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Shinkawa et al.

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(45) **Date of Patent:** **Dec. 19, 2006**

(54) **DROPLET EJECTION APPARATUS AND
EJECTION FAILURE RECOVERY METHOD**

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(21) Appl. No.: **10/789,819**

(Continued)

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Communication from European Patent Office re: counterpart application.

(Continued)

(30) **Foreign Application Priority Data**

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Mar. 18, 2003 (JP) 2003-074628

Primary Examiner—Shih-Wen Hsieh

(74) Attorney, Agent, or Firm—Harness, Dickey & Pierce, P.L.C.

(51) **Int. Cl.**

B41J 2/165 (2006.01)
B41J 29/393 (2006.01)
B41J 2/19 (2006.01)

(57) **ABSTRACT**

(52) **U.S. Cl.** **347/23; 347/19; 347/92**

(58) **Field of Classification Search** 347/14, 347/19, 10, 11, 22–35, 68, 92

See application file for complete search history.

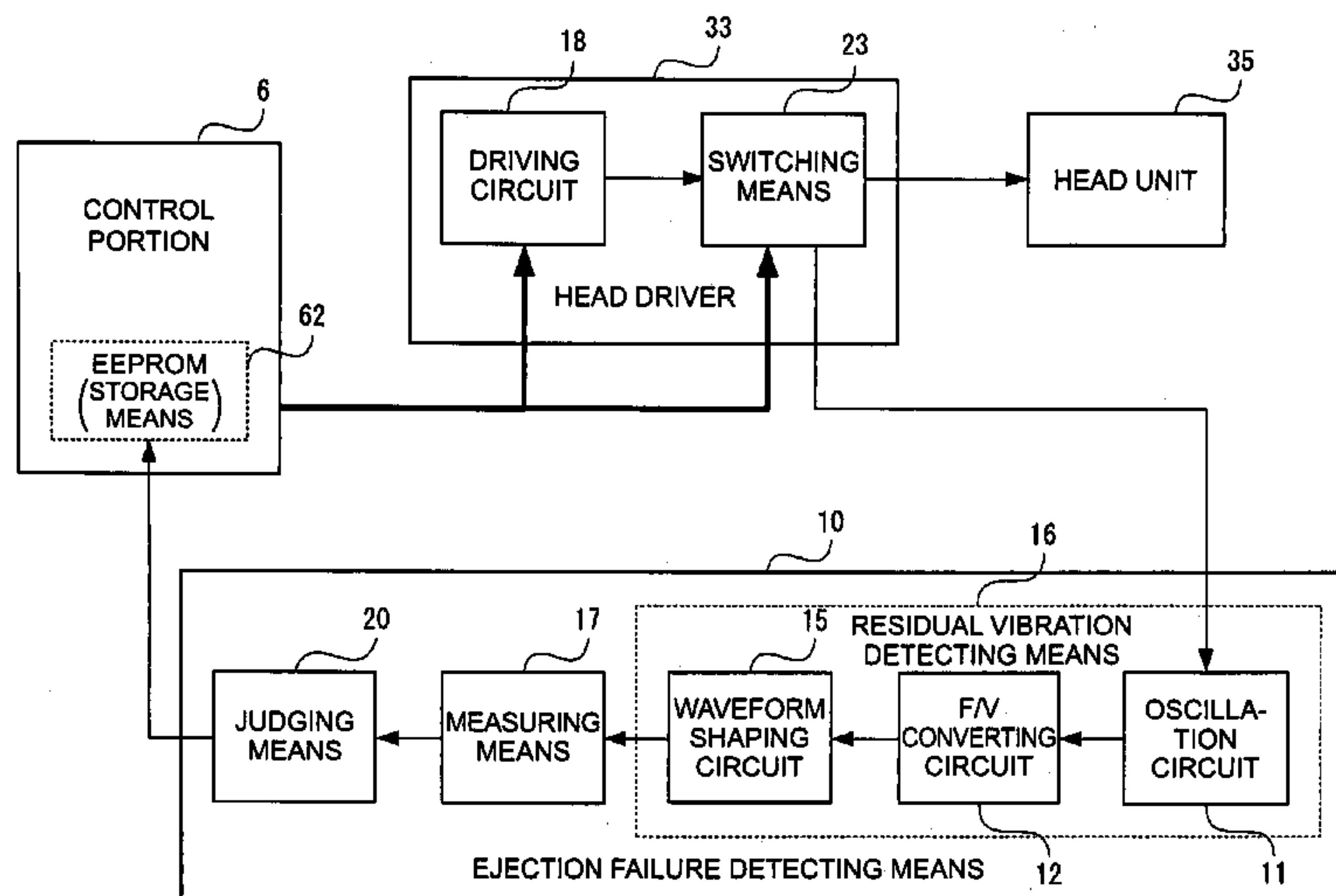
A droplet ejection apparatus is provided having a plurality of droplet ejection heads each ejecting liquid within a cavity through a nozzle in the form of droplets by driving an actuator with a driving circuit. The apparatus includes: ejection failure detecting means for detecting an ejection failure of the droplet ejection heads and a cause thereof; and recovery means for performing a recovery process depending on the cause of the ejection failure if the ejection failure detecting means detects the ejection failure when the droplets are ejected through the nozzles. Also, if a failing nozzle is detected, a recovery process is performed depending on the cause of the ejection failure at least for the failing nozzle. Thereafter, detection by the ejection failure detecting means is repeated by forcing the failing nozzle to perform a droplet ejection operation alone.

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70 Claims, 48 Drawing Sheets



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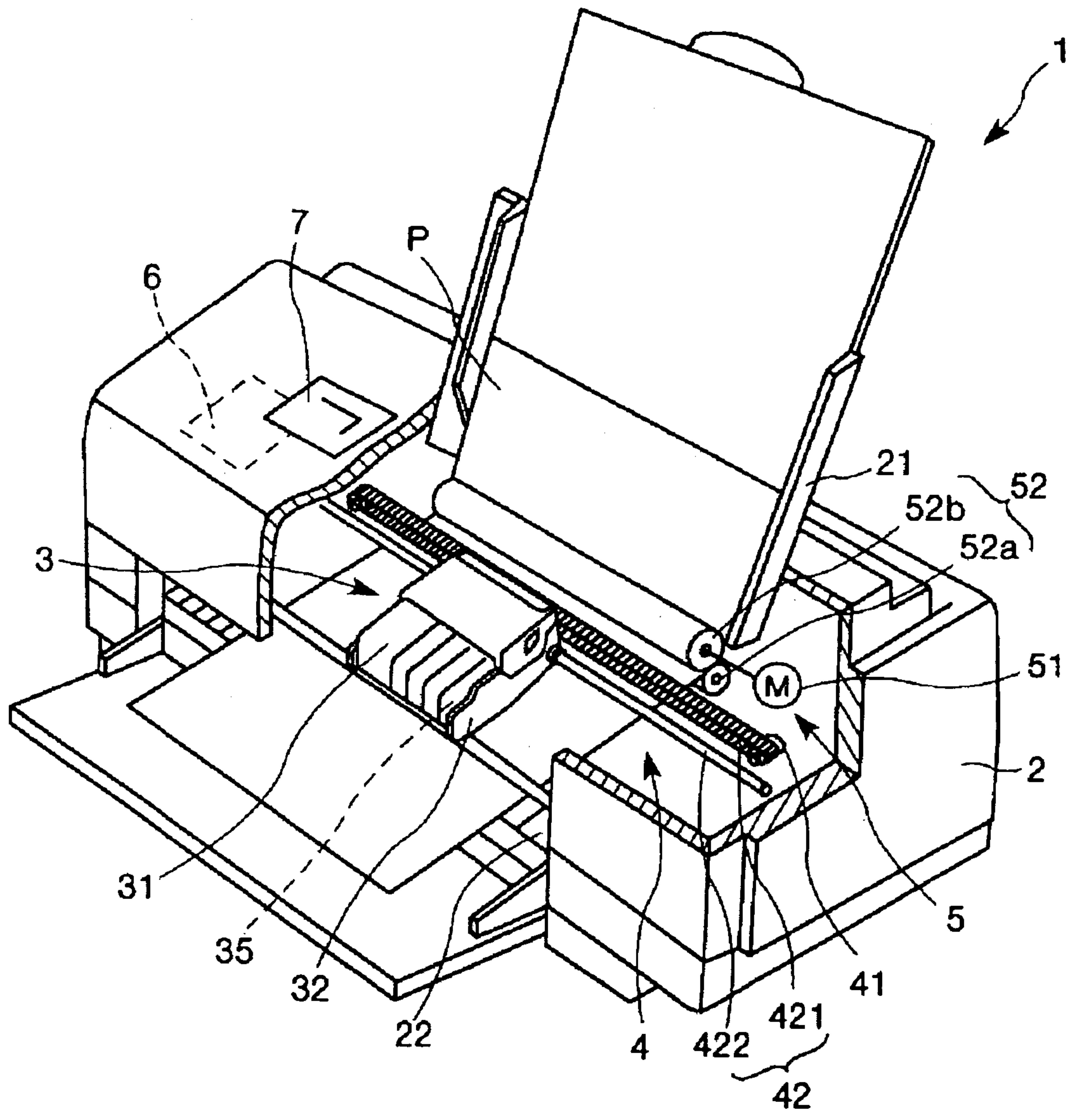


