

US006567053B1

(12) **United States Patent**
Yablonovitch et al.

(10) **Patent No.: US 6,567,053 B1**
(45) **Date of Patent: May 20, 2003**

(54) **MAGNETIC DIPOLE ANTENNA
STRUCTURE AND METHOD**

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(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 76 days.

(21) Appl. No.: **09/781,720**

(22) Filed: **Feb. 12, 2001**
(Under 37 CFR 1.47)

(51) **Int. Cl.⁷** **H01Q 13/10**

(52) **U.S. Cl.** **343/767; 343/700 MS;**
343/770; 343/789; 343/895

(58) **Field of Search** 343/700 MS, 702,
343/767, 770, 789, 795, 895; H01Q 13/10

(56) **References Cited**

U.S. PATENT DOCUMENTS

3,648,172 A * 3/1972 Nakahara et al. 324/51
3,845,487 A * 10/1974 Lammers 343/768
4,328,502 A * 5/1982 Scharp 343/771
5,184,144 A * 2/1993 Thombs 343/781 R

5,337,065 A * 8/1994 Bonnet et al. 343/767
5,726,666 A * 3/1998 Hoover et al. 343/770
5,754,143 A * 5/1998 Warnagiris et al. 343/767
5,764,190 A 6/1998 Murch et al.
5,900,843 A * 5/1999 Lee 343/767

OTHER PUBLICATIONS

Wheeler, Harold A., Small Antennas, IEEE Transactions on
Antennas and Propagation. Jul. 1975.

Sievenpiper, D.; Zhang, L.; Broas, Romulo F. Jimenez;
Alexopolous, Nicholas G; Yablonovitch, Eli. High-Imped-
ance Electromagnetic Surfaces With a Forbidden Frequency
Band—IEEE Transactions on Microwave Theory and Tech-
niques, vol. 47, No. 11, Nov., 1999.

* cited by examiner

Primary Examiner—Tho Phan

(57) **ABSTRACT**

The spiral sheet antenna allows a small efficient antenna
structure that is much smaller than the electromagnetic
wavelength. It achieves the small size by introducing a high
effective dielectric constant through geometry rather than
through a special high dielectric constant material. It typi-
cally includes a rectangular cylinder-like shape, with a seam.
The edges of the seam can overlap to make a high
capacitance, or they can make a high capacitance by simply
having the edges of the seam very close to each other. The
high capacitance serves the same role as a high dielectric
constant material in a conventional compact antenna.

