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(54) **HYDROUS ZIRCONIUM OXIDE, HYDROUS HAFNIUM OXIDE AND METHOD OF MAKING SAME**

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C01G 25/00 (2006.01)

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See application file for complete search history.

(57) **ABSTRACT**

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The present invention features a method of making hydrous zirconium oxide having desirable properties, including resistance to moisture content, predetermined particle size, and developed porosity and surface area. The inventive material is suitable for use as an ion exchanger, a catalyst and a catalyst support. The process comprises providing a liquid comprising a zirconium compound and an alkali metal-containing reagent. The alkali metal-containing reagent may comprise a compound selected from the group consisting of MOH-M₂SO₄, MOH-M₃PO₄, and combinations thereof, where M is at least one of Li, Na and K. The zirconium compound may be treated with the alkali metal-containing reagent effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.5 to 2.5 meq/g. The mixture is reacted to form the hydrous zirconium oxide. A molar ratio of SO₄/Zr and PO₄/Zr in the mixture may range from 0.2-0.7:1. The mixture may be heated at a temperature ranging from 80 to 150° C. to produce a reaction product. The reaction product may be treated with acid having a pH ranging from 4 to 8 at a temperature ranging from 20 to 60° C. to form the hydrous zirconium oxide. Also featured is a method of making hydrous hafnium oxide. The inventive hydrous zirconium oxide and hydrous hafnium oxide are characterized by at least one of the following: stability against moisture loss, a particular surface area, a particular pore size distribution, an affinity towards anions including at least one of PO₄, HPO₄, H₂PO₄, AsO₄, HAsO₄, H₂AsO₄ and AsO₃, oxoanions of Cr, Se, B, Mo, and W, and/or resistance against poisoning by SiO₃ and SO₄.

40 Claims, 2 Drawing Sheets

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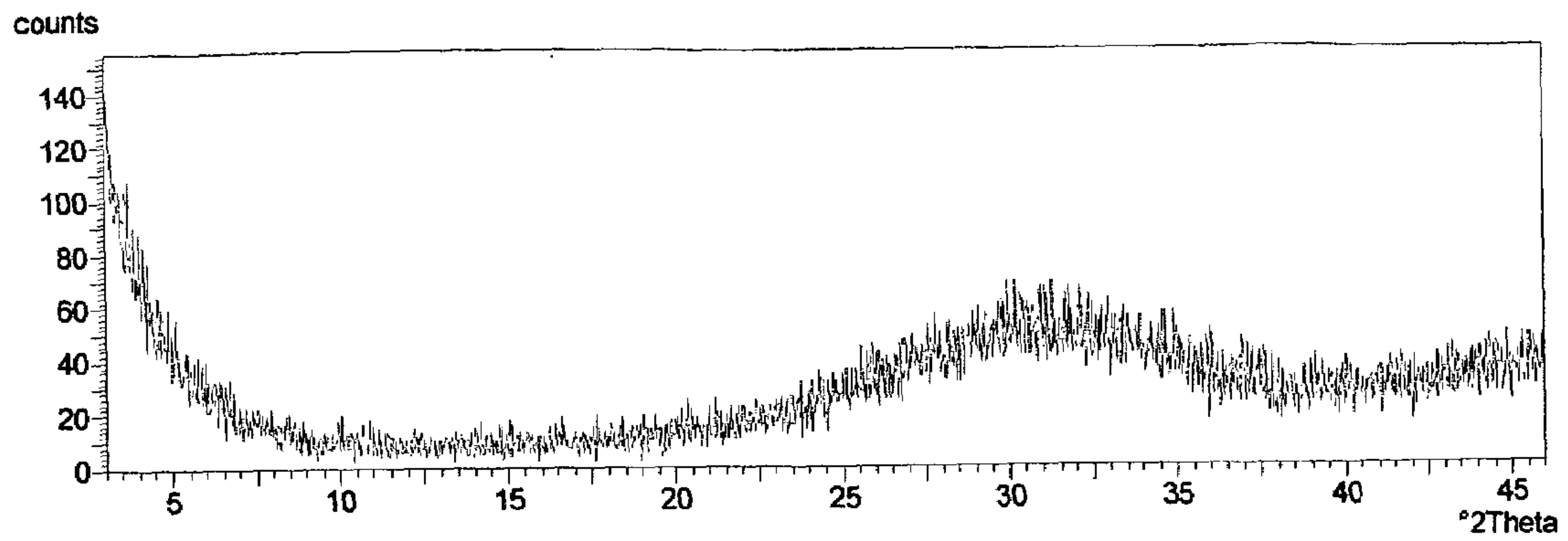


