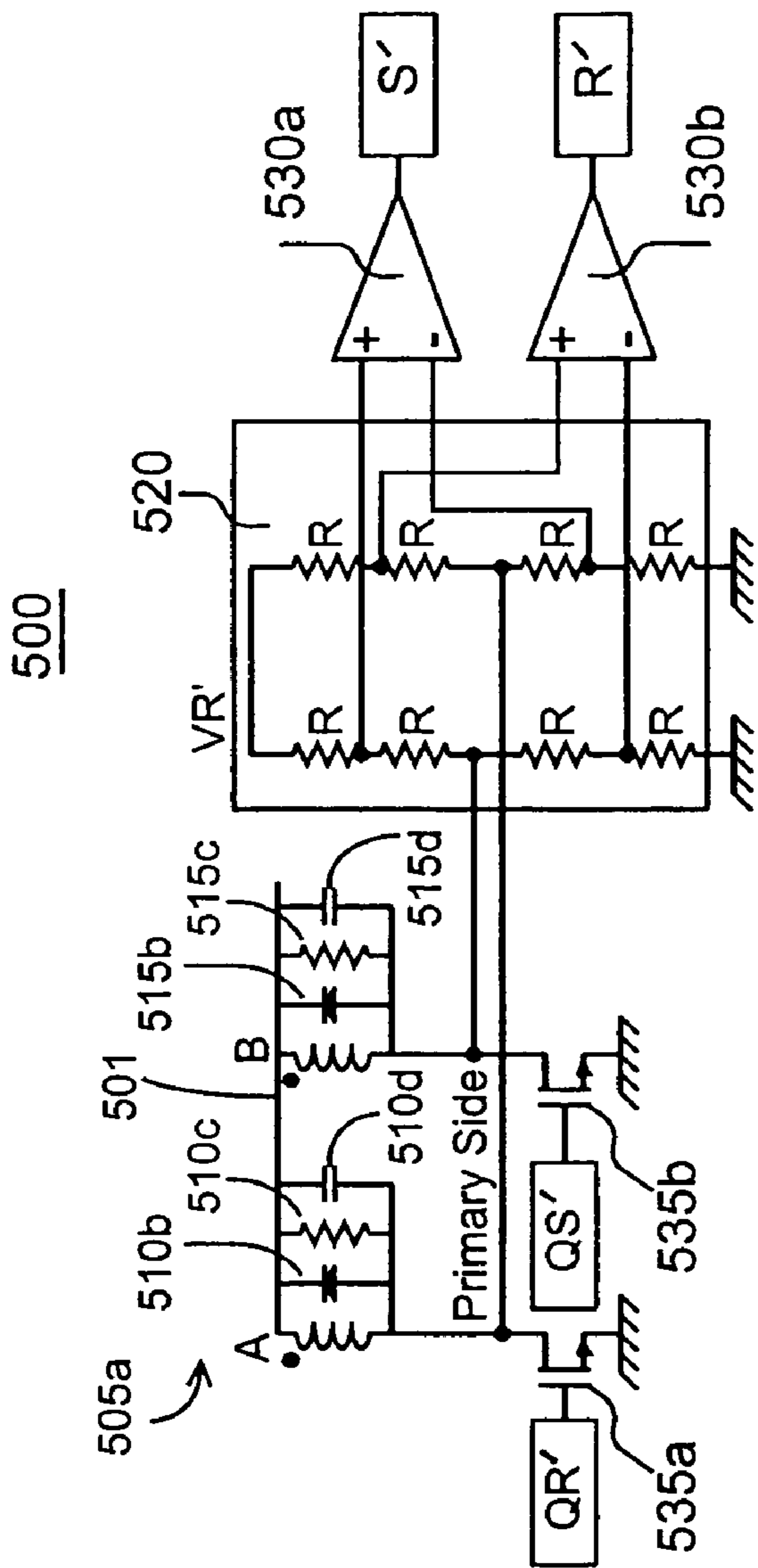


Figure 6a

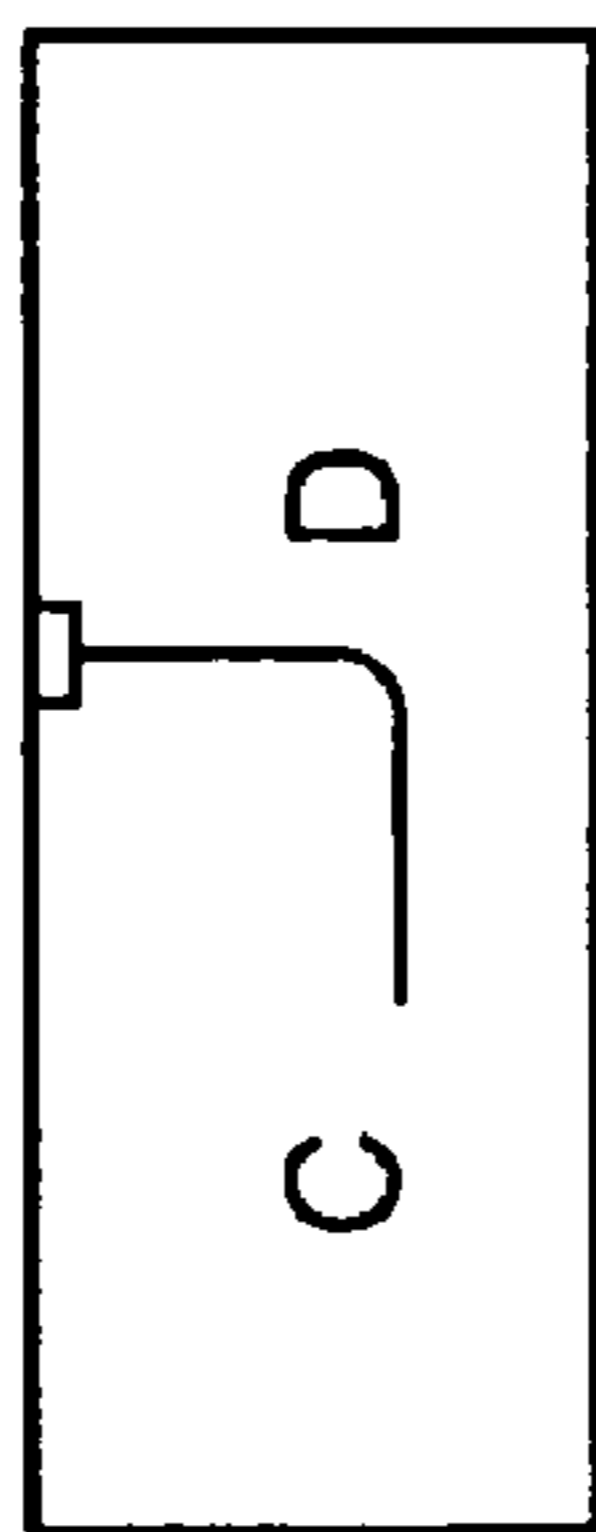


