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Zheng

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(54) **1XN FANOUT WAVEGUIDE
PHOTODETECTOR**

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(52) **U.S. Cl.** **385/39**

(58) **Field of Search** 385/12-14, 39, 385/24, 37; 356/356, 358, 357, 345; 372/6, 32, 18; 359/116, 124, 127, 130

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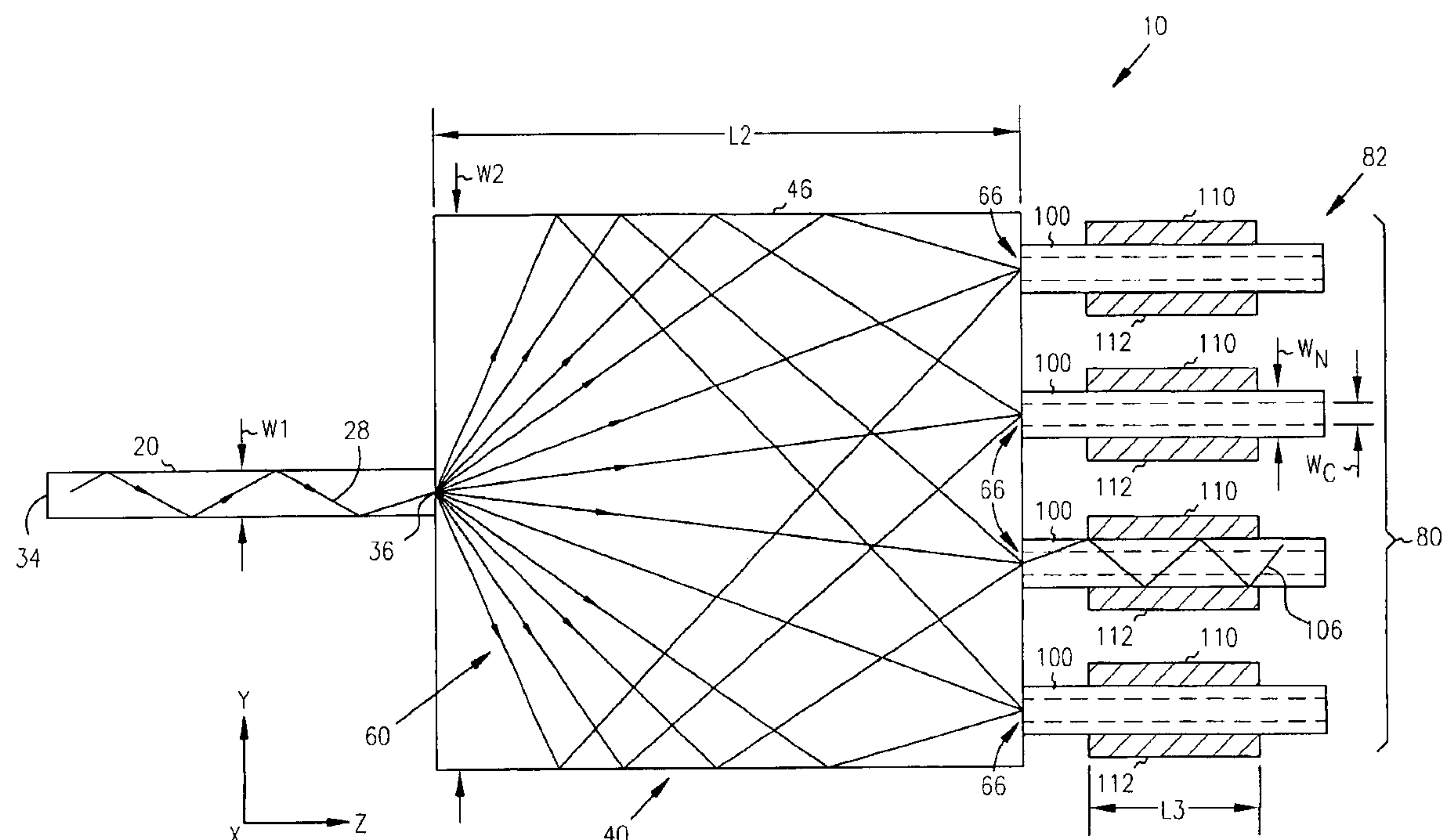
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(57) **ABSTRACT**

A 1×N fanout waveguide detector is disclosed. The detector includes a multiple-mode interference (MMI) cavity with input and output ends. A single-mode waveguide is optically coupled to the input end of the MMI cavity so that the optical power in the guided mode is distributed over N modes. The MMI cavity forms N interference nodes at or near its output end. N waveguide detectors are optically coupled to the output end at or near the N interference nodes. The waveguide detectors each have a waveguide that is evanescently coupled to an intrinsic region of a PIN detector. The width of the detector waveguide core, which can be sub-micron, defines the carrier collection distance between the electrodes of the PIN detector. Further, the length of the detector waveguide can be selected to maximize optical absorption to provide optimum quantum efficiency. The waveguide detectors are connected in parallel to provide a high-output photocurrent.