FIG. 1

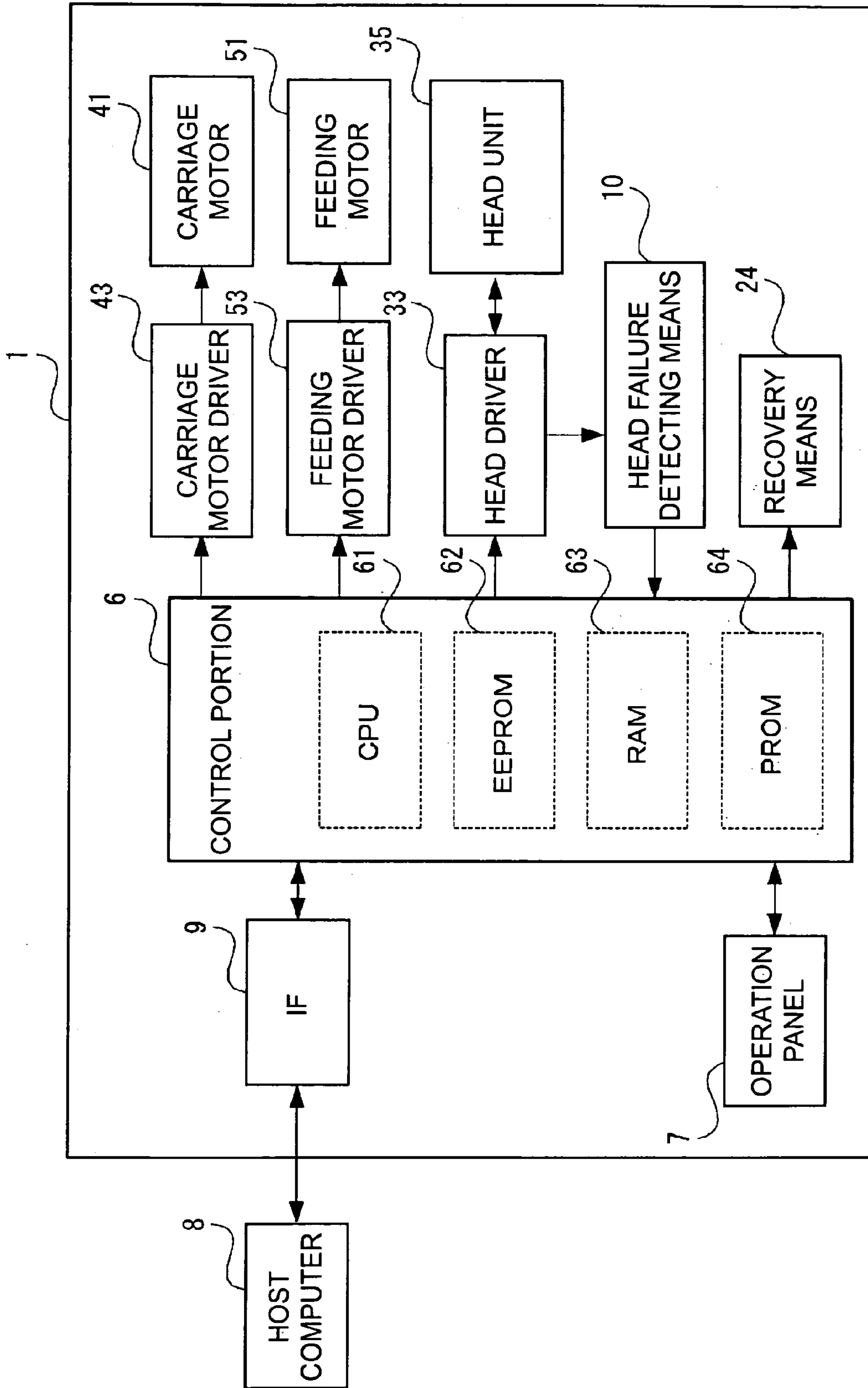


FIG. 2

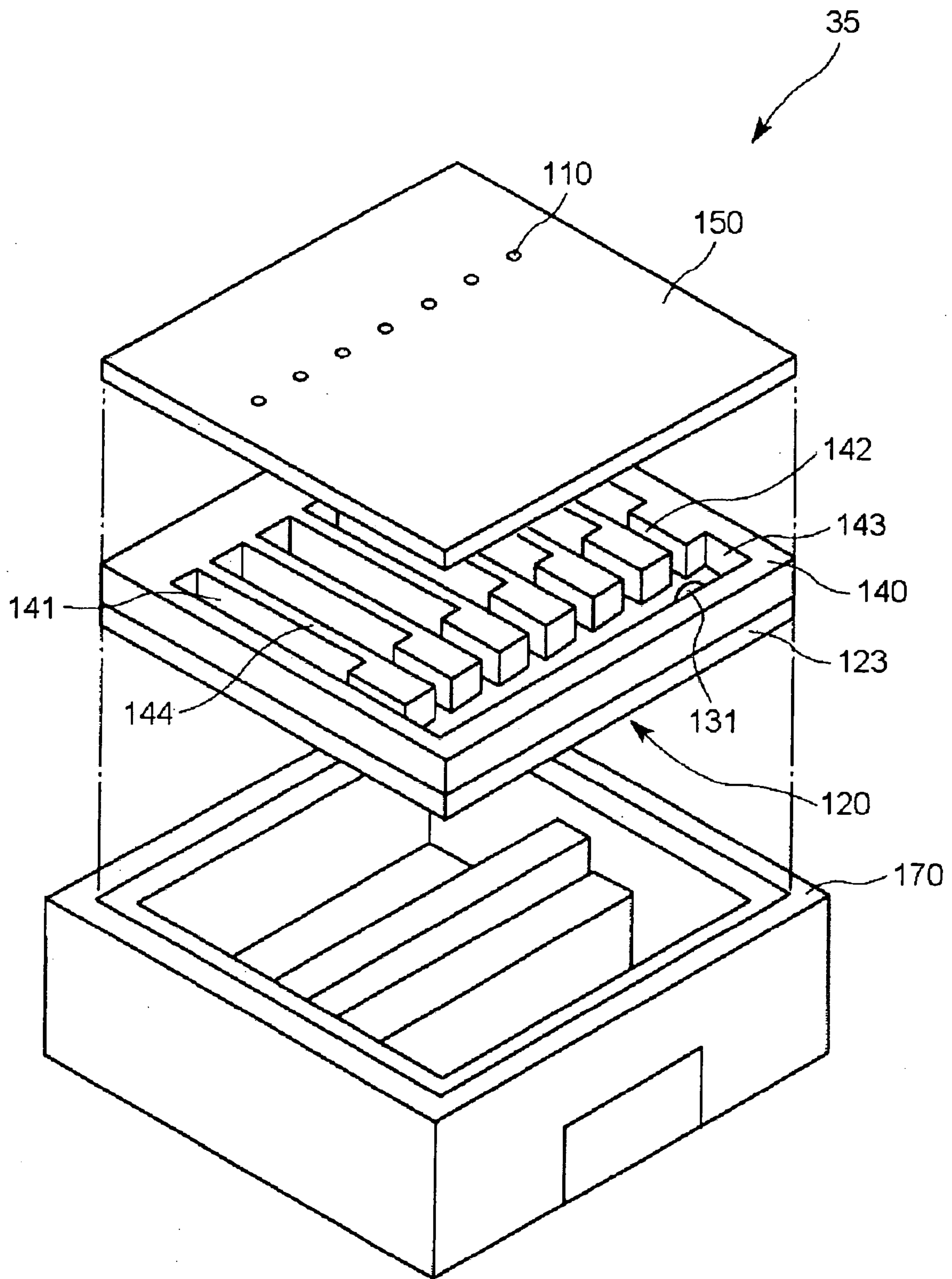


FIG. 4

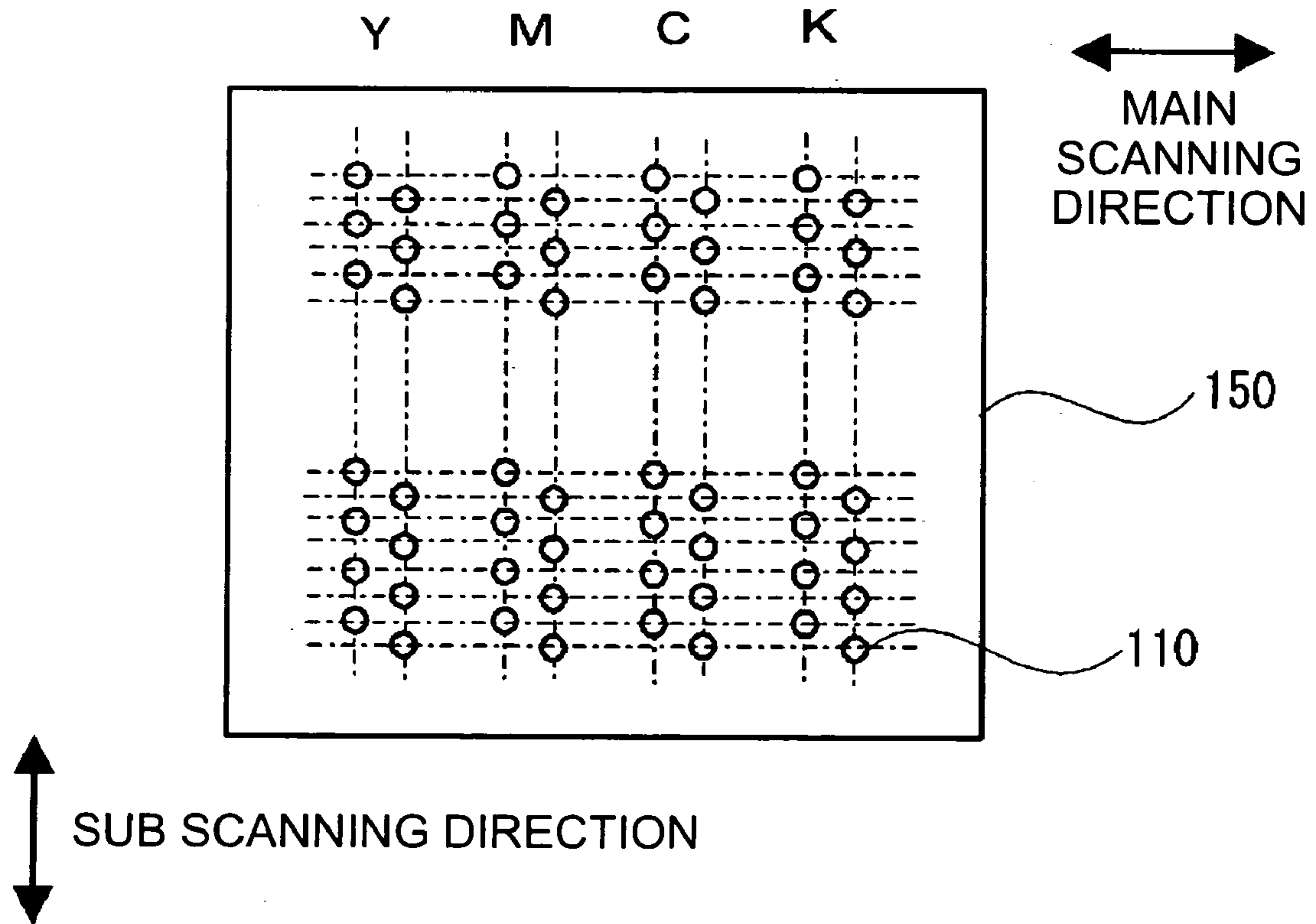


FIG. 5

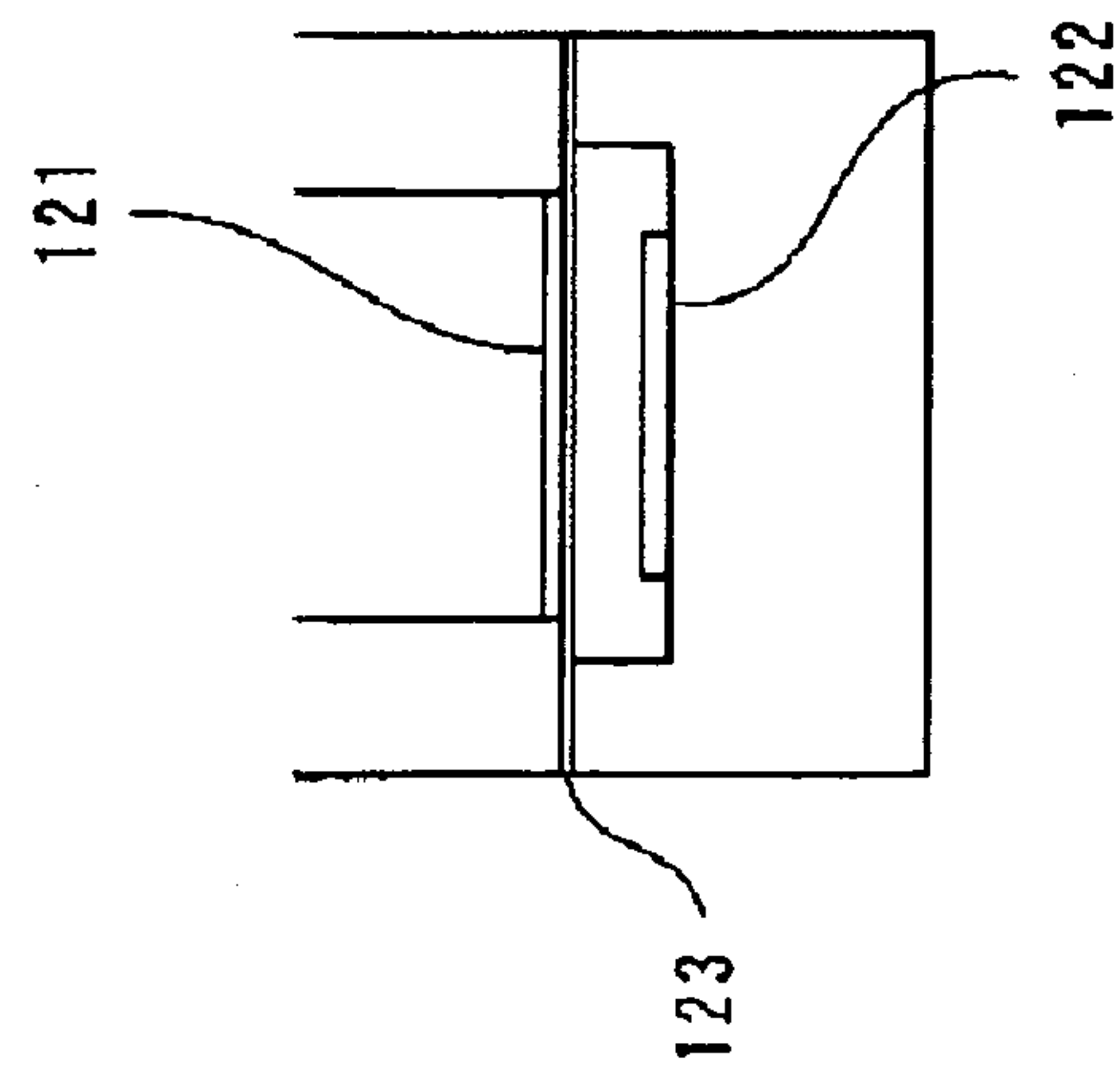


FIG. 6A

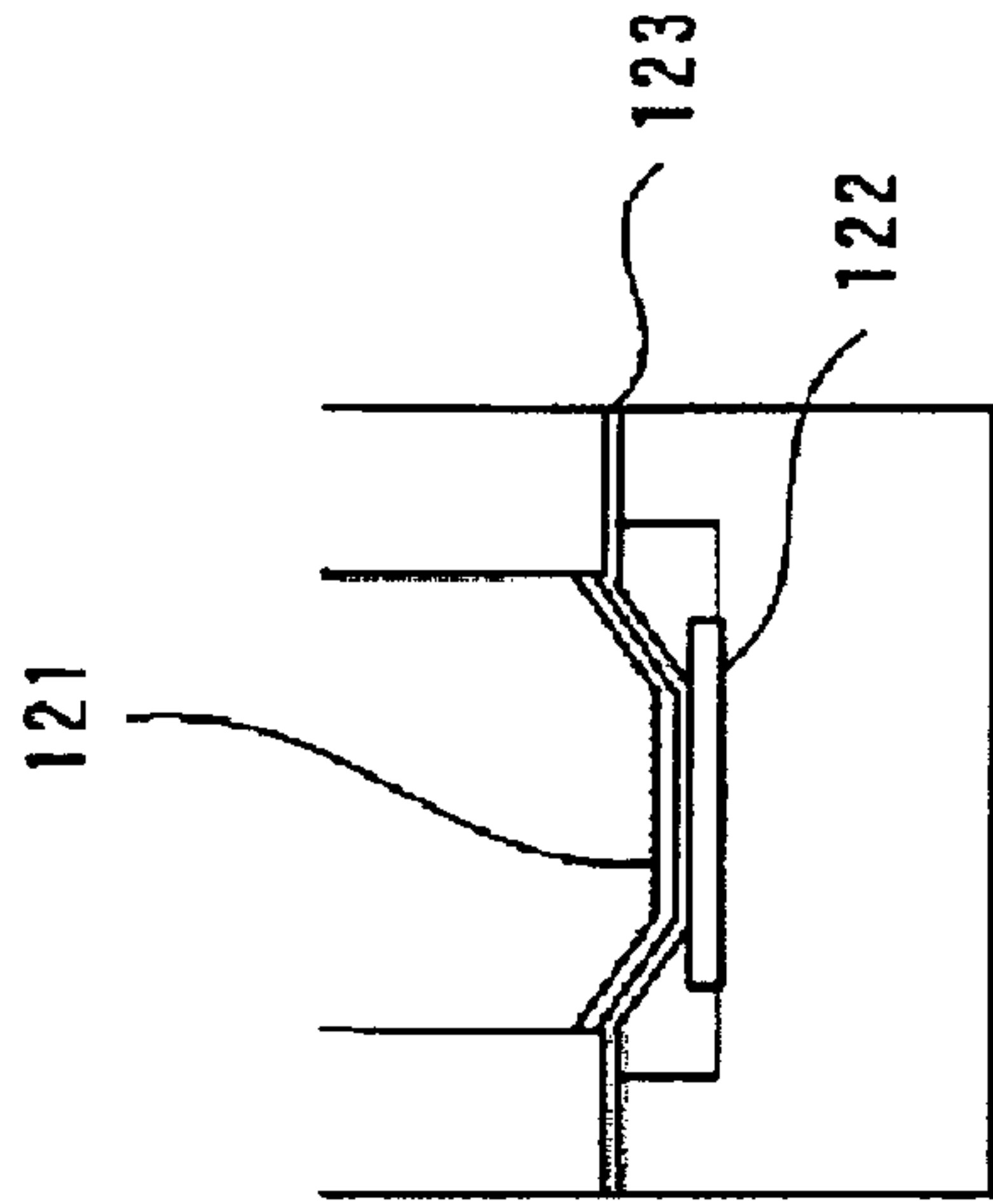


FIG. 6B

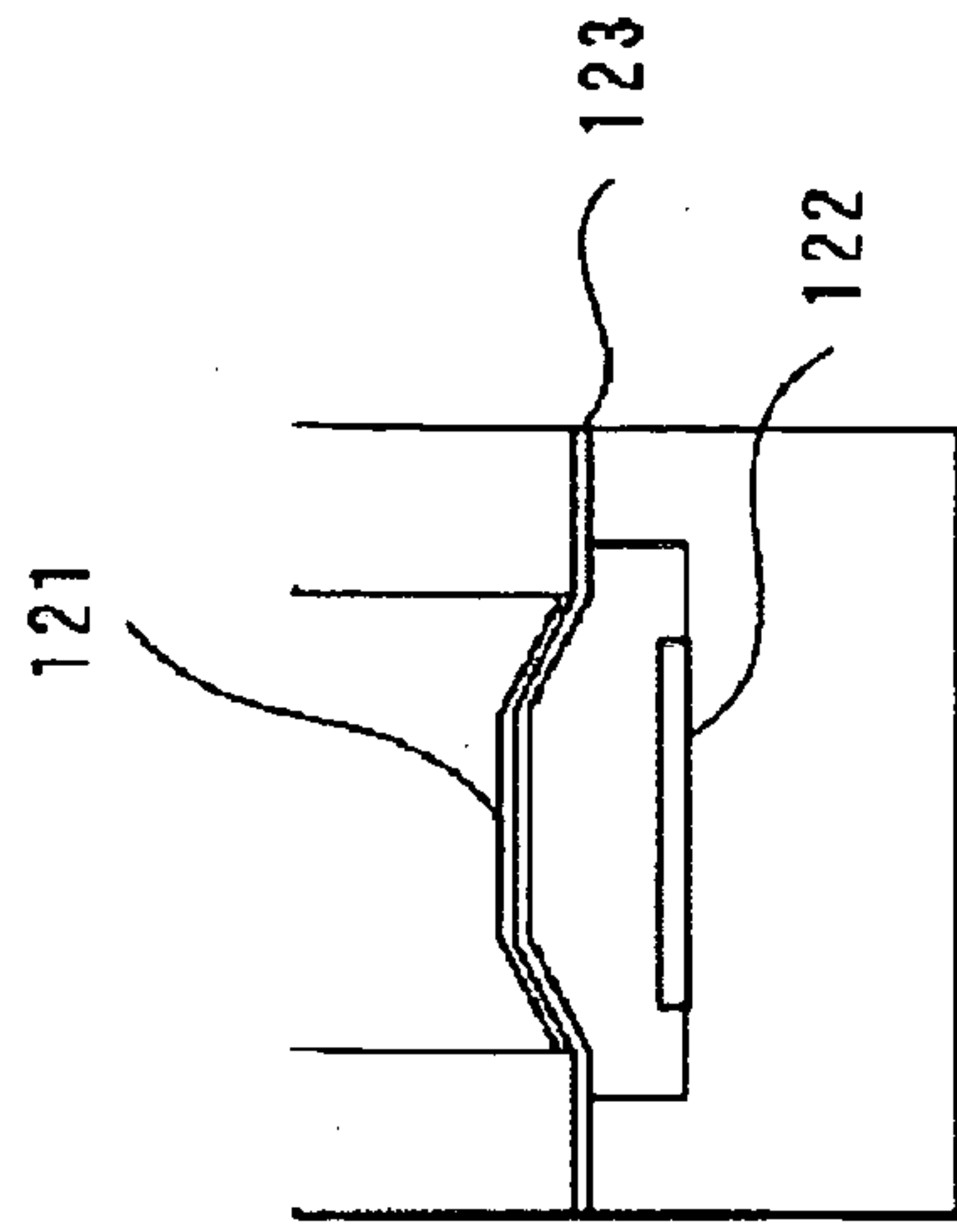


FIG. 6C

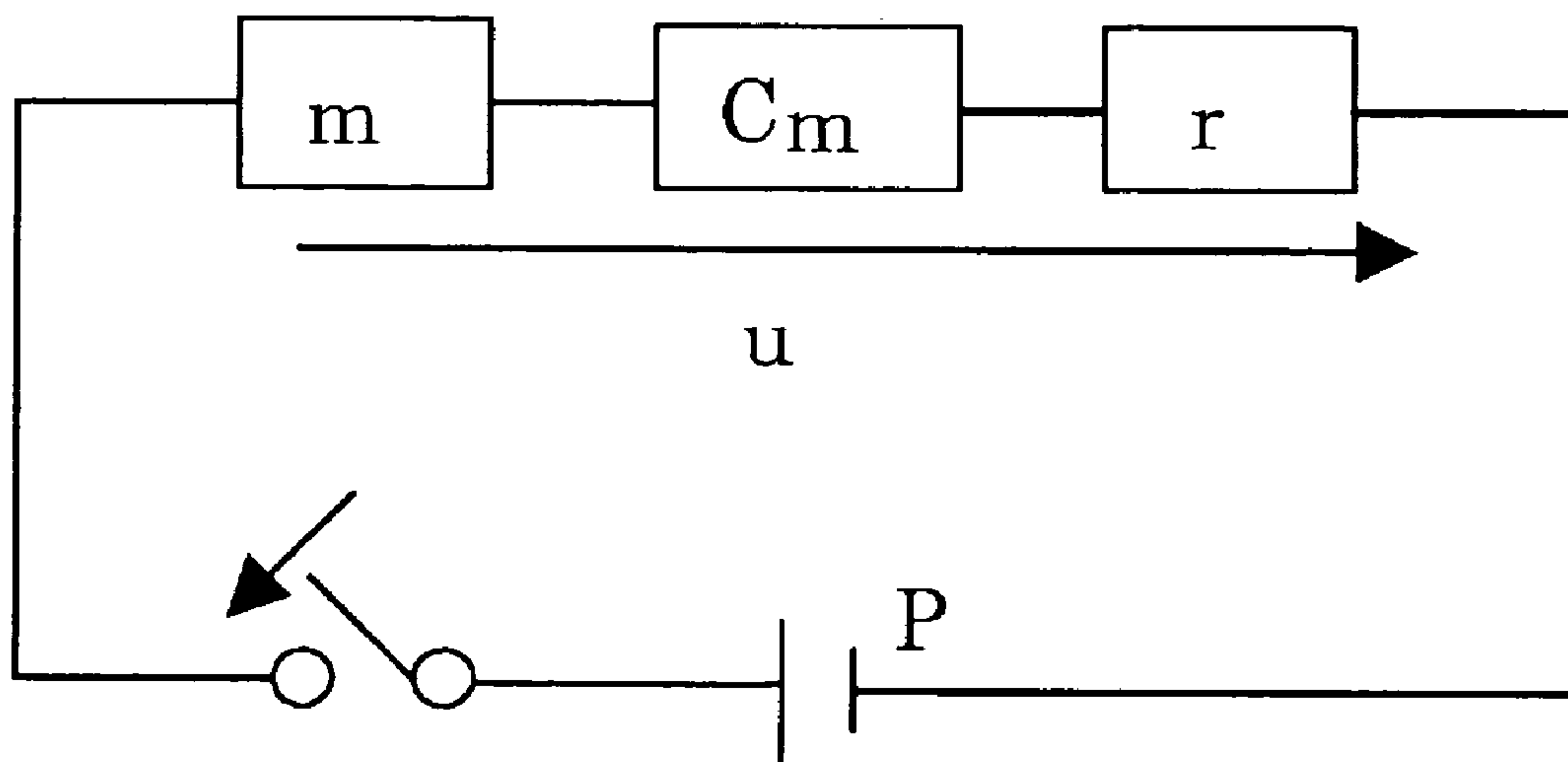


FIG. 7

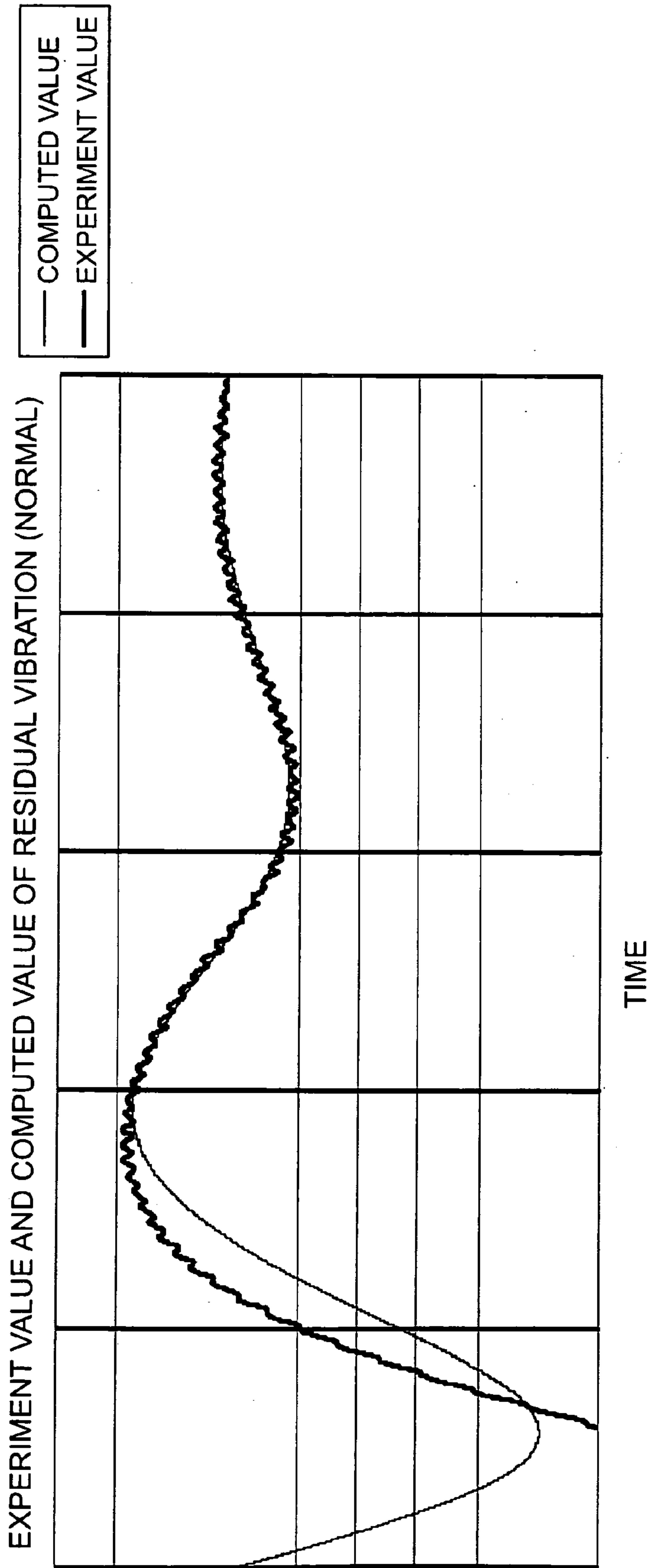


FIG. 8

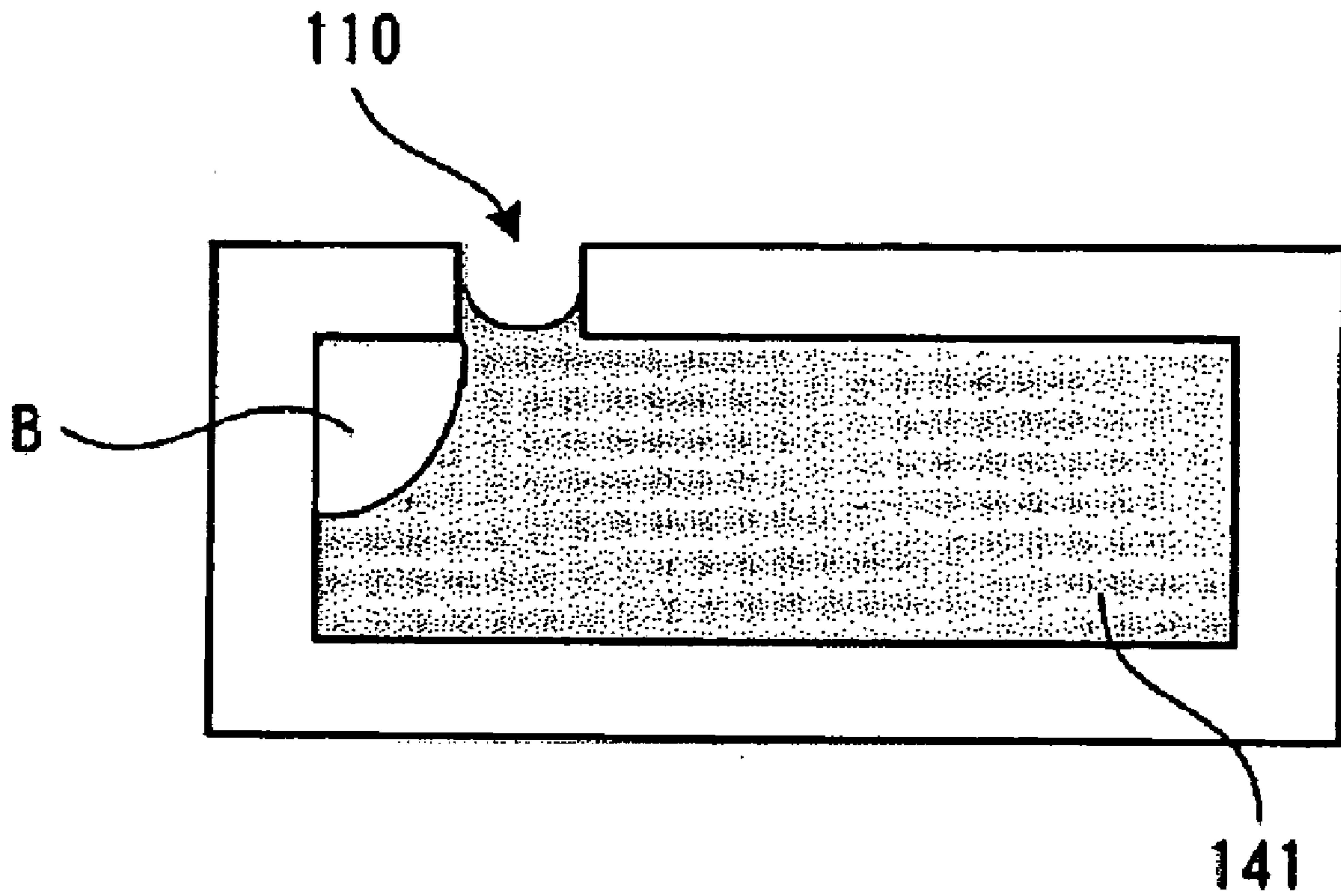


FIG. 9

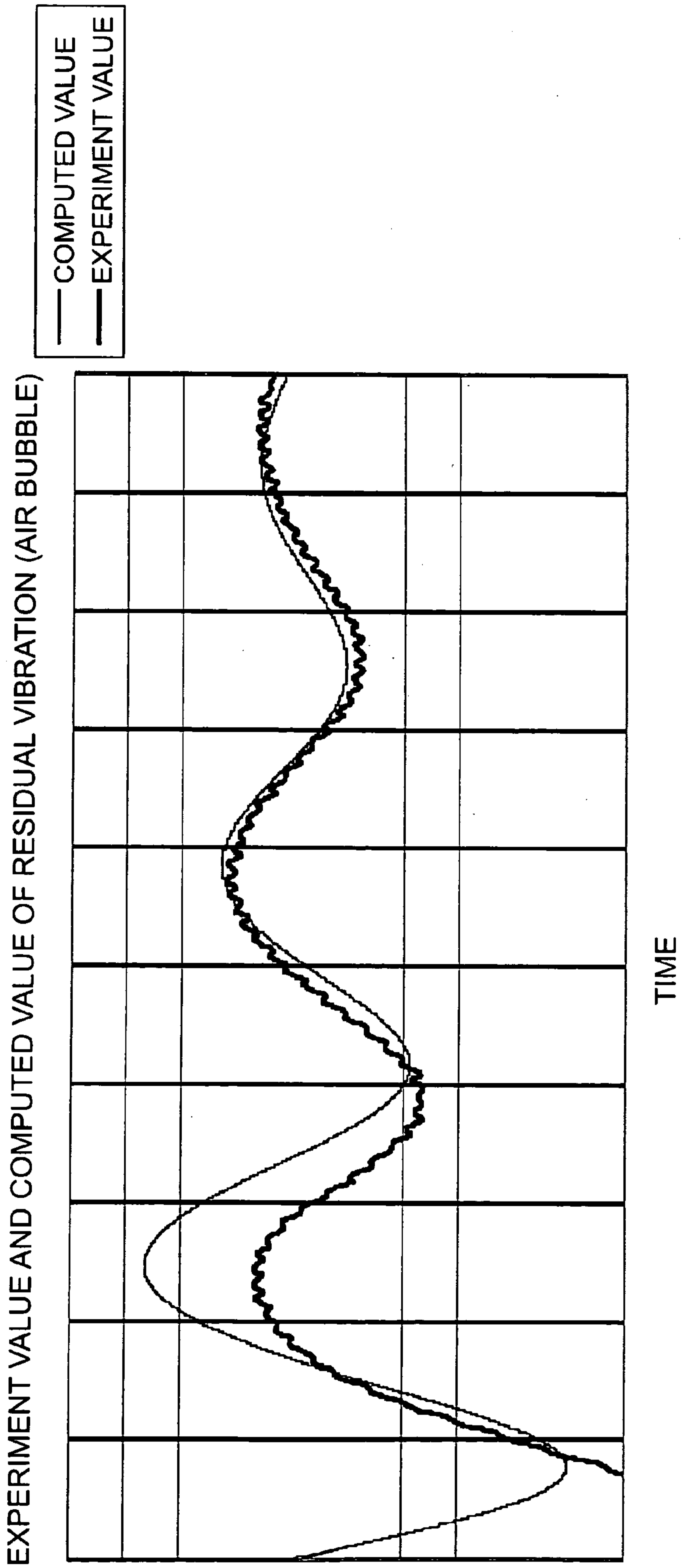


FIG.10

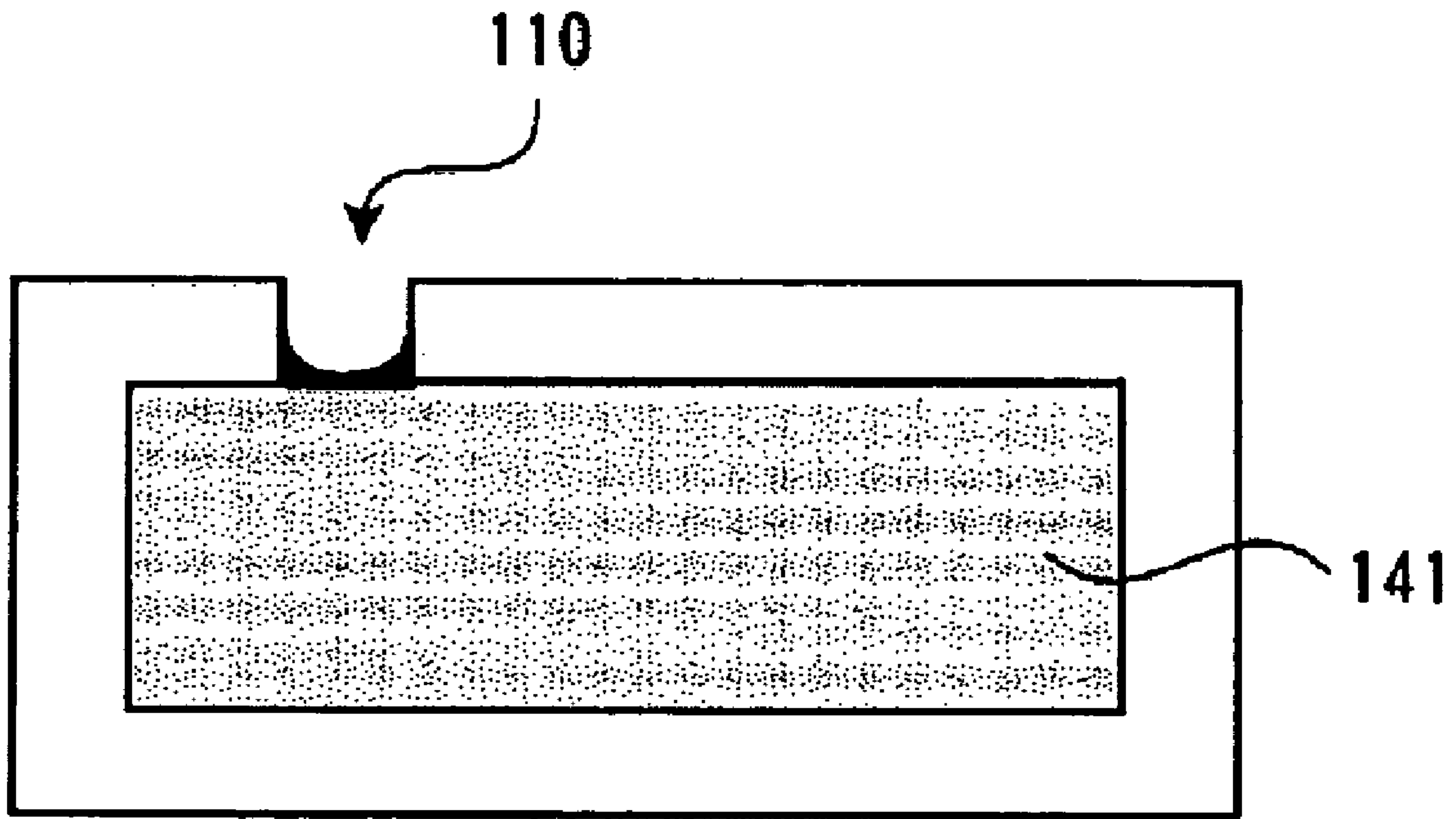


FIG. 11

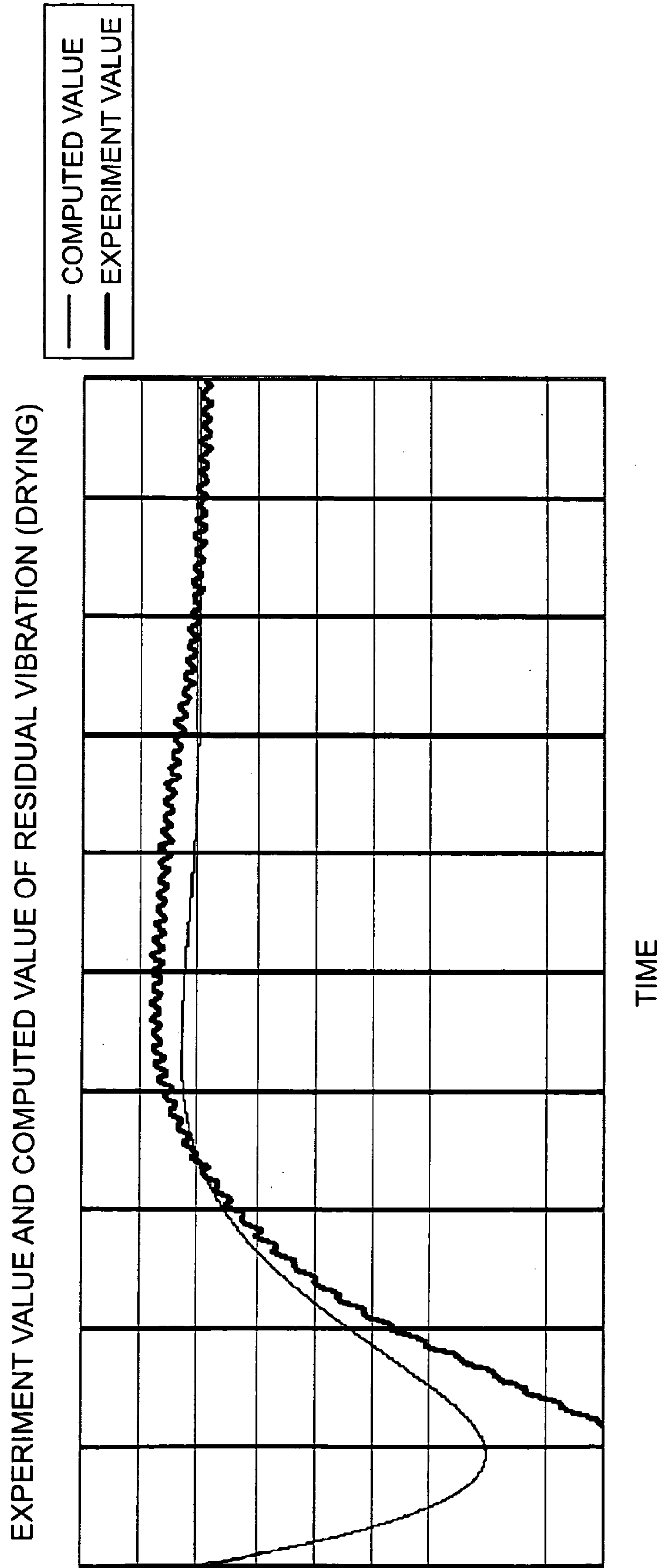


FIG.12

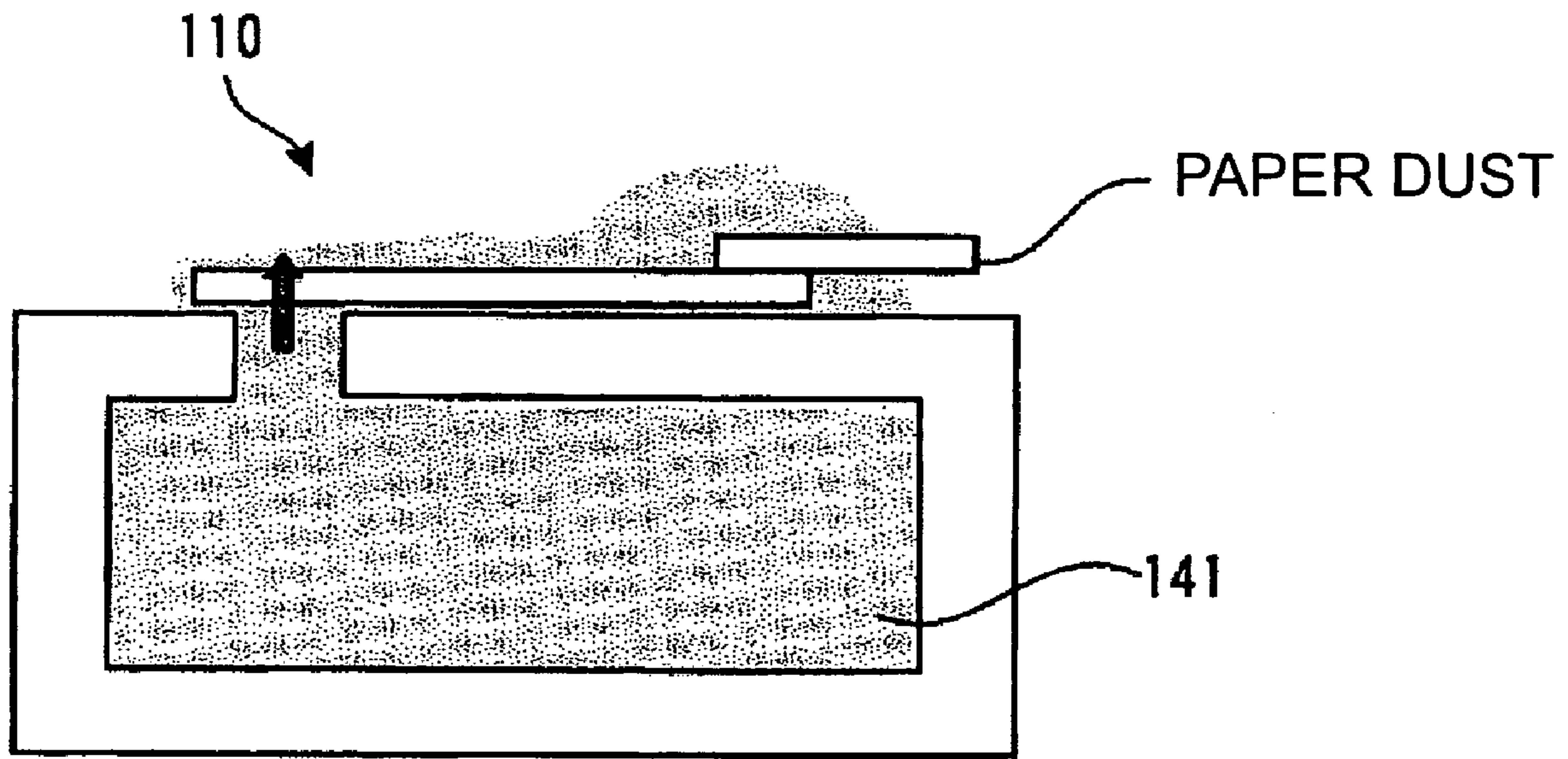


FIG.13

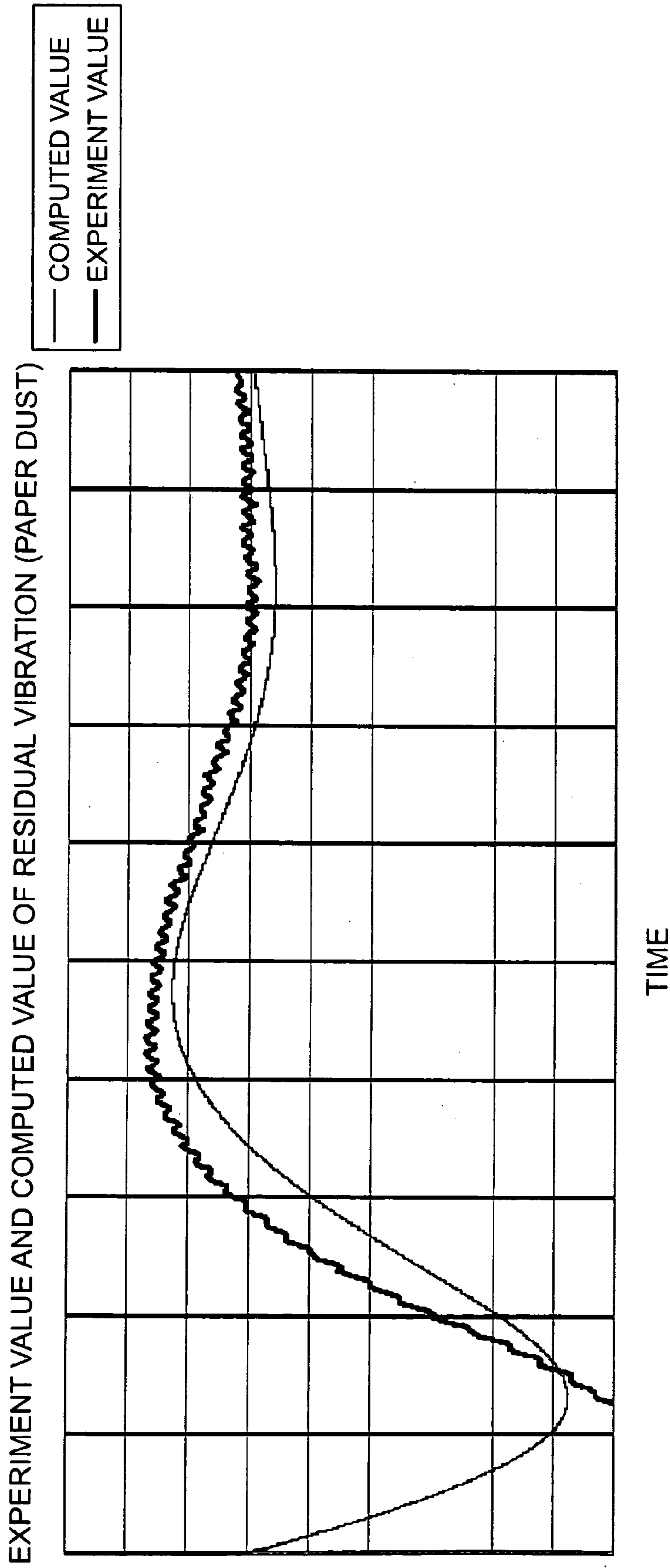


FIG.14



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BEFORE
ADHESION OF
PAPER DUST