Fig.1

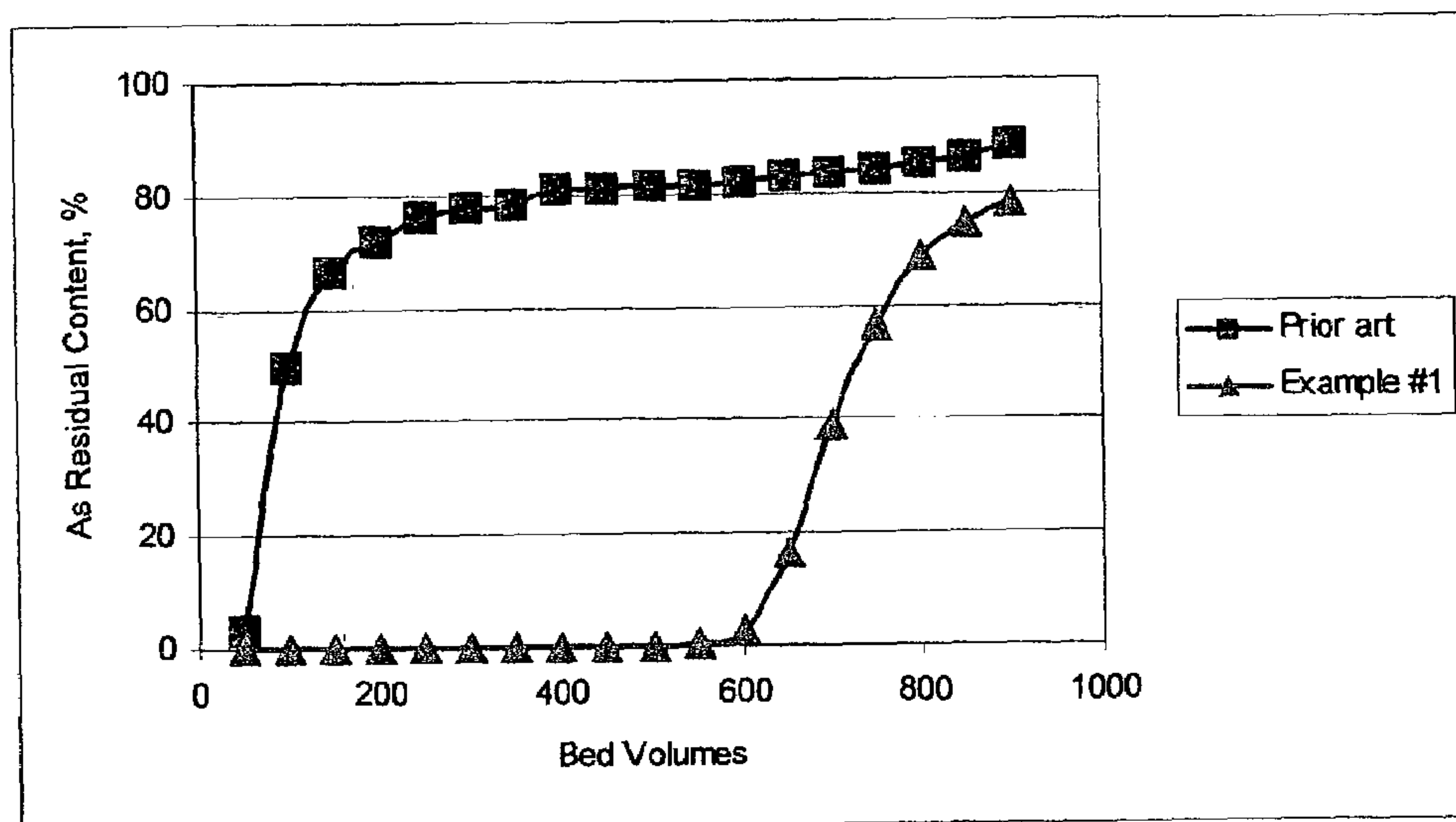


Fig. 2a

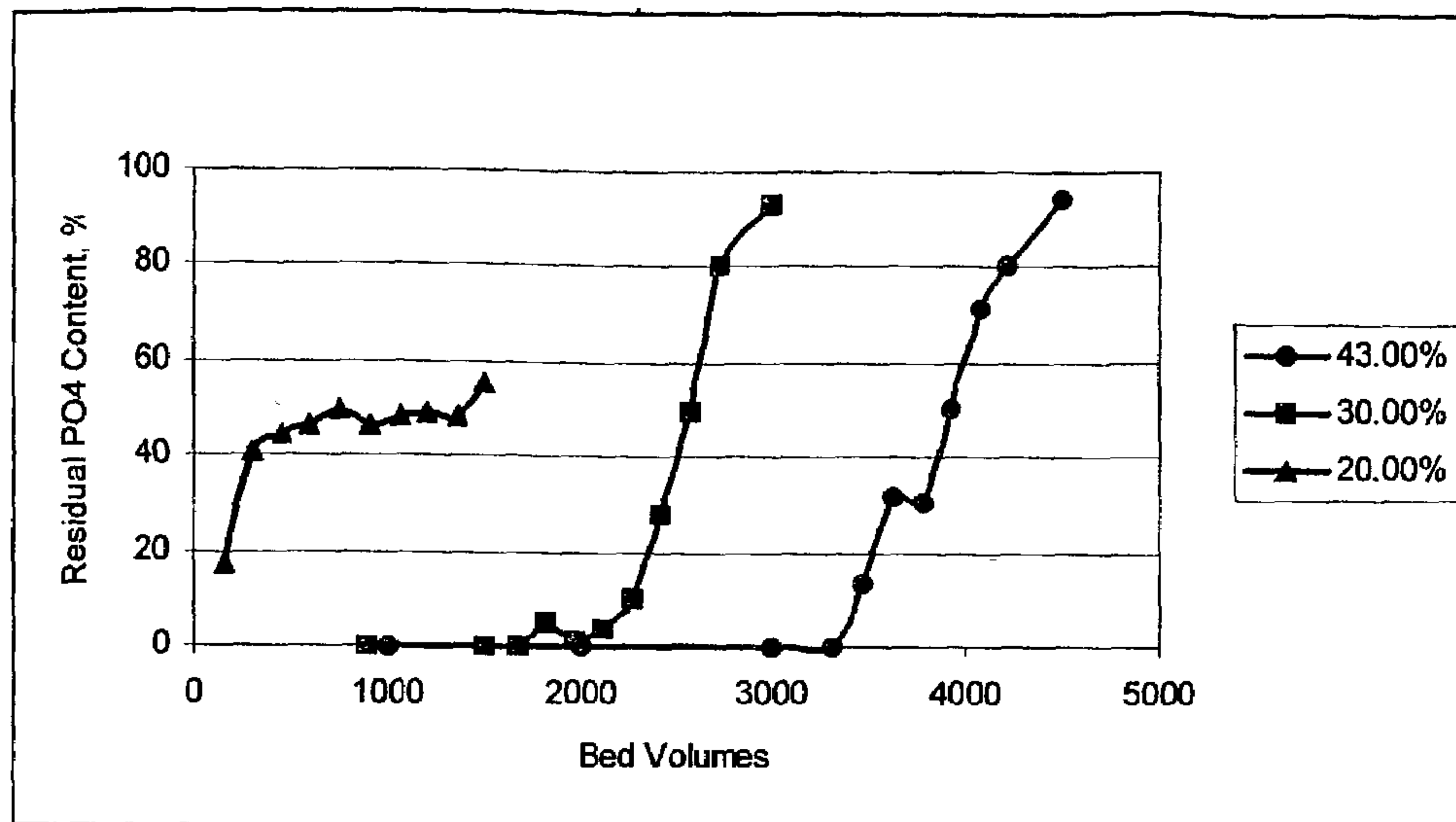


Fig. 2b

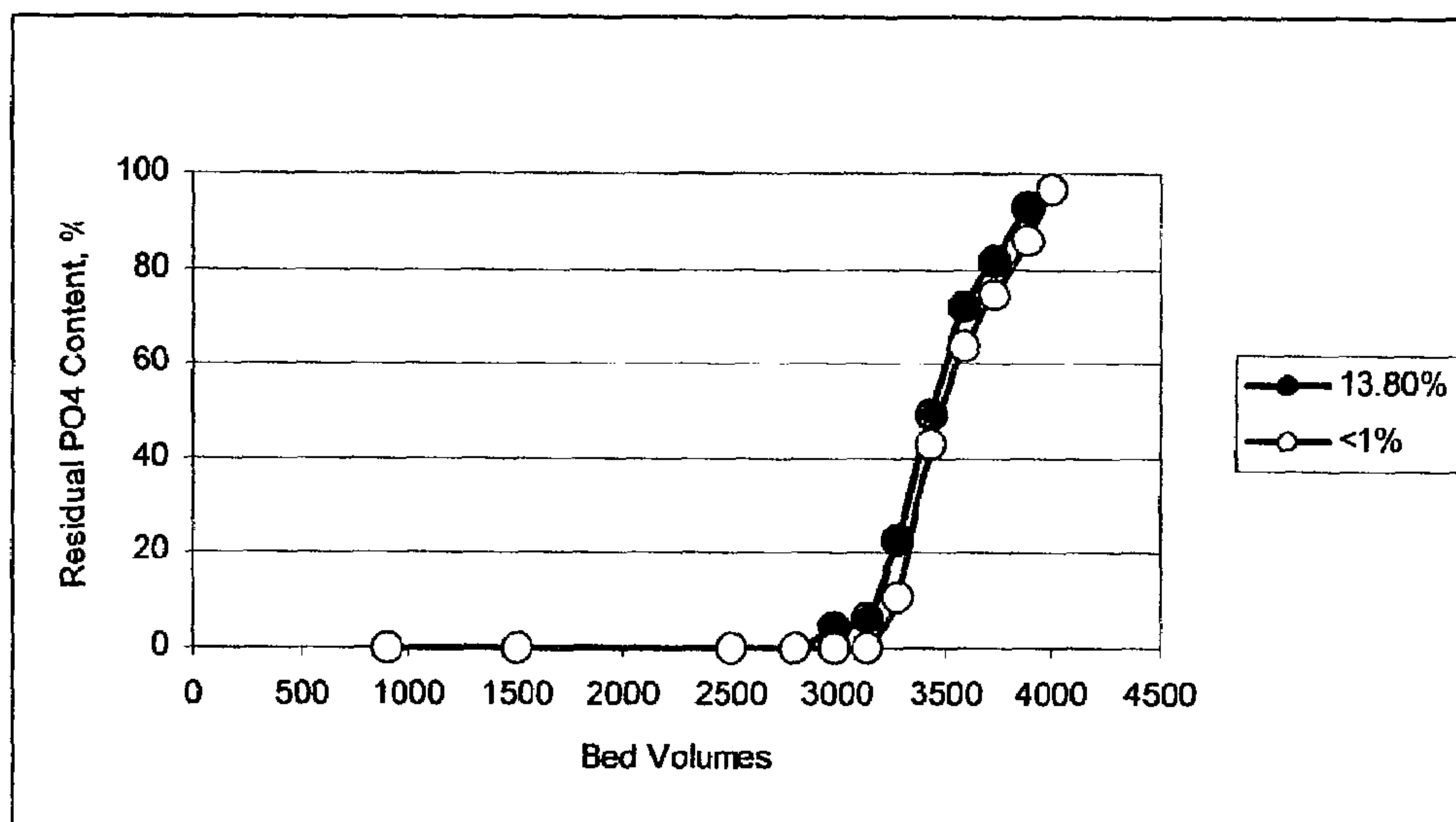


Fig. 3

HYDROUS ZIRCONIUM OXIDE, HYDROUS HAFNIUM OXIDE AND METHOD OF MAKING SAME

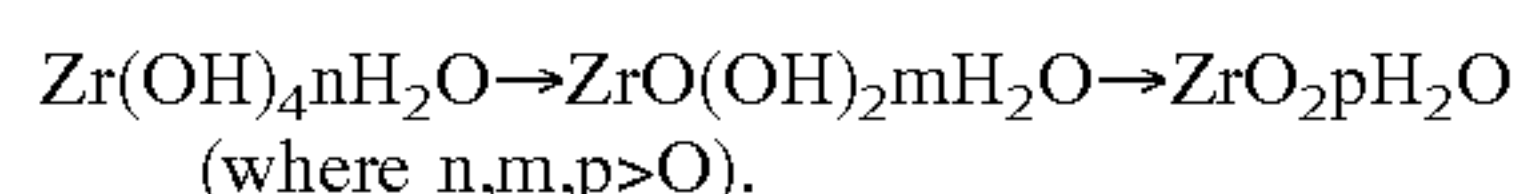
FIELD OF THE INVENTION

The present invention relates to hydrous zirconium oxide and hydrous hafnium oxide useful in applications including ion exchange and catalysis.

BACKGROUND OF THE INVENTION

Ion exchange is an important separation technique that is widely used for water and waste treatment, biochemistry, medicine and environmental protection. The efficiency of separation depends on many factors, including the selectivity of the adsorbent in use. Inorganic ion exchangers and adsorbents, due to properties such as chemical and thermal stability, resistance to oxidation and unique selectivity to certain ions, have definite advantages in comparison with traditionally used organic resins. Inorganic ion exchangers are able to operate in extreme conditions (high temperature or strong radiation fields, in the presence of organic solvents and/or oxidants and in a great excess of competitive ions), where organic resins fail to work efficiently. Among the known inorganic adsorbents, hydrous zirconium oxide (HZO) attracts special attention. HZO shows amphoteric properties and can behave as a cation exchanger in alkaline media or an anion exchanger in acidic media. However, the practical use of HZO is relatively limited because of several factors, among them being poor reproducibility of ion exchange properties and a strong dependency of adsorption performance on moisture content.

There are several methods for making amorphous hydrous zirconium oxides (A. Ruvarac, Group IV Hydrous Oxides—Synthetic Ion Exchangers, in the book, Inorganic Ion Exchange Materials, Ed. A. Clearfield, CRC Press, 1982, pp.141-160). Typically, in the first stage hydrolysis of a zirconium salt takes place, which is followed by condensation of primary particles, formed with hydrated polynuclear species. Hydrolysis of zirconium salts can be achieved by boiling an aqueous zirconium salt for a long period of time or by neutralization with alkali (e.g., LiOH, NaOH, KOH and NH₄OH). Freshly prepared hydrous zirconium oxides are amorphous. Upon ageing (e.g., contact with air at room or elevated temperature or treatment with neutral, acidic or alkaline reagents at room or elevated temperature), the primary particles of HZO undergo both intra- and inter-particle condensation reactions, with resultant structural ordering of the precipitates. The severity of the ordering strongly depends on the ageing conditions. However, in general an increased degree of ordering in aged hydrous zirconium oxides accounts for the decrease in sorption capacity, due to loss of free hydroxo groups according to the reactions:



Therefore, HZO is the most active when freshly precipitated and its ion exchange performance deteriorates with time (especially at elevated temperature). This is a serious drawback of amorphous materials.

Since the hydrous zirconium oxides obtained by the above mentioned methods are usually in the form of a fine powder, difficulties are encountered in handling them in separation processes. To overcome this disadvantage, several approaches have been proposed to make granulated HZO type materials. Among them are the following:

Impregnation of a porous substrate with a zirconium salt, followed by its hydrolysis via treatment with alkali (M. Ozawa et al., J. Mater. Sci. Lett., 9, 446 (1990)). The drawback of this approach is the ease in removing HZO from the pores of the carrier;

Granulation of amorphous hydrous zirconium oxides with the use of binders. The drawbacks of the use of binders include: lower ion exchange capacity, deterioration of kinetics of adsorption and possibility of contamination of the product with the binder components;

Sol-gel or gel routes. The sol-gel granulation process, based on the oil-drop principle, includes conversion of ZrO₂ sol into spherical granules of hydrous zirconium oxide gel in organic water immiscible media. The gel method, also based on the oil-drop principle, may include neutralization of zirconium salt with hexamethyltetraamine at 70-80° C. (R. Caletka, M. Tympl, J. Radioanal. Chem., 30: 155 (1976)). Spherically granulated amorphous hydrous zirconium oxides prepared via sol-gel and gel routes have high crush strength and good attrition resistance. However, granulated materials have the drawback of a strong dependency between ion exchange performance and moisture content. Amorphous hydrous polyvalent metal oxides regardless of the method of preparation, lose water continuously during storage in air and especially with an increase of heating temperature (See, for example, J. D. Donaldson, M. J. Fuller, J. Inorg. Nucl. Chem., 30, 1083 (1968)).

Highly ordered mesoporous zirconium oxides can be prepared via surfactant-controlled synthesis (U. Ciesla, et al, Chem. Mater., 11, 227 (1999)). The products show high thermal stability up to 400-500° C., which allows the removal of organic surfactants by calcination. Surfactant-controlled synthesis employs the presence of SO₄ or PO₄ anions as pore and structure-building elements (H. R. Chen et al, Mater. Letters, 51, 187 (2001)).

Different crystalline phases of zirconium oxide can be prepared by thermal treatment of amorphous gels.

Hydrolysis of aqueous zirconium salts under hydrothermal conditions typically results in crystalline modification of HZO. For example, B. Mottet et al. (J. Am. Ceram. Soc., 75, 2515 (1992)) reported the formation of monoclinic HZO by treatment of zirconium oxychloride in the presence of the additives NaOH, Na₂CO₃, H₂SO₄, NH₄F.