15 Claims, 13 Drawing Sheets



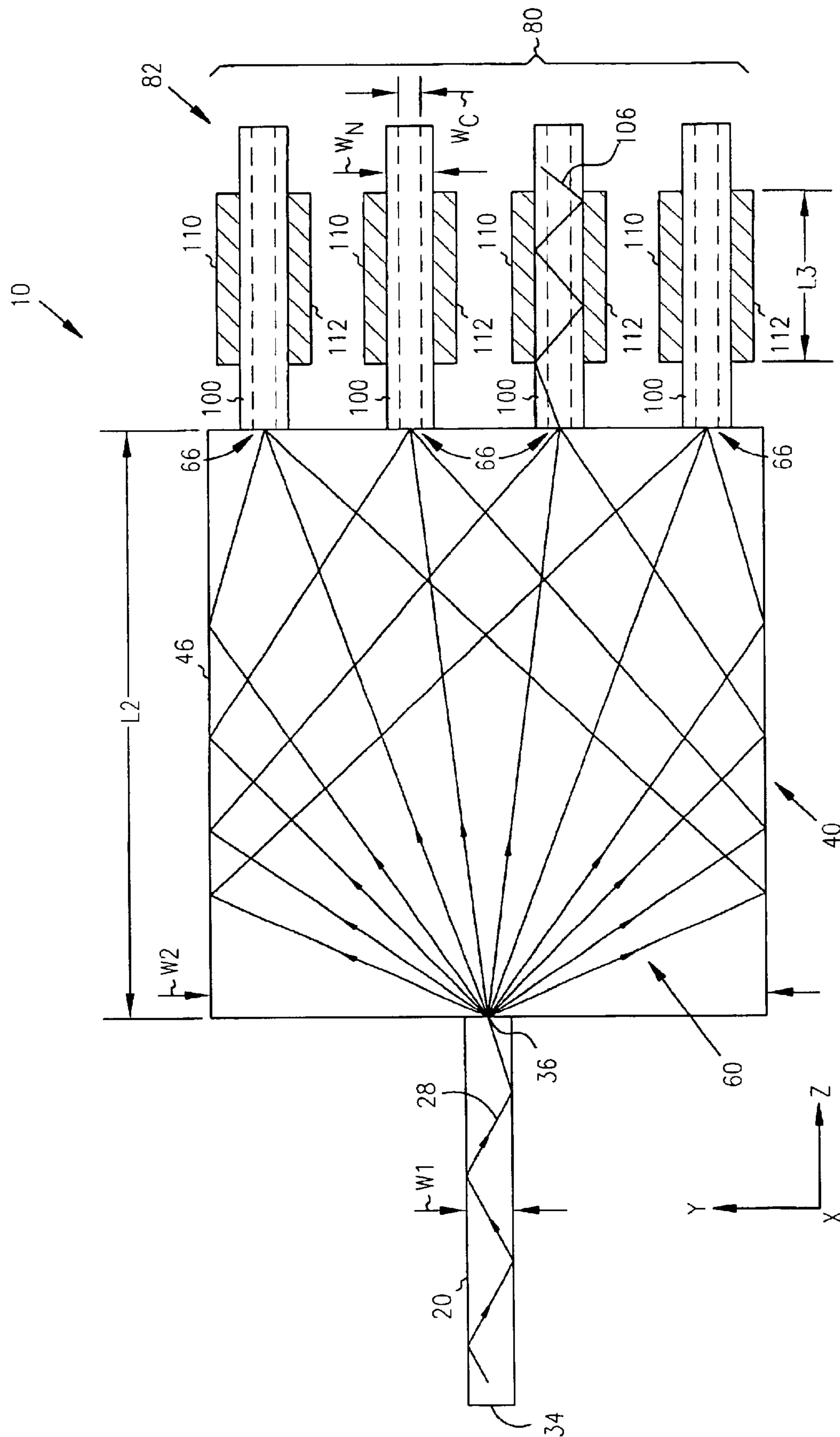


FIG. 1

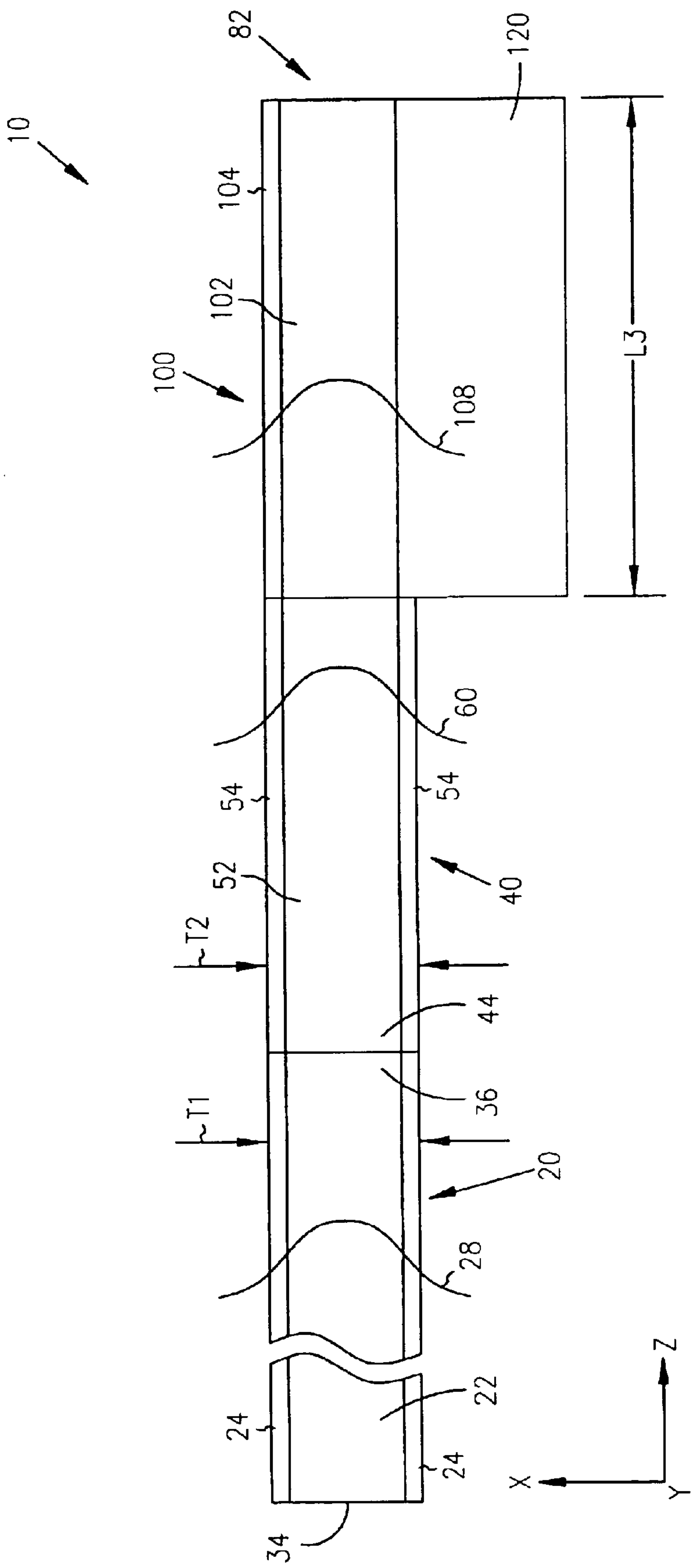


FIG. 2

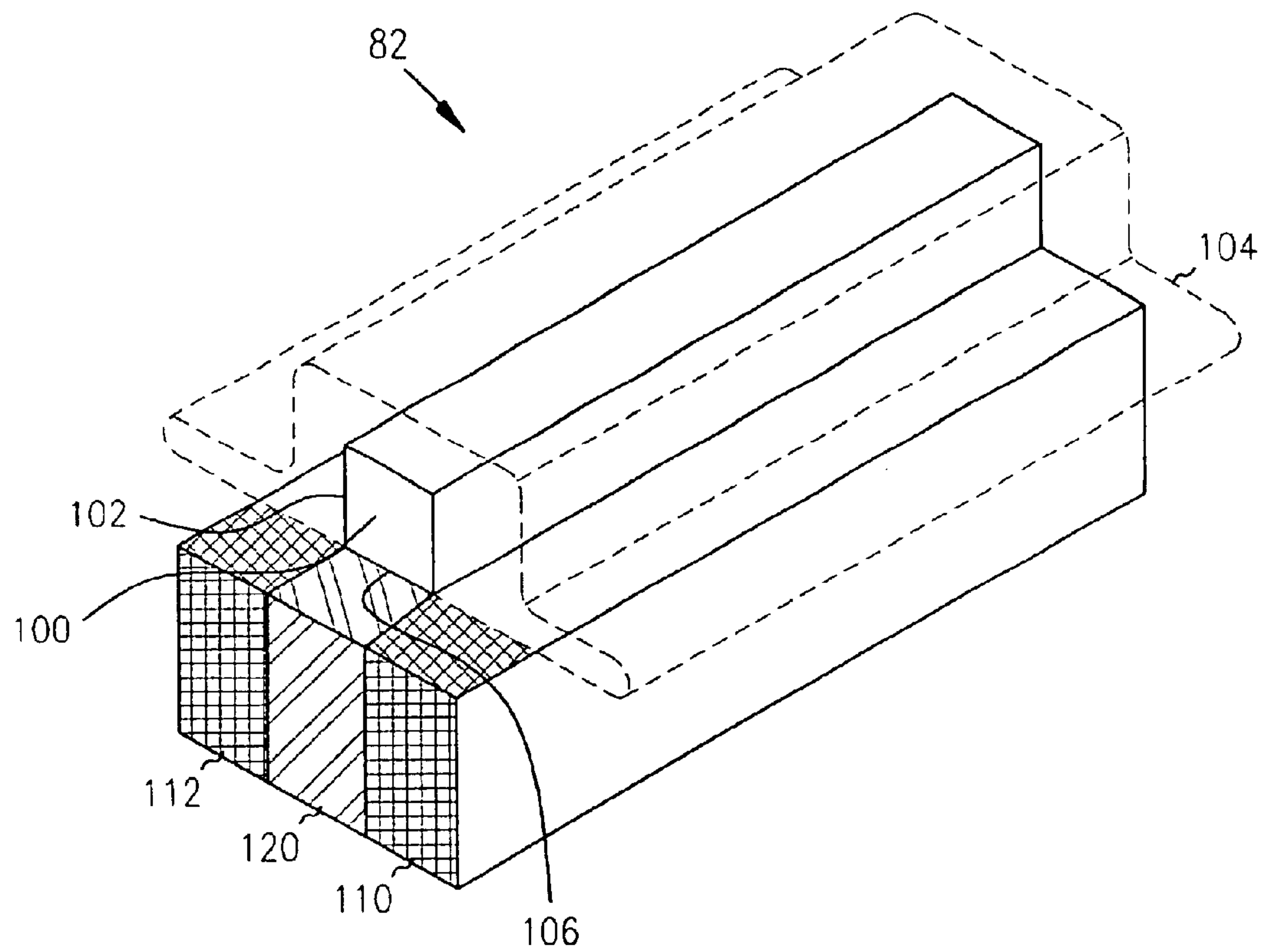


FIG. 3

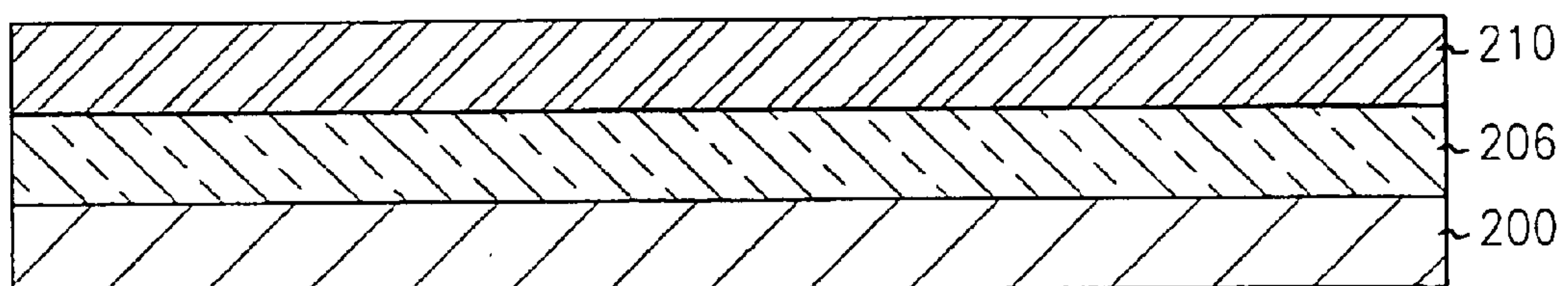


FIG. 4

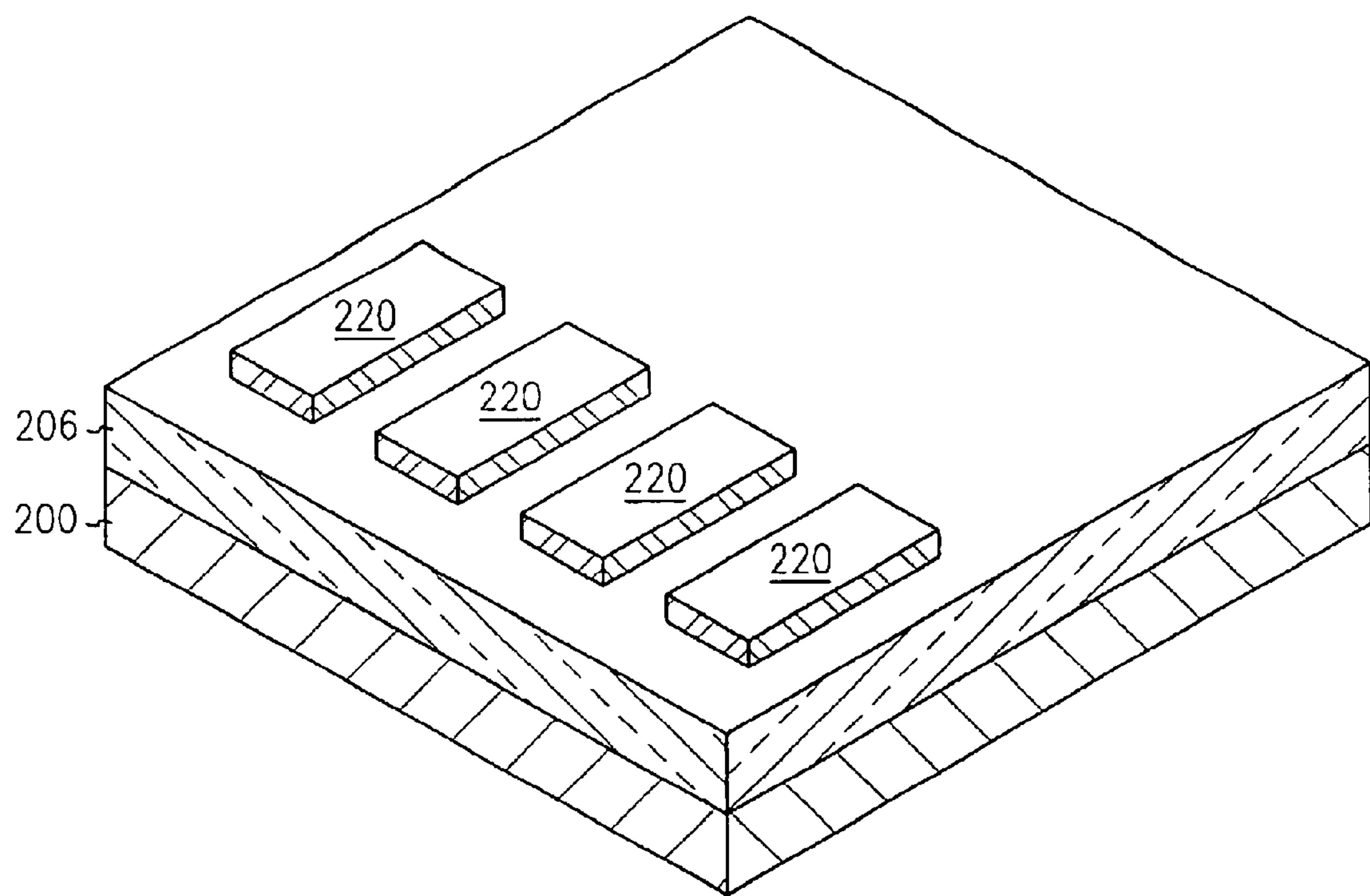


FIG. 5

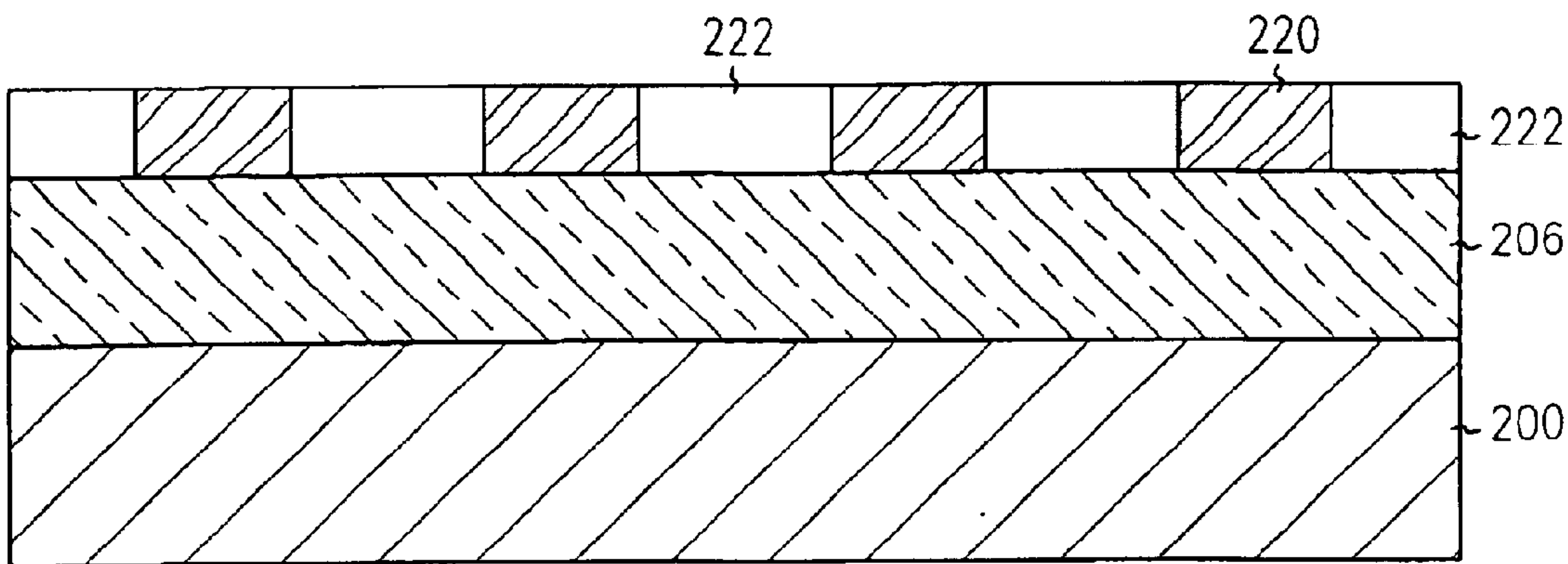


FIG. 6A

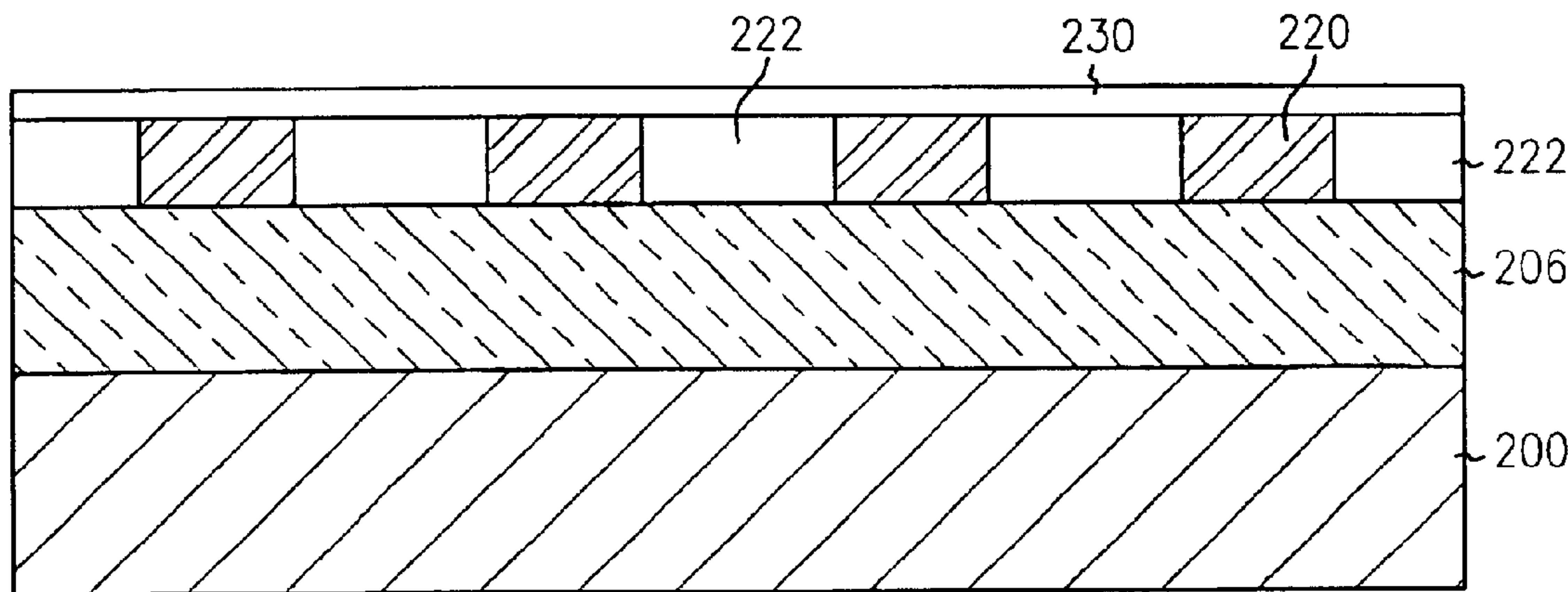


FIG. 6B

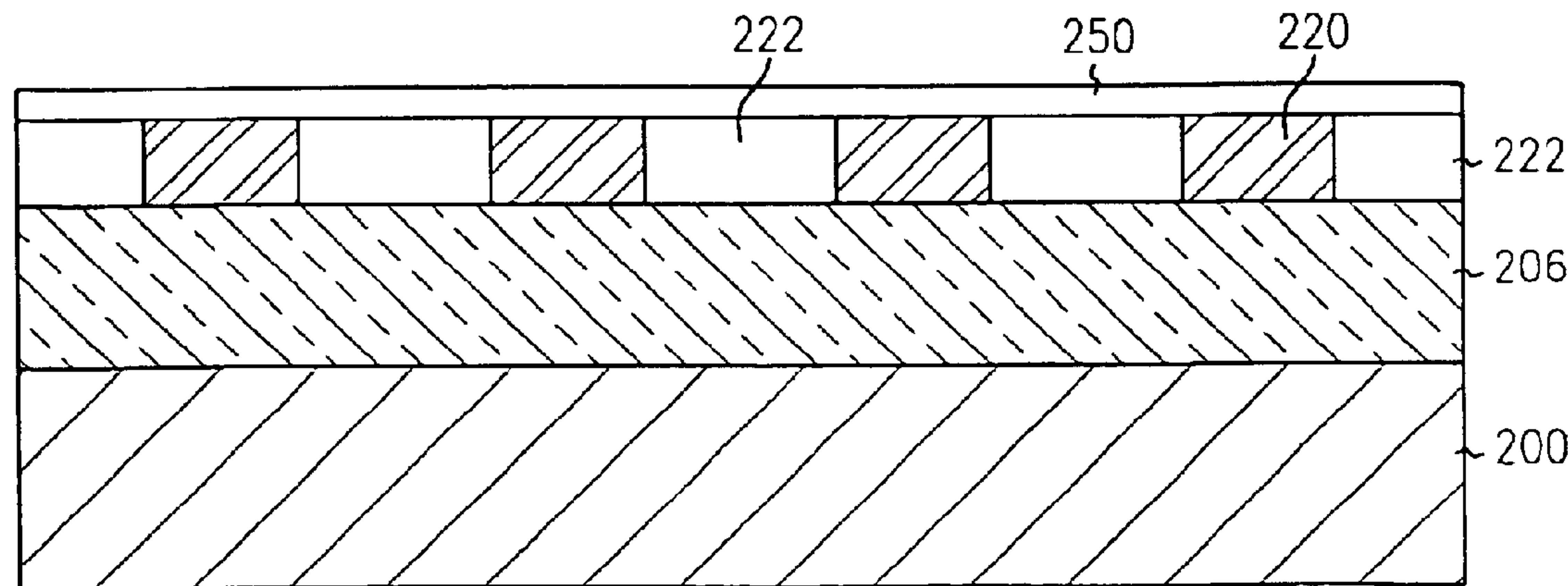


FIG. 7A

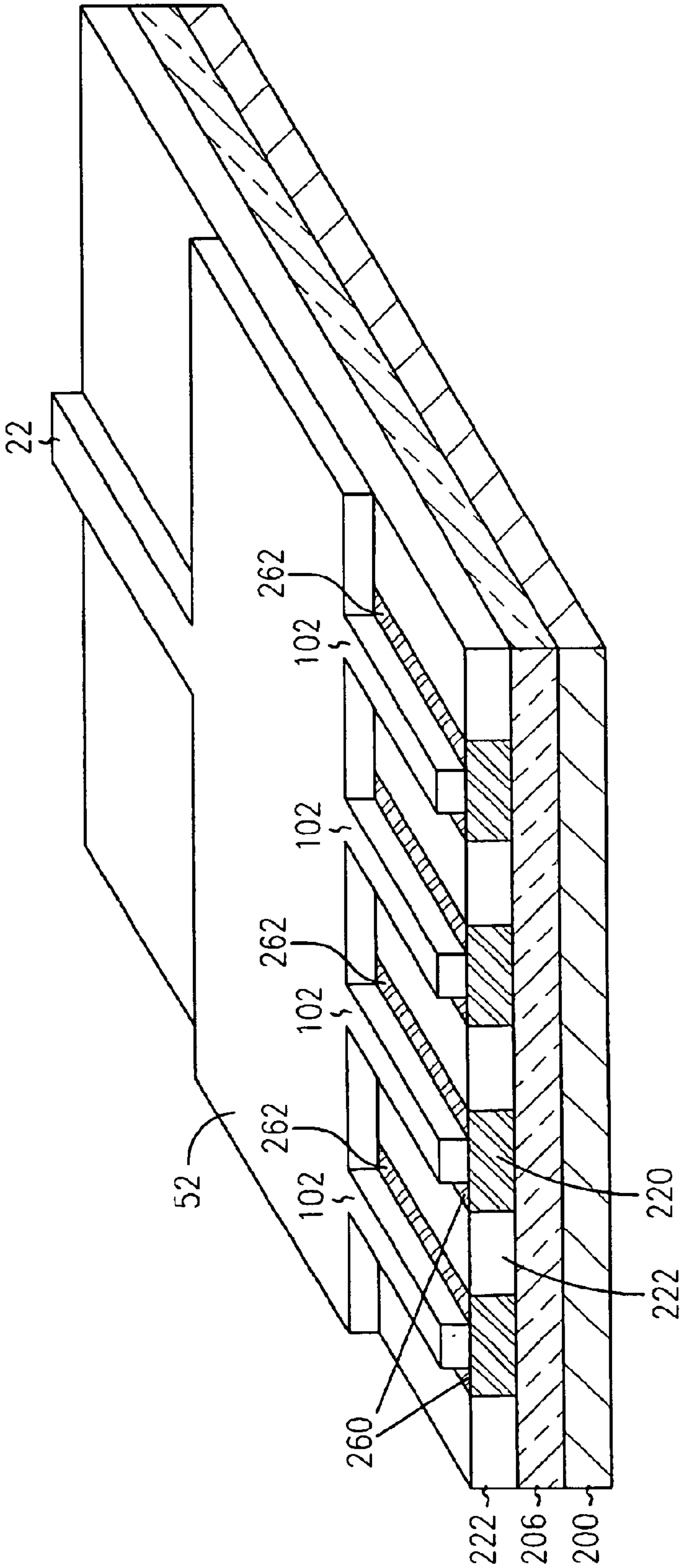


FIG. 7B

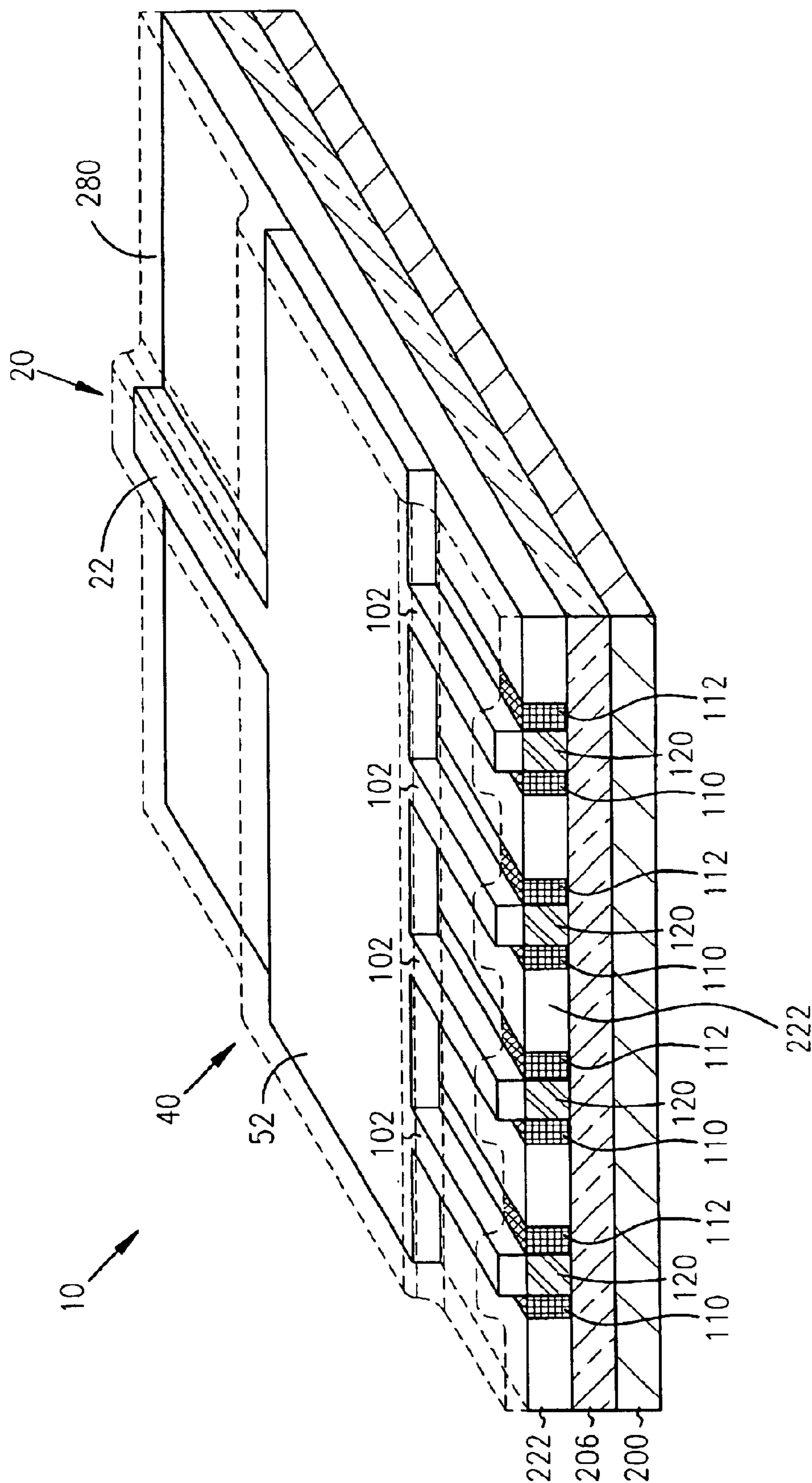


FIG. 8

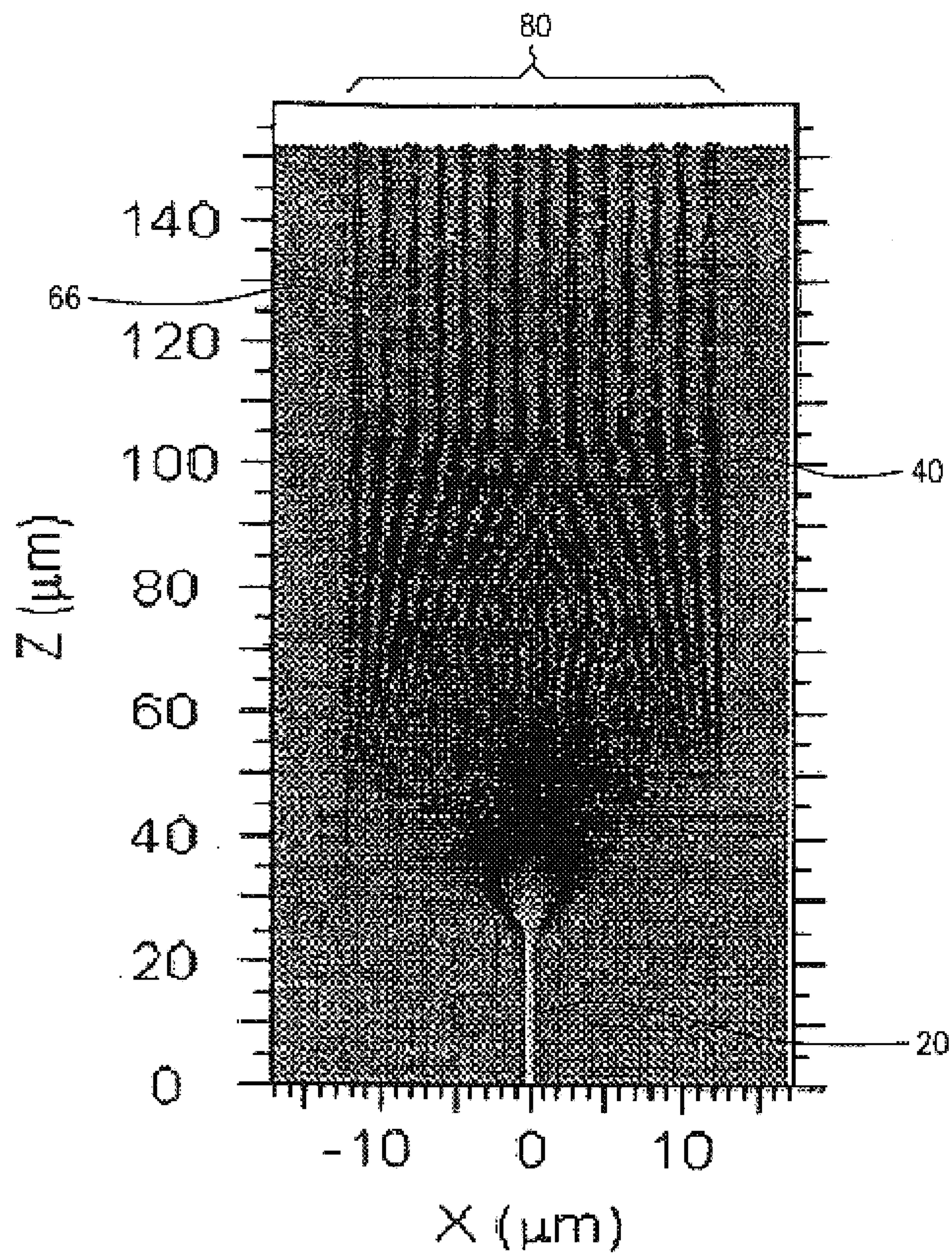


FIG. 9A

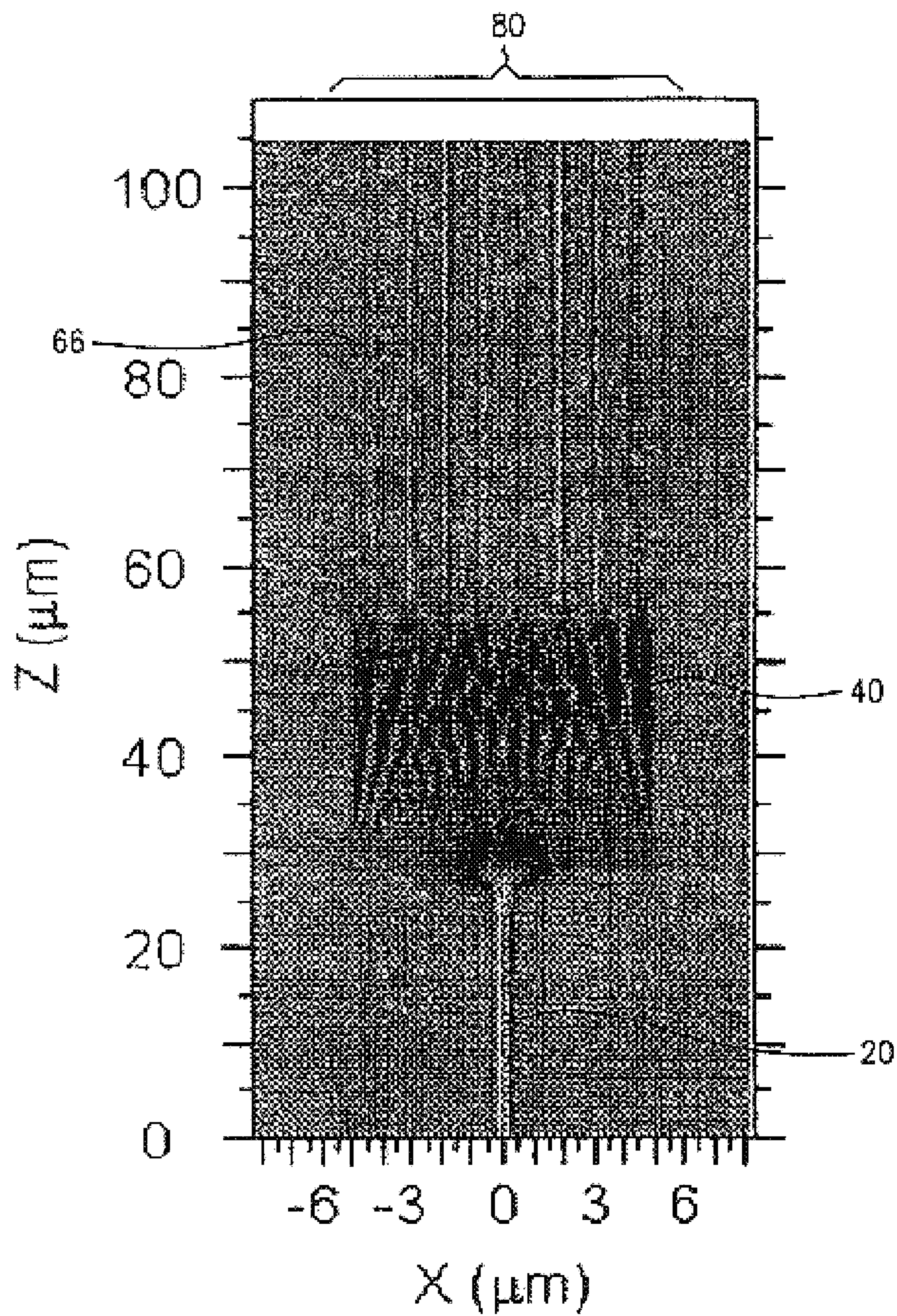


FIG. 9B

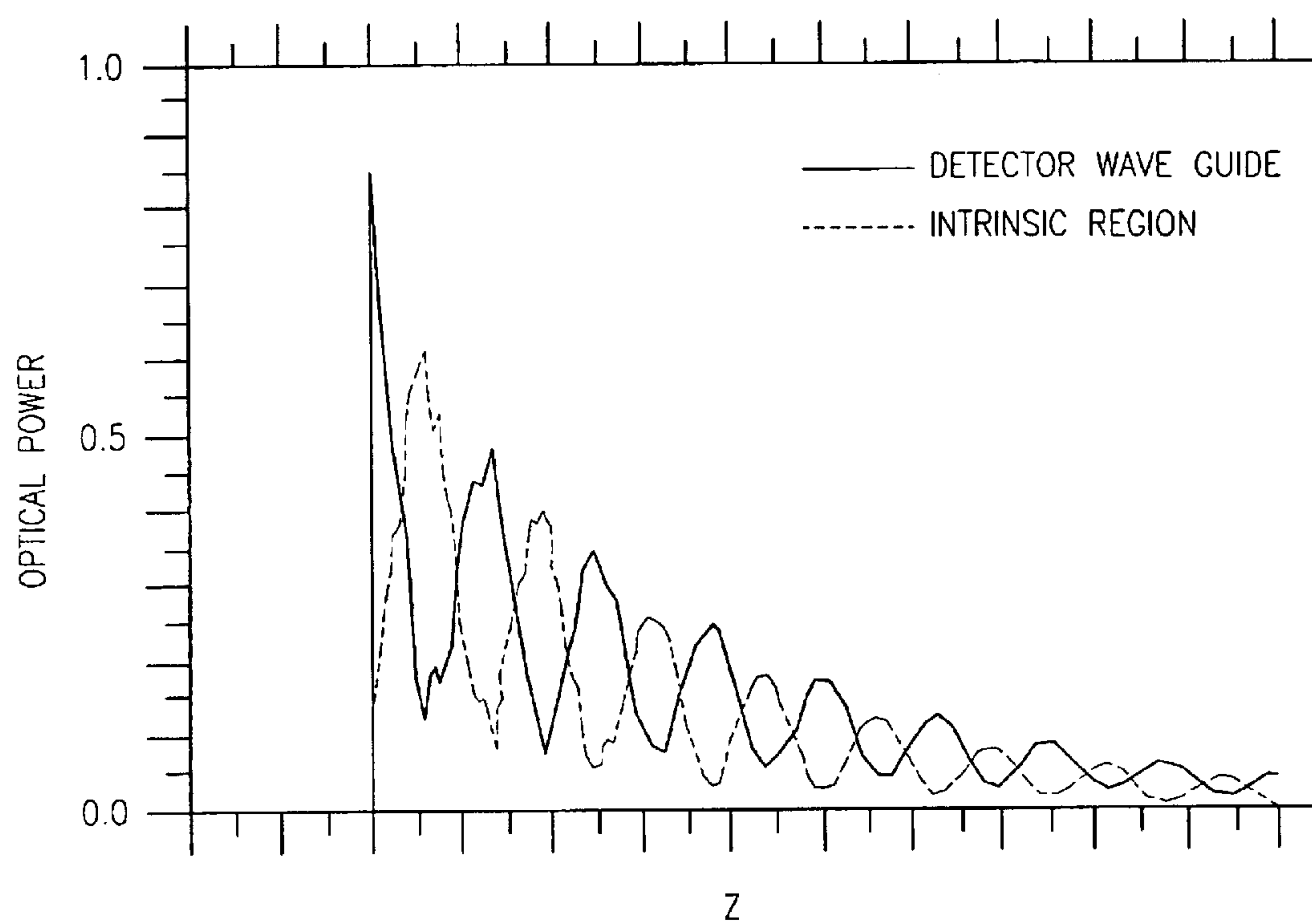


FIG. 10

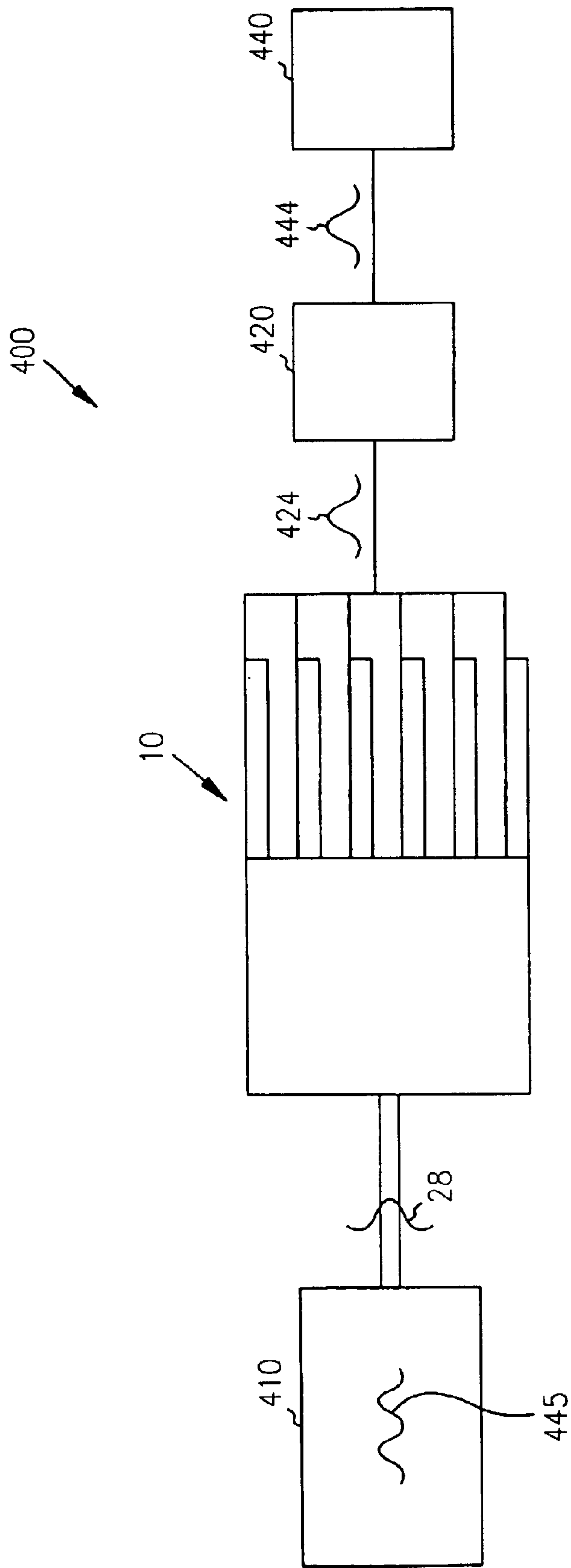


FIG. 11

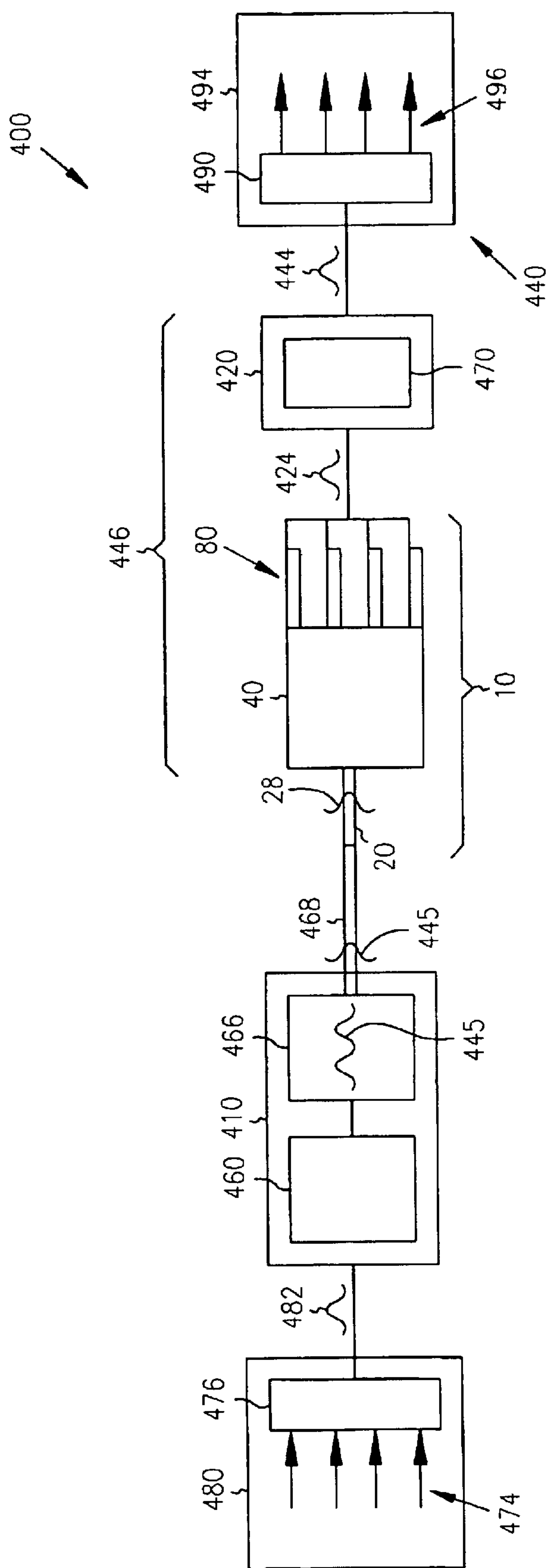


FIG. 12

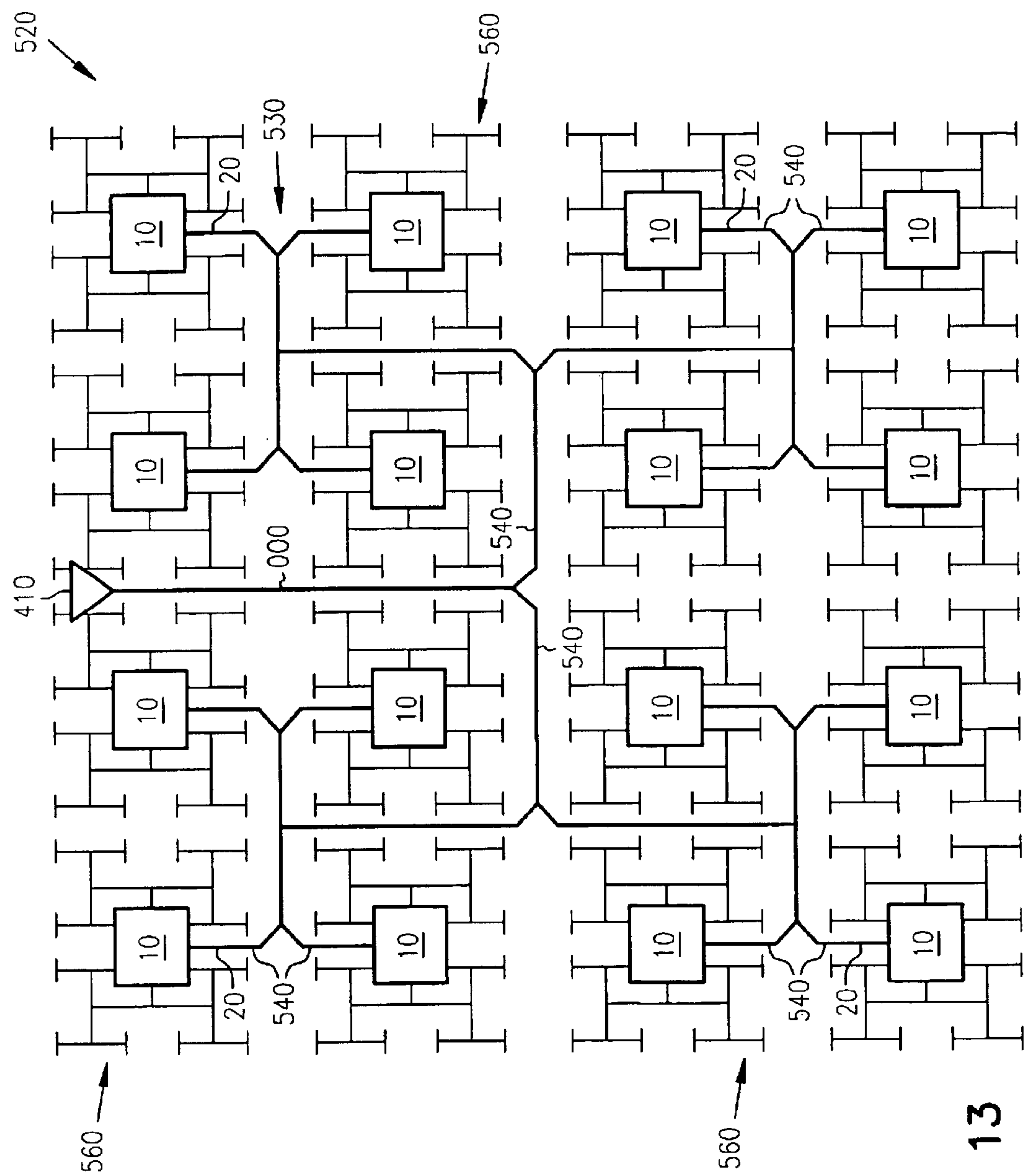


FIG. 13

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1XN FANOUT WAVEGUIDE
PHOTODETECTOR

FIELD OF THE INVENTION

The present invention pertains to photodetectors, and in particular to waveguide-based high-speed photodetectors.

BACKGROUND OF THE INVENTION

There are many lightwave applications, such as optical telecommunications and chip interconnects, that involve transmitting optical signals and converting them to electrical signals at high data rates. The systems for performing such transmission and conversion usually require a photodetector compatible with the speed and bandwidth of the optical signal. The typical photodetectors are PIN (p-type/intrinsic semiconductor material/n-type) semiconductor detectors.