27 Claims, 19 Drawing Sheets

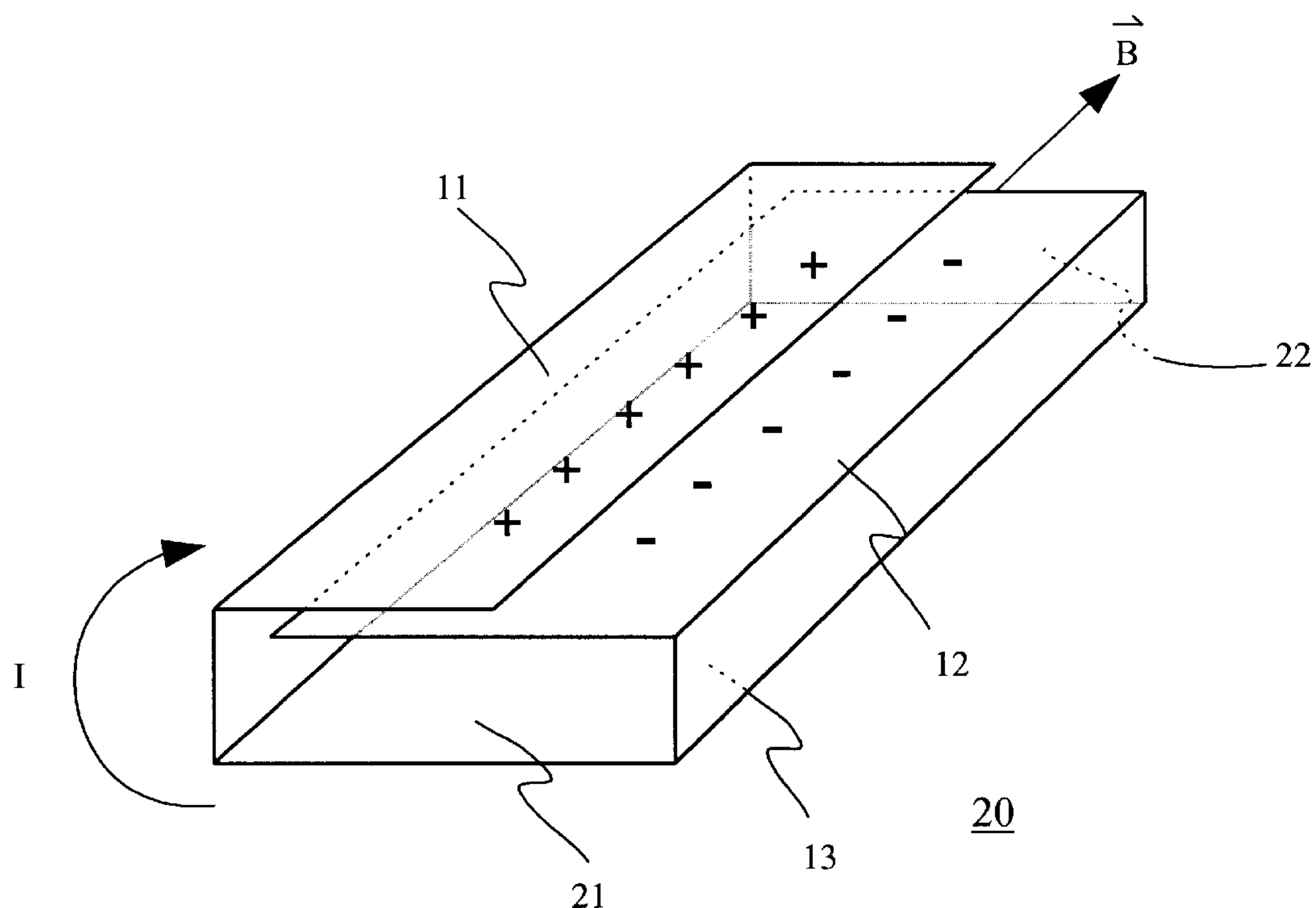


Fig 1

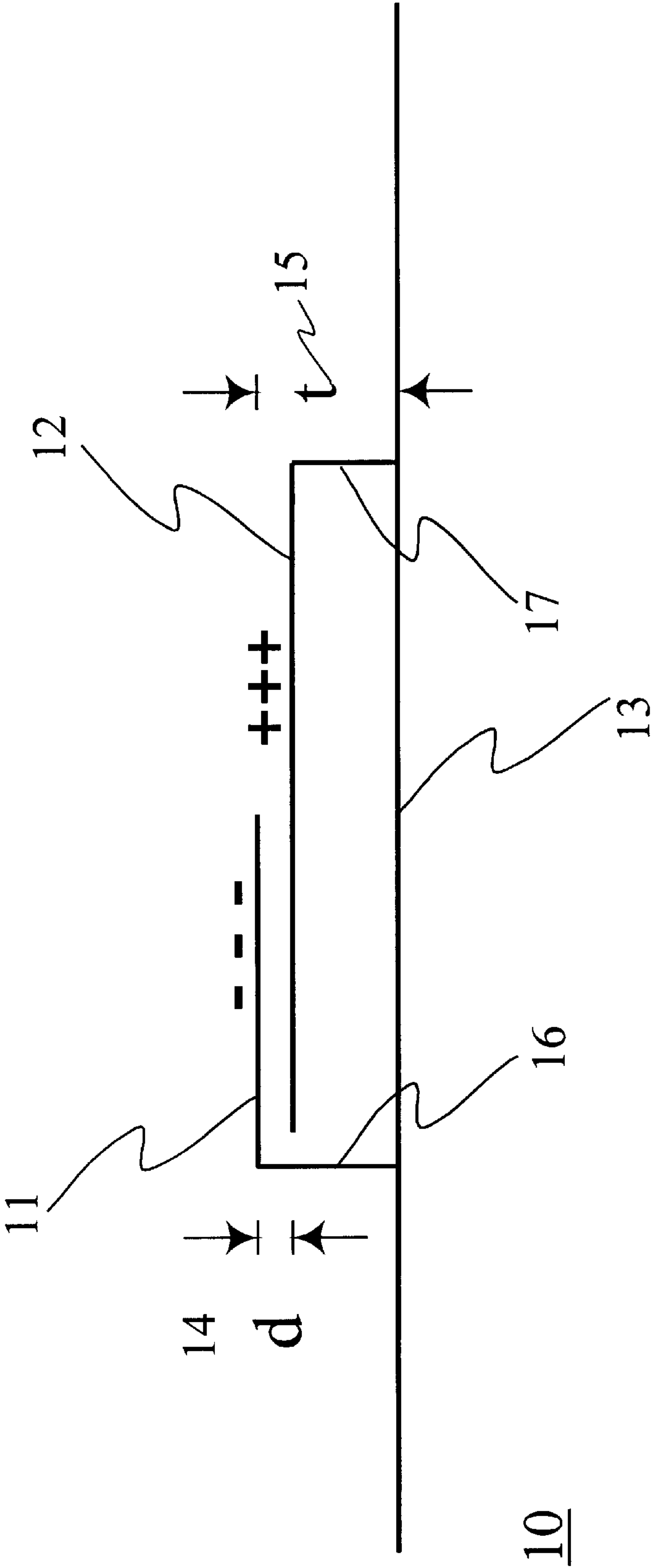


Fig 2A

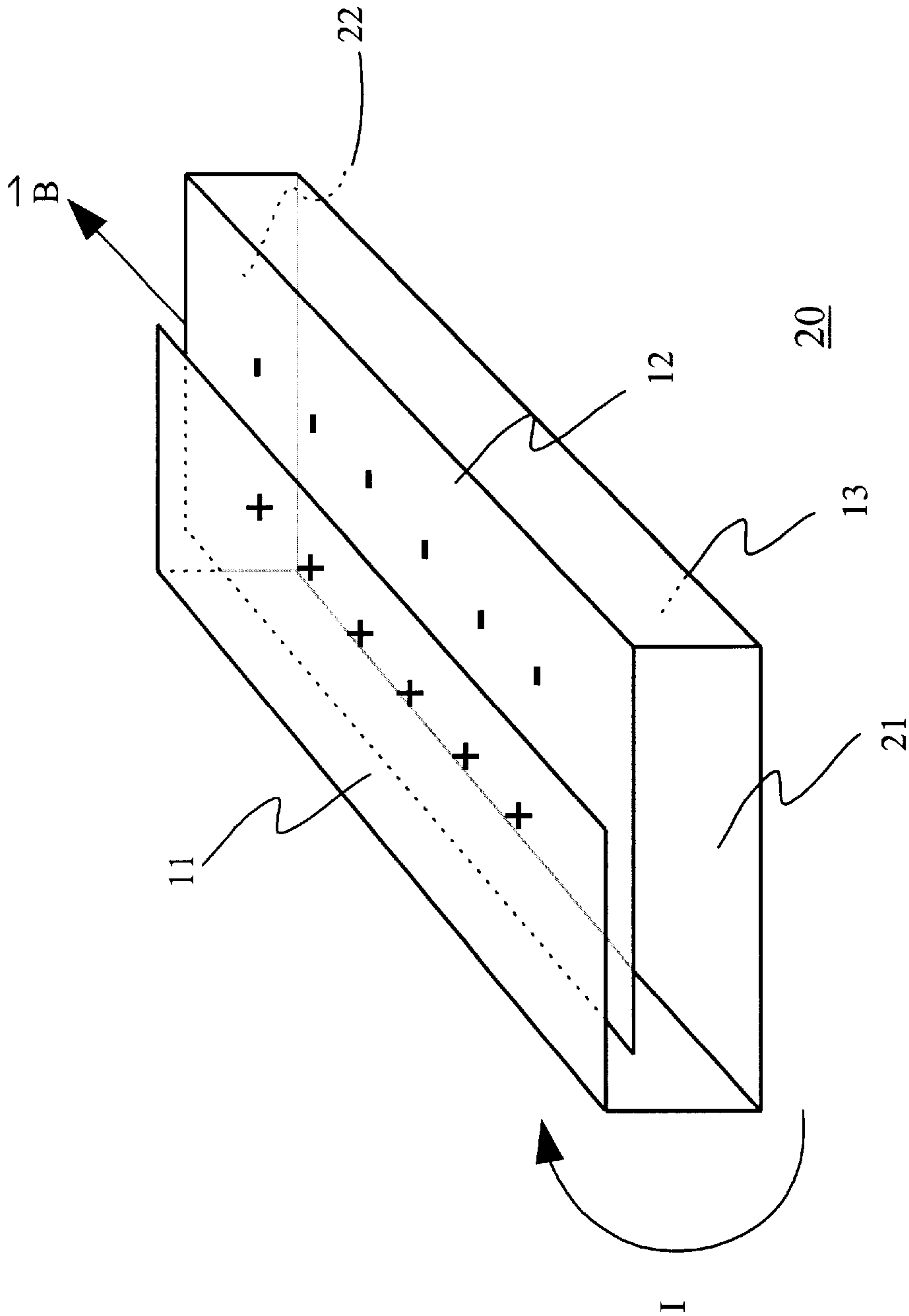


Fig 2B

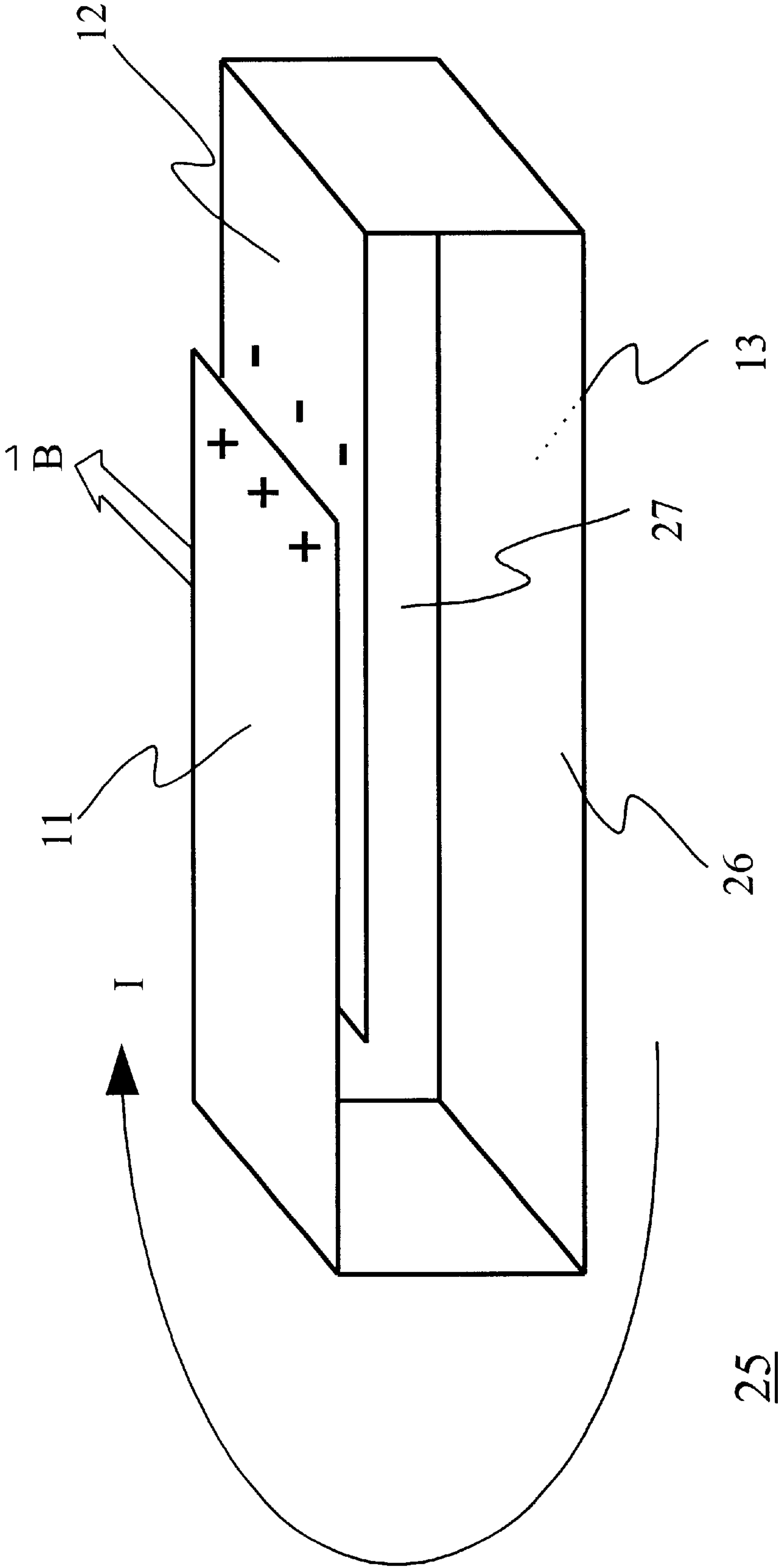