An advantage of crystalline materials is that they are less susceptible to moisture content (water loss) than amorphous sorbents and, as result, are more thermally stable. Ion exchange properties and selectivity of crystalline materials depends on the type of crystal structure. Typically, adsorption capacity of crystalline materials is lower than that of freshly prepared amorphous hydrous zirconium oxide. Another disadvantage of crystalline ion exchangers is poor kinetics of adsorption. Moreover, their powdered form prevents use in column applications.

SUMMARY OF THE INVENTION

In general, the inventive method of making hydrous zirconium oxide comprises the steps of providing a liquid comprising a zirconium compound and an alkali metal-containing reagent. The alkali metal-containing reagent comprises a compound selected from the group consisting of MOH-M₂SO₄, MOH-M₃PO₄, and combinations thereof, where M is at least one of Li, Na and K. The zirconium compound is treated with the alkali metal-containing reagent effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.5 to 2.5 meq/g. The mixture is reacted to form the hydrous zirconium oxide. The

invention also features making hydrous hafnium oxide by the same method except that a hafnium compound rather than a zirconium compound is used.

In the present invention a low extent of substitution of OH groups with alkali metals occurs at a pH of 10-12. These alkaline conditions, in combination with the presence of SO_4^{2-} , PO_4^{3-} anions, allow the hydrous zirconium oxide to retain an amorphous structure even after extended heat treatment. The ability of HZO to remain amorphous is advantageous in that it maintains the particle size of the final product.

Referring now to specific aspects of the method, the liquid mixture is formed by mixing a suspension comprising the zirconium compound and an aqueous solution comprising the alkali metal-containing reagent. A molar ratio of SO_4/Zr and PO_4/Zr in the liquid mixture ranges from (0.2-0.7):1. The liquid mixture comprising the zirconium compound and the alkali metal-containing reagent is heated at a temperature ranging from 80 to 150° C. for 0.5 to 24 hours. In one aspect of the method the liquid mixture is heated at a temperature ranging from 80 to 100° C. for 2 to 24 hours. In another aspect of the method the liquid mixture is heated at a temperature ranging from 100 to 150° C. at a pressure not exceeding 100 psi for 0.5-12 hours. The mixture achieves an uptake of the alkali metal in an amount ranging from 0.8 to 2.0 meq/g.

The zirconium compound comprises a compound selected from the group consisting of zirconium tetrachloride, zirconium oxychloride, zirconium acetate, zirconium sulfate, zirconium nitrate, ammonium zirconium carbonate, potassium zirconium carbonate, zirconium oxide, zirconium sulfate, zirconium basic sulfate, zirconium phosphate and combinations thereof. The zirconium compound is preferably water insoluble. In this regard, the zirconium compound may comprise a water insoluble salt selected from the group consisting of zirconium oxide, zirconium sulfate, zirconium basic sulfate, zirconium phosphate and combinations thereof. The zirconium compound may have a particle size distribution ranging from 10 to 100 microns.

A preferred embodiment of the invention is directed to a method of making hydrous zirconium oxide, comprising the steps of:

providing a suspension comprising a zirconium compound and an aqueous solution comprising an alkali metal-containing reagent, the alkali metal-containing reagent comprising a compound selected from the group consisting of $\text{MOH-M}_2\text{SO}_4$, $\text{MOH-M}_3\text{PO}_4$, and combinations thereof, where M is at least one of Li, Na and K;

treating the suspension with the aqueous solution effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.8 to 2.0 meq/g and wherein a molar ratio of SO_4/Zr and PO_4/Zr in the mixture ranges from 0.2-0.7:1;

heating the mixture at a temperature ranging from 80 to 150° C. to produce a reaction product; and

treating the reaction product with acid to form the hydrous zirconium oxide.

Turning now to specific aspects of the method which may be used in the preferred embodiment, the suspension comprises 10 to 30 wt % of the zirconium compound. In one aspect of this method, the mixture is heated for 0.5 to 24 hours. In another aspect of the method the mixture is heated at a temperature ranging from 100 to 150° C. at a pressure not exceeding 100 psi, which heating may be conducted for 0.5-12 hours. The treatment of the reaction product with acid is conducted at a pH ranging from 4 to 8 and at a temperature ranging from 20 to 60° C. for 0.5 to 2 hours. The acid

comprises an acid selected from the group consisting of HCl, HNO_3 , HBr, HClO, HClO_4 , CH_3COOH , CHOOH and combinations thereof. The invention may also feature filtering and washing the reaction product, redispersing in water the filtered and washed reaction product and filtering, washing and drying the treated reaction product. The mixture is treated at a pH ranging from 10 to 12.

In another embodiment of the invention a method of making hydrous zirconium oxide comprises providing an aqueous mixture comprising a water insoluble zirconium compound and an alkali metal-containing reagent. The aqueous mixture is heated at a temperature ranging from 80 to 150° C. to produce a reaction product. The reaction product is treated with acid having a pH ranging from 4 to 8 at a temperature ranging from 20 to 60° C. to form the hydrous zirconium oxide.

The inventive hydrous zirconium oxide and hydrous hafnium oxide, and particular features of the method for making them, may be characterized in terms of the material's stability against moisture loss. While stability against moisture loss is defined in terms of capacity and selectivity of chemical species removed, it should be understood that this does not require use of the inventive material for ion exchange, but rather quantifies the stability of the material against moisture loss, regardless of use of the material as an ion exchanger, catalyst, catalyst support or in another application.

The hydrous zirconium oxide and hydrous hafnium oxide may be amorphous and, while not wanting to be bound by theory, have a quasi-framework structure. Porous inorganic materials can be fully amorphous, para- or semi-crystalline, or crystalline. Amorphous materials do not possess long range order, whereas crystalline materials do. This can be seen in X-ray diffraction patterns in which non-crystalline materials do not exhibit sharp XRD peaks. Semi-crystalline materials may exhibit some chemical structure ordering as shown by broad XRD peaks. The hydrous zirconium oxide of the present invention is amorphous, meaning it has a chemical structure ranging from fully amorphous (no detectable XRD peaks) to semicrystalline (as determined by the existence of broad peaks), but not crystalline (lack of sharp XRD peaks). In particular, amorphous is defined herein by having an XRD pattern in which a height of a peak above baseline across 2θ values ranging from 20 to 38 degrees ranges up to 150 counts and, in particular, from 40 to 150 counts. The XRD pattern of FIG. 1 is used as a reference to define the amorphous character of the inventive material. The inventive material has a quasi-framework structure which, as defined herein, means having an irregular, non-ordered framework structure. The inventive material does not exhibit sharp XRD peaks upon intercalation with n-alkyl amines and thus, possesses a framework, rather than a layered, structure. However, being amorphous, the inventive material does not possess a fully framework structure.

The inventive material is a hydrous or hydrated oxide of zirconium and hafnium which includes hydroxides of zirconium and hafnium but excludes nonhydrated metal oxides (e.g., ZrO_2). The type of inventive hydrous zirconium oxide may also be referred to as hydrous or hydrated zirconium dioxide, hydrous or hydrated zirconium oxide, zirconium hydroxide and hydrous or hydrated zirconia. The inventive material includes a composite metal hydroxide and/or a hydrous or hydrated composite metal oxide.