Figure 6b

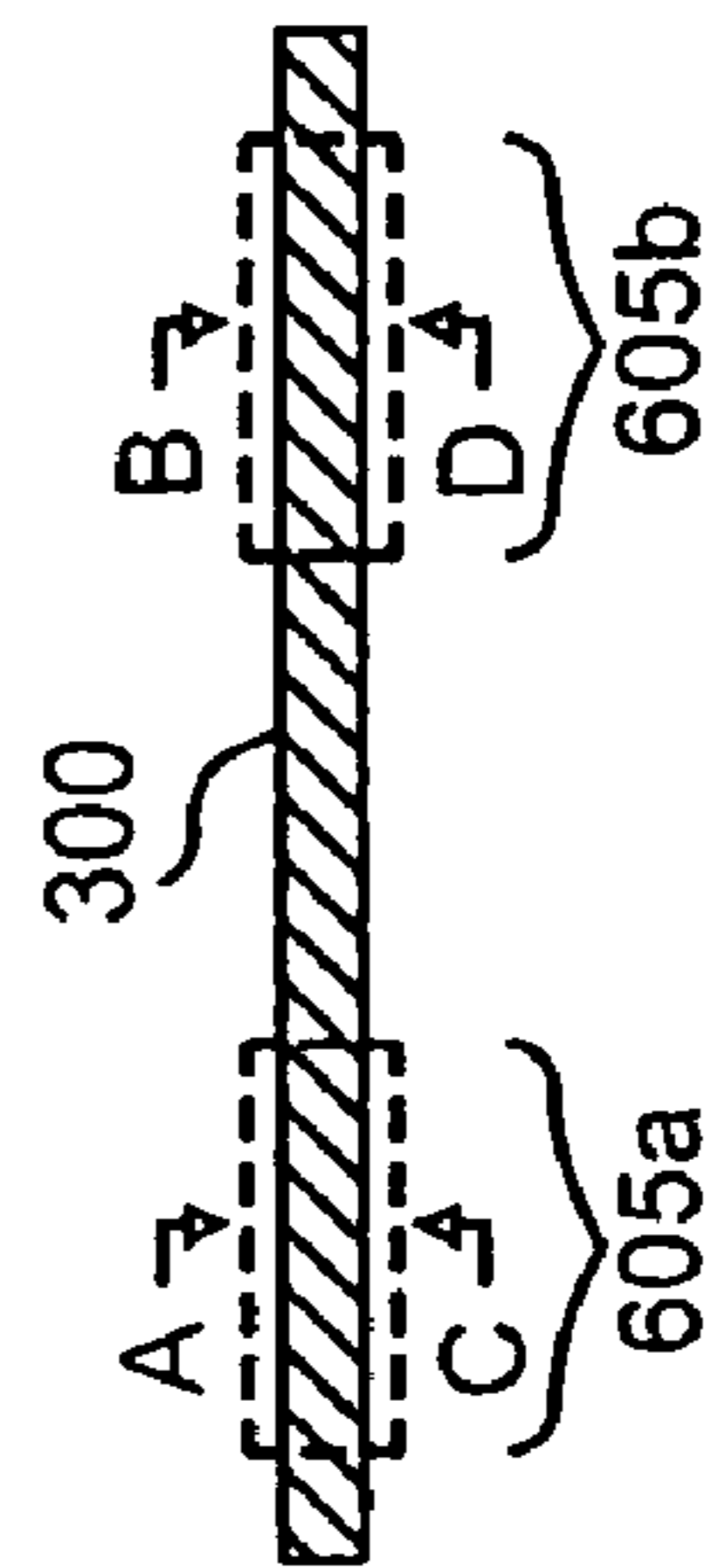


Figure 6c

Figure 5