PAPER DUST

AFTER
ADHESION OF
PAPER DUST

FIG.15A

FIG.15B

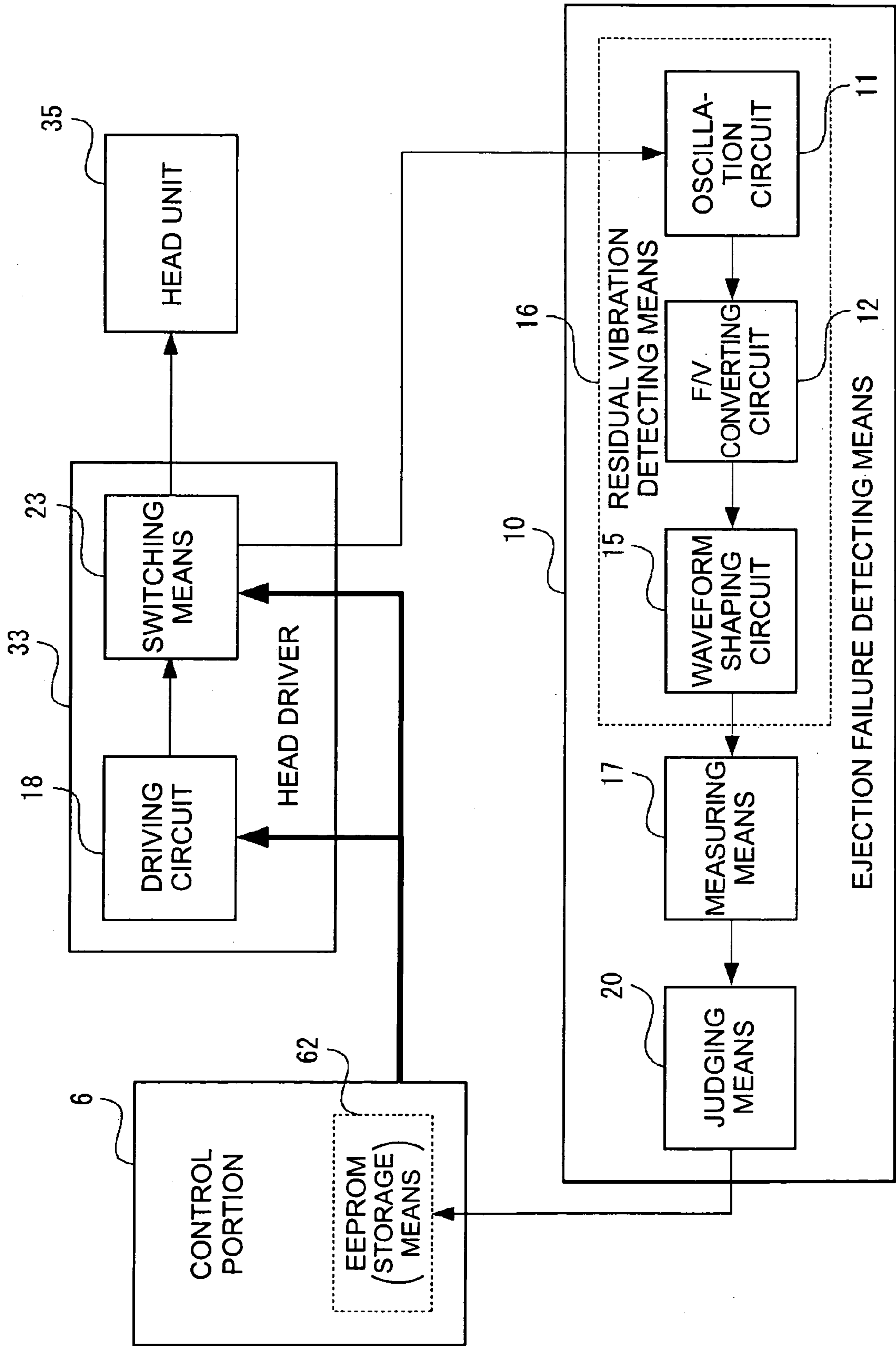


FIG.16

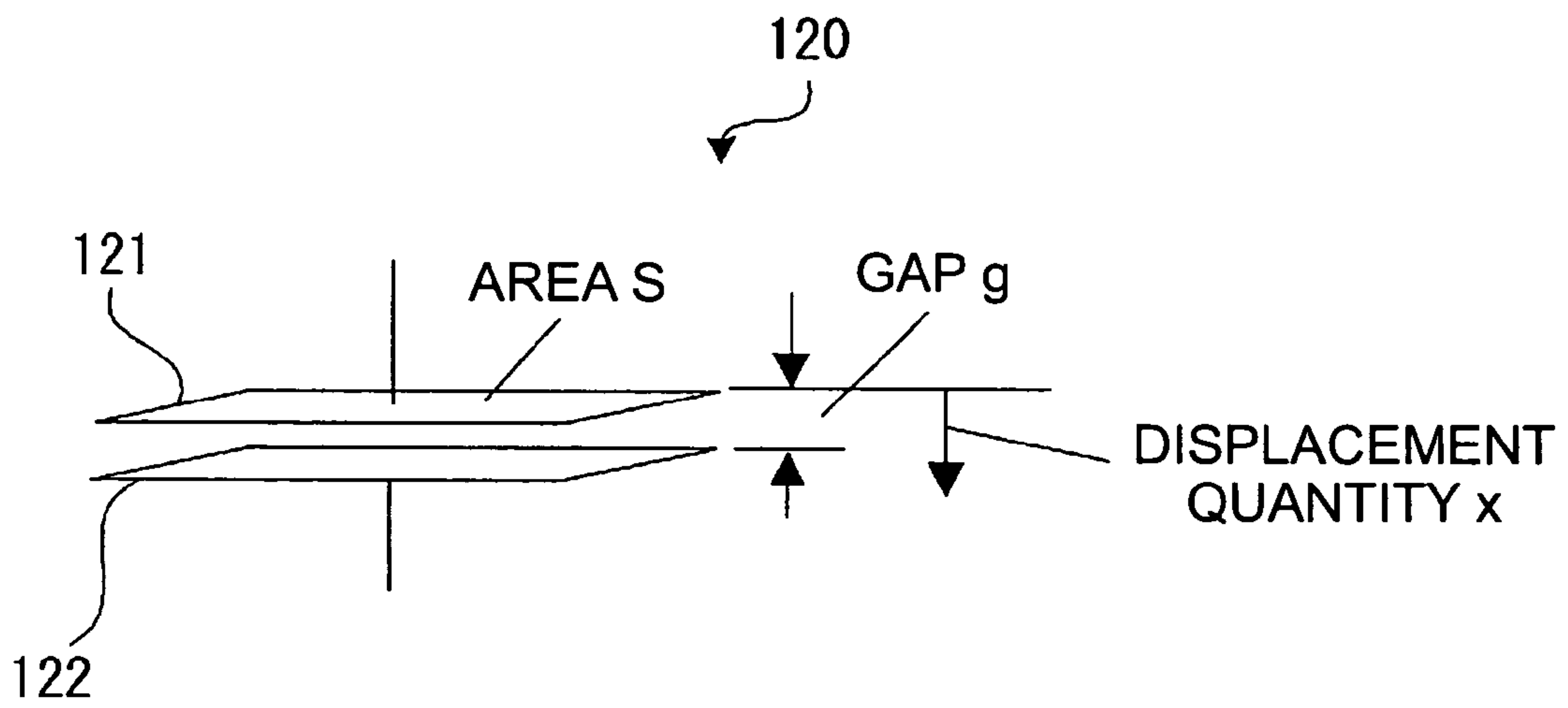


FIG.17

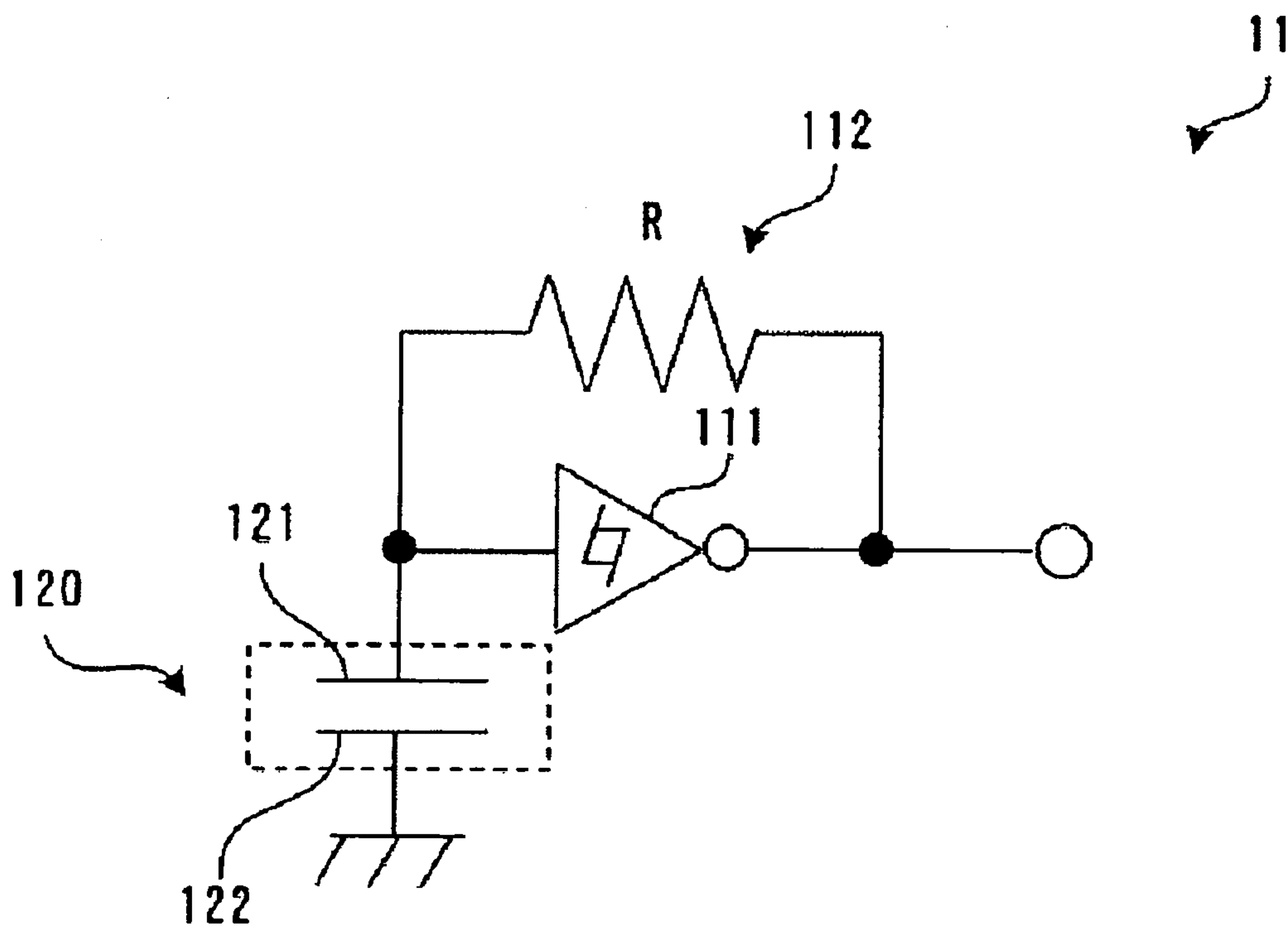


FIG.18

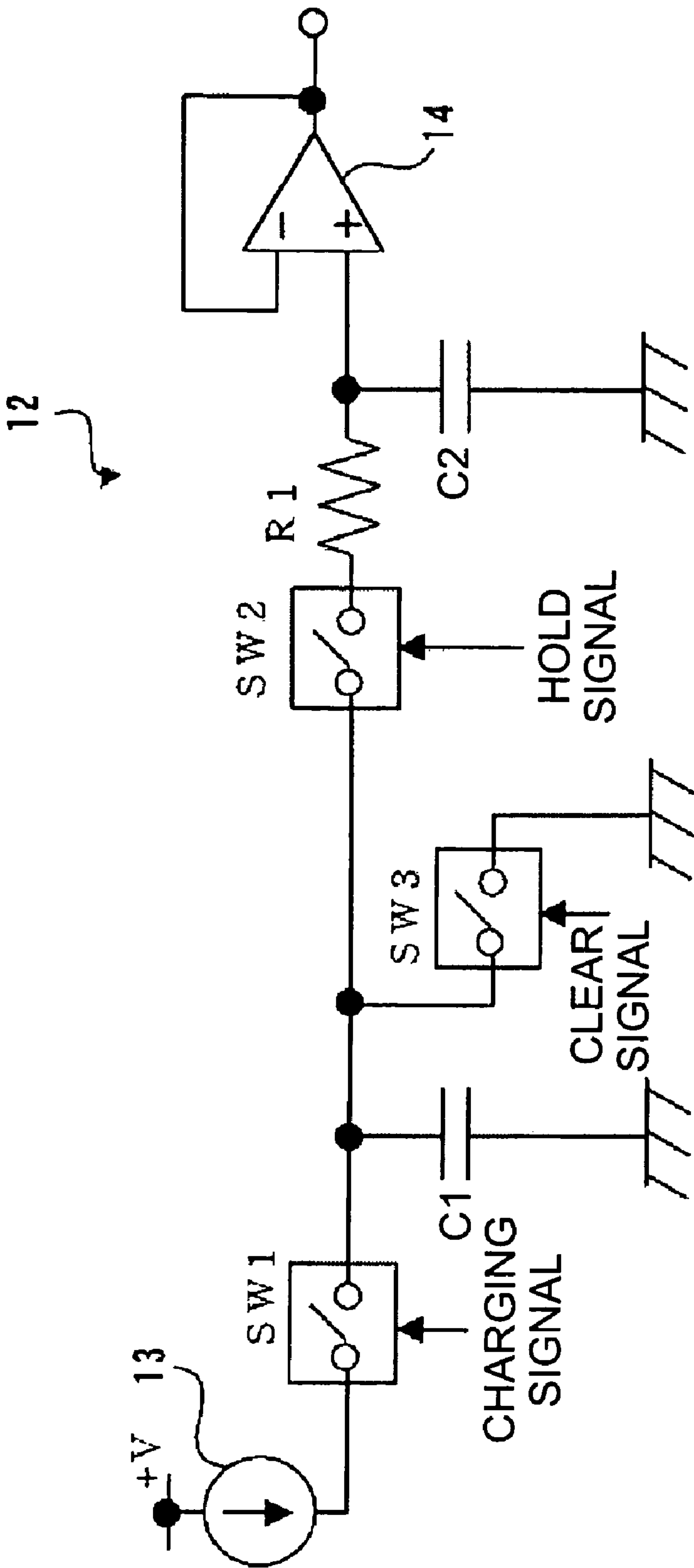


FIG.19

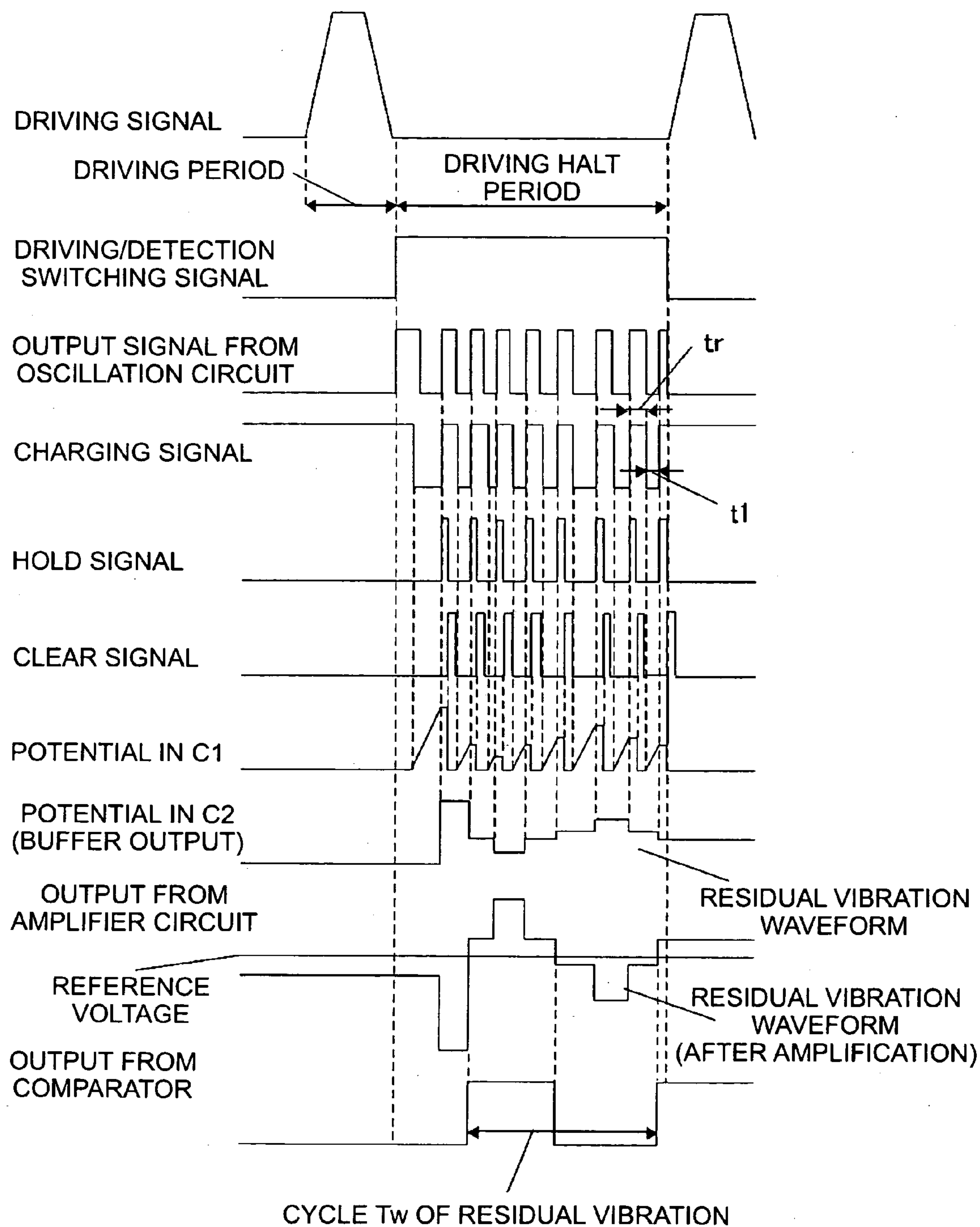


FIG.20

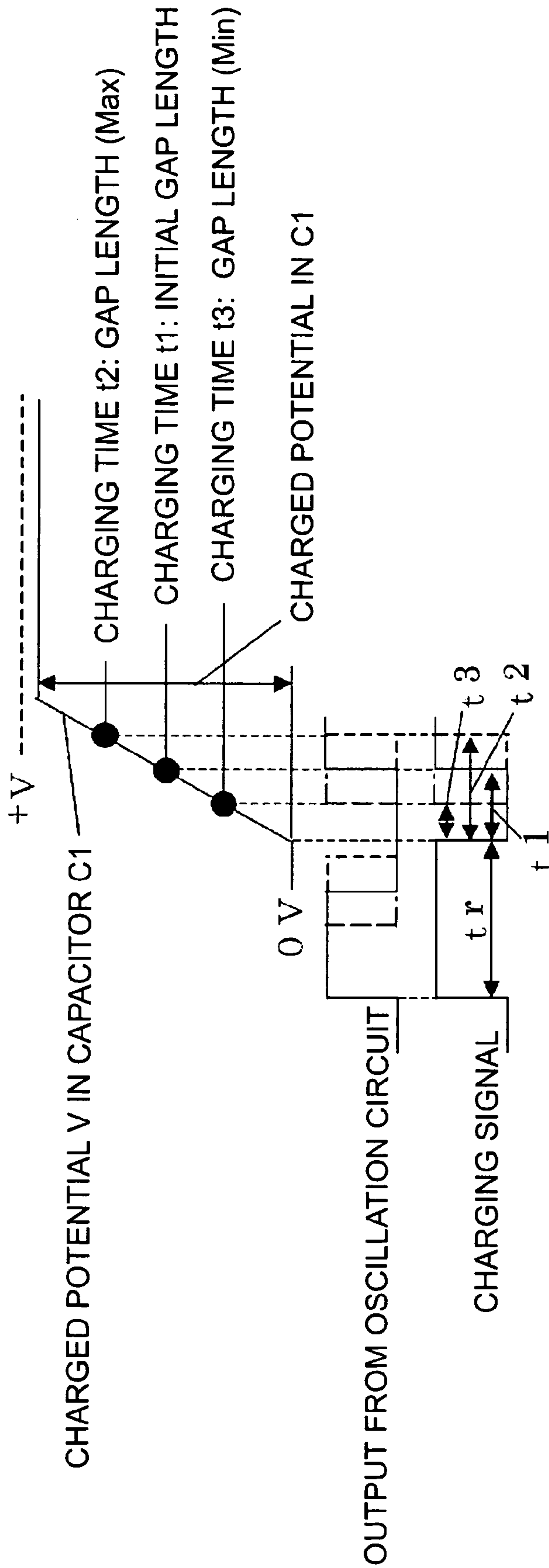


FIG.21

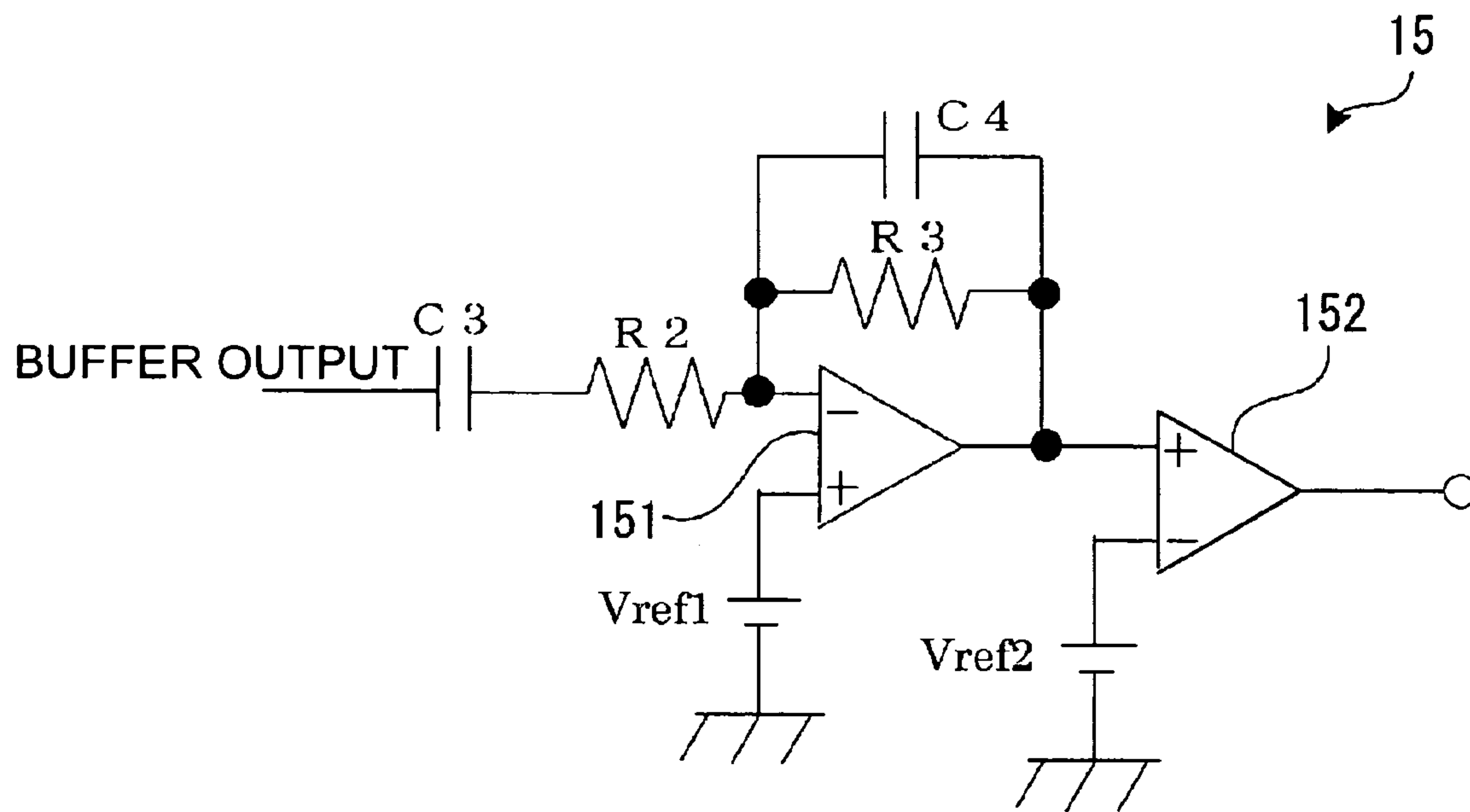


FIG.22

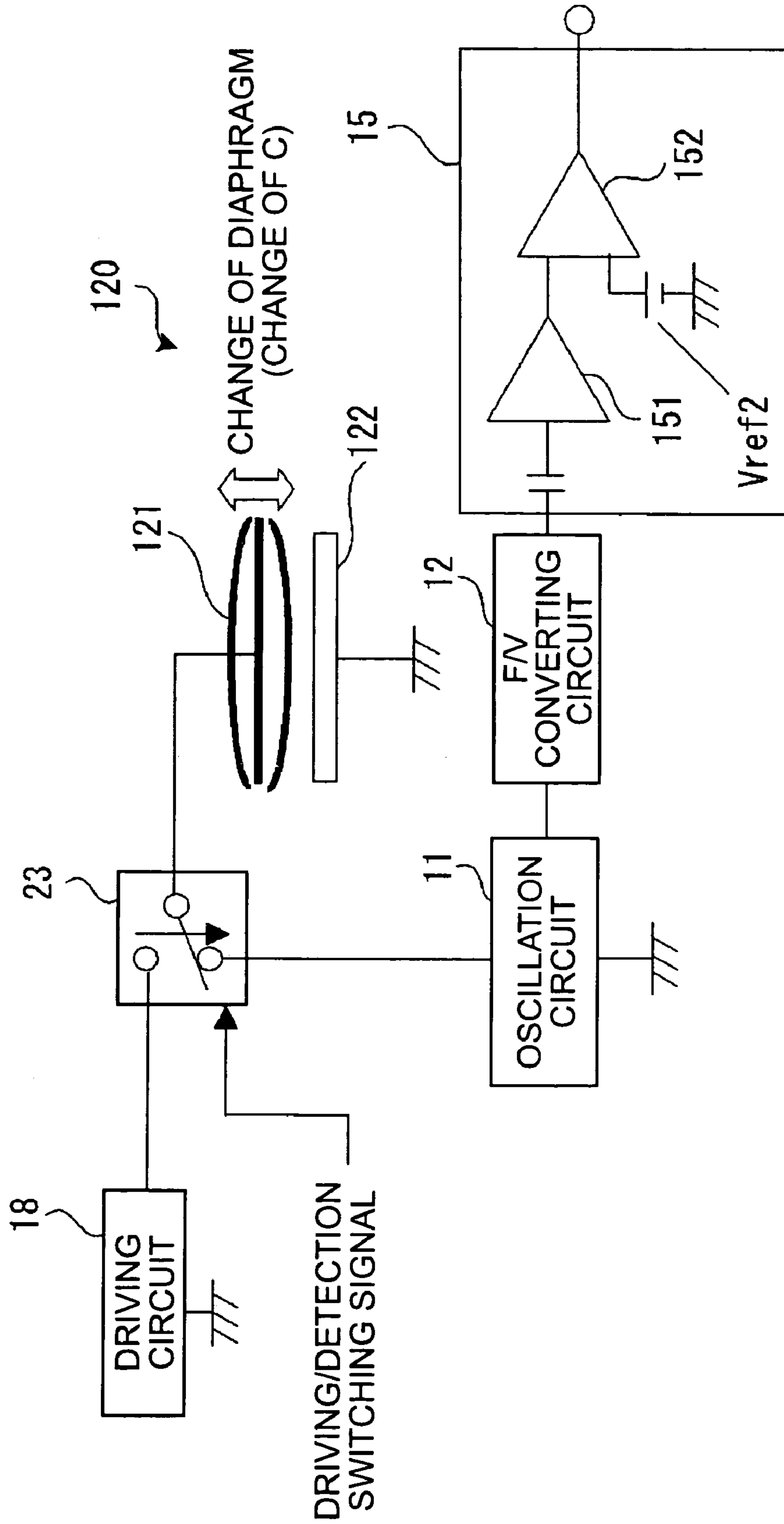


FIG.23

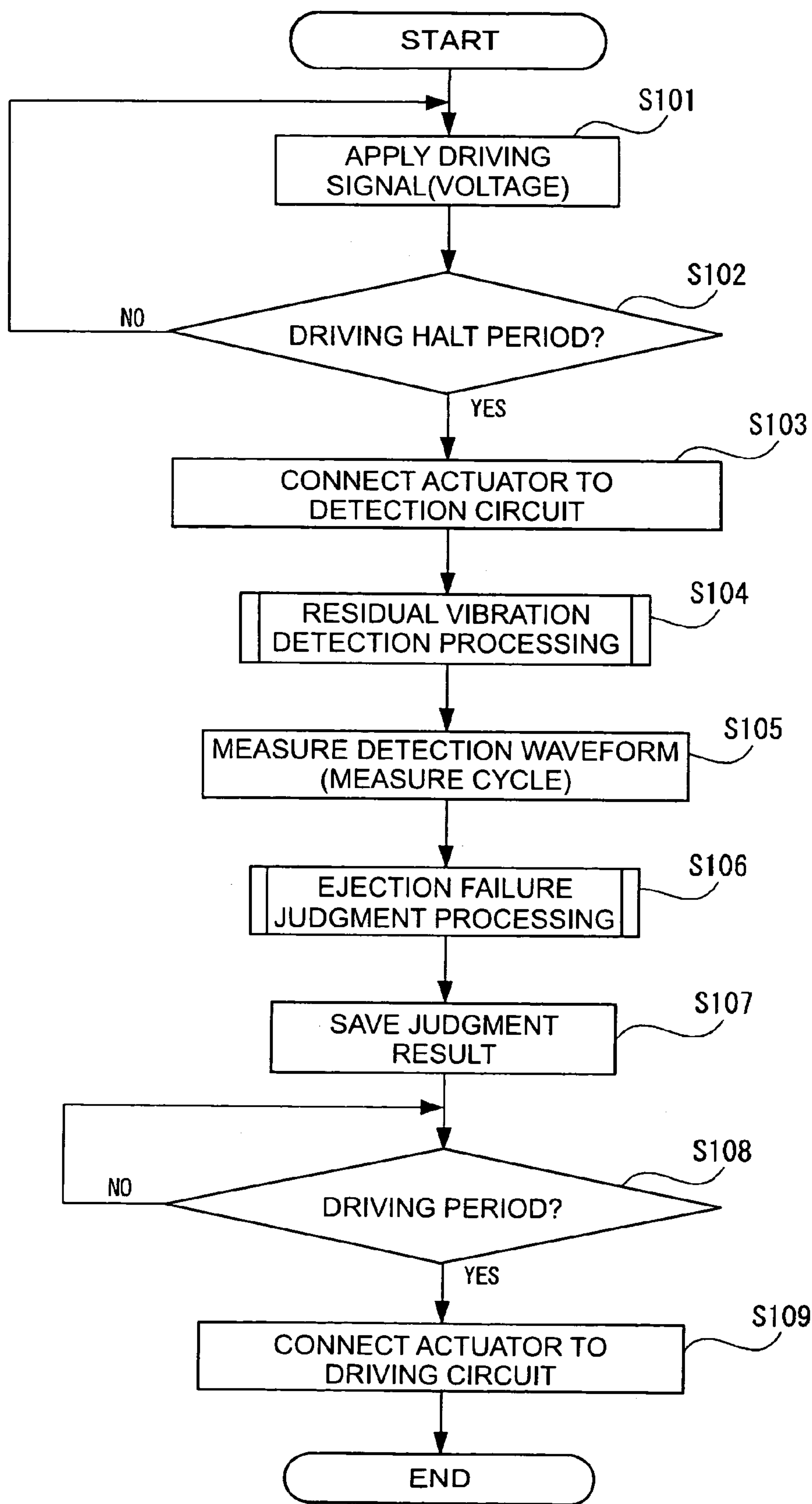


FIG.24

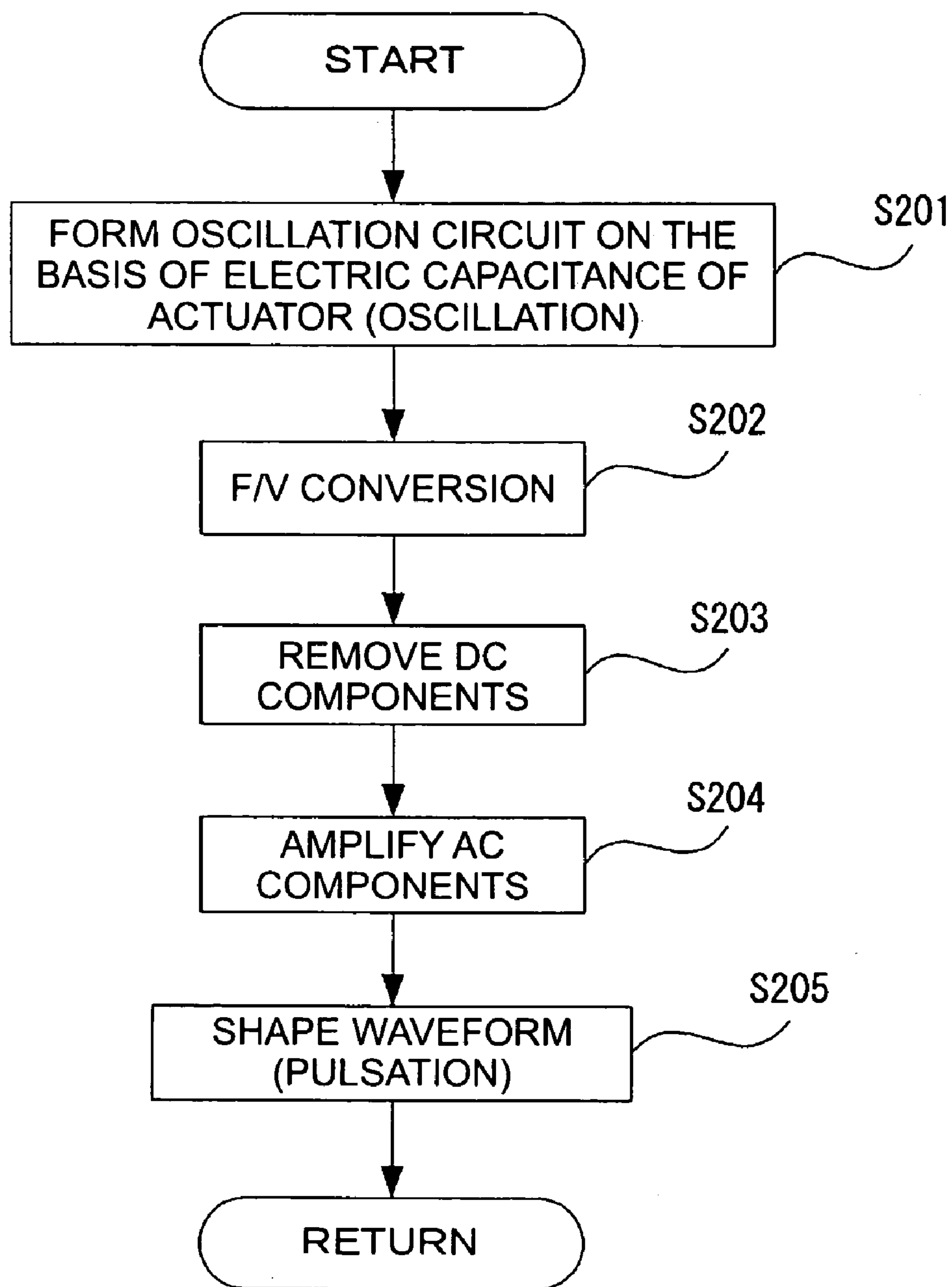


FIG.25

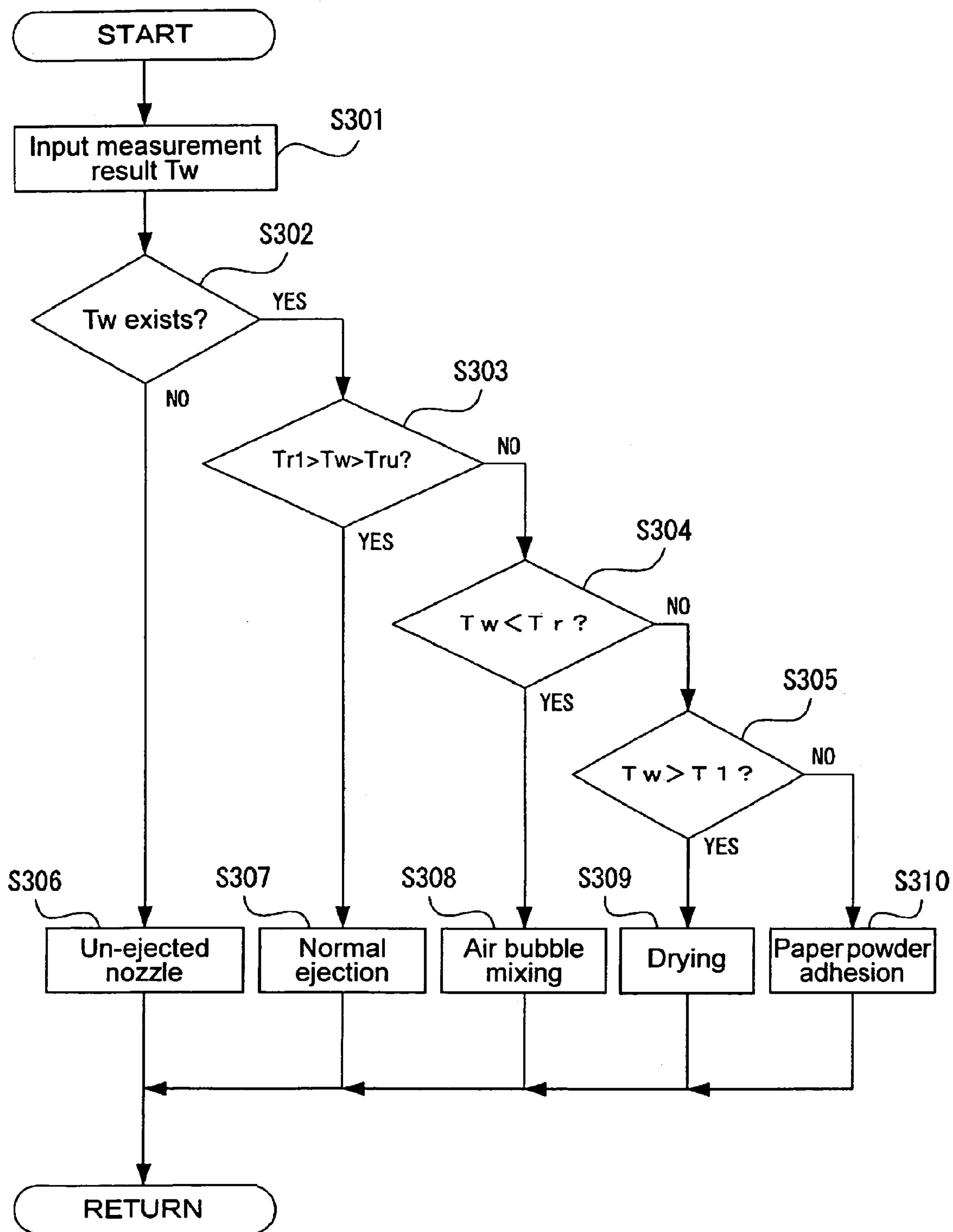


FIG.26

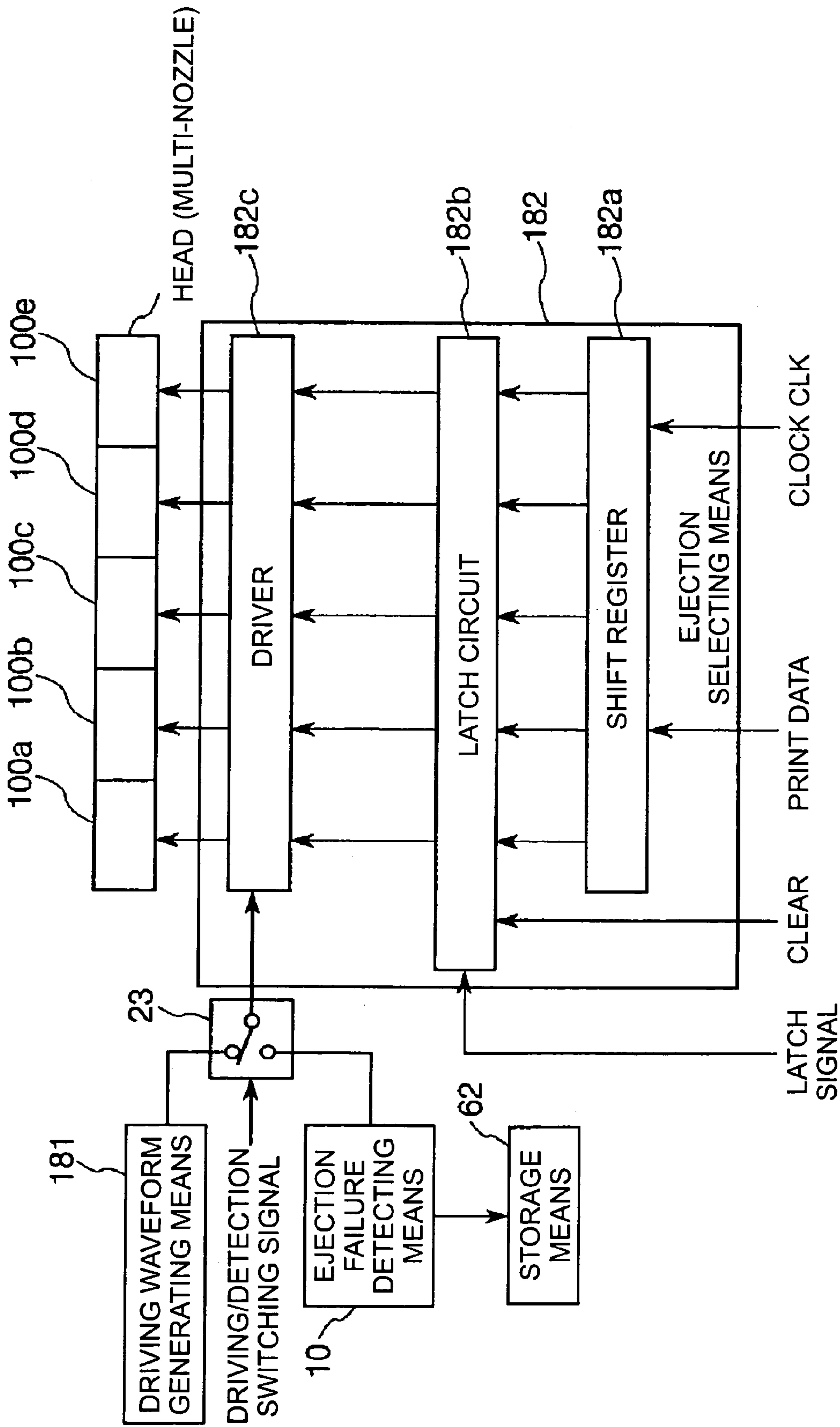


FIG. 27

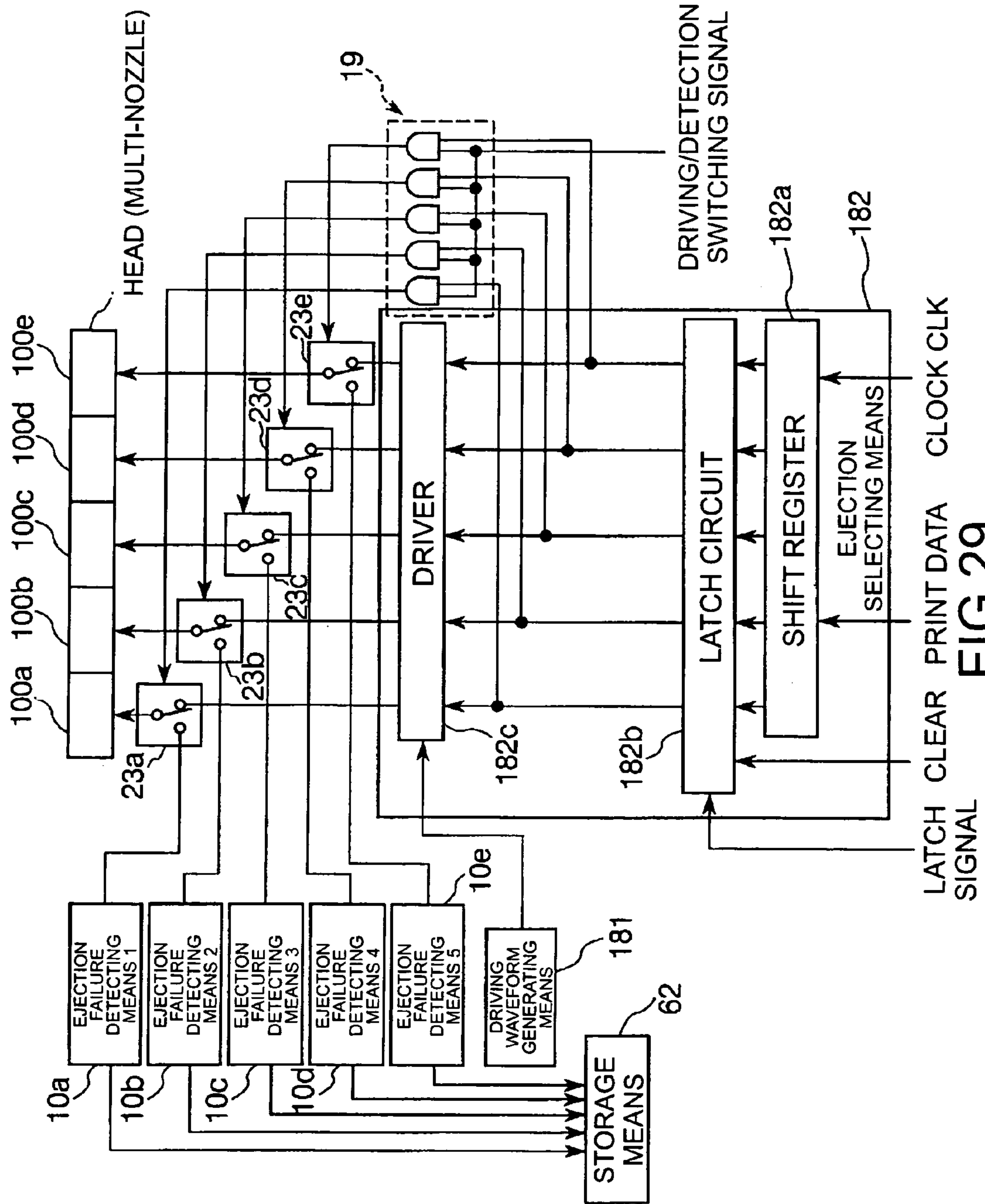


FIG. 29

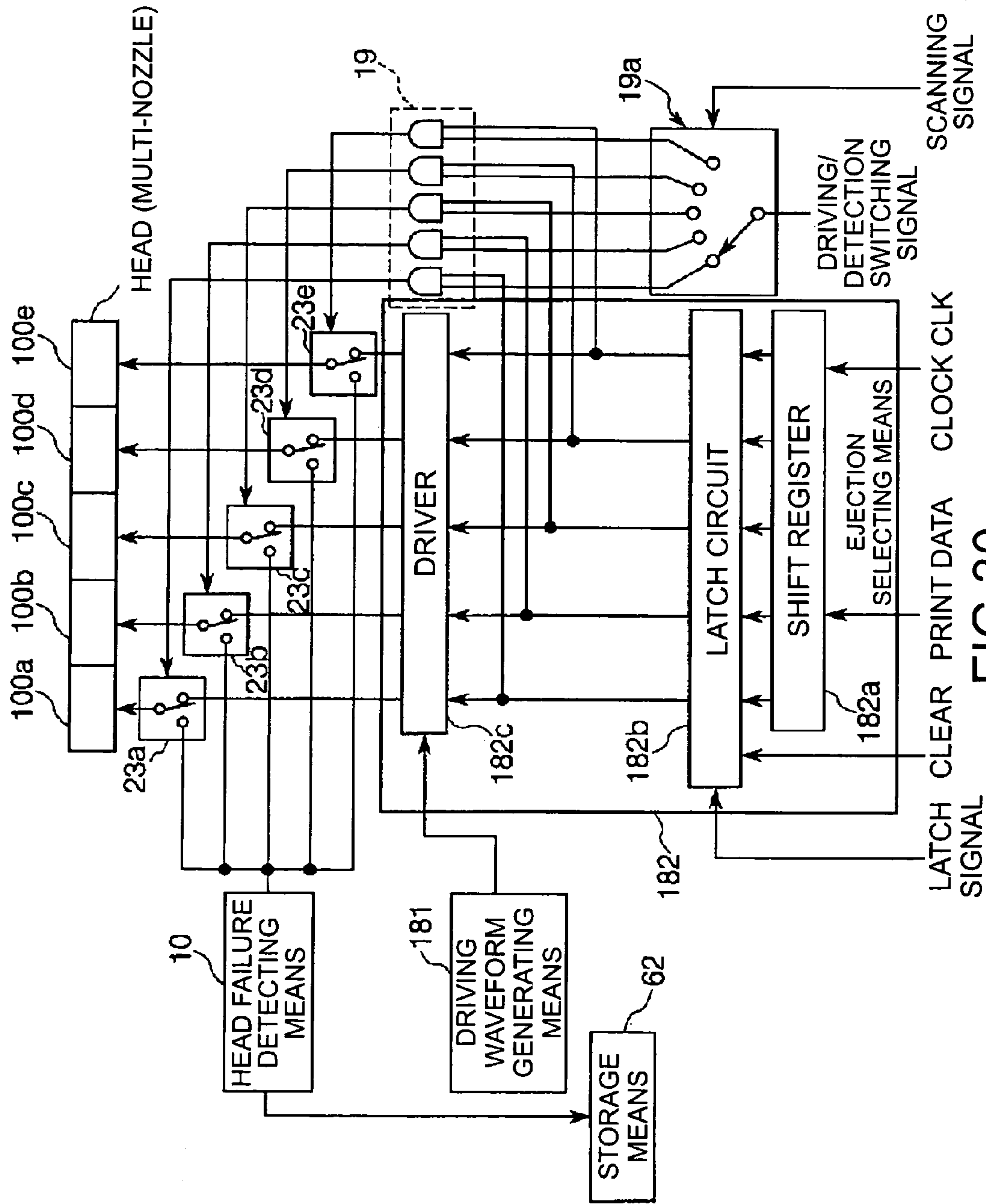


FIG. 30

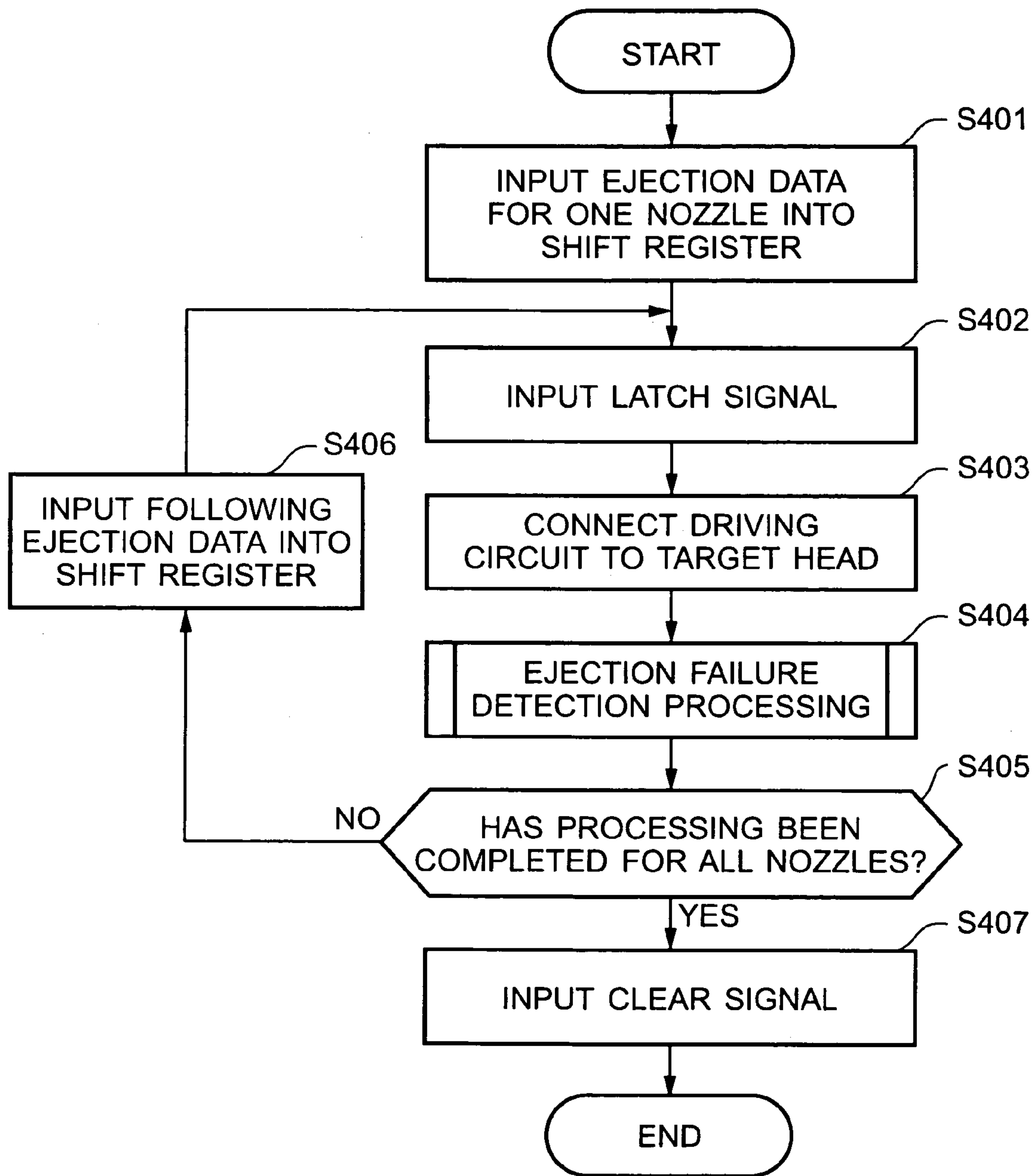


FIG.31

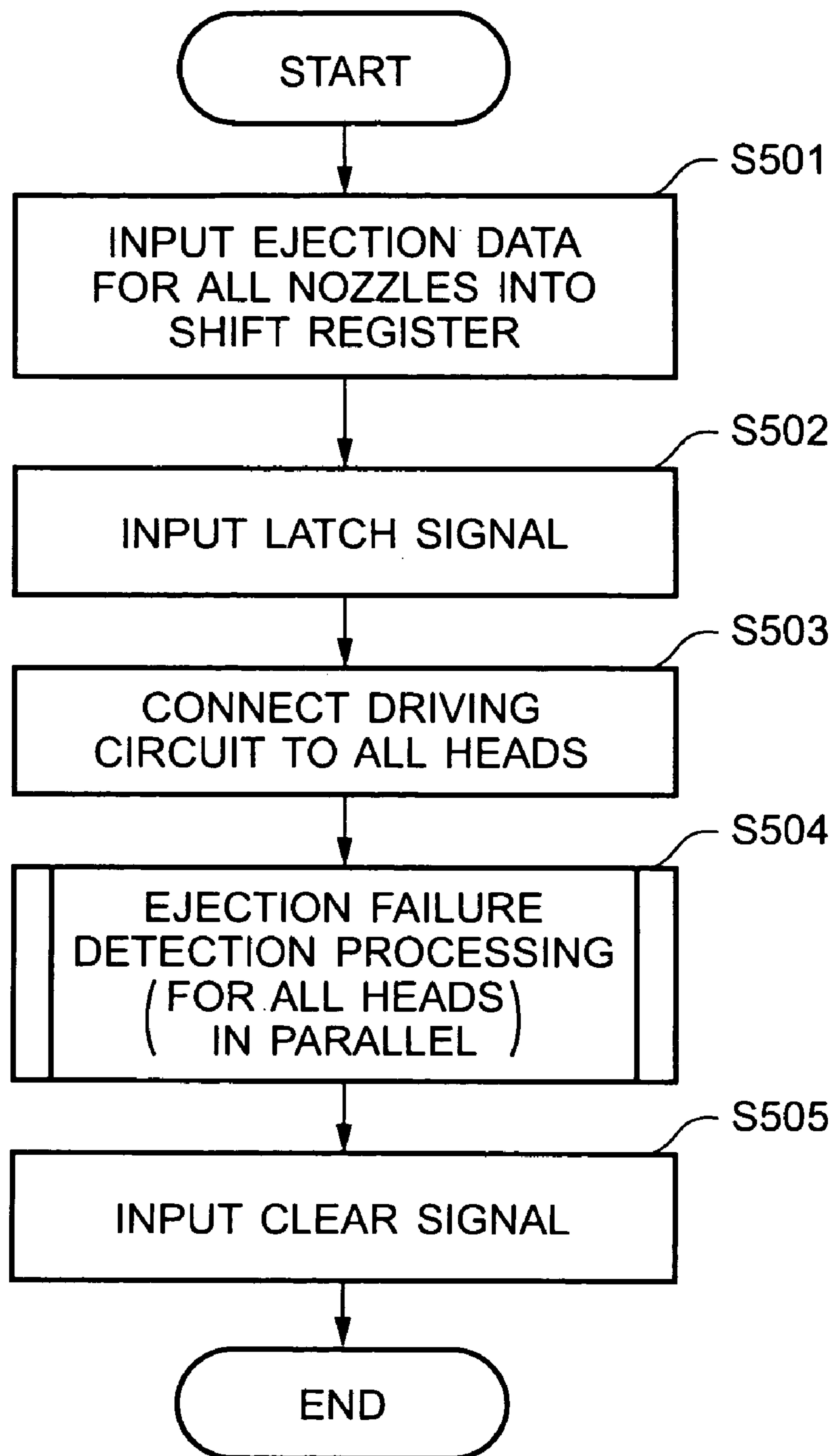


FIG.32

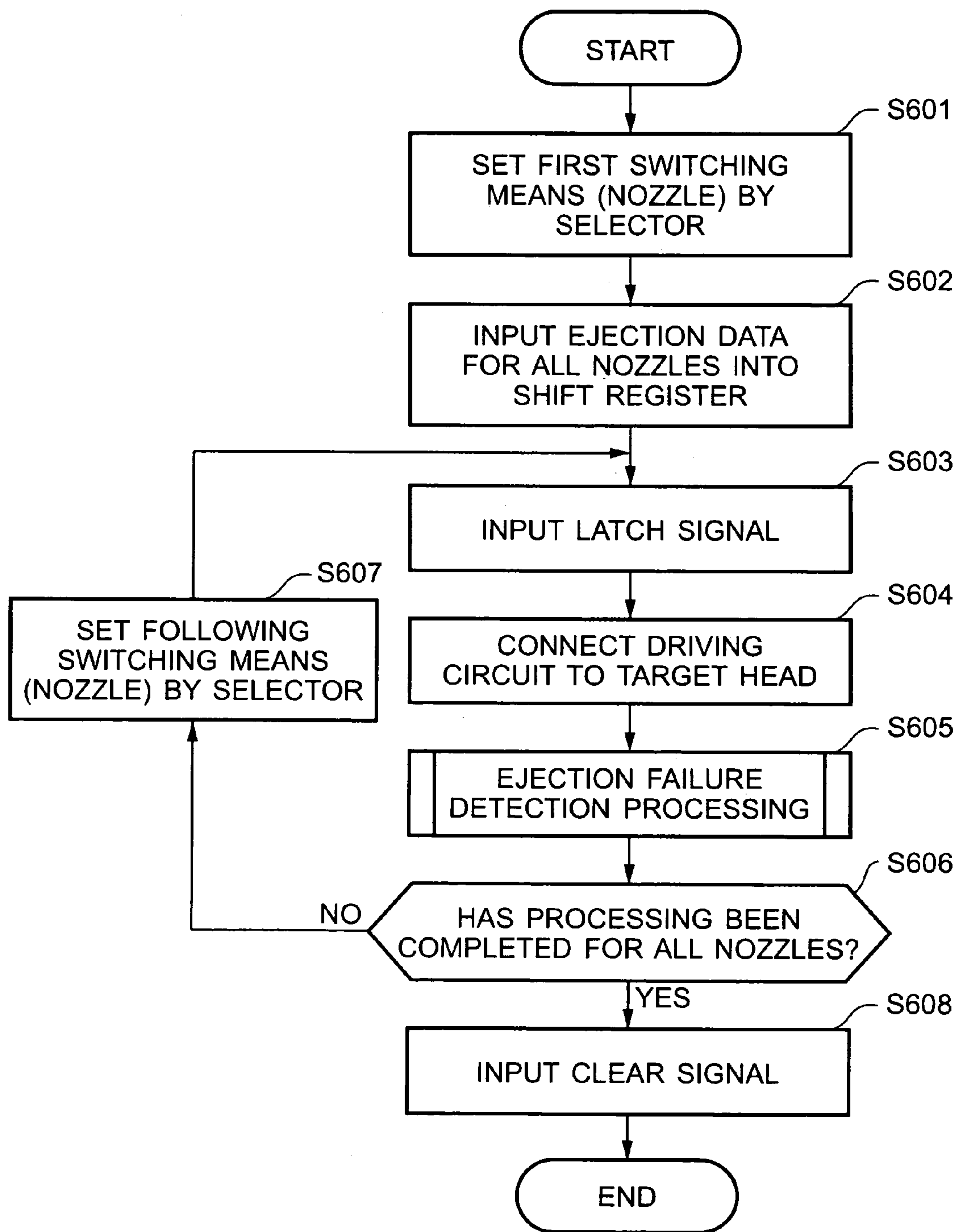


FIG.33

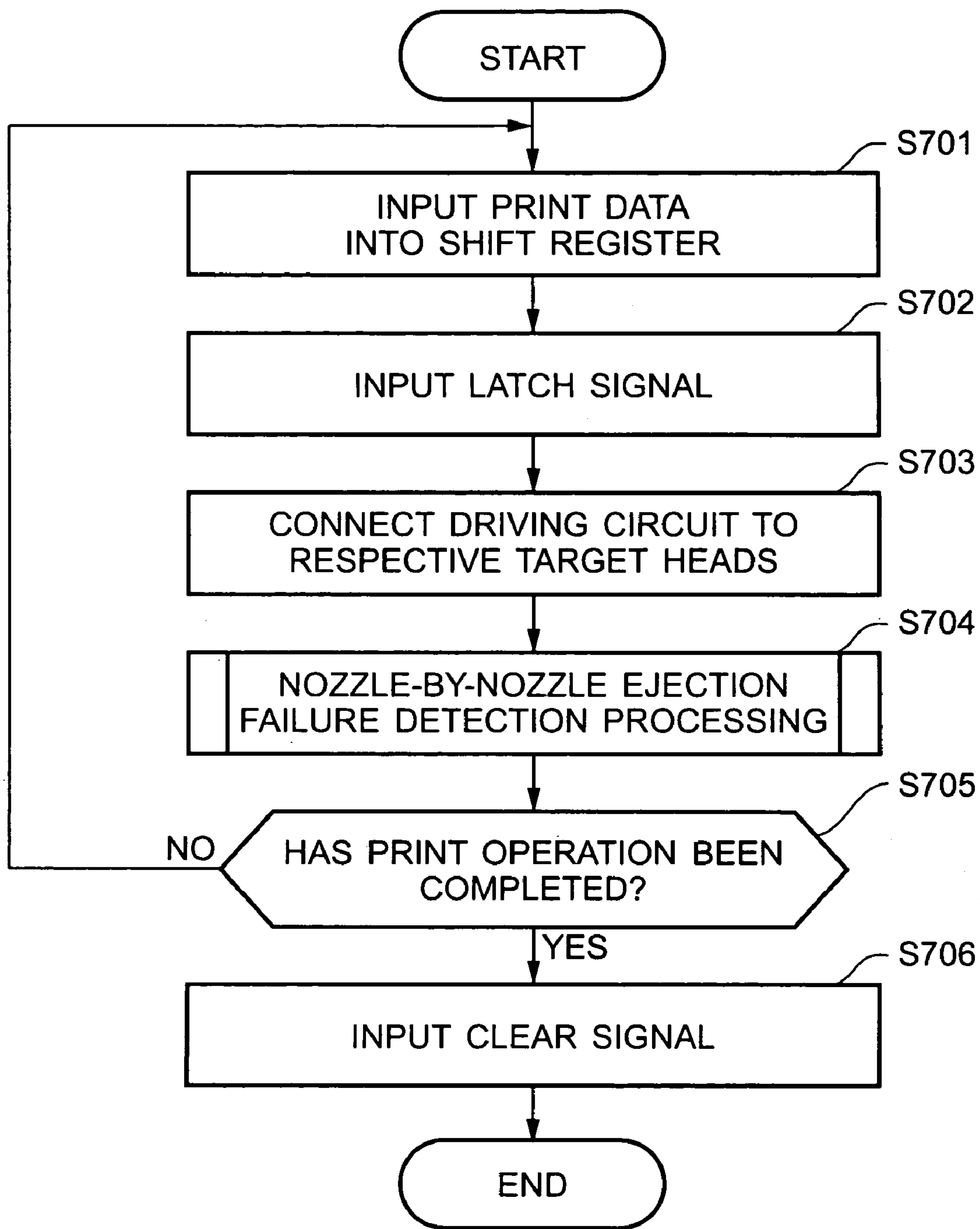


FIG.34

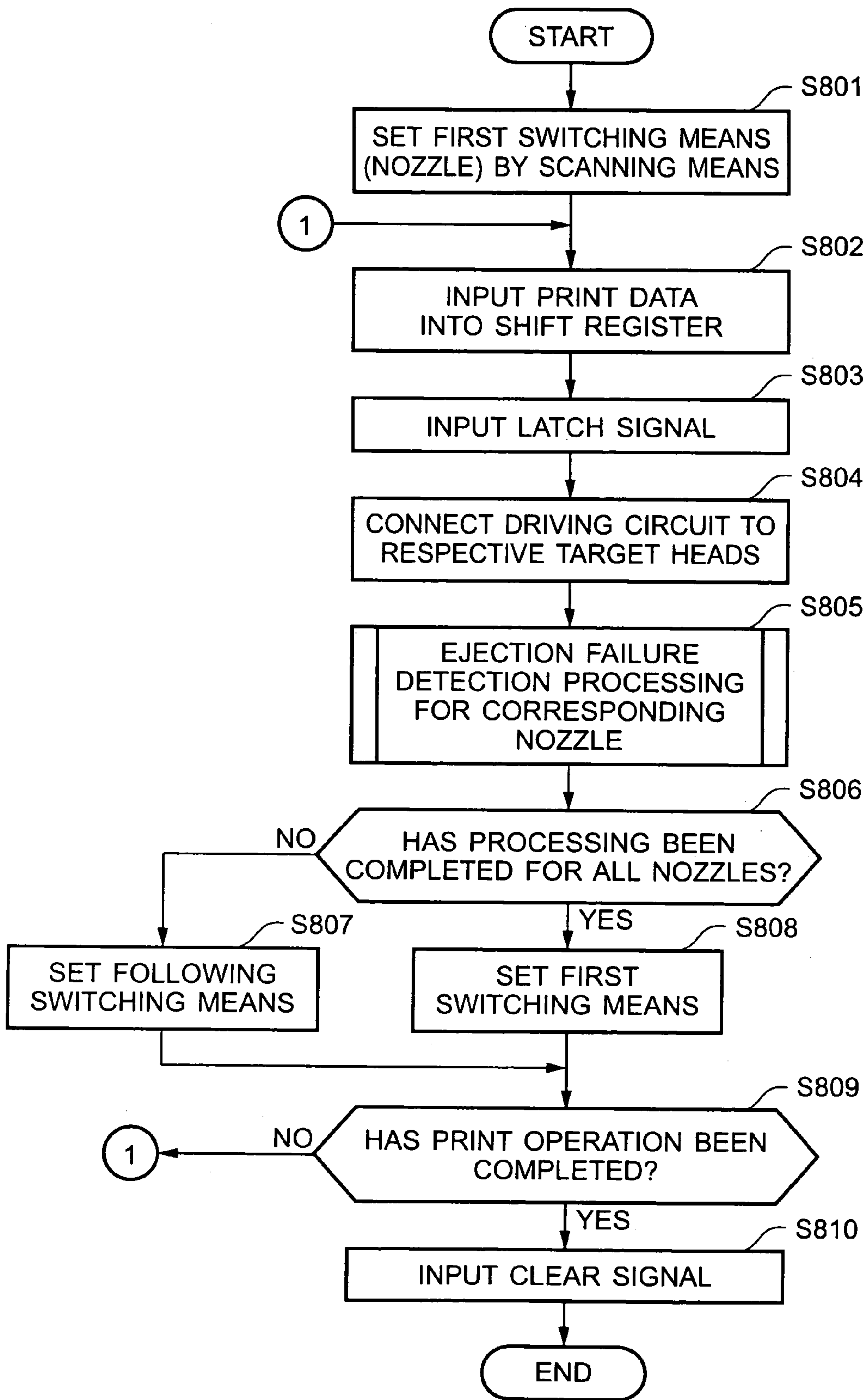


FIG.35

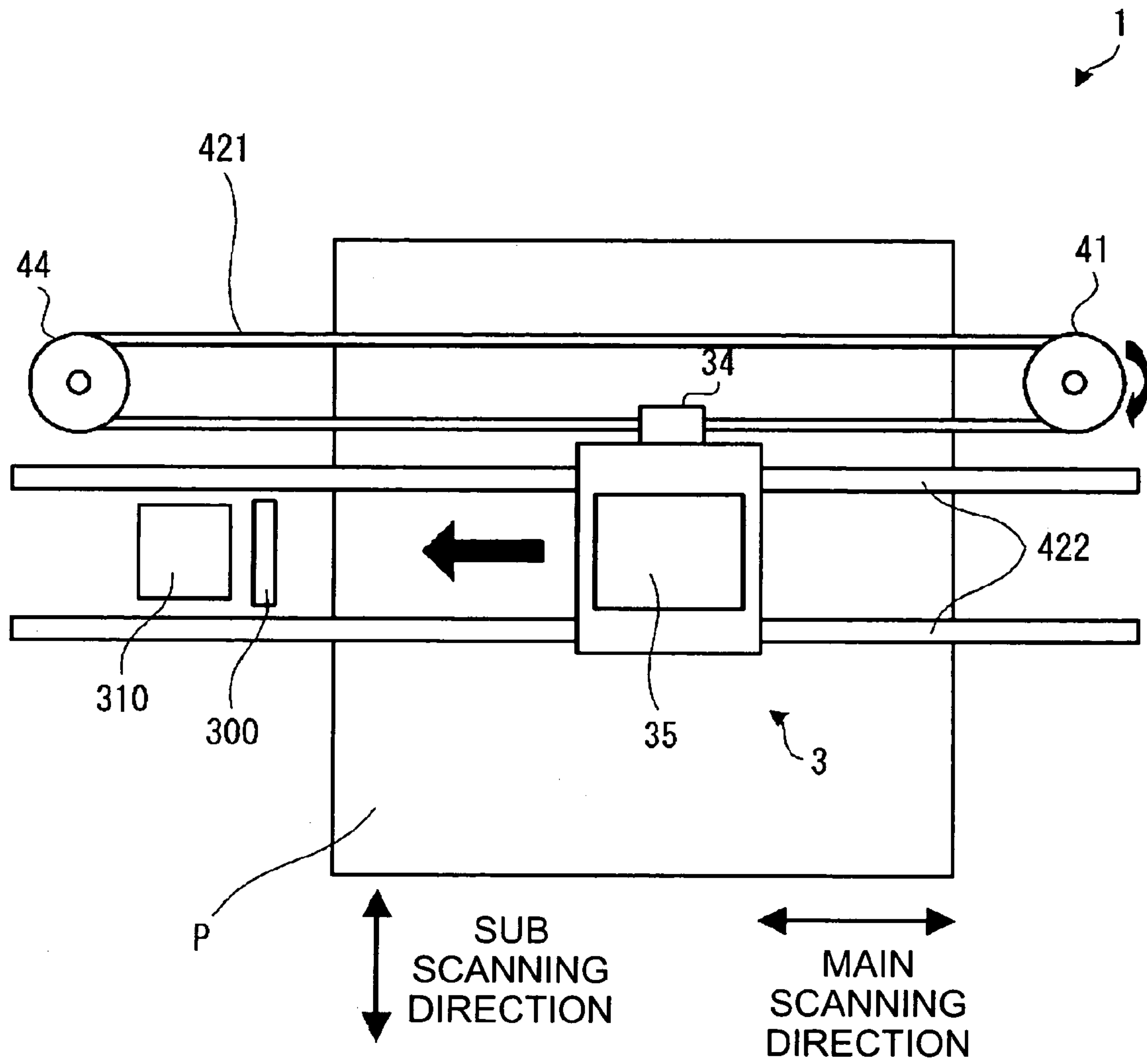


FIG.36

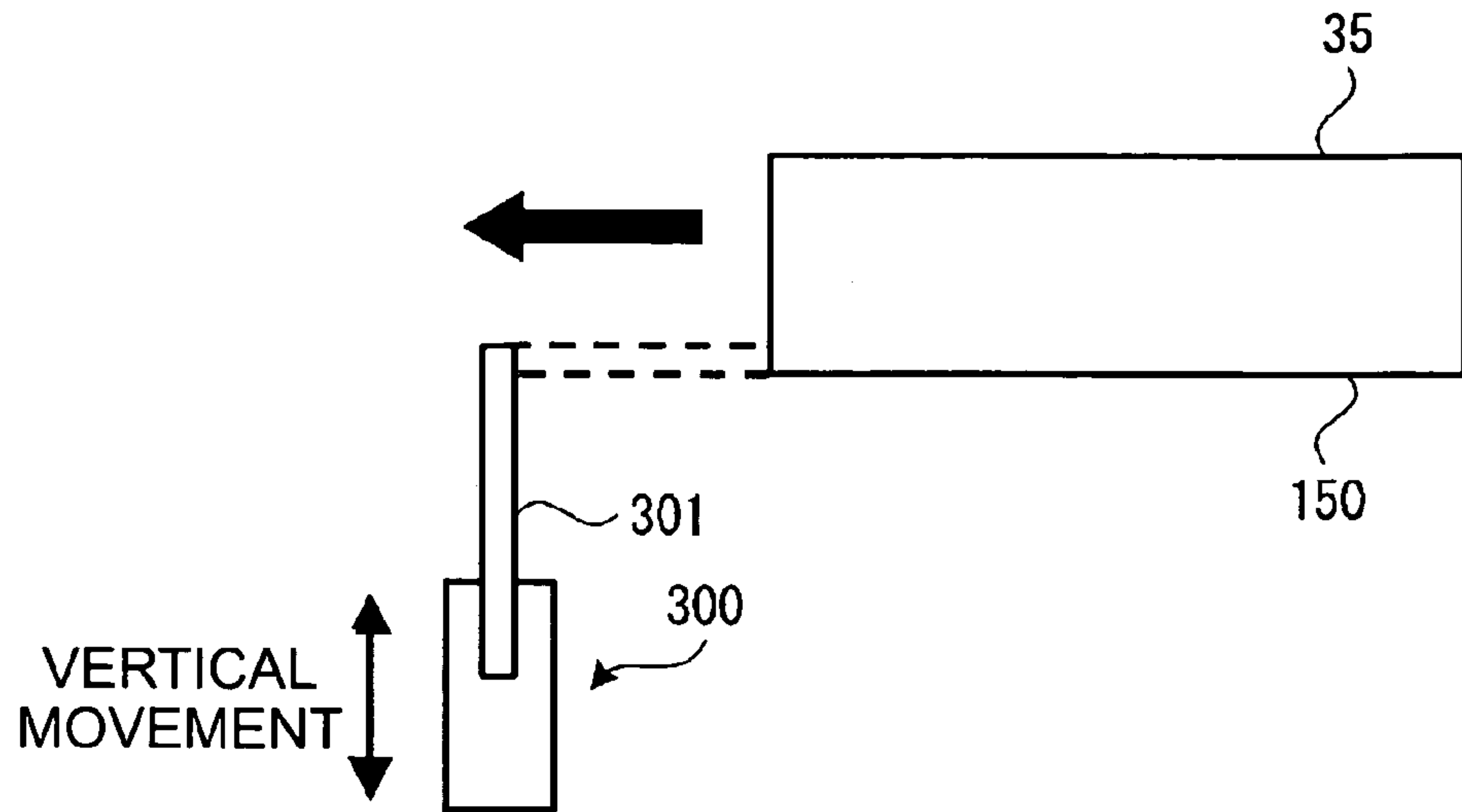


FIG. 37A

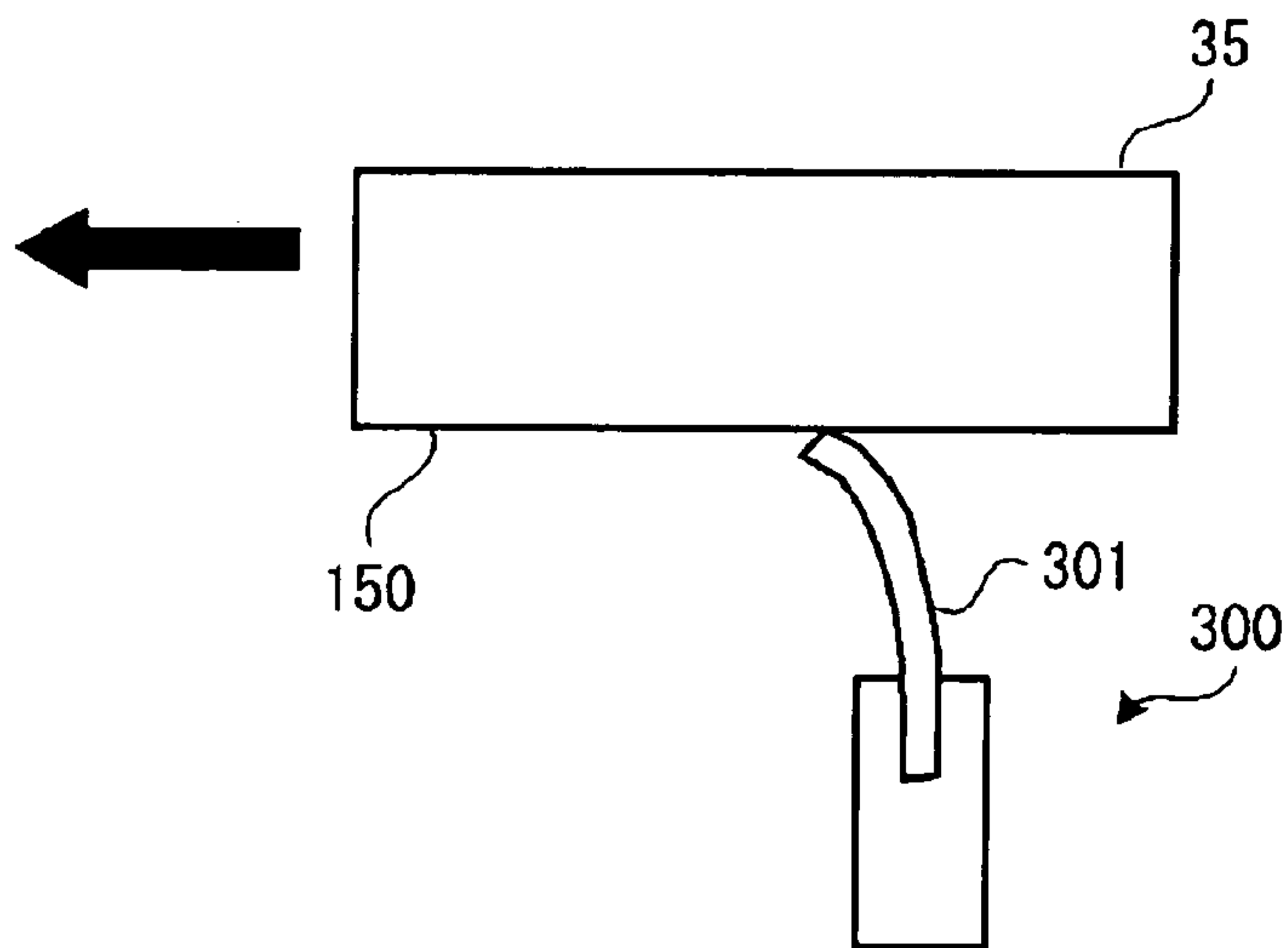


FIG. 37B

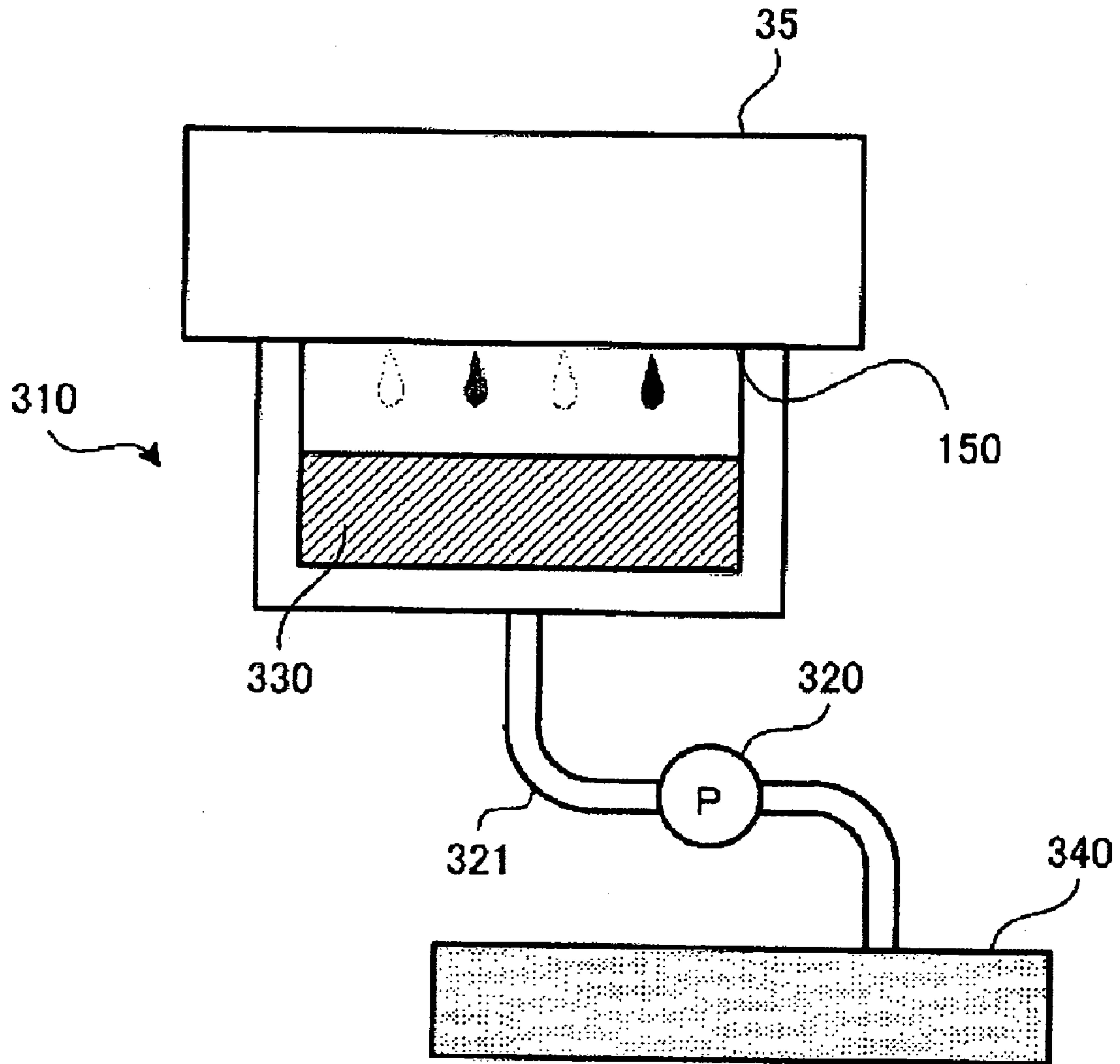


FIG.38

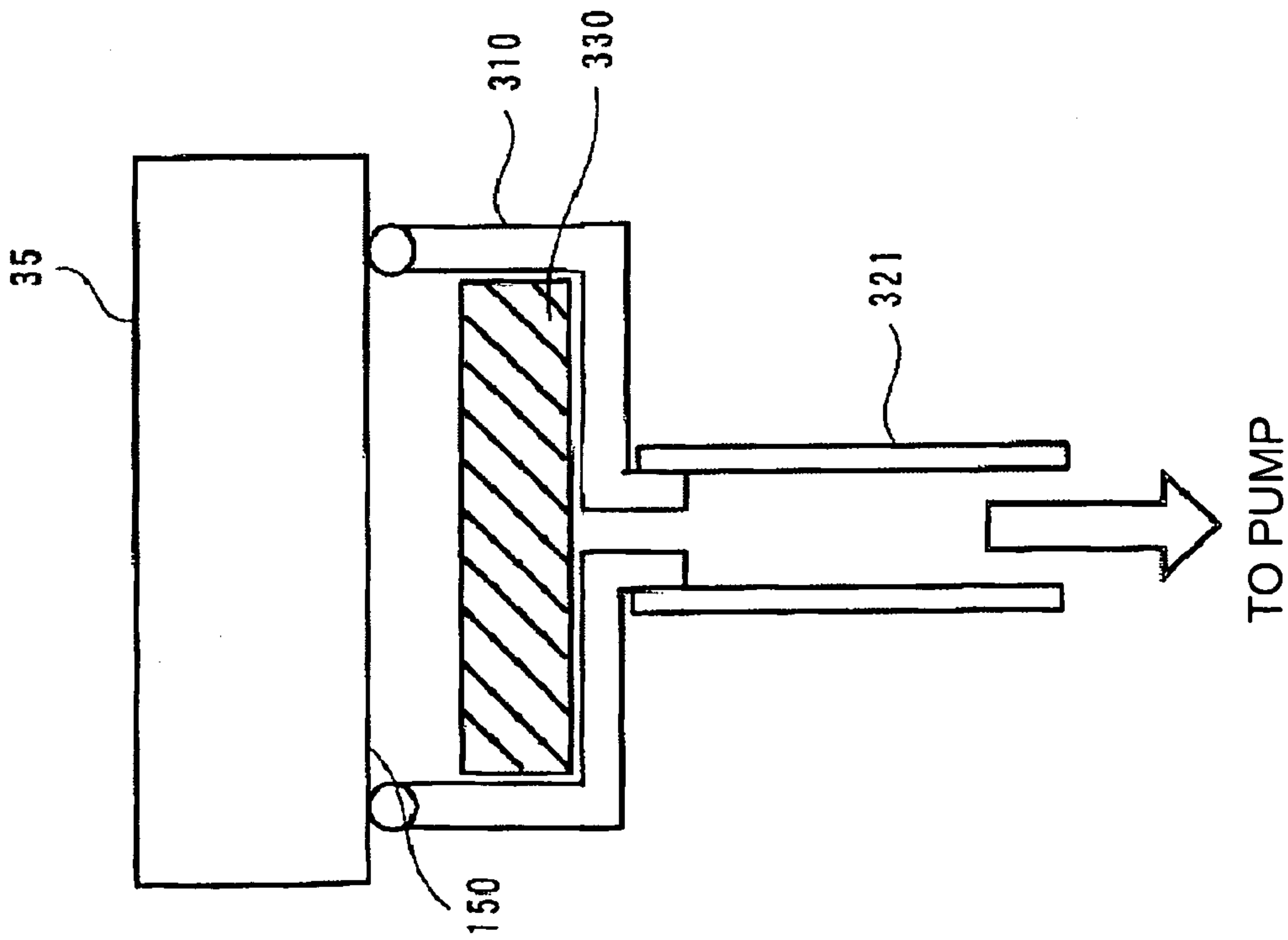


FIG. 39A

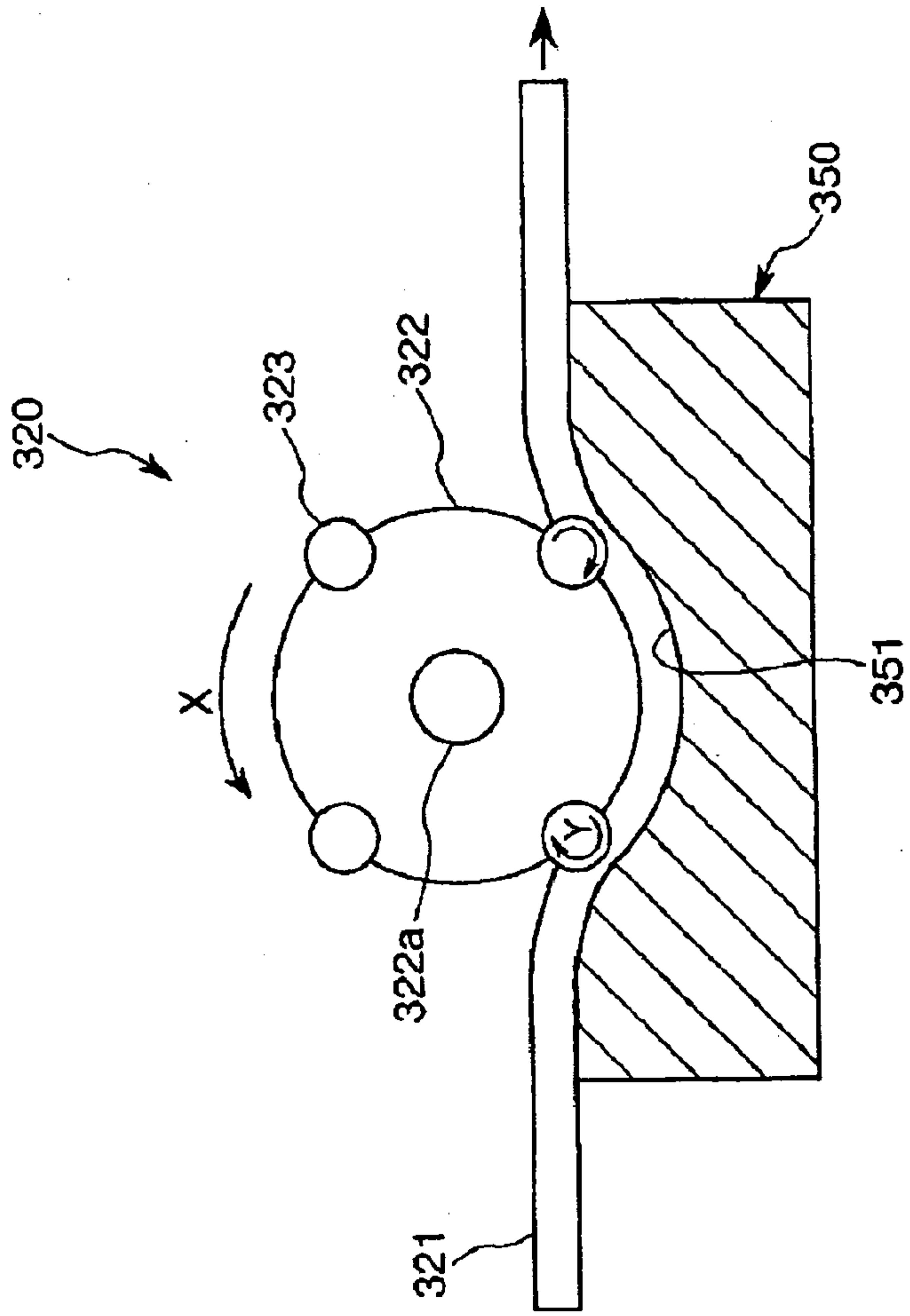


FIG. 39B

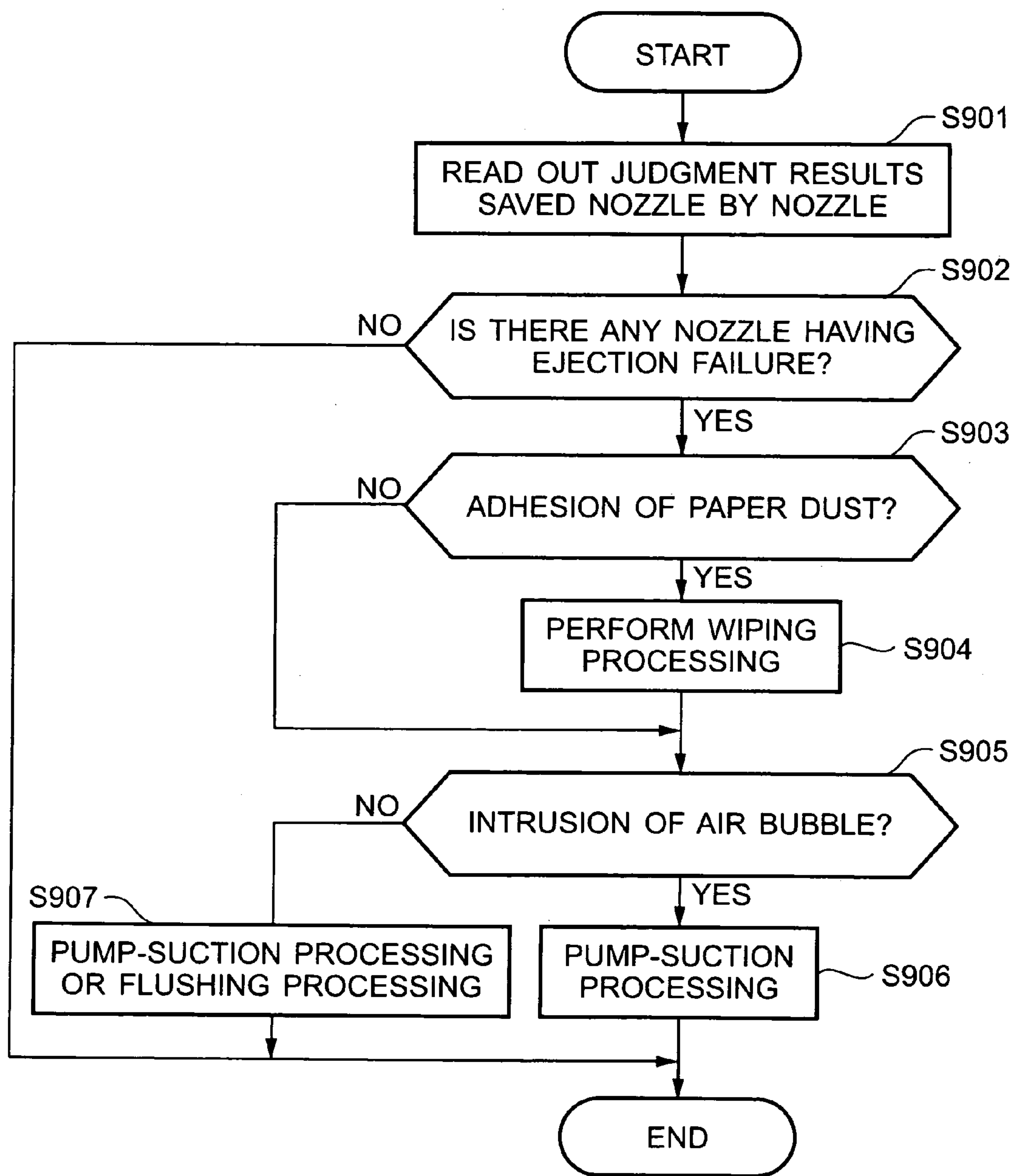


FIG.40

FIG.41A

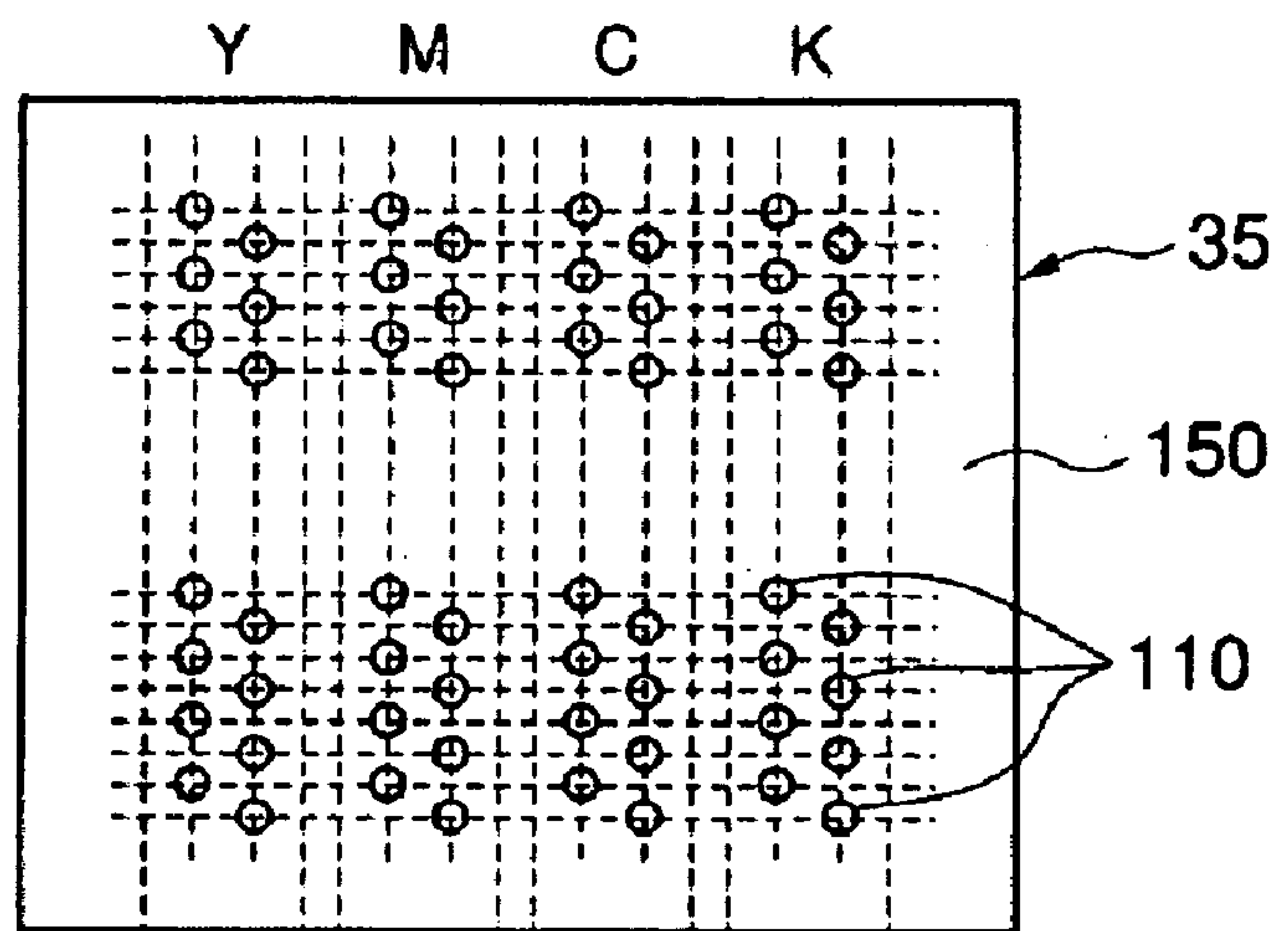
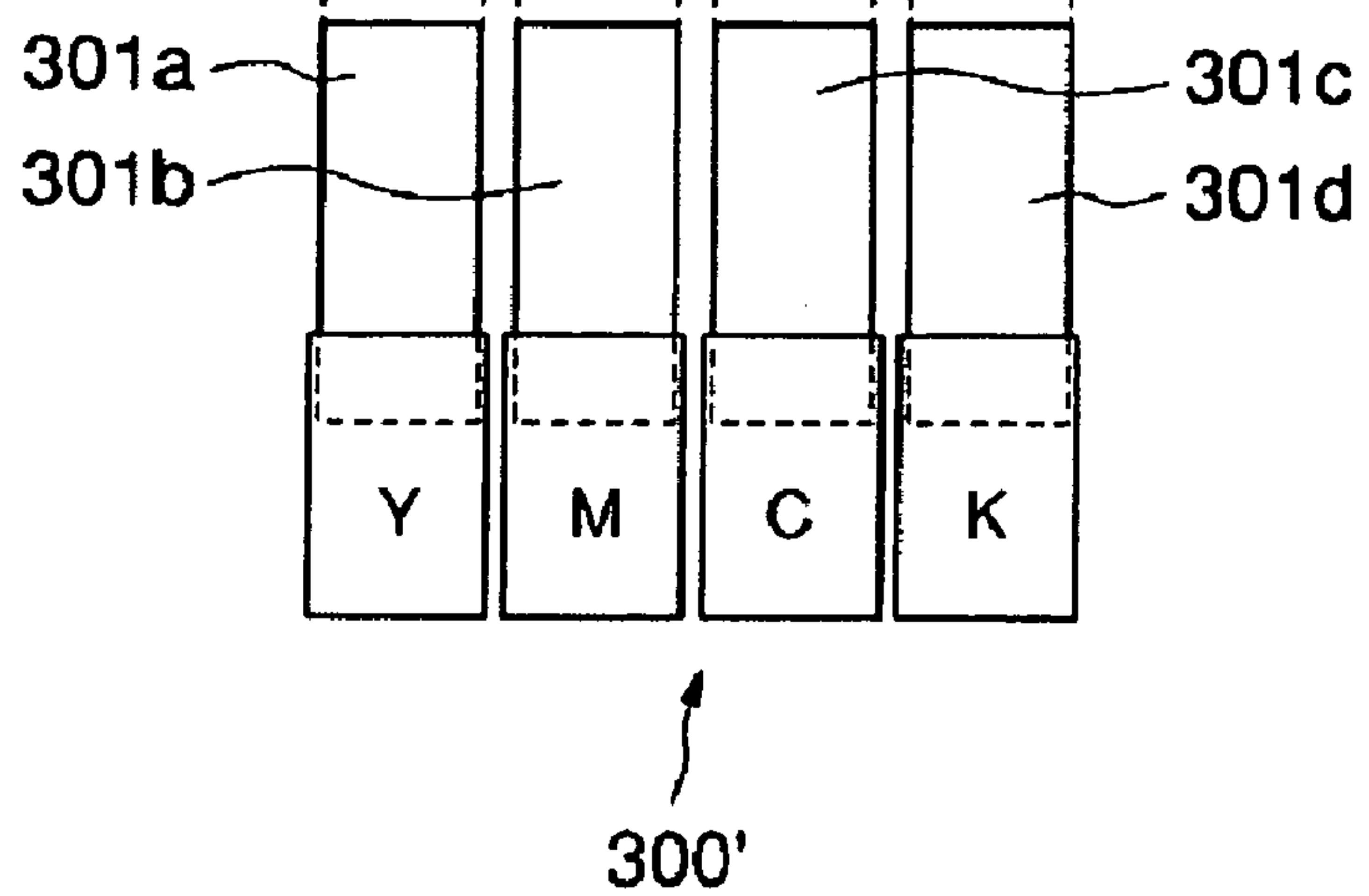


FIG.41B



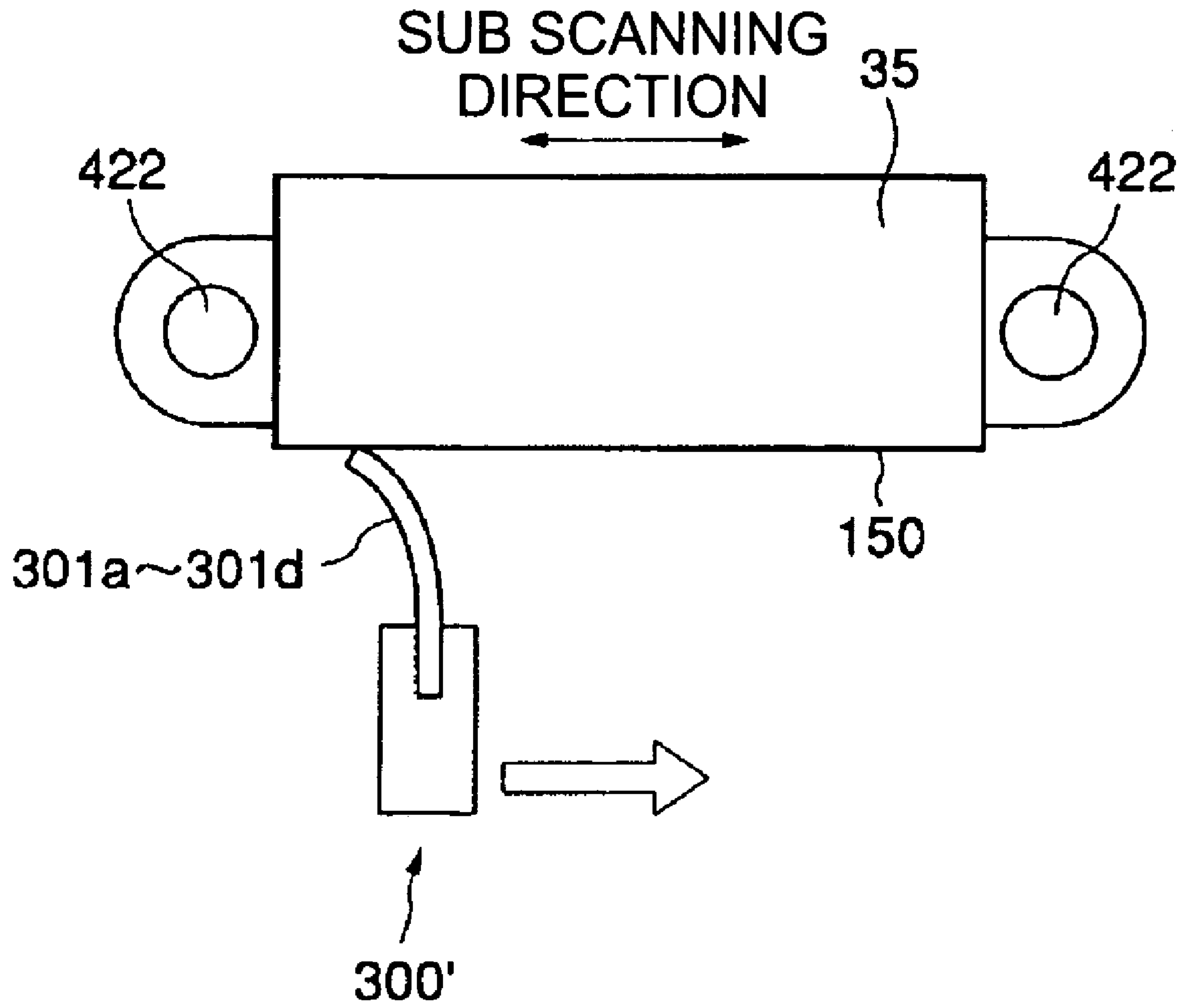


FIG.42

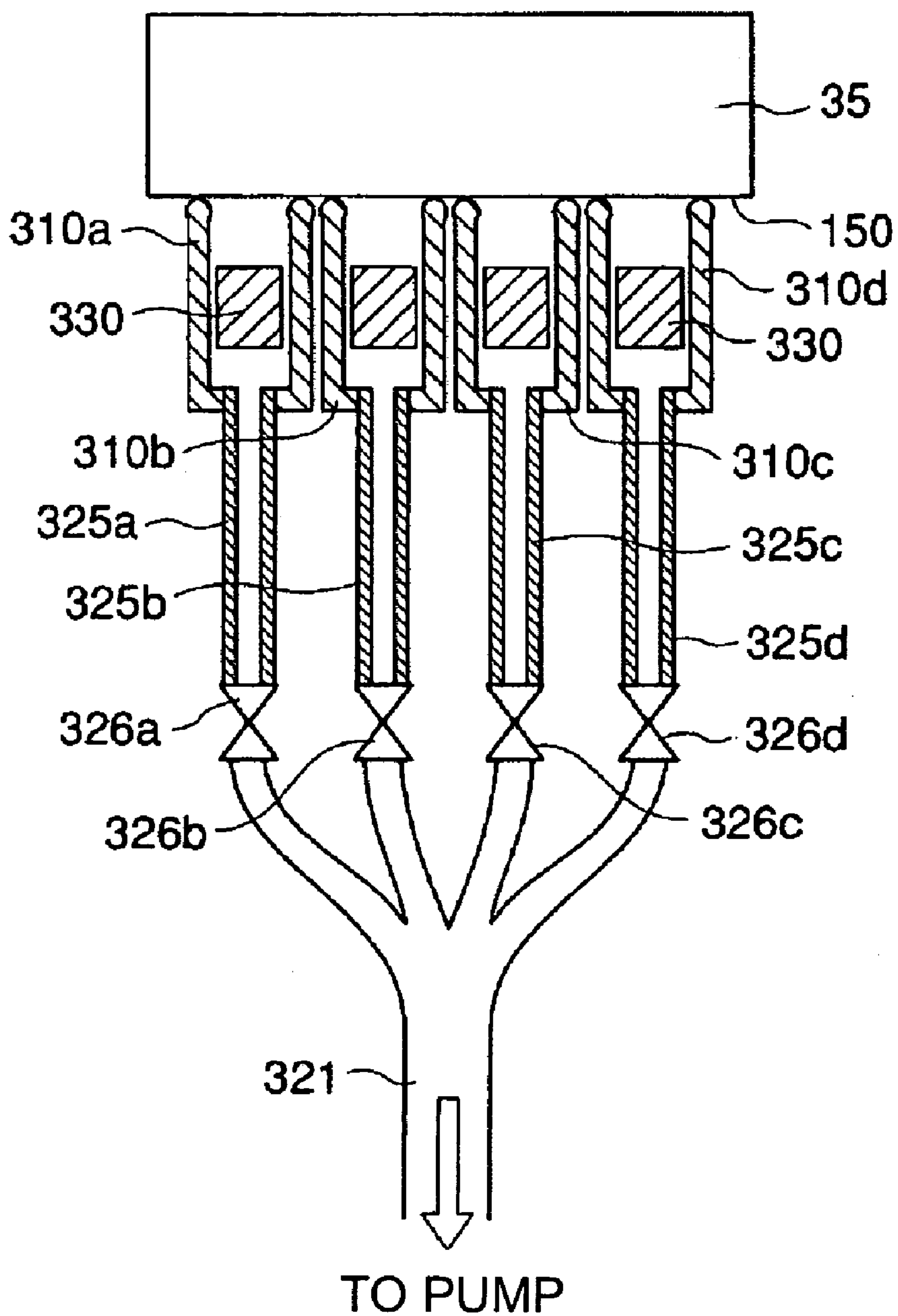


FIG.43

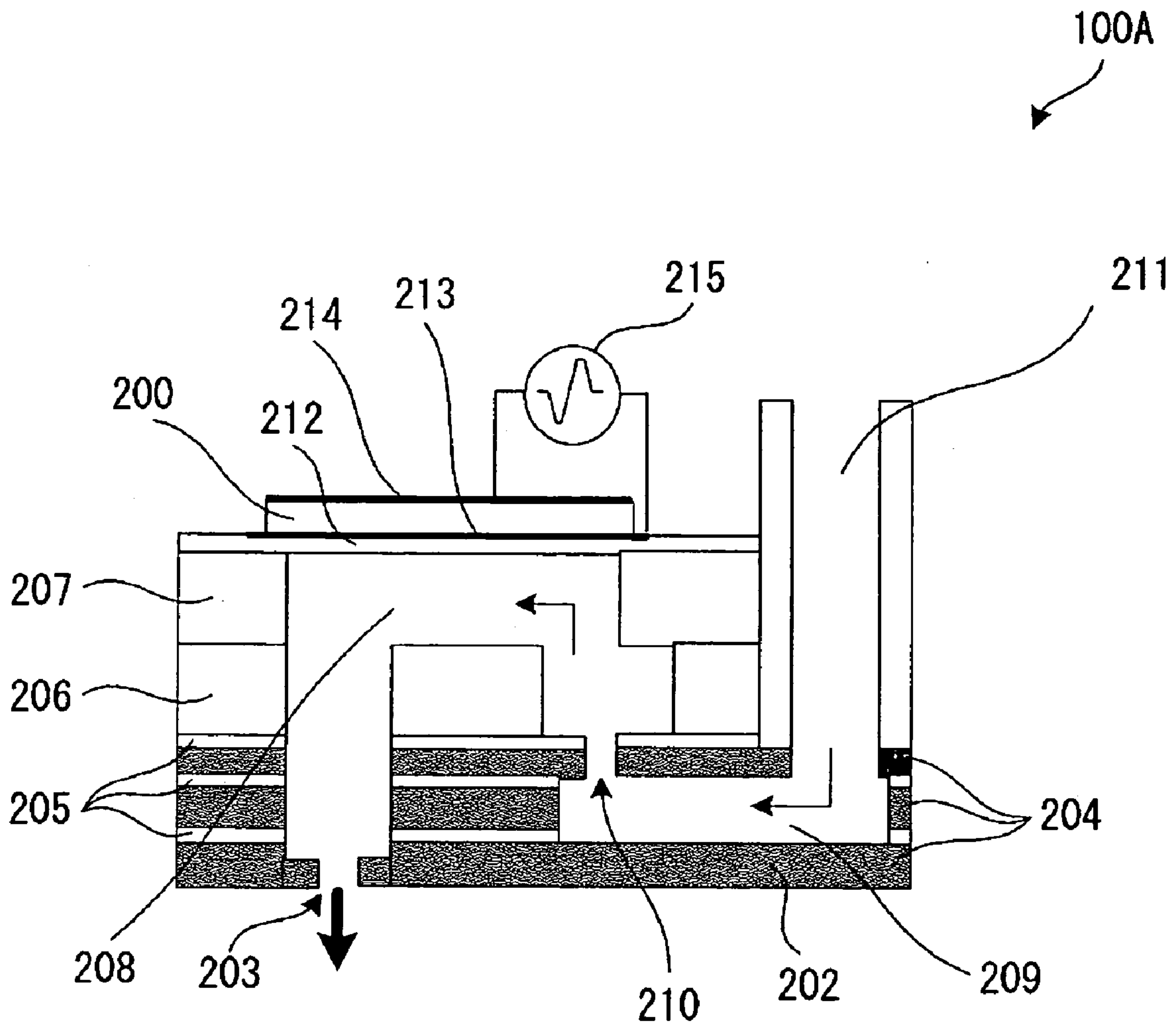


FIG.44

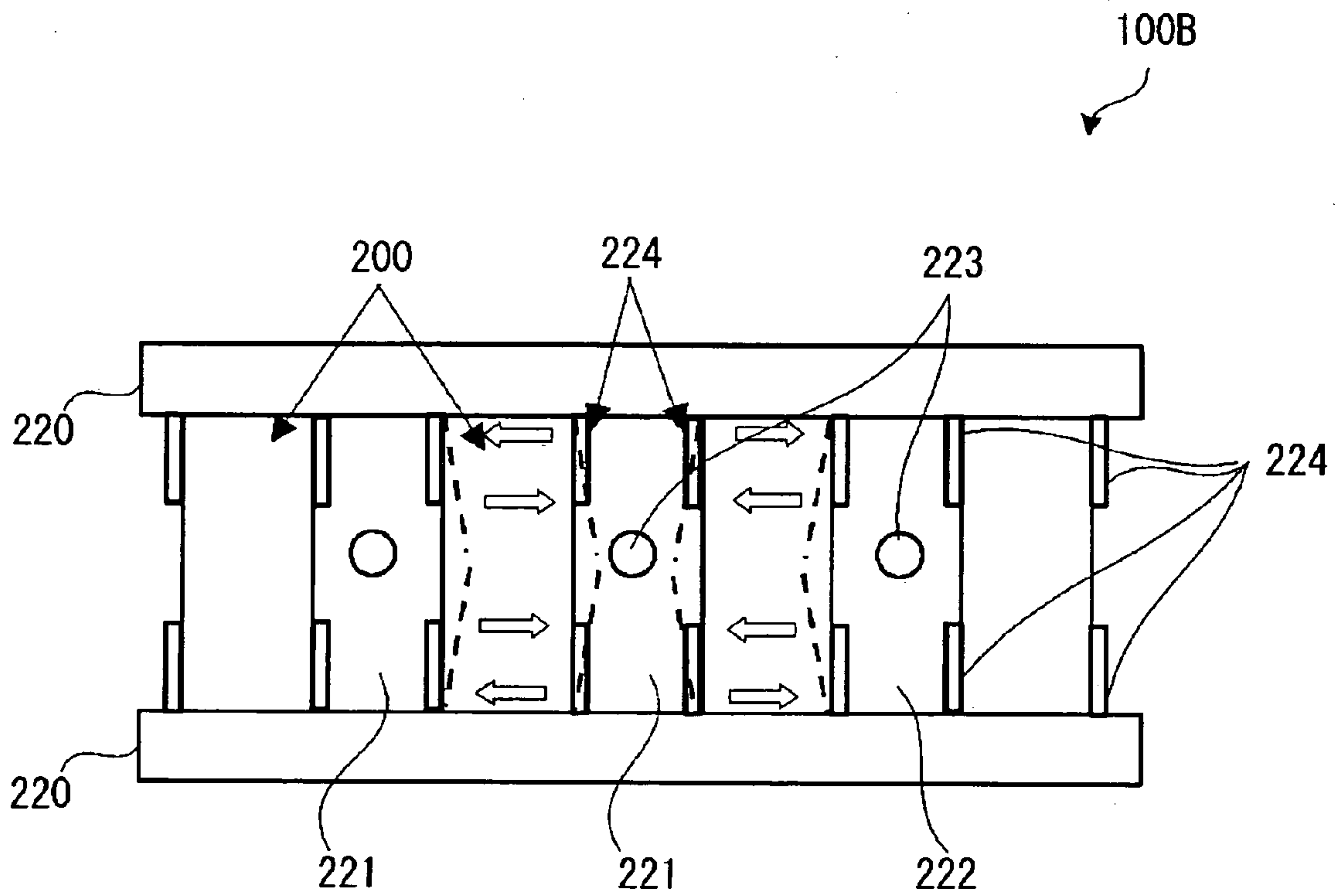


FIG.45

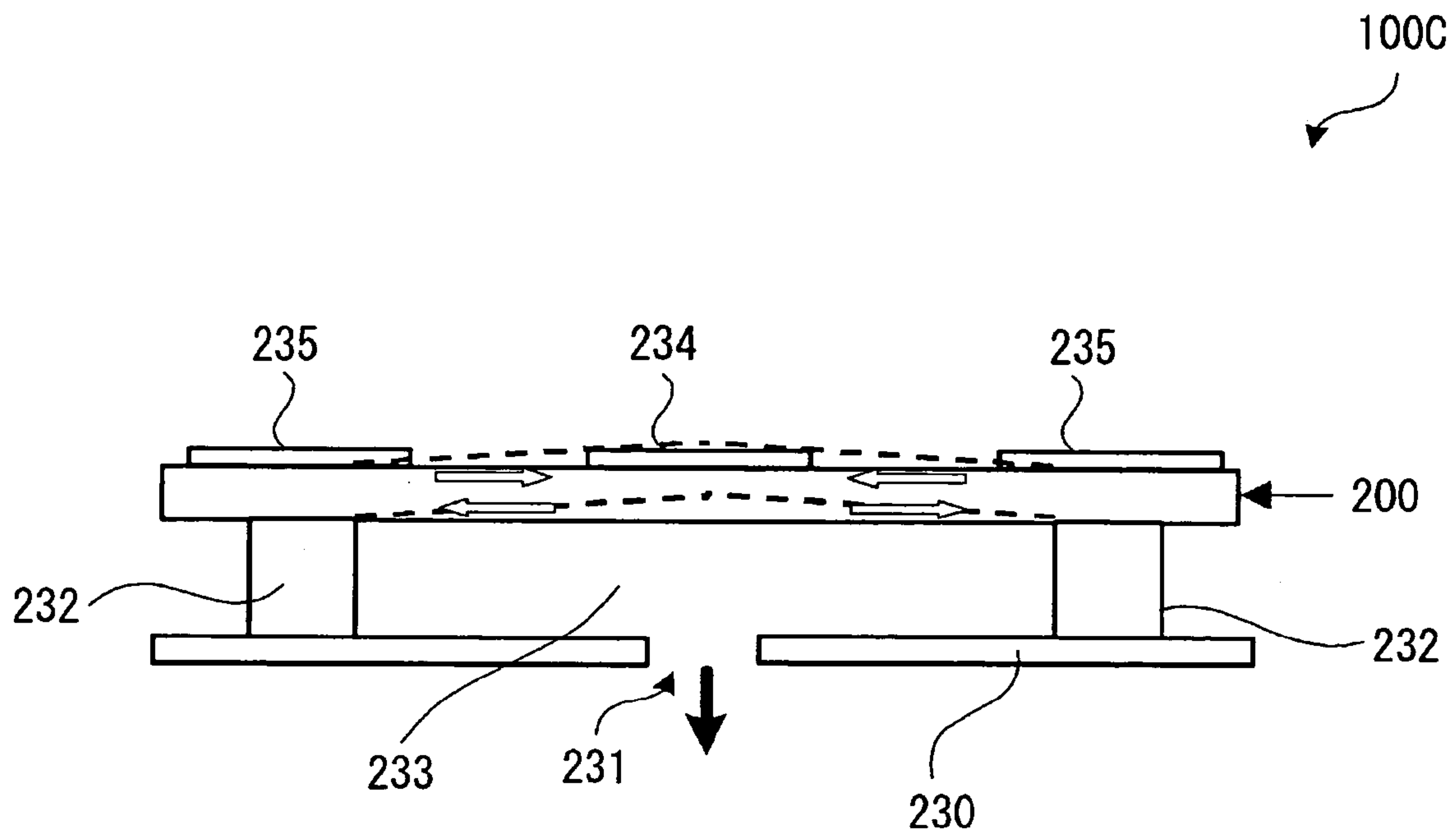


FIG.46

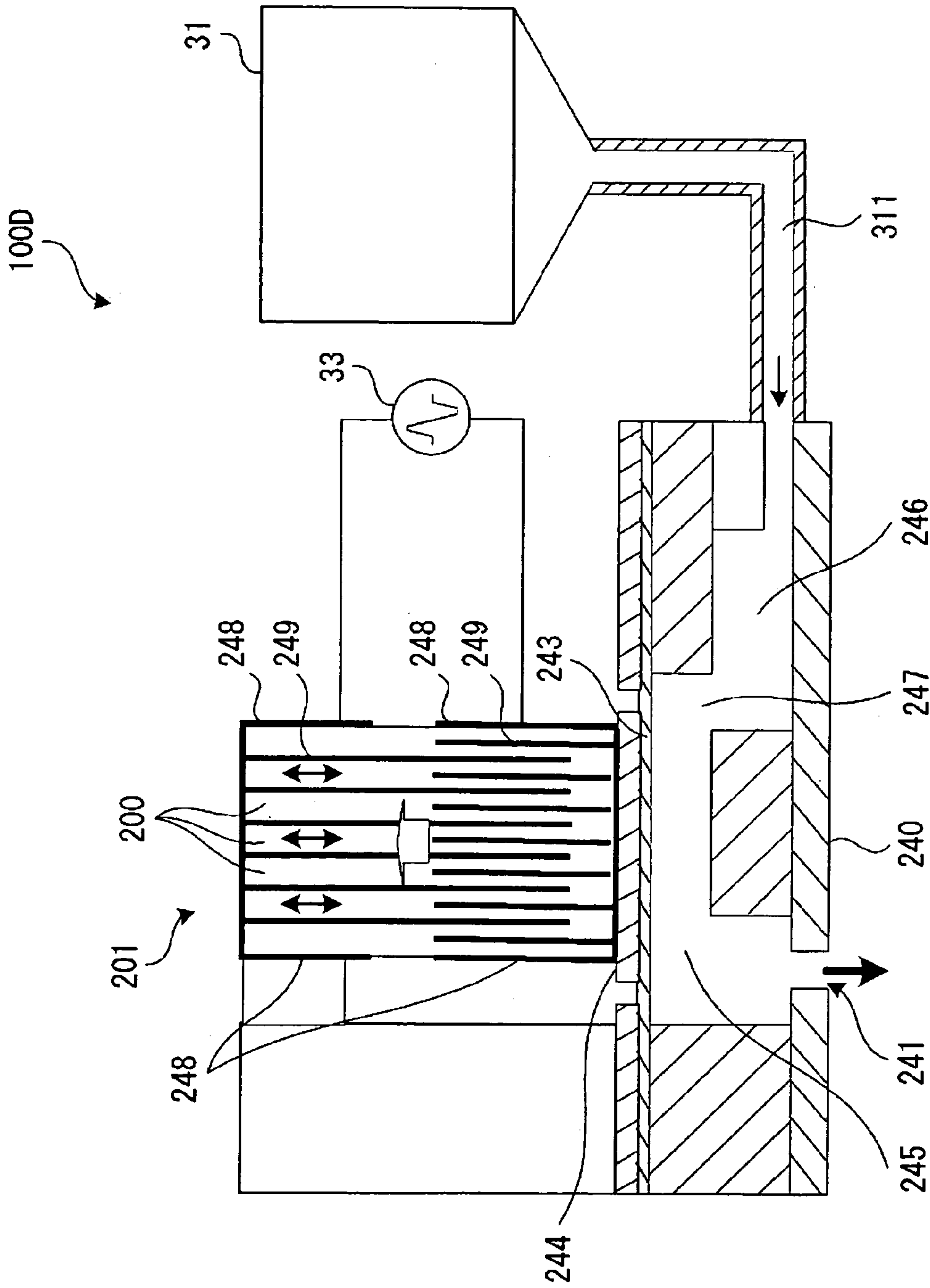


FIG.47

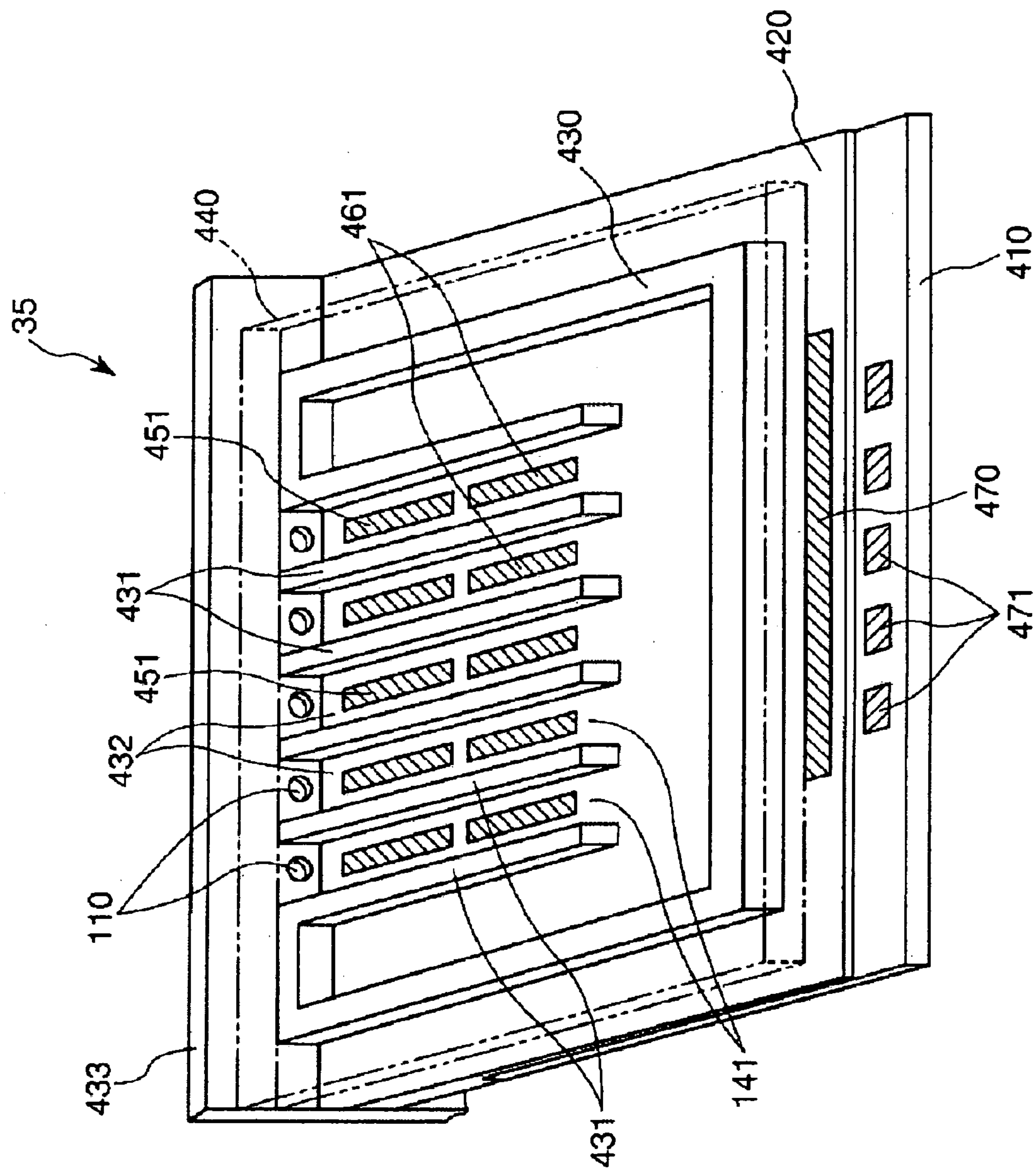


FIG. 48

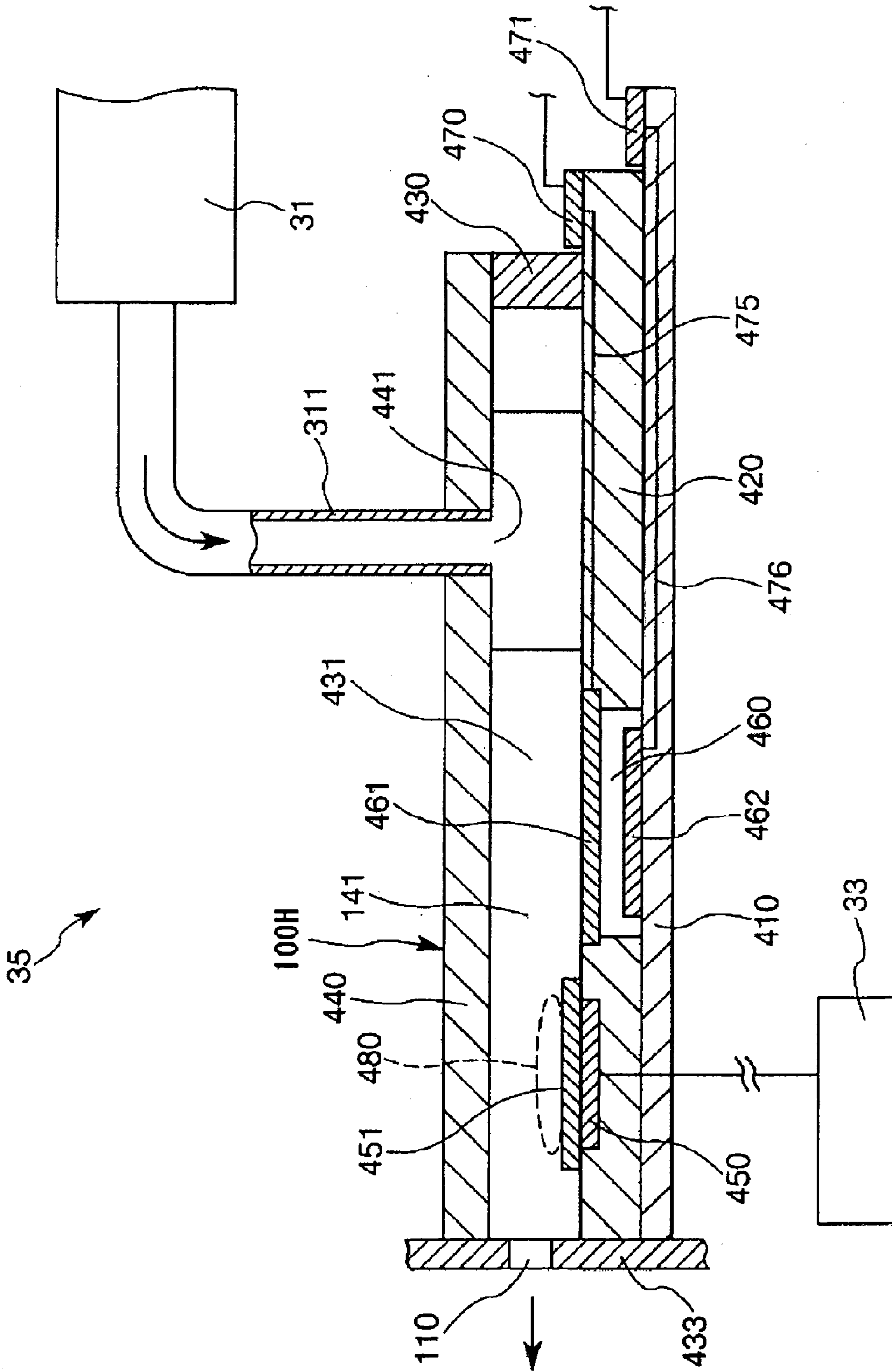


FIG. 49

DROPLET EJECTION APPARATUS AND EJECTION FAILURE RECOVERY METHOD

RELATED APPLICATIONS

This application claims priority to Japanese Patent Application Nos. 2003-055021 filed Feb. 28, 2003 and 2003-074628 filed Mar. 18, 2003 which are hereby expressly incorporated by reference herein in their entireties.

BACKGROUND

1. Technical Field

The present invention relates to a droplet ejection apparatus and an ejection failure recovery method.

2. Background Art

An ink jet printer, which is one type of a droplet ejection apparatus, forms an image on a predetermined sheet of paper by ejecting ink drops (droplets) through a plurality of nozzles. A printing head (ink jet head) of the ink jet printer is provided with a number of nozzles. However, at times, some of the nozzles are blocked due to an increase of ink viscosity, intrusion of air bubbles, adhesion of dust or paper dust, etc., and become unable to eject ink drops. When the nozzles are blocked, a missing dot occurs within a printed image, which results in deterioration of image quality.