Another embodiment of the present invention is directed to the hydrous zirconium oxide or hydrous hafnium oxide which may be made according to the aforementioned methods or some other as yet unforeseen method. The hydrous

zirconium oxide and hydrous hafnium oxide may be characterized by one or more of the following properties. These properties have been measured for the hydrous zirconium oxide and are believed to occur with the hydrous hafnium oxide as well. The material exhibits stability against moisture loss as characterized by a capacity and selectivity for chemical species that the material can remove from a liquid, which do not decrease more than 20% across a moisture content LOD of the material ranging from $0 \leq \text{LOD} \leq 40\%$ across a temperature range of up to 200° C. The material has a surface area of at least 150 m²/g, in particular 250 m²/g, and, more particularly at least 300 m²/g. The surface area of a preferred material may range from 300-400 m²/g and/or have a pore size distribution ranging from 20 to 40 Å. The material has a particle size distribution which is at least 10 microns, in particular, is at least 100 microns, and may range from 10 to 100 microns. Another feature of the material is that it exhibits an affinity towards anions comprising at least one of the following: PO₄, HPO₄, H₂PO₄, AsO₄, HAsO₄, H₂AsO₄, and AsO₃, the affinity being characterized by a Kd value of at least 1000 ml/g from 0.001 mol of an aqueous solution comprising phosphorus or arsenic at volume: mass=100:1 ml/g. The material also exhibits an affinity towards species comprising species selected from the group consisting of oxoanions of Cr, Se, B, Mo, W, the affinity being characterized by a Kd value of at least 200 ml/g from 0.001 mol of an aqueous solution comprising these elements at V:m=100:1 ml/g. The material is resistant against poisoning by SiO₃ and SO₄ anions as characterized wherein Kd values for P- and As-containing oxyanions do not change more than 10% from an initial Kd value in the absence of SiO₃ and SO₄ anions, compared to a Kd value when adsorption takes place in the presence of an equimolar amount of SiO₃ and SO₄ anions. The invention features ion exchange media, a catalyst, and a catalyst support comprised of the inventive material.

The present invention is also directed to a method of removing species from a feed liquid comprising the steps of providing an ion exchange material comprising hydrous zirconium oxide. Passing into contact with the ion exchange material is a feed liquid comprising at least one of the following species: PO₄, HPO₄, H₂PO₄, AsO₄, HAsO₄, H₂AsO₄ and AsO₃. The hydrous zirconium oxide removes the at least one species from the feed liquid. The ion exchange material has an affinity towards the at least one species which is characterized by a Kd value of at least 1000 ml/g from 0.001 mol of an aqueous solution comprising phosphorus or arsenic at V:m=100:1 ml/g. The ion exchange material used in this method may have stability against moisture loss characterized by a capacity and selectivity for the at least one chemical species, which do not decrease more than 20% across a moisture content LOD of the material ranging from $0 \leq \text{LOD} \leq 40\%$ across a temperature range of up to 200° C. In particular, the feed liquid may be comprised of a biological liquid comprising at least one of the phosphate-containing species. The phosphate-containing species is removed from the biological liquid such as in dialysis. In another aspect of the method, the feed liquid is aqueous and, in particular, drinking water.

Another method of removing species from a feed liquid comprises providing an ion exchange material comprising hydrous zirconium oxide. Passed into contact with the ion exchange material is the feed liquid comprising species selected from the group consisting of oxoanions of Cr, Se, B, Mo, W and combinations thereof. At least one of the species is removed from the feed liquid. The ion exchange material has an affinity towards the at least one of the species

which is characterized by a Kd value of at least 200 ml/g from 0.001 mol of an aqueous solution comprising these elements at V:m=100:1 ml/g.

The process steps may be varied to produce a material having particular particle size, surface area and porosity. This is especially advantageous in ion exchange where selected size, surface area and porosity provide advantages including avoiding the problem of restricted flow of the feed liquid exhibited by ion exchange powders. The material may have a granular form without the need for binders which tend to reduce ion exchange capability. The process steps may also affect the affinity of the material for certain species. The inventive material is also advantageously not dependent upon moisture content. While not wanting to be bound by theory, features of the process may inhibit the loss of non-bridging hydroxo groups. This is unexpected and overcomes the problem of traditional HZO materials of a significant decreased ion exchange ability as the water content of the material decreases. The inventive material also is unique in that it overcomes the problem of loss of amorphous character upon heating, which is exhibited by conventional HZO materials. The inventive material is selective for certain ions while being resistant to SiO₃, SO₄ poisoning. Being inorganic, the inventive material possesses superior chemical and thermal stability and oxidation resistance compared to organic resinous ion exchangers.

Other features, details and advantages of the invention will be apparent from the attached drawings and detailed description that follows.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 an X-ray diffraction (XRD) pattern of the inventive amorphous hydrous zirconium oxide prepared according to Example 1;

FIG. 2 shows phosphate breakthrough curves for amorphous hydrous zirconium oxide obtained according to Example 1 (FIG. 2a) and prior art hydrous zirconium oxide (FIG. 2b) as a function of residual moisture content in the sorbent; and

FIG. 3 shows Arsenic(V) breakthrough curves from 0.1 M Na₂SO₄+0.001 M Na₂HAsO₄ solution for inventive amorphous hydrous zirconium oxide obtained according to Example 1 and dried to 0% residual moisture content and prior art hydrous zirconium oxide dried to residual water content of 30%.

DETAILED DESCRIPTION

The present invention provides a method of making hydrous zirconium oxide having desirable properties, including resistance to moisture content, predetermined particle size, and developed porosity and surface area. The inventive material is suitable for use as an ion exchanger, a catalyst and a catalyst support. The process comprises providing a liquid comprising a zirconium compound and an alkali metal-containing reagent. The alkali metal-containing reagent comprises a compound selected from the group consisting of MOH-M₂SO₄, MOH-M₃PO₄, and combinations thereof, where M is at least one of Li, Na and K. The zirconium compound is treated with the alkali metal-containing reagent effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.5 to 2.5 meq/g, in particular 0.8 to 2.0 meq/g. A molar ratio of SO₄/Zr and PO₄/Zr in the mixture ranges from 0.2-0.7:1.

The mixture is reacted to form the hydrous zirconium oxide.

In particular, the zirconium compound comprises at least one of the following: zirconium tetrachloride, zirconium oxychloride, zirconium acetate, zirconium sulfate, zirconium nitrate, ammonium zirconium carbonate, and potassium zirconium carbonate. The zirconium compound may comprise at least one of the following water insoluble zirconium salts: zirconium oxide, zirconium sulfate, zirconium basic sulfate and zirconium phosphate. More particularly, the water insoluble zirconium compound has a narrow particle size distribution in the range of from 10 to 100 microns. The use of a zirconium compound with an average granule size of 10-100 microns permits producing the inventive amorphous hydrous zirconium oxide ion exchanger with a similar particle size distribution. This particle size distribution is ideally suited (low back pressure, quick kinetics of exchange) for some separation applications, like removal of toxic anions (e.g., As, Se, Cr) from drinking water (e.g., under column conditions) or phosphate anions from biological liquors (e.g., dialysis).

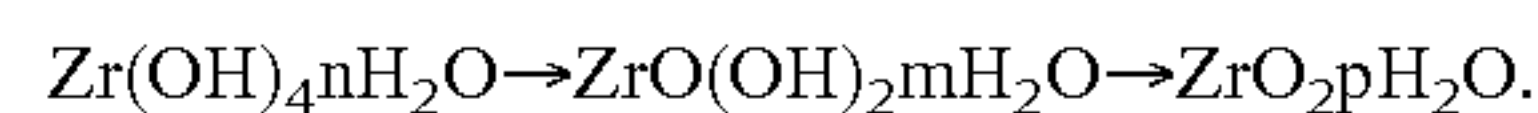
An aqueous suspension of the zirconium compound (e.g., 10 to 30 wt %) is reacted with an aqueous solution of the alkali metal-containing reagent. The treatment of the suspension and the aqueous solution is conducted at a temperature ranging from 80 to 100° C. for 2 to 24 hours or at a temperature ranging from 100 to 150° C. under hydrothermal conditions and autogeneous pressure not exceeding 100 psi for 0.5 to 12 hours.