To date, it has been a challenge to make a Si-based semiconductor PIN photodetector with a bandwidth of 10 GHz or greater. Conventional discrete PIN Si detectors operate at speeds of 2 GHz or less because of their relatively low absorption coefficient and low carrier collection efficiency. The best Si detector known today is the interdigitated lateral trench device (LTD), which operates at speeds of up to 6.5 GHz due to improved absorption by the trench structure.

It is well known that excess optical power density in PIN photodetectors causes detector speed degradation. This is especially true for waveguide-based PIN photodetectors because light is coupled in to a small region about the size of the waveguide. As a result, the detector may not be able to operate at high photocurrent where high-speed operation may require a high current. Where such a system employs evanescent coupling to the intrinsic region of the PIN detector, the intrinsic region can be expanded to dilute the optical power, which in turn prevents the creation of excess carriers. However, the light distribution in the expanded waveguide region (i.e., the waveguide plus the intrinsic region) is not uniform so that the detector electrodes need to be made relative large to ensure adequate detection of the photon-generated carriers. Unfortunately, the relatively large electrode area results in a relatively high detector capacitance, which reduces detector speed. Further, the non-uniform distribution of light in the expanded waveguide region can result in high optical fields, which generate local excess photon-generated carriers. This reduces the detector speed when the excess carriers have to diffuse out of the local excess carrier area to be collected by the electrodes.