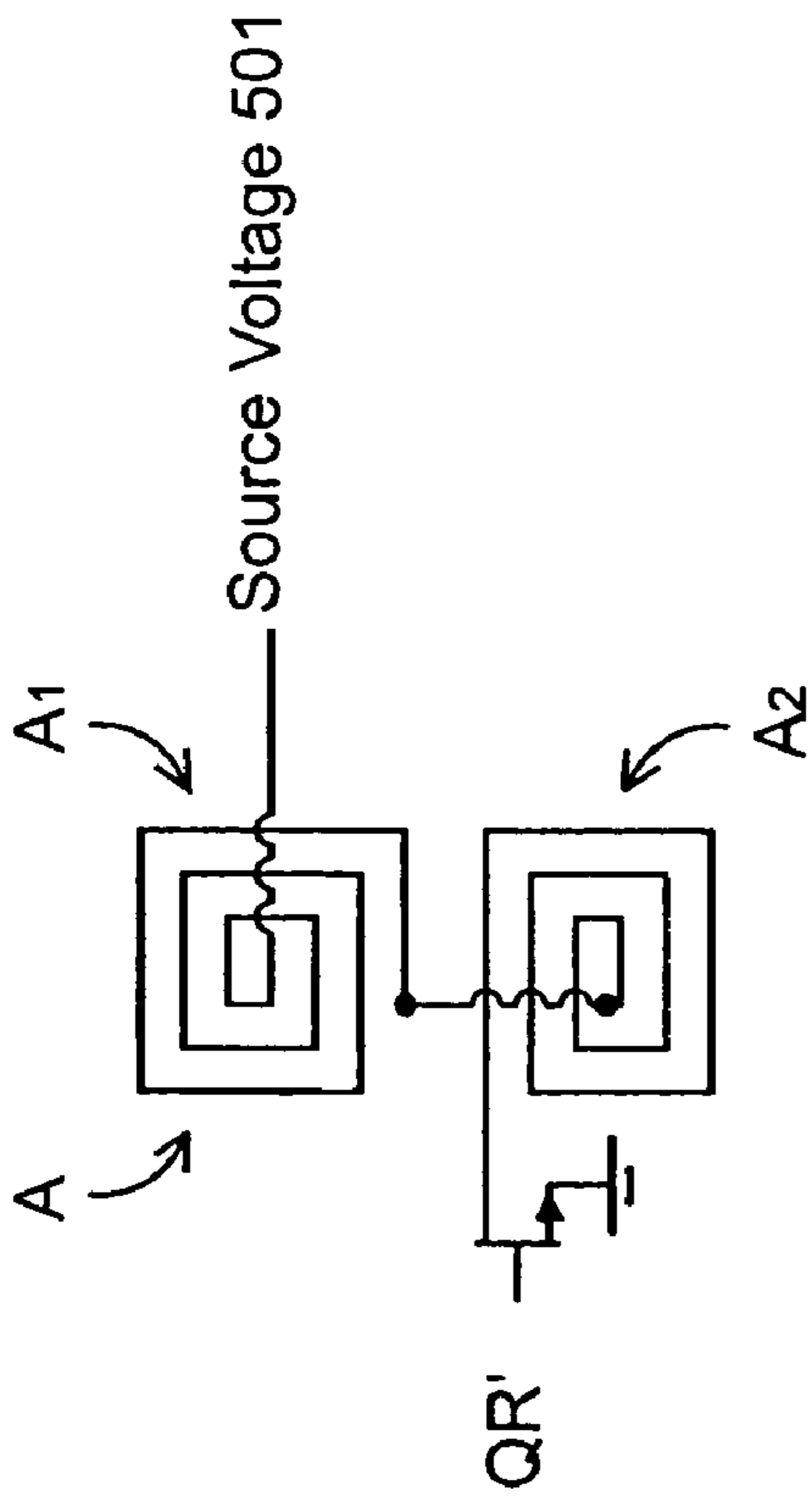
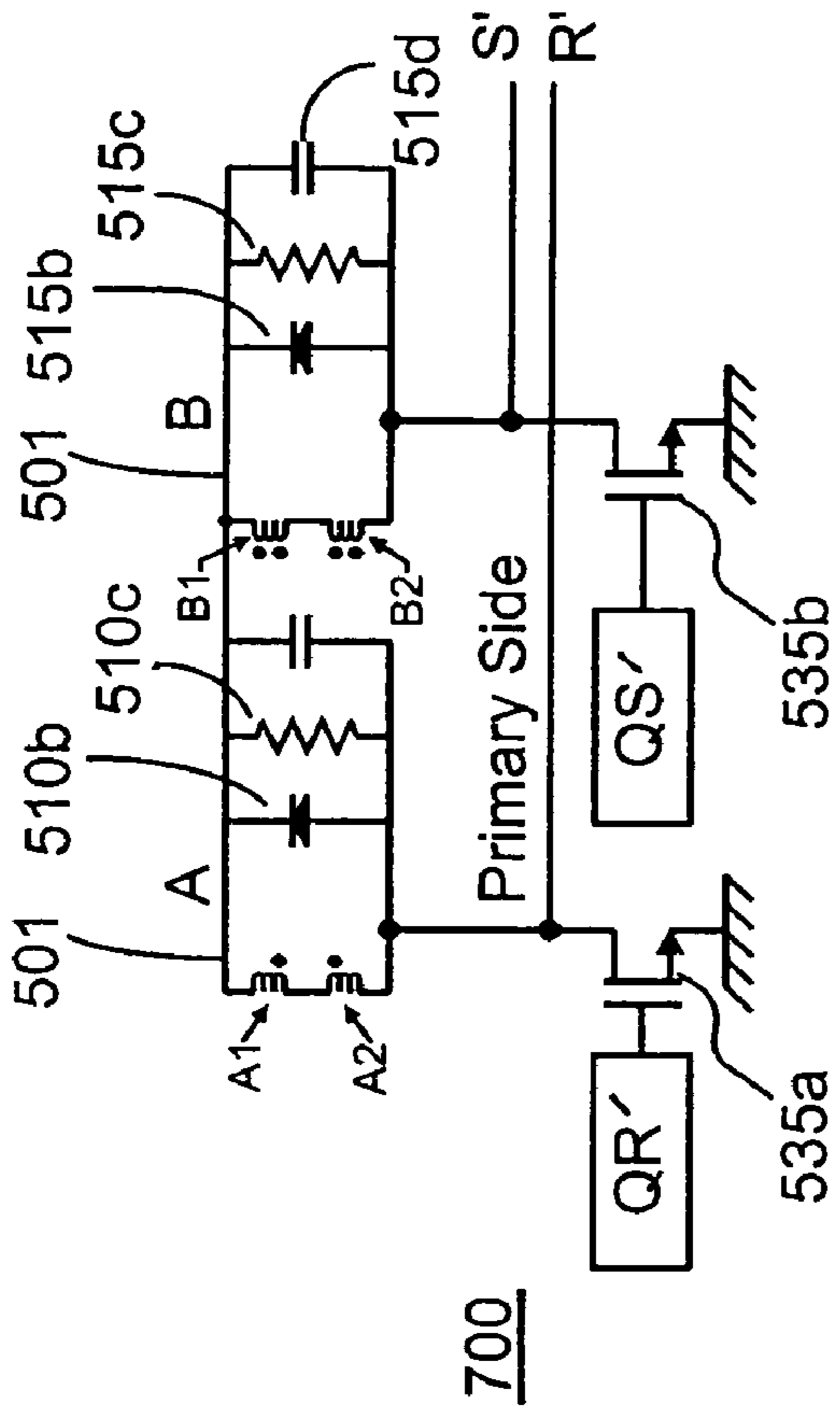


