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**Miller**

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(54) **UNIFORM THERMAL PROCESSING BY  
INTERNAL IMPEDANCE HEATING OF  
ELONGATED SUBSTRATES**

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(US)

U.S. Appl. No. 10/782,545, titled "High Throughput Surface Treatment on Coiled Flexible Substrates", filed Feb. 19, 2004, (NSL-025).

(73) Assignee: **Nanosolar, Inc.**, Palo Alto, CA (US)

U.S. Appl. No. 10/782,017, titled "Solution-Based Fabrication of Photovoltaic Cell", filed Feb. 19, 2004, (NSL-029).

(\* ) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 443 days.

U.S. Appl. No. 10/943,658, titled "Formation of CIGS Absorber Layer Materials Using Atomic Layer Deposition and High Throughput Surface Treatment", filed Sep. 18, 2004, (NSL-035).

U.S. Appl. No. 10/943,685, titled "Formation of CIGS Absorber Layers on Foil Substrates", filed Sep. 18, 2004 (NSL-038).

(21) Appl. No.: **10/943,659**

\* cited by examiner

(22) Filed: **Sep. 18, 2004**

*Primary Examiner*—Daniel Robinson

(51) **Int. Cl.**  
**H05B 6/60** (2006.01)  
**H05B 6/10** (2006.01)

(74) *Attorney, Agent, or Firm*—Joshua D. Isenberg; JDI Patent

(52) **U.S. Cl.** ..... **219/645**; 219/646

(57) **ABSTRACT**

(58) **Field of Classification Search** ..... 219/645,  
219/646, 635, 637, 643, 619, 773, 216; **H05B 6/60**  
See application file for complete search history.

An elongated substrate may be heated in a roll processing system. At least a portion of the elongated substrate is loaded into the roll processing system. A sufficient electrical current is caused to flow in the portion of the elongated substrate to heat the portion to a desired temperature. The heating may be either resistive or inductive. The roll processing system may be a roll-to-roll type where the substrate moves as a portion of it is heated. Alternatively, the substrate may be wound into a coiled substrate and the turns of the coil insulated against undesired electrical contact. The entire coiled substrate may then be heated either resistively or inductively.

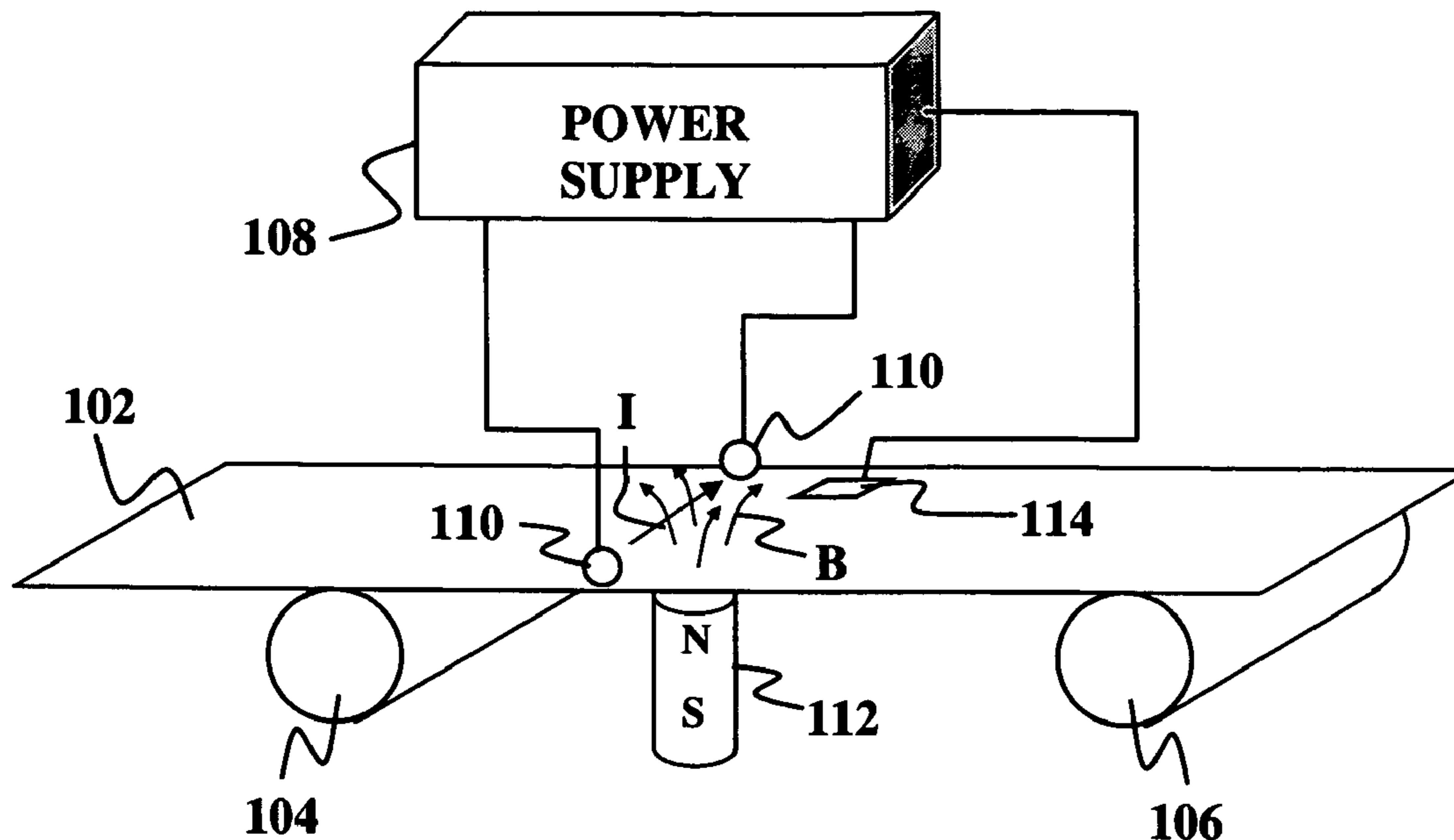
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**23 Claims, 3 Drawing Sheets**