Fig 3

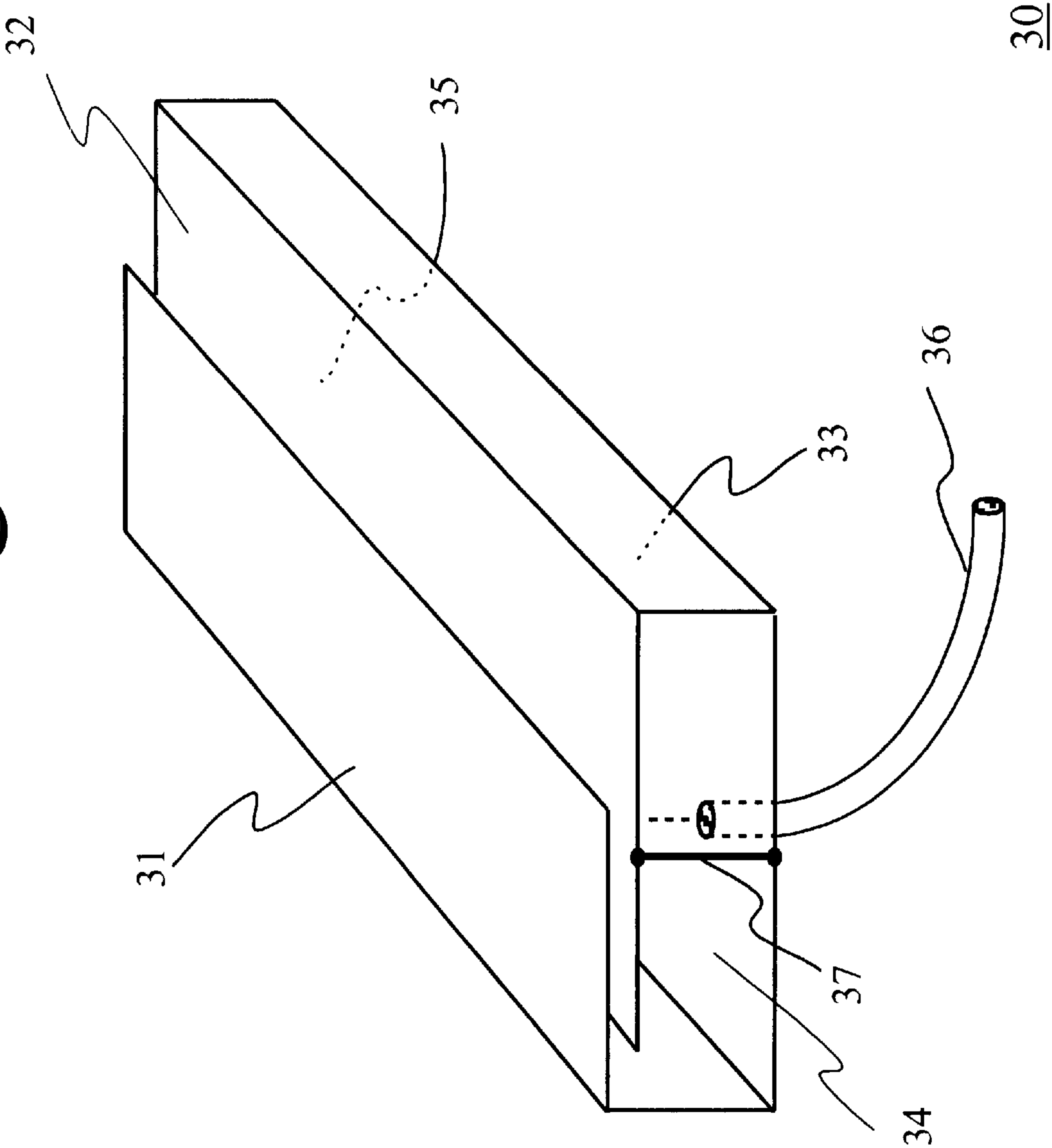


Fig 4

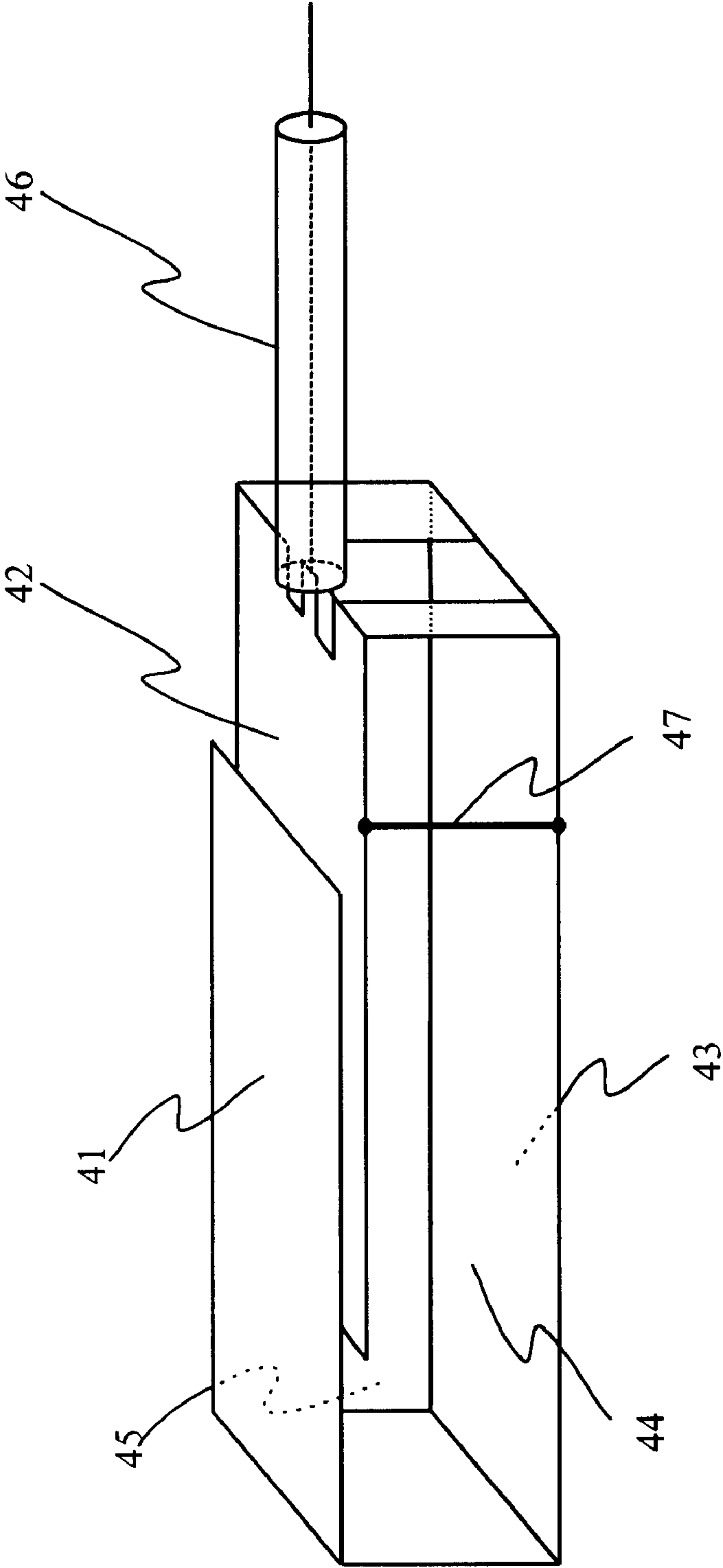


Fig 5

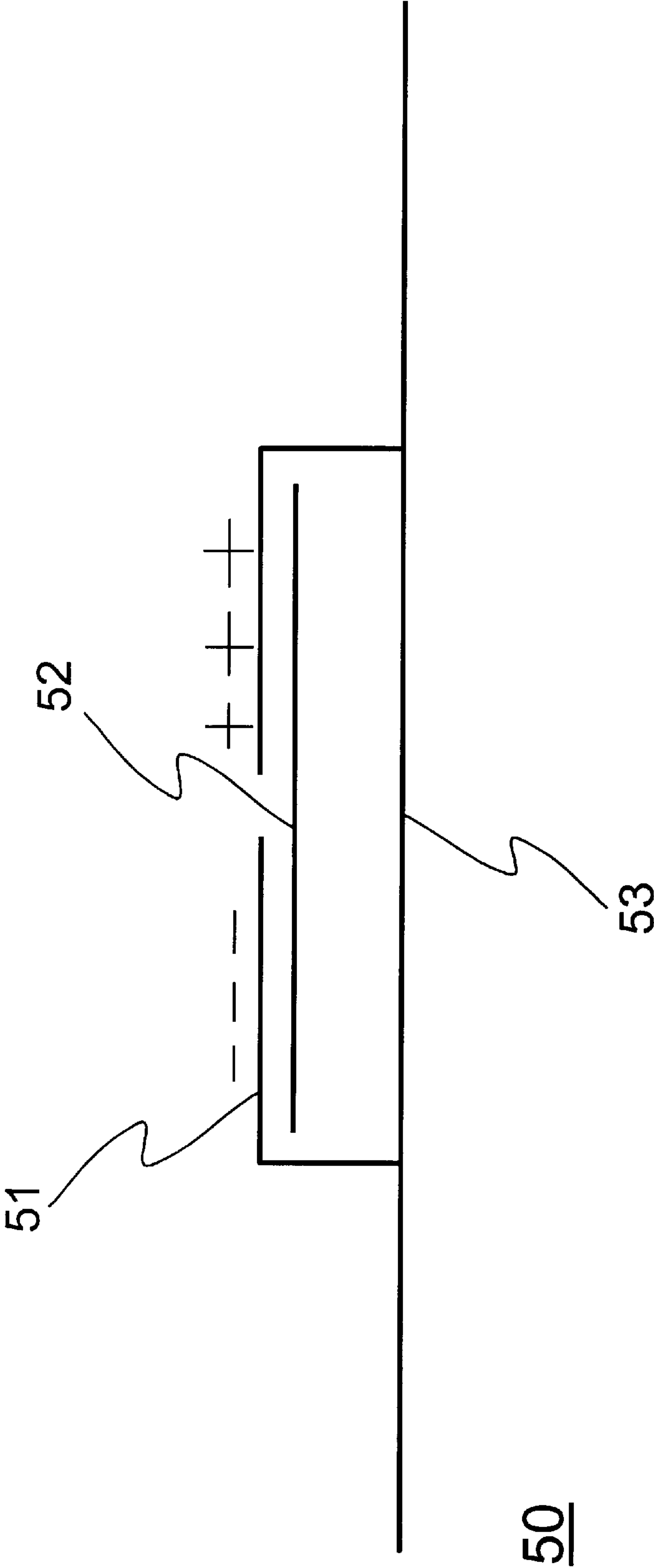


Fig 6

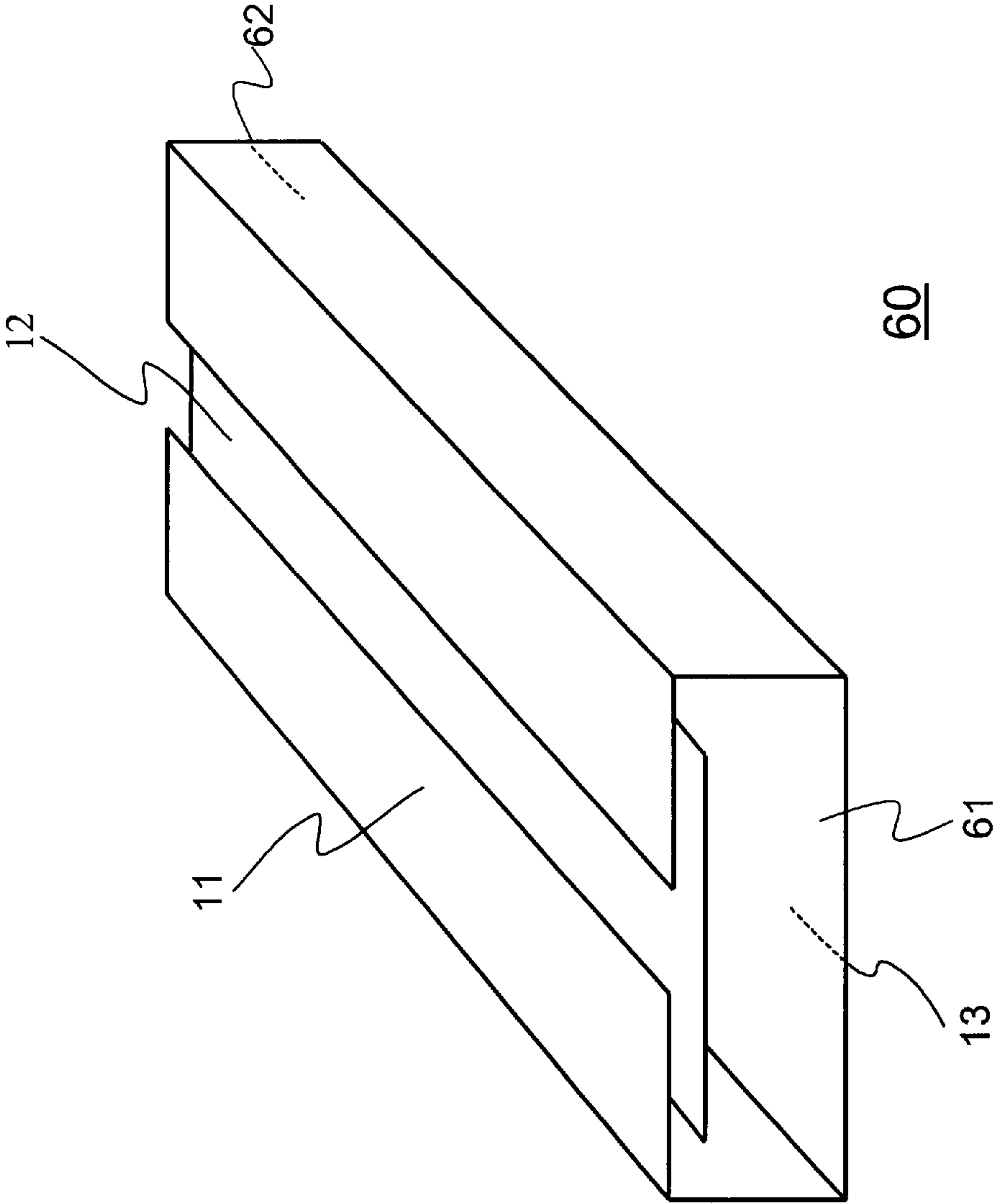


