



US006420935B1

(12) **United States Patent**  
**Harris et al.**

(10) **Patent No.:** **US 6,420,935 B1**  
(45) **Date of Patent:** **Jul. 16, 2002**

(54) **CONTROLLER-BASED RADIO FREQUENCY AMPLIFIER MODULE AND METHOD**

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(\*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **09/587,344**

(22) Filed: **Jun. 5, 2000**

#### Related U.S. Application Data

(63) Continuation of application No. 08/887,940, filed on Jul. 3, 1997, now Pat. No. 6,078,222.

(60) Provisional application No. 60/021,271, filed on Jul. 5, 1996.

(51) Int. Cl.<sup>7</sup> ..... **H03K 3/68; H03F 1/52**

(52) U.S. Cl. .... **330/295; 330/298**

(58) Field of Search ..... **330/277, 285, 330/286, 295, 298, 310**

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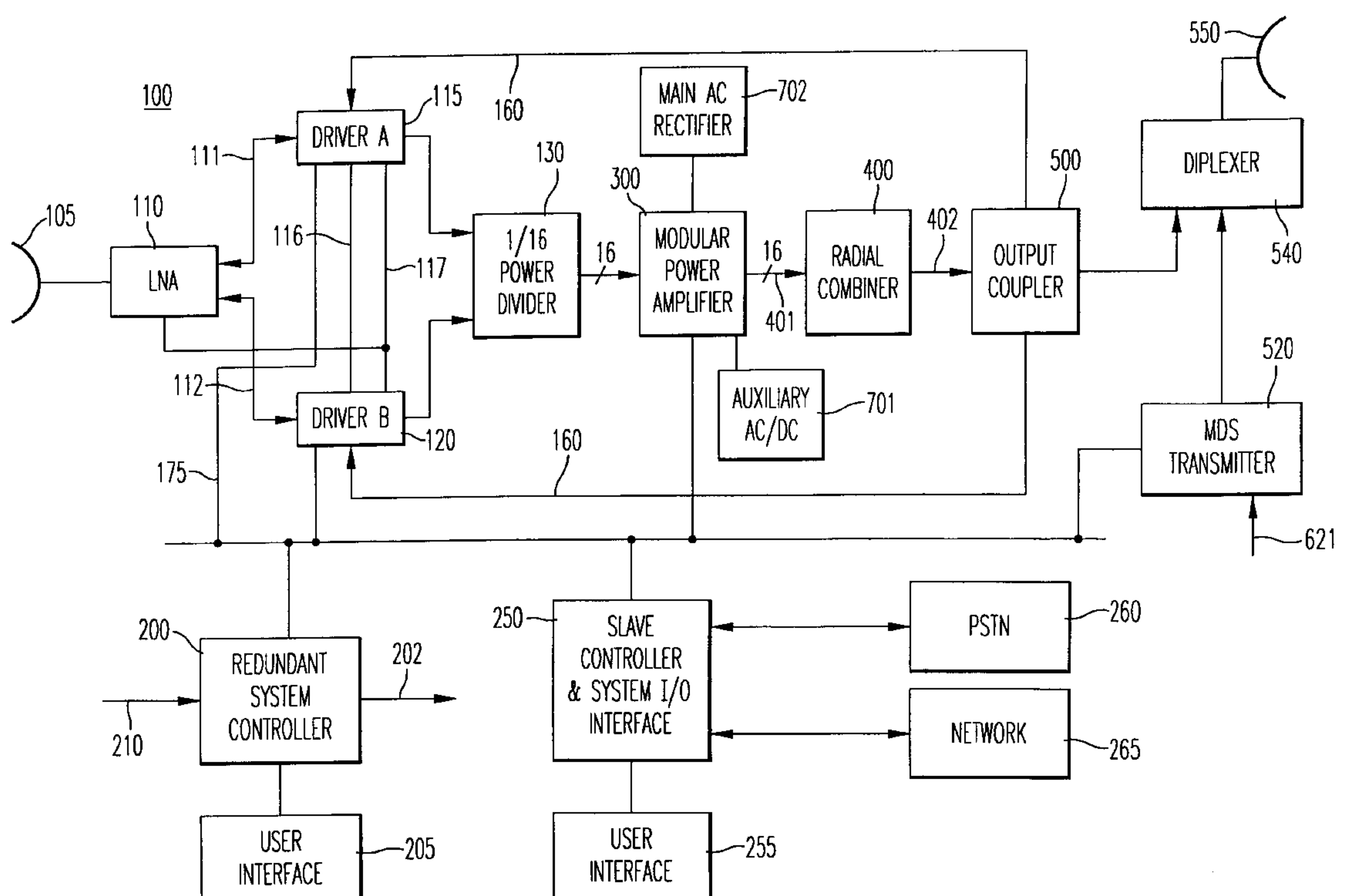
Primary Examiner—Steven J. Mottola