Conventionally, as a method of detecting such an ejection failure of ink drops (hereinafter, also referred to as the missing dot), JP-A-8-309963 has disclosed a method of optically detecting when no ink drops are ejected through the nozzles of the ink jet head (ink drop ejection failing state) for each nozzle of the ink jet head. This method makes it possible to identify a nozzle causing the missing dot (ejection failure).

According to the optical missing dot (droplet ejection failure) detecting method described above, however, a detector including a light source and an optical sensor is attached to a droplet ejection apparatus (for example, an ink jet printer). Hence, this detecting method generally has a problem that the light source and the optical sensor have to be set (provided) with exact accuracy (high degree of accuracy), so that droplets ejected through the nozzles of the droplet ejection head (ink jet head) pass through a space between the light source and the optical sensor and intercept light between the light source and the optical sensor. In addition, such a detector is generally expensive, which poses another problem in that the manufacturing costs of the ink jet printer are increased. Further, the output portion of the light source or the detection portion of the optical sensor may be smeared by ink mist through the nozzles or paper dust from printing sheets or the like, and the reliability of the detector may become a matter of concern.

Also, according to the optical missing dot detecting method described above, the missing dot, that is, an ejection failure (non-ejection) of ink drops of the nozzles can be detected; however, the cause of the missing dot (ejection failure) cannot be identified (judged) on the basis of the detection result. Hence, there is still another problem in that it is impossible to select and perform adequate recovery processing depending on the cause of the missing dot. For this reason, sequential recovery processing is performed independently of the cause of the missing dot in the conventional missing dot detecting method. For example, ink may be pump-sucked (vacuumed) from the ink jet head under circumstances where a wiping process is sufficient for recovery. This increases discharged ink (wasted ink), or causes recovery processing of several types to be performed

because adequate recovery processing is not performed, and thereby reduces or deteriorates throughput of the ink jet printer (droplet ejection apparatus).

Incidentally, the droplet ejection apparatus (ink jet head) generally includes a plurality of nozzles and actuators corresponding to the respective nozzles, and it is difficult for such a droplet ejection apparatus having a plurality of nozzles to detect an ejection failure (non-ejection) of droplets (ink drops), that is, the missing dot during a printing (recording) operation, without reducing or deteriorating the throughput of the apparatus.

SUMMARY

One object of the invention is to provide a droplet ejection apparatus and an ejection failure recovery method, by which, in the presence of an ejection failure of a droplet ejection head, the cause of the ejection failure is identified, so that adequate recovery processing can be performed depending on the cause of the ejection failure instead of conventional sequential recovery processing.