Further, photon-generated carriers formed in the intrinsic region of a PIN detector may be collected either via electrodes in the top or bottom of the detector as discussed above, or by metal-semiconductor-metal (MSM) interdigitated electrodes on the surface of the intrinsic region. In the first design, the carrier collection distance is set by the required minimum detector thickness for efficient light absorption due to evanescent coupling with the waveguide. This thickness, however, limits the detector speed. In the latter design, photon-generated carriers also have to travel to the interdigitated electrodes across the detector, so that the detector thickness also limits the detector speed.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a plan view of the waveguide photodetector of the present invention, with the guided modes illustrated schematically as light rays;

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FIG. 2 is a cross-sectional view of the waveguide photodetector of FIG. 1 showing the core and cladding for the input waveguide, the MMI cavity and one of the detector waveguides, with the guided modes illustrated as electromagnetic waves;

FIG. 3 is a perspective end view of one of the waveguide detectors, showing the relationship between the waveguide portion of the detector, the underlying intrinsic layer, and the p+ and n+ electrodes surrounding the intrinsic layer, along with the conformal cladding layer (dashed line);

FIG. 4 is side view of a substrate with a silicon-on-insulator (SOI) structure formed thereon;

FIG. 5 is a top-down perspective view of the SOI structure of FIG. 4, with islands formed from a portion of the silicon layer;

FIG. 6A is a side view of the structure of FIG. 5, with insulation regions formed between the silicon islands;

FIG. 6B is the same side view as FIG. 6A, further including an optional thin layer of oxide atop the structure;

FIG. 7A is a side view of the structure of FIG. 6A, with a waveguide layer formed atop the structure;

FIG. 7B is a top-down perspective view of the structure of FIG. 7A, but with the waveguide layer processed to create the core regions for the input waveguide, the MMI cavity, and the N detector waveguides;

FIG. 8 is top-down perspective view of the structure of FIG. 7, with n+ and p+ electrodes formed in portions of the silicon island adjacent each waveguide detector core to form PIN detectors beneath each waveguide detector, and also showing the conformal cladding layer formed over the structure;

FIG. 9A is two-dimensional simulation of the optical power distribution in an example waveguide photodetector of the present invention having a 1x8 fanout MMI coupled to a single-mode input waveguide with a silicon core having a width of 0.25 microns surrounded by a SiO₂ cladding, the guided light having a wavelength of 1.3 microns;

FIG. 9B is two-dimensional simulation of the optical power distribution in an example of a waveguide photodetector of the present invention having a 1x14 fanout MMI coupled to a single-mode waveguide with a Si₃N₄ core having a width of 0.6 microns surrounded by a SiO₂ cladding, the guided light having a wavelength of 850 nm;