**100**



100

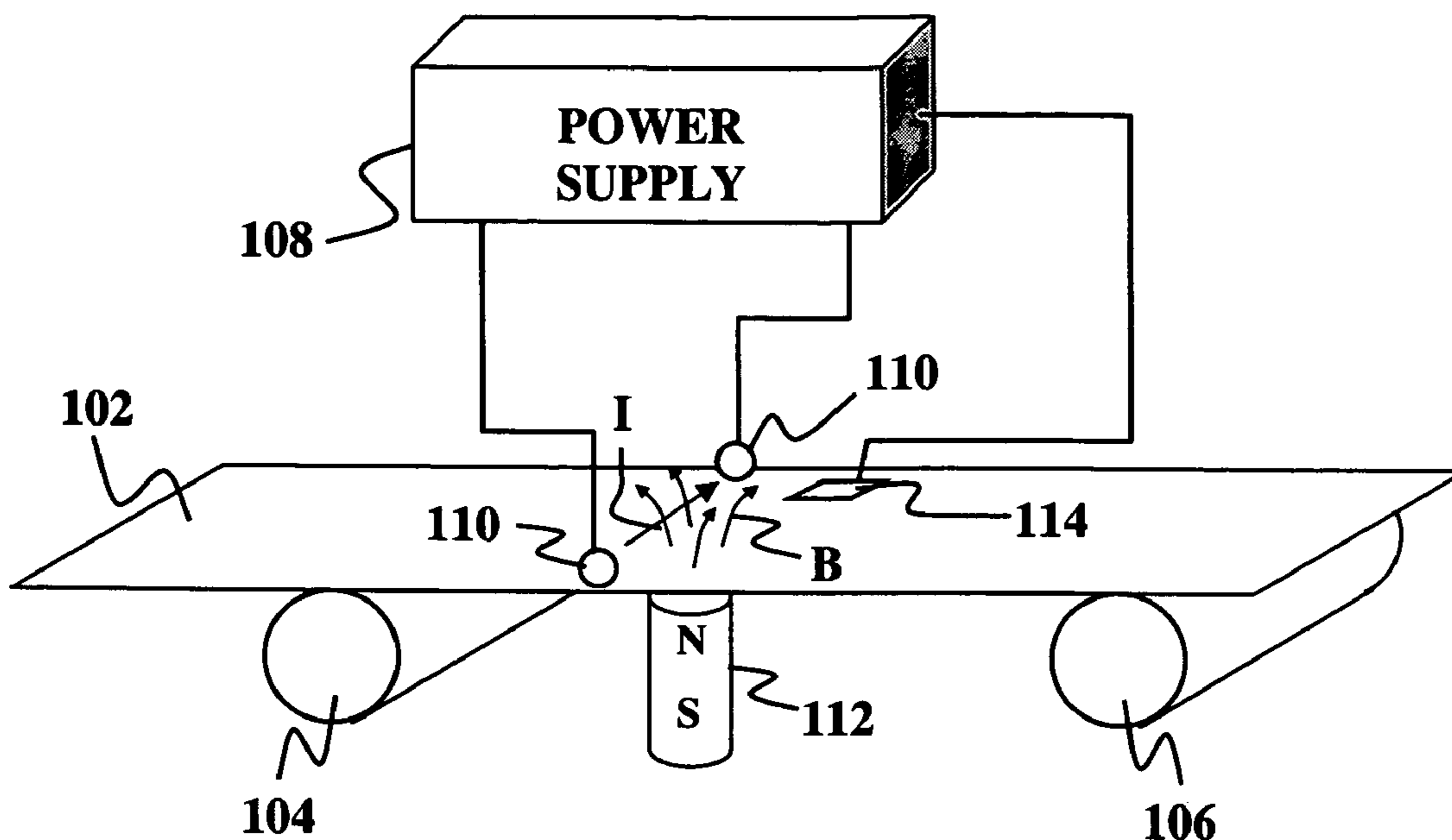


FIG. 1

200

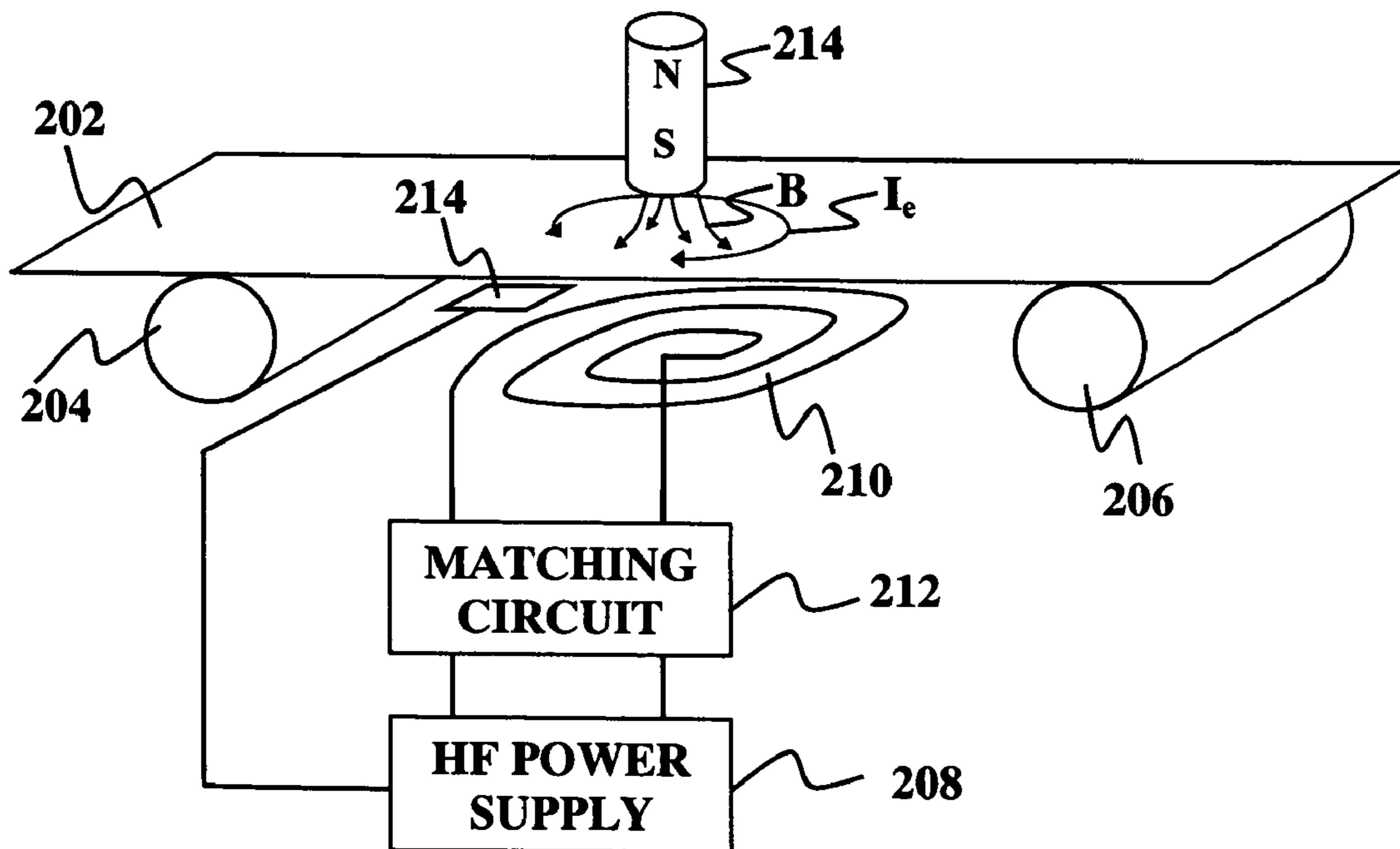


FIG. 2

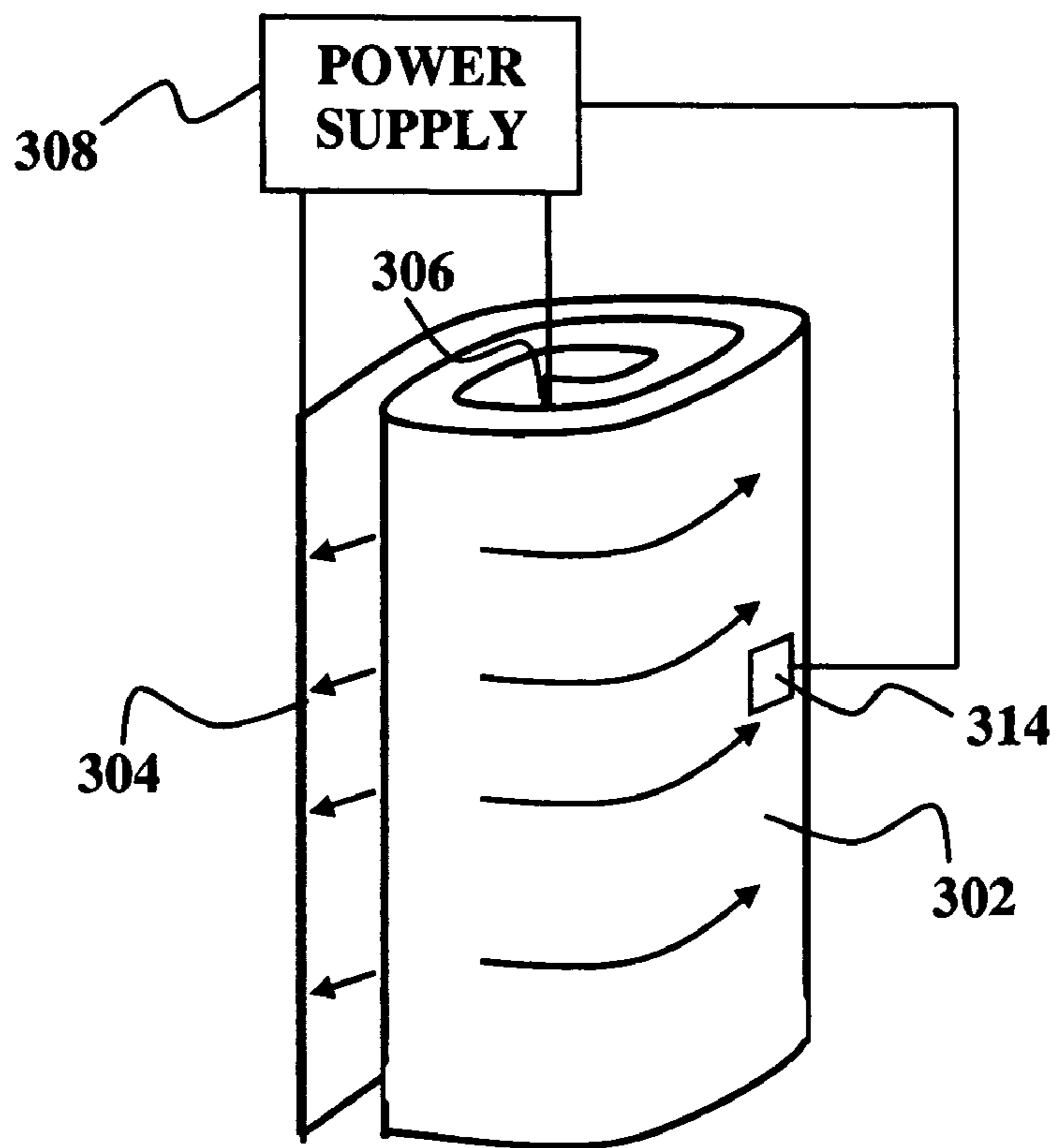


FIG. 3A

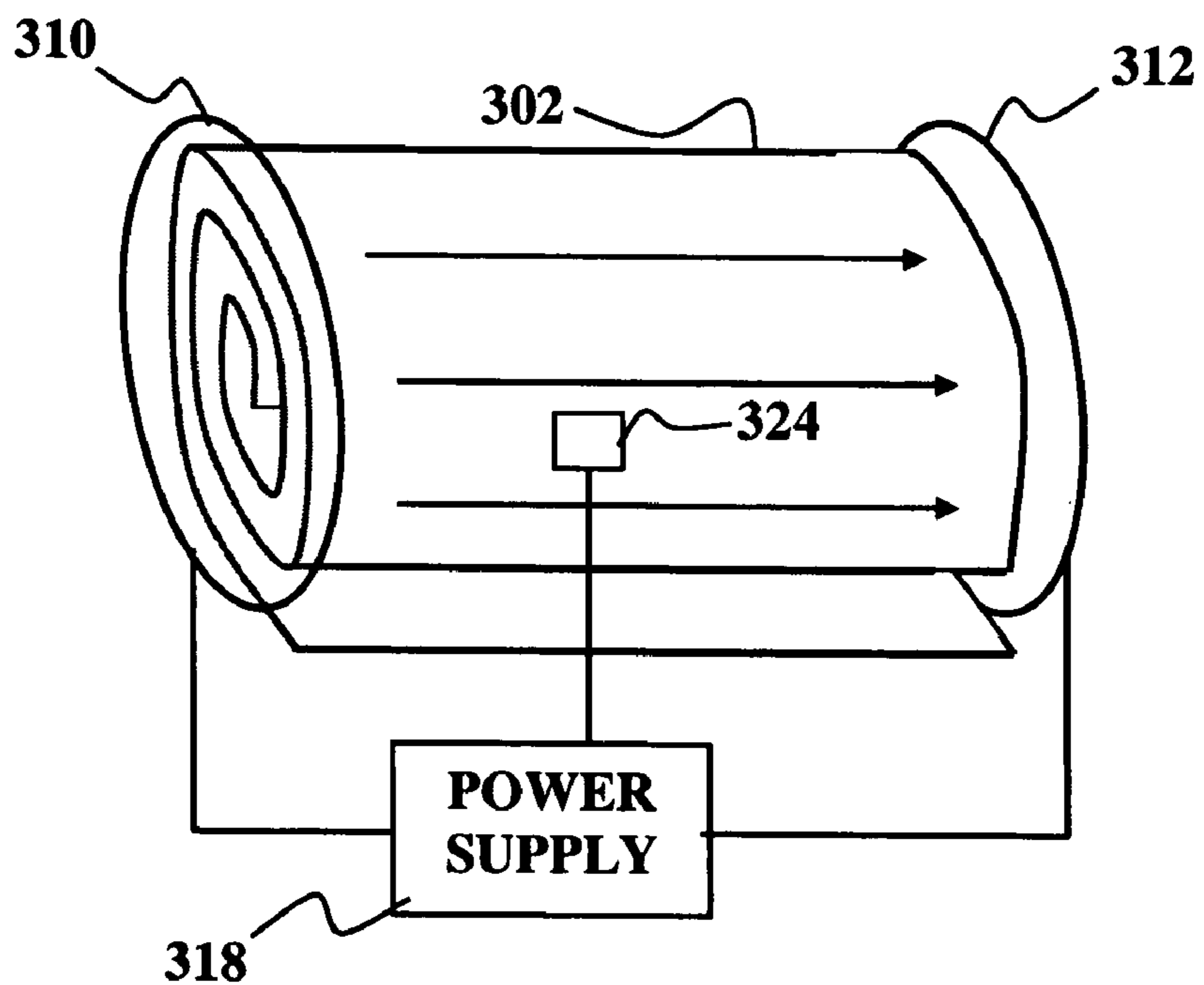


FIG. 3B

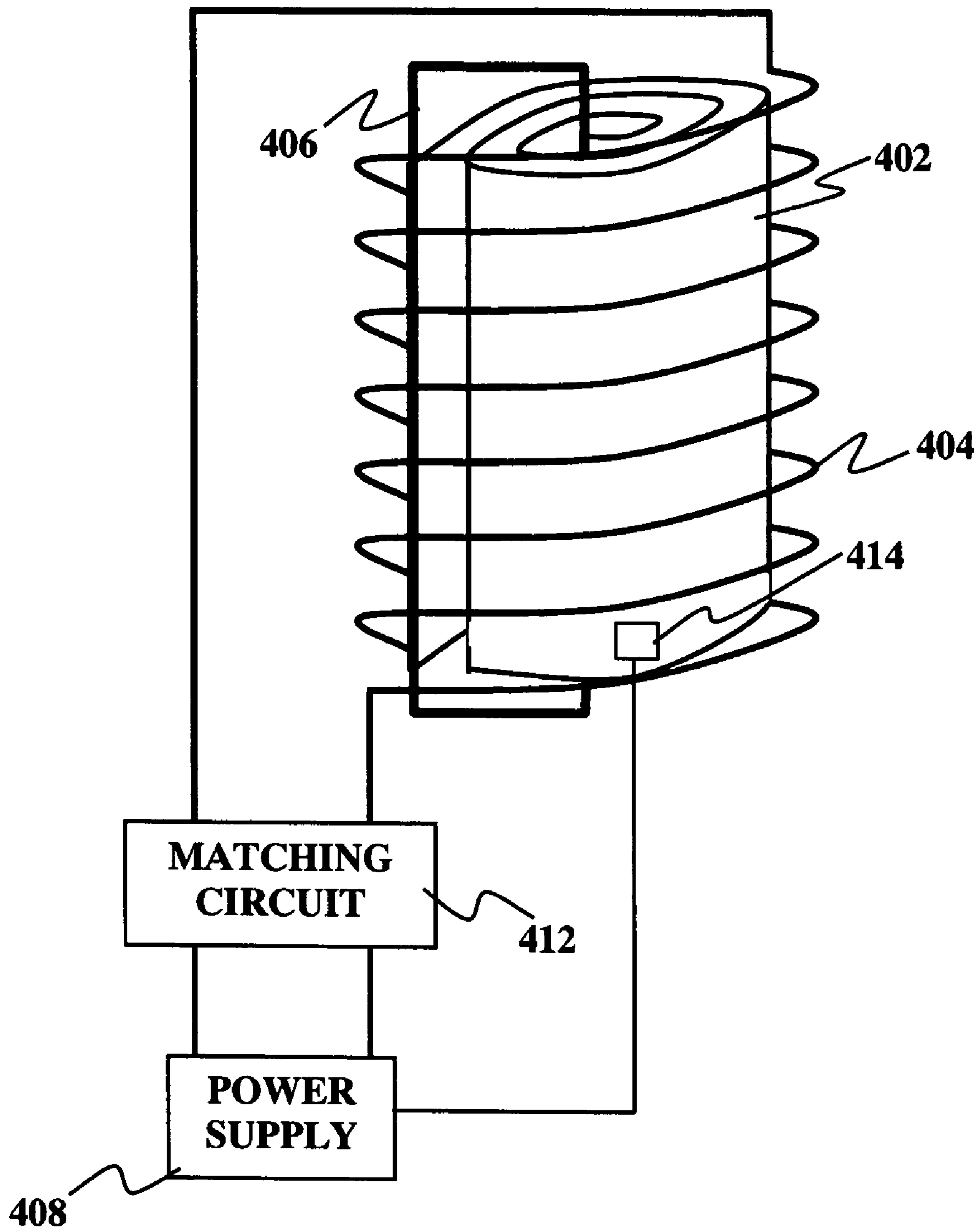


FIG. 4

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## UNIFORM THERMAL PROCESSING BY INTERNAL IMPEDANCE HEATING OF ELONGATED SUBSTRATES

### CROSS-REFERENCE TO RELATED APPLICATION

This application is related to commonly-assigned, co-  
pending application Ser. No. 10/943,685, entitled "FORMA-  
TION OF SOLAR CELLS ON FOIL SUBSTRATES" which is filed the same day as the present application the  
entire disclosures of which are incorporated herein by ref-  
erence. This application is also related to U.S. patent appli-  
cation Ser. No. 10/782,545, filed Feb. 19, 2004, entitled  
"HIGH THROUGHPUT SURFACE TREATMENT ON  
COILED FLEXIBLE SUBSTRATES", the entire disclo-  
sures of which are incorporated herein by reference.

### FIELD OF THE INVENTION

The present invention is related to substrate processing  
and more particularly to heating elongated substrates during  
processing.

### BACKGROUND OF THE INVENTION

Substrate processing typically involves forming structures  
on a substrate by formation of a sequence of layers of  
material on a substrate. Often the layer formation processes  
involve heating the substrate, e.g., to anneal a layer of  
material. In the semiconductor industry, substrates are often  
silicon wafers that are 300 mm in diameter or less. Such  