In order to achieve the above object, a first aspect of the invention provides a droplet ejection apparatus having a head unit including a plurality of droplet ejection heads each ejecting liquid within a cavity through a nozzle in the form of droplets by driving an actuator with a driving circuit, and the droplet ejection apparatus of the invention is characterized by including:

ejection failure detecting means for detecting an ejection failure of the droplet ejection heads and a cause thereof; and recovery means for performing recovery processing depending on the cause of the ejection failure if the ejection failure detecting means detects the ejection failure when the droplets are ejected through the nozzles.

According to the droplet ejection apparatus of the invention, an ejection failure of the droplet ejection heads and the cause thereof are detected, and adequate recovery processing is performed depending on the detected cause. Hence, in contrast to the sequential recovery processing by the conventional droplet ejection apparatus, it is possible to prevent a reduction or deterioration of the throughput of the droplet ejection apparatus by reducing wastefully discharged ink during the recovery process.

It is preferable that the recovery means includes: wiping means for performing, with the use of a wiper, a wiping process on the nozzle surfaces of the droplet ejection heads where the nozzles are aligned; flushing means for performing a flushing process by which the droplets are preliminarily ejected through the nozzles by driving the actuators; and pumping means for performing a pump-suction process with the use of a pump connected to a cap covering the nozzle surfaces of the droplet ejection heads.

Also, it is preferable that the cause of an ejection failure detectable by the ejection failure detecting means includes intrusion of an air bubble inside the cavity, thickening of the liquid caused by drying in a vicinity of the nozzle, and adhesion of dust, e.g., paper dust, in a vicinity of an outlet of the nozzle; and

the recovery means performs the pump-suction process by the pumping means in the case of the intrusion of an air bubble, the flushing process by the flushing means or the pump-suction process by the pumping means in the case of thickening caused by drying, and at least the wiping process by the wiper in the case of the adhesion of paper dust. In the invention, "paper dust" is not limited to mere paper dust generated from a recording sheet or the like, but includes all substances that could adhere in the vicinity of the nozzles

and impede ejection of droplets, such as pieces of rubber from the advancing roller (feeding roller) and dust afloat in air. In this case, it is preferable that, when the ejection failure detecting means detects the intrusion of an air bubble and the thickening caused by drying that need the pump-suction process for more than one droplet ejection head of the head unit, the recovery means performs the pump-suction process at a time for the droplet ejection heads with which the intrusion of an air bubble and the thickening caused by drying are detected.

The droplet ejection apparatus of the invention may be configured in such a manner that:

each of the droplet ejection heads includes a diaphragm that is displaced when the actuator is driven; and

the ejection failure detecting means detects residual vibration of the diaphragm and detects an ejection failure of the droplets on the basis of a vibration pattern of the detected residual vibration of the diaphragm. In this case, it is preferable that the ejection failure detecting means includes judging means for judging the presence or absence of an ejection failure of the droplets in the droplet ejection head on the basis of the vibration pattern of the residual vibration of the diaphragm, and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in the droplet ejection head. The residual vibration of the diaphragm referred to herein means a state that the diaphragm keeps vibrating while damping by the droplet ejection operation after the actuator performed the droplet ejection operation according to a driving signal (voltage signal) from the driving circuit until the actuator performs the droplet ejection operation again upon input of the following driving signal.

Also, the vibration pattern of the residual vibration of the diaphragm may preferably include a cycle of the residual vibration. In this case, it is preferable that the judging means judges that an air bubble has intruded inside the cavity when the cycle of the residual vibration of the diaphragm is shorter than a cycle of a predetermined range, the liquid has thickened by drying in the vicinity of the nozzle when the cycle of the residual vibration of the diaphragm is longer than a predetermined threshold, and paper dust is adhering in the vicinity of the outlet of the nozzle when the cycle of the residual vibration of the diaphragm is longer than the cycle of the predetermined range and shorter than the predetermined threshold. It is thus possible to judge the cause of an ejection failure of droplets, which cannot be judged by the conventional droplet ejection apparatus capable of performing missing dot detection, such as an optical detection device. This enables adequate recovery processing depending on the cause of an ejection failure as described above to be selected and performed as needed.

According to one embodiment of the invention, the apparatus may be configured in such a manner that the ejection failure detecting means includes an oscillation circuit, and the oscillation circuit oscillates on the basis of an electric capacitance component of the actuator that varies with the residual vibration of the diaphragm. In this case, it is preferable that the oscillation circuit forms a CR oscillation circuit from the electric capacitance component of the actuator and a resistance component of a resistor element connected to the actuator. Because the droplet ejection apparatus of the invention detects the residual vibration waveform (voltage waveform of the residual vibration) of the diaphragm as a minute change (change of the oscillation cycle) with time of the electric capacitance component of the actuator, the residual vibration waveform of the diaphragm

can be detected with accuracy independently of the magnitude of an electromotive voltage when a piezoelectric element is used as the actuator.

It is preferable that the oscillation frequency of the oscillation circuit is about one or more orders of magnitude higher than the vibration frequency of the residual vibration of the diaphragm. By setting the oscillation frequency of the oscillation circuit several tens times higher than the vibration frequency of the residual vibration of the diaphragm in this manner, the residual vibration of the diaphragm can be detected accurately, which in turn enables an ejection failure of the droplets to be detected accurately.

Also, it is preferable that the ejection failure detecting means includes an F/V converting circuit that generates a voltage waveform of the residual vibration of the diaphragm from a predetermined signal group generated on the basis of a change of an oscillation frequency in an output signal from the oscillation circuit. By generating the voltage waveform with the use of the F/V converting circuit in this manner, the detection sensitivity can be set to a larger magnitude when the residual vibration waveform is detected, without affecting the driving of the actuator. In addition, the ejection failure detecting means may preferably include a waveform shaping circuit that shapes the voltage waveform of the residual vibration of the diaphragm generated in the F/V converting circuit into a predetermined waveform.

Herein, it is preferable to configure the apparatus in such a manner so that the waveform shaping circuit includes: DC component removing means for removing a direct current component from the voltage waveform of the residual vibration of the diaphragm generated in the F/V converting circuit; and a comparator that compares the voltage waveform, from which the direct current component has been removed by the DC component removing means, with a predetermined voltage value, so that the comparator generates and outputs a rectangular wave on the basis of the voltage comparison. In this case, it is more preferable that the ejection failure detecting means includes measuring means for measuring a cycle of the residual vibration of the diaphragm from the rectangular wave generated in the waveform shaping circuit. It is further preferable that the measuring means has a counter, so that it measures a time between rising edges or between a rising edge and a falling edge of the rectangular wave by counting pulses of a reference signal with the counter, allowing measurement of a cycle of the residual vibration. By measuring the cycle of the rectangular wave with the use of the counter in this manner, it is possible to detect the cycle of the residual vibration of the diaphragm accurately in a simple manner.

Also, it is preferable that the droplet ejection apparatus of the invention further includes switching means for switching a connection of the actuator from the driving circuit to the ejection failure detecting means after an ejection operation of the droplets is performed by driving the actuator. It is preferable to configure the droplet ejection apparatus of the invention to include more than one ejection failure detecting means and more than one switching means, so that switching means corresponding to a droplet ejection head that has performed the droplet ejection operation switches the connection of the actuator from the driving circuit to corresponding ejection failure detecting means, and the switched ejection failure detecting means detects an ejection failure of the droplets. Instead of the foregoing configuration, the switching means may preferably include more than one unit switching means corresponding to the droplet ejection heads, respectively. Also, in the droplet ejection apparatus of the invention, the ejection failure detecting means may

5

further include detection determining means for determining for which nozzle among the nozzles detection of an ejection failure of the droplets is to be performed. In this case, the switching means may switch the connection of the actuator from the driving circuit to the ejection failure detecting means after the ejection operation of the droplets is performed by driving the actuator corresponding to the nozzle of the droplet ejection head determined by the detection determining means.

According to one embodiment of the invention, the apparatus may be configured in such a manner that the ejection failure detecting means detects an ejection failure of the droplets at timing of the droplet ejection operation during the flushing process or the droplet ejection operation during a print operation by the nozzle as a target of detection. Because the droplet ejection apparatus of the invention is able to detect an ejection failure of the droplets even during a printing (recording) operation, that is, during the droplet ejection operation in the middle of the print operation, the throughput of the droplet ejection apparatus will be neither reduced nor deteriorated.

Also, the actuator may be an electrostatic actuator, or a piezoelectric actuator using a piezoelectric effect of a piezoelectric element. In addition, it may be preferable that the droplet ejection apparatus of the invention further includes storage means for storing the cause of an ejection failure of the droplets detected by the ejection failure detecting means, in connection with the nozzle as the target of detection.

Another object of the invention is to provide a droplet ejection apparatus capable of identifying the cause of an ejection failure when the ejection failure of a droplet ejection head is detected and performing adequate recovery processing depending on the cause of the ejection failure instead of the conventional sequential recovery processing, as well as efficiently confirming whether the droplet ejection head has been restored to a normal state by the recovery processing.

In order to achieve the above object, another aspect of the invention provides a droplet ejection apparatus, provided with a plurality of droplet ejection heads each ejecting liquid through a nozzle communicating with a cavity in the form of droplets by changing an internal pressure of the cavity filled with the liquid by driving an actuator with a driving circuit, for ejecting the droplets through the nozzles while scanning the droplet ejection heads relatively with respect to a droplet receptor so that the droplets land on the droplet receptor, and the droplet ejection apparatus of the invention is characterized by including:

ejection failure detecting means for detecting an ejection failure of the droplets through the nozzles and a cause thereof;

recovery means for performing recovery processing for the droplet ejection heads to eliminate the cause of the ejection failure of the droplets; and

storage means for storing a nozzle with which the ejection failure is detected by the ejection failure detecting means, in connection with the cause thereof,

wherein if detection by the ejection failure detecting means is performed for all of the nozzles and the presence of a failing nozzle in which an ejection failure is occurring is detected, recovery processing depending on the cause of the ejection failure is performed by the recovery means at least for the failing nozzle, after which detection by the ejection failure detecting means is performed again by forcing the failing nozzle alone to perform a droplet ejection operation.

6

Consequently, when an ejection failure of the droplet ejection head is detected, adequate recovery processing is performed depending on the cause of the ejection failure of the failing nozzle. Hence, rather than performing the sequential recovery processing by the conventional droplet ejection apparatus, it is possible to prevent liquid intended to be ejected, such as ink, from being wastefully discharged during the recovery processing, and consumption of the liquid to be ejected can be thereby reduced. Also, because the recovery processing of certain types that need not to be performed will not be performed, a time needed for the recovery processing can be shortened, which in turn makes it possible to improve the throughput (the number of printed sheets per unit time) of the droplet ejection apparatus.

Also, because detection by the ejection failure detecting means is performed again for the failing nozzle after the recovery processing in order to confirm whether the failing nozzle has been restored to a normal state, the occurrence of an ejection failure during the printing operation performed later can be prevented in a more reliable manner. Also, because detection by the ejection failure detecting means is performed by forcing the failing nozzle alone to perform the droplet ejection operation, the nozzles judged as being normal in the last detection do not have to eject droplets. It is thus possible to avoid wasteful ejection of the liquid to be ejected, which can in turn further reduce consumption of the liquid to be ejected. Moreover, the load on the ejection failure detecting means or the like can be reduced.

With the droplet ejection apparatus of the invention, it is preferable that the recovery means includes: wiping means for performing a wiping process by which nozzle surfaces of the droplet ejection heads, where the nozzles are aligned, are wiped off by a wiper; flushing means for performing a flushing process by which the droplets are preliminarily ejected through the nozzles by driving the actuators; and pumping means for performing a pump-suction process with the use of a pump connected to a cap covering the nozzle surfaces of the droplet ejection heads.

This allows the recovery means to perform adequate and waste-less recovery processing by selecting such processing from the wiping process, the flushing process, and the pump-suction process depending on the cause of an ejection failure.

With the droplet ejection apparatus of the invention, it is preferable that the cause of an ejection failure detectable by the ejection failure detecting means includes intrusion of an air bubble inside the cavity, thickening of the liquid caused by drying in a vicinity of the nozzle, and adhesion of paper dust in a vicinity of an outlet of the nozzle; and

the recovery means performs the pump-suction process by the pumping means in a case where the cause of the ejection failure of the failing nozzle is the intrusion of an air bubble, the flushing process by the flushing means or the pump-suction process by the pumping means in a case where the cause of the ejection failure of the failing nozzle is the thickening caused by drying, and at least the wiping process by the wiper in a case where the cause of the ejection failure of the failing nozzle is the adhesion of paper dust.

It is thus possible to perform adequate and waste-less recovery processing depending on the cause of an ejection failure including intrusion of an air bubble inside the cavity, drying and thickening of the liquid in the vicinity of the nozzle, and adhesion of paper dust in the vicinity of the outlet of the nozzle. In the invention, "paper dust" is not limited to mere paper dust generated from a recording sheet or the like, but includes all the substances that could adhere

in the vicinity of the nozzles and impede ejection of droplets, such as pieces of rubber from the advancing roller (feeding roller) and dust afloat in air.

A droplet ejection apparatus of the invention is a droplet ejection apparatus, provided with a plurality of droplet ejection heads each ejecting liquid through a nozzle communicating with a cavity in the form of droplets by changing an internal pressure of the cavity filled with the liquid by driving an actuator with a driving circuit, for ejecting the droplets through the nozzles while scanning the droplet ejection heads relatively with respect to a droplet receptor so that the droplets land on the droplet receptor, and the droplet ejection apparatus of the invention is characterized by including:

ejection failure detecting means for detecting an ejection failure of the droplets through the nozzles and a cause thereof;

recovery means for performing recovery processing for the droplet ejection heads to eliminate the cause of the ejection failure of the droplets; and

storage means for storing a nozzle with which the ejection failure is detected by the ejection failure detecting means, in connection with the cause thereof, wherein:

the recovery means includes flushing means for performing a flushing process by which the droplets are preliminarily ejected through the nozzles by driving the actuators; and

in a case where the presence of a failing nozzle in which an ejection failure is occurring is detected when detection by the ejection failure detecting means is performed for all of the nozzles, the flushing process is performed for the failing nozzle alone, after which detection by the ejection failure detecting means is performed again by forcing the failing nozzle alone to perform a droplet ejection operation, and when the presence of a re-failing nozzle in which the ejection failure has not been eliminated is detected, recovery processing depending on the cause of the ejection failure of the re-failing nozzle is performed by the recovery means at least for the re-failing nozzle, after which detection by the ejection failure detecting means is performed once again by forcing the re-failing nozzle alone to perform the droplet ejection operation.

Hence, if an ejection failure of the droplet ejection head is detected and the cause of the ejection failure of this failing nozzle is minor, the failing nozzle can be restored to the normal state quickly by the flushing process. Also, because the normally operating nozzles do not eject droplets in this testing sequence, liquid to be ejected, such as ink, is not consumed wastefully.

Also, because detection by the ejection failure detecting means is performed again for the failing nozzle after the flushing process in order to confirm whether the failing nozzle has been restored to a normal state, the occurrence of an ejection failure during the printing operation performed later can be prevented in a more reliable manner. Also, because detection by the ejection failure detecting means is performed by forcing the failing nozzle alone to perform the droplet ejection operation, the nozzles judged as being normal in the last detection do not have to eject droplets. It is thus possible to avoid wasteful ejection of the liquid to be ejected, which can in turn further reduce consumption of the liquid to be ejected.

Also, when the recovery processing of the failing nozzle is confirmed and the result shows the presence of a re-failing nozzle in which the ejection failure has not been eliminated, adequate recovery processing is performed depending on the cause of the ejection failure of this re-failing nozzle. Hence, in contrast to the sequential recovery processing by the

conventional droplet ejection apparatus, it is possible to prevent liquid from being wastefully discharged during the recovery processing, which can in turn further reduce consumption of the liquid. Also, because the recovery processing of the types that need not be performed will not be performed, a time needed for the recovery processing can be shortened, which in turn makes it possible to improve the throughput (the number of printed sheets per unit time) of the droplet ejection apparatus.

Also, because detection by the ejection failure detecting means is performed once again for the re-failing nozzle after the recovery processing for the re-failing nozzle in order to confirm whether the re-failing nozzle has been restored to the normal state, the occurrence of an ejection failure during the printing operation performed later can be prevented in a more reliable manner. Also, because detection by the ejection failure detecting means is performed by forcing the re-failing nozzle alone to perform the droplet ejection operation, the nozzles judged as operating normally in the last detection do not have to eject droplets. It is thus possible to avoid wasteful ejection of the liquid to be ejected, which can in turn further reduce consumption of the liquid to be ejected. Moreover, the load on the ejection failure detecting means or the like can be reduced.

With the droplet ejection apparatus of the invention, it is preferable that the recovery means further includes: wiping means for performing a wiping process by which nozzle surfaces of the droplet ejection heads, where the nozzles are aligned, are wiped off by a wiper; and pumping means for performing a pump-suction process with the use of a pump connected to a cap covering the nozzle surfaces of the droplet ejection heads.

This allows recovery means to perform adequate and waste-less recovery processing by selecting such processing from the wiping process, the flushing process, and the pump-suction process depending on the cause of an ejection failure.

With the droplet ejection apparatus of the invention, it is preferable that:

the cause of an ejection failure detectable by the ejection failure detecting means includes intrusion of an air bubble inside the cavity, thickening of the liquid caused by drying in a vicinity of the nozzle, and adhesion of paper dust in a vicinity of an outlet of the nozzle; and

the recovery means performs the pump-suction process by the pumping means if the cause of the ejection failure of the re-failing nozzle is the intrusion of an air bubble or the thickening caused by drying, and at least the wiping process by the wiper if the cause of the ejection failure of the re-failing nozzle is the adhesion of paper dust.

It is thus possible to perform adequate and waste-less recovery processing depending on the cause of an ejection failure including the intrusion of an air bubble inside the cavity, the drying and thickening of the liquid in the vicinity of the nozzle, and the adhesion of paper dust in the vicinity of the outlet of the nozzle.

With the droplet ejection apparatus of the invention, it is preferable that the recovery means performs the flushing process for each of the nozzles after the recovery processing depending on the cause of the ejection failure is performed.

It is thus possible to forestall the mixing of liquid to be ejected of various kinds in different colors or the like remaining on the nozzle surfaces.

With the droplet ejection apparatus of the invention, it is preferable that the wiping means is formed to be able to perform the wiping process separately for plural sets of nozzle groups, so that when performing the wiping process

depending on the cause of the ejection failure of the failing nozzle or the re-failing nozzle, the wiping means performs the wiping process only for a nozzle group including the failing nozzle or the re-failing nozzle.

Hence, because the wiping process can be performed selectively only for the nozzle group including the nozzle that needs the wiping process, a waste-less and efficient wiping process can be performed compared with a case where the wiping process is performed for all the nozzles at a time.

With the droplet ejection apparatus of the invention, it is preferable that the pumping means is formed to be able to perform the pump-suction process separately for plural sets of nozzle groups, so that when performing the pump-suction process depending on the cause of the ejection failure of the failing nozzle or the re-failing nozzle, the pumping means performs the pump-suction process only for a nozzle group including the failing nozzle or the re-failing nozzle.

Hence, because the pump-suction process can be performed selectively only for the nozzle group including the nozzle that needs the pump-suction process, a waste-less and efficient pump-suction process can be performed compared with a case where the pump-suction process is performed for all the nozzles at a time.

With the droplet ejection apparatus of the invention, it is preferable that the plural sets of nozzle groups have different kinds of droplets to be ejected.

It is thus possible to perform the wiping process or the pump-suction process for individual nozzle groups used for ejecting different kinds of liquid to be ejected. Hence, not only can waste-less and efficient recovery processing be performed, but also the mixing of different kinds of liquid to be ejected can be forestalled.

It is preferable that the droplet ejection apparatus of the invention further include informing means for informing a detection result when a result of detection by the ejection failure detecting means shows the presence of a nozzle with which an ejection failure is detected.

It is thus possible to inform the user (operator) of the occurrence of an ejection failure quickly.

With the droplet ejection apparatus of the invention, it is preferable that:

the actuator of each of the droplet ejection heads have a diaphragm that can be displaced in such a manner so as to change an internal pressure of the corresponding cavity; and

the ejection failure detecting means detects residual vibration of the diaphragm and detects an ejection failure on the basis of a vibration pattern of the detected residual vibration of the diaphragm.

It is thus possible to detect an ejection failure and the cause thereof with accuracy in a reliable manner by a relatively simple configuration.

With the droplet ejection apparatus of the invention, it is preferable that the actuator is an electrostatic actuator.

Hence, in the case of the droplet ejection head employing an electrostatic actuator, an ejection failure and the cause thereof can be detected with accuracy in a reliable manner by a relatively simple configuration.

With the droplet ejection apparatus of the invention, it is preferable that the actuator is a piezoelectric actuator using a piezoelectric effect of a piezoelectric element.

Hence, in the case of the droplet ejection head employing a piezoelectric actuator, an ejection failure and the cause thereof can be detected with accuracy in a reliable manner by a relatively simple configuration.

With the droplet ejection apparatus of the invention, it is preferable that the ejection failure detecting means includes

an oscillation circuit, and the oscillation circuit oscillates on the basis of an electric capacitance component of the actuator that varies with the residual vibration of the diaphragm.

It is thus possible to detect an ejection failure accurately by an inexpensive circuit of a simple design.

With the droplet ejection apparatus of the invention, it is preferable that the oscillation circuit form a CR oscillation circuit from the electric capacitance component of the actuator and a resistance component of a resistor element connected to the actuator.

It is thus possible to detect the residual vibration of the diaphragm accurately, which in turn enables an ejection failure to be detected accurately.

With the droplet ejection apparatus of the invention, it is preferable that the actuator of each of the droplet ejection heads has a heating element that can give rise to film boiling by heating the liquid filled in the corresponding cavity;

each of the droplet ejection heads further includes a diaphragm that is displaced elastically in association with a change in internal pressure of the cavity, and an electrode provided opposite to the diaphragm; and

the ejection failure detecting means detects residual vibration of the diaphragm and detects an ejection failure on the basis of a vibration pattern of the detected residual vibration of the diaphragm.

Hence, in the case of the droplet ejection head of the thermal jet method, an ejection failure and the cause thereof can be detected with accuracy in a reliable manner by a relatively simple configuration.

With the droplet ejection apparatus of the invention, it is preferable that the ejection failure detecting means includes an oscillation circuit, and the oscillation circuit oscillates on the basis of a variance with time of an electric capacitance of a capacitor formed from the diaphragm and the electrode, associated with the residual vibration of the diaphragm.

It is thus possible to detect an ejection failure accurately by an inexpensive circuit of a simple design.

With the droplet ejection apparatus of the invention, it is preferable that the oscillation circuit forms a CR oscillation circuit from an electric capacitance component of the capacitor and a resistance component of a resistor element.

It is thus possible to detect the residual vibration of the diaphragm accurately, which in turn enables an ejection failure to be detected accurately.

With the droplet ejection apparatus of the invention, it is preferable that the vibration pattern of the residual vibration of the diaphragm include a cycle of the residual vibration.

It is thus possible to detect an ejection failure with a high degree of accuracy.

With the droplet ejection apparatus of the invention, it is preferable that: the ejection failure detecting means include judging means for judging the presence or absence of an ejection failure of the droplets in the corresponding droplet ejection head on the basis of the vibration pattern of the residual vibration of the diaphragm, and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in the droplet ejection head.

It is thus possible to judge the presence or absence of an ejection failure and the cause thereof in a reliable manner.

With the droplet ejection apparatus of the invention, it is preferable that the judging means judges that an air bubble has intruded inside the cavity when the cycle of the residual vibration of the diaphragm is shorter than a cycle of a predetermined range, the liquid has thickened by drying in the vicinity of the nozzle when the cycle of the residual vibration of the diaphragm is longer than a predetermined threshold, and paper dust is adhering in the vicinity of the

11

outlet of the nozzle when the cycle of the residual vibration of the diaphragm is longer than the cycle of the predetermined range and shorter than the predetermined threshold.

It is thus possible to differentiate the intrusion of air bubbles inside the cavity from drying, thickening of the liquid in the vicinity of the nozzle and adhesion of paper dust in the vicinity of the outlet of the nozzle, as the cause of an ejection failure.

With the droplet ejection apparatus of the invention, it is preferable that the ejection failure detecting means includes an F/V converting circuit that generates a voltage waveform of the residual vibration of the diaphragm from a predetermined signal group generated on the basis of a change of an oscillation frequency in an output signal from the oscillation circuit.

It is thus possible to set the detection sensitivity to a larger magnitude when the residual vibration waveform is detected.

With the droplet ejection apparatus of the invention, it is preferable that the ejection failure detecting means include a waveform shaping circuit that shapes the voltage waveform of the residual vibration of the diaphragm generated in the F/V converting circuit into a predetermined waveform.

It is thus possible to set the detection sensitivity to a larger magnitude when the residual vibration waveform is detected.

With the droplet ejection apparatus of the invention, it is preferable that the waveform shaping circuit includes: DC component removing means for removing a direct current component from the voltage waveform of the residual vibration of the diaphragm generated in the F/V converting circuit; and a comparator that compares the voltage waveform, from which the direct current component has been removed by the DC component removing means, with a predetermined voltage value, so that the comparator generates and outputs a rectangular wave on the basis of the voltage comparison.

It is thus possible to set the detection sensitivity to a larger magnitude when the residual vibration waveform is detected.

With the droplet ejection apparatus of the invention, it is preferable that the ejection failure detecting means include measuring means for measuring a cycle of the residual vibration of the diaphragm from the rectangular wave generated in the waveform shaping circuit.

It is thus possible to detect the cycle of the residual vibration of the diaphragm accurately in a simple manner.

With the droplet ejection apparatus of the invention, it is preferable that the measuring means has a counter, and measures a time between rising edges or between a rising edge and a falling edge of the rectangular wave by counting pulses of a reference signal with the counter.

It is thus possible to detect the cycle of the residual vibration of the diaphragm accurately in a simple manner.

Still another aspect of the invention provides an ejection failure recovery method for a droplet ejection apparatus having a head unit including a plurality of droplet ejection heads each ejecting liquid within a cavity through a nozzle in the form of droplets by driving an actuator with a driving circuit, and the ejection failure recovery method for a droplet ejection apparatus of the invention is characterized by including:

detecting an ejection failure of the droplet ejection heads and a cause thereof; and performing recovery processing depending on the cause of the ejection failure if the ejection failure is detected when the droplets are ejected through the nozzles.

12

According to the ejection failure recovery method for a droplet ejection apparatus of the invention, the same advantages as those achieved by the droplet ejection apparatus described above can be obtained.

BRIEF DESCRIPTION OF THE DRAWINGS

The above and other objects, features, and the advantages of the invention will readily become more apparent from the following detailed description of preferred embodiments of the invention with reference to the accompanying drawings.

FIG. 1 is a schematic view showing the configuration of an ink jet printer as one type of a droplet ejection apparatus of the invention;

FIG. 2 is a block diagram schematically showing a major portion of the ink jet printer of the invention;

FIG. 3 is a schematic cross section of a head unit (ink jet head) in the ink jet printer shown in FIG. 1;

FIG. 4 is an exploded perspective view showing the configuration of the head unit of FIG. 3;

FIG. 5 shows one example of a nozzle alignment pattern in a nozzle plate of the head unit using four colors of ink;

FIG. 6 shows views of respective states of a cross section taken along the line III—III of FIG. 3 upon input of a driving signal;

FIG. 7 is a circuit diagram showing a computation model of simple harmonic vibration on the assumption of residual vibration of a diaphragm of FIG. 3;

FIG. 8 is a graph showing the relation between an experiment value and a computed value of residual vibration of the diaphragm of FIG. 3 in the case of normal ejection;

FIG. 9 is a conceptual view in the vicinity of a nozzle in a case where an air bubble has intruded inside a cavity of FIG. 3;

FIG. 10 is a graph showing the computed value and the experiment value of residual vibration in a state where ink drops are not ejected due to intrusion of an air bubble inside the cavity;

FIG. 11 is a conceptual view in the vicinity of the nozzle in a case where ink has fixed by drying in the vicinity of the nozzle of FIG. 3;

FIG. 12 is a graph showing the computed value and the experiment value of residual vibration in a state where ink has thickened by drying in the vicinity of the nozzle;

FIG. 13 is a conceptual view of the vicinity of the nozzle in a case where paper dust is adhering in the vicinity of the outlet of the nozzle of FIG. 3;

FIG. 14 is a graph showing the computed value and the experiment value of residual vibration in a state where paper dust is adhering to the outlet of the nozzle;

FIG. 15 shows pictures of the nozzle states before and after adhesion of paper dust in the vicinity of the nozzle;

FIG. 16 is a schematic block diagram of ejection failure detecting means;

FIG. 17 is a conceptual view in a case where a parallel plate capacitor is used as an electrostatic actuator of FIG. 3;

FIG. 18 is a circuit diagram of an oscillation circuit including a capacitor comprising the electrostatic actuator of FIG. 3;

FIG. 19 is a circuit diagram of an F/V converting circuit in the ejection failure detecting means shown in FIG. 16;

FIG. 20 is a timing chart showing the timing of output signals from respective portions based on an oscillation frequency outputted from the oscillation circuit;

FIG. 21 is a view used to explain a setting method of fixed times t_r and t_1 ;

13

FIG. 22 is a circuit diagram showing the circuitry of a waveform shaping circuit of FIG. 16;

FIG. 23 is a block diagram schematically showing switching means switching between a driving circuit and a detection circuit;

FIG. 24 is a flowchart detailing ejection failure detection and judgment processing;

FIG. 25 is a flowchart detailing residual vibration detection processing;

FIG. 26 is a flowchart detailing ejection failure judgment processing;

FIG. 27 shows one example of detection timing of an ejection failure for a plurality of ink jet heads (in a case where there is one ejection failure detecting means);

FIG. 28 shows one example of detection timing of an ejection failure for a plurality of ink jet heads (in a case where the number of the ejection failure detecting means is equal to the number of ink jet heads);

FIG. 29 shows one example of detection timing of an ejection failure for a plurality of ink jet heads (in a case where the number of the ejection failure detecting means is equal to the number of ink jet heads, and detection of an ejection failure is performed in the presence of print data);

FIG. 30 shows one example of detection timing of an ejection failure for a plurality of ink jet heads (in a case where the number of the ejection failure detecting means is equal to the number of ink jet heads, and detection of an ejection failure is performed by making rounds at the respective ink jet heads);

FIG. 31 is a flowchart detailing the detection timing of an ejection failure during a flushing operation by the ink jet printer shown in FIG. 27;

FIG. 32 is a flowchart detailing the detection timing of an ejection failure during the flushing operation by the ink jet printers shown in FIG. 28 and FIG. 29;

FIG. 33 is a flowchart detailing the detection timing of an ejection failure during the flushing operation by the ink jet printer shown in FIG. 30;

FIG. 34 is a flowchart detailing the detection timing of an ejection failure during a print operation by the ink jet printers shown in FIG. 28 and FIG. 29;

FIG. 35 is a flowchart detailing the detection timing of an ejection failure during the print operation by the ink jet printer shown in FIG. 30;

FIG. 36 is a view schematically showing the structure (part of which is omitted) when viewed from the top of the ink jet printer shown in FIG. 1;

FIG. 37 is a view showing the positional relation between a wiper and the head unit shown in FIG. 36;

FIG. 38 is a view showing the relation among the head unit, a cap, and a pump during a pump-suction process;

FIG. 39 is a schematic view showing the configuration of a tube pump shown in FIG. 38;

FIG. 40 is a flowchart detailing ejection failure recovery processing in an ink jet printer of the invention;

FIG. 41 shows views used to explain an example of another configuration of the wiper (wiping means), (a) being a view showing a nozzle surface of the print means (head unit), and (b) being a view showing the wiper;

FIG. 42 is a view showing an operation state of the wiper shown in FIG. 41;

FIG. 43 is a view used to explain an example of another configuration of the pumping means;

FIG. 44 is a cross section schematically showing an example of another configuration of the ink jet head of the invention;

14

FIG. 45 is a cross section schematically showing an example of still another configuration of the ink jet head of the invention;

FIG. 46 is a cross section schematically showing an example of still another configuration of the ink jet head of the invention;

FIG. 47 is a cross section schematically showing an example of still another configuration of the ink jet head of the invention;

FIG. 48 is a perspective view showing the configuration of a head unit according to a third embodiment; and

FIG. 49 is a cross section of the head unit (ink jet head) shown in FIG. 48.

DETAILED DESCRIPTION

Preferred embodiments of a droplet ejection apparatus and an ejection failure recovery method of the invention will now be described in detail with reference to FIG. 1 through FIG. 49. It is to be understood that these embodiments are for the purpose of illustration and interpretations of the content of the invention are not limited to these embodiments. It should be noted that, in the embodiments below, an ink jet printer that prints an image on a recording sheet (droplet receptor) by ejecting ink (liquid material) will be described as one example of the droplet ejection apparatus of the invention.

First Embodiment

FIG. 1 is a schematic view showing the configuration of an ink jet printer 1 as one type of a droplet ejection apparatus according to a first embodiment of the invention. Hereinafter, the upper side and the lower side of FIG. 1 are referred to as "top" and "bottom", respectively. First, the configuration of the ink jet printer 1 will be described.

The ink jet printer 1 shown in FIG. 1 includes an apparatus main body 2. A tray 21, on which a recording sheet P is placed, is provided rearward of the top, a sheet discharge port 22, through which the recording sheet P is discharged, is provided frontward of the bottom, and an operation panel 7 is provided on the top surface.

The operation panel 7 comprises, for example, a liquid crystal display, an organic EL display, an LED lamp, etc., and is provided with a display portion (not shown) to display an error message or the like and an operation portion (not shown) comprising various kinds of switches or the like. The display portion of the operation panel 7 functions as informing means.

Also, the apparatus main body 2 chiefly encloses a printing apparatus (printing means) 4 equipped with print device (movable body) 3 performing a reciprocating motion, a feeding apparatus (droplet receptor transporting means) 5 feeding/discharging a recording sheet P to/from the printing apparatus 4, and a control portion (control means) 6 controlling the printing apparatus 4 and the feeding apparatus 5.

The feeding apparatus 5 intermittently feeds recording sheets P one by one under the control of the control portion 6. The recording sheet P passes by the vicinity of the bottom of the print device 3. In this instance, the print device 3 reciprocates in a direction intersecting at almost right angles with the feeding direction of the recording sheet P, and printing on the recording sheet P is thereby performed. In other words, printing by the ink jet method is performed while the reciprocating motion of the print device 3 and the

intermittent feeding of the recording sheet P take place as the main scanning and the sub scanning of printing, respectively.

The printing apparatus 4 is provided with the print device 3, a carriage motor 41 serving as a driving source for moving the print device 3 (causing it to reciprocate) in the main scanning direction, and a reciprocating mechanism 42 receiving rotations of the carriage motor 41 and causing the print device 3 to reciprocate.

The print device 3 includes a plurality of head units 35 corresponding to the kinds of ink and provided with a number of nozzles 110, ink cartridges (I/Cs) 31 supplying the respective head units 35 with ink, a carriage 32 on which the respective head units 35 and ink cartridges 31 are mounted.

Also, as will be described below with reference to FIG. 3, each head unit 35 is provided with a number of ink jet recording heads (ink jet heads or droplet ejection heads) 100, each comprising one nozzle 110, one diaphragm 121, one electrostatic actuator 120, one cavity 141, and one ink supply port 142, etc. FIG. 1 shows the configuration in which the head units 35 include the ink cartridges 31; however, the head units 35 are not limited to this configuration. For example, in the case of an ink jet printer consuming a large quantity of ink, the ink cartridges 31 may be provided in another place, so that the head units 35 are supplied with ink by a tube or the like. Hence, hereinafter, apart from the print device 3, those provided with a plurality of ink jet heads 100, each comprising one nozzle 110, one diaphragm 121, one electrostatic actuator 120, one cavity 141, and one ink supply port 142, etc., are referred to as the head units 35.

By using cartridges respectively filled with four colors of ink, including yellow, cyan, magenta, and black, as the ink cartridges 31, full-color printing becomes possible. In this case, head units 35 corresponding to the respective colors are provided to the print device 3 (the configuration of which will be described in detail below). Herein, FIG. 1 shows four ink cartridges 31 corresponding to four colors of ink, respectively; however, the print device 3 may be configured to further include an ink cartridge 31 for ink of a special color, for example, light cyan, light magenta, or dark yellow.

The reciprocating mechanism 42 includes a carriage guide shaft 422 supported by a frame (not shown) at both ends, and a timing belt 421 extending in parallel with the carriage guide shaft 422.

The carriage 32 is supported by the carriage guide shaft 422 of the reciprocating mechanism 42 so as to be free to reciprocate while being fixed to part of the timing belt 421.

When the timing belt 421 is run forward and backward via a pulley by the operation of the carriage motor 41, the print device 3 is guided by the carriage guide shaft 422 and starts to reciprocate. During this reciprocating motion, ink drops are ejected through the respective ink jet heads 100 of the head units 35 as needed in response to image data (printing data) to be printed, and printing on the recording sheet P is thereby performed.

The feeding apparatus 5 includes a feeding motor 51 serving as a driving source, and a feeding roller 52 rotating in association with the operation of the feeding motor 51.

The feeding roller 52 comprises a driven roller 52a and a driving roller 52b opposing vertically with a transportation path of a recording sheet P (recording sheet P) in between. The driving roller 52b is coupled to the feeding motor 51. This allows the feeding roller 52 to feed a number of recording sheets P on the tray 21 to the printing apparatus 4 one by one, or discharge the recording sheets P from the

printing apparatus 4 one by one. Instead of the tray 21, a feeding cassette accommodating the recording sheets P may be removably attached.

Further, the feeding motor 51 advances a recording sheet P depending on the resolution of an image in association with the reciprocating motion of the print device 3. The feeding operation and the advancing operation may be performed individually by separate motors, or alternatively, they may be performed by the same motor with the use of a part that switches torque transmission, such as an electromagnetic clutch.

The control portion 6 performs printing processing on a recording sheet P by controlling the printing apparatus 4, the feeding apparatus 5, etc. according to the printing data inputted from a host computer 8, such as a personal computer (PC) and a digital camera (DC). The control portion 6 also controls the display portion of the operation panel 7 to display an error message or the like, or an LED lamp or the like to switch ON/OFF, and controls the respective portions to perform corresponding processing according to depressed signals of various switches inputted from the operation portion. Further, the control portion 6 may be configured to transfer information, such as an error message or an ejection failure, to the host computer 8 via an interface portion 9 as the necessity arises.

FIG. 2 is a block diagram schematically showing a major portion of the ink jet printer of the invention. Referring to FIG. 2, an ink jet printer 1 of the invention is provided with the interface portion (IF) 9 receiving printing data or the like inputted from the host computer 8, the control portion 6, the carriage motor 41, a carriage motor driver 43 driving the carriage motor 41 under its control, the feeding motor 51, a feeding motor driver 53 driving the feeding motor 51 under its control, the head units 35, a head driver 33 driving the head units 35 under its control, ejection failure detecting means (device) 10, recovery means (device) 24, and the operation panel 7. The ejection failure detecting device 10, the recovery device 24, and the head driver 33 will be described below in detail.

Referring to FIG. 2, the control portion 6 is provided with a CPU (Central Processing Unit) 61 performing various types of processing including printing processing, ejection failure detection processing, etc., an EEPROM (Electrically Erasable Programmable Read-Only Memory) (storage means) 62 as one kind of non-volatile semiconductor memory used to store printing data inputted from the host computer 8 via the IF 9 in an unillustrated data storage region, a RAM (Random Access Memory) 63 temporarily storing various kinds of data when ejection failure detection processing or the like described below is performed or temporarily developing an application program for printing processing or the like, and a PROM 64 as one kind of non-volatile semiconductor memory used to store control programs or the like for controlling the respective portions. The respective components of the control portion 6 are electrically connected via an unillustrated bus.

As has been described, the print device 3 is provided with a plurality of head units 35 corresponding to the respective colors of ink. Also, each head unit 35 is provided with a plurality of nozzles 110 and the electrostatic actuators 120 corresponding to the respective nozzles 110. In other words, each head unit 35 is configured to include a plurality of ink jet heads 100 (droplet ejection heads) each comprising a set including the nozzle 110 and the electrostatic actuator 120. Meanwhile, the head driver 33 comprises a driving circuit 18 controlling ejection timing of ink by driving the electrostatic actuators 120 of the respective ink jet heads 100, and

switching means (device) 23 (see FIG. 16). The configurations of the ink jet head 100 and the electrostatic actuator 120 will be described below.

Although it is not shown in the drawing, various kinds of sensors capable of detecting, for example, a remaining quantity of ink in the ink cartridges 31, the position of the print device 3, printing environments, such as temperature and humidity, etc. are electrically connected to the control portion 6.

Upon receipt of printing data from the host computer 8 via the IF 9, the control portion 6 stores the printing data in the EEPROM 62. The CPU 61 then performs predetermined processing on the printing data, and outputs driving signals to each of the drivers 33, 43, and 53 according to the processing data thus obtained and input data from the various kinds of sensors. Upon input of these driving signals through each of the drivers 33, 43, and 53, the electrostatic actuators 120 corresponding to a plurality of ink jet heads 100 of the head units 35, the carriage motor 41 of the printing apparatus 4, and the feeding apparatus 5 start to operate individually. Printing processing is thus performed on a recording sheet P.

The structure of each ink jet head 100 in each head unit 35 will now be described. FIG. 3 is a schematic cross section (including a common portion, such as the ink cartridge 31) of one ink jet head 100 of each head unit 35 shown in FIG. 1. FIG. 4 is an exploded perspective view schematically showing the configuration of the head unit 35 corresponding to one color of ink. FIG. 5 is a plan view showing an example of a nozzle surface of the print device 3 adopting the head unit 35 shown in FIG. 3 and FIG. 4. It should be noted that FIG. 3 and FIG. 4 are shown upside down from the normally used state.

As shown in FIG. 3, the head unit 35 is connected to the ink cartridge 31 via an ink intake port 131, a damper chamber 130; and an ink supply tube 311. The damper chamber 130 is provided with a damper 132 made of rubber. The damper chamber 130 can absorb fluctuation of ink and a change in ink pressure when the carriage 32 reciprocates, which makes it possible to supply the respective ink jet heads 100 of the head unit 35 with a predetermined quantity of ink in a stable manner.

Also, the head unit 35 is of a triple-layer structure, comprising a silicon substrate 140 in the middle, a nozzle plate 150 also made of silicon layered on the upper side, and a borosilicate glass substrate (glass substrate) 160, having a coefficient of thermal expansion close to that of silicon, layered on the lower side. The silicon substrate 140 in the middle is provided with a plurality of independent cavities (pressure chambers) 141 (seven cavities are shown in FIG. 4), one reservoir (common ink chamber) 143, and grooves each functioning as an ink supply port (orifice) 142 allowing communication between the reservoir 143 and the respective cavities 141. Each groove is formed, for example, by applying etching processing from the surface of the silicon substrate 140. The nozzle plate 150, the silicon substrate 140, and the glass substrate 160 are bonded to each other in this order, and the respective cavities 141, the reservoir 143, and the respective ink supply ports 142 are thereby defined.

Each of these cavities 141 is formed in the shape of a strip (rectangular prism), and is configured in such a manner that a volume thereof is variable with vibration (displacement) of a diaphragm 121 described below, and this change in volume causes ink (liquid material) to be ejected through the nozzle 110. The nozzles 110 are formed in the nozzle plate 150 at positions corresponding to the respective cavities 141 at the portions on the tip side, and communicate with the respec-

tive cavities 141. Also, the ink intake port 131 communicating with the reservoir 143 is formed in the glass substrate 160 at a portion where the reservoir 143 is located. Ink is supplied from the ink cartridge 31 to the reservoir 143 by way of the ink supply tube 311 and the damper chamber 130 through the ink intake port 131. Ink supplied to the reservoir 143 passes through the respective ink supply ports 142 and is then supplied to the respective independent cavities 141. The respective cavities 141 are defined by the nozzle plate 150, sidewalls (partition walls) 144, and bottom walls 121.

The bottom wall 121 of each of the independent cavity 141 is formed thin, and the bottom wall 121 is formed to function as a diaphragm that can undergo elastic deformation (elastic displacement) in the out-of-plane direction (thickness direction), that is, in the vertical direction of FIG. 3. Hence, hereinafter, the portion of this bottom wall 121 will be occasionally referred to as the diaphragm 121 for ease of explanation (in other words, the same reference numeral 121 is used for both the bottom wall and the diaphragm).

Shallow concave portions 161 are formed on the surface of the glass substrate 160 on the silicon substrate 140 side, at the positions corresponding to the respective cavities 141 in the silicon substrate 140. Hence, the bottom wall 121 of each cavity 141 opposes, with a predetermined clearance in between, the surface of an opposing wall 162 of the glass substrate 160 in which the concave portions 161 are formed. In other words, a clearance of a predetermined thickness (for example, approximately 0.2 micron) is present between the bottom wall 121 of each cavity 141 and a segment electrode 122 described below. The concave portions 161 can be formed, for example, by etching.

The bottom wall (diaphragm) 121 of each cavity 141 forms part of a common electrode 124 on the respective cavities 141 side for accumulating charges by a driving signal supplied from the head driver 33. In other words, the diaphragm 121 of each cavity 141 also serves as one of the counter electrodes (counter electrodes of the capacitor) of the corresponding electrostatic actuator 120 described below. The segment electrodes 122 serving as electrodes opposing the common electrode 124 are formed respectively on the surfaces of the concave portions 161 in the glass substrate 160 so as to face the bottom walls 121 of the respective cavities 141. Also, as shown in FIG. 3, the surfaces of the bottom walls 121 of the respective cavities 141 are covered with an insulation layer 123 made of a silicon dioxide (SiO₂) film. In this manner, the bottom walls 121 of the respective cavities 141, that is, the diaphragms 121 and the corresponding respective segment electrodes 122 form (constitute) the counter electrodes (counter electrodes of the capacitor) via the insulation layer 123 formed on the surfaces of the bottom walls 121 of the cavities 141 on the lower side of FIG. 3 and clearances within the concave portions 161. Hence, the diaphragm 121, the segment electrode 122, and the insulation layer 123 and the clearance therebetween together form the major portion of the electrostatic actuator 120.

As shown in FIG. 3, the head driver 33 including the driving circuit 18 used to apply a driving voltage between these counter electrodes charges and discharges these counter electrodes in response to a print signal (print data) inputted from the control portion 6. One output terminal of the head driver (voltage applying means) 33 is connected to the respective segment electrodes 122, and the other output terminal is connected to an input terminal 124a of the common electrode 124 formed in the silicon substrate 140. Because the silicon substrate 140 is doped with impurities

and therefore has electrical conduction by itself, it is possible to supply the common electrode **124** of the bottom walls **121** with a voltage from the input terminal **124a** of the common electrode **124**. Alternatively, for example, a thin film made of an electrically conductive material, such as gold and copper, may be formed on one surface of the silicon substrate **140**. This allows a voltage (charges) to be supplied to the common electrode **124** at low electric resistance (efficiently). This thin film may be formed, for example, by vapor deposition, sputtering, etc. In this embodiment, for example, because the silicon substrate **140** and the glass substrate **160** are coupled (bonded) to each other through anode bonding, an electrical conductive film used as an electrode in this anode bonding is formed on the silicon substrate **140** on the channel forming surface side (on the top side of the silicon substrate **140** shown in FIG. 3). This electrically conductive film is directly used as the input terminal **124a** of the common electrode **124**. It should be appreciated, however, that in the invention, for example, the input terminal **124a** of the common electrode **124** may be omitted and the bonding method of the silicon substrate **140** and the glass substrate **160** is not limited to the anode bonding.

As shown in FIG. 4, the head unit **35** is provided with the nozzle plate **150** in which a plurality of nozzles **110** are formed, the silicon substrate (ink chamber substrate) **140** in which a plurality of cavities **141**, a plurality of ink supply ports **142**, and one reservoir **143** are formed, and the insulation layer **123**, all of which are accommodated in a base body **170** containing the glass substrate **160**. The base body **170** is made of, for example, various kinds of resin materials, various kinds of metal materials, etc., and the silicon substrate **140** is fixed to and supported by the base body **170**.

The nozzles **110** formed in the nozzle plate **150** are aligned linearly almost parallel to the reservoir **143** in FIG. 4 to make the illustration simple. However, the alignment pattern of the nozzles is not limited to this, and in general, for example, they are aligned in shifted stages as in the nozzle alignment pattern shown in FIG. 5. Also, the pitch between the nozzles **110** can be set appropriately depending on the printing resolution (dpi: dot per inch). FIG. 5 shows the alignment pattern of the nozzles **110** in a case where four colors of ink (ink cartridges **31**) are used.

FIG. 6 shows respective states of the cross section taken along the line III—III of FIG. 3 upon input of a driving signal. When a driving voltage is applied between the counter electrodes from the head driver **33**, a Coulomb's force develops between the counter electrodes. The bottom wall (diaphragm) **121** then bends towards the segment electrode **122** from the initial state (FIG. 6(a)), which causes the volume of the cavity **141** to increase (FIG. 6(b)). When the charges between the counter electrodes are discharged abruptly in this state under the control of the head driver **33**, the diaphragm **121** restores upward in the drawing due to its elastic restoring force, and moves upwards above its initial position which causes the volume of the cavity **141** to contract abruptly (FIG. 6(c)). In this instance, part of the ink (liquid material) filled in the cavity **141** is ejected through the nozzle **110** communicating with this cavity **141** in the form of ink drops by the compression pressure generated within the cavity **141**.