Figure 7b

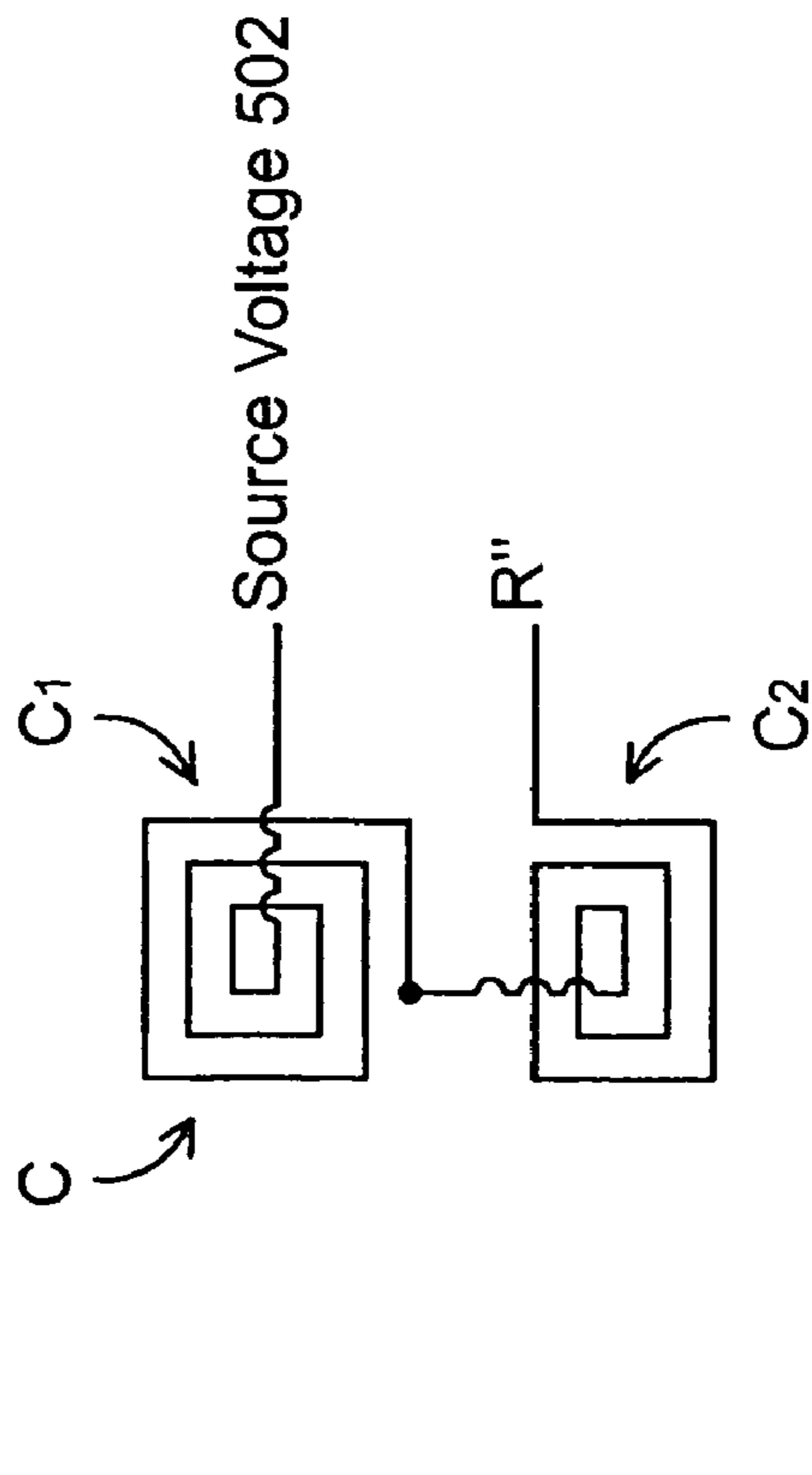
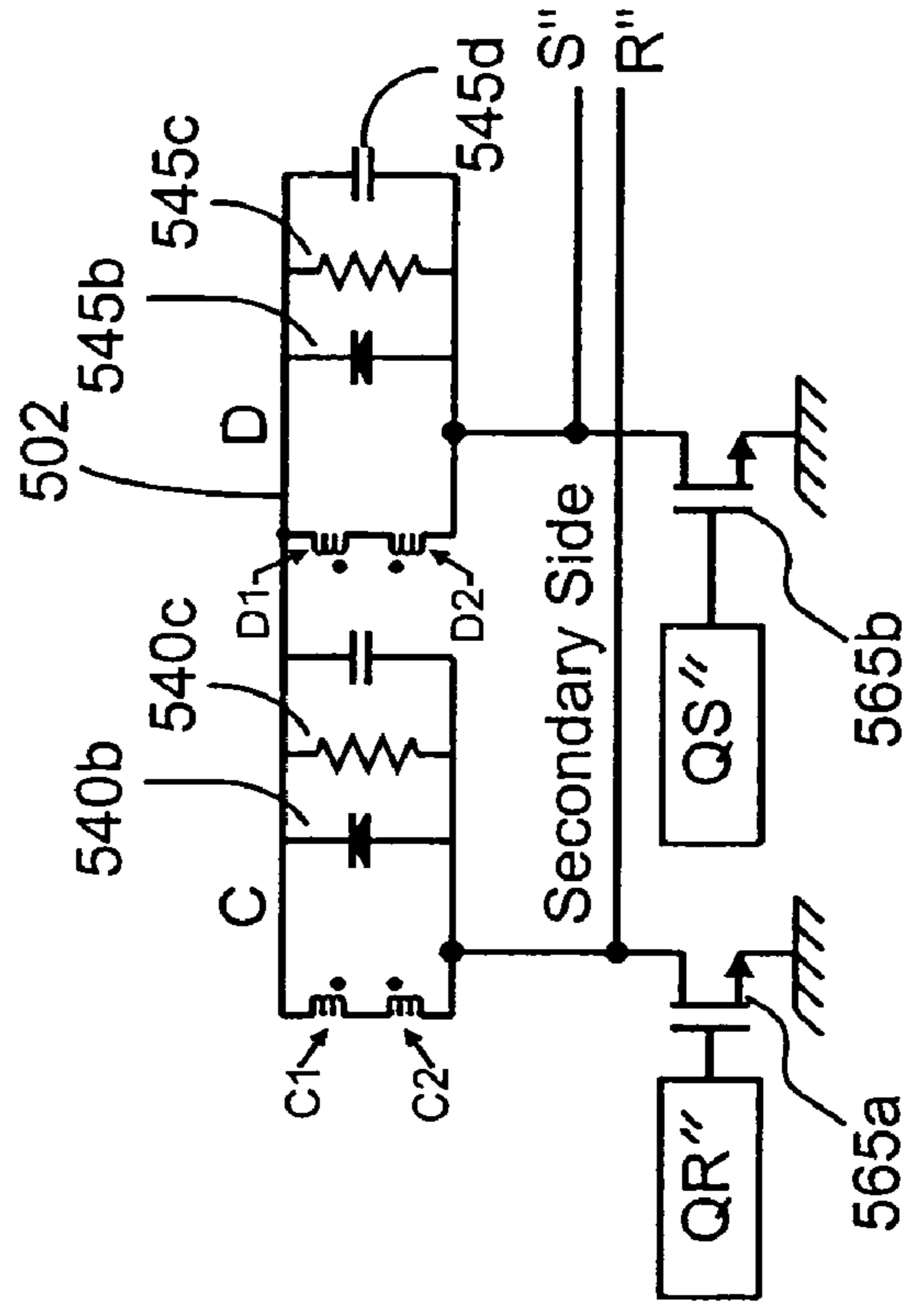