substrates may be easily heated using standard semiconduc-  
tor processing equipment.

In the past, photovoltaic devices, such as solar cells, were  
made on silicon substrates and processed much like semi-  
conductor integrated circuits. Recently, however, in an effort  
to reduce the cost of solar cells, the solar cell industry has  
been trying to develop techniques for high-volume fabrica-  
tion of solar cells, e.g. using roll-to-roll processing. Such  
techniques often use convective heating or radiative heating  
(e.g., with infrared lamps). Unfortunately, these prior art  
techniques often produce non-homogenous heating of the  
substrate. For example, in a standard furnace, a roll of  
devices would experience a large temperature gradient  
depending on whether the 'layer' in question is near the  
inside or outside of the roll. In addition, these heating  
techniques can be difficult to design and expensive to  
implement.

Thus, there is a need in the art, for a method of uniform  
heating of large area substrates.

### BRIEF DESCRIPTION OF THE DRAWINGS

The teachings of the present invention can be readily  
understood by considering the following detailed descrip-  
tion in conjunction with the accompanying drawings, in  
which:

FIG. 1 is a schematic diagram of an apparatus for resistive  
heating of an elongated substrate according to an embodi-  
ment of the present invention.

FIG. 2 is a schematic diagram of an apparatus for induc-  
tive heating of an elongated substrate according to an  
alternative embodiment of the present invention.