The damped vibration of the diaphragm **121** in each cavity **141** is continued by this series of operations (the ink ejection operation by the driving signal from the head driver **33**) until ink drops are ejected again upon input of the following driving signal (driving voltage). Hereinafter, this

damped vibration is also referred to as the residual vibration. The residual vibration of the diaphragm **121** is assumed to have an intrinsic vibration frequency that is determined by the acoustic resistance r given by the shapes of the nozzles **110** and the ink supply ports **142** or a degree of ink viscosity, the inertance m given by a weight of ink within the channel, and the compliance C_m of the diaphragm **121**.

The computation model of the residual vibration of the diaphragm **121** based on the above assumption will now be described. FIG. 7 is a circuit diagram showing the computation model of simple harmonic vibration on the assumption of the residual vibration of the diaphragm **121**. In this manner, the computation model of the residual vibration of the diaphragm **121** can be represented by a sound pressure P , and the aforementioned inertance m , compliance C_m and acoustic resistance r . Then, by computing a step response in terms of a volume velocity u when the sound pressure P is given to the circuit of FIG. 7, following equations are obtained.

(Mathematical Expression 1)

$$u = \frac{P}{\omega \cdot m} e^{-\alpha x} \cdot \sin \omega t \quad (1)$$

$$\omega = \sqrt{\frac{1}{m \cdot C_m} - \alpha^2} \quad (2)$$

$$\alpha = \frac{r}{2m} \quad (3)$$

The computation result obtained from the equations above is compared with the experiment result from an experiment performed separately as to the residual vibration of the diaphragm **121** after ejection of ink drops. FIG. 8 is a graph showing the relation between the experiment value and the computed value of the residual vibration of the diaphragm **121**. As can be understood from the graph shown in FIG. 8, two waveforms of the experiment value and the computed value almost agree with each other.

Incidentally, a phenomenon may occur in the respective ink jet heads **100** of the head unit **35** that ink drops are not ejected normally through the nozzles **110** even when the aforementioned ejection operation is performed, that is, the occurrence of an ejection failure of droplets. The occurrence of an ejection failure is attributed to, as will be described below, (1) intrusion of an air bubble inside the cavity **141**, (2) drying and thickening (fixing) of ink in the vicinity the nozzle **110**, (3) adhesion of paper dust in the vicinity the outlet of the nozzle **110**, etc.

Once the ejection failure occurs, it typically results in non-ejection of droplets through the nozzle **110**, that is, the advent of a droplet non-ejection phenomenon, which gives rise to the missing dot in pixels forming an image printed (drawn) on a recording sheet P . Also, in the case of the ejection failure, even when droplets are ejected through the nozzle **110**, the ejected droplets do not land on the recording sheet P adequately because a quantity of droplets is too small or the flying direction (trajectory) of droplets is deviated, which also appears as a missing dot in the pixels. For this reason, hereinafter, an ejection failure of droplets may also be referred to simply as the missing dot.

In the following, values of the acoustic resistance r and/or the inertance m are adjusted on the basis of the comparison result shown in FIG. 8 for each cause of the missing dot (ejection failure) phenomenon (droplet non-ejection phenomenon) during the printing processing occurring in the

nozzle **110** of the ink jet head **100**, so that the computed value and the experiment value of the residual vibration of the diaphragm **121** match (almost agree) with each other. Herein, three causes, that is, intrusion of an air bubble, thickening caused by drying, and adhesion of paper dust, will be discussed.

Firstly, intrusion of an air bubble inside the cavity **141**, which is one of the causes of the missing dot, will be discussed. FIG. **9** is a conceptual view in the vicinity of the nozzle **110** in a case where an air bubble B has intruded inside the cavity **141** of FIG. **3**. As is shown in FIG. **9**, the air bubble B thus generated is assumed to be generated and adhering to the wall surface of the cavity **141** (FIG. **9** shows a case where the air bubble B is adhering in the vicinity of the nozzle **110**, as one example of the adhesion position of the air bubble B).

When the air bubble B has intruded inside the cavity **141** in this manner, a total weight of ink filling the cavity **141** is thought to decrease, which in turn lowers the inertance m . Also, because the air bubble B is adhering to the wall surface of the cavity **141**, the nozzle **110** is thought to be in a state where its diameter is increased in size by the diameter of the air bubble B, which in turn lowers the acoustic resistance r .

Hence, by setting both the acoustic resistance r and the inertance m smaller than in the case of FIG. **8** where ink is ejected normally, to be matched with the experiment value of the residual vibration in the case of intrusion of an air bubble, the result (graph) as shown in FIG. **10** was obtained. As can be understood from the graphs of FIG. **8** and FIG. **10**, in the case of intrusion of an air bubble inside the cavity **141**, a residual vibration waveform, characterized in that the frequency becomes higher than in the case of normal ejection, is obtained. It is also confirmed that the damping rate of amplitude of the residual vibration becomes smaller as the acoustic resistance r is lowered, and the amplitude of the residual vibration thus becomes smaller slowly.

Next, drying (fixing and thickening) of ink in the vicinity of the nozzle **110**, which is another cause of the missing dot, will be discussed. FIG. **11** is a conceptual view in the vicinity of the nozzle **110** in a case where ink has fixed by drying in the vicinity of the nozzle **110** of FIG. **3**. As is shown in FIG. **11**, in a case where ink has fixed by drying in the vicinity of the nozzle **110**, ink within the cavity **141** is in a situation that it is trapped within the cavity **141**. When ink dries and thickens in the vicinity of the nozzle **110** in this manner, the acoustic resistance r is thought to increase.

Hence, by setting the acoustic resistance r larger than in the case of FIG. **8** where ink is ejected normally, to be matched with the experiment value of the residual vibration in the case of fixing (thickening) of ink caused by drying in the vicinity of the nozzle **110**, the result (graph) as shown in FIG. **12** was obtained. The experiment values shown in FIG. **12** are those obtained by measuring the residual vibration of the diaphragm **121** in a state that the head unit **35** was allowed to stand for a few days without attaching an unillustrated cap, so that ink could not be ejected because the ink had dried and thickened (ink had fixed) in the vicinity of the nozzle **110**. As can be understood from the graphs of FIG. **8** and FIG. **12**, in a case where ink has thickened by drying in the vicinity of the nozzle **110**, a residual vibration waveform, characterized in that not only the frequency becomes extremely low compared with the case of normal ejection, but also the residual vibration is over-damped, is obtained. The reason for this is that when the diaphragm **121** moves upward in FIG. **3** after the diaphragm **121** is attracted downward in FIG. **3** in order to eject ink drops and ink thereby flows into the cavity **141** from the reservoir **143**,

there is no escape for ink within the cavity **141** and the diaphragm **121** suddenly becomes unable to vibrate anymore (is over-damped).

Next, adhesion of paper dust in the vicinity of the outlet of the nozzle **110**, which is still another cause of the missing dot, will be described. FIG. **13** is a conceptual view in the vicinity of the nozzle **110** in the case of adhesion of paper dust in the vicinity of the outlet of the nozzle **110** of FIG. **3**. As is shown in FIG. **13**, in a case where paper dust is adhering in the vicinity of the outlet of the nozzle **110**, not only ink seeps out from the cavity **141** through paper dust, but also it becomes impossible to eject ink through the nozzle **110**. In a case where paper dust is adhering in the vicinity of the outlet of the nozzle **110** and ink seeps out from the nozzle **110** in this manner, a quantity of ink within the cavity **141** when viewed from the diaphragm **121** and ink seeping out is thought to increase compared with the normal state, which in turn causes the inertance m to increase. Also, fibers of the paper dust adhering in the vicinity of the outlet of the nozzle **110** are thought to cause the acoustic resistance r to increase.

Hence, by setting both the inertance m and the acoustic resistance r larger than in the case of FIG. **8** where ink is ejected normally, to be matched with the experiment value of the residual vibration in the case of adhesion of paper dust in the vicinity of the outlet of the nozzle **110**, the result (graph) as shown in FIG. **14** was obtained. As can be understood from the graphs of FIG. **8** and FIG. **14**, in a case where paper dust is adhering in the vicinity of the outlet of the nozzle **110**, a residual vibration waveform, characterized in that the frequency becomes lower than in the case of normal ejection, is obtained (it is also understood from the graphs of FIG. **12** and FIG. **14** that in the case of adhesion of paper dust, the frequency of the residual vibration is higher than in the case of thickening ink). FIG. **15** shows pictures of the states of the nozzle **110** before and after adhesion of paper dust. It can be seen from FIG. **15(b)** that once paper dust adheres in the vicinity of the outlet of the nozzle **110**, ink seeps out along the paper dust.

Note that in both the cases where ink has thickened by drying in the vicinity of the nozzle **110** and where paper dust is adhering in the vicinity of the outlet of the nozzle **110**, the frequency of the damped vibration is lower than in the case where ink drops are ejected normally. Hence, a comparison is made, for example, with the frequency or the cycle (period) of the damped vibration, or with a predetermined threshold in the phase to identify these two causes of the missing dot (non-ejection of ink: ejection failure) from the waveform of the residual vibration of the diaphragm **121**, or alternatively the causes can be identified from a change of the cycle of the residual vibration (damped vibration) or the damping rate of a change in amplitude. In this manner, an ejection failure of the respective ink jet heads **100** can be detected from a change of the residual vibration of the diaphragm **121**, in particular, a change of the frequency thereof, when ink drops are ejected through the nozzles **110** of the respective ink jet heads **100**. Also, by comparing the frequency of the residual vibration in this case with the frequency of the residual vibration in the case of normal ejection, the cause of the ejection failure can be identified.

The ejection failure detecting device **10** will now be described. FIG. **16** is a schematic block diagram of the ejection failure detecting device **10** shown in FIG. **3**. As is shown in FIG. **16**, the ejection failure detecting device **10** is provided with residual vibration detecting means (device) **16** comprising an oscillation circuit **11**, an F/V (frequency-to-voltage) converting circuit **12**, and a waveform shaping

circuit **15**, measuring means (device) **17** for measuring the cycle or amplitude from the residual vibration waveform data detected in the residual vibration detecting device **16**, and judging means (device) **20** for judging an ejection failure of the ink jet head **100** on the basis of the cycle or the like measured by the measuring device **17**. In the ejection failure detecting device **10**, the residual vibration detecting device **16** detects the vibration waveform, which is formed in the F/V converting circuit **12** and the waveform shaping circuit **15** from the oscillation frequency of the oscillation circuit **11** that oscillates on the basis of the residual vibration of the diaphragm **121** of the electrostatic actuator **120**. The measuring device **17** then measures the cycle or the like of the residual vibration on the basis of the vibration waveform thus detected, and the judging device **20** detects and judges an ejection failure of the respective ink jet heads **100** provided to the respective head units **35** in the print device **3**, on the basis of the cycle or the like of the residual vibration thus measured. In the following, respective components of the ejection failure detecting device **10** will be described.

First, a method of using the oscillation circuit **11** to detect the frequency (the number of vibration) of the residual vibration of the diaphragm **121** of the electrostatic actuator **120** will be described. FIG. **17** is a conceptual view in a case where a parallel plate capacitor is used as the electrostatic actuator **120** of FIG. **3**. FIG. **18** is a circuit diagram of the oscillation circuit **11** including a capacitor comprising the electrostatic actuator **120** of FIG. **3**. The oscillation circuit **11** shown in FIG. **18** is a CR oscillation circuit using the hysteresis characteristic of a schmitt trigger; however, in the invention, the oscillation circuit is not limited to such a CR oscillation circuit, and any oscillation circuit can be used provided that it is an oscillation circuit using electric capacitance components (capacitor C) of the actuator (including the diaphragm). The oscillation circuit **11** may comprise, for example, the one using an LC oscillation circuit. Also, this embodiment describes an example case using a schmitt trigger inverter; however, a CR oscillation circuit using inverters in three stages may be formed.

In the ink jet head **100** shown in FIG. **3**, as has been described above, the diaphragm **121** and the segment electrode **122** spaced apart therefrom by an extremely small interval (clearance) together form the electrostatic actuator **120** that forms the counter electrodes. The electrostatic actuator **120** can be deemed as the parallel plate capacitor as shown in FIG. **17**. Let C be the electric capacitance of the capacitor, S be the surface area of each of the diaphragm **121** and the segment electrode **122**, g be a distance (gap length) between the two electrodes **121** and **122**, and ϵ be a dielectric constant of the space (clearance) sandwiched by both electrodes (given ϵ_0 as a dielectric constant in vacuum and ϵ_r as a specific dielectric constant in the clearance, then $\epsilon = \epsilon_0 \cdot \epsilon_r$), then an electric capacitance C(x) of the capacitor (electrostatic actuator **120**) shown in FIG. **17** can be expressed by the following equation.

(Mathematical Expression 4)

$$C(x) = \epsilon_0 \cdot \epsilon_r \frac{S}{g-x} \quad (F) \quad (4)$$

As is shown in FIG. **17**, x in Equation (4) above indicates a displacement quantity of the diaphragm **121** from the reference position thereof, caused by the residual vibration of the diaphragm **121**.

As can be understood from Equation (4) above, the smaller the gap length g (gap length g—displacement quantity x), the larger the electric capacitance C(x) becomes, and conversely, the larger the gap length g (gap length g—displacement quantity x), the smaller the electric capacitance C(x) becomes. In this manner, the electric capacitance C(x) is inversely proportional to (gap length g—displacement quantity x)(the gap length g when x is 0). For the electrostatic actuator **120** shown in FIG. **3**, a specific dielectric constant, $\epsilon_r=1$, because the clearance is fully filled with air.

Also, because ink drops (ink dots) to be ejected become finer with an increase of the resolution of the droplet ejection apparatus (the ink jet printer **1** in this embodiment), the electrostatic actuator **120** is increased in density and decreased in size. The surface area S of the diaphragm **121** of the ink jet head **100** thus becomes smaller and a smaller electrostatic actuator **120** is assembled. Further, the gap length g of the electrostatic actuator **120** that varies with the residual vibration caused by ink drop ejection is approximately one tenth of the initial gap g_0 . Hence, as can be understood from Equation (4) above, a quantity of change of the electric capacitance of the electrostatic actuator **120** takes an extremely small value.

In order to detect a quantity of change of the electric capacitance of the electrostatic actuator **120** (varies with the vibration pattern of the residual vibration), a method as follows is used, that is, a method of forming an oscillation circuit as the one shown in FIG. **18** on the basis of the electric capacitance of the electrostatic actuator **120**, and analyzing the frequency (cycle) of the residual vibration on the basis of the oscillation signal. The oscillation circuit **11** shown in FIG. **18** comprises a capacitor (C) composed of the electrostatic actuator **120**, a schmitt trigger inverter **111**, and a resistor element (R) **112**.

When an output signal from the schmitt trigger inverter **111** is in the high level, the capacitor C is charged via the resistor element **112**. When the charged voltage in the capacitor C (a potential difference between the diaphragm **121** and the segment electrode **122**) reaches an input threshold voltage V_{T+} of the schmitt trigger inverter **111**, the output signal from the schmitt trigger inverter **111** inverts to a low level. Then, when the output signal from the schmitt trigger inverter **111** shifts to the low level, charges charged in the capacitor C via the resistor element **112** are discharged. The voltage of the capacitor C reaches the input threshold voltage V_{T-} of the schmitt trigger inverter **111** through this discharge, and the output signal from the schmitt trigger inverter **111** inverts again to the high level. Thereafter, this oscillation operation is performed repetitively.

In order to detect a change with time of the electric capacitance of the capacitor C in each of the aforementioned phenomena (intrusion of an air bubble, drying, adhesion of paper dust, and normal ejection), the oscillation frequency of the oscillation circuit **11** has to be set to an oscillation frequency at which the frequency in the case of intrusion of an air bubble (see FIG. **10**), where the frequency of the residual vibration is the highest, can be detected. For this reason, the oscillation frequency of the oscillation circuit **11** has to be increased, for example, to a few or several tens of times or more than the frequency of the residual vibration to be detected, that is, it has to be one or more orders of magnitude higher than the frequency in the case of intrusion of an air bubble. In this case, it is preferable to set the oscillation frequency to an oscillation frequency at which the residual vibration frequency in the case of intrusion of an air bubble can be detected, because the frequency of the

residual vibration in the case of intrusion of an air bubble shows a high frequency in comparison with the case of normal ejection. Otherwise, the frequency of the residual vibration cannot be detected accurately for the phenomenon of the ejection failure. In this embodiment, therefore, a time constant of the CR of the oscillation circuit **11** is set in response to the oscillation frequency. By setting the oscillation frequency of the oscillation circuit **11** high in this manner, it is possible to detect the residual vibration waveform accurately on the basis of a minute change of the oscillation frequency.

The digital information for each oscillation frequency can be obtained for the residual vibration waveform by counting pulses of the oscillation signal outputted from the oscillation circuit **11** in every cycle (pulse) of the oscillation frequency with the use of a measuring count pulse (counter), and by subtracting a count quantity of the pulses of the oscillation frequency when the oscillation circuit **11** is oscillated with an electric capacitance of the capacitor C at the initial gap go from the count quantity thus measured. By performing D/A (digital-to-analog) conversion on the basis of the digital information, a schematic residual vibration waveform can be generated. The method as described above may be used; however, the measuring count pulse (counter) of a type having a high frequency (high resolution) that can measure a minute change of the oscillation frequency is needed. Such a count pulse (counter) increases the cost, and for this reason, the ejection failure detecting device **10** uses the F/V converting circuit **12** shown in FIG. **19**.

FIG. **19** is a circuit diagram of the F/V converting circuit **12** in the ejection failure detecting device **10** shown in FIG. **16**. As is shown in FIG. **19**, the F/V converting circuit **12** comprises three switches SW**1**, SW**2**, and SW**3**, two capacitors C**1** and C**2**, a resistor element R**1**, a constant current source **13** from which a constant current Is is outputted, and a buffer **14**. The operation of the F/V converting circuit **12** will be described with the use of the timing chart of FIG. **20** and the graph of FIG. **21**.

First, a method of generating a charging signal, a hold signal, and a clear signal shown in the timing chart of FIG. **20** will be described. The charging signal is generated in such a manner that a fixed time tr is set from the rising edge of the oscillation pulse of the oscillation circuit **11** and the signal remains in the high level for the fixed time tr. The hold signal is generated in such a manner that the signal rises in sync with the rising edge of the charging signal, and falls to the low level after it is held in the high level for a predetermined fixed time. The clear signal is generated in such a manner that the signal rises in sync with the falling edge of the hold signal and falls to the low level after it is held in the high level for a predetermined fixed time. As will be described below, because charges move from the capacitor C**1** to the capacitor C**2** and the capacitor C**1** discharges instantaneously, in regard to pulses of the hold signal and the clear signal, it is sufficient for each signal to include one pulse until the following rising edge of the output signal from the oscillation circuit **11** comes, and the rising edge and the falling edge are not limited to those described above.

With reference to FIG. **21**, a setting method of the fixed times tr and t1 in obtaining a sharp waveform (voltage waveform) of the residual vibration will be described. The fixed time tr is adjusted from the cycle of the oscillation pulse oscillated with the electric capacitance C when the electrostatic actuator **120** is at the initial gap length go, and is set so that a charged potential by the charging time t1 is about half the charging range of C**1**. Also, a gradient of the charged potential is set so as not to exceed the charging

range of the capacitor C**1** from a charging time t2 at the position at which the gap length g is the maximum (Max) to a charging time t3 at the position at which the gap length g is minimum (Min). In other words, because the gradient of the charged potential is determined by $dV/dt = I_s/C1$, it is sufficient to set the output constant current Is from the constant current source **13** to an adequate value. By setting the output constant current Is of the constant current source **13** as high as possible within the range, a minute change of the electric capacitance of the capacitor comprising the electrostatic actuator **120** can be detected with high sensitivity, which enables a minute change of the diaphragm **121** of the electrostatic actuator **120** to be detected.

The configuration of the waveform shaping circuit **15** shown in FIG. **16** will now be described with reference to FIG. **22**. FIG. **22** is a circuit diagram showing the circuitry of the waveform shaping circuit **15** of FIG. **16**. The waveform shaping circuit **15** outputs the residual vibration waveform to the judging device **20** in the form of a rectangular wave. As is shown in FIG. **22**, the waveform shaping circuit **15** comprises two capacitors C**3** (DC component removing means) and C**4**, two resistor elements R**2** and R**3**, two direct current voltage sources Vref**1** and Vref**2**, an operational amplifier **151**, and a comparator **152**. The waveform shaping circuit **15** may be configured to measure the amplitude of the residual vibration waveform by outputting a wave height value detected in the waveform shaping processing of the residual vibration waveform intact.

The output from the buffer **14** in the F/V converting circuit **12** includes electric capacitance components of DC components (direct current components) based on the initial gap go of the electrostatic actuator **120**. Because the direct current components vary with each ink jet head **100**, the capacitor C**3** is used to remove the direct current components of the electric capacitance. The capacitor C**3** thus removes the DC components from an output signal from the buffer **14**, and outputs only the AC components of the residual vibration to the inverting input terminal of the operational amplifier **151**.

The operational amplifier **151** inverts and amplifies the output signal from the buffer **14** in the F/V converting circuit **12**, from which the direct current components have been removed, and also forms a low-pass filter to remove a high band of the output signal. The operational amplifier **151** is assumed to be a single power source circuit. The operational amplifier **151** forms an inverting amplifier from the two resistor elements R**2** and R**3**, and the residual vibration (alternating current components) inputted therein is therefore amplified by a factor of $-R3/R2$.

Also, because of the single power source operation, the operational amplifier **151** outputs an amplified residual vibration waveform of the diaphragm **121** that vibrates about the potential set by the direct current voltage source Vref**1** connected to the non-inverting input terminal thereof. Here, the direct current voltage source Vref**1** is set to about half the voltage range within which the operational amplifier **151** is operable with a single power source. Further, the operational amplifier **151** forms a low-pass filter, having a cut-off frequency of $1/(2\pi \times C4 \times R3)$, from the two capacitors C**3** and C**4**. Then, as is shown in the timing chart of FIG. **20**, the residual vibration waveform of the diaphragm **121**, which is amplified after the direct current components are removed therefrom, is compared with the potential of the other direct current voltage source Vref**2** in the comparator **152** in the following stage, and the comparison result is outputted from the waveform shaping circuit **15** in the form of a rectangular

wave. The direct current voltage source V_{ref1} may be used commonly as the other direct current voltage source V_{ref2} .

The operations of the F/V converting circuit **12** and the waveform shaping circuit **15** of FIG. **19** will now be described with reference to the timing chart shown in FIG. **20**. The F/V converting circuit **12** shown in FIG. **19** operates according to the charging signal, the clear signal, and the hold signal generated as described above. Referring to the timing chart of FIG. **20**, when the driving signal of the electrostatic actuator **120** is inputted into the ink jet head **100** via the head driver **33**, the diaphragm **121** of the electrostatic actuator **120** is attracted toward the segment electrode **122** as shown in FIG. **6(b)**, and abruptly contracts upward in FIG. **6** in sync with the falling edge of the driving signal (see FIG. **6(c)**).

A driving/detection switching signal that switches between the driving circuit **18** and the ejection failure detecting device **10** shifts to the high level in sync with the falling edge of the driving signal. The driving/detection switching signal is held in the high level during the driving halt period of the corresponding ink jet head **100**, and shifts to the low level before the following driving signal is inputted. While the driving/detection switching signal remains in the high level, the oscillation circuit **11** of FIG. **18** keeps oscillating while changing the oscillation frequency in response to the residual vibration of the diaphragm **121** of the electrostatic actuator **120**.

As has been described, the charging signal is held in the high level from the falling edge of the driving signal, that is, the rising edge of the output signal from the oscillation circuit **11** until the elapse of the fixed time t_r , which is set in advance so that the waveform of the residual vibration will not exceed the chargeable range of the capacitor **C1**. It should be noted that the switch **SW1** remains OFF while the charging signal is held in the high level.

When the fixed time t_r elapses and the charging signal shifts to the low level, the switch **SW1** is switched ON in sync with the falling edge of the charging signal (see FIG. **19**). The constant current source **13** and the capacitor **C1** are then connected to each other, and the capacitor **C1** is charged with the gradient $I_s/C1$ as described above. That is, the capacitor **C1** is kept charged while the charging signal remains in the low level, that is, until it shifts to the high level in sync with the rising edge of the following pulse of the output signal from the oscillation circuit **11**.

When the charging signal shifts to the high level, the switch **SW1** is switched OFF (opens), and the constant current source **13** is isolated from the capacitor **C1**. In this instance, the capacitor **C1** holds a potential charged during the period t_1 during which the charging signal remained in the low level (that is, ideally speaking, $I_s \times t_1 / C1(V)$). When the hold signal shifts to the high level in this state, the switch **SW2** is switched ON (see FIG. **19**), and the capacitor **C1** and the capacitor **C2** are connected to each other via the resistor element **R1**. After the switch **SW2** is connected, charging and discharging are performed due to a charged potential difference between the two capacitors **C1** and **C2**, and the charges move from the capacitor **C1** to the capacitor **C2** so that the potential differences in the two capacitors **C1** and **C2** become almost equal.

Herein, the electric capacitance of the capacitor **C2** is set to approximately one tenth or less of the electric capacitance of the capacitor **C1**. For this reason, a quantity of charges that move (are used) due to the charging and discharging caused by a potential difference between the two capacitors **C1** and **C2** is one tenth or less of the charges charged in the capacitor **C1**. Hence, after the charges moved from the

capacitor **C1** to the capacitor **C2**, a potential difference in the capacitor **C1** varies little (drops little). In the F/V converting circuit **12** of FIG. **19**, a primary low-pass filter is formed from the resistor element **R1** and the capacitor **C2** in preventing the charged potential from rising abruptly by the inductance or the like of the wiring in the F/V converting circuit **12** when the capacitor **C2** is charged.

After the charged potential, which is almost equal to the charged potential in the capacitor **C1**, is held in the capacitor **C2**, the hold signal shifts to the low level, and the capacitor **C1** is isolated from the capacitor **C2**. Further, when the clear signal shifts to the high level and the switch **SW3** is switched ON, the capacitor **C1** is connected to the ground **GND**, and a discharge operation is performed so that the charges charged in the capacitor **C1** is reduced to 0. After the capacitor **C1** is discharged, the clear signal shifts to the low level, and the switch **SW3** is switched OFF, in response to which the electrode of the capacitor **C1** at the top in FIG. **19** is isolated from the ground **GND**, and stands by until the following charging signal is inputted, that is, until the charging signal shifts to the low level.

The potential held in the capacitor **C2** is updated at each rising time of the charging signal, that is, at each timing at which the charging to the capacitor **C2** is completed, and is outputted to the waveform shaping circuit **15** of FIG. **22** in the form of the residual vibration waveform of the diaphragm **121** via the buffer **14**. Hence, by setting the electric capacitance of the electrostatic actuator **120** (in this case, a variation width of the electric capacitance due to the residual vibration has to be taken into account) and the resistance value of the resistor element **112** so that the oscillation frequency of the oscillation circuit **11** becomes high, each step (step difference) in the potential in the capacitor **C2** (output from the buffer **14**) shown in the timing chart of FIG. **20** can be more in detail, which enables a change with time of the electric capacitance due to the residual vibration of the diaphragm **121** to be detected more in detail.

Thereafter, the charging signal repetitively shifts to the low level \rightarrow high level \rightarrow low level and so forth, and the potential held in the capacitor **C2** is outputted at the predetermined timing to the waveform shaping circuit **15** via the buffer **14**. In the waveform shaping circuit **15**, the direct current components are removed by the capacitor **C3** from the voltage signal (the potential in the capacitor **C2** in the timing chart of FIG. **20**) inputted from the buffer **14**, and the resulting signal is inputted into the inverting input terminal of the operational amplifier **151** via the resistor element **R2**. The alternating current (AC) components of the residual vibration thus inputted are inverted and amplified in the operational amplifier **151**, and outputted to one input terminal of the comparator **152**. The comparator **152** compares the potential (reference voltage) set in advance by the direct current voltage source V_{ref2} with the potential of the residual vibration waveform (alternating current components), and outputs a rectangular wave (output from the comparator in the timing chart of FIG. **20**).

The switching time between an ink drop ejection operation (driving) and an ejection failure detection operation (driving halt) of the ink jet head **100** will now be described. FIG. **23** is a block diagram schematically showing the switching device **23** switching between the driving circuit **18** and the ejection failure detecting device **10**. Referring to FIG. **23**, the driving circuit **18** in the head driver **33** shown in FIG. **16** will be described as the driving circuit of the ink jet head **100**. As is shown in the timing chart of FIG. **20**, the ejection failure detection processing is performed in a period

between the driving signals of the ink jet head 100, that is, during the driving halt period.

Referring to FIG. 23, the switching device 23 is initially connected to the driving circuit 18 side to drive the electrostatic actuator 120. As has been described, when the driving signal (voltage signal) is inputted from the driving circuit 18 to the diaphragm 121, the electrostatic actuator 120 starts to be driven, and the diaphragm 121 is attracted toward the segment electrode 122. Then, when the applied voltage drops to 0, the diaphragm 121 displaces abruptly in a direction to move away from the segment electrode 122 and starts to vibrate (residual vibration). In this instance, ink drops are ejected through the nozzle 110 of the ink jet head 100.

When the pulse of the driving signal falls, the driving/detection switching signal is inputted into the switching device 23 in sync with the falling edge thereof (see the timing chart of FIG. 20), and the switching device 23 is switched from the driving circuit 18 to the ejection failure detecting device (detection circuit) 10 side, so that the electrostatic actuator 120 (used as the capacitor of the oscillation circuit 11) is connected to the ejection failure detecting device 10.

Then, the ejection failure detecting device 10 performs the detection processing of an ejection failure (missing dot) as described above, and converts the residual vibration waveform data (rectangular wave data) of the diaphragm 121 outputted from the comparator 152 in the waveform shaping circuit 15 into numerical forms, such as the cycle or the amplitude of the residual vibration waveform, with the use of the measuring device 17. In this embodiment, the measuring device 17 measures a particular vibration cycle from the residual vibration waveform data, and outputs the measurement result (numerical value) to the judging device 20.

To be more specific, in order to measure a time (cycle of the residual vibration) from the first rising edge to the following rising edge of the waveform (rectangular wave) of the output signal from the comparator 152, the measuring device 17 counts the pulses of the reference signal (predetermined frequency) with the use of an unillustrated counter, and measures the cycle (particular vibration cycle) of the residual vibration from the count value. Alternatively, the measuring device 17 may measure a time from the first rising edge to the following falling edge, and output a time two times longer than the measured time to the judging device 20 as the cycle of the residual vibration. Hereinafter, the cycle of the residual vibration obtained in either manner is referred to as T_w .

The judging device 20 judges the presence or absence of an ejection failure of the nozzle, the cause of the ejection failure, a comparative deviation, etc. on the basis of the particular vibration cycle (measurement result) of the residual vibration waveform measured by the measuring device 17, and outputs the judgment result to the control portion 6. The control portion 6 then saves the judgment result in a predetermined storage region of the EEPROM (storage means) 62. The driving/detection switching signal is inputted into the switching device 23 again at the timing at which the following driving signal from the driving circuit 18 is inputted, and the driving circuit 18 and the electrostatic actuator 120 are thereby connected to each other. Because the driving circuit 18 holds the ground (GND) level once the driving voltage is applied thereto, the switching device 23 performs the switching as described above (see the timing chart of FIG. 20). It is thus possible to detect the residual vibration waveform of the diaphragm 121 of the electrostatic

actuator 120 accurately without being influenced by a disturbance or the like from the driving circuit 18.

In the invention, the residual vibration waveform data is not limited to that made into a rectangular wave by the comparator 152. For example, it may be arranged in such a manner that the residual vibration amplitude data outputted from the operational amplifier 151 is converted into numerical forms as needed in the measuring device 17 that performs the A/D (analog-to-digital) conversion, without performing the comparison processing by the comparator 152, then the presence or absence of an ejection failure or the like is judged by the judging device 20 on the basis of the data converted into the numerical forms in this manner, and the judgment result is stored into the storage device 62.

Also, because the meniscus (the surface on which ink within the nozzle 110 comes in contact with air) of the nozzle 110 vibrates in sync with the residual vibration of the diaphragm 121, the ink jet head 100 waits for the residual vibration of the meniscus to be damped by the acoustic resistance r in almost a determined time after the ink drops ejection operation (stand by for a predetermined time), and then starts the following ejection operation. In the invention, because the residual vibration of the diaphragm 121 is detected by effectively using this stand-by time, detection of an ejection failure can be performed without influencing the driving of the ink jet head 100. In other words, it is possible to perform the ejection failure detection processing of the nozzle 110 of the ink jet head 100 without reducing the throughput of the ink jet printer 1 (droplet ejection apparatus).

As has been described, in a case where an air bubble has intruded inside the cavity 141 of the ink jet head 100, because the frequency becomes higher than that of the residual vibration waveform of the diaphragm 121 in the case of normal ejection, the cycle thereof conversely becomes shorter than the cycle of the residual vibration in the case of normal ejection. Also, in a case where ink has thickened or fixed by drying in the vicinity of the nozzle 110, the residual vibration is over-damped. Hence, because the frequency becomes extremely low in comparison with the residual vibration waveform in the case of normal ejection, the cycle thereof becomes markedly longer than the cycle of the residual vibration in the case of normal ejection. Also, in a case where paper dust is adhering in the vicinity of the outlet of the nozzle 110, the frequency of the residual vibration is lower than the frequency of the residual vibration in the case of normal ejection and higher than the frequency of the residual vibration in the case of drying/thickening of ink. Hence, the cycle thereof becomes longer than the cycle of the residual vibration in the case of normal ejection and shorter than the cycle of the residual vibration in the case of drying of ink.

Hence, by setting a predetermined range T_r (upper limit T_{r1} , lower limit T_{r2}) as the cycle of the residual vibration in the case of normal ejection, and by setting a predetermined threshold T_1 to differentiate the cycle of the residual vibration in a case where paper dust is adhering to the outlet of the nozzle 110 from the cycle of the residual vibration in a case where ink has dried in the vicinity of the outlet of the nozzle 110, it is possible to determine the cause of such an ejection failure of the ink jet head 100. The judging device 20 judges the cause of an ejection failure depending on whether the cycle T_w of the residual vibration waveform detected in the ejection failure detection processing described above is a cycle within the predetermined range, and longer than the predetermined threshold.

The operation of the droplet ejection apparatus of the invention will now be described on the basis of the configuration of the ink jet printer **1** as described above. Firstly, the ejection failure detection processing (including the driving/detection switching processing) for the nozzle **110** of one ink jet head **100** will be described. FIG. **24** is a flowchart detailing the ejection failure detection and judgment process. When print data to be printed (or ejection data used for the flushing operation) is inputted into the control portion **6** from the host computer **8** via the interface (IF) **9**, the ejection failure detection processing is performed at the predetermined timing. In the flowchart shown in FIG. **24**, the ejection failure detection processing corresponding to an ejection operation of one ink jet head **100**, that is one nozzle **110**, will be detailed for ease of explanation.

Initially, the driving signal corresponding to the print data (ejection data) is inputted from the driving circuit **18** of the head driver **33**, in response to which the driving signal (voltage signal) is applied between both electrodes of the electrostatic actuator **120** according to the timing of the driving signal as shown in the timing chart of FIG. **20** (Step **S101**). The control portion **6** then judges whether the ink jet head **100** that has ejected ink drops is in a driving halt period on the basis of the driving/detection switching signal (Step **S102**). At this point, the driving/detection switching signal shifts to the high level in sync with the falling edge of the driving signal (see FIG. **20**), and is inputted into the switching device **23** from the control portion **6**.

When the driving/detection switching signal is inputted into the switching device **23**, the electrostatic actuator **120**, that is, the capacitor forming the oscillation circuit **11**, is isolated from the driving circuit **18** by the switching device **23**, and is connected to the ejection failure detecting device **10** (detection circuit) side, that is, to the oscillation circuit **11** of the residual vibration detecting device **16** (Step **S103**). Subsequently, the residual vibration detection processing described below is performed (Step **S104**), and the measuring device **17** measures the predetermined numerical value from the residual vibration waveform data detected in the residual vibration detection processing (Step **S105**). In this instance, the measuring device **17** measures the cycle of the residual vibration from the residual vibration waveform data as described above.

Subsequently, the ejection failure judgment processing described below is performed by the judging device **20** on the basis of the measurement result by the measuring device (Step **S106**), and the judgment result is saved in the predetermined storage region in the EEPROM (storage means) **62** of the control portion **6** (Step **S107**). In subsequent Step **S108**, whether the ink jet head **100** is in the driving period is judged. In other words, whether the driving halt period has ended and the following driving signal is inputted is judged, and the flow is suspended in Step **S108** until the following driving signal is inputted.

When the driving/detection switching signal shifts to the low level in sync with the rising edge of the driving signal at the timing at which the following driving signal is inputted (YES in Step **S108**), the switching device **23** switches the connection of the electrostatic actuator **120** from the ejection failure detecting device (detection circuit) **10** to the driving circuit **18** (Step **S109**), and ends the ejection failure detection processing.

The flowchart shown in FIG. **24** shows a case where the measuring device **17** measures the cycle from the residual vibration waveform detected in the residual vibration detection processing (the residual vibration detecting device **16**); however, the invention is not limited to this case. For

example, the measuring device **17** may measure a phase difference or amplitude of the residual vibration waveform from the residual vibration waveform data detected in the residual vibration detection processing.

The residual vibration detection processing (sub routine) in Step **S104** of the flowchart shown in FIG. **24** will now be described. FIG. **25** is a flowchart detailing the residual vibration detection processing. When the electrostatic actuator **120** and the oscillation circuit **11** are connected to each other by the switching device **23** as described above (Step **S103** of FIG. **24**), the oscillation circuit **11** forms a CR oscillation circuit, and starts to oscillate in response to the change of the electric capacitance of the electrostatic actuator **120** (residual vibration of the diaphragm **121** of the electrostatic actuator **120**) (Step **S201**).

As is shown in the timing chart described above, the charging signal, the hold signal, and the clear signal are generated in the F/V converting circuit **12** according to the output signal (pulse signal) from the oscillation circuit **11**, and the F/V conversion processing is performed according to these signals by the F/V converting circuit **12**, by which the frequency of the output signal from the oscillation circuit **11** is converted into a voltage (Step **S202**), and the residual vibration waveform data of the diaphragm **121** is outputted from the F/V converting circuit **12**. The DC components (direct current components) are removed from the residual vibration waveform data outputted from the F/V converting circuit **12** in the capacitor **C3** of the waveform shaping circuit **15** (Step **S203**), and the residual vibration waveform (AC components) from which the DC components have been removed is amplified in the operational amplifier **151** (Step **S204**).

The residual vibration waveform data after the amplification is subjected to waveform shaping in the predetermined processing and converted into pulses (Step **S205**). In other words, in this embodiment, the voltage value (predetermined voltage value) set by the direct current voltage source **Vref2** is compared with the output voltage from the operational amplifier **151** in the comparator **152**. The comparator **152** outputs the binarized waveform (rectangular wave) on the basis of the comparison result. The output signal from the comparator **152** is the output signal from the residual vibration detecting device **16**, and is outputted to the measuring device **17** for the ejection failure judgment processing to be performed, upon which the residual vibration detection processing is completed.

The ejection failure judgment processing (sub routine) in Step **S106** of the flowchart shown in FIG. **24** will now be described. FIG. **26** is a flowchart detailing the ejection failure judgment processing performed by the control portion **6** and the judging device **20**. The judging device **20** judges whether ink drops were ejected normally from the corresponding ink jet head **100** on the basis of the measurement data (measurement result), such as the cycle, measured by the measuring device **17** described above, and when ink drops were not ejected normally, that is, in the case of an ejection failure, it further judges the cause thereof.

Initially, the control portion **6** outputs the predetermined range **Tr** of the cycle of the residual vibration and the predetermined threshold **T1** of the cycle of the residual vibration saved in the EEPROM **62** to the judging device **20**. The predetermined range **Tr** of the cycle of residual vibration is the residual vibration cycle in the case of normal ejection given with an allowance (upper limit **Tru**, lower limit **Trl**) for the cycle to be judged as normal. The data is stored in an unillustrated memory of the judging device **20**, and the processing as follows is performed.

The measurement result measured in the measuring device 17 in Step S105 of FIG. 24 is inputted into the judging device 20 (Step S301). In this embodiment, the measurement result is the cycle Tw of the residual vibration of the diaphragm 121.

In Step S302, the judging device 20 judges whether the cycle Tw of the residual vibration is present, that is, whether the ejection failure detecting device 10 failed to obtain the residual vibration waveform data. Upon judging the absence of the cycle Tw of the residual vibration, the judging device 20 judges that the nozzle 110 of the ink jet head 100 in question is a not-yet-ejected nozzle that did not eject ink drops in the ejection failure detection processing (Step S306). Also, upon judging the presence of the residual vibration waveform data, the judging device 20 judges, in the following Step S303, whether the cycle Tw is within the predetermined range Tr that can be deemed as the cycle in the case of normal ejection.

When it is judged that the cycle Tw of the residual vibration is within the predetermined range Tr, it means that ink drops were ejected normally from the corresponding ink jet head 100. Hence, the judging device 20 judges that the nozzle 110 of the ink jet head 100 in question normally ejected ink drops (normal ejection) (Step S307). Also, when it is judged that the cycle Tw of the residual vibration is not within the predetermined range Tr, the judging device 20 judges, in the following Step S304, whether the cycle Tw of the residual vibration is shorter than the lower limit Tr1.

When it is judged that the cycle Tw of the residual vibration is shorter than the lower limit Tr1, it means that the frequency of the residual vibration is high and an air bubble is thought to have intruded inside the cavity 141 of the ink jet head 100 as described above. Hence, the judging device 20 judges that an air bubble has intruded inside the cavity 141 of the ink jet head 100 in question (intrusion of an air bubble) (Step S308).

When it is judged that the cycle Tw of the residual vibration is longer than the upper limit Tru, the judging device 20 subsequently judges whether the cycle Tw of the residual vibration is longer than the predetermined threshold T1 (Step S305). When it is judged that the cycle Tw of the residual vibration is longer than the predetermined threshold T1, the residual vibration is thought to be over-damped. Hence, the judging device 20 judges that ink has thickened by drying in the vicinity of the nozzle 110 of the ink jet head 100 in question (drying) (Step S309).

When it is judged that the cycle Tw of the residual vibration is shorter than the predetermined threshold T1 in Step S305, the cycle Tw of the residual vibration takes a value that falls within the range satisfying the relation, $Tru < Tw < T1$, and as has been described above, paper dust is thought to be adhering in the vicinity of the outlet of the nozzle 110, in case of which the frequency is higher than in the case of drying. Hence, the judging device 20 judges that paper dust is adhering in the vicinity of the outlet of the nozzle 110 of the ink jet head 100 in question (adhesion of paper dust) (Step S310).

When normal ejection or the cause of an ejection failure of the target ink jet head 100 is judged by the judging device 20 (Steps S306 through S310) in this manner, the judgment result is outputted to the control portion 6, upon which the ejection failure judgment processing is completed.

On the assumption of the ink jet printer 1 provided with a plurality of ink jet heads (droplet ejection heads) 100, that is, a plurality of nozzles 110, ejection selecting means (nozzle selector) 182 of the ink jet printer 1 and the detection

and judgment timing of an ejection failure for the respective ink jet heads 100 will now be described.

In the following, of a plurality of head units 35 provided to the print device 3, one head unit 35 will be described for ease of explanation, and it is assumed that the head unit 35 is provided with five ink jet heads 100a through 100e (that is, five nozzles 110). However, in the invention, the number of the head units 35 provided to the print device 3 and the number of the ink jet heads 100 (nozzles 110) provided to each head unit 35 are both arbitrary.

FIG. 27 through FIG. 30 are block diagrams showing some examples of the detection and judgment timing of an ejection failure in the ink jet printer 1 provided with the ejection selecting means (device) 182. Examples of the configuration in the respective drawings will now be described one by one.

FIG. 27 shows one example of detection timing of an ejection failure for a plurality of (five) ink jet heads 100a through 100e (in a case where there is one ejection failure detecting device 10). As is shown in FIG. 27, the ink jet printer 1 having a plurality of ink jet heads 100a through 100e is provided with driving waveform generating means (device) 181 for generating a driving waveform, ejection selecting means 182 capable of selecting from which nozzle 110 ink drops are to be ejected, and a plurality of ink jet heads 100a through 100e selected by the ejection selecting means 182 and driven by the driving waveform generating means 181. Because the configuration of FIG. 27 is the same as those shown in FIG. 2, FIG. 16, and FIG. 23 except for the aforementioned configuration, the description of the same portion is omitted.

In this example, the driving waveform generating means 181 and the ejection selection means 182 are described as they are included in the driving circuit 18 of the head driver 33 (they are indicated as two blocks via the switching device 23 in FIG. 27; however, both of them are generally formed inside the head driver 33). The invention, however, is not limited to this configuration. For example, the driving waveform generating means 181 may be provided independently of the head driver 33.

As is shown in FIG. 27, the ejection selecting means 182 is provided with a shift register 182a, a latch circuit 182b, and a driver 182c. Print data (ejection data) outputted from the host computer 8 shown in FIG. 2 and underwent the predetermined processing in the control portion 6 as well as a clock signal (CLK) are sequentially inputted into the shift register 182a. The print data is shifted and inputted sequentially from the first stage to the latter stages in the shift register 182a in response to an input pulse of the clock signal (CLK) (each time the clock signal is inputted), and is then outputted to the latch circuit 182b as print data corresponding to the respective ink jet heads 100a through 100e. In the ejection failure detection processing described below, ejection data used at the time of flushing (preliminary ejection) is inputted instead of the print data. However, the ejection data referred to herein means print data for all the ink jet heads 100a through 100e. Alternatively, a value such that all the outputs from the latch circuit 182b will trigger ejection may be set by hardware at the time of flushing.

The latch circuit 182b latches the respective output signals from the shift register 182a by the latch signal inputted therein after print data corresponding to the number of the nozzles 110 of the head unit 35, that is, the number of the ink jet heads 100, is stored into the shift register 182a. In a case where a CLEAR signal is inputted, the latch state is released, and the output signal from the shift register 182a being latched becomes 0 (output of the latch is stopped), upon

which the print operation is stopped. In a case where no CLEAR signal is inputted, the print data from the shift register **182a** being latched is outputted to the driver **182c**. After the print data outputted from the shift register **182a** is latched in the latch circuit **182b**, the following print data is inputted into the shift register **182a**, so that the latch signal in the latch circuit **182b** is successively updated at the print timing.

The driver **182c** connects the driving waveform generating means **181** to the electrostatic actuators **120** of the respective ink jet heads **100**, and inputs the output signal (driving signal) from the driving waveform generating means **181** to the respective actuators **120** specified (identified) by the latch signal outputted from the latch circuit **182b** (any or all of the electrostatic actuators **120** of the ink jet heads **100a** through **100e**). The driving signal (voltage signal) is thus applied between both electrodes of the electrostatic actuator **120**.

The ink jet printer **1** shown in FIG. **27** is provided with one driving waveform generating means **181** for driving a plurality of ink jet heads **100a** through **100e**, ejection failure detecting device **10** for detecting an ejection failure (ink drops non-ejection) for the ink jet head **100** in any of the respective ink jet heads **100a** through **100e**, storage device **62** for saving (storing) the judgment result, such as the cause of the ejection failure, obtained by the ejection failure detecting device **10**, and one switching device **23** for switching between the driving waveform generating means **181** and the ejection failure detecting device **10**. Hence, in this ink jet printer **1**, one or more of the ink jet heads **100a** through **100e** selected by the driver **182c** is driven according to the driving signal inputted from the driving waveform generating means **181**, and the switching device **23** switches the connection of the electrostatic actuator **120** of the ink jet head **100** from the driving waveform generating means **181** to the ejection failure detecting device **10** when the driving/detection switching signal is inputted into the switching device **23** after the ejection driving operation. Then, the ejection failure detecting device **10** detects whether an ejection failure (ink drops non-ejection) exists in the nozzle **110** of the ink jet head **100** in question as well as judges the cause thereof in the event of ejection failure, on the basis of the residual vibration waveform of the diaphragm **121**.

Also, in the ink jet printer **1**, when an ejection failure is detected and judged for the nozzle **110** of one ink jet head **100**, an ejection failure is detected and judged for the nozzle **110** of the ink jet head **100** specified next, according to the driving signal subsequently inputted from the driving waveform generating means **181**. Thereafter, an ejection failure is detected and judged sequentially for the nozzles **110** of the ink jet heads **100** to be driven by an output signal from the driving waveform generating means **181** in the same manner. Then, as has been described above, when the residual vibration detecting device **16** detects the residual vibration waveform of the diaphragm **121**, the measuring device **17** measures the cycle or the like of the residual vibration waveform on the basis of the waveform data thereof. The judging device **20** then judges normal ejection or an ejection failure on the basis of the measurement result in the measuring device **17**, judges the cause of the ejection failure in the event of ejection failure (head failure), and outputs the judgment result to the storage device **62**.

In this manner, because the ink jet printer **1** shown in FIG. **27** is configured in such a manner that an ejection failure is detected and judged sequentially for the respective nozzles **110** of a plurality of ink jet heads **100a** through **100e** during the ink drop ejection driving operation, it is sufficient to

provide one ejection failure detecting device **10** and one switching device **23**. Also, not only can the circuitry of the ink jet printer **1** capable of detecting and judging an ejection failure be scaled down, but also an increase of the manufacturing costs can be prevented.