Fig 7A

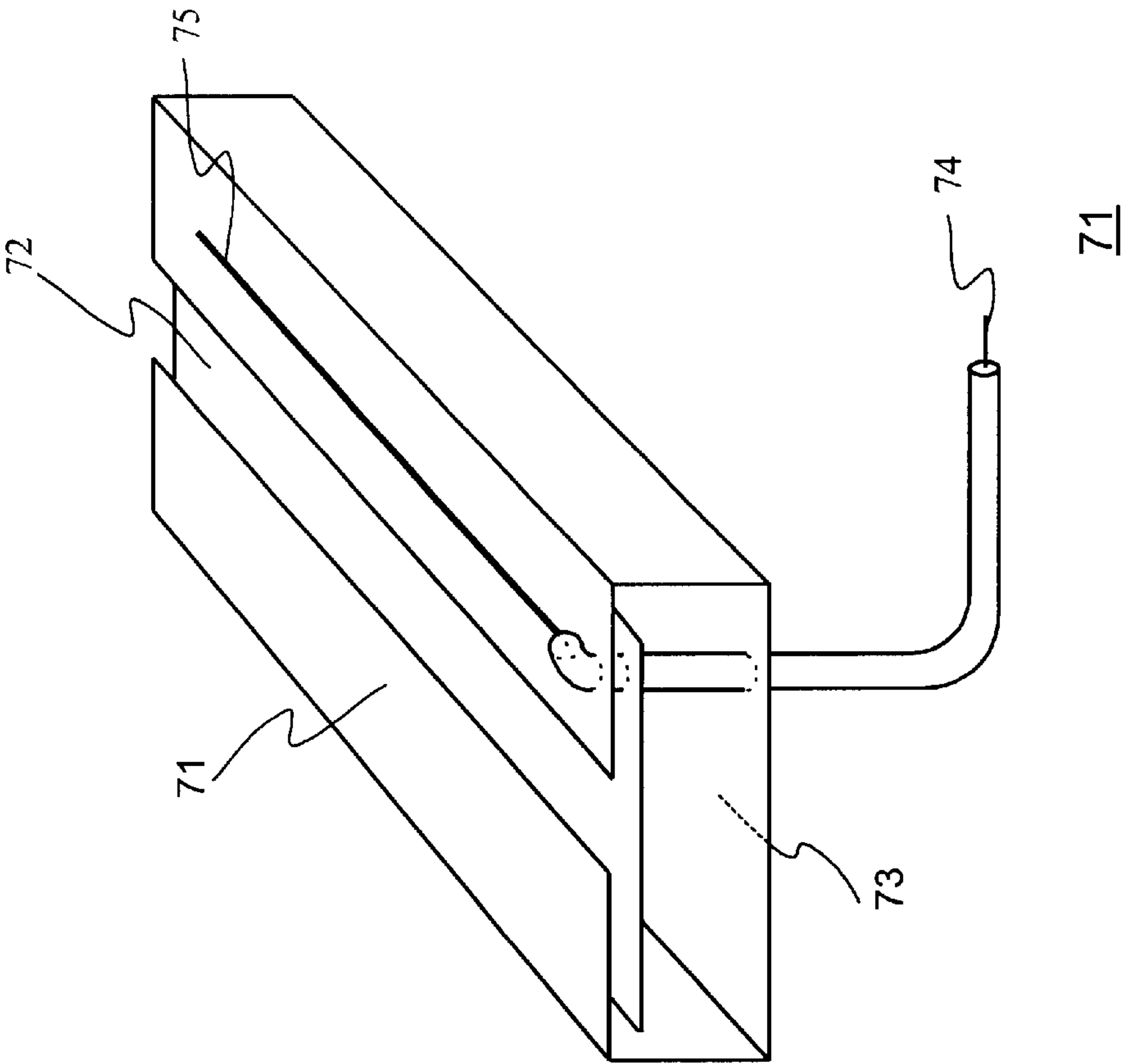


Fig 7B

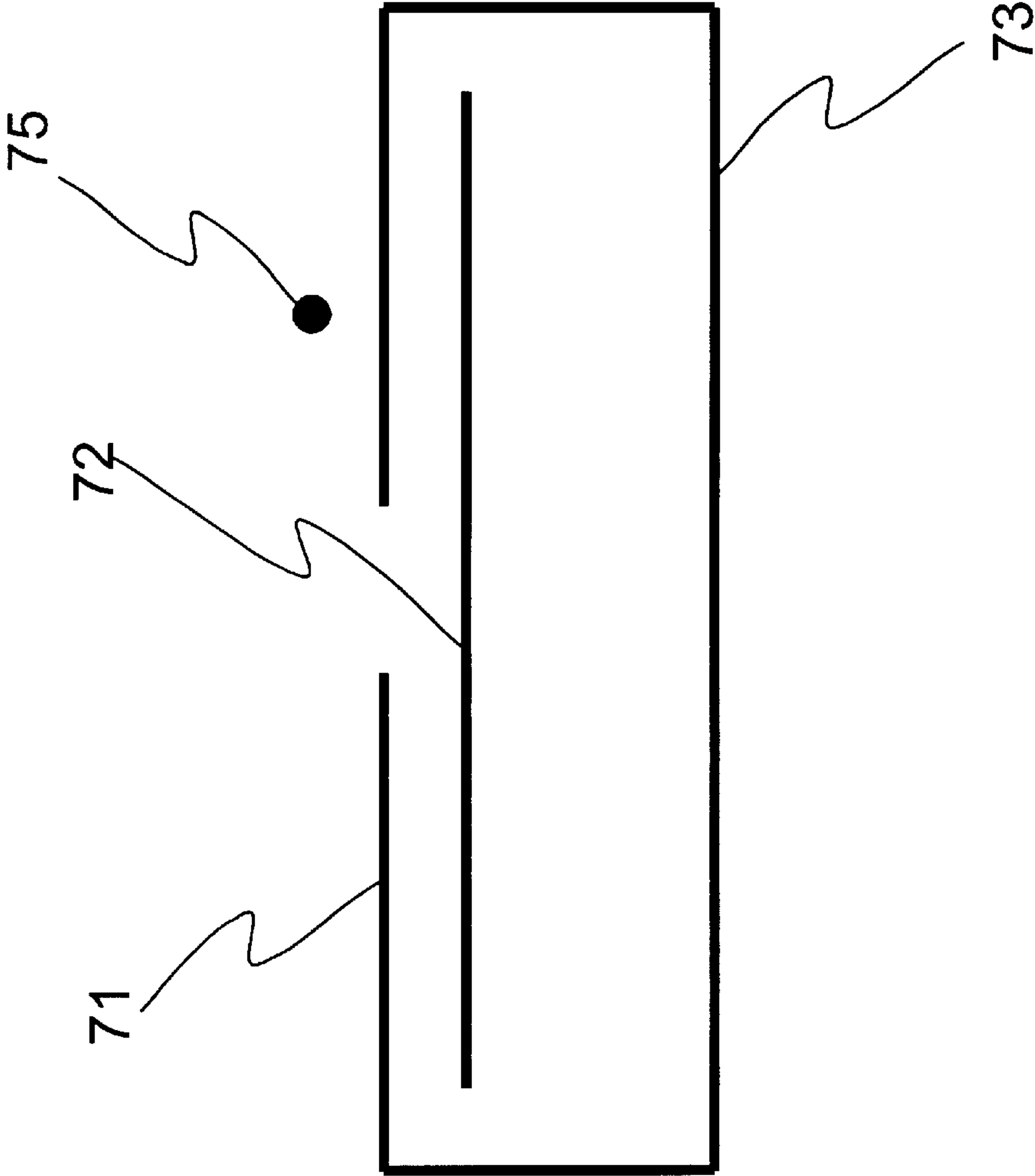


Fig 8

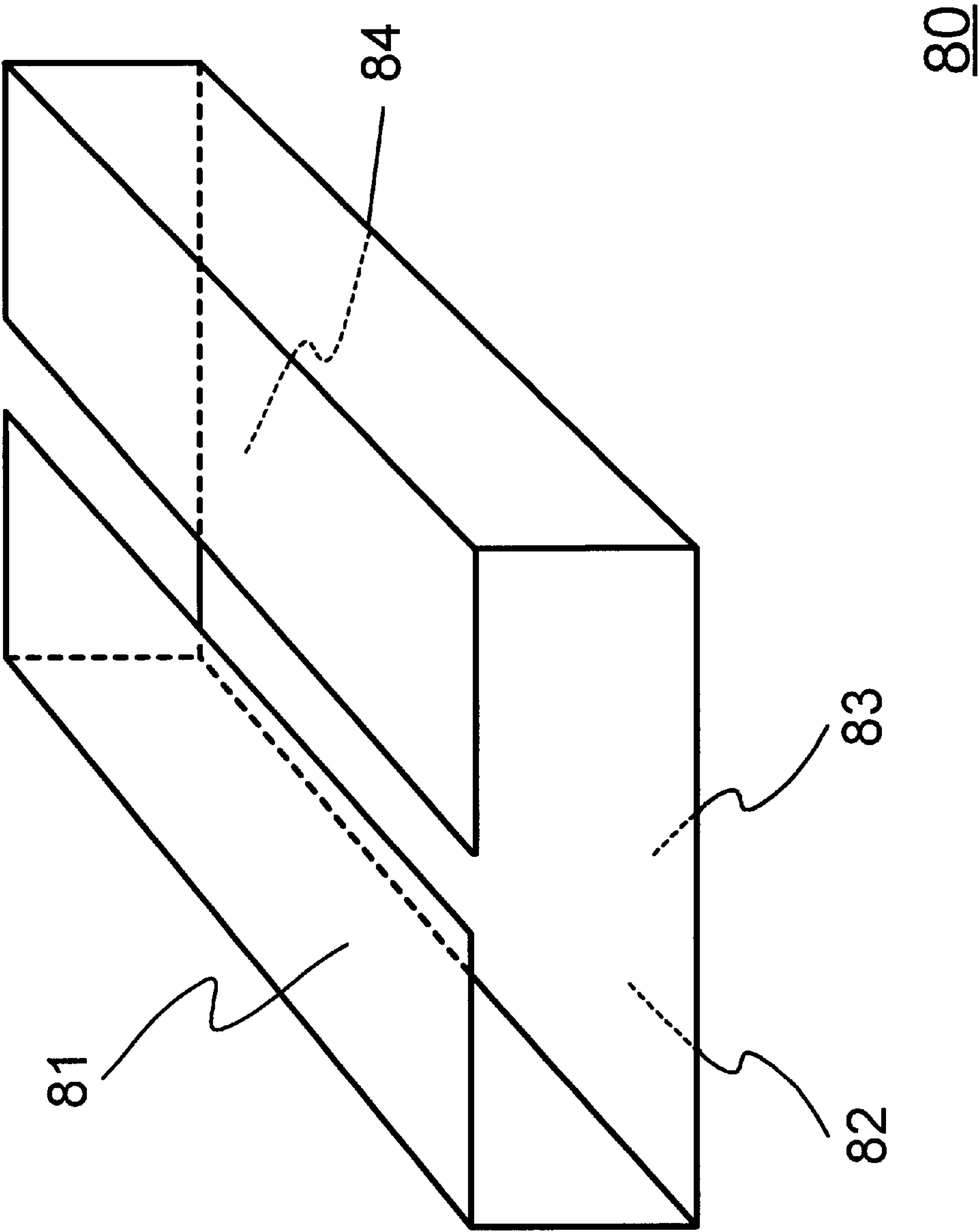


Fig 9A

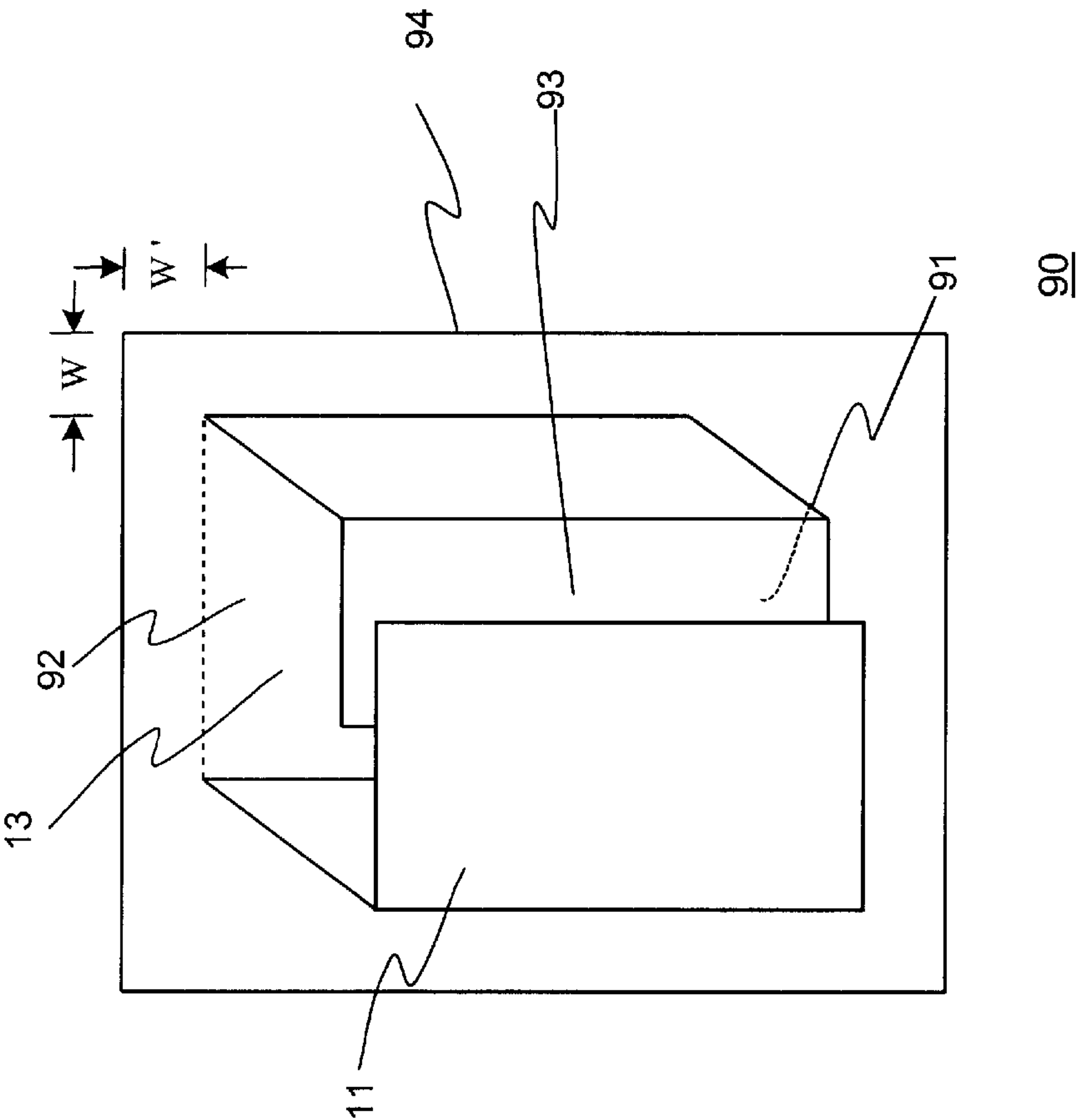