Conversion of the reaction product into the OH-form by treatment with acid comprising at least one of HCl, HNO₃, HBr, HClO, HClO₄, CH₃COOH and CHOOH having a pH ranging from 4 to 8 at a temperature ranging from 20 to 60, followed by filtration, washing and drying of the material, makes the sorbent ready for direct application and long-term storage.

The inventive hydrous zirconium oxide based ion exchange material exhibits a high affinity towards at least one of the following anions, PO₄, HPO₄, H₂PO₄, AsO₄, HAsO₄, H₂AsO₄ and AsO₃ and a high resistance against poisoning thereof by at least one of SiO₃ and SO₄ anions. The high affinity is characterized by Kd values of at least 1,000 mL/g from 0.001 Mol phosphorus or arsenic-containing aqueous solution at V:m=100:1, mL/g. See Example 9. Resistance against poisoning is characterized wherein the Kd values for P- and As-containing oxyanions do not change more than up to 10% and, in particular 5-10%, from an initial Kd value in the absence of SiO₃ and SO₄ anions, compared to a Kd value when adsorption takes place in the presence of an equimolar amount of SiO₃ and SO₄ anions. The hydrous zirconium oxide of the invention also has an affinity towards species comprising species selected from the group consisting of oxoanions of Cr, Se, B, Mo, W, the affinity being characterized by a Kd value of at least 200 ml/g from 0.001 mol of an aqueous solution comprising these elements at V:m=100:1 ml/g. The inventive material exhibits stability against moisture loss, which means that capacity and selectivity do not change significantly (no more than 20% and, in particular, 5-20%) when the sorbent loses water from LOD=40% to LOD=0% even when the material is heated in a temperature range up to 200° C. In particular, it is also characterized by a pore size distribution ranging from 20 to 40 Å and a surface area of at least 300 M²/g and, in particular, a surface area ranging from 300 to 400 m²/g.

The process is practical from an industrial standpoint. To make HZO resistant to moisture loss, its structure is "stabilized." Freshly prepared amorphous hydrous zirconium oxides (Zr(OH)₄ nH₂O) contain large quantities of non-

bridging hydroxo groups (in an amount >12-15 mMol/g). These groups are highly reactive and participate readily in condensation reactions leading to a loss of ion exchange properties and porous structure collapse according to the reactions:



In the present invention, while not wanting to be bound by theory, non-bridging hydroxo groups are removed or substituted in the early stages of material polymerization to achieve HZO stabilization. Thermal treatment of HZO in air allows the removal of non-bridging hydroxo groups. However, this process is accompanied by a simultaneous collapse of the porous structure. Under some conditions (e.g., preliminary partial conversion of hydrous zirconium oxide into a cation exchange form in the presence of sulfate and/or phosphate anions, followed by treatment at elevated temperature (normal or high pressure), the hydrous zirconium oxide structure can be stabilized without crystallization of the material. While not wanting to be bound by theory, a partial conversion of HZO into the cation exchange form (0.5-2.5 meq/g alkali metal uptake, more specifically, 0.8-2.0 meq/g alkali metal uptake) directly protects some of the non-bridging hydroxo groups from participating in condensation reactions, while protecting other groups indirectly by creating steric hindrances to reaction. As a result, only a relatively small part of the existing non-bridging hydroxo groups are able to participate in the condensation-polymerization reactions. Moreover, because condensation reactions take place in the presence of "bulky" alkali cations and SO₄²⁻, PO₄³⁻ anions, a mesoporous and sufficiently robust framework sorbent may be formed while avoiding porous structure collapse. These mesoporous materials have a narrow pore size distribution ranging from 20 to 40 Å and a surface area ranging from 250 to 400 m²/g.

The inventive method and the role of the reaction components used therein differ from those described in the prior art. The conventional role of SO₄²⁻, PO₄³⁻ anions in producing mesoporous zirconium oxides is as structure building elements (H. R. Chen et al, Mater. Letters, 51, 187 (2001)). These anions remain in the HZO after synthesis and their presence is believed to be necessary for the existence of this type of structure. In the present invention the primary role of the sulfate and phosphate ions is not to serve as structure building elements, but rather is to serve as template agents and agents preventing crystallization of HZO. In the present invention SO₄²⁻ and PO₄³⁻ anions do not significantly incorporate into the structure of the zirconium oxide, which is confirmed by the fact that only trace amounts (less than 0.5 wt. %) of them are found in the final product. The use of these ions in the inventive process may be responsible for improving the inventive adsorbent's resistance to poisoning by SiO₃ and SO₄ anions. It is known that crystalline compounds are more thermally stable than their amorphous analogues. In the present invention a low extent of substitution of OH groups with alkali metals occurs at a pH of 10-12. These alkaline conditions, in combination with the presence of SO₄²⁻, PO₄³⁻ anions, allow the hydrous zirconium oxide to retain an amorphous structure even after 12 hours of treatment at 150° C. under high pressure, while improving thermal resistance of the material. The ability of HZO to remain amorphous is advantageous in that it maintains the particle size of the final product.

Experimental Equipment

This describes the equipment used in the following examples to characterize the inventive hydrous zirconium

oxide material of the present invention. Powder X-ray diffraction measurements were carried out in a Phillips diffractometer, model PW 1729/1720 (scan speed 1 deg/min, step width 0.04 degree, Cu K α radiation, $\lambda=1.5418$ E). Particle size distribution (PSD) was measured using Leeds-Northrup, Microtrack X100. BET surface area measurements and pore size determination were done on Coulter SA3100, nitrogen adsorption. Samples were degassed at 280° C. in a vacuum. Water loss was determined at 209° C. on a Denver Instrument hot plate. Residual sulfur content in HZO was determined by Sulfur & Carbon analyzer LECO SC-444. Phosphorus, arsenic and alkali metals in solution were determined by the ICP method, VARIAN, VISTA-MPX instrument.

The present invention will now be described more specifically by reference to the following examples which are not intended to limit the invention described in the appended claims.

EXAMPLE 1

The inventive amorphous hydrous zirconium oxide was prepared in all the examples. In this example the material was prepared according to the following procedure. In the first stage, a slurry was made containing 250 g of basic zirconium sulfate (i.e., 40% ZrO₂) (MEI, HCP PP142A), with a predetermined particle size of 50 to 60 microns, in 1.0 L of 0.1 M H₂SO₄. Under constant mixing the required amount of 30 wt. % NaOH solution was added gradually to raise the pH of the reaction mixture to 11.5. The slurry was transferred into an autoclave, sealed and heated at 120° C. for 6 hours under constant stirring. Then, the product of conversion was filtered, washed with 0.5 kg of water and re-slurried in 1 L of water. To the HZO suspension 30 wt. % HNO₃ solution was added gradually, effective to adjust the pH to 6.0. Then, the HZO was filtered, washed with 1 kg of water and dried at 100° C. for 12 hours in air (at ambient pressure).