FIG. **28** shows one example of detection timing of an ejection failure for a plurality of ink jet heads **100** (in a case where the number of the ejection failure detecting device **10** is equal to the number of the ink jet heads **100**). The ink jet printer **1** shown in FIG. **28** is provided with one ejection selecting means **182**, five ejection failure detecting devices **10a** through **10e**, five switching devices **23a** through **23e**, one driving waveform generating means **181** common for five ink jet heads **100a** through **100e**, and one storage device **62**. Because the respective components have been described with reference to FIG. **27**, the description of these components is omitted and only the connections of these components will be described.

As with the case shown in FIG. **27**, the ejection selecting means **182** latches print data corresponding to the respective ink jet heads **100a** through **100e** in the latch circuit **182b** on the basis of the print data (ejection data) and the clock signal CLK inputted from the host computer **8**, and drives the electrostatic actuators **120** of the ink jet heads **100a** through **100e** corresponding to the print data in response to the driving signal (voltage signal) inputted from the driving waveform generating means **181** into the driver **182c**. The driving/detection switching signal is inputted into the respective switching device **23a** through **23e** corresponding to all the ink jet heads **100a** through **100e**. The switching devices **23a** through **23e** then input the driving signal into the electrostatic actuators **120** of the ink jet heads **100** according to the driving/detection switching signal regardless of the presence or absence of the corresponding print data (ejection data), after which they switch the connection of the ink jet heads **100** from the driving waveform generating means **181** to the ejection failure detecting devices **10a** through **10e**.

After an ejection failure is detected and judged for the respective ink jet heads **100a** through **100e** by all the ejection failure detecting devices **10a** through **10e**, the judgment results for all the ink jet heads **100a** through **100e** obtained in the detection processing are outputted to the storage device **62**. The storage device **62** stores the presence or absence of an ejection failure and the cause of the ejection failure for the respective ink jet heads **100a** through **100e** into the predetermined saving region.

In this manner, in the ink jet printer **1** shown in FIG. **28**, a plurality of ejection failure detecting devices **10a** through **10e** are provided for the respective nozzles **110** of a plurality of ink jet heads **100a** through **100e**, and an ejection failure is detected and the cause thereof is judged by performing the switching operation with the use of a plurality of switching devices **23a** through **23e** corresponding to the ejection failure detecting devices **10a** through **10e**. It is thus possible to detect an ejection failure and judge the cause thereof in a short time for all the nozzles **110** at a time.

FIG. **29** shows an example of detection timing of an ejection failure for a plurality of ink jet heads **100** (in a case where the number of the ejection failure detecting device **10** is equal to the number of the ink jet heads **100**, and detection of an ejection failure is performed in the presence of print data). The ink jet printer **1** shown in FIG. **29** is of the same configuration as that of the ink jet printer **1** shown in FIG. **28** except that switching control means (device) **19** is added (appended). In this example, the switching control device **19** comprises a plurality of AND circuits (logical conjunction

circuits) ANDa through ANDe, and upon input of the print data to be inputted into the respective ink jet heads 100a through 100e and the driving/detection switching signal, it outputs an output signal in the high level to the correspond-
 ing switching devices 23a through 23e. The switching control device 19 is not limited to AND circuits (logical
 conjunction circuits), and it only has to be formed in such a manner that it selects the switching device 23 that corre-
 sponds to an output from the latch circuit 182b selecting the ink jet head 100 to be driven.

The respective switching devices 23a through 23e switch the connection of the electrostatic actuators 120 of the corresponding ink jet heads 100a through 100e from the driving waveform generating means 181 to the correspond-
 ing ejection failure detecting devices 10a through 10e, according to the output signals from the corresponding AND
 circuits ANDa through ANDe of the switching control device 19. To be more specific, when the output signals from the corresponding AND circuits ANDa through ANDe are in
 the high level, in other words, in a case where print data to be inputted into the corresponding ink jet heads 100a
 through 100e is outputted from the latch circuit 182b to the driver 182c while the driving/detection switching signal
 remains in the high level, the switching devices 23a through 23e corresponding to the AND circuits in question switch
 the connections of the corresponding ink jet heads 100a through 100e from the driving waveform generating means
 181 to the ejection failure detecting devices 10a through 10e.

After the presence or absence of an ejection failure for the respective ink jet heads 100 and the cause thereof in the event of ejection failure are detected by the ejection failure
 detecting devices 10a through 10e corresponding to the ink jet heads 100 into which the print data has been inputted, the
 corresponding ejection failure detecting device 10 outputs the judgment results obtained in the detection processing to the
 storage device 62. The storage device 62 stores one or more than one judgment result inputted (obtained) in this manner
 into the predetermined saving region.

In this manner, in the ink jet printer 1 shown in FIG. 29, a plurality of ejection failure detecting devices 10a through 10e are provided to correspond to the respective nozzles 110
 of a plurality of ink jet heads 100a through 100e, and when print data corresponding to the respective ink jet heads 100a
 through 100e is inputted into the ejection selecting means 182 from the host computer 8 via the control portion 6, an
 ejection failure of the ink jet head 100 is detected and the cause thereof is judged by allowing any of the switching
 devices 23a through 23e specified by the switching control device 19 alone to perform the predetermined switching
 operation. Hence, the detection and judgment processing is not performed for the ink jet heads 100 that have not
 performed the ejection driving operation. It is thus possible to avoid useless detection and judgment processing in this
 ink jet printer 1.

FIG. 30 shows one example of the detection timing of an ejection failure for a plurality of ink jet heads 100 (in a case where the number of the ejection failure detecting devices 10
 is equal to the number of the ink jet heads 100, and detection of an ejection failure is performed by making rounds at the respective ink jet heads 100). The ink jet
 printer 1 shown in FIG. 30 is of the same configuration as that of the ink jet printer 1 shown in FIG. 29 except that there
 is one ejection failure detecting device 10 and switching selecting device 19a for scanning the driving/detection

switching signal (identifying the ink jet heads 100 one by one for which the detection and judgment processing is to be performed).

The switching selecting device 19a is connected to the switching control device 19 shown in FIG. 29, and is a selector that scans (selects and switches) the input of the driving/detection switching signal into the AND circuits
 ANDa through ANDe corresponding to a plurality of ink jet heads 100a through 100e, according to a scanning signal
 (selection signal) inputted from the control portion 6. The scanning (selection) order of the switching selecting device
 19a may be the same as the order of print data inputted into the shift register 182a, that is, the order of ejection by a
 plurality of ink jet heads 100; however, it may simply be the order of a plurality of ink jet heads 100a through 100e.

In a case where the scanning order is the order of print data inputted into the shift register 182a, when the print data is inputted into the shift register 182a of the ejection
 selecting means 182, the print data is latched in the latch circuit 182b, and outputted to the driver 182c upon the input
 of the latch signal. The scanning signal to identify the ink jet head 100 corresponding to the print data is inputted into the
 switching selecting device 19a in sync with the input of the print data into the shift register 182a or the input of the latch
 signal into the latch circuit 182b, and the driving/detection switching signal is outputted to the corresponding AND
 circuit. The output terminal of the switching selecting device 19a outputs a low level when no selection is made.

The corresponding AND circuit (switching control device (means) 19) performs the logical operation AND of the print data inputted from the latch circuit 182b and the driving/
 detection switching signal inputted from the switching selecting device 19a, and thereby outputs an output signal in
 the high level to the corresponding switching device 23. Upon input of the output signal in the high level from the
 switching control device 19, the switching device 23 switches the connection of the electrostatic actuator 120 of
 the corresponding ink jet head 100 from the driving waveform generating means 181 to the ejection failure detecting
 device 10.

The ejection failure detecting device 10 then detects an ejection failure of the ink jet head 100 into which the print data has been inputted, and judges the cause thereof in the
 event of ejection failure, after which it outputs the judgment result to the storage device 62. The storage device 62 stores
 the judgment result inputted (obtained) in this manner into the predetermined saving region.

In a case where the scanning order is simply the order of the ink jet heads 100a through 100e, when the print data is inputted into the shift register 182a of the ejection selecting
 means 182, the print data is latched in the latch circuit 182b, and outputted to the driver 182c upon the input of the latch
 signal. The scanning (selection) signal to identify the ink jet head 100 corresponding to the print data is inputted into the
 switching selecting device 19a in sync with the input of the print data into the shift register 182a or the input of the latch
 signal into the latch circuit 182b, and the driving/detection switching signal is outputted to the corresponding AND
 circuit of the switching control device 19.

When the print data corresponding to the ink jet head 100 determined by the scanning signal inputted into the switch-
 ing selecting device 19a is inputted into the shift register 182a, the output signal from the corresponding AND circuit
 (switching control device (means) 19) shifts to the high level, and the switching device 23 switches the connection
 of the corresponding ink jet head 100 from the driving waveform generating means 181 to the ejection failure

detecting device 10. However, when no print data is inputted into the shift register 182a, the output signal from the AND circuit remains in the low level, and the corresponding switching device 23 does not perform the predetermined switching operation. Hence, the ejection failure detection processing of the ink jet head 100 is performed on the basis of the AND of the selection result by the switching selecting device 19a and the result specified by the switching control device 19.

When the switching operation is performed by the switching device 23, the ejection failure detecting device 10 detects an ejection failure of the ink jet head 100 into which the print data has been inputted and judges the cause thereof in the event of ejection failure in the same manner as above, after which it outputs the judgment result to the storage device 62. The storage device 62 stores the judgment result inputted (obtained) in this manner into the predetermined saving region.

When there is no print data corresponding to the ink jet head 100 specified by the switching selecting device 19a, the corresponding switching device 23 does not perform the switching operation as described above, and for this reason, it is not necessary for the ejection failure detecting device 10 to perform the ejection failure detection processing; however, such processing may be performed as well. In a case where the ejection failure detection processing is performed without performing the switching operation, as is detailed in the flowchart of FIG. 26, the judging device 20 of the ejection failure detecting device 10 judges that the nozzle 110 of the corresponding ink jet head 100 as being a not-yet ejected nozzle (Step S306), and stores the judgment result into the predetermined saving region of the storage device 62.

In this manner, the ink jet printer 1 shown in FIG. 30 is different from the ink jet printer 1 shown in FIG. 28 or FIG. 29 in that only one ejection failure detecting device 10 is provided for the respective nozzles 110 of a plurality of ink jet heads 100a through 100e, and because the print data corresponding to the respective ink jet heads 100a through 100e is inputted into the ejection selecting means 182 from the host computer 8 via the control portion 6 while only the switching device 23, corresponding to the ink jet head 100 identified by the scanning (selection) signal to perform the ejection driving operation in response to the print data, performs the switching operation, so that an ejection failure is detected and the cause thereof is judged only for the corresponding ink jet head 100. This eliminates the need to process a large volume of detection results at one time, and thereby reduces the load on the CPU 61 of the control portion 6. Also, because the ejection failure detecting device 10 makes rounds at nozzle states other than the ejection operation, it is possible to keep track of an ejection failure of each nozzle while being driven for printing, and the state of the nozzles 110 in the entire head unit 35 can be known. Because an ejection failure is detected periodically, this can reduce, for example, the steps of detecting an ejection failure nozzle by nozzle while the printing is halted. In view of the foregoing, it is possible to efficiently detect an ejection failure of the ink jet head 100 and judge the cause thereof.

Also, in contrast to the ink jet printer 1 shown in FIG. 28 or FIG. 29, the ink jet printer 1 shown in FIG. 30 only has to be provided with one ejection failure detecting device 10, and in comparison with the ink jet printers 1 shown in FIG. 28 and FIG. 29, not only can the circuitry of the ink jet printer 1 be scaled down, but also an increase of the manufacturing costs can be prevented.

The operations of the ink jet printers 1 shown in FIG. 27 through FIG. 30, that is, the ejection failure detection processing (chiefly, detection timing) in the ink jet printer 1 provided with a plurality of ink jet heads 100, will now be described. In the ejection failure detection and judgment processing (multi-nozzle processing), the residual vibration of the diaphragm 121 when the electrostatic actuators 120 of the respective ink jet heads 100 perform the ink drop ejection operation is detected, and the occurrence of an ejection failure (missing dot, ink drop non-ejection) is judged for the ink jet head 100 in question on the basis of the cycle of the residual vibration; moreover, in the event of a missing dot (ink drop non-ejection), the cause thereof is judged. In this manner, in the invention, when the ejection operation of ink drops (droplets) by the ink jet heads 100 is performed, the detection and judgment processing for the ink jet heads 100 can be performed. However, the ink jet heads 100 eject ink drops not only when the printing (print) is actually performed on a recording sheet P, but also when the flushing operation (preliminary ejection or preparatory ejection) is performed. Hereinafter, the ejection failure detection and judgment processing (multi-nozzle) in these two cases will be described.

The flushing (preliminary ejection) processing referred to herein is defined as a head cleaning operation by which ink drops are ejected through all or only target nozzles 110 of the head unit 35 while a cap not shown in FIG. 1 is attached or in a place where ink drops (droplets) do not reach the recording sheet P (media). The flushing process (flushing operation) is performed, for example, when ink within the cavities 141 is discharged periodically to maintain the viscosity of ink in the nozzles 110 at a value within an adequate range, or as a recovery operation when ink has thickened. Further, the flushing process is also performed when the respective cavities 141 are initially filled with ink after the ink cartridges 31 are attached to the print device 3.

A wiping process (processing by which build-ups (paper dust or dust) adhering on the head surface of the print device 3 are wiped off by a wiper not shown in FIG. 1) may be performed to clean the nozzle plate (nozzle surface) 150. In this instance, however, a negative pressure may be produced inside the nozzles 110 and ink of other colors (droplets of other kinds) may be sucked therein. Hence, the flushing operation is performed after the wiping process in order to force a predetermined quantity of ink drops to be ejected through all the nozzles 110 of the head unit 35. Further, the flushing process may be performed from time to time in order to ensure satisfactory printing by maintaining the meniscus of the nozzles 110 in a normal state.

First, the ejection failure detection and judgment processing during the flushing process will be described with reference to flowcharts shown in FIG. 31 through FIG. 33. These flowcharts will be explained with reference to the block diagrams of FIG. 27 through FIG. 30 (the same can be said in the print operations below). FIG. 31 is a flowchart detailing the detection timing of an ejection failure during the flushing operation by the ink jet printer 1 shown in FIG. 27.

When the flushing process of the ink jet printer 1 is performed at the predetermined timing, the ejection failure detection and judgment processing shown in FIG. 31 is performed. The control portion 6 inputs ejection data for one nozzle into the shift register 182a of the ejection selecting means 182 (Step S401), then the latch signal is inputted into the latch circuit 182b (Step S402), and the ejection data is thus latched. In this instance, the switching device 23 connects the electrostatic actuator 120 of the ink jet head

100, the target of the ejection data, to the driving waveform generating means **181** (Step S403).

Subsequently, the ejection failure detection and judgment processing detailed in the flowchart of FIG. 24 is performed for the ink jet head **100** that has performed the ink ejection operation, by the ejection failure detecting device **10** (Step S404). In Step S405, the control portion **6** judges whether the ejection failure detection and judgment processing has been completed for all the nozzles **110** of the ink jet heads **100a** through **100e** in the ink jet printer **1** shown in FIG. 27, on the basis of the ejection data outputted to the ejection selecting means **182**. Upon judging that the processing is not completed for all the nozzles **110**, the control portion **6** inputs the ejection data corresponding to the nozzle **110** of the following ink jet head **100** into the shift register **182a** (Step S406). The control portion **6** then returns to Step S402 and repeats the processing in the same manner.

Also, upon judging in Step S405 that the ejection failure detection and judgment processing described above is completed for all the nozzles **110**, the control portion **6** releases the latch circuit **182b** from the latch state by inputting a CLEAR signal into the latch circuit **182b**, and ends the ejection failure detecting and judgment processing in the ink jet printer **1** shown in FIG. 27.

As has been described, because the detection circuit comprises one ejection failure detecting device **10** and one switching device **23** for the ejection failure detection and judgment processing in the printer **1** shown in FIG. 27, the ejection failure detection processing and judgment processing is repeated as many times as the number of the ink jet heads **100**; however, there is an advantage that the circuit forming the ejection failure detecting device **10** is increased little in size.

FIG. 32 is a flowchart detailing the detection timing of an ejection failure during the flushing operation by the ink jet printers **1** shown in FIG. 28 and FIG. 29. The ink jet printer **1** shown in FIG. 28 and the ink jet printer **1** shown in FIG. 29 are slightly different in terms of the circuitry, but the same in that the number of the ejection failure detecting device **10** and the switching device **23** correspond to (are equal to) the number of ink jet heads **100**. For this reason, the ejection failure detection and judgment processing during the flushing operation comprises the same steps.

When the flushing process in the ink jet printer **1** is performed at the predetermined time, the control portion **6** inputs ejection data for all the nozzles into the shift register **182a** of the ejection selecting means **182** (Step S501), then the latch signal is inputted into the latch circuit **182b** (Step S502), and the ejection data is thus latched. In this instance, the switching devices **23a** through **23e** connect all the ink jet heads **100a** through **100e** to the driving waveform generating means **181** respectively (Step S503).

The ejection failure detection and judgment processing detailed in the flowchart of FIG. 24 is performed in parallel for all the ink jet heads **100** that have performed the ink ejection operation, by the ejection failure detecting devices **10a** through **10e** corresponding to the respective ink jet heads **100a** through **100e** (Step S504). In this case, the judgment results corresponding to all the ink jet heads **100a** through **100e** are correlated with the ink jet heads **100** as the targets of processing, and stored into the predetermined storage region of the storage device **62** (Step S107 of FIG. 24).

In order to clear the ejection data latched in the latch circuit **182b** of the ejection selecting means **182**, the control portion **6** releases the latch circuit **182b** from the latch state by inputting a CLEAR signal into the latch circuit **182b**

(Step S505), and ends the ejection failure detection processing and judgment processing in the ink jet printers **1** shown in FIG. 28 and FIG. 29.

As has been described, according to the processing in the printers **1** shown in FIG. 28 and FIG. 29, the detection and judgment circuit comprises a plurality of (five, in this embodiment) ejection failure detecting devices **10** and a plurality of switching devices **23** corresponding to the ink jet heads **100a** through **100e**. Hence, there can be provided an advantage that the ejection failure detection and judgment processing can be performed in a short time for all the nozzles **110** at a time.

FIG. 33 is a flowchart detailing the detection timing of an ejection failure during the flushing operation by the ink jet printer **1** shown in FIG. 30. The ejection failure detection processing and the cause judgment processing during the flushing operation will now be described with the use of the circuitry of the ink jet printer **1** shown in FIG. 30.

When the flushing process in the ink jet printer **1** is performed at the predetermined timing, the control portion **6** first outputs a scanning signal to the switching selecting device (selector) **19a**, and sets (identifies) first switching device **23a** and ink jet head **100a** by the switching selecting device **19a** and the switching control device **19** (Step S601).

The control portion **6** then inputs ejection data for all the nozzles into the shift register **182a** of the ejection selecting means **182** (Step S602), then the latch signal is inputted into the latch circuit **182b** (Step S603), and the ejection data is thus latched. In this instance, the switching device **23a** connects the electrostatic actuator **120** of the ink jet head **100a** to the driving waveform generating means **181** (Step S604).

Subsequently, the ejection failure detection and judgment processing detailed in the flowchart of FIG. 24 is performed for the ink jet head **100a** that has performed the ink ejection operation (Step S605). In this case, the driving/detection switching signal as the output signal from the switching selecting device **19a** and the ejection data outputted from the latch circuit **182b** are inputted into the AND circuit ANDa and the output signal from the AND circuit ANDa shifts to the high level in Step S103 of FIG. 24, in response to which the switching device **23a** connects the electrostatic actuator **120** of the ink jet head **100a** to the ejection failure detecting device **10**. The judgment result in the ejection failure judgment processing performed in Step S106 of FIG. 24 is correlated with the ink jet head **100** as the target of processing (**100a** herein), and is saved in the predetermined storage region of the storage device **62** (Step S107 of FIG. 24).

In Step S606, the control portion **6** judges whether the ejection failure detection and judgment processing has been completed for all the nozzles. Upon judging that the ejection failure detection and the judgment processing is not completed for all the nozzles **110**, the control portion **6** outputs a scanning signal to the switching selecting device (selector) **19a**, and sets (identifies) the following switching device **23b** and ink jet head **100b** by the switching selecting device **19a** and the switching control device **19** (Step S607), after which the control portions **6** returns to Step S603 and repeats the processing in the same manner. Thereafter, this loop is repeated until the ejection failure detection and judgment processing is completed for all the ink jet heads **100**.

Upon judging that the ejection failure detection processing and judgment processing is completed for all the nozzles **110** in Step S606, the control portion **6** releases the latch circuit **182b** from the latch state by inputting a CLEAR signal into the latch circuit **182b** (Step S609) in order to clear the ejection data latched in the latch circuit **182b** of the

ejection selecting means **182**, and ends the ejection failure detection processing and judgment processing in the ink jet printer **1** shown in FIG. **30**.

As has been described, according to the processing in the ink jet printer **1** shown in FIG. **30**, the detection circuit comprises a plurality of switching devices **23** and one ejection failure detecting device **10**, and the ejection failure of the corresponding ink jet head **100** is detected and the cause thereof is judged by allowing only the switching device **23**, identified by the scanning signal from the switching selecting device (selector) **19a** and corresponding to the ink jet head **100** to perform ejection driving in response to the ejection data, to perform the switching operation. It is thus possible to detect an ejection failure of the ink jet head **100** and to judge the cause thereof more efficiently.

In Step **S602** of this flowchart, the ejection data corresponding to all the nozzles **110** is inputted into the shift register **182b**. However, as in the flowchart shown in FIG. **31**, the ejection failure detection and judgment processing may be performed for the nozzles **110** one by one by inputting the ejection data to be inputted into the shift register **182a** into one corresponding ink jet head **100** in the scanning order of the ink jet heads **100** by the switching selecting device **19a**.

The ejection failure detection and judgment processing in the ink jet printer **1** during the print operation will now be described with reference to the flowcharts shown in FIG. **34** and FIG. **35**. Because the ink jet printer **1** shown in FIG. **27** is chiefly suitable for the ejection failure detection processing and judgment processing during the flushing operation, the description of the flowchart and the operation thereof during the print operation is omitted. However, the ejection failure detection and judgment processing may be performed during the print operation as well in the ink jet printer **1** shown in FIG. **27**.

FIG. **34** is a flowchart detailing the detection timing of an ejection failure during the print operation by the ink jet printers **1** shown in FIG. **28** and FIG. **29**. The processing according to this flowchart is performed (started) at a printing (print) command from the host computer **8**. When the print data is inputted to the shift register **182a** of the ejection selecting means **182** from the host computer **8** via the control portion **6** (Step **S701**), then the latch signal is inputted into the latch circuit **182b** (Step **S702**), and the print data is thus latched. In this instance, the switching devices **23a** through **23e** connect all the ink jet heads **100a** through **100e** to the driving waveform generating means **181** (Step **S703**).

The ejection failure detecting device **10** corresponding to the ink jet heads **100** that have performed the ink ejection operation then perform the ejection failure detection and judgment processing detailed in the flowchart of FIG. **24** (Step **S704**). In this case, the judgment results corresponding to the respective ink jet heads **100** are correlated with the ink jet heads **100** as the targets of processing, and saved in the predetermined storage region of the storage device **62**.

In the case of the ink jet printer **1** shown in FIG. **28**, the switching devices **23a** through **23e** connect the ink jet heads **100a** through **100e** to the ejection failure detecting devices **10a** through **10e** according to the driving/detection switching signal outputted from the control portion **6** (Step **S103** of FIG. **24**). Hence, the electrostatic actuator **120** is not driven in the ink jet head **100** in which the print data is absent, and the residual vibration detecting device **16** of the ejection failure detecting device **10** therefore does not detect the residual vibration waveform of the diaphragm **121**. On the other hand, in the case of the ink jet printer **1** shown in FIG.

29, the switching devices **23a** through **23e** connect the ink jet head **100** in which the print data is present to the ejection failure detecting device **10** according to the output signal from the AND circuit into which the driving/detection switching signal outputted from the control portion **6** and the print data outputted from the latch circuit **182b** are inputted (Step **S103** of FIG. **24**).

In Step **S705**, the control portion **6** judges whether the print operation by the ink jet printer **1** has been completed. Upon judging that the print operation is not completed, the control portion **6** returns to Step **S701**, and inputs the following print data into the shift register **182a** to repeat the processing in the same manner. Upon judging that the printing operation is completed, the control portion **6** releases the latch circuit **182b** from the latch state by inputting a CLEAR signal into the latch circuit **182b** (Step **S707**) in order to clear the ejection data latched in the latch circuit **182b** of the ejection selecting means **182**, and ends the ejection failure detection processing and judgment processing in the ink jet printers **1** shown in FIG. **28** and FIG. **29**.

As has been described, in the ink jet printers **1** shown in FIG. **28** and FIG. **29**, a plurality of switching devices **23a** through **23e** and a plurality of ejection failure detecting devices **10a** through **10e** are provided, so that the ejection failure detection and judgment processing is performed for all the ink jet heads **100** at a time. Hence, the processing can be performed in a short time. Also, the ink jet printer **1** shown in FIG. **29** is further provided with the switching control device **19**, that is, the AND circuits **ANDa** through **ANDe** performing the logical operation AND of the driving/detection switching signal and the print data, so that the switching operation is performed by the switching device **23** for only the ink jet head **100** that will perform the print operation. Hence, the ejection failure detection processing and judgment processing can be performed by omitting useless detection.

FIG. **35** is a flowchart detailing the detection timing of an ejection failure during the print operation by the ink jet printer **1** shown in FIG. **30**. The processing according to this flowchart is performed by the ink jet printer **1** shown in FIG. **30** at a printing command from the host computer **8**. The switching selecting device **19a** sets (identifies) in advance first switching device **23a** and ink jet head **100a** (Step **S801**).

When the print data is inputted into the shift register **182a** of the ejection selecting means **182** from the host computer **8** via the control portion **6** (Step **S802**), the latch signal is inputted into the latch circuit **182b** (Step **S803**), and the print data is thus latched. At this stage, the switching devices **23a** through **23e** connect all the ink jet heads **100a** through **100e** to the driving waveform generating means **181** (the driver **182c** of the ejection selecting means **182**) (Step **S804**).

In a case where the print data is present in the ink jet head **100a**, the control portion **6** controls the switching selecting device **19a** to connect the electrostatic actuator **120** to the ejection failure detecting device **10** after the ejection operation (Step **S103** of FIG. **24**), and performs the ejection failure detection and judgment processing detailed in the flowchart of FIG. **24** (FIG. **25**) (Step **S805**). The judgment result in the ejection failure judgment processing performed in Step **S106** of FIG. **24** is correlated with the ink jet head **100** as the target of processing (**100a**, herein), and saved in the predetermined storage region of the storage device **62** (Step **S107** of FIG. **24**).

In Step **S806**, the control portion **6** judges whether the ejection failure detection and judgment processing described above has been completed for all the nozzles **110** (all the ink

jet heads 100). Upon judging that the above processing is completed for all the nozzles 110, the control portion 6 sets the switching device 23a corresponding to the first nozzle 110 according to the scanning signal (Step S808). Upon judging that the above processing is not completed for all the nozzles 110, the control portion 6 sets the switching device 23b corresponding to the following nozzle 110 (Step S807).

In Step S809, the control portion 6 judges whether the predetermined print operation specified by the host computer 8 has been completed. Upon judging that the print operation is not completed, the control portion 6 inputs the following print data into the shift register 182a (Step S802), and repeats processing in the same manner. Upon judging that the print operation is completed, the control portion 6 releases the latch circuit 182b from the latch state by inputting a CLEAR signal into the latch circuit 182b (Step S811) in order to clear the ejection data latched in the latch circuit 182b of the ejection selecting means 182, and ends the ejection failure detection and judgment processing in the ink jet printer 1 shown in FIG. 30.

As has been described, the droplet ejection apparatus (ink jet printer 1) of the invention is provided with a plurality of ink jet heads (droplet ejection heads) 100 each having the diaphragm 121, the electrostatic actuator 120 that displaces the diaphragm 121, the cavity 141 filled with liquid and the internal pressure thereof varies (increases or decreases) with the displacement of the diaphragm 121, and the nozzle 110 communicating with the cavity 141 and through which the liquid within the cavity 141 is ejected in the form of droplets due to a change (increase and decrease) in internal pressure of the cavity 141. The apparatus is further provided with the driving waveform generating means 181 for driving the electrostatic actuators 120, the ejection selecting means 182 for selecting from which nozzle 110 out of a plurality of nozzles 110 the droplets are to be ejected, one or more than one ejection failure detecting device 10 for detecting the residual vibration of the diaphragm 121 and detecting an ejection failure of the droplets on the basis of the residual vibration of the diaphragm 121 thus detected, and one or more than one switching device 23 for switching the electrostatic actuator 120 to the ejection failure detecting device 10 from the driving waveform generating means 181 after the ejection operation of the droplets by driving the electrostatic actuator 120, according to the driving/detection switching signal or on the basis of the print data, or alternatively according to the scanning signal. Hence, an ejection failure of a plurality of nozzles 110 can be detected either at one time (in parallel) or sequentially.

Thus, an ejection failure can be detected and the cause thereof can be judged in a short time by the droplet ejection apparatus of the invention. Meanwhile, the circuitry of the detection circuit including the ejection failure detecting device 10 can be scaled down, which makes it possible to prevent an increase of the manufacturing costs of the droplet ejection apparatus. Also, because an ejection failure is detected and the cause thereof is judged by switching to the ejection failure detecting device 10 after the electrostatic actuators 120 are driven, the driving of the actuators is not influenced at all, and therefore the throughput of the droplet ejection apparatus of the invention will be neither reduced nor deteriorated. Also, it is possible to provide the ejection failure detecting device 10 to an existing droplet ejection apparatus (ink jet printer 1) provided with predetermined components.

In contrast to the configuration described above, another droplet ejection apparatus of the invention is provided with a plurality of switching device 23, the switching control

device 19, and one or as many as ejection failure detecting device 10 as nozzles 110, and an ejection failure is detected and the cause thereof is judged by switching the corresponding electrostatic actuator 120 from the driving waveform generating means 181 or the ejection selecting means 182 to the ejection failure detecting device 10, according to the driving/detection switching signal and on the basis of the ejection data (print data) or according to the scanning signal and the driving/detection switching signal and on the basis of the ejection data (print data).

Hence, the switching means corresponding to the electrostatic actuator 120 into which the ejection data (print data) has not been inputted, that is, the one that has not performed the ejection driving operation, does not perform the switching operation. The droplet ejection apparatus of the invention is thus able to avoid useless detection and judgment processing. Also, in the case of using the switching selecting device 19a, because the droplet ejection apparatus only has to be provided with one ejection failure detecting device 10, not only can the circuitry of the droplet ejection apparatus be scaled down, but also an increase of the manufacturing costs of the droplet ejection apparatus can be prevented.

In the first embodiment, the ink jet printers 1 shown in FIG. 27 through FIG. 30 used to explain the detection timing of an ejection failure are of the configuration including five ink jet heads 100 (nozzles 110) in the head unit 35 and such configuration was described for ease of explanation. The number of the ink jet heads (droplet ejection heads) 100, however, is not limited to five in the droplet ejection apparatus of the invention, and an ejection failure can be detected and judged for any number of the nozzles 110 actually mounted.

The configuration (recovery means (device) 24) to perform recovery processing by which the cause of an ejection failure (head failure) is eliminated for the ink jet head 100 (head unit 35) in the droplet ejection apparatus of the invention will now be described. FIG. 36 is a view schematically showing the structure (part of which is omitted) when viewed from the top of the ink jet printer 1 shown in FIG. 1. The ink jet printer 1 shown in FIG. 36 is provided with a wiper 300 and a cap 310 used to perform the recovery processing of ink drop non-ejection (head failure) in addition to the configuration shown in the perspective view of FIG. 1.

The recovery processing performed by the recovery device 24 includes the flushing process by which droplets are ejected preliminarily through the nozzles 110 of the respective ink jet heads 100, the wiping process by the wiper 300 described below (see FIG. 37), and a pumping process (pump-suction processing) by a tube pump 320 described below. In other words, the recovery device 24 is provided with the tube pump 320, a pulse motor driving the same, the wiper 300 and a vertical driving mechanism of the wiper 300, and a vertical driving mechanism (not shown) of the cap 310, and the head driver 33, the head unit 35, etc., and the carriage motor 41 and the like function as part of the recovery device 24 in the flushing process and in the wiping process, respectively. Because the flushing process is already described above, the wiping process and the pumping process will be described below.

The wiping process referred to herein is defined as the processing by which foreign substances, such as paper dust, adhering to the nozzle plate 150 (nozzle surface) of the head unit 35 is wiped off with the wiper 300. The pumping process (pump-suction processing) referred to herein is defined as processing by which ink inside the cavities 141 is

sucked (removed by a vacuum) and discharged through the respective nozzles 110 of the head unit 35 by driving the tube pump 320 described below. As has been described, the wiping process is adequate processing as the recovery processing for a state of adhesion of paper dust, which is one of the causes of an ejection failure of droplets of the ink jet head 100 described above. Also, the pump-suction process is adequate processing as the recovery processing for removing air bubbles inside the cavities 141 which cannot be removed by the flushing process described above, or for removing thickened ink when ink has thickened by drying in the vicinity of the nozzles 110 or when ink inside the cavities 141 has thickened by aged deterioration. The recovery processing may be performed by the flushing process described above in a case where ink has thickened slightly and the viscosity is not noticeably high. In this case, because a quantity of ink to be discharged is small, adequate recovery processing can be performed without deteriorating the throughput or the running costs.

The head unit 35 provided with a plurality of ink jet heads (droplet ejection heads) 100 is mounted on the carriage 32, guided by the two carriage guide shafts 422, and moved by the carriage motor 41 as it is coupled to the timing belt 421 via a coupling portion 34 provided at the top edge in the drawing. The head unit 35 mounted on the carriage 32 is allowed to move in the main scanning direction via the timing belt 421 (in association with the timing belt 421) that moves when driven by the carriage motor 41. The carriage motor 41 plays a role of a pulley for continuously turning the timing belt 421, and a pulley 44 is provided at the other end as well.

The cap 310 is used to cap the nozzle plate 150 (see FIG. 5) of the head unit 35. The cap 310 is provided with a hole on the side surface of the bottom portion, and as will be described below, a flexible tube 321, one component of the tube pump 320, is connected to the bottom portion. The tube pump 320 will be described below with reference to FIG. 39.

During the recording (print) operation, a recording sheet P moves in the sub scanning direction, that is, downward in FIG. 36, and the print device 3 moves in the main scanning direction, that is, the horizontal direction in FIG. 36 while the electrostatic actuator 120 of the predetermined ink jet head 100 (droplet ejection head) is being driven, so that the ink jet printer (droplet ejection apparatus) 1 prints (records) a predetermined image or the like on the recording sheet P on the basis of the printing data (print data) inputted from the host computer 8.

FIG. 37 is a view showing the positional relation between the wiper 300 and the print device 3 (head unit 35) shown in FIG. 36. Referring to FIG. 37, the head unit 35 and the wiper 300 are shown as part of the side view of the ink jet printer 1 shown in FIG. 36 when viewed from bottom to top in the drawing. As is shown in FIG. 37(a), the wiper 300 is provided so that it is allowed to move vertically to abut the nozzle surface of the print device 3, that is, the nozzle plate 150 of the head unit 35.

The wiping process as the recovery processing using the wiper 300 will now be described. When the wiping process is performed, as is shown in FIG. 37(a), the wiper 300 is moved upward by an unillustrated driving device, so that the tip end of the wiper 300 is positioned above the nozzle surface (nozzle plate 150). In this case, when the print device 3 (head unit 35) is moved to the left of the drawing (a direction indicated by an arrow) by driving the carriage motor 41, a wiping member 301 abuts the nozzle plate 150 (nozzle surface).

Because the wiping member 301 comprises a flexible rubber member or the like, as is shown in FIG. 37(b), the tip end portion of the wiping member 301 abutting the nozzle plate 150 is bent, and the wiping member 301 thereby cleans (wipes off) the surface of the nozzle plate 150 (nozzle surface) by the tip end portion thereof. This removes foreign substances, such as paper dust (for example, paper dust, dust afloat in air, pieces of rubber), adhering to the nozzle plate 150 (nozzle surface). The wiping process may be performed more than once depending on the adhesion state of such foreign substances (when a large quantity of foreign substances are adhering) by allowing the print device 3 to reciprocate above the wiper 300.

FIG. 38 is a view showing the relation among the head unit 35, the cap 310, and the pump 320 during the pump-suction process. The tube 321 forms an ink discharge path used in the pumping process (pump-suction processing), and is connected to the bottom portion of the cap 310 at one end as described above, and connected to a discharged ink cartridge 340 at the other end via the tube pump 320.

An ink absorber 330 is placed on the inner bottom surface of the cap 310. The ink absorber 330 absorbs and temporarily preserves ink ejected through the nozzles 110 of the ink jet heads 100 during the pump-suction process or the flushing process. The ink absorber 330 prevents ejected droplets from splashing back and thereby smearing the nozzle plate 150 during the flushing operation inside the cap 310.

FIG. 39 is a schematic view showing the configuration of the tube pump 320 shown in FIG. 38. As is shown in FIG. 39(B), the tube pump 320 is a rotary pump, and is provided with a rotor 322, four rollers 323 placed to the circumferential portion of the rotor 322, and a guiding member 350. The rollers 323 are supported by the rotor 322, and apply a pressure to the flexible tube 321 placed arc-wise along a guide 351 of the guiding member 350.

In this tube pump 320, the rotor 322 is rotated about the shaft 322a in a direction X indicated by an arrow of FIG. 39, which allows one or two rollers 323 abutting on the tube 321 to sequentially apply pressure to the tube 321 placed on the arc-shaped guide 351 of the guiding member 350 while rotating in the Y direction. The tube 321 thereby undergoes deformation, and ink (liquid material) within the cavities 141 of the respective ink jet heads 100 is sucked via the cap 310 due to a negative pressure generated in the tube 321. Then, unwanted ink intruded with air bubbles or having thickened by drying is discharged into the ink absorber 330 through the nozzles 110, and the discharged ink absorbed in the ink absorber 330 is then discharged to the discharged ink cartridge 340 (see FIG. 38) via the tube pump 320.

The tube pump 320 is driven by an unillustrated motor, such as a pulse motor. The pulse motor is controlled by the control portion 6. Driving information as to the rotational control of the tube pump 320, including, for example, a look-up table written with the rotational speed and the number of rotations, a control program written with sequence control, etc., is stored in the PROM 64 of the control portion 6. The tube pump 320 is controlled by the CPU 61 of the control portion 6 according to the driving information specified above.

The operation (ejection failure recovery processing) of the recovery device 24 will now be described. FIG. 40 is a flowchart detailing the ejection failure recovery processing in the ink jet printer 1 (droplet ejection apparatus) of the invention. When an ejection failure of the nozzle 110 is detected and the cause thereof is judged in the ejection failure detection and judgment processing described above

(see the flowchart of FIG. 24), the print device 3 is moved to the predetermined stand-by region (for example, the position at which the nozzle plate 150 of the print device 3 is covered with the cap 310 or a position at which the wiping process by the wiper 300 can be performed in FIG. 36) at the predetermined time while the printing operation (print operation) or the like is not performed, and the ejection failure recovery processing is performed.

The control portion 6 first reads out the judgment results corresponding to the respective nozzles 110, which are saved in the EEPROM 62 of the control portion 6 in Step S107 of FIG. 24 (it should be noted that the judgment results to be read out are not the judgment results whose contents are limited to the respective nozzles 110, but those for the respective ink jet heads 100. Hence, hereinafter, the nozzles 110 having an ejection failure also means the ink jet head 100 in which an ejection failure is occurring) (Step S901). In Step S902, the control portion 6 judges whether the judgment results thus read out include those for a nozzle 110 having an ejection failure. Upon judging the absence of the nozzle 110 having an ejection failure, that is, in a case where droplets were ejected normally through all the nozzles 110, the control portion 6 simply ends the ejection failure recovery processing.

On the other hand, upon judging the presence of a nozzle 110 having an ejection failure, the control portion 6 judges in Step S903 whether paper dust is adhering in the nozzle 110 judged as having an ejection failure. Upon judging that no paper dust is adhering in the vicinity of the outlet of the nozzle 110, the control portion 6 proceeds to Step S905. Upon judging that paper dust is adhering, the control portion 6 performs the wiping process to the nozzle plate 150 by the wiper 300 as described above (Step S904).

In Step S905, the control portion 6 subsequently judges whether an air bubble has intruded inside the nozzle 110 judged as having an ejection failure. Upon judging that an air bubble has intruded, the control portion 6 performs the pump-suction process by the tube pump 320 for all the nozzles 110 (Step S906), and ends the ejection failure recovery processing. On the other hand, upon judging that an air bubble has not intruded, the control portion 6 performs the pump-suction process by the tube pump 320 or the flushing process for the nozzle 110 judged as having an ejection failure alone or for all the nozzles 110, on the basis of the length of the cycle of the residual vibration of the diaphragm 121 measured by the measuring means (device) 17 (Step S907), and ends the ejection failure recovery processing.

FIG. 41 is a view used to explain an example of another configuration (wiper 300') of the wiper (wiping means). FIG. 41(a) is a view showing the nozzle surface (nozzle plate 150) of the print device 3 (head unit 35), and FIG. 41(b) is a view showing a wiper 300'. FIG. 42 is a view showing an operation state of the wiper 300' shown in FIG. 41.

The wiper 300' as an example of another configuration of the wiper will now be described with reference to these drawings; however, the difference from the wiper 300 described above will be chiefly described, and the description of similar portions is omitted.

As is shown in FIG. 41(a), a plurality of nozzles 110 are divided into four sets of nozzle groups in correspondence with respective colors of ink, including yellow (Y), magenta (M), cyan (C), and black (K), on the nozzle surface of the print device 3. The wiper 300' of this example is able to perform the wiping process separately for the four sets of nozzle groups for the respective colors of nozzle groups due to the configuration described below.

As is shown in FIG. 41(b), the wiper 300' includes a wiping member 301a for a nozzle group of yellow, a wiping member 301b for a nozzle group of magenta, a wiping member 301c for a nozzle group of cyan, and a wiping member 301d for a nozzle group of black. As is shown in FIG. 42, the respective wiping members 301a through 301d are allowed to move independently in the sub scanning direction by an unillustrated moving mechanism.

The wiper 300 described above is of a type that performs a wiping process on the nozzle surfaces of all the nozzles 110 at one time. According to the wiper 300' of this example, however, it is possible to wipe only a nozzle group that needs the wiping process, and waste-less recovery processing can be thus performed.

FIG. 43 is a view used to explain an example of another configuration of the pumping means (device). The example of another configuration of the pumping means will now be described with reference to the drawing; however, the difference from the pumping means described above will be chiefly described, and the description of similar portions is omitted.

As is shown in FIG. 43, the pumping means of this example includes a cap 310a for the nozzle group of yellow, a cap 310b for the nozzle group of magenta, a cap 310c for the nozzle group of cyan, and a cap 310d for the nozzle group of black.

The tube 321 of the tube pump 320 is branched into four branched tubes 325a through 325d, and the caps 310a through 310d are connected to the branched tubes 325a through 325d, respectively. Valves 326a through 326d are provided at some mid points in the branched tubes 325a through 325d, respectively.

The pumping means of this example as described above is able to perform the pump-suction process separately for the four sets of nozzle groups of the print device 3 for the respective colors of nozzle groups by selecting the OPEN/CLOSE states of the respective valves 326a through 326d. This makes it possible to suck (vacuum) only the nozzle group that needs the pump-suction process, and waste-less recovery processing can be thus performed. FIG. 43 shows a case where tube pump 320 sucks four colors of ink by the same tube 321; however, the tube pump 320 may include tubes for respective four colors.

The ink jet printer 1 of the invention as described above operates along the flow described below when detection by the ejection failure detecting device 10 is performed for all the nozzles 110. The following description will describe sequentially two patterns of the flow of the operation by the ink jet printer 1 of the invention after detection by the ejection failure detecting device 10 is performed. To begin with, a first pattern will be described.

1A. The ink jet printer 1 performs detection by the ejection failure detecting device 10 for all the nozzles 110 during the flushing process (flushing operation) or the printing operation as described above.

When the result of the detection shows the presence of a nozzle 110 in which an ejection failure is occurring (hereinafter, referred to as the failing nozzle), it is preferable that the ink jet printer 1 informs the user of such detection. Informing means (method) is not particularly limited, and any means can be used, for example, a display on the operation panel 7, a sound, an alarming sound, illumination of the lamp, transmission of ejection failure information to the host computer 8 via the IF 9 or to a print server over a network, etc.

2A. When the result of the detection in 1A shows the presence of a nozzle 110 in which an ejection failure is

51

occurring (failing nozzle), the recovery processing is performed by the recovery device **24** (the printing operation is suspended when the printer **1** is performing the printing operation). In this case, the recovery device **24** performs the recovery processing of the type corresponding to the cause of an ejection failure of the failing nozzle according to the flowchart of FIG. **40** described above. This prevents, for example, the pump-suction process from being performed even in a case where the cause of an ejection failure of the failing nozzle is adhesion of paper dust, that is, in a case where the pump-suction process need not to be performed. It is thus possible to prevent ink from being wastefully discharged, which can in turn reduce ink consumption. Also, because the recovery processing of the types that need not to be performed will not be performed, a time needed for the recovery processing can be shortened, and the throughput (the number of printed sheets per unit time) of the inkjet printer **1** can be improved.

The recovery processing may be performed for all the nozzles **110**; however, it is sufficient to perform the recovery processing at least for the failing nozzle. For example, in a case where the flushing process is performed as the recovery processing, only the failing nozzle may be forced to perform the flushing operation. In a case where the wiping means and the pumping means are configured to perform the recovery processing separately for the nozzle groups of respective colors as shown in FIG. **41** through FIG. **43**, the wiping process or the pump-suction process may be performed only for the nozzle group including the failing nozzle detected in **1A**.

In a case where a plurality of failing nozzles each having a different cause of an ejection failure are detected in **1A**, it is preferable to perform the recovery processing of several types in order to eliminate the causes of all the ejection failures.

3A. When the recovery processing in **2A** ends, the failing nozzle detected in **1A** alone is forced to perform the droplet ejection operation, so that detection by the ejection failure detecting device **10** is performed again for this failing nozzle alone. This makes it possible to confirm whether the failing nozzle detected in **1A** has been restored to a normal state, and the occurrence of an ejection failure during the printing operation performed later can be prevented in a more reliable manner.

Also, because the detection by the ejection failure detecting device **10** is performed by forcing the failing nozzle alone to perform the droplet ejection operation, the nozzles **110** judged as being normal in **1A** do not have to eject ink drops. Hence, wasteful ejection of ink can be avoided, and ink consumption can be reduced. Further, the load on the ejection failure detecting device **10** and the control portion **6** can be reduced.

In a case where the detection in **3A** still shows the presence of a nozzle **110** having an ejection failure, it is preferable to perform the recovery processing by the recovery device **24** again.

The following description will describe a second pattern of the flow of the operation after detection by the ejection failure detecting device **10** is performed in the ink jet printer **1** of the invention. In other words, in the invention, the control may be effected according to the flow including **1B** through **5B** below instead of **1A** through **3A** described above.

1B. As with the above **1A**, detection by the ejection failure detecting device **10** is performed for all the nozzles **110**.

2B. When the result of the detection in **1B** shows the presence of a nozzle **110** in which an ejection failure is

52

occurring (hereinafter, referred to as the failing nozzle), the flushing process is performed for this failing nozzle alone (the printing operation is suspended when the printer **1** is performing the printing operation). In a case where the cause of an ejection failure of the failing nozzle is minor, the failing nozzle can be restored to the normal state by this flushing process. In this case, because ink drops are not ejected through the normal nozzles **110**, ink is not consumed wastefully. When detection by the ejection failure detecting device **10** is performed frequently, the causes of ejection failures are often minor. Hence, by performing the flushing process first for the failing nozzle regardless of the cause of an ejection failure in this manner, the recovery processing can be performed efficiently and quickly.

3B. When the flushing process in **2B** ends, the failing nozzle detected in **1B** alone is forced to perform the droplet ejection operation, so that detection by the ejection failure detecting device **10** is performed again for this failing nozzle alone. This makes it possible to confirm whether the failing nozzle detected in **1B** has been restored to the normal state, and the occurrence of an ejection failure during the printing operation performed later can be prevented in a more reliable manner.

Also, because detection by the ejection failure detecting device **10** is performed by forcing the failing nozzle alone to perform the droplet ejection operation, the nozzles **110** judged as being normal in **1B** do not have to eject ink drops. Hence, wasteful ejection of ink can be avoided, and ink consumption can be reduced. Further, the load on the ejection failure detecting device **10** and the control portion **6** can be reduced.

4B. When the result of the detection in **3B** shows the presence of a nozzle **110** in which an ejection failure has not been eliminated (hereinafter, referred to as the re-failing nozzle), the recovery processing by the recovery device **24** is performed. In this case, the recovery device **24** performs the recovery processing of the type corresponding to the cause of an ejection failure of the re-failing nozzle according to the flowchart of FIG. **40** described above. This prevents, for example, the pump-suction process from being performed even in a case where the cause of an ejection failure of the re-failing nozzle is adhesion of paper dust, that is, in a case where the pump-suction process need not be performed. It is thus possible to prevent ink from being wastefully discharged, which can in turn reduce ink consumption. Also, because the recovery processing of the types that need not to be performed will not be performed, a time needed for the recovery processing can be shortened, and the throughput (the number of printed sheets per unit time) of the ink jet printer **1** can be improved.