Fig 9B

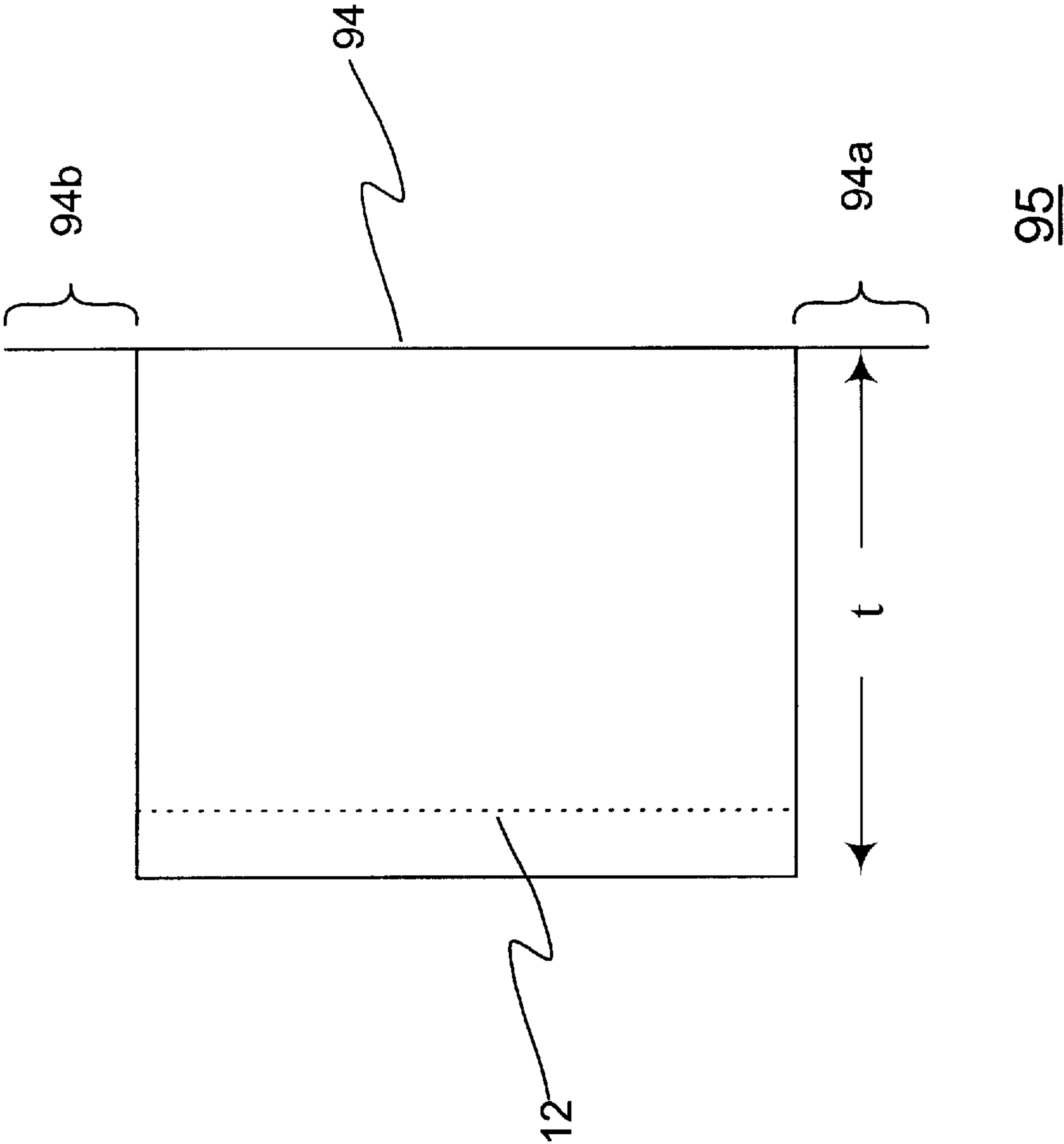


Fig 10A

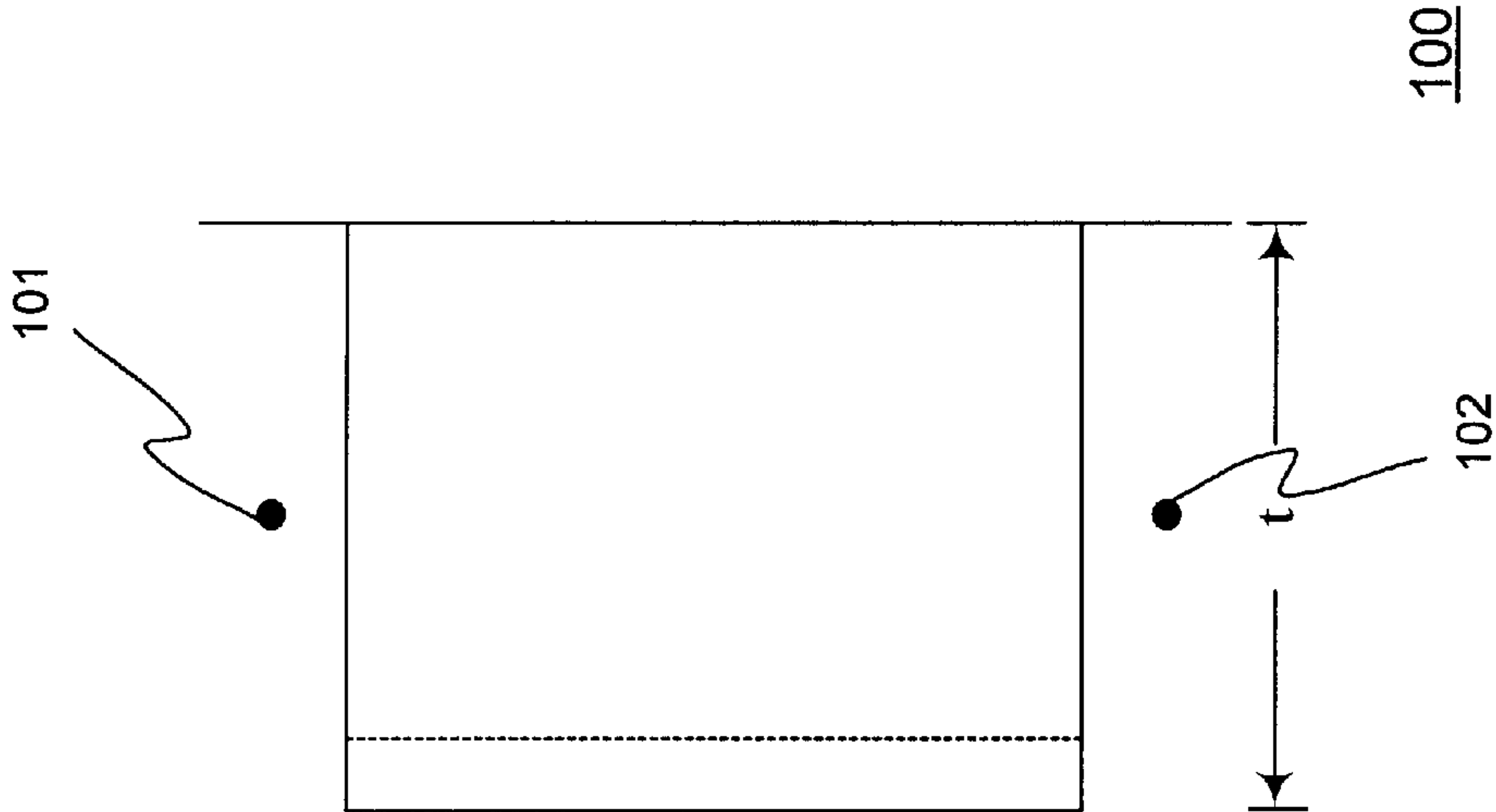


Fig 10B

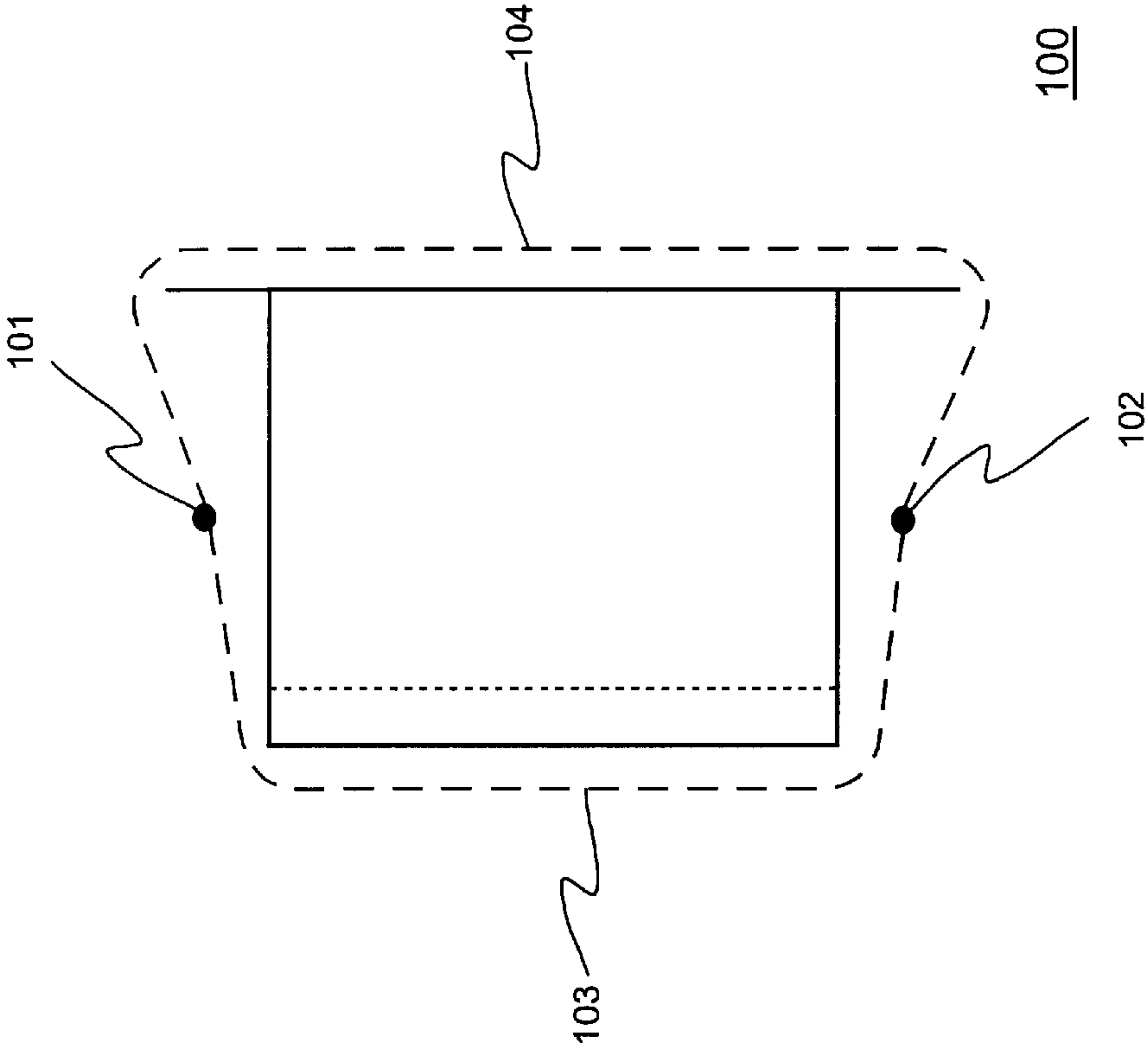


Fig 11

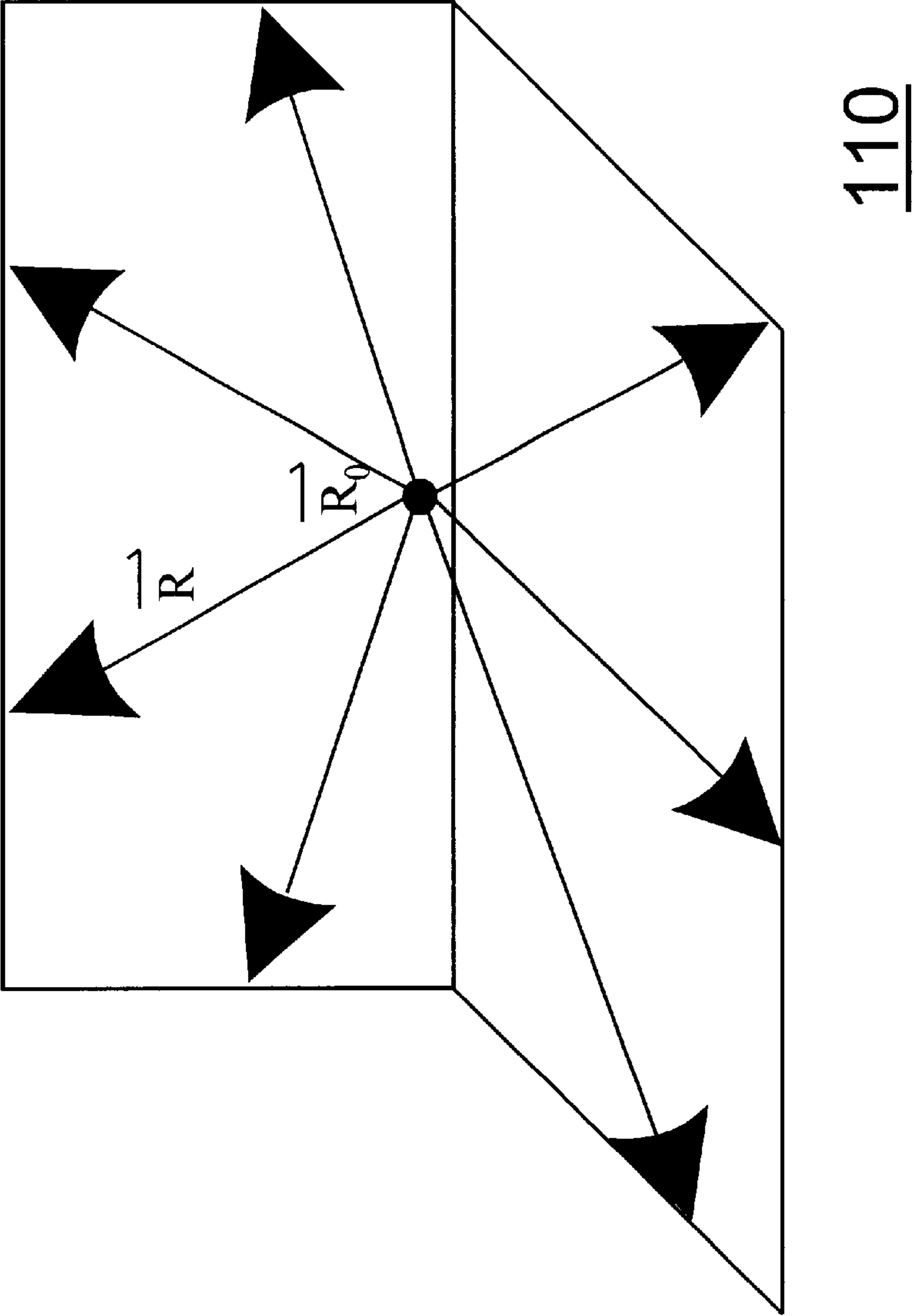