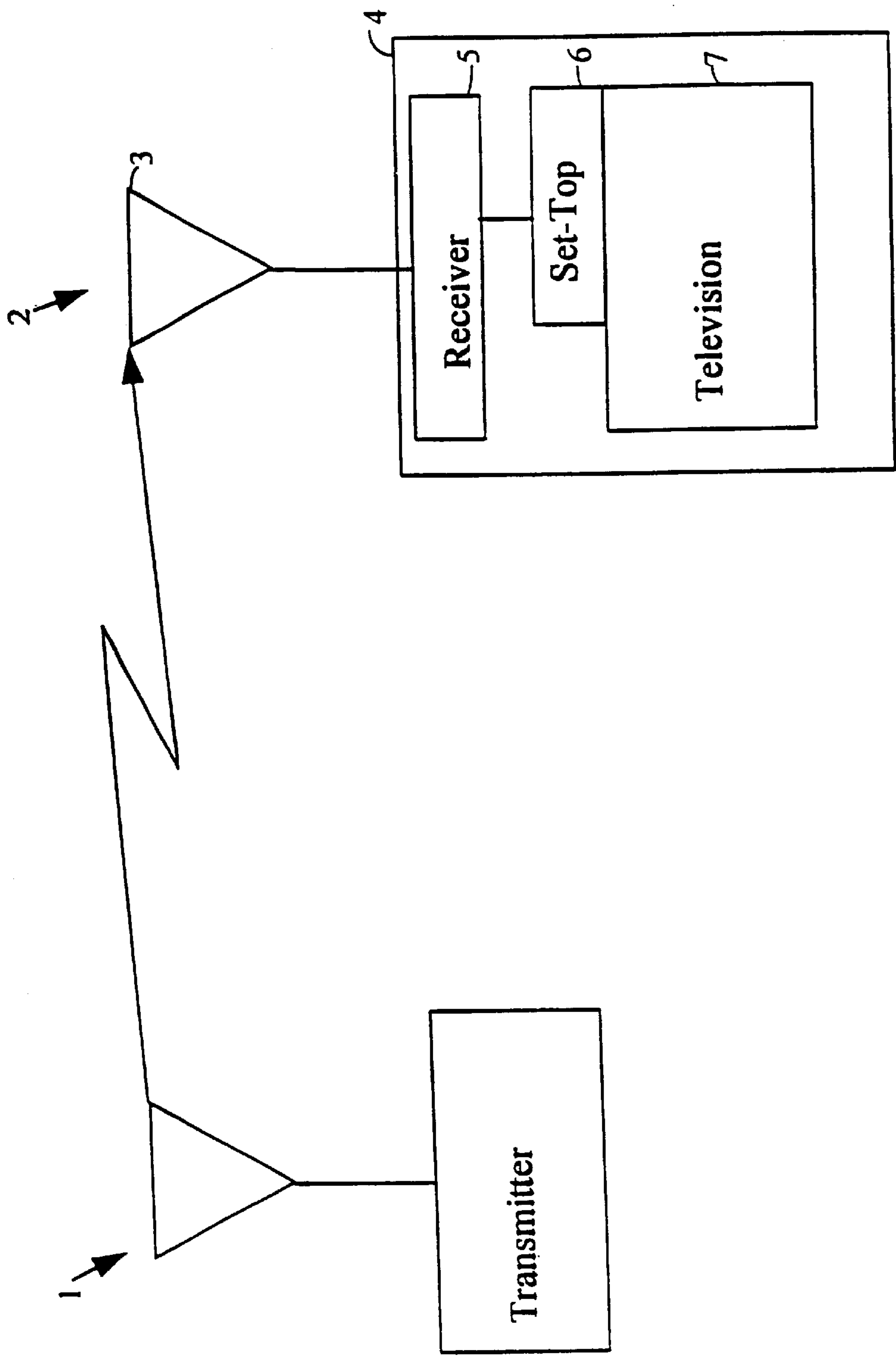
(74) Attorney, Agent, or Firm—Oblon, Spivak, McClelland, Maier & Neustadt, P.C.