Figure 7c

Figure 7a

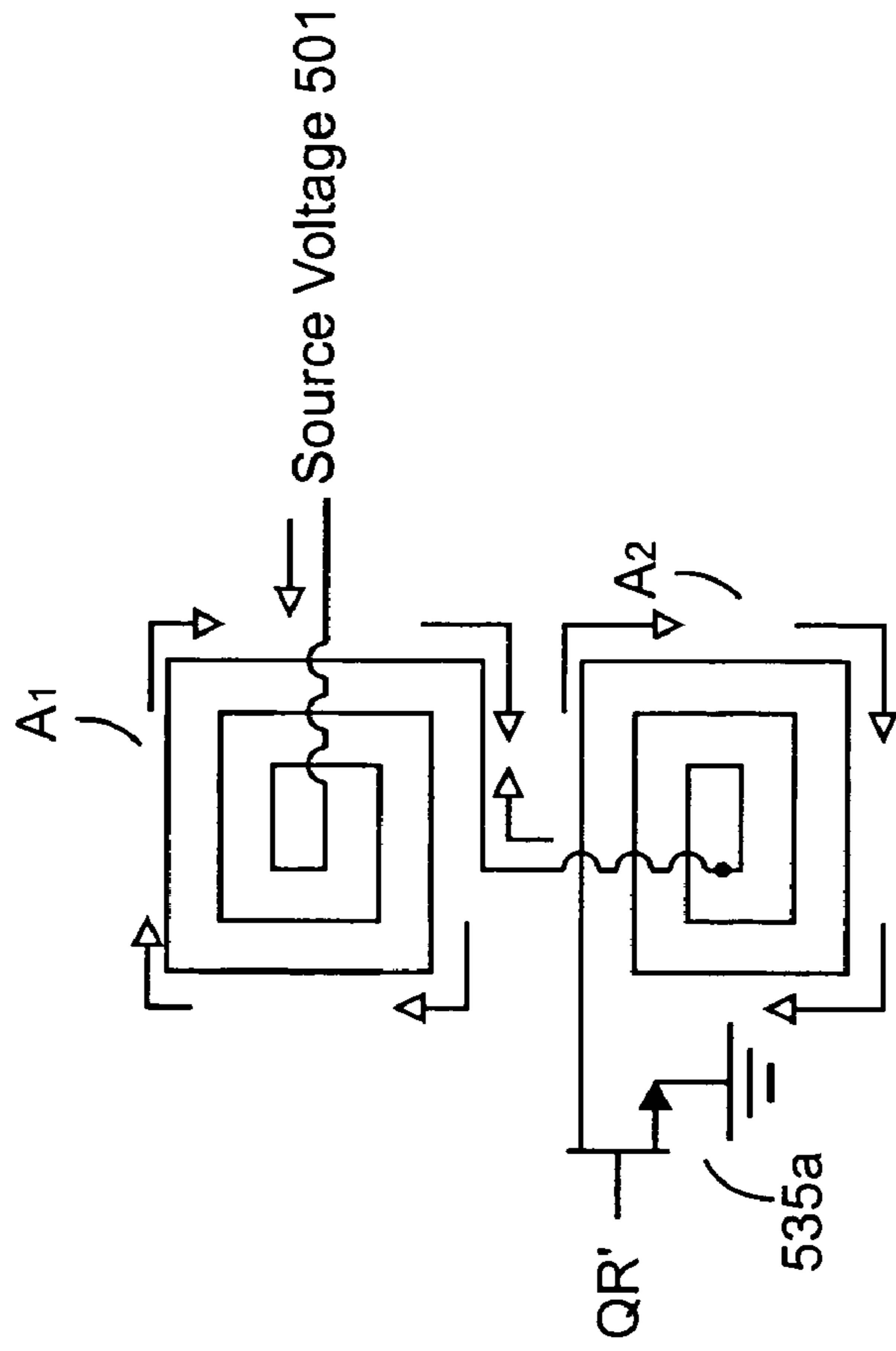


Figure 8b

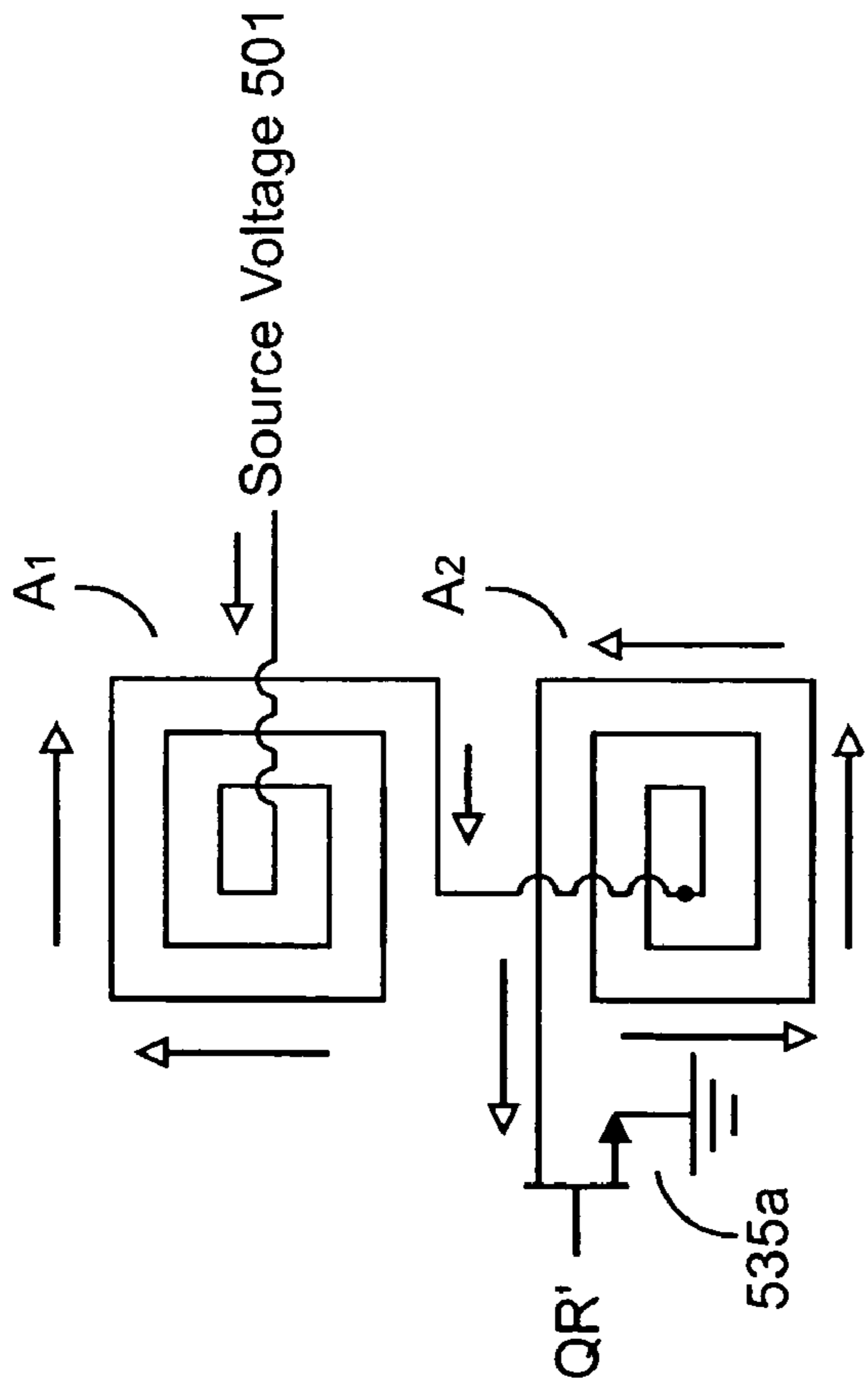


Figure 8a

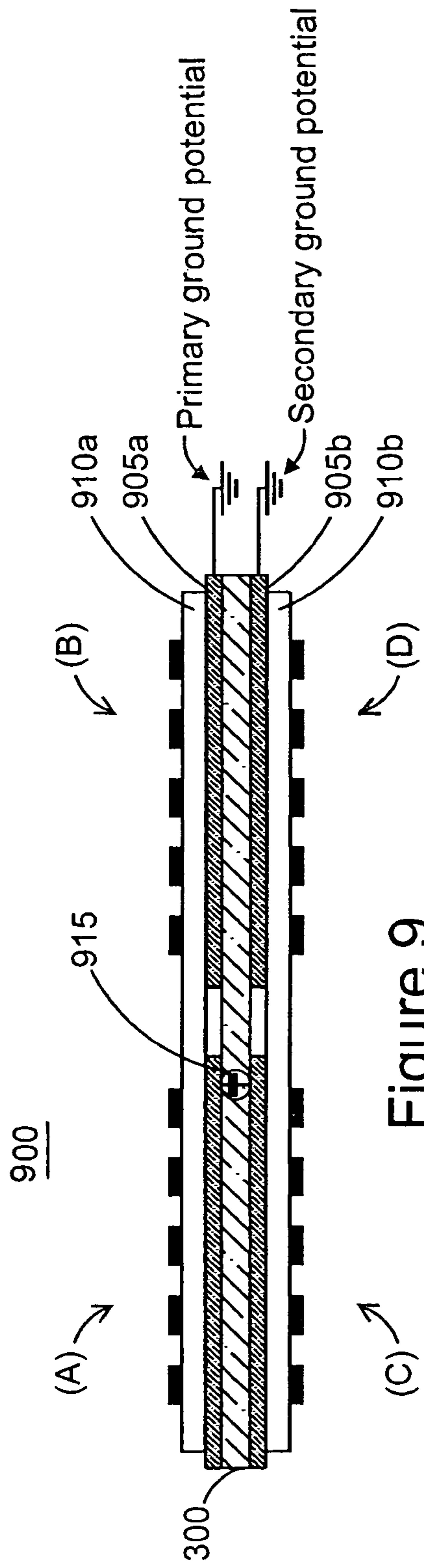


Figure 9

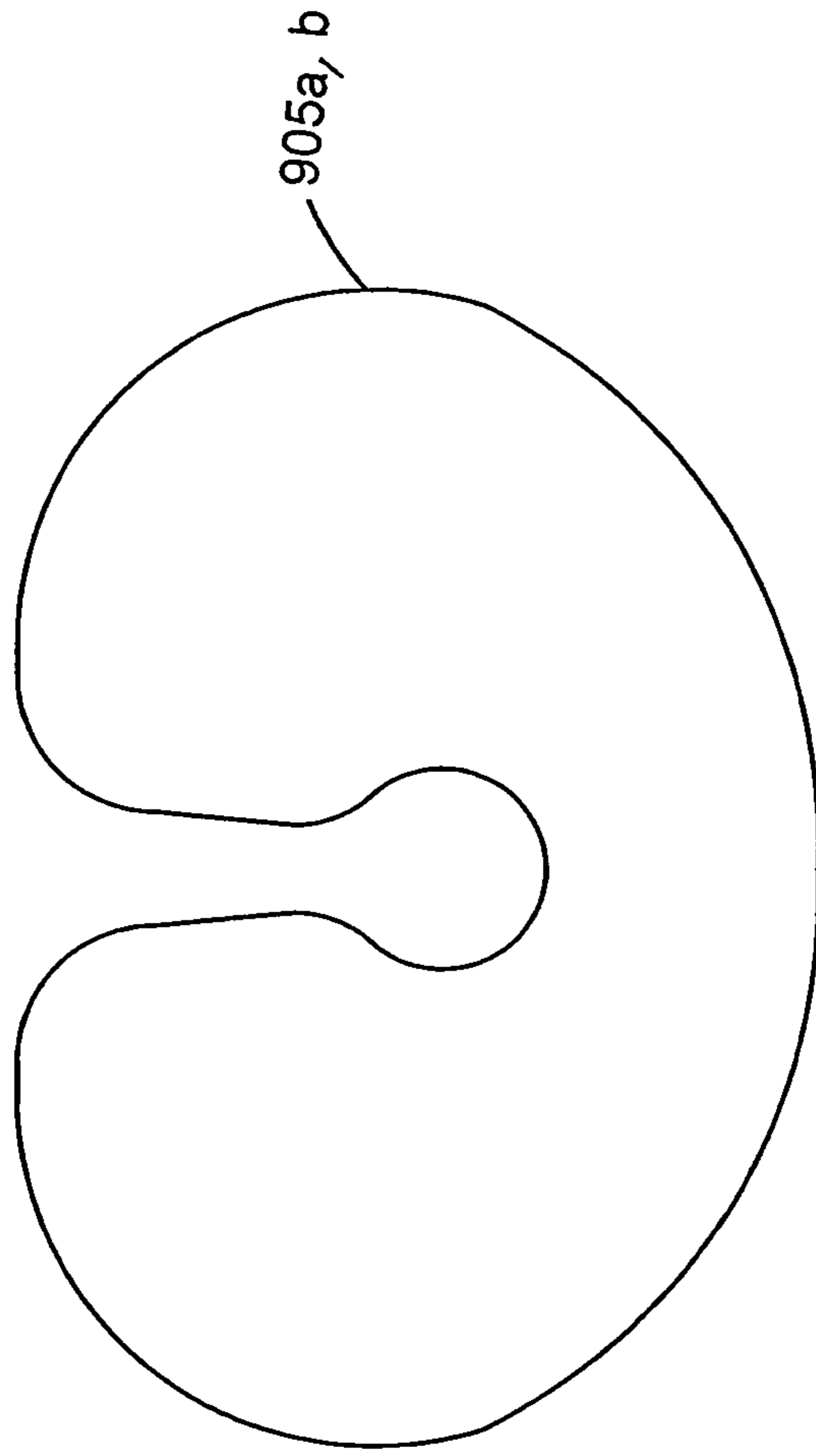


Figure 10

PLANAR TRANSFORMER ARRANGEMENT

CROSS REFERENCE TO RELATED APPLICATIONS

The present application is a divisional of U.S. patent application Ser. No. 10/452,679 filed May 30, 2003, entitled PLANAR TRANSFORMER ARRANGEMENT and is based on and claims the benefit of U.S. Provisional Application No. 60/384,724, filed on May 31, 2002, entitled "PLANAR TRANSFORMER AND DIFFERENTIAL STRUCTURE," and U.S. Provisional Application No. 60/420,914, filed on Oct. 23, 2002, entitled "SWITCHING VOLTAGE REGULATOR FOR SWITCH MODE POWER SUPPLY WITH PLANAR TRANSFORMER," the entire contents of these applications being expressly incorporated herein by reference.

FIELD OF THE INVENTION

The present invention relates to a planar transformer arrangement and method for isolating driver circuitry and communication circuitry to eliminate magnetic field interference and parasitic capacitance.

BACKGROUND INFORMATION

Transformers are often used in floating gate driver circuits for driving high power/voltage switches, for example, high voltage IGBTs for motor control and other applications. In such an application, a transformer provides isolation between low voltage driver circuitry and high voltage power switch circuitry. Such transformers may also be employed to communicate data signals between electrically isolated circuits (e.g., to communicate signals via a transceiver).

Traditionally, high-voltage isolation has required the use of bulky transformers. However, such transformers may be costly, cumbersome, and all transformers may be negatively affected by unwanted common-mode noise, such as noise generated by parasitic capacitances and/or an external magnetic field.

Conventional transformers inherently exhibit two kinds of parasitic capacitances: distributed parasitic capacitances between adjacent windings on a transformer; and interwinding parasitic capacitances between primary and secondary windings of the transformer. These parasitic capacitances result from the close proximity between transformer windings. The magnetic core is generally arranged between the primary and secondary