FIG. 3A is a schematic diagram illustrating resistive  
heating along the length of a coiled elongated substrate  
according to an alternative embodiment of the present  
invention.

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FIG. 3B is a schematic diagram illustrating resistive  
heating across the width of a coiled elongated substrate  
according to an alternative embodiment of the present  
invention.

FIG. 4 is a schematic diagram illustrating inductive heat-  
ing of a coiled elongated substrate according to an alterna-  
tive embodiment of the present invention.

### DESCRIPTION OF THE SPECIFIC EMBODIMENTS

Although the following detailed description contains  
many specific details for the purposes of illustration, anyone  
of ordinary skill in the art will appreciate that many varia-  
tions and alterations to the following details are within the  
scope of the invention. Accordingly, the exemplary embodi-  
ments of the invention described below are set forth without  
any loss of generality to, and without imposing limitations  
upon, the claimed invention.

According to embodiments of the present invention an  
elongated substrate may be heated in a roll processing  
system. At least a portion of the elongated substrate is loaded  
into the roll processing system. A sufficient electrical current  
is caused to flow in the portion of the elongated substrate to  
heat the portion to a desired temperature. The heating may  
be either resistive or inductive. The roll processing system  
may be a roll-to-roll type where the substrate moves as a  
portion of it is heated. Alternatively, the roll processing  
system may be a type in which the elongated substrate is  
wound into a coiled substrate and the turns of the coiled  
substrate are insulated against undesired electrical contact.  
The entire coiled substrate may then be heated either resis-  
tively or inductively. Examples of embodiments of the  
present invention are described below and illustrated in FIG.  
1 through FIG. 4.

FIG. 1 depicts a roll-to-roll processing apparatus 100  
according to a first embodiment of the present invention. In  
the apparatus 100 an elongated substrate 102 moves from a  
first roller 104 to a second roller 106. One or both of the  
rollers may be motorized to impart movement to the elon-  
gated substrate 102. The substrate 102 may be provided to  
the apparatus 100 from a feed roll (not shown). The elon-  
gated substrate 102 is preferably made of sheet of an  
electrically conductive material, e.g., a metal such as alu-  
minum, stainless steel, copper, molybdenum, etc. Alterna-  
tively, the substrate 102 may include multiple layers, at least  
one of which is an electrically conductive material layer. The  
substrate 102 may include one or more electronic or photo-  
voltaic devices that are to be heated. The substrate 102 is  
preferably able to handle the current required to dissipate the  
necessary power to heat the devices. The substrate 102 may  
be a 'transfer' or 'host' that enhances the heating properties  
of another substrate that is attached to it.