The dried product had a particle size of 45 to 55 microns. According to elemental analysis the sulfur content was <0.05% and the sodium content was <0.1%. The surface area was 360 m²/g. The average pore size was 30 Å. Water loss at 209° C. (LOD) was <1%.

EXAMPLE 2

All of the operations and amounts of reagents used in Example 1 were used in this example, with the only difference being that thermal treatment of basic zirconium sulfate was carried out at 100° C. and ambient pressure for 24 hours. The dried product had a particle size ranging from 45 to 55 microns. According to elemental analysis the sulfur content was <0.05% and the sodium content was <0.1%. The surface area was 330 m²/g. The average pore size was 30 Å. Water loss at 209° C. (LOD) was <1%.

EXAMPLE 3

All of the operations and amounts of reagents used in Example 1 were used in this example, with the only difference being that 30 wt. % KOH solution was used instead of sodium hydroxide. The dried product had a particle size ranging from 45 to 55 microns. According to elemental analysis the sulfur content was <0.05% and the potassium content was <0.1%. The surface area was 300 m²/g. The average pore size was 40 Å. Water loss at 209° C. (LOD) was <1%.

EXAMPLE 4

All of the operations and amounts of reagents used in Example 1 were used in this example, with the only difference being that 10 wt. % LiOH solution was used instead of sodium hydroxide. The dried product had a particle size ranging from 45 to 55 microns. According to elemental analysis the sulfur content was <0.05% and the lithium content was <0.1%. The surface area was 400 m²/g. The average pore size was 30 Å. Water loss at 209° C. (LOD) was <1%.

EXAMPLE 5

All of the operations and amounts of reagents used in Example 1 were used in this example, with the only difference being that hydrous zirconium oxide with a particle size ranging from 40 to 50 microns was used as a source of the zirconium compound. The dried product had a particle size ranging from 35 to 45 microns. According to elemental analysis the sulfur content was <0.05% and the sodium content was <0.1%. The surface area was 360 m²/g. The average pore size was 30 Å. The water loss at 209° C. (LOD) was <1%.

EXAMPLE 6

All of the operations and amounts of reagents used in Example 1 were used in this example with the only difference being that hydrous zirconium oxide with a particle size ranging from 40 to 50 microns was used as a source of the zirconium compound and it was slurried in 1.0 L of 0.2 M H₃PO₄. The dried product had a particle size ranging from 35 to 45 microns. According to elemental analysis the phosphorus content was <0.05% and the sodium content was <0.1%. The surface area was 250 m²/g. The average pore size was 40 Å. The water loss at 209° C. (LOD) was <1%.

EXAMPLE 7

The affinity of the amorphous hydrous zirconium oxide towards phosphate was tested under column conditions. In these experiments 5.00 g of hydrous zirconium oxide made according to Example 1 was put in a vertical column with an inner diameter of 8 mm. A simulant solution (0.02 M Na₂SO₄+0.001 M Na₂HPO₄) was passed through the adsorbent bed at a flow rate of 120 mL/hour (24 bed volumes/hour) with the use of a peristaltic pump. The concentration of phosphorus in solution (before and after passing the adsorbent layer) was determined using an ICP technique. The breakthrough curves were plotted as residual concentration of ion in solution (in %) versus amounts of bed volumes (BV) of solution passed through the adsorbent (FIG. 2a). For comparison similar data are presented for prior art amorphous hydrous zirconium oxide (MEI, HCP PP142F) (FIG. 2b).

The data show that amorphous hydrous zirconium oxide from Example 1 has a high capacity for phosphate uptake in the presence of excess sulfate ions: ~3 mMol/g (before breakthrough). Moreover, drying of the inventive sorbent to LOD <1% does not affect PO₄ uptake, which indicates that HZO is resistant to moisture content. In comparison, the prior art HZO shows high affinity and capacity on PO₄ ion only when the hydrous zirconium oxide is highly hydrated (LOD >40%). Even mild drying (residual water content 20-30%) of the prior art HZO results in a drastic loss of

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capacity. A total loss of capacity was found for prior art HZO dried to LOD <1% (not shown on a graph).

EXAMPLE 8

The affinity of the inventive amorphous hydrous zirconium oxide towards arsenic was tested under column conditions. For these experiments 2.00 g of hydrous zirconium oxide prepared according to Example 1 was put in a vertical column with an inner diameter of 7 mm. A simulant solution, 0.1 M Na₂SO₄+0.001 M Na₂HAsO₄, was passed through the adsorbent bed at a flow rate of 120 ml/hour (or 60 bed volumes/hour) with the use of a peristaltic pump. Concentration of arsenic in solution (before and after passing the adsorbent layer) was determined using an ICP technique. The breakthrough curves were plotted as residual concentration of ion in solution (in %) versus amounts of bed volumes (BV) of solution passed through the inventive adsorbent (FIG. 3). For comparison, similar data are presented for prior art amorphous hydrous zirconium oxide (MEI, HCP PP142F).

The data show that the amorphous hydrous zirconium oxide of Example 1 (dried to a residual moisture content of 0%) has a high capacity for arsenate ions in the presence of excess sulfate ions: ~0.6 mMol/g (before breakthrough). In comparison, the prior art hydrous zirconium oxide shows extremely low affinity and capacity (<0.02 mMol/g before breakthrough) for arsenic (V) even after mild drying to a residual water content of 30%. A total loss of a capacity was found for the prior art HZO dried to LOD <1 % (not shown on a graph).

EXAMPLE 9

The affinity of HZO from Example 1 and prior art HZO (MEI, HCP PP142F) towards AsO₄ uptake in the presence of competitive ions as a function of residual water content is shown in Table 1 where V:m=100:1 (mL/g) and contact time was 24 hours. The affinity of the HZO samples towards elements of interest was expressed through the distribution coefficient (K_d, mL/g) values. The K_d values were found according to the formula $K_d = (C_o - C_i / C_i) \cdot V / m$, where C_o is initial concentration in solution, C_i is concentration after equilibration with adsorbent, V is volume in mL, m is mass of exchanger in grams.

TABLE 1

Sorbent	LOD, wt. %	0.001 M AsO ₄	0.001 M AsO ₄ + 0.001 M SO ₄	0.001 M AsO ₄ + 0.001 M SiO ₃
Ex #1	40	120,000	120,000	110,000
Ex #1	20	125,000	125,000	120,000
Ex #1	<1	140,000	140,000	135,000
Prior Art	40	100,000	70,000	15,000
Prior Art	20	600	500	400
Prior Art	<1	40	30	10

Although the present invention has been described with reference to the examples and with some degree of particularity in the detailed description, it should be understood that various modifications and variations can be made by those skilled in the art without departing from the spirit and scope of the invention as set forth hereafter in the appended claims.

What is claimed is:

1. A method of making hydrous zirconium oxide comprising the steps of providing a liquid comprising a zirconium compound and an alkali metal-containing reagent, said alkali metal-containing reagent comprising a compound selected from the group consisting of MOH-M₂SO₄, MOH-

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M₃-PO₄, and combinations thereof, where M is at least one selected from the group consisting of Li, Na and K, treating said zirconium compound with said alkali metal-containing reagent effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.5 to 2.5 milliequivalents/gram, heating said mixture to produce a reaction product and treating said reaction product with acid to form said hydrous zirconium oxide.

2. The method of claim 1 wherein said acid comprises an acid selected from the group consisting of HCl, HNO₃, HBr, HClO, HClO₄, CH₃COOH, CHOOH and combinations thereof.