FIG. 10 is a plot of the normalized optical power distribution in a detector waveguide (solid line) along with a plot of the optical power in the intrinsic region below the waveguide (dashed line) illustrating the power transfer from the detector waveguide to the intrinsic region of the PIN detector as a function of the length of the intrinsic region;

FIG. 11 is a schematic diagram of an optoelectronic system that includes the waveguide photodetector of the present invention;

FIG. 12 is a schematic diagram of an on-board or on-chip optoelectronic communication system incorporating the waveguide photodetector of the present invention as a more detailed example of the generalized optoelectronic system of FIG. 11; and

FIG. 13 is a schematic diagram of an optoelectronic clocking circuit incorporating the waveguide photodetector of the present invention, as a more detailed example of the generalized optoelectronic system of FIG. 11.

DETAILED DESCRIPTION OF THE
INVENTION

In the following detailed description of the embodiments of the invention, reference is made to the accompanying

drawings that form a part hereof, and in which is shown by way of illustration specific embodiments in which the invention may be practiced. These embodiments are described in sufficient detail to enable those skilled in the art to practice the invention, and it is to be understood that other embodiments may be utilized and that changes may be made without departing from the scope of the present invention. The following detailed description is, therefore, not to be taken in a limiting sense, and the scope of the present invention is defined only by the appended claims.