An electric power supply 108 is electrically coupled to a  
portion of the elongated substrate 102 via leads 110. The  
power supply 108 may be a direct current (DC) supply or an  
alternating current (AC) supply. In the example depicted in  
FIG. 1, the leads 110 make electrical contact at or near the  
edges of the substrate 102. When a voltage is applied  
between the leads 110 an electric current I flows widthwise  
through the substrate 102 between leads 110. Alternatively,  
the leads 110 may be configured such that the current I flows  
along the length of the substrate 102. For example, leads  
may be incorporated into the first and second rollers 104,  
106 so that the current I flows between them through the  
substrate 102. A temperature or current flux sensor 114 or

array of sensors may be employed to form a closed control loop to adjust the output of the power supply **108**.

The voltage between the leads **110** is such that the current  $I$  dissipates a power equal to  $I^2R$ , where  $R$  is the resistance of the substrate **102** (or that portion of the substrate through which the current flows). The power density (power divided by the area of the substrate through which the current flows) must be high enough locally to appropriately heat the desired portion of the substrate **102** and any devices formed on it.

The leads **110** may be in the form of rollers or sliding contacts that permit the substrate to move past as the current flows between the leads **110**. The leads **110** preferably make contact over a suitable length of the substrate **102** so that the current  $I$  is neither too concentrated nor too widely dispersed within the substrate **102**. In the example depicted in FIG. **1** two leads **110** (one lead on each side of the substrate **102**) are shown for the sake of clarity. A greater number of leads may be used to spread out the current over a greater length of the substrate **102**. One or more magnets **112** may provide a magnetic field  $B$  that focuses or defocuses the current  $I$  so that the substrate **102** is uniformly heated. It is preferable that electromagnets have an adjustable field controlled by an array of temperature and/or current flux sensors **114** which may serve in a closed loop control system with a magnet controller (not shown). The magnet controller may adjust the magnetic field  $B$  by adjusting current to an electromagnet or by changing the position or orientation of the magnets **112**. Although a single power supply and a single pair of leads are depicted, those of skill in the art will recognize that the above embodiment may be implemented using multiple power supplies connected to multiple pairs of leads.

FIG. **2** depicts an alternative roll-to-roll processing apparatus **200** according to a second embodiment of the present invention. In this embodiment, an elongated substrate **202** moves past rollers **204**, **206** much as described above. However, instead of electrical leads, the substrate moves past an inductor **210** that is disposed proximate a surface of the substrate **202**. The inductor may be disposed either above or below the substrate **202**. The inductor **210** is connected to a high-frequency (HF) power supply **208**, where the frequency range is about 1 KHz or greater. The inductor **210** may be in the form of a substantially flat coil having multiple turns. Preferably, the inductor spans the width of the substrate **210**. When the HF power supply **208** energizes the inductor with HF power eddy currents  $I_e$  are induced in the substrate **202**. If sufficient HF power is applied to the inductor **210**, the resulting eddy currents can heat the substrate **202** to the desired temperature. The frequency of the HF power may be selected to optimize or allow the substrate to have an impedance in a range that provides an efficient transfer of power by induction to the substrate **202**. An HF matching circuit **212** may be coupled between the HF power supply **208** and the inductor **210** to maximize power transfer to the inductors. A temperature sensing circuit **214** may optionally be employed to ensure that the frequency of the HF power is optimal for the substrate material and geometry. The temperature sensing circuit **214** senses the temperature of the substrate **202** and feeds back a corresponding signal to the power supply **208**. By way of example, the sensor **214** may be a temperature sensor of any suitable type, e.g., a thermocouple, thermistor, solid-state infrared sensor, and the like. Alternatively, the sensor **214** may be a current flux sensor and/or magnetic field sensor (e.g. configured as a Hall effect sensor) can be used. Combinations of such sensors or arrays of sensors can also be used. The sensing circuit **214** ensures that the HF

power and/or frequency are optimal for the substrate material and geometry. This circuitry would allow a closed-loop control situation to ensure stability of substrate heating by the apparatus **200**. In addition, one or more magnets **216** may optionally provide a magnetic field  $B$  that focuses or defocuses the eddy currents  $I_e$ . The magnets/electromagnets **216** may be in a closed loop control system comprised in part of a sensing circuit based on temperature and/or current flux at or near a local position.

An advantage of the apparatus **200** is that the substrate **202** can be heated without direct contact between the substrate **202** and the inductor **210**. Inductively coupled power transfer eliminates complex substrate contacting equipment and bypass issues associated with them in a continuous process. This would improve the speed at which a continuous process could operate and would eliminate additional contacting equipment. In order to increase the temperature of the substrate, a higher HF power may be used by simply increasing the power output on the power supply. Alternatively, the frequency of the HF power may be changed to increase or lower the impedance of the substrate, which in turn would affect the rate of temperature change. This would allow such a process to work on a wide variety of substrate materials with a multitude of conductivities without requiring a re-design of power supplies and other equipment. In particular, through the use of a variable frequency, the impedance of a substrate can be changed, resulting in a requirement for less current even for the same power dissipation, which allows both thinner materials and/or materials with higher conductivities to be employed.

In the embodiments depicted in FIG. **1** and FIG. **2**, a portion of the substrate is heated as it moves past electrical leads or inductors. As stated above, in alternative embodiments of the present invention an elongated substrate may be wound into a coil and then heated in its entirety. Coiled substrates are particularly advantageous in the context of vapor deposition processes such as atomic layer deposition (ALD). Atomic layer deposition on coiled substrates is described, e.g., in U.S. patent application Ser. No. 10/782,545, which has been incorporated herein by reference. Heating such a coiled substrate is problematic for conventional methods such as IR lamps or convection heating due to the narrow spacing between adjacent turns of the coils. If the substrate is electrically conductive, however, the substrate may be heated resistively or inductively.

A key feature for resistive or inductive heating of coiled substrates is to be able to electrically insulate adjacent turns of the coiled substrate from each other in order to prevent electrical shorts that would otherwise result in non-uniform heating. U.S. patent application Ser. No. 10/782,545 describes spacers that are placed between the turns of the coiled substrate to prevent undesired contact between adjacent turns of the coiled substrate. The spacers can be put in place as the substrate is wound into a coil. These spacers can be in the form of slats that are placed at intervals across the width of the coiled substrate or "spacer tapes" that run lengthwise along the edges of the coiled substrate. In either case, the spacers preferably electrically insulating and do not melt or otherwise react adversely during heating of the substrate.