Fig 12A

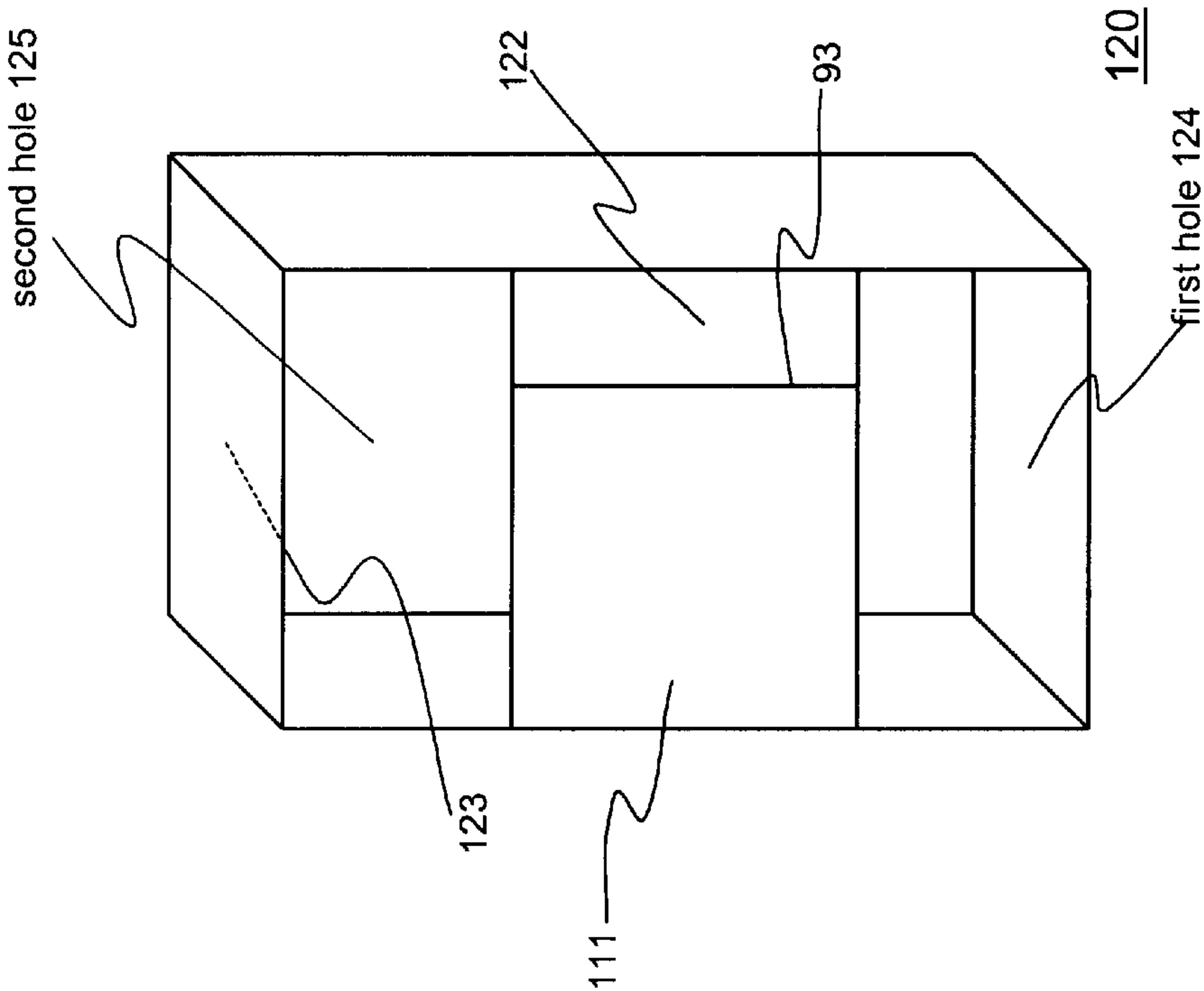


Fig 12B

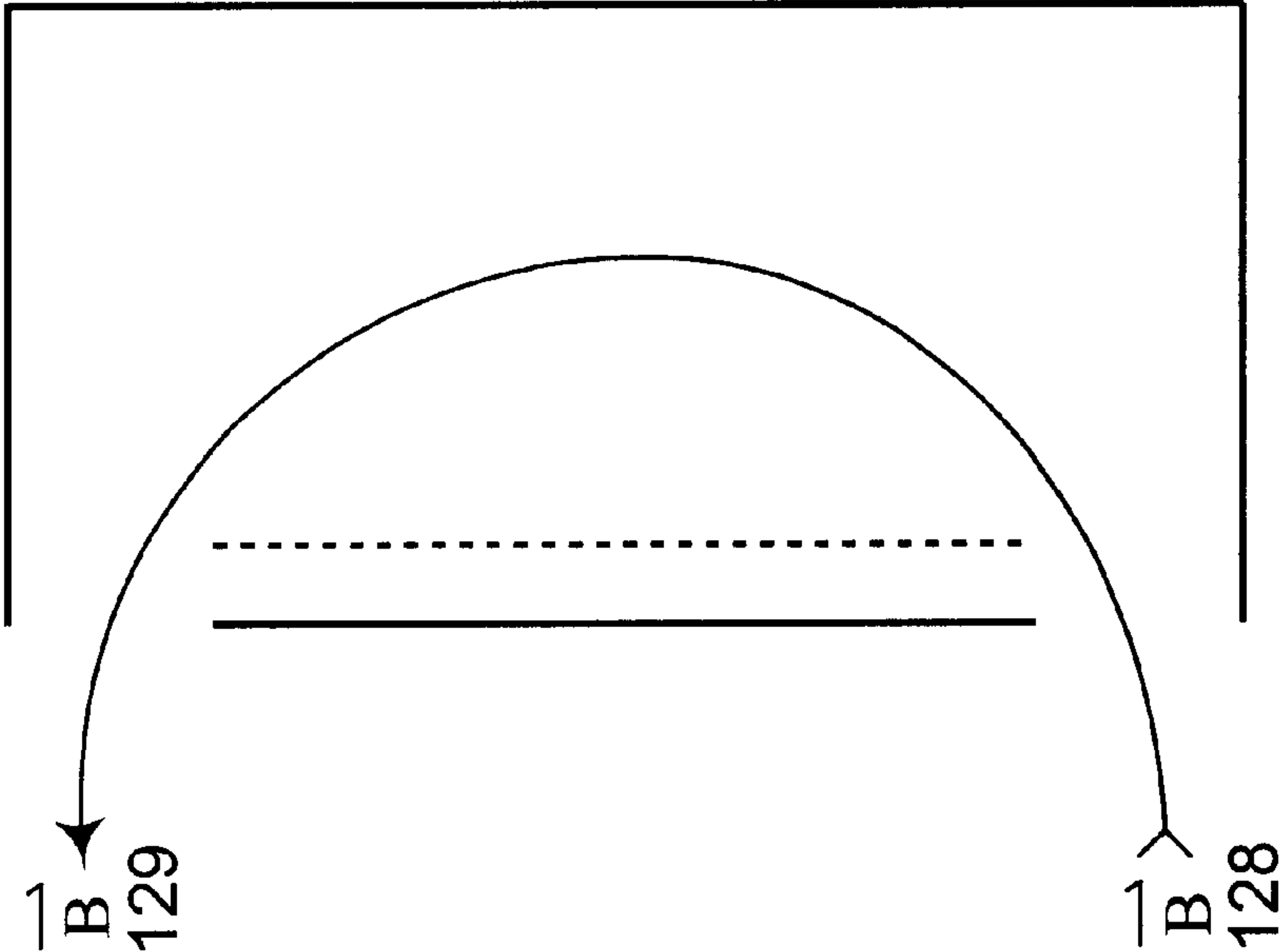
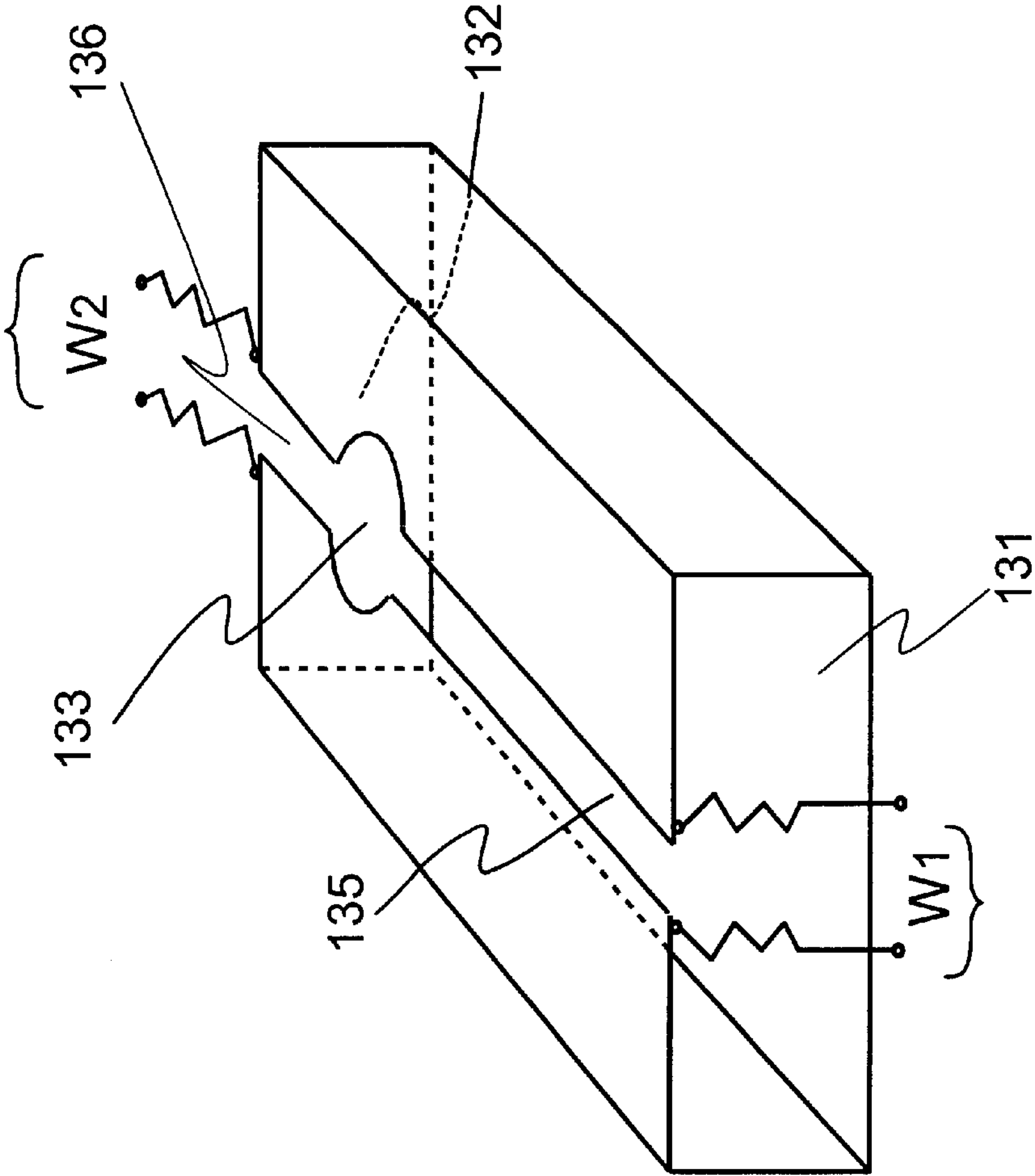
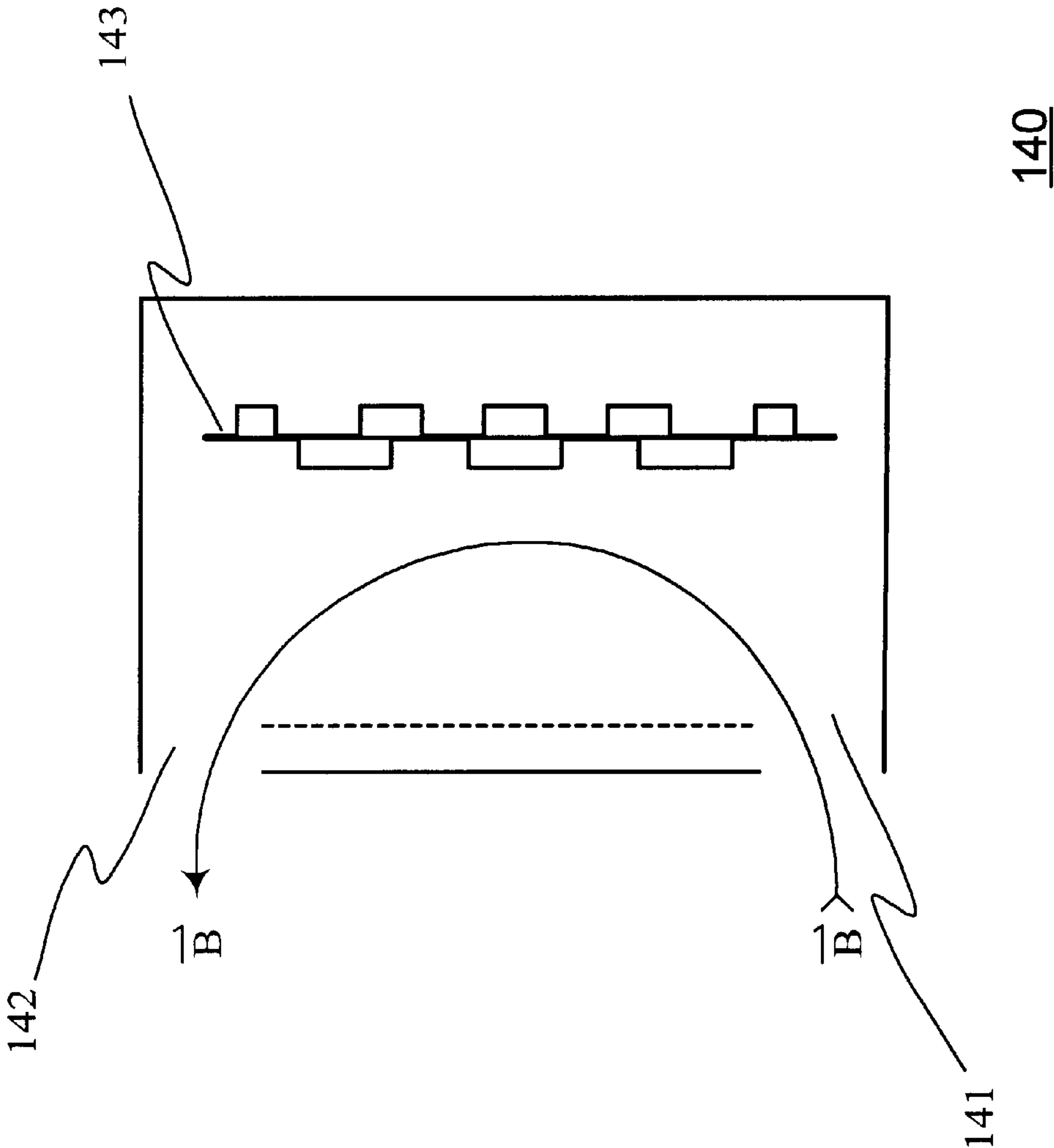