3. The method of claim 1 wherein said uptake of alkali metal ranges from 0.8 to 2.0 milliequivalents/gram.

4. The method of claim 1 wherein a molar ratio of SO₄/Zr and PO₄/Zr in said mixture ranges from 0.2-0.7:1.

5. The method of claim 1 wherein said zirconium compound comprises a compound selected from the group consisting of zirconium tetrachloride, zirconium oxychloride, zirconium acetate, zirconium sulfate, zirconium nitrate, ammonium zirconium carbonate, potassium zirconium carbonate, zirconium oxide, zirconium basic sulfate, zirconium phosphate and combinations thereof.

6. The method of claim 1 wherein said zirconium compound has a particle size distribution ranging from 10 to 100 microns.

7. The method of claim 1 wherein said zirconium compound comprises a salt selected from the group consisting of zirconium oxide, zirconium sulfate, zirconium basic sulfate, zirconium phosphate and combinations thereof.

8. The method of claim 1 wherein said zirconium compound is water insoluble.

9. The method of claim 1 wherein said heating is conducted at a temperature of 80° C. to 150° C.

10. A method of making hydrous hafnium oxide, comprising the steps of providing a liquid comprising a hafnium compound and an alkali metal-containing reagent, said alkali metal-containing reagent comprising a compound selected from the group consisting of MOH-M₂SO₄, MOH-M₃PO₄, and combinations thereof, where M is at least one selected from the group consisting of Li, Na and K, treating said hafnium compound with said alkali metal-containing reagent effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.5 to 2.5 milliequivalents/gram, heating said mixture to produce a reaction product and treating said reaction product with acid to form said hydrous hafnium oxide.

11. The method of claim 10 wherein said heating is conducted at a temperature of 80° C. to 150° C.

12. A method of making hydrous zirconium oxide, comprising the steps of:

providing a suspension comprising a zirconium compound and an aqueous solution comprising an alkali metal-containing reagent, said alkali metal-containing reagent comprising a compound selected from the group consisting of MOH-M₂SO₄, MOH-M₃PO₄, and combinations thereof, where M is at least one selected from the group consisting of Li, Na and K;

treating said suspension with said aqueous solution effective to form a mixture which achieves an uptake of alkali metal in an amount ranging from 0.8 to 2.0 milliequivalents/gram and wherein a molar ratio of SO₄/Zr and PO₄/Zr in said mixture ranges from 0.2-0.7:1;

heating said mixture at a temperature ranging from 80 to 150° C. to produce a reaction product; and

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treating said reaction product with acid to form said hydrous zirconium oxide.

13. The method of claim 12 wherein said suspension comprises 10 to 30 wt % of said zirconium compound.

14. The method of claim 12 wherein said heating of said mixture is conducted for 0.5 to 24 hours.

15. The method of claim 12 wherein said heating of said mixture is conducted at a temperature ranging from 100 to 150° C. at a pressure not exceeding 100 psi.

16. The method of claim 12 wherein said heating of said mixture is conducted at a temperature ranging from 100 to 150° C. at a pressure not exceeding 100 psi, and wherein said heating of said mixture is conducted for 0.5-12 hours.

17. The method of claim 12 wherein said acid has a pH ranging from 4 to 8.

18. The method of claim 12 wherein said reaction product is treated with said acid at a temperature ranging from 20 to 60° C.

19. The method of claim 12 wherein said reaction product is treated with said acid at a temperature ranging from 20 to 60° C., and wherein said treatment of said reaction product with acid is conducted for 0.5 to 2 hours.

20. The method of claim 12 comprising filtering and washing said reaction product, redispersing in water said filtered and washed reaction product and filtering, washing and drying said treated reaction product.

21. The method of claim 12 comprising treating said mixture at a pH ranging from 10 to 12.

22. A method of making hydrous zirconium oxide, comprising the steps of:

providing an aqueous mixture comprising a water insoluble zirconium compound and an alkali metal-containing reagent;

heating said aqueous mixture at a temperature ranging from 80 to 150° C. to produce a reaction product; and treating said reaction product with acid having a pH ranging from 4 to 8 at a temperature ranging from 20 to 60° C. to form said hydrous zirconium oxide.

23. Hydrous zirconium oxide that is granular, amorphous, has no binder that reduces ion exchange capability, has stability against moisture loss and is made by the method of claim 1, wherein said stability against moisture loss is characterized by an affinity for arsenic as measured by a distribution coefficient Kd in a 0.001 M AsO₄ solution that does not decrease across a moisture content LOD of said hydrous zirconium oxide ranging from 0<LOD<40%.

24. Hydrous zirconium oxide that is granular, amorphous, has no binder that reduces ion exchange capability and has stability against moisture loss, wherein said stability against moisture loss is characterized by an affinity for arsenic as measured by a distribution coefficient Kd in a 0.001 M AsO₄ solution that does not decrease across a moisture content LOD of said hydrous zirconium oxide ranging from 0<LOD<40%.

25. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide exhibits an affinity towards anions selected from the group consisting of PO₄, HPO₄, H₂PO₄, AsO₄, HAsO₄, H₂AsO₄, AsO₃, and combinations thereof.

26. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has an affinity towards species selected from the group consisting of oxoanions of Cr, oxoanions of Se, oxoanions of B, oxoanions of Mo, and oxoanions of W.

27. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a pore size distribution ranging from 20 to 40 Å.

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28. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a surface area of at least 150 m²/g.

29. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a surface area of at least 250 m²/g.

30. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a surface area of at least 300 m²/g.

31. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a surface area ranging from 300 to 400 m²/g.

32. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a particle size distribution of at least 10 microns.

33. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a particle size distribution of at least 100 microns.

34. The hydrous zirconium oxide of claim 24 wherein said hydrous zirconium oxide has a particle size distribution ranging from 10 to 100 microns.

35. Ion exchange media, catalyst or catalyst support comprising the hydrous zirconium oxide of claim 24.

36. A method of removing species from a feed liquid comprising the steps of:

providing an ion exchange material comprising hydrous zirconium oxide that is granular, amorphous, has no binder that reduces ion exchange capability and has stability against moisture loss characterized by an affinity for arsenic as measured by a distribution coefficient Kd in a 0.001 M AsO₄ solution that does not decrease across a moisture content LOD of said hydrous zirconium oxide ranging from 0<LOD<40%;
passing into contact with said ion exchange material said feed liquid comprising species selected from the group consisting of PO₄, HPO₄, H₂PO₄, AsO₄, HAsO₄, H₂AsO₄, AsO₃, and combinations thereof; and removing from said feed liquid at least one of said species.

37. The method of claim 36 wherein said feed liquid is comprised of a biological liquid comprising at least one of said phosphate-containing species, comprising removing said phosphate-containing species from said biological liquid.

38. The method of claim 36 wherein said feed liquid is aqueous.

39. The method of claim 36 wherein said feed liquid is drinking water.

40. A method of removing species from a feed liquid comprising the steps of:

providing an ion exchange material comprising hydrous zirconium oxide that is granular, amorphous, has no binder that reduces ion exchange capability and has stability against moisture loss characterized by an affinity for arsenic as measured by a distribution coefficient Kd in a 0.001 M AsO₄ solution that does not decrease across a moisture content LOD of said hydrous zirconium oxide ranging from 0<LOD<40%;
passing into contact with said ion exchange material said feed liquid comprising species selected from the group consisting of oxoanions of Cr, oxoanions of Se, oxoanions of B, oxoanions of Mo, and oxoanions of W; and removing from said feed liquid at least one of said species.