FIGS. **3A-3B** depict alternative schemes for resistively heating a coiled substrate. In FIG. **3A** in FIG. **3A** an elongated substrate has been rolled into a coil to form a coiled substrate **302**. Electrical leads **304**, **306** are connected at the ends of the coiled substrate **302**. The electrical leads **304**, **306** are connected to a power supply (AC or DC). When a power supply **308** applies a voltage between the leads **304**,

**306**, a current flows along the length of the coiled substrate as indicated by the arrows. The current may be regulated, e.g., through use of a sensor **314** coupled to the power supply **318** in a closed control loop circuit. In FIG. 3B, by contrast, electrodes **310**, **312** are electrically connected to the edges of the coiled substrate **302**. The electrodes **310**, **312** are connected to a power supply **318**. When a voltage is applied between the electrodes **310**, **312** a current flows across the width of the substrate **302** as indicated by the arrows. The current may be regulated, e.g., through use of a sensor **324** coupled to the power supply **318** in a closed control loop circuit.

FIG. 4 depicts an example of inductive heating of a coiled substrate **402**. An elongated substrate is wound into a coil, e.g., as described above, to form the coiled substrate **402**. The coiled substrate **402** is then placed within an induction coil **404**. A bus bar **406** makes electrical contact between first and second ends of the coiled substrate **402**. The induction coil **404** is electrically coupled to a radio frequency (or other high-frequency) power supply **408**. A matching circuit **412** and sensing circuit **414** may be electrically coupled between the induction coil **404** and the power supply **408**. When the power supply is energized, a current is induced in the coiled substrate **402**. The power supplied to the induction coil **404** may be regulated through the use of the sensing circuit **414** connected to the power supply **408** in a closed control loop.

Embodiments of the present invention may be used, e.g., for fabrication of absorber layers on aluminum foil substrates. Absorber layers are a key component of efficient photovoltaic devices such as solar cells. Fabrication of the absorber layer on the aluminum foil substrate is relatively straightforward. First, the nascent absorber layer is deposited on the substrate either directly on the aluminum or on an uppermost layer such as an electrode layer. Then the nascent absorber layer may be annealed by rapid resistive or inductive heating of the substrate.

The nascent absorber layer may include material containing elements of groups IB, IIIA, and (optionally) VIA. Preferably, the absorber layer copper (Cu) is the group IB element, Gallium (Ga) and/or Indium (In) and/or Aluminum may be the group IIIA elements and Selenium (Se) and/or Sulfur (S) as group VIA elements. The group VIA element may be incorporated into the nascent absorber layer when it is initially deposited or during subsequent processing to form a final absorber layer from the nascent absorber layer. The nascent absorber layer may be about 1000 nm thick when deposited. Subsequent rapid thermal processing and incorporation of group VIA elements may change the morphology of the resulting absorber layer such that it increases in thickness (e.g., to about twice as much as the nascent layer thickness under some circumstances).

By way of example, a nascent absorber layer containing elements of group IB and IIIA (and optionally VIA) may be formed on an aluminum substrate. The nascent absorber layer may be annealed by rapid resistive or inductive heating of the substrate (or a portion thereof) from an ambient temperature to a plateau temperature range of between about 200° C. and about 600° C. The substrate may be heated at a rate of between about 5° C./sec and about 150° C./sec. The temperature is maintained in the plateau range for between about 2 minutes and about 30 minutes, and subsequently reduced. Alternatively, the annealing temperature could be modulated to oscillate within a temperature range without being maintained at a particular plateau temperature. Rapid thermal processing of such absorber layers is described in commonly-assigned co-pending U.S. patent application Ser.

No. 10/943,685, entitled "FORMATION OF SOLAR CELLS ON FOIL SUBSTRATES", which has been incorporated herein by reference.

The nascent absorber layer may be deposited in the form of a film of a solution-based precursor material containing nanoparticles that include one or more elements of groups IB, IIIA and (optionally) VIA. Examples of such films of such solution-based printing techniques are described e.g., in commonly-assigned U.S. patent application Ser. No. 10/782,017, entitled "SOLUTION-BASED FABRICATION OF PHOTOVOLTAIC CELL" and also in PCT Publication WO 02/084708, entitled "METHOD OF FORMING SEMI-CONDUCTOR COMPOUND FILM FOR FABRICATION OF ELECTRONIC DEVICE AND FILM PRODUCED BY SAME" the disclosures of both of which are incorporated herein by reference.

Alternatively, the nascent absorber layer may be formed by a sequence of atomic layer deposition reactions or any other conventional process normally used for forming such layers. Atomic layer deposition of IB-III A-VIA absorber layers is described, e.g., in commonly-assigned, co-pending application Ser. No. 10/643,658, entitled "FORMATION OF CIGS ABSORBER LAYER MATERIALS USING ATOMIC LAYER DEPOSITION AND HIGH THROUGH-PUT SURFACE TREATMENT ON COILED FLEXIBLE SUBSTRATES", which has been incorporated herein by reference above.

Embodiments of the present invention can implement substrate heating at relatively low cost since the substrate material is already an integral part of the device. Embodiments of the present invention can also solve issues of thermal non-uniformity that is critical in CIGS cells by heating the entire area of the devices simultaneously with no dependence on substrate or roll geometry.

While the above is a complete description of the preferred embodiment of the present invention, it is possible to use various alternatives, modifications and equivalents. Therefore, the scope of the present invention should be determined not with reference to the above description but should, instead, be determined with reference to the appended claims, along with their full scope of equivalents. In the claims that follow, the indefinite article "A", or "An" refers to a quantity of one or more of the item following the article, except where expressly stated otherwise. The appended claims are not to be interpreted as including means-plus-function limitations, unless such a limitation is explicitly recited in a given claim using the phrase "means for."