With reference to FIGS. 1 and 2, there is shown an integrated waveguide-based photodetector system 10 comprising an input waveguide 20 having a core 22 and a cladding 24. In an example embodiment, the waveguide is designed to support a single waveguide mode 28, as illustrated schematically in FIG. 1 as a light ray and in FIG. 2 as an electromagnetic wave. The waveguide may be designed to support more than a single waveguide mode.

Input waveguide 20 also has an input end 34, an output end 36, and is optically coupled to a multi-mode interference (MMI) cavity 40 at the output end. The input waveguide may comprise any semiconductor or dielectric material transparent to the wavelength of light being detected. In an example embodiment, the material making up core 22 is preferably high index, and the material making up cladding 24 is preferably low index. For example, the waveguide may comprise Si_3N_4 for transmission of light having a wavelength of 850 nm or intrinsic silicon for wavelengths of 1 micron or greater. Input waveguide cladding 24 may be, for example, SiO_2 , which has a relatively low refractive index (about 1.5) as compared to that of Si_3N_4 (about 3.5) at near-infra-red and infra-red wavelengths. Use of a high-index core and a low-index cladding allows for the input waveguide to have a relatively small (i.e., sub-micron) thickness T1 (X-dimension) and width W1 (Y-dimension).

MMI cavity 40 has an input end 44 to which output end 36 of input waveguide 20 is optically coupled. MMI cavity 40 also has an output end 46 opposite input end 44, and a length L2. MMI cavity 40 is formed from a semiconductor or dielectric material transparent to the wavelength of light being detected. For the sake of convenience, MMI cavity 40 preferably comprises the same material as input waveguide 20 so that the input waveguide and the MMI cavity can be formed as an integrated structure. In an example embodiment, the thickness T2 of MMI cavity 40 is the same as the thickness T1 of waveguide 20, while the width (Y-dimension) W2 of the MMI cavity is greater than the width W1 of the waveguide.

By way of example, input waveguide 20 may have a width W1 in the range from about 0.1 to about 0.5 microns, while MMI cavity 40 may have a width W2 in the range from about 5 microns to 10 microns. MMI cavity 40 includes a core 52 and a cladding 54 surrounding the core. In an example embodiment, core 52 comprises the same material as core 22 and cladding 54 comprises the same material as cladding 24. Further in an example embodiment, cores 22 and 52 are contiguous and claddings 24 and 54 are contiguous.

The length L2 of MMI cavity 40 is designed so that the incoming single waveguide mode 28 from waveguide 20 spreads (i.e., “fans out”) in the Y-direction into N multiple waveguide modes 60 within the MMI cavity. Each mode 60 carries a corresponding fraction of the input energy of waveguide mode 28. In FIG. 1, multiple waveguide modes 60 are schematically represented as light rays. MMI cavity 40 serves to disperse the optical power density of single

waveguide mode 28 by a factor of N. Further, the length L2 of MMI cavity 40 is designed so that interference nodes 66 arising from the constructive interference of the N waveguide modes (i.e., the intersection of the light rays) are located at or near cavity output end 46.

System 10 further includes an array 80 of N ($N \geq 2$) waveguide detectors 82 optically coupled to MMI cavity 40 at output end 44 at or near interference nodes 66. Each waveguide detector 82 includes a waveguide 100 with a core 102, a cladding 104, a lower surface 106, a core width W_C and an overall width (core plus cladding) of W_N . Waveguide 100 preferably supports a single guided mode 106. Widths W_C and W_N can vary between waveguides but is preferably the same for each waveguide for the sake of convenience. Waveguide detectors 82 further include p+ and n+ electrodes 110 and 112 arranged on opposite sides of waveguide 100 below the plane defined by waveguide lower surface 106.

FIG. 3 is a perspective close-up endview of one of waveguide detectors 82. Electrodes 110 and 112 are separated by an intrinsic region 120 residing directly underneath waveguide lower surface 106, which is optically coupled to waveguide 100. Intrinsic region 120 therefor has a width equal to or substantially equal to the core width W_C of waveguide 100. In an example embodiment, intrinsic region 120 is formed under waveguide 100 in combination with the self-aligned formation of n+ and p+ electrodes 110 and 112, formed with respect to waveguide core 102. Intrinsic region 120 is made from a semiconductor material, and in example embodiments comprises either silicon or germanium.

Thus, each waveguide detector 82 has a PIN configuration with the photo-generated carrier collection distance within intrinsic region 120 equal to or substantially equal to core width W_C of waveguide 100. As mentioned above, it is preferable that waveguides 100 be single mode so that the core width W_C is as small as possible. The core width W_C can be made sub-micron by using a high-index contrast between core 102 and cladding 104. In an example embodiment, core 102 includes a high-index integrated-circuit (IC) compatible material, such as Si_3N_4 surrounded by cladding 104 that includes a low index dielectric such as silicon dioxide. This allows for very fast detector speeds, e.g., greater than about 10 GHz when detectors 82 have an intrinsic region comprising silicon, and greater than about 40 GHz when detectors 82 have an intrinsic region comprising germanium.

The difference in detector speeds between silicon and germanium is related to the higher absorption coefficient and carrier mobility of germanium, which is 4× faster than that of silicon. An advantage of using germanium in forming intrinsic region 120 is that the length L3 of the intrinsic region can be made short (e.g., about 5 microns) as compared with the length associated with silicon (e.g., about 80 microns long). Thus, forming intrinsic region 120 from germanium provides for a compact waveguide photodetector system 10 with smaller capacitance.

Each waveguide detector 82 has a longitudinal configuration where light is transferred to and absorbed by intrinsic region 120 as it propagates down detector waveguide 100 (i.e., the Z direction). This allows each waveguide detector 82 to have high total quantum efficiency (e.g., greater than about 80%), since the length L3 of intrinsic region 120 can be tailored to provide the optimum absorption efficiency. The length L3 of intrinsic region 120 (also called the “absorption length”) has minimal impact on detector speed since the photon carrier collection direction is the Y-direction, which is perpendicular to the light propagation and absorption direction, which is the Z-direction.

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Further, photon-generated carriers are formed mostly in intrinsic region **120** rather than under n+ electrode **110** and p+ electrode **112** because there is no direct light path to the electrodes. Thus, fewer slow-drift carriers, which reduce the speed of the detector, are generated.

In waveguide detector system **10**, the screening effect of high-density space-charge fields due to high-density photon-generated carriers by high optical power density is mitigated by dividing the incoming power density by a factor of N and then coupling the diluted power into the N separate waveguide detectors **82**. This allows for fast detection speeds. Further, detectors **82** can be arranged to operate in parallel so that a high-output photocurrent (e.g., greater than about 100 microamperes) is generated. The amount of output photocurrent depends on the number of parallel waveguide detectors used. In example embodiment, 10 parallel waveguide detectors are used to generate an output photocurrent of about 100 microamperes. The use of multiple parallel waveguide detectors **82** provides for a minimum electrode area and thus a minimum capacitance and resistance, further increasing the speed of waveguide photodetector system **10**.

Method of Fabrication (FIGS. 4–10)

With reference now to FIG. 4, the method of fabricating an integrated waveguide-based photodetector system **10** as described above begins with providing a substrate **200**. Substrate **200** is preferably formed from an IC-compatible material, such as a semiconductor material such as silicon, or sapphire. For the sake of discussion, it is presumed below that substrate **200** is silicon.

Atop silicon substrate **200** is formed a insulating layer **206**, such as silicon dioxide or other dielectric. Insulating layer **206** serves to optically and electrically isolate substrate **200** from system **10** to be formed thereon. Thus, in an example embodiment, insulating layer **206** may have a thickness, for example, of about 1 to about 3 microns.

Atop insulating layer **206** is formed a semiconductor layer **210**, which can be Si, Ge, $\text{Ge}_x\text{Si}_{1-x}$, or Ge on Si. For the sake of discussion, it is assumed layer **210** is Si, thereby forming a silicon-on-insulator (SOI) structure. Silicon layer **210** may have a thickness, for example, of 0.25 to 0.5 microns.

In FIG. 5, silicon layer **210** is lithographically processed using well known techniques (e.g., coating with a layer of photoresist, photolithographically exposing the resist with a pattern, developing the resist and then etching the resist) to define silicon islands **220** over a portion of insulating layer **206**.

In FIG. 6A, an oxide layer **222** (e.g., SiO_2) is deposited over the structure of FIG. 5 and is polished, e.g., via a chemical-mechanical polish (CMP) process, until the top of islands **220** are exposed. This results in silicon islands **220** being insulated from each other by portions of oxide layer **222**.

In an example embodiment, the surface of silicon islands **220** may be optionally processed using a standard gate oxide cycle, which includes buff oxidation to remove CMP-induced damage, pre-clean, gate oxidation, and a passivation anneal. Further, with reference to FIG. 6B, in another example embodiment, a stress release layer **230** of oxide of about 100 to 200 Angstroms thick is optionally formed atop silicon islands **220** to facilitate the next step in the process. The stress release layer may also serve as cladding **104** formed between intrinsic region **120** and core **104** of waveguide **100** (FIG. 2).

In FIG. 7A, a waveguide layer **250** is formed atop the structure of FIG. 6A (or alternatively, atop the structure of FIG. 6B). In one example embodiment, waveguide layer **250**

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comprises one of Si, Ge, Ge on Si, $\text{Ge}_x\text{Si}_{1-x}$, SiO_xN_y , and Si_3N_4 . Waveguide layer **250** has a thickness designed to support a given number of waveguide modes at a given wavelength when surrounded by a cladding layer of a given material. Thus, in an example embodiment, the thickness of waveguide layer **250** can range from the sub-micron (e.g., from about 0.1 micron) to several microns.

In FIG. 7B, waveguide layer **250** is lithographically processed to define core **22** of waveguide **20**, core **52** of MMI cavity **40** and cores **102** of waveguides **100**, with cores **102** aligned to silicon islands **220**. Each core **102** does not cover the entire silicon island **220** so that portions **260** and **262** of each island on either side of the core are exposed.

Exposed portions **260** are n+ doped and exposed portions **262** are p+ doped to form n+ electrode **110** and a p+ electrode **112** adjacent each core **102**. In an example embodiment, doping is achieved by ion implantation in a manner that makes n+ electrode **110** and p+ electrode self-aligned with core **102**.

In FIG. 8, a cladding layer **280** is conformally deposited atop the remaining waveguide layer **250** to complete the formation of input waveguide **20**, MMI cavity **40** and detector waveguides **100**. Cladding layer **280** may be any dielectric, such as silicon dioxide or polyimide, so long as the index of the cladding layer is less than that of waveguide layer **250** for the particular operating wavelength.