Fig 13



130

Fig 14



MAGNETIC DIPOLE ANTENNA STRUCTURE AND METHOD

CROSS REFERENCE TO RELATED APPLICATIONS

This application relates to concurrently filed, co-pending application U.S. patent application Ser. No. 09/781,779, entitled "Spiral Sheet Antenna Structure and Method" by Eli Yablonovitch et al., owned by the assignee of this application and incorporated herein by reference, filed on Feb. 12, 2001.

This application relates to concurrently filed, co-pending application U.S. patent application Ser. No. 09/781,780, entitled "Shielded Spiral Sheet Antenna Structure and Method" by Eli Yablonovitch et al., owned by the assignee of this application and incorporated herein by reference, filed on Feb. 12, 2001.

This application relates to concurrently filed, co-pending application U.S. patent application Ser. No. 09/781,723, entitled "Internal Circuit Board in an Antenna Structure and Method Thereof" by Eli Yablonovitch et al., owned by the assignee of this application and incorporated herein by reference, filed on Feb. 12, 2001.

BACKGROUND INFORMATION

1. Field of the Invention

The present invention relates generally to the field of wireless communication, and particularly to the design of an antenna.

2. Description of Related Art

Small antennas are required for portable wireless communications. To produce a resonant antenna structure at a certain radio frequency, it is usually necessary for the structure to be of a size equal to one-half of the electromagnetic wavelength, or for some designs, one-quarter of the electromagnetic wavelength. This is usually still too large.

A conventional solution, to reduce the size further, is to reduce the effective wavelength of the electromagnetic waves, by inserting a material of a high dielectric constant. Then, the internal wavelength is reduced by the square root of the dielectric constant. This requires special high dielectric constant materials that add cost, weight and cause an efficiency penalty. Accordingly, the present invention addresses these needs.

SUMMARY OF THE INVENTION

The present invention provides an effective increase in the dielectric constant purely by geometry, using a spiral sheet configuration. The dielectric material can have a dielectric constant >1 , or it can simply be air with dielectric constant 1. Therefore cheaper dielectric materials can be used. Indeed there is nothing cheaper than air.

An antenna, comprising a first plate and a second plate, the combination of the first and second plates serving as a capacitive structure; and a third metallic structure, coupled to the first and second plates, thereby producing a cylindrical or substantially cylindrical current distribution, with two openings or holes at either end of the cylinder-like shape. Although a cylindrical current distribution is described, other shapes of current distribution can be practiced provided that the current is distributed around two openings or holes, that would construct an antenna without departing from the spirit of the present invention. In effect, the overlap between the first and second plates, on the edge of the

cylinder, forms a seam between the two holes at the ends of the cylinder-like structure.

Advantageously, the present invention discloses an antenna structure that is more compact, reducing the overall size of a wireless device. The present invention further advantageously reduces the cost of building an antenna by using air as the dielectric.

Other structures and methods are disclosed in the detailed description below. This summary does not purport to define the invention. The invention is defined by the claims.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a pictorial diagram illustrating a cross-sectional view of a spiral sheet antenna for producing a spiral sheet current distribution in accordance with the present invention. The overlapping plates 11 and 12 form a seam between the two openings at the ends.

FIGS. 2A–2B are pictorial diagrams illustrating a perspective view of two similar antenna structures having different aspect ratio in length and width, respectively, of a spiral sheet antenna for producing a spiral sheet current distribution in accordance with the present invention.

FIG. 3 is a pictorial diagram illustrating a first possible drive configuration for a spiral sheet antenna in accordance with the present invention.

FIG. 4 is a pictorial diagram illustrating a second possible drive configuration for a spiral sheet antenna in accordance with the present invention.

FIG. 5 is a pictorial diagram illustrating a first embodiment of a cylinder-like antenna having two holes at the ends, with a seam between the two holes for producing a circular current distribution with a double parallel plate in accordance with the present invention.

FIG. 6 is a pictorial diagram illustrating a perspective view of a cylinder-like antenna having two holes at the ends, with a seam between the two holes for producing a circular current distribution with a double parallel plate in accordance with the present invention.

FIGS. 7A–7B are pictorial diagrams illustrating a perspective view and a cross-section view, respectively, of a third drive configuration of the cylinder-like antenna shown in FIG. 6 for exciting a circular current distribution with a double parallel plate seam in accordance with the present invention.

FIG. 8 is a pictorial diagram illustrating a third embodiment of a magnetic dipole sheet antenna having two holes at the ends, with a slot seam between the two holes, allowing a circular current distribution in accordance with the present invention.

FIGS. 9A–9B are pictorial diagrams illustrating a perspective view and a side cross-section view, respectively, of a first embodiment of a shielded spiral sheet antenna having two holes at the ends and an overlapping seam between the holes, providing shielding from absorbers adjacent to the antenna.

FIGS. 10A–10B are pictorial diagrams illustrating side views of an operational mathematical technique for determining shielding effectiveness in a shield spiral sheet antenna in accordance with the present invention.

FIG. 11 is a pictorial diagram illustrating an operational procedure for determining the center of a hole in a shielded spiral sheet antenna in accordance with the present invention.

FIGS. 12A–12B are pictorial diagrams illustrating a second embodiment of a shielded spiral sheet antenna with

overlapping capacitive seam structure in accordance with the present invention. FIG. 12B is a side cross-section view showing the path 128–129 followed by magnetic field lines B.

FIG. 13 is a pictorial diagram illustrating a multi-frequency, multi-tap antenna with spring contacts W1 and W2 in accordance with the present invention.

FIG. 14 is a pictorial diagram illustrating the placement of internal circuit boards inside an antenna in accordance with the present invention.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENT(S)

FIG. 1 is a pictorial diagram illustrating a cross-sectional view of a spiral sheet antenna 10, resembling a rectangular cylindrical shape, with two holes at the ends, and a capacitive seam connecting the two holes, for producing a cylindrical current distribution. The spiral sheet antenna 10 can be constructed with three plates, a first plate 11, a second plate 12, and a third plate 13. The variable d 14 represents the spacing between the first plate 11 and the second plate 12, and the variable t 15 represents the thickness of all three plates. A vertical connection 16 connects between the third plate 13 and the first plate 11, while the third plate 13 connects to the second plate 12 via a vertical connection 17. The length of the third plate 13, between vertical connections 16 and 17 is selected to be less than a quarter wavelength, $\lambda/4n$, where n is the square root of the dielectric constant.

The structure of the spiral sheet antenna 10 increases the effective dielectric constant by a factor of t/d . Effective increase in capacitance is due to overlapping plates between the plate 11 and the plate 12. In effect, the spiral antenna 10 produces a large dielectric constant, without the need for a high dielectric constant material, just from electrode geometry alone, i.e. $\epsilon_{relative}=t/d$. Effectively, treating the spiral sheet antenna as a patch type antenna, the required length of the patch then becomes

$$a = \frac{\lambda}{4} \sqrt{\frac{d}{t}} \times \frac{1}{\sqrt{\epsilon_r}},$$

where ϵ_r is the relative dielectric constant of the capacitor dielectric.

FIG. 2A is a pictorial diagram illustrating a perspective view of a spiral sheet antenna 20 for producing a cylinder-like current distribution. The spiral sheet antenna 20 has a first hole 21 and a second hole 22, at the ends, and a capacitive seam connecting the two holes. The alternating current (AC) magnetic field vector B^ω , is shown entering hole 21 and exiting hole 22.

FIG. 2B is a pictorial diagram illustrating a spiral sheet antenna 25 for producing a cylinder-like current distribution with a different aspect ratio, with a first hole 26 and a second hole 27. The structure shape in FIG. 2B is the same as the structure shape in FIG. 2A. However, the aspect ratio, in FIG. 2B, is different from the aspect ratio in FIG. 2A. The curved vector I represents the general direction of the AC currents.

The spiral antennas 20 and 25 in FIGS. 2A and 2B operate like a single-turn solenoids. A single-turn solenoid consists of a cylinder-like current distribution. A significant portion of the electromagnetic radiation produced by the spiral antennas 20 and 25 arises from the alternating current (AC) magnetic field vector B^ω that enters and exits from the holes at the end of the single turn solenoid.

Advantageously, the antennas 20 and 25 do not require a high dielectric constant ceramic to attain a small dimensional size. The inherent capacitance in the structure of the antennas 20 and 25 allows a low frequency operation according to the formula: $\omega=1/LC$, where ω is the frequency in radians/second, L is the inductance of the single turn solenoid formed by 11, 16, 13, 17 and 12 in FIG. 1., and C is the capacitance from the thin overlapping region labeled as the thickness d 15, or the spacing 14.

FIG. 3 is a pictorial diagram illustrating a first drive or feed configuration 30 for a spiral sheet antenna producing a cylindrical current distribution. The first drive configuration 30 has a first plate 31, a second plate 32, a third plate 33, a first hole 34, and a second hole 35. A drive cable 36 attaches and drives the spiral sheet antenna 20. In this embodiment, the co-axial drive cable 36 matches any desired input impedance. An optional vertical short circuit wire, 37, can assist in providing an impedance matching shunt to the spiral sheet antenna 20.

FIG. 4 is a pictorial diagram illustrating a second drive configuration 40 of a spiral sheet antenna for producing a rectangular cylinder-like current distribution. The second drive configuration 40 has a first plate 41, a second plate 42, a third plate 43, a first hole 44, and a second hole 45 at the rear opening of the rectangular cylinder. A feed or drive cable 46 attaches and drives the spiral sheet antenna 20, with an optional impedance matching vertical shunt wire 47 connecting between the second plate 42 and the third plate 43. Preferably, the material used to construct an antenna might have a high electrical conductivity, e.g. copper depending on the required antenna Q-factor.

FIGS. 3 and 4 illustrate two sample drive configurations applied to the spiral sheet antenna 20, and are not meant to be an exhaustive listing since many possibilities abound. One of ordinary skill in the art should recognize that there are numerous other similar, equivalent, or different drive configurations that can be practiced without departing from the spirit of the present invention. A spiral sheet antenna 20 produces an AC magnetic field that radiates efficiently in a structure that is smaller than

$$\frac{\lambda}{4\sqrt{\epsilon_r}},$$

that is a typical restriction for a patch antenna, where λ is the electromagnetic wavelength in vacuum, and $\sqrt{\epsilon_r}$ is the microwave refractive index.

The antenna being described here can be regarded as a rectangular metallic enclosure with two openings, (at the ends of the rectangle), and a seam connecting the two holes. The seam functions as a capacitor and can be implemented in several different ways. First, the seam can be constructed as an overlapping region as shown in 20. Second, a seam can be constructed as slot between two metal sheets as shown in 80 where two edges meet. Third, a seam can be constructed with a slot under which there is an additional metal sheet underneath as shown in 60.