windings of the transformer, so that the magnetic field generated by the transformer may be better conducted. However, operation of the transformer may induce the flow of disadvantageous currents within the magnetic core, if the core, for example, contacts the transformer windings. These currents may result in a degradation of the galvanic insulation between primary and secondary windings.

Furthermore, an externally applied magnetic field may result in disadvantageous common mode magnetic interference within conventional transformers. Such a magnetic field may induce the flow of unwanted currents within the primary and/or secondary windings of the transformer. These common-mode currents may cause a magnetic flux to form around the conductors of the primary and/or secondary windings, thereby inducing noise within the windings.

SUMMARY OF THE INVENTION

It is an object of the present invention to overcome these disadvantages of conventional transformers. To achieve this object, the present invention provides for a planar transformer arrangement, comprising a plurality of meandering windings (e.g., circular or polygonal printed meandering windings) to be arranged on a planar medium (e.g., a printed circuit board or a general interlayer structure (e.g., metal-oxide-metal) of an integrated circuit), such that at least one primary winding of the planar transformer arrangement is provided on one layer (e.g., one side) of the planar medium (e.g., on one layer of a printed circuit board or on one metal layer of a integrated circuit), and at least one secondary winding of the planar transformer arrangement is provided on another layer (e.g., the other side) of the planar medium, the primary and secondary windings forming a planar transformer.

By arranging the planar transformer arrangement in this manner, a dielectric layer of the planar medium (e.g., the printed circuit board or a dielectric oxide layer of the integrated circuit) provides voltage isolation and an open magnetic path between the two primary and secondary windings of the planar transformer arrangement. The voltage isolation provided by the planar medium permits the present invention to be used, for example, in circuits that isolate a gate driver from high voltage IGBT power switches, which may operate at high voltages and at high currents.