Because the flushing process is already performed in **2B**, it is preferable to perform other types of the recovery processing in **4B**. In other words, in a case where the cause of an ejection failure of the re-failing nozzle is intrusion of an air bubble or thickening caused by drying, it is preferable to perform the pump-suction process, and in a case where the cause is adhesion of paper dust, it is preferable to perform the wiping process by the wiper **300** or **300'**.

It should be noted that **4B** is the same as the above **2A** other than the points described above.

5B. When the recovery processing in **4B** ends, the re-failing nozzle detected in **3B** alone is forced to perform the droplet ejection operation, so that detection by the ejection failure detecting device **10** is performed once again for this re-failing nozzle alone. This makes it possible to confirm whether the re-failing nozzle detected in **3B** has been restored to the normal state, and the occurrence of an

ejection failure during the printing operation performed later can be prevented in a more reliable manner.

Also, because detection by the ejection failure detecting device **10** is performed by forcing the re-failing nozzle alone to perform the droplet ejection operation, the nozzles **110** 5 judged as being normal in 1B or 3B do not have to eject ink drops. Hence, wasteful ejection of ink can be avoided, and ink consumption can be reduced. Further, the load on the ejection failure detecting device **10** and the control portion **6** can be reduced.

In 1A through 3A and 1B through 5B described above, it is preferable to perform the flushing process for the respective nozzles **110** (all the nozzles **110**) after the recovery processing of the type corresponding to the cause of an ejection failure is performed. This makes it possible to 15 prevent mixing of ink of respective colors by forestalling ink of respective colors remaining on the nozzle surface (nozzle plate **150**) from being mixed.

As has been described, the droplet ejection apparatus (ink jet printer **1**) and the ejection failure recovery method for the droplet ejection apparatus in this embodiment include: the ejection failure detecting device **10** for detecting an ejection failure and the cause thereof for a plurality of droplet ejection heads (a plurality of ink jet heads **100** of the head unit **35**); and the recovery means (for example, the tube pump **320** used in the pump-suction process, the wiper **300** used in the wiping process, etc.) for performing the recovery processing depending on the cause of an ejection failure in a case where an ejection failure is detected for a nozzle **110** by the ejection failure detecting device **10** when the nozzles **110** of the droplet ejection heads **100** performed the ejection operation of the droplets. 20

Hence, because adequate recovery processing (one or two of the flushing process, pump-suction process, and wiping process) corresponding to the cause of an ejection failure can be performed by the droplet ejection apparatus and the ejection failure recovery method of the invention, different from the sequential recovery processing performed in the conventional droplet ejection apparatus, it is possible to 25 reduce wastefully discharged ink generated when the recovery processing is performed, which can in turn prevent a reduction or deterioration of the throughput of the entire droplet ejection apparatus.

Also, the droplet ejection apparatus (ink jet printer **1**) of the invention is configured in such a manner that the diaphragm **121**, which is displaced when the electrostatic actuator **120** is driven, is provided to the droplet ejection head (ink jet head **100**), and the ejection failure detecting device **10** detects an ejection failure of the droplets on the basis of the vibration pattern (for example, the cycle of the residual vibration) of the residual vibration of the diaphragm **121** during the droplet ejection operation. 30

Hence, compared with the conventional droplet ejection apparatus capable of detecting an ejection failure, the invention does not need other parts (for example, optical missing dot detecting device or the like). As a result, not only can an ejection failure of the droplets be detected without increasing the size of the droplet ejection head, but also the manufacturing costs of the droplet ejection apparatus capable of performing ejection failure (missing dot) detection can be reduced. Also, because the droplet ejection apparatus of the invention detects an ejection failure of the droplets through the use of the residual vibration of the diaphragm after the droplet ejection operation, an ejection failure of the droplets can be detected even during the print operation. 35

Examples of other configurations of the ink jet head of the invention will now be described. FIG. **44** through FIG. **47** are cross sections schematically showing examples of other configurations of the ink jet head (head unit). Hereinafter, an explanation will be given with reference to these drawings; however, differences from the embodiment described above are chiefly described, and the description of the similar 40 portions is omitted.

An ink jet head **100A** shown in FIG. **44** is of a type that ejects ink (liquid) within a cavity **208** through a nozzle **203** as a diaphragm **212** vibrates when a piezoelectric element **200** is driven. A metal plate **204** made of stainless steel is bonded to a nozzle plate **202** made of stainless steel in which the nozzle (hole) **203** is formed, via an adhesive film **205**, and another metal plate **204** made of stainless steel is further bonded to the first-mentioned metal plate **204** via an adhesive film **205**. Further, a communication port forming plate **206** and a cavity plate **207** are sequentially bonded to the second-mentioned metal plate **204**. 45

The nozzle plate **202**, the metal plates **204**, the adhesive films **205**, the communication port forming plate **206**, and the cavity plate **207** are molded into their respective predetermined shapes (a shape in which a concave portion is formed), and the cavity **208** and a reservoir **209** are defined by laminating these components. The cavity **208** and the reservoir **209** communicate with each other via an ink supply port **210**. Also, the reservoir **209** communicates with an ink intake port **211**. 50

The diaphragm **212** is placed at the upper surface opening portion of the cavity plate **207**, and a piezoelectric element **200** is bonded to the diaphragm **212** via a lower electrode **213**. Also, an upper electrode **214** is bonded to the piezoelectric element **200** on the opposite side of the lower electrode **213**. A head drive **215** is provided with a driving circuit that generates a driving voltage waveform. The piezoelectric element **200** starts to vibrate when a driving voltage waveform is applied (supplied) between the upper electrode **214** and the lower electrode **213**, and so does the diaphragm **212** bonded to the piezoelectric element **200**. The volume (internal pressure of the cavity) of the cavity **208** varies with the vibration of the diaphragm **212**, and ink (liquid) filled in the cavity **208** is thereby ejected through the nozzle **203** in the form of droplets. 55

A reduced quantity of liquid in the cavity **208** due to the ejection of droplets is replenished as ink is supplied from the reservoir **209**. Also, ink is supplied to the reservoir **209** through the ink intake port **211**.

Likewise, an ink jet head **100B** shown in FIG. **45** is of a type that ejects ink (liquid) within a cavity **221** through a nozzle when the piezoelectric element **200** is driven. The ink jet head **100B** includes a pair of opposing substrates **220**, and a plurality of piezoelectric elements **200** are placed intermittently at predetermined intervals between both substrates **220**. 60

Cavities **221** are formed between adjacent piezoelectric elements **200**. A plate (not shown) and a nozzle plate **222** are placed in front and behind the cavities **221** of FIG. **45**, respectively, and nozzles (holes) **223** are formed in the nozzle plate **222** at positions corresponding to the respective cavities **221**.

A pair of electrodes **224** is placed on one surface and also on the other surface of each piezoelectric element **200**. That is to say, four electrodes **224** are bonded to one piezoelectric element **200**. When a predetermined driving voltage waveform is applied between predetermined electrodes of these 65

electrodes **224**, the piezoelectric element **200** undergoes share-mode deformation and starts to vibrate (indicated by arrows in FIG. **45**). The volume of the cavities **221** (internal pressure of cavity) varies with the vibration, and ink (liquid) filled in the cavities **221** is thereby ejected through nozzles **223** in the form of droplets. In other words, the piezoelectric elements **200** per se function as the diaphragms in the ink jet head **100B**.

Likewise, an ink jet head **100C** shown in FIG. **46** is of a type that ejects ink (liquid) within a cavity **233** through a nozzle **231** when the piezoelectric element **200** is driven. The ink jet head **100C** is provided with a nozzle plate **230** in which the nozzle **231** is formed, spacers **232**, and the piezoelectric element **200**. The piezoelectric element **200** is placed to be spaced apart from the nozzle plate **230** by a predetermined distance with the spacers **232** in between, and the cavity **233** is defined by a space surrounded by the nozzle plate **230**, the piezoelectric element **200**, and the spacers **232**.

A plurality of electrodes are bonded to the top surface of the piezoelectric element **200** of FIG. **46**. To be more specific, a first electrode **234** is bonded to nearly the center portion of the piezoelectric element **200**, and a second electrode **235** is bonded on either side thereof. When a predetermined driving voltage waveform is applied between the first electrode **234** and the second electrodes **235**, the piezoelectric element **200** undergoes share-mode deformation and starts to vibrate (indicated by arrows of FIG. **46**). The volume of the cavity **233** (internal pressure of cavity) varies with the vibration, and ink (liquid) filled in the cavity **233** is thereby ejected through nozzle **231** in the form of droplets. In other words, the piezoelectric element **200** per se functions as the diaphragm in the ink jet head **100C**.

Likewise, an ink jet head **100D** shown in FIG. **47** is of a type that ejects ink (liquid) within a cavity **245** through a nozzle **241** when the piezoelectric element **200** is driven. The ink jet head **100D** is provided with a nozzle plate **240** in which the nozzle **241** is formed, a cavity plate **242**, a diaphragm **243**, and a layered piezoelectric element **201** comprising a plurality of layered piezoelectric elements **200**.

The cavity plate **242** is molded into a predetermined shape (a shape in which a concave portion is formed), by which the cavity **245** and a reservoir **246** are defined. The cavity **245** and the reservoir **246** communicate with each other via an ink supply port **247**. Also, the reservoir **246** communicates with an ink cartridge **31** via an ink supply tube **311**.

The lower end of the layered piezoelectric element **201** of FIG. **47** is bonded to the diaphragm **243** via an intermediate layer **244**. A plurality of external electrodes **248** and internal electrodes **249** are bonded to the layered piezoelectric element **201**. To be more specific, the external electrodes **248** are bonded to the outer surface of the layered piezoelectric element **201** and the internal electrodes **249** are provided in spaces (or inside each piezoelectric element) between piezoelectric elements **200** that together form the layered piezoelectric element **201**. In this case, the external electrodes **248** and the internal electrodes **249** are placed so that parts of them are layered alternatively in the thickness direction of the piezoelectric element **200**.

By applying a driving voltage waveform between the external electrodes **248** and the internal electrodes **249** by the head driver **33**, the layered piezoelectric element **201** undergoes deformation (contracts in the vertical direction of FIG. **47**) and starts to vibrate as is indicated by arrows of FIG. **47**, and so do the diaphragms **243** due to this vibration. The volume of the cavity **245** (internal pressure of cavity) varies with the vibration of the diaphragm **243**, and ink

(liquid) filled in the cavity **245** is thereby ejected through the nozzle **241** in the form of droplets.

A reduced quantity of liquid in the cavity **245** due to the ejection of droplets is replenished as ink is supplied from the reservoir **246**. Also, ink is supplied to the reservoir **246** from the ink cartridge **31** through the ink supply tube **311**.

As with the ink jet head **100** of the electric capacitance type as described above, the ink jet heads **100A** through **100D** provided with piezoelectric elements are also able to detect an ejection failure of droplets and identify the cause of the failure on the basis of the residual vibration of the diaphragm or the piezoelectric element functioning as the diaphragm. Alternatively, for the ink jet heads **100B** and **100C**, a diaphragm (diaphragm used to detect the residual vibration) serving as a sensor may be provided at a position facing the cavity, so that the residual vibration of this diaphragm is detected.

Third Embodiment

An example of still another configuration of the ink jet head of the invention will now be described. FIG. **48** is a perspective view showing the configuration of a head unit **35** of this embodiment. FIG. **49** is a cross section of the head unit **35** (ink jet head **100H**) shown in FIG. **48**. Hereinafter, an explanation will be given with reference to these drawings; however, differences from the embodiments above will be chiefly described, and the description of the similar portions is omitted.

The head unit **35** (ink jet head **100H**) shown in FIG. **48** and FIG. **49** is of a so-called film boiling ink jet type (thermal jet type), and is provided with a supporting plate **410**, a substrate **420**, an outer wall **430**, partition walls **431**, and a top plate **440**, which are bonded to each other in this order from bottom to top of FIG. **48** and FIG. **49**.

The substrate **420** and the top plate **440** are placed so that they are spaced apart by a predetermined interval with having in between the outer wall **430** and a plurality of (six in the case of the drawings) partition walls **431** aligned in parallel at regular intervals. A plurality of (five in the case of the drawings) cavities (pressure chambers: ink chambers) **141** are defined in a space between the substrate **420** and the top plate **440** by the partition walls **431**. Each cavity **141** is shaped like a strip (rectangular prism).

Also, as is shown in FIG. **48** and FIG. **49**, the left ends of the respective cavities **141** of FIG. **49** (top ends of FIG. **48**) are covered with a nozzle plate (front plate) **433**. The nozzle plate **433** is provided with nozzles (holes) **110** communicating with the respective cavities **141**, and ink (liquid material) is ejected through these nozzles **110**.

In FIG. **48**, the nozzles **110** are aligned linearly, that is, in a row, with respect to the nozzle plate **433**. It goes without saying, however, that the alignment pattern of the nozzles is not limited to this pattern.

The nozzle plate **433** may be omitted, and instead, it may be configured in such a manner that the top ends of the respective cavities **141** of FIG. **48** (left ends of FIG. **49**) are open, and these opened openings are used as the nozzles.

Also, an ink intake port **441** is formed in the top plate **440**, and an ink cartridge **31** is connected to the ink intake port **441** via an ink supply tube **311**.

Heating elements **450** are provided (buried) in the substrate **420** at positions corresponding to the respective cavities **141**. The heating elements **450** electrically conduct and heat separately with the use a head driver (electrically conducting means) **33** including a driving circuit **18**. The head driver **33** outputs, for example, a pulsed signal, as a

driving signal of the heating elements **450** in response to the printing signal (print data) inputted from the control portion **6**.

The surface of each heating element **450** on the cavity **141** side is covered with a protection film (cavitation-proof film) **451**. The protection film **451** is provided to prevent the heating elements **450** from coming into direct contact with ink within the cavities **141**. By providing the protection film **451**, it is possible to prevent degeneration, deterioration, etc. caused when the heating elements **450** come into contact with ink.

Concave portions **460** are formed in the substrate **420** at the positions in the vicinity of the respective heating elements **450** and corresponding to the respective cavities **141**. The concave portions **460** can be formed, for example, by etching, stamping, etc.

A diaphragm **461** is provided to shield each concave portion **460** on the cavity **141** side. The diaphragm **461** undergoes elastic deformation (displaces elastically) in the vertical direction of FIG. **49** in association with a change in internal pressure (liquid pressure) of the cavity **141**.

The diaphragm **461** also functions as an electrode. The diaphragm **461** may comprise an electrical conductive material as a whole or a lamination of an electrical conductive layer and a dielectric layer.

On the other hand, the other side of the concave portion **460** is covered with the supporting plate **410**, and electrodes (segment electrodes) **462** are provided on the supporting plate **410** on the top surface of FIG. **49** at positions corresponding to the respective diaphragms **461**.

The diaphragm **461** and the electrode **462** are provided oppositely in approximately parallel to be spaced apart by a predetermined distance.

A parallel plate capacitor can be formed by placing the diaphragm **461** and the electrode **462** to be spaced apart by a slight distance in this manner. When the diaphragm **461** displaces (deforms) elastically in the vertical direction of FIG. **49** in association with an internal pressure of the cavity **141**, a distance of the space between the diaphragm **461** and the electrode **462** varies as well, which causes the electric capacitance of the parallel plate capacitor to vary. In the ink jet head **100H**, the diaphragm **461** and the electrode **462** function as a sensor that detects a failure of the ink jet head **100H** on the basis of variance with time of the electric capacitance associated with the vibration (residual vibration (damped vibration)) of the diaphragm **461**.

A common electrode **470** is formed on the substrate **420** outside of the cavities **141**. Also, segment electrodes **471** are formed on the supporting plate **410** outside of the cavities **141**. Each of the electrodes **462**, the common electrode **470**, and the segment electrodes **471** can be formed, for example, by bonding of metal foil, plating, vapor deposition, sputtering, etc.

The respective diaphragms **461** and the common electrode **470** are electrically connected to each other by a conductor **475**. The respective electrodes **462** and the respective segment electrodes **471** are electrically connected to each other by a conductor **476**.

The conductors **475** and **476** may comprise (1) installation of conducting wire, such as a metal wire, (2) a thin film-made on the surface of the substrate **420** or the supporting plate **410** out of an electrical conductive material, such as gold and copper, (3) a conductor forming site in the substrate **420** or the like provided with electrical conduction by doping ions therein, etc.

The function (operation principle) of the ink jet head **100H** will now be described.

When the heating elements **450** electrically conduct as a driving signal (pulse signal) is outputted from the head driver **33**, the heating elements **450** heat instantaneously to a temperature as high as or higher than 300° C. This generates an air bubble (different from the aforementioned air bubble that is generated and intrudes inside the cavity to cause an ejection failure) **480** on the protection film **451** due to film boiling, and the air bubble **480** swells instantaneously. This raises the liquid pressure of ink (liquid material) filled in the cavity **141**, and part of ink is thereby ejected through the nozzle **110** in the form of droplets.

A reduced quantity of liquid within the cavity **141** due to the ejection of the ink drops is replenished as new ink is supplied through the ink intake port **441** to the cavity **141**. This ink is supplied from the ink cartridge **31** by flowing through the ink supply tube **311**.

The air bubble **480** contracts abruptly immediately after the droplets of ink are ejected, and restores to the original state. The diaphragm **461** displaces (deforms) elastically with a change in internal pressure of the cavity **141** in this instance, which gives rise to damped vibration (residual vibration) that lasts until ink drops are ejected again upon input of the following driving signal. Once the diaphragm **461** starts the damped vibration, the electric capacitance of the capacitor comprising the diaphragm **461** and the opposing electrode **462** starts to vary. The ink jet head **100H** of this embodiment is able to detect an ejection failure in the same manner as the ink jet head **100** of the first embodiment described above, by using variance with time of the electric capacitance.

While the droplet ejection apparatus and the ejection failure recovery method for the droplet ejection apparatus of the invention have been described by way of embodiments shown in the drawings, it is to be understood that the invention is not limited to these embodiments, and respective portions forming the droplet ejection head or the droplet ejection apparatus can be replaced with an arbitrary arrangement capable of functioning in the same manner. Also, another arbitrary component may be added to the droplet ejection head or the droplet ejection apparatus of the invention.

Liquid to be ejected (droplets) ejected through a droplet ejection head (ink jet head **100** in the embodiments above) in the droplet ejection apparatus of the invention is not particularly limited, and for example, it may be liquid (including dispersion liquid, such as suspension and emulsion) containing various materials as follows. That is, a filter material (ink) for a color filter, a light-emitting material forming an EL (Electroluminescence) light-emitting layer in an organic EL apparatus, a fluorescent material forming a fluorescent body on an electrode in an electron emitting device, a fluorescent material forming a fluorescent body in a PDP (Plasma Display Panel), a migration material forming a migration body in an electrophoresis display device, a bank material forming a bank on the surface of a substrate **W**, coating materials of various kinds, a liquid electrode material forming an electrode, a particle material forming a spacer to provide a minute cell gap between two substrates, a liquid metal material forming metal wiring, a lens material forming a micro lens, a resist material, a light-scattering material for forming a light-scattering body, liquid materials for various tests used in a bio-sensor, such as a DNA chip and a protein chip, etc.

Also, in the invention, a droplet receptor to which droplets are ejected is not limited to paper, such as a recording sheet, and it may be other media, such as a film, a woven cloth, and

a non-woven cloth, or a workpiece, such as various substrates including a glass substrate and a silicon substrate.

Also, in the droplet ejection apparatus and the ejection failure recovery method for the droplet ejection apparatus of the invention, the means and method of detecting an ejection failure and the cause thereof are not limited to the method of detecting and analyzing the vibration pattern of the residual vibration of the diaphragm **121** as described above, and adequate recovery processing can be selected by using any detecting method, as long as the cause of an ejection failure is identified. As an ejection failure (missing dot) detecting method, for example, methods as follows are conceivable. That is, a method in which a beam of light from an optical sensor, such as a laser, is directly irradiated to and reflected from the ink meniscus inside the nozzle, and the vibration state of the meniscus is detected by a light-reception element, so that the cause of blocking is identified from the vibration state; a method in which the presence or absence of the droplets is detected with the use of a typical optical missing dot detecting device (detecting whether flight droplets fall within a detectable range of the sensor) and from the measurement result of an elapsed time after the ejection operation, and a phenomenon occurring within a drying time is assumed as drying, and a phenomenon occurring outside the drying time is assumed as paper dust or air bubbles on the basis of the elapsed time data of the ink jet head in the event of a missing dot; and a method in which a vibration sensor is added to the above configuration, and whether vibration that allows intrusion of air bubbles is added before the occurrence of the missing dot is judged, so that an air bubble is assumed to have intruded when such vibration was added (in this case, the missing dot detecting means is not limited to an optical type, and for example, the detecting means may be of a heat sensitive type that detects a change in temperature of a heat sensor portion upon ejection of ink, a method of detecting a change in quantity of charges in a detection electrode onto which charged ink drops are ejected and land, or of an electric capacitance type in which a change is caused when ink droplets pass through a space between the electrodes). Also, as a detecting method of the adhesion of paper dust, a method of detecting a state of the head surface by a camera or the like as image information, or a method of detecting the presence or absence of adhesion of paper dust by scanning the vicinity of the head surface with the use of an optical sensor, such as a laser, are conceivable.

The pump-suction recovery process, one type of recovery processing performed by the recovery device **24**, is the process effective in the case of serious thickening caused by drying and in the case of intrusion of an air bubble, and a similar recovery process can be performed for each cause. Hence, when ink jet heads **100** failing due to the intrusion of an air bubble and thickening caused by drying that need the pump-suction process are detected in the head unit **35**, the processing may not be determined separately as in Steps **S905** through **S907** in the flowchart of FIG. **40**, and instead, the pump-suction process may be performed at one time for both the ink jet head **100** failing due to intrusion of an air bubble and the ink jet head **100** failing due to thickening caused by drying. In other words, after the judgment is made as to whether paper dust is adhering in the vicinity of the nozzle **110**, the pump-suction process may be performed without judging whether the cause is intrusion of an air bubble or thickening caused by drying.

What is claimed is:

1. A droplet ejection apparatus having a head unit including a plurality of droplet ejection heads each ejecting liquid within a cavity through a nozzle in the form of droplets by driving an actuator by way of a driving circuit, said apparatus comprising:
 - ejection failure detecting means for detecting an ejection failure of said droplet ejection heads and a cause thereof; and
 - recovery means for performing recovery processing depending on the cause of the ejection failure if said ejection failure detecting means detects the ejection failure;
 wherein each of said droplet ejection heads includes a diaphragm that is displaced when the actuator is driven and said ejection failure detecting means detects a residual vibration of said diaphragm and determines an ejection failure of said droplets based on a vibration pattern of the detected residual vibration of said diaphragm;
 - wherein said ejection failure detecting means includes judging means for judging at least one of a presence and an absence of an ejection failure of the droplets in the corresponding droplet ejection head based on the vibration pattern of the residual vibration of said diaphragm, and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in said droplet ejection head, said vibration pattern of the residual vibration of said diaphragm including a cycle of the residual vibration; and
 - wherein said judging means judges that:
 - an air bubble has intruded inside said cavity when the cycle of the residual vibration of said diaphragm is shorter than a predetermined first period;
 - the liquid has thickened in the vicinity of said nozzle when the cycle of the residual vibration of said diaphragm is longer than a predetermined second period; and
 - dust is adhering in the vicinity of the outlet of said nozzle when the cycle of the residual vibration of said diaphragm is longer than said first period and shorter than said second period.
2. The droplet ejection apparatus according to claim 1, wherein said recovery means includes:
 - wiping means for performing, with the use of a wiper, a wiping process on nozzle surfaces of said droplet ejection heads where said nozzles are aligned;
 - flushing means for performing a flushing process by which the droplets are preliminarily ejected through said nozzles by driving said actuators; and
 - pumping means for performing a pump-suction process with the use of a pump connected to a cap covering the nozzle surfaces of said droplet ejection heads.
3. The droplet ejection apparatus according to claim 2, wherein:
 - the cause of an ejection failure detectable by said ejection failure detecting means includes:
 - intrusion of an air bubble inside said cavity;
 - thickening of the liquid in a vicinity of said nozzle; and
 - adhesion of dust in a vicinity of an outlet of said nozzle; and
 - said recovery means performs the pump-suction process by said pumping means in a case of the intrusion of an air bubble, at least one of the flushing process by said flushing means and the pump-suction process by said

61

pumping means in a case of the thickening of the liquid, and at least the wiping process by said wiper in a case of the adhesion of dust.

4. The droplet ejection apparatus according to claim 3, wherein:

when said ejection failure detecting means detects the intrusion of an air bubble and the thickening of the liquid that need said pump-suction process in more than one droplet ejection head of said head unit, said recovery means performs the pump-suction process for the droplet ejection heads where the intrusion of an air bubble and the thickening of the liquid are detected.

5. The droplet ejection apparatus according to claim 1, wherein:

said ejection failure detecting means includes an oscillation circuit and said oscillation circuit oscillates based on an electric capacitance component of said actuator that varies with the residual vibration of said diaphragm.

6. The droplet ejection apparatus according to claim 5, wherein:

said oscillation circuit forms a CR oscillation circuit from the electric capacitance component of said actuator and a resistance component of a resistor element connected to said actuator.

7. The droplet ejection apparatus according to claim 5, wherein:

said ejection failure detecting means includes an F/V converting circuit that generates a voltage waveform of the residual vibration of said diaphragm from a predetermined signal group generated based on a change of an oscillation frequency in an output signal from said oscillation circuit.

8. The droplet ejection apparatus according to claim 7, wherein:

said ejection failure detecting means includes a waveform shaping circuit that shapes the voltage waveform of the residual vibration of said diaphragm generated in said F/V converting circuit into a predetermined waveform.

9. The droplet ejection apparatus according to claim 8, wherein said waveform shaping circuit includes:

DC component removing means for removing a direct current component from the voltage waveform of the residual vibration of said diaphragm generated in said F/V converting circuit; and

a comparator that compares the voltage waveform, from which the direct current component has been removed by said DC component removing means with a predetermined voltage value,

said comparator generating and outputting a rectangular wave based on the voltage comparison.

10. The droplet ejection apparatus according to claim 9, wherein:

said ejection failure detecting means includes measuring means for measuring a cycle of the residual vibration of said diaphragm from said rectangular wave generated in said waveform shaping circuit.

11. The droplet ejection apparatus according to claim 10, wherein:

said measuring means has a counter, and measures at least one of a time between rising edges and a time between a rising edge and a falling edge of said rectangular wave by counting pulses of a reference signal with said counter.

62

12. The droplet ejection apparatus according to claim 1, further comprising:

switching means for switching a connection of said actuator from said driving circuit to said ejection failure detecting means after an ejection operation of the droplets is performed by driving said actuator.

13. The droplet ejection apparatus according to claim 12, wherein:

said droplet ejection apparatus comprises more than one ejection failure detecting means and more than one switching means; and

the switching means corresponding to said droplet ejection head that has performed the droplet ejection operation switches the connection of said actuator from said driving circuit to a corresponding ejection failure detecting means, and said switched ejection failure detecting means detects an ejection failure of said droplets.

14. The droplet ejection apparatus according to claim 12, wherein:

said switching means comprises more than one unit switching means corresponding to said droplet ejection heads, respectively;

said ejection failure detecting means further includes detection determining means for determining for which nozzle among said nozzles detection of an ejection failure of said droplets is to be performed; and

said switching means switches a connection of said actuator from said driving circuit to said ejection failure detecting means after the ejection operation of said droplets is performed by driving said actuator corresponding to the nozzle of said droplet ejection head determined by said detection determining means.

15. The droplet ejection apparatus according to claim 1, wherein:

said ejection failure detecting means detects an ejection failure of said droplets at a time of at least one of the droplet ejection operation during the flushing process and the droplet ejection operation during a print operation by said nozzle as a target of detection.

16. The droplet ejection apparatus according to claim 1, wherein:

said actuator comprises an electrostatic actuator.

17. The droplet ejection apparatus according to claim 1, wherein:

said actuator comprises a piezoelectric actuator using a piezoelectric effect of a piezoelectric element.

18. The droplet ejection apparatus according to claim 1, further comprising:

storage means for storing the cause of an ejection failure of said droplets detected by said ejection failure detecting means, in connection with said nozzle as the target of detection.

19. A droplet ejection apparatus, provided with a plurality of droplet ejection heads each ejecting a liquid through a nozzle communicating with a cavity in the form of droplets by changing an internal pressure of said cavity filled with the liquid by driving an actuator with a driving circuit, for ejecting the droplets through said nozzles while scanning said droplet ejection heads relatively with respect to a droplet receptor so that the droplets land on said droplet receptor, said apparatus comprising:

ejection failure detecting means for detecting an ejection failure of the droplets through said nozzles and a cause thereof;

63

recovery means for performing recovery processing for said droplet ejection heads to eliminate the cause of the ejection failure of the droplets; and

storage means for storing a nozzle where the ejection failure is detected by said ejection failure detecting means, in connection with the cause thereof,

wherein if detection by said ejection failure detecting means is performed for all of said nozzles and the presence of a failing nozzle in which an ejection failure is occurring is detected, recovery processing depending on the cause of the ejection failure is performed by said recovery means at least for said failing nozzle, after which detection by said ejection failure detecting means is performed again by forcing said failing nozzle alone to perform a droplet ejection operation.

20. The droplet ejection apparatus according to claim **19**, wherein said recovery means includes:

wiping means for performing a wiping process by which nozzle surfaces of said droplet ejection heads, where said nozzles are aligned, are wiped with a wiper;

flushing means for performing a flushing process by which the droplets are preliminarily ejected through said nozzles by driving said actuators; and

pumping means for performing a pump-suction process with the use of a pump connected to a cap covering the nozzle surfaces of said droplet ejection heads.

21. The droplet ejection apparatus according to claim **20**, wherein:

the cause of an ejection failure detectable by said ejection failure detecting means includes:

intrusion of an air bubble inside said cavity;

thickening of the liquid in a vicinity of said nozzle; and

adhesion of dust in a vicinity of an outlet of said nozzle;

and

said recovery means performs the pump-suction process by said pumping means if the cause of the ejection failure of said failing nozzle is the intrusion of an air bubble, at least one of the flushing process by said flushing means and the pump-suction process by said pumping means if the cause of the ejection failure of said failing nozzle is the thickening of the liquid, and at least the wiping process by said wiper if the cause of the ejection failure of said failing nozzle is the adhesion of dust.

22. The droplet ejection apparatus according to claim **20**, wherein:

said recovery means performs the flushing process for each of said nozzles after the recovery processing depending on the cause of the ejection failure is performed.

23. The droplet ejection apparatus according to claim **20**, wherein:

said wiping means is adapted to perform the wiping process separately for plural sets of nozzle groups, so that when performing the wiping process depending on the cause of the ejection failure of said failing nozzle or said re-failing nozzle, said wiping means performs the wiping process only for a nozzle group including said failing nozzle or said re-failing nozzle.

24. The droplet ejection apparatus according to claim **23**, wherein:

said plural sets of nozzle groups have different droplets to be ejected.

25. The droplet ejection apparatus according to claim **20**, wherein:

said pumping means is adapted to perform the pump-suction process separately for plural sets of nozzle

64

groups, so that when performing the pump-suction process depending on the cause of the ejection failure of said failing nozzle or said re-failing nozzle, said pumping means performs the pump-suction process only for a nozzle group including said failing nozzle or said re-failing nozzle.

26. The droplet ejection apparatus according to claim **25**, wherein:

said plural sets of nozzle groups have different droplets to be ejected.

27. The droplet ejection apparatus according to claim **19**, further comprising:

informing means for informing a detection result when a result of detection by said ejection failure detecting means detects a nozzle with an ejection failure.

28. The droplet ejection apparatus according to claim **19**, wherein:

the actuator of each of said droplet ejection heads has a diaphragm that can be displaced so as to change an internal pressure of said cavity; and

said ejection failure detecting means detects residual vibration of said diaphragm and detects an ejection failure based on a vibration pattern of the detected residual vibration of said diaphragm.

29. The droplet ejection apparatus according to claim **28**, wherein:

said actuator comprises an electrostatic actuator.

30. The droplet ejection apparatus according to claim **28**, wherein:

said actuator comprises a piezoelectric actuator using a piezoelectric effect of a piezoelectric element.

31. The droplet ejection apparatus according to claim **28**, wherein:

said ejection failure detecting means includes an oscillation circuit and said oscillation circuit oscillates based on an electric capacitance component of said actuator that varies with the residual vibration of said diaphragm.

32. The droplet ejection apparatus according to claim **31**, wherein:

said oscillation circuit forms a CR oscillation circuit from the electric capacitance component of said actuator and a resistance component of a resistor element connected to said actuator.

33. The droplet ejection apparatus according to claim **31**, wherein:

said ejection failure detecting means includes an F/V converting circuit that generates a voltage waveform of the residual vibration of said diaphragm from a predetermined signal group generated based on a change of an oscillation frequency in an output signal from said oscillation circuit.

34. The droplet ejection apparatus according to claim **33**, wherein:

said ejection failure detecting means includes a waveform shaping circuit that shapes the voltage waveform of the residual vibration of said diaphragm generated in said F/V converting circuit into a predetermined waveform.

35. The droplet ejection apparatus according to claim **34**, wherein said waveform shaping circuit includes:

DC component removing means for removing a direct current component from the voltage waveform of the residual vibration of said diaphragm generated in said F/V converting circuit; and

65

a comparator that compares the voltage waveform, from which the direct current component has been removed by said DC component removing means, with a predetermined voltage value,

said comparator generating and outputting a rectangular wave based on the voltage comparison.

36. The droplet ejection apparatus according to claim **35**, wherein:

said ejection failure detecting means includes measuring means for measuring a cycle of the residual vibration of said diaphragm from said rectangular wave generated in said waveform shaping circuit.

37. The droplet ejection apparatus according to claim **36**, wherein:

said measuring means has a counter, and measures at least one of a time between rising edges and a time between a rising edge and a falling edge of said rectangular wave by counting pulses of a reference signal with said counter.

38. The droplet ejection apparatus according to claim **28**, wherein:

the vibration pattern of the residual vibration of said diaphragm includes a cycle of said residual vibration.

39. The droplet ejection apparatus according to claim **28**, wherein:

said ejection failure detecting means includes judging means for judging at least one of a presence and an absence of an ejection failure of the droplets in said droplet ejection head based on the vibration pattern of the residual vibration of said diaphragm, and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in said droplet ejection head.

40. The droplet ejection apparatus according to claim **39**, wherein:

said judging means judges that:

an air bubble has intruded inside said cavity when the cycle of the residual vibration of said diaphragm is shorter than a first predetermined period;

the liquid has thickened in the vicinity of said nozzle when the cycle of the residual vibration of said diaphragm is longer than a second predetermined period; and

dust is adhering in the vicinity of the outlet of said nozzle when the cycle of the residual vibration of said diaphragm is longer than said first predetermined period and shorter than said second predetermined period.

41. The droplet ejection apparatus according to claim **19**, wherein:

the actuator of each of said droplet ejection heads has a heating element that can film boil the liquid filled in said cavity;

each of said droplet ejection heads further includes a diaphragm that is displaced elastically in association with a change in internal pressure of said cavity, and an electrode provided opposite said diaphragm; and

said ejection failure detecting means detects residual vibration of said diaphragm and detects an ejection failure based on a vibration pattern of the detected residual vibration of said diaphragm.

42. The droplet ejection apparatus according to claim **41**, wherein:

said ejection failure detecting means includes an oscillation circuit, and said oscillation circuit oscillates based on a variance with time of an electric capacitance of a

66

capacitor comprising said diaphragm and said electrode, associated with the residual vibration of said diaphragm.

43. The droplet ejection apparatus according to claim **42**, wherein:

said oscillation circuit forms a CR oscillation circuit from an electric capacitance component of said capacitor and a resistance component of a resistor element.

44. The droplet ejection apparatus according to claim **42**, wherein:

said ejection failure detecting means includes an F/V converting circuit that generates a voltage waveform of the residual vibration of said diaphragm from a predetermined signal group generated based on a change of an oscillation frequency in an output signal from said oscillation circuit.

45. The droplet ejection apparatus according to claim **44**, wherein:

said ejection failure detecting means includes a waveform shaping circuit that shapes the voltage waveform of the residual vibration of said diaphragm generated in said F/V converting circuit into a predetermined waveform.

46. The droplet ejection apparatus according to claim **45**, wherein: said waveform shaping circuit includes:

DC component removing means for removing a direct current component from the voltage waveform of the residual vibration of said diaphragm generated in said F/V converting circuit; and

a comparator that compares the voltage waveform, from which the direct current component has been removed by said DC component removing means, with a predetermined voltage value,

said comparator generating and outputting a rectangular wave based on the voltage comparison.

47. The droplet ejection apparatus according to claim **46**, wherein:

said ejection failure detecting means includes measuring means for measuring a cycle of the residual vibration of said diaphragm from said rectangular wave generated in said waveform shaping circuit.

48. The droplet ejection apparatus according to claim **46**, wherein:

said measuring means has a counter and measures at least one of a time between rising edges and a time between a rising edge and a falling edge of said rectangular wave by counting pulses of a reference signal with said counter.

49. A droplet ejection apparatus, provided with a plurality of droplet ejection heads each ejecting a liquid through a nozzle communicating with said-a_cavity in the form of droplets by changing an internal pressure of said cavity filled with the liquid by driving an actuator with a driving circuit, for ejecting the droplets through said nozzles while scanning said droplet ejection heads relatively with respect to a droplet receptor so that the droplets land on said droplet receptor, said apparatus comprising:

ejection failure detecting means for detecting an ejection failure of the droplets through said nozzles and a cause thereof;

recovery means for performing recovery processing for said droplet ejection heads to eliminate the cause of the ejection failure of the droplets; and

storage means for storing a nozzle where the ejection failure is detected by said ejection failure detecting means, in connection with the cause thereof,

67

wherein:

said recovery means includes flushing means for performing a flushing process by which the droplets are preliminarily ejected through said nozzles by driving said actuators; and

if the presence of a failing nozzle in which an ejection failure is occurring is detected when detection by said ejection failure detecting means is performed for all of said nozzles, the flushing process is performed for said failing nozzle alone, after which detection by said ejection failure detecting means is performed again by forcing said failing nozzle alone to perform a droplet ejection operation, and when the presence of a re-failing nozzle in which the ejection failure has not been eliminated is detected, recovery processing depending on the cause of the ejection failure of said re-failing nozzle is performed by said recovery means at least for said re-failing nozzle, after which detection by said ejection failure detecting means is performed once again by forcing said re-failing nozzle alone to perform the droplet ejection operation.

50. The droplet ejection apparatus according to claim **49**, wherein said recovery means further includes:

wiping means for performing a wiping process by which nozzle surfaces of said droplet ejection heads, where said nozzles are aligned, are wiped off by a wiper; and pumping means for performing a pump-suction process with the use of a pump connected to a cap covering the nozzle surfaces of said droplet ejection heads.

51. The droplet ejection apparatus according to claim **50**, wherein:

the cause of an ejection failure detectable by said ejection failure detecting means includes:

intrusion of an air bubble inside said cavity;
thickening of the liquid in a vicinity of said nozzle; and
adhesion of dust in a vicinity of an outlet of said nozzle;
and

said recovery means performs the pump-suction process by said pumping means if the cause of the ejection failure of said re-failing nozzle is at least one of the intrusion of an air bubble and the thickening of the liquid, and at least the wiping process by said wiper if the cause of the ejection failure of said re-failing nozzle is the adhesion of dust.

52. The droplet ejection apparatus according to claim **50**, wherein:

said recovery means performs the flushing process for each of said nozzles after the recovery processing depending on the cause of the ejection failure is performed.

53. The droplet ejection apparatus according to claim **50**, wherein:

said wiping means is adapted to perform the wiping process separately for plural sets of nozzle groups, so that when performing the wiping process depending on the cause of the ejection failure of said failing nozzle or said re-failing nozzle, said wiping means performs the wiping process only for a nozzle group including said failing nozzle or said re-failing nozzle.

54. The droplet ejection apparatus according to claim **50**, wherein:

said pumping means is adapted to perform the pump-suction process separately for plural sets of nozzle groups, so that when performing the pump-suction process depending on the cause of the ejection failure of said failing nozzle or said re-failing nozzle, said

68

pumping means performs the pump-suction process only for a nozzle group including said failing nozzle or said re-failing nozzle.

55. The droplet ejection apparatus according to claim **49**, further comprising:

informing means for informing a detection result when a result of detection by said ejection failure detecting means detects a nozzle with an ejection failure.

56. The droplet ejection apparatus according to claim **49**, wherein:

the actuator of each of said droplet ejection heads has a diaphragm that can be displaced so as to change an internal pressure of said cavity; and

said ejection failure detecting means detects residual vibration of said diaphragm and detects an ejection failure based on a vibration pattern of the detected residual vibration of said diaphragm.

57. The droplet ejection apparatus according to claim **56**, wherein:

said actuator comprises an electrostatic actuator.

58. The droplet ejection apparatus according to claim **56**, wherein:

said actuator comprises a piezoelectric actuator using a piezoelectric effect of a piezoelectric element.

59. The droplet ejection apparatus according to claim **56**, wherein:

said ejection failure detecting means includes an oscillation circuit and said oscillation circuit oscillates based on an electric capacitance component of said actuator that varies with the residual vibration of said diaphragm.

60. The droplet ejection apparatus according to claim **59**, wherein:

said oscillation circuit forms a CR oscillation circuit from the electric capacitance component of said actuator and a resistance component of a resistor element connected to said actuator.

61. The droplet ejection apparatus according to claim **56**, wherein:

the vibration pattern of the residual vibration of said diaphragm includes a cycle of said residual vibration.

62. The droplet ejection apparatus according to claim **56**, wherein:

said ejection failure detecting means includes judging means for judging at least one of a presence and an absence of an ejection failure of the droplets in said droplet ejection head based on the vibration pattern of the residual vibration of said diaphragm, and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in said droplet ejection head.

63. The droplet ejection apparatus according to claim **62**, wherein:

said judging means judges that:

an air bubble has intruded inside said cavity when the cycle of the residual vibration of said diaphragm is shorter than a first predetermined period;

the liquid has thickened in the vicinity of said nozzle when the cycle of the residual vibration of said diaphragm is longer than a second predetermined period; and

dust is adhering in the vicinity of the outlet of said nozzle when the cycle of the residual vibration of said diaphragm is longer than said first predetermined period and shorter than said second predetermined period.

69

64. The droplet ejection apparatus according to claim 49, wherein:

the actuator of each of said droplet ejection heads has a heating element that can film boil the liquid filled in said cavity;

each of said droplet ejection heads further includes a diaphragm that is displaced elastically in association with a change in internal pressure of said cavity, and an electrode provided opposite said diaphragm; and

said ejection failure detecting means detects residual vibration of said diaphragm and detects an ejection failure based on a vibration pattern of the detected residual vibration of said diaphragm.

65. The droplet ejection apparatus according to claim 64, wherein:

said ejection failure detecting means includes an oscillation circuit, and said oscillation circuit oscillates based on a variance with time of an electric capacitance of a capacitor comprising said diaphragm and said electrode, associated with the residual vibration of said diaphragm.

66. The droplet ejection apparatus according to claim 65, wherein:

said oscillation circuit forms a CR oscillation circuit from an electric capacitance component of said capacitor and a resistance component of a resistor element.

67. An ejection failure recovery method for a droplet ejection apparatus having a head unit including a plurality of droplet ejection heads each ejecting liquid within a cavity through a nozzle in the form of droplets by driving an actuator with a driving circuit, said method comprising:

displacing a diaphragm associated with each of said droplet ejection heads during driving of said actuator; detecting an ejection failure of said droplet ejection heads and a cause thereof by detecting a residual vibration of said diaphragm and determining an ejection failure of said droplets based on a vibration pattern of the detected residual vibration of said diaphragm, said vibration pattern of the residual vibration of said diaphragm including a cycle of the residual vibration;

judging at least one of a presence and an absence of an ejection failure of the droplets in the corresponding droplet ejection head based on the vibration pattern of the residual vibration of said diaphragm and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in said droplet ejection head; and

performing recovery processing depending on the cause of the ejection failure in a case where the ejection failure is detected;

wherein said judging means idles that;

an air bubble has intruded inside said cavity when the cycle of the residual vibration of said diaphragm is shorter than a predetermined first period;

the liquid has thickened in the vicinity of said nozzle when the cycle of the residual vibration of said diaphragm is longer than a predetermined second period; and

dust is adhering in the vicinity of the outlet of said nozzle when the cycle of the residual vibration of said diaphragm is longer than said first period and shorter than said second period.

68. A droplet ejection apparatus having a head unit including a plurality of droplet ejection heads each ejecting liquid within a cavity through a nozzle in the form of

70

droplets by driving an actuator by way of a driving circuit, said apparatus comprising:

an ejection failure detector which detects an ejection failure of said droplet ejection heads and a cause thereof; and

a recovery device which performs recovery processing depending on the cause of the ejection failure if said ejection failure detector detects the ejection failure;

wherein each of said droplet ejection heads includes a diaphragm that is displaced when the actuator is driven and said ejection failure detector detects a residual vibration of said diaphragm and determines an ejection failure of said droplets based on a vibration pattern of the detected residual vibration of said diaphragm;

wherein said ejection failure detector includes judging means for judging at least one of a presence and an absence of an ejection failure of the droplets in the corresponding droplet ejection head based on the vibration pattern of the residual vibration of said diaphragm, and judging the cause of the ejection failure upon judging the presence of the ejection failure of the droplets in said droplet ejection head, said vibration pattern of the residual vibration of said diaphragm including a cycle of the residual vibration; and

wherein said judging means judges that:

an air bubble has intruded inside said cavity when the cycle of the residual vibration of said diaphragm is shorter than a predetermined first period;

the liquid has thickened in the vicinity of said nozzle when the cycle of the residual vibration of said diaphragm is longer than a predetermined second period; and

dust is adhering in the vicinity of the outlet of said nozzle when the cycle of the residual vibration of said diaphragm is longer than said first period and shorter than said second period.

69. A droplet ejection apparatus, provided with a plurality of droplet ejection heads each ejecting a liquid through a nozzle communicating with a cavity in the form of droplets by changing an internal pressure of said cavity filled with the liquid by driving an actuator with a driving circuit, for ejecting the droplets through said nozzles while scanning said droplet ejection heads relatively with respect to a droplet receptor so that the droplets land on said droplet receptor, said apparatus comprising:

an ejection failure detector which detects an ejection failure of the droplets through said nozzles and a cause thereof;

a recovery device which performs recovery processing for said droplet ejection heads to eliminate the cause of the ejection failure of the droplets; and

a storage device which stores a nozzle where the ejection failure is detected by said ejection failure detector, in connection with the cause thereof,

wherein if detection by said ejection failure detector is performed for all of said nozzles and the presence of a failing nozzle in which an ejection failure is occurring is detected, recovery processing depending on the cause of the ejection failure is performed by said recovery device at least for said failing nozzle, after which detection by said ejection failure detector is performed again by forcing said failing nozzle alone to perform a droplet ejection operation.

70. A droplet ejection apparatus, provided with a plurality of droplet ejection heads each ejecting a liquid through a nozzle communicating with a cavity in the form of droplets by changing an internal pressure of said cavity filled with the

71

liquid by driving an actuator with a driving circuit, for ejecting the droplets through said nozzles while scanning said droplet ejection heads relatively with respect to a droplet receptor so that the droplets land on said droplet receptor, said apparatus comprising:

an ejection failure detector which detects an ejection failure of the droplets through said nozzles and a cause thereof;

a recovery device for performing recovery processing for said droplet ejection heads to eliminate the cause of the ejection failure of the droplets; and

a storage device which stores a nozzle where the ejection failure is detected by said ejection failure detector, in connection with the cause thereof,

wherein:

said recovery device includes a flusher for performing a flushing process by which the droplets are preliminarily ejected through said nozzles by driving said actuators; and

72

if the presence of a failing nozzle in which an ejection failure is occurring is detected when detection by said ejection failure detector is performed for all of said nozzles, the flushing process is performed for said failing nozzle alone, after which detection by said ejection failure detector is performed again by forcing said failing nozzle alone to perform a droplet ejection operation, and when the presence of a re-failing nozzle in which the ejection failure has not been eliminated is detected, recovery processing depending on the cause of the ejection failure of said re-failing nozzle is performed by said recovery device at least for said re-failing nozzle, after which detection by said ejection failure detector is performed once again by forcing said re-failing nozzle alone to perform the droplet ejection operation.

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UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

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DATED : December 19, 2006
INVENTOR(S) : Osamu Shinkawa et al.

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Col. 25, line 19: "go" should be -- g_0 --

Col. 26, line 5: " $dV/dt = I_s/C_1$," should be -- $dV/dt = I_s/C_1$, --

Col. 26, line 33: "go" should be -- g_0 --

Col. 51, line 61: "1 B" should be -- 1B --

Col. 66, line 25: after "wherein:" start new paragraph with "said"

Col. 66, line 51: "said-a_cavity" should be -- a cavity --

Col. 69, line 52: "idles that;" should be -- judges that: --

Signed and Sealed this

Sixth Day of January, 2009



JON W. DUDAS

Director of the United States Patent and Trademark Office