FIG. 5 is a pictorial diagram 50 illustrating a first embodiment of a rectangular cylindrical sheet antenna with an opening at each end of the rectangular cylinder, and with a seam connecting the two holes at the ends. The seam comprises of a slot over a double parallel plate. The rectangular cylindrical current distribution structure 50 has a second plate 52 overlapping with a first plate 51 in two areas on either side of the slot or seam to provide capacitance. The third plate 53 is far from the first and second plates 51 and 52, and therefore contributes little to the capacitance. The

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rectangular cylindrical current distribution structure **50** thus yields the benefit of a large dielectric constant, without the need for a special dielectric material. However, the capacitance is diminished by a factor **4** due to the two capacitors in series from the overlap of the first and second plates **51** and **52**, compared to the same two plates in parallel.

FIG. **6** is a pictorial diagram **60**, a perspective view illustrating the second embodiment of a seam configuration in a rectangular cylindrical sheet antenna. A first hole **61** is positioned in the front of the pictorial diagram **60**, while a second hole **62** is positioned at the back of the pictorial diagram **60**. The rectangular cylindrical sheet antenna may be driven in a number of different ways. A possible approach is to place a wire parallel to the long axis, but off-center to drive currents across the slot. FIG. **7A** is a pictorial diagram **70** illustrating this, the second type of drive configuration (of the third seam example, illustrated in FIG. **6**) for the rectangular cylindrical sheet antenna. A coaxial feed cable **74** extends and connects through a third plate **73**, a second plate **72**, and a first plate **71**, to an off-center drive wire **75**. FIG. **7B** is a pictorial diagram **76** illustrating a side view of this second type of drive configuration. A drive wire **77** is shown in cross-section in FIG. **7B**.

FIG. **8** is a pictorial diagram **80** illustrating a third embodiment of a rectangular cylindrical sheet antenna with a slot seam for producing a magnetic dipole current distribution. The pictorial diagram **80** will not operate at as low a frequency as the spiral sheet structure, all other things being equal, since the capacitance of a slot seam is less than the capacitance of the over-lapping sheets in the spiral sheet structure.

FIG. **9A** is a pictorial diagram illustrating a perspective view, and FIG. **9B** illustrating a side view, of a first embodiment of a shielded spiral sheet antenna **90** for producing a cylinder-like current distribution. The structure in the shielded spiral sheet antenna **90** is similar to the structure in the spiral sheet antenna **20**. A first hole **91** is at one end of the rectangle, and a second hole **92** is at the other end of the rectangle. An over-lapping seam **93**, connects the two holes together. In the case of a cellphone the pair of holes **91** and **92** is positioned to face away from a user's ear. A base plate **94**, of the shielded spiral sheet antenna **90**, is positioned facing the human body, extending **94a** beyond the third plate **13** at one end and extending **94b** beyond the third plate **13** at the other end. The shielded spiral sheet antenna **90** therefore faces away from the human body. The width of the border w and w' determines the degree of front-to-back shielding ratio. If $w \approx t$ and $w' \approx t$, then a shielding ratio of 3 dB or better can be achieved.

FIGS. **10A** and **10B** are pictorial diagrams illustrating side views of a operational mathematical technique for defining a shielded spiral sheet antenna. To define the shielded spiral sheet antenna **100**, two center points are chosen, a geometrical center point of a top opening **101** and a geometrical center point of a bottom opening **102**. A path **103**, L_s , represents the shortest path between the geometrical center point of a top opening **101** and the geometrical center point of a bottom opening **102** on the short side. A path **104**, L_e , represents the longest path between the geometrical center point of a top opening **101** and the geometrical center point of a bottom opening **102** on the longer side. The path **103** is shorter than the path **104** that faces a user.

The mathematical relationship between the different variables should be governed by the following inequality, $L_s - L_e > \alpha t$, Eq. (1), in order to provide a good shielding, front-to-back. A value of $\alpha \approx 1$ provides some good degree of shielding.

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FIG. **11** is a pictorial diagram **110** illustrating an operational procedure for determining the center of a hole for the purposes of our operational mathematical technique for defining a shielded spiral antenna. The geometrical center of the top and bottom openings can be defined as a type of geometrical "center-of-gravity":

$$\sum_{\text{edges of opening}} (\vec{R} - \vec{R}_0) = 0 \quad \text{Eq. (2)}$$

where R^ω is the set of position vectors at the edges of the opening, and R_0^ω is the center-of-gravity center point that satisfies the Eq. (2).

This equation defines the center point for use in the mathematical specification in Eq (1). The point around which all the vectors sum to zero, defines the center of the hole, or opening. The type of metallic shielding specified FIGS. **9A**, **9B**, **10A**, and **10B**, are useful for shielding cell phone antennas from the user.

FIG. **12A** is a pictorial diagram **120** illustrating a perspective view of a second embodiment of a shielded spiral sheet antenna (with overlapping capacitive structure). A first hole **124** and a second hole **125** are positioned to face away from the user. In effect, both the first and second holes **124** and **125** are facing the front. A seam **126** connects between the first hole **124** and the second hole **125**.

FIG. **12B** is a pictorial diagram **127** illustrating a side cross-sectional view of FIG. **12A**, with AC magnetic field illustrated. The structure diagram has two holes for the magnetic field entering **128** and exiting **129** the antenna. The rectangular openings shown, may be smaller than the width of the rectangle. A rectangular container is intended as an illustration. The rectangular container may be in a shape resembling a cell phone body instead.

FIG. **13** is a pictorial diagram illustrating a dual frequency, dual-tap antenna **130** with a first hole **131**, a second hole **132**, and a third hole **133**. A first seam **135** connects between the first hole **131** and the third hole **133**. A second seam **136** connects between the hole **132** and the hole **133**. Spring contacts w_1 and w_2 can connect to different circuits on a circuit board, such as for operating with main cell phone bands including Personal Communication System (PCS) at 1900 MHz, Global Positioning Systems (GPS) at 1575 MHz, bluetooth, Advanced mobile phone system (amps) at 850 MHz, and 900 MHz cell phone bands. The spring contacts are only an example. The concept is to use multiple taps for the different frequencies that might be needed in a wireless system. The multi-taps would be derived from a single antenna structure.

In general, the antenna structure consists of a metallic enclosure, with holes, or openings. For each independent antenna, or for each frequency band, an additional hole or opening must be provided on the metallic enclosure. For the example in FIG. **13**, two frequencies, require 3 holes. Likewise n -frequencies would require $(n+1)$ holes or openings, connected by n seams. Some of the n -frequencies might be identical, for the purpose of space or polarization diversity.

FIG. **14** is a pictorial diagram **140** illustrating the placement of one or more internal circuit boards **143** inside an antenna. Radio Frequency Magnetic fields enter a first hole **141** and exit through a second hole **142**. The internal volume in an antenna can be wisely utilized as not to waste any unused empty space. The extra space can be filled with one or more active circuit boards **143** for operation of a cell phone. The internal circuit boards do not interfere much with

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the internal AC RF magnetic fields inside the antenna structure. This allows the antenna volume to be put to good use in a small volume cell phone.

The above embodiments are only illustrative of the principles of this invention and are not intended to limit the invention to the particular embodiments described. For example, the basic concept in this invention teaches a metallic structure with at least two holes, and a seam. One of ordinary skill in the art should recognize that any type of antenna structure, which possesses these types of characteristics, is within the spirit of the present invention. Furthermore, although the term "holes" are used, it is apparent to one of ordinary skill in the art that other similar or equivalent concepts may be used, such as opening, gaps, spacing, etc. Accordingly, various modifications, adaptations, and combinations of various features of the described embodiments can be practiced without departing from the scope of the invention as set forth in the appended claims.

We claim:

1. An antenna, comprising:

a metallic structure having a first hole at the front opening and a second hole at the rear opening; and

at least one seam connecting between the first hole at the front opening and the second hole at the rear opening, wherein the at least one seam comprises a capacitive structure of a spiral sheet type, the at least one seam being constructed between a top plate and a middle plate, the top plate overlapping with the middle plate, the top plate having a left edge connected to the metallic structure, the middle plate having a right edge connected to the metallic structure.

2. The antenna of claim 1, wherein the at least one seam comprises a capacitive structure.

3. The antenna of claim 1, further comprising a pair of wires coupled to the antenna, the pair of wires providing energy to the antenna.

4. The antenna of claim 1, further comprising a wire and a ground, the wire and the ground coupled to the antenna for providing energy to the antenna.

5. The antenna of claim 1, wherein an electrical length of the antenna is less than one-quarter wavelength.

6. The antenna of claim 1, wherein the first and second holes are on the same side of the metallic structure.

7. The antenna of claim 1, wherein the position of the first and second holes are facing in the same direction.

8. An antenna, comprising:

a metallic structure having a first hole at the front opening and a second hole at the rear opening; and

at least one seam connecting between the first hole at the front opening and the second hole at the rear opening, wherein the at least one seam comprises a capacitive structure of a slot type, the at least one seam being constructed in a gap between a top left plate and a top right plate, the top left plate having a left edge connected to the metallic structure, the top right plate having a right edge connected to the metallic structure.

9. The antenna of claim 8, wherein the at least one seam comprises a capacitive structure.

10. The antenna of claim 8, further comprising a pair of wires coupled to the antenna, the pair of wires providing energy to the antenna.

11. The antenna of claim 8, further comprising a wire and a ground, the wire and the ground coupled to the antenna for providing energy to the antenna.

12. The antenna of claim 8, wherein an electrical length of the antenna is less than one-quarter wavelength.

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13. The antenna of claim 8, wherein the first and second holes are on the same side of the metallic structure.

14. The antenna of claim 8, wherein the position of the first and second holes are facing in the same direction.

15. An antenna, comprising:

a metallic structure having a first hole at the front opening and a second hole at the rear opening; and

at least one seam connecting between the first hole at the front opening and the second hole at the rear opening, wherein the at least one seam comprises a capacitive structure of a double parallel plate type, a top left plate having a left edge and a right edge, a top right plate having a left edge and a right edge, the at least one seam being constructed between a gap on the right edge of the top left plate and on the left edge of a top right plate, the top left plate overlapping with a middle plate, the top right plate overlapping with the middle plate, the top having plate having the left edge connected to the metallic structure, the top right plate having the right edge connected to the metallic structure.

16. The antenna of claim 15, wherein the at least one seam comprises a capacitive structure.

17. The antenna of claim 15, further comprising a pair of wires coupled to the antenna, the pair of wires providing energy to the antenna.

18. The antenna of claim 15, further comprising a wire and a ground, the wire and the ground coupled to the antenna for providing energy to the antenna.

19. The antenna of claim 15, wherein an electrical length of the antenna is less than one-quarter wavelength.

20. The antenna of claim 15, wherein the first and second holes are on the same side of the metallic structure.

21. The antenna of claim 15, wherein the position of the first and second holes are facing in the same direction.

22. An antenna comprising:

a metallic enclosure with a plurality of openings or holes, each opening or hole corresponding to a different frequency band; and

one or more capacitive seams connecting the openings together, the capacitive seams including slots in the metal or allow for overlap of metal at the capacitive seam, to provide more capacitance, wherein the at least one or more seams comprises a capacitive structure of a spiral sheet type, the at least one seam being constructed between a top plate and a middle plate, the top plate overlapping with the middle plate, the top plate having a left edge connected to the metallic structure, the middle plate having a right edge connected to the metallic structure.

23. The antenna of claim 22, wherein the one or more capacitive seams comprises a spiral sheet type, a slot type, or a double plate parallel type.

24. An antenna comprising:

a metallic enclosure with a plurality of openings or holes, each opening or hole corresponding to a different frequency band; and

one or more capacitive seams connecting the openings together, the capacitive seams including slots in the metal or allow for overlap of metal at the capacitive seam, to provide more capacitance, wherein the one or more seams comprises a capacitive structure of a slot type, the at least one seam being constructed in a gap between a top left plate and a top right plate, the top left plate having a left edge connected to the metallic structure, the top right plate having a right edge connected to the metallic structure.

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25. The antenna of claim 24, wherein the one or more capacitive seams comprises a spiral sheet type, a slot type, or a double plate parallel type.

26. An antenna comprising:

a metallic enclosure with a plurality of openings or holes, 5
each opening of hole corresponding to a different frequency band; and

one or more capacitive seams connecting the openings together, the capacitive seams including slots in the metal or allow for overlap of metal at the capacitive seam, to provide more capacitance, wherein the at least one seam comprises a capacitive structure of a double parallel plate type, a top left plate having a left edge and a right edge, a top right plate having a left edge and a

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right edge, the at least one seam being constructed between a gap on the right edge of the top left plate and on the left edge of a top right plte, the top left plate overlapping with a middle plate, the top right plate overlapping with the middle plate, the top having plate having the left edge connected to the metallic structure, the top right plate having the right edge connected to the metallic structure.

10 27. The antenna of claim 26, wherein the one or more capacitive seams comprises a spiral sheet type, a slot type, or a double plate parallel type.

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