In accordance with an exemplary embodiment of the present invention, the planar transformer arrangement includes a second planar transformer comprising at least one second primary winding provided on one layer (e.g., on one side) of the planar medium, and at least one second secondary winding provided on another layer (e.g., the other side) of the planar medium. By placing the two planar transformers in close proximity, a differential amplifier arrangement may be used to detect and compensate for common mode electromagnetic interference applied to the two planar transformers (e.g., to compensate for noise caused by an external magnetic field and/or parasitic capacitance between windings).

In accordance with still another exemplary embodiment of the present invention, the magnetic mode interference is canceled without using a differential amplifier circuit. For this purpose, each of the windings of the planar transformer includes two windings connected in anti-series. In this manner, magnetic common mode interference may be automatically canceled without need for external compensating circuitry, such as a differential amplifier circuit.

In accordance with yet another exemplary embodiment of the present invention, the electromagnetic coupling between the windings of the planar transformer arrangement is improved by providing a magnetic core, for example, a ferrite core, to couple the windings of the two planar transformers. The planar magnetic core may, for example, be applied over the windings of the respective planar transformers on both sides of the planar medium, respectively.

In accordance with still another exemplary embodiment of the present invention, two respective metallic shields are provided between the two windings and coupled respectively to primary and secondary ground voltages. In this manner, the shields help prevent interwinding parasitic capacitance from interfering with the planar transformers by operating to magnetically isolate the magnetic flux produced by the interwinding parasitic capacitance.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of a first exemplary planar transformer arrangement according to the present invention.

FIG. 2 is a block diagram of an exemplary mode interference elimination arrangement according to the present invention.

FIGS. 3a through 3c are top, bottom, and cross-sectional views, respectively, of the exemplary planar transformer shown in FIG. 1.

FIGS. 4a and 4b are exemplary planar transformer arrangements provided with a magnetic core according to the present invention.

FIG. 5 illustrates another exemplary planar transformer arrangement according to the present invention, including a transceiver circuit to drive planar transformer.

FIGS. 6a through 6c are top, bottom, and cross-sectional views of the exemplary planar transformer arrangement shown in FIG. 5.

FIGS. 7a through 7c illustrates yet another exemplary planar transformer arrangement according to the present invention.

FIGS. 8a and 8b illustrate a primary winding connected in anti-series according to the present invention.

FIG. 9 illustrates another exemplary planar transformer arrangement provided with metallic shields according to the present invention.

FIG. 10 is a top view of a metallic shield illustrated in FIG. 9.

DETAILED DESCRIPTION

Referring now to FIG. 1, there is seen a first exemplary planar transformer arrangement 100 according to the present invention. Planar transformer arrangement 100 includes a planar transformer 105 having primary and secondary windings 105a, 105b arranged on respective sides of a planar medium (not shown), e.g., a printed circuit board or an integrated circuit, a single mode detect winding 110 on the same side of the planar medium as the secondary winding 105b, a mode interference elimination circuit 115 electrically connected to the secondary winding 105b of the planar transformer 105 and the single mode detect winding 110.

The exemplary planar transformer arrangement 100 of FIG. 1 is operable to communicate an input signal 120 applied to the primary winding 105a of the planar transformer 105 to an output signal 125, while providing voltage isolation between the input signal 120 and the output signal 125. Specifically, an input signal 120 applied to the primary winding 105a of the planar transformer 105 induces a current flow within the primary winding 105a. The magnetic flux caused by the increasing current flow induces a voltage signal (S) across the secondary winding 105b of the planar transformer 105, which is then transmitted by the mode interference elimination circuit 115 as output signal 125.

The mode interference elimination circuit 115 is also configured to prevent common mode magnetic noise interference from corrupting the signal flow between the input and output signals 120, 125. Referring now to FIG. 2, there is seen an exemplary mode interference elimination circuit 115 according to the present invention for eliminating a common mode magnetic interference caused by an externally applied magnetic field. Mode interference elimination circuit 115 includes a summation circuit 205 having a high impedance positive input 205a electrically connected to the voltage (S) across the secondary winding 105b, and a high impedance

negative input 205b electrically connected to the voltage (R) across the mode detect winding 110.

If an external magnetic field is applied to the planar transformer arrangement 100, a common mode interference voltage will be superimposed on both the voltage (S) across the secondary winding 105b and the voltage (R) across the mode detect winding 110. However, since the interference voltage appears across both windings 105b, 110, the summation circuit 205 operates to cancel the interference voltage effects of the externally applied magnetic field, thereby generating the output signal 125 free of common mode interference.

Referring now to FIGS. 3a through 3c, there is seen top, bottom, and cross-sectional views, respectively, of the exemplary planar transformer 105 and exemplary mode detect winding 110 shown in FIG. 1. As shown in FIGS. 3a through 3c, the windings 105a, 105b, 110 of the exemplary planar transformer arrangement 100 may be implemented, for example, as meandering traces on a planar medium 300 (e.g., a printed circuit board or an integrated circuit), which forms an open magnetic path between the primary and secondary windings 105a, 105b of the planar transformer 105.

Referring now to FIG. 5, there is seen a second exemplary planar transformer arrangement 500 according to the present invention. The planar transformer arrangement 500 includes primary circuitry 505a arranged on one side of a planar medium (not shown) and secondary circuitry 505b arranged on the other side of the planar medium (not shown).

In applications in which the planar medium is an integrated circuit, the primary and secondary circuitry 505a, 505b may be arranged on separate silicon dies or, alternatively, may be arranged on the same silicon die. If the primary and secondary circuitry 505a, 505b are arranged on separate dies, magnetic coupling between the circuitry 505a, 505b may be effected using two metal interconnection layers separated by a dielectric layer.

Planar transformer arrangement 500 is operable as an isolation transceiver to permit input signals (QR') and (QS') of primary circuitry 505a to be communicated as respective output voltage signals (R'') and (S'') of secondary circuitry 505b, and to permit input signals (QR'') and (QS'') of the secondary circuitry 505b to be communicated as respective output voltage signals (R') and (S') of primary circuitry 505a. In this manner, various signals may be communicated between the primary circuitry 505a and the secondary circuitry 505b, while maintaining electrical isolation.

For this purpose, primary circuitry 505a includes a primary winding (A) electrically connected to both the negative input terminal of a comparator 530a and the positive input terminal of a comparator 530b via resistor network 520, and a primary winding (B) electrically connected to both the positive input terminal of the comparator 530a and the negative input terminal of the comparator 530b via the resistor network 520. The first and second primary windings (A), (B) are also electrically connected in parallel to respective diodes 510b, 515b, resistors 510c, 515c, and capacitors 510d, 515d, all of which terminate at source voltage 501.

Secondary circuitry 505b includes a secondary winding (C) electrically connected to both the negative input terminal of a comparator 560a and the positive input terminal of a comparator 560b via resistor network 550, and a secondary winding (D) electrically connected to both the positive input terminal of the comparator 560a and the negative input terminal of the comparator 560b via the resistor network 550. The first and second secondary windings (C), (D) are also electrically connected in parallel to respective diodes 540b, 545b, resistors 540c, 545c, and capacitors 540d, 545d, all of which terminate at source voltage 502.