What is claimed is:

1. A method for heating an elongated substrate in a roll processing system, comprising the steps of:
  - loading at least a portion of the elongated substrate into the roll processing system; and
  - causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature, wherein causing includes:
    - electrically contacting first and second leads to the portion of the elongated substrate at spaced apart locations;
    - applying an electrical voltage between the first and second leads whereby an electric current flows through the substrate between the first and second leads.
2. The method of claim 1 wherein the substrate moves past the first and second leads while the electrical voltage is applied between the first and second leads.
3. The method of claim 1 wherein the first lead electrically contacts the elongated substrate proximate a first edge and

the second lead electrically contacts the elongated substrate proximate a second edge whereby the electric current flows across a width of the elongated substrate.

4. The method of claim 1 wherein the first and second leads are configured such that the electric current flows along a length of the elongated substrate.

5. The method of claim 1 wherein causing a sufficient electrical current to flow in the portion of the elongated substrate includes:

disposing an inductor proximate the portion of the elongated substrate; and

applying high-frequency power to the inductor.

6. The method of claim 5 wherein the inductor is disposed above the portion of the elongated substrate.

7. The method of claim 5 wherein the inductor is disposed below the portion of the elongated substrate.

8. The method of claim 5 wherein the substrate moves past the inductor while the high-frequency power is applied between the inductor.

9. The method of claim 5 further comprising controlling power from the source of high-frequency power using one or more temperature or flux sensors coupled to a source of the high-frequency power in a closed control loop.

10. The method of claim 1 further comprising loading at least a portion of the elongated substrate into the roll processing system includes coiling the elongated substrate into a coiled substrate.

11. The method of claim 10, further comprising insulating adjacent turns of the coiled substrate against undesired electrical contact.

12. The method of claim 10 wherein causing a sufficient electrical current to flow in the portion of the elongated substrate includes:

electrically contacting a first lead at or near a first edge of the coiled substrate and electrically contacting a second lead at or near a second edge of the of the coiled substrate; and

applying an electrical voltage between the first and second leads, whereby the electrical current flows across a width of the coiled substrate.

13. A method for heating an elongated substrate in a roll processing system, comprising:

loading at least a portion of the elongated substrate into the roll processing system;

causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature; and

forming a nascent photovoltaic absorber layer containing one or more elements of group IB and one or more elements of group IIIA on an aluminum foil substrate.

14. A method for heating an elongated substrate in a roll processing system, comprising the steps of:

loading at least a portion of the elongated substrate into the roll processing system;

causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature, wherein causing comprises:

electrically contacting first and second leads to the portion of the elongated substrate at spaced apart locations;

applying an electrical voltage between the first and second leads whereby an electric current flows through the substrate between the first and second leads; and

focusing or defocusing the electric current with a magnetic field.

15. The method of claim 14, further comprising controlling the magnetic field using one or more temperature sensors, magnetic field sensors or current flux sensors coupled to a magnet controller in a closed control loop.

16. A method for heating an elongated substrate in a roll processing system, comprising the steps of:

loading at least a portion of the elongated substrate into the roll processing system;

causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature, wherein causing comprises:

electrically contacting first and second leads to the portion of the elongated substrate at spaced apart locations;

applying an electrical voltage between the first and second leads whereby an electric current flows through the substrate between the first and second leads; and

controlling the electrical voltage using one or more temperature sensors, magnetic field sensors or current flux sensors coupled to a power supply in a closed control loop.

17. A method for heating an elongated substrate in a roll processing system, comprising the steps of:

loading at least a portion of the elongated substrate into the roll processing system; causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature, wherein causing comprises:

disposing an inductor proximate the portion of the elongated substrate; and

applying high-frequency power to the inductor focusing or defocusing the electric current with a magnetic field.

18. The method of claim 17, further comprising controlling the magnetic field using one or more temperature sensors, magnetic field sensors or current flux sensors coupled to a magnet controller in a closed control loop.

19. A method for heating an elongated substrate in a roll processing system, comprising the steps of:

loading at least a portion of the elongated substrate into the roll processing system;

causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature;

wherein loading at least a portion of the elongated substrate into the roll processing system includes:

coiling the elongated substrate into a coiled substrate; and

insulating adjacent turns of the coiled substrate against undesired electrical contact;

wherein causing a sufficient electrical current to flow in the portion of the elongated substrate includes:

electrically contacting a first lead at or near a first end of the coiled substrate and electrically contacting a second lead at or near a second end of the of the coiled substrate; and

applying an electrical voltage between the first and second leads, whereby the electrical current flows along a length of the coiled substrate.

20. The method of claim 19 further comprising measuring a temperature of the coiled substrate with a sensor and controlling a source of the high-frequency power with a signal from the sensor using a closed-loop circuit.

21. A method for heating an elongated substrate in a roll processing system, comprising the steps of:



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loading at least a portion of the elongated substrate into the roll processing system;  
 causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature;  
 loading at least a portion of the elongated substrate into the roll processing system includes coiling the elongated substrate into a coiled substrate; and  
 insulating adjacent turns of the coiled substrate against undesired electrical contact;  
 wherein causing a sufficient electrical current to flow in the portion of the elongated substrate includes:  
 electrically contacting a first end of the coiled substrate to a second end of the coiled substrate;  
 placing the coiled substrate within an induction coil;  
 and  
 energizing the induction coil to inductively heat the coiled substrate.

**22.** A method for heating an elongated substrate in a roll processing system, comprising the steps of:  
 loading at least a portion of the elongated substrate into the roll processing system;

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causing a sufficient electrical current to flow in the portion of the elongated substrate to heat the portion to a desired temperature;  
 forming a nascent absorber layer containing one or more elements of group IB and one or more elements of group IIIA on an aluminum foil substrate;  
 rapidly heating the nascent absorber layer and/or substrate from an ambient temperature to a plateau temperature range of between about 200° C. and about 600° C.;  
 maintaining the absorber layer and/or substrate in the plateau temperature range for between about 2 minutes and about 30 minutes; and  
 reducing the temperature of the absorber layer and/or substrate.

**23.** The method of claim 22 wherein rapidly heating the nascent absorber layer and/or substrate includes increasing the temperature of the absorber layer and/or substrate at a rate of between about 5° C./sec and about 150° C./sec.

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