The undoped silicon region remaining beneath each waveguide core **102** becomes intrinsic region **120**. The width of intrinsic layer **120** is substantially equal to the width W_c of core **102** and defines the carrier collection distance. All the n+ electrodes **110** and p+ electrodes **112** are preferably connected in parallel so that detectors **82** form array **80** of N parallel detectors capable of generating a high photocurrent current.

With reference to FIGS. 9A and 9B, there is shown two-dimensional simulations of the distribution of optical power in two example waveguide photodetector systems **10** according to the present invention. The simulations were performed using a commercial software package called the rSoft BPM simulator, available from www.rssoftinc.com.

In FIG. 9A, core **22** of waveguide **20** is modeled based on a silicon core of width 0.25 microns surrounded by an SiO_2 cladding, thereby providing an index differential between the core and cladding of about 1.5. The guided light has a wavelength of 1.3 microns. In the present invention, the dimensions of MMI cavity needed to achieve a given value of N for the fanout can be readily determined by simulation. MMI cavity **40** of FIG. 9A has a length L_2 of approximately 30 microns and a width W_2 of approximately 10 microns and supports a fanout of $N=8$. The total optical power preserved within the 1×8 fanout is calculated at about 81%. The simulation also shows interference nodes **66** at which waveguide detectors **82** are located.

In FIG. 9B, core **22** of waveguide **20** is modeled based on Si_3N_4 core with a width of 0.6 microns surrounded by an SiO_2 cladding. The guided light has a wavelength of 0.85 microns. MMI cavity **40** of FIG. 9B has a length L_2 of approximately 100 microns and a width W_2 of approximately 25 microns and supports a fanout of $N=14$. The total optical power preserved within the 1×14 fanout is calculated at about 84%.

In FIG. 10, there is shown a three-dimensional simulation of the optical power distribution in a Si_3N_4 detector waveguide **100** having a core width W_c of 0.4 microns. The wavelength of the guided light is 850 nm, and intrinsic region **120** beneath the waveguide is silicon with dimensions $1 \text{ micron} \times 1.2 \text{ microns} \times 75 \text{ microns}$. The capacitance of the

waveguide detector is about 10 fF. From the plot, it can be seen how the optical power in the waveguide (solid line) oscillates and decays as the light propagating in waveguide **100** is evanescently coupled to and absorbed by underlying intrinsic region **120**. Likewise, the optical power in intrinsic region **120** (dashed line) also oscillates in synchrony (but 90 degrees out of phase) with the waveguide optical power, and decays as the light is absorbed in the intrinsic region. The absorbed light results in the generation of photon-generated carriers, resulting in a current detected by surrounding electrodes **110** and **112**. The coupling efficiency is calculated to be in excess of about 90%. Quantum efficiency can be optimized by selecting the appropriate length **L3** of intrinsic region **120**. The longer **L3** is, the higher the quantum efficiency. However, the length **L3** is limited to minimize the capacitance. The carrier collection speed is optimized by selecting the smallest possible cross-section core width W_c for waveguide **100**.

Optoelectronic Systems

With reference to FIG. 11, there is shown a generalized optoelectronic system **400** that includes the waveguide photodetector **10** of the present invention. Optoelectronic system **400** includes an optical or optoelectronic input device **410** optically coupled to input waveguide **20** of waveguide photodetector **10**. Input device **410** may include, for example, a laser diode or a vertical cavity surface emitting laser (VCSEL). Optoelectronic system **400** further includes an electronic or optoelectronic output device **420** electrically coupled to waveguide detectors **82** to receive a photocurrent electrical signal **424** generated by waveguide photodetector **10**. Optionally included in optoelectronic system **400** is a second output device operatively coupled to the first output device for receiving an electrical signal **444** from the first output device and further processing the signal.

In operation, input device **410** generates an optical signal (i.e., light) **445** and inputs the optical signal to input waveguide **20**. Optical signal **445** propagates down input waveguide **20** as guided mode **28**. As discussed above, guided mode **28** is fanned out (dispersed) into **N** guided modes **60** by MMI cavity **40**, which forms **N** interference nodes **66** (FIG. 1). Waveguide detectors **82** detect the light at interference nodes **66** and convert the light into a photocurrent electrical signal **424**, which is outputted to and received by output device **420**.

Optoelectronic system **400** represents a large number of possible systems. By way of example, with reference to FIG. 12, optoelectronic system **400** represents an on-board or on-chip communication system, wherein input device **410** constitutes an optical transmitter, and waveguide photodetector **10** and output device **420** together constitute an optical receiver **446**. Input device/optical transmitter **410** includes driver electronics **460** (e.g., a transimpedance amplifier) electrically connected to a laser diode **466**, and a waveguide **468**. Waveguide **468** is optically coupled to the laser diode at one end and to waveguide **20** of input device/optical transmitter **410** at its other end. In an example embodiment, waveguide **468** is single mode. In a further example embodiment, output device **420** includes preamplifier electronics **470**.

In operation, a plurality of electronic signals **474** are multiplexed by a time-division multiplexer **476** residing on a first chip or board **480** to form a multiplexed electrical signal **482**. Multiplexed electrical signal **482** is passed to input device/optical transmitter **410**. Input device/optical transmitter **410** receives multiplexed electrical signal **482** and converts it to optical signal **445**, which is inputted to waveguide **468**. Optical signal **445** is transmitted through

waveguide **468** as a guided mode and passes to waveguide **20**, where it continues to propagate as waveguide mode **28**. As described above in connection with FIG. 1, waveguide mode **28** enters MMI cavity **40** and is fanned out (dispersed) by MMI cavity **40** and detected by waveguide detector array **80** to produce photocurrent electrical signal **424**.

Photocurrent electrical signal **424** is outputted to and received by pre-amplifier electronics **470** in output device **420**. Signal **424** is processed by preamplifier electronics **470** to form an electronic signal **444**, which is passed to a time-division demultiplexer **490** as part of a second chip or board **494** constituting second output device **440** (FIG. 11). Time-division demultiplexer **490** receives electronic signal **444** and forms demultiplexed electronic signals **496** to be processed by other electronic elements (not shown) on second chip or board **494**.

In another example embodiment, optoelectronic system **400** constitutes a telecommunication/data communication system similar in design to the on-chip or on-board system described above, with waveguide **490** being a length of optical fiber (single mode or multimode), and including analogous multiplexing and demultiplexing processing elements and processes.

In yet another example embodiment, optoelectronic system **400** can be used to form an optoelectronic clocking source. An optoelectronic clocking source utilizing the waveguide photodetector of the present invention can perform high-speed clocking, since the large amounts of optical power and the corresponding high photocurrent required can be handled by the waveguide photodetector of the present invention.

With reference to FIG. 13, there is shown an example optical clocking source system **520** that includes optical/optoelectronic input device **410** coupled to an optical edge tree **530**. Optical edge tree **530** comprises a main waveguide **536** from which extends a number of equal length waveguide branches **540**, each capable of supporting a portion of optical signal **445**. Each waveguide branch **530** is equal in length and is connected to the input waveguide **20** of a waveguide photodetector **10**.

The output of each waveguide photodetector **10** is connected to an electrical edge tree **560** having electrical (e.g., conducting) branches **570** of equal length that support a portion of photocurrent electrical signal **424**. Each electrical branch **570** of electrical edge tree **560** is connected to an output device **420**, such as a transimpedance amplifier (FIG. 11). The equal lengths of the waveguide branches and the equal lengths of the electrical branches provide for the equal timing of the optical and electrical signals necessary in a clocking circuit. As optical waveguide branches can be longer than electrical branches when forming clocking circuits, the clocking signal source (e.g., input device **410**) can be located relatively far away (e.g., off-chip) in an optoelectronic clocking circuit as compared to an all-electrical clocking circuit.

While the present invention has been described in connection with preferred embodiments, it will be understood that it is not so limited. On the contrary, it is intended to cover all alternatives, modifications and equivalents as may be included within the spirit and scope of the invention as defined in the appended claims.

What is claimed is:

1. A waveguide photodetector system, comprising:
 - a multiple mode interference (MMI) cavity having an input end and an output end;
 - an input waveguide optically coupled to the MMI cavity at the input end; and

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an array of detector waveguides optically coupled to the MMI cavity at the output end, each detector waveguide including a waveguide having a core, a cladding, and a lower surface and an intrinsic region disposed underneath the lower surface and surrounded by first and second electrodes, wherein the core is longitudinally aligned along the intrinsic region and optically coupled to the intrinsic region.

2. The system of claim 1, wherein the input waveguide is single-mode.

3. The system of claim 2, wherein the MMI cavity produces N interference nodes at the output end, and wherein each detector waveguide is arranged at or near an interference node.

4. The system of claim 1, wherein the input waveguide, MMI cavity and detector waveguides comprise a material selected from the group of materials comprising: Si, Ge, Ge on Si, $\text{Ge}_x\text{Si}_{1-x}$, SiO_xN_y , and Si_3N_4 .

5. The system of claim 3, wherein the intrinsic region comprises silicon.

6. The system of claim 3, wherein the intrinsic region comprises germanium.

7. The system of claim 1, wherein the first and second electrodes associated with each of the intrinsic regions are connected in parallel.

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8. The system of claim 7, further including:

an input device optically coupled to the input waveguide to provide an optical signal to be detected; and

an output device electrically coupled to the first and second electrodes so as to receive an outputted photocurrent.

9. The system of claim 8, wherein the input device includes a laser.

10. The system of claim 1, wherein the first and electrodes are respectively n+ doped and p+ doped silicon.

11. The system of claim 1, wherein the detector waveguides are coupled to the respective intrinsic regions by evanescent coupling.

12. The system of claim 1, wherein the intrinsic region has a carrier collection distance of less than 1 micron.

13. The system of claim 1, wherein the core of each detector waveguide has a core width, and wherein each intrinsic region has a carrier collection distance substantially equal to the core width.

14. The system of claim 1, wherein the detector waveguides are single mode.

15. The system of claim 1, wherein the system has a detection speed of 10 GHz or greater.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 6,856,733 B2
APPLICATION NO. : 10/008922
DATED : February 15, 2005
INVENTOR(S) : Zheng

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Title Page, Item (56), under "U.S. Patent Documents", in column 1, line 5,
delete "2003/0027797 * 2/2003" and insert -- 2003/0002797 * 1/2003 --, therefor.

In column 9, line 2, in Claim 1, delete "waveauide" and insert -- waveguide --,
therefor.

Signed and Sealed this

Thirteenth Day of May, 2008

A handwritten signature in black ink, reading "Jon W. Dudas". The signature is stylized, with a large, looped initial "J" and a cursive "Dudas".

JON W. DUDAS
Director of the United States Patent and Trademark Office