5

As shown in FIGS. 6a and 6c, each of the primary and secondary windings (A), (B), (C), (D) is implemented as a separate meandering trace on a planar medium 300 (e.g., a printed circuit board or integrated circuit), with primary windings (A), (B) being arranged on one layer (e.g., one side) of planar medium 300 and secondary windings (C), (D) being arranged on another layer (e.g., the other side) of planar medium 300. Specifically, primary winding (A) is arranged over secondary winding (C) to form a first planar transformer 605a, and primary winding (B) is arranged over secondary winding (D) to form a second planar transformer 605b, as shown in FIG. 6c.

In operation, if a pulsed input signal, for example, signal (QR'), is applied to the gate of FET 535a of primary circuitry 505a, a current will be induced within the primary winding (A). The magnetic flux caused by the increasing current flow induces a voltage across the secondary winding (C) of the first planar transformer 605a, which causes the comparator 560b of the secondary circuitry 505b to produce a positive output voltage signal (R").

If the primary windings (A), (B) and the secondary windings (C), (D) are arranged adjacent to one another on respective sides of the planar medium, common mode magnetic interference caused by an externally applied magnetic field will induce an interference voltage across both the secondary windings (C), (D). However, since the output stage of the secondary circuitry 505b includes two differential comparators 560a, 560b, the interference voltage caused by the common mode magnetic field is effectively eliminated. Specifically, the output stage of the secondary circuitry 505b provides the interference voltage to both the positive and negative inputs of the output comparator 560b, thereby canceling the disadvantageous effects of the interference voltage on the output voltage signal (R").

As described above, the magnetic mode interference may be more effectively canceled by arranging the primary windings (A), (B) and the secondary windings (C), (D) adjacent to one another on respective layers of the planar medium. However, it should be appreciated that the primary windings (A), (B) and the secondary windings (C), (D) may be arranged at a distance from one another, if a particular application of the present invention does not require the compensation of effects caused by common mode magnetic field interference.

It should also be appreciated that, although the operation of the exemplary planar transformer arrangement 500 is described only for generating output voltage signal (R") from input voltage signal (QR'), the exemplary planar transformer arrangement 500 operates similarly to produce output signal (S") from input signal (QS'), output signal (R') from input signal (QR"), and output signal (S') from input signal (QS"). In this manner, the exemplary planar transformer arrangement 500 may operate as a transceiver between the primary and secondary circuits 505a, 505b.

Referring now to FIGS. 4a and 4b, there is seen two variants, respectively, of the exemplary planar transformer arrangement 500 shown in FIGS. 5 through 6c. In these exemplary embodiments, the primary windings (A), (B) of planar transformers 605a, 605b and the secondary windings (C), (D) of planar transformers 605a, 605b are provided with respective magnetic cores 405a, 405b (e.g., ferrite) for magnetically coupling the respective windings (A), (B), (C), (D). In this manner, the two windings (A) and (C) of the first planar transformer 605a are coupled through both magnetic cores 405a, 405b and through the open magnetic circuit (e.g., 25 kv/mm) provided by the planar medium 300. Likewise, the two windings (B) and (D) of the second planar transformer

6

605b are coupled by the same two magnetic cores 405a, 405b and by the open magnetic circuit provided by the planar medium 300.

Referring now to FIGS. 7a through 7c, there is seen a third exemplary planar transformer arrangement 700 according to the present invention. In this exemplary embodiment, disadvantageous mode interference is canceled without need for the differential comparators 530a, 530b, 560a, 560b of FIG. 5. For this purpose, each of the primary windings (A), (B) and secondary windings (C), (D) is formed from two sub-windings connected in anti-series. Specifically, primary winding (A) is formed from two sub-windings (A₁), (A₂) connected in anti-series, primary winding (B) is formed from two sub-windings (B₁), (B₂) connected in anti-series, secondary winding (C) is formed from two sub-windings (C₁), (C₂) connected in anti-series, and secondary winding (D) is formed from two sub-windings (D₁), (D₂) connected in anti-series.

In operation, the third exemplary planar transformer arrangement 700 operates similarly to the exemplary planar transformer arrangement 500 of FIG. 5. For example, if a pulsed input signal (QR') is applied to the gate of FET 535a of primary circuitry 505a, a current will be induced within the sub-windings (A₁), (A₂) of the primary winding (A), as shown in FIG. 8a. The magnetic flux caused by the increasing current flow induces a voltage across the sub-windings (C₁), (C₂) of the secondary winding (C), which is output as a positive output voltage signal (R").

If a common mode magnetic field (e.g., noise caused by an external magnetic field) is applied, for example, to primary winding (A), the field will cause a current to flow within the primary winding (A). However, unlike the embodiment shown in FIG. 5, since the sub-windings (A₁), (A₂) of the primary winding (A) are connected in anti-series, the externally applied magnetic field will induce the flow of equal currents in opposite directions through each of the sub-windings (A₁), (A₂), thereby canceling the effects of the common mode interference effects, as shown in FIG. 7b. In this manner, no interference voltages are generated and, as such, no additional circuitry is required to compensate for the effects of the common mode magnetic field.

To help compensate for a noise interference caused by parasitic capacitance, metallic shields may be provided between the windings and the planar medium 300. Referring now to FIG. 9, there is seen an exemplary planar transformer arrangement 900, including respective metallic shields 905a, 905b respectively connected to primary and secondary ground voltages. Transformer arrangement 900 is arranged between the planar medium 300 and respective windings (A), (B) and (C), (D). To electrically isolate the windings (A), (B), (C), (D) from the grounded shields 905a, 905b, respective insulator layers 910a, 910b are arranged between the shields 905a, 905b and the respective windings (A), (B) and (C), (D). Furthermore, to prevent current circulation in the metallic shields 905a, 905b, a slit may be cut into the shields 905a, 905b, as shown in FIG. 10.

By arranging the metallic shields 905a, 905b in this fashion, the interwinding parasitic capacitance 915 is located between the metallic shields 905a, 905b and, in this manner, the interwinding parasitic capacitance is better prevented from interfering with the planar transformers 605a, 605b, since the two shields 905a, 905b operate to magnetically isolate the magnetic flux produced by the interwinding parasitic capacitance 915.

What is claimed is:

1. A planar transformer arrangement to provide isolation between an input signal and an output signal, the planar transformer arrangement comprising:

7

a planar dielectric medium having a first side and a second side;

at least two meandering primary windings arranged on the first side of the planar medium, a current flow being induced within the primary windings in accordance with the input signal; and

at least two meandering secondary windings arranged on the second side of the planar medium, the primary and secondary windings forming a planar transformer, whereby a voltage is induced across the secondary windings in accordance with the current flow within the primary windings; and

wherein the planar medium provides a voltage isolation between the primary and secondary windings, and wherein the planar medium is an integrated circuit.

8

2. The planar transformer arrangement of claim 1, wherein each of the primary and secondary windings includes at least two sub windings.

3. The planar transformer arrangement of claim 2, wherein the at least two sub windings are connected in anti-series.

4. The planar transformer arrangement of claim 3, wherein if a common mode magnetic field is applied to the primary windings causing a current to flow within the primary windings, a flow of equal currents in opposite directions will be induced through each of the sub-windings, thereby canceling interference effects of the common mode magnetic field and preventing generation of interference voltages.

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