#### (57) ABSTRACT

A controller-based radio frequency amplifier method and module are employed in a modular transmission system in which respective of the controller-based radio frequency amplifier modules amplify a portion of a signal that is input into the system. Each amplifier module includes an amplifier submodule have a plurality of discrete amplifiers arranged in an amplifier chain, a processor submodule is configured to control a level of the amplified output signal that is output from each amplifier module, a power supply module, and an enclosure. The processor submodule is configured to control the discrete amplifiers in the amplifier submodule such that the module may be removed or added to the system without damaging the power amplifier module or other system components.

**20 Claims, 45 Drawing Sheets**





Prior Art

FIG. 1

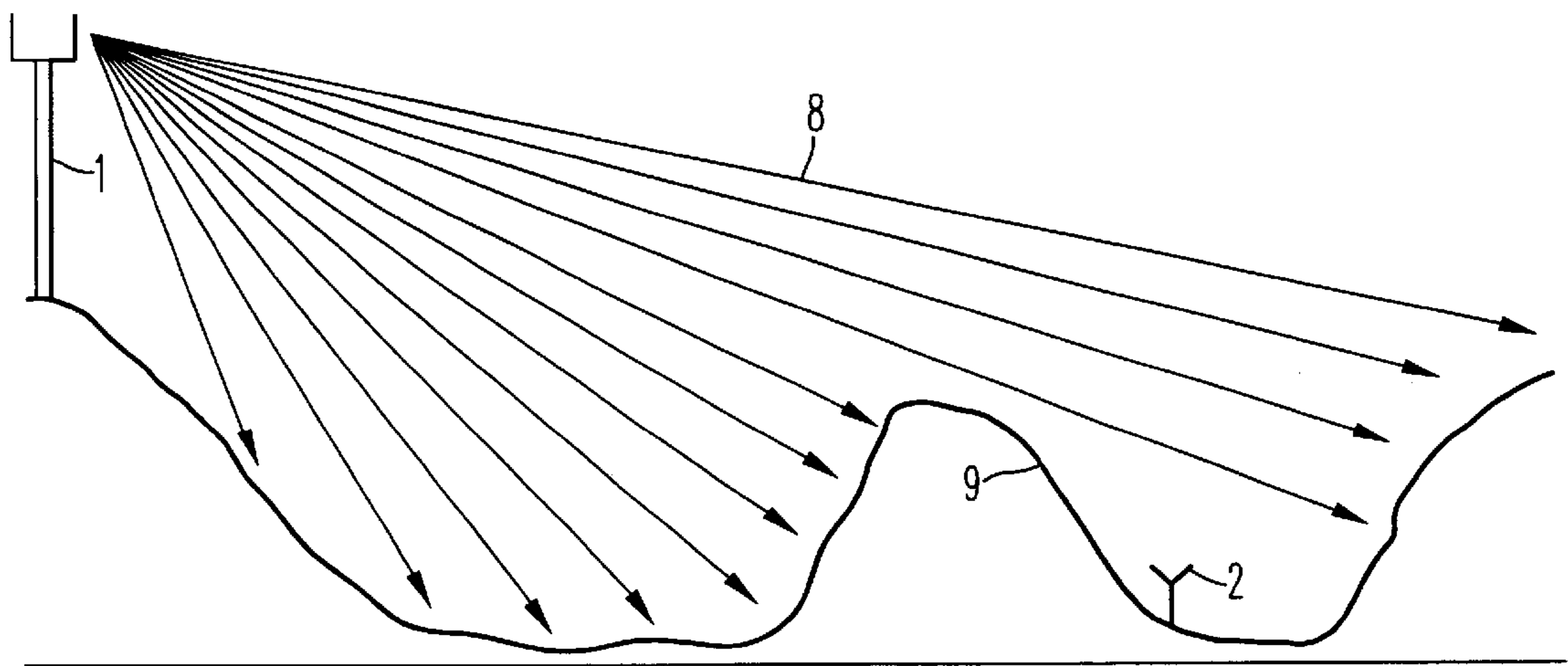


FIG. 2

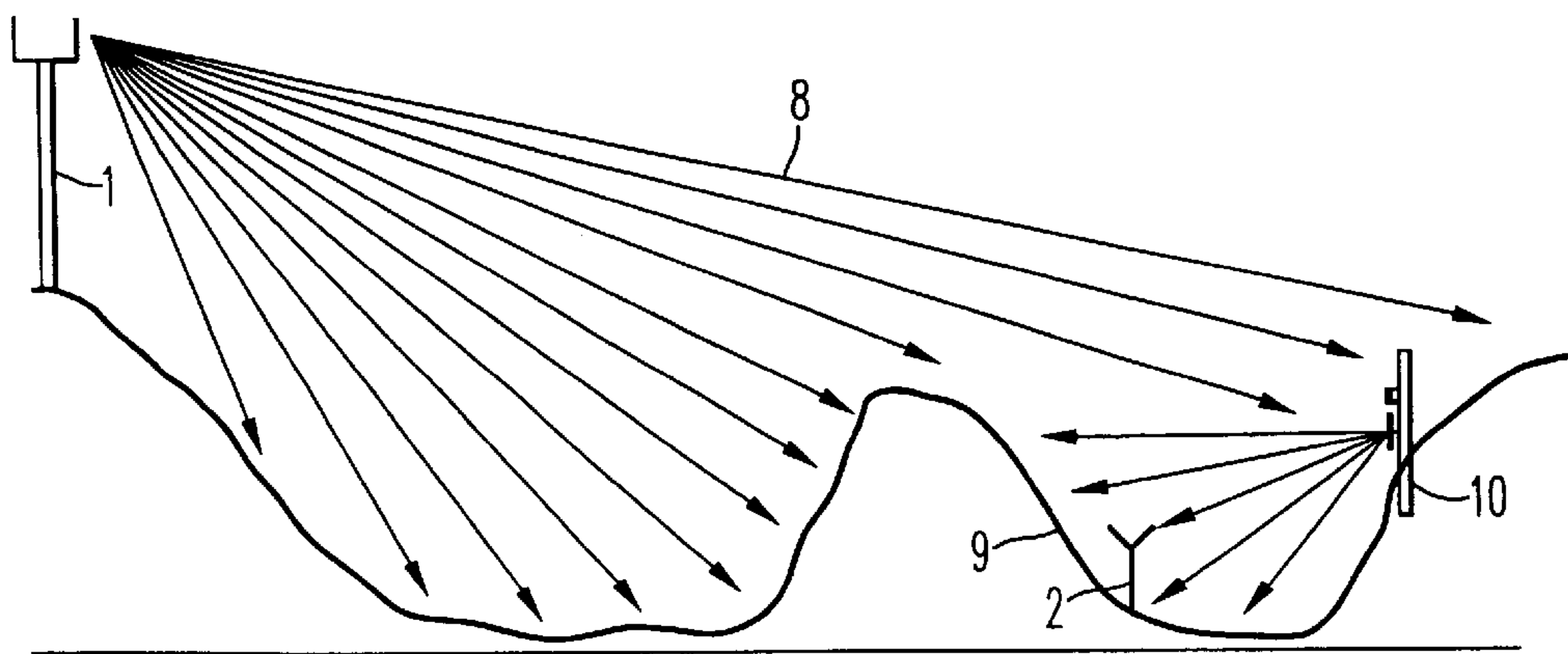


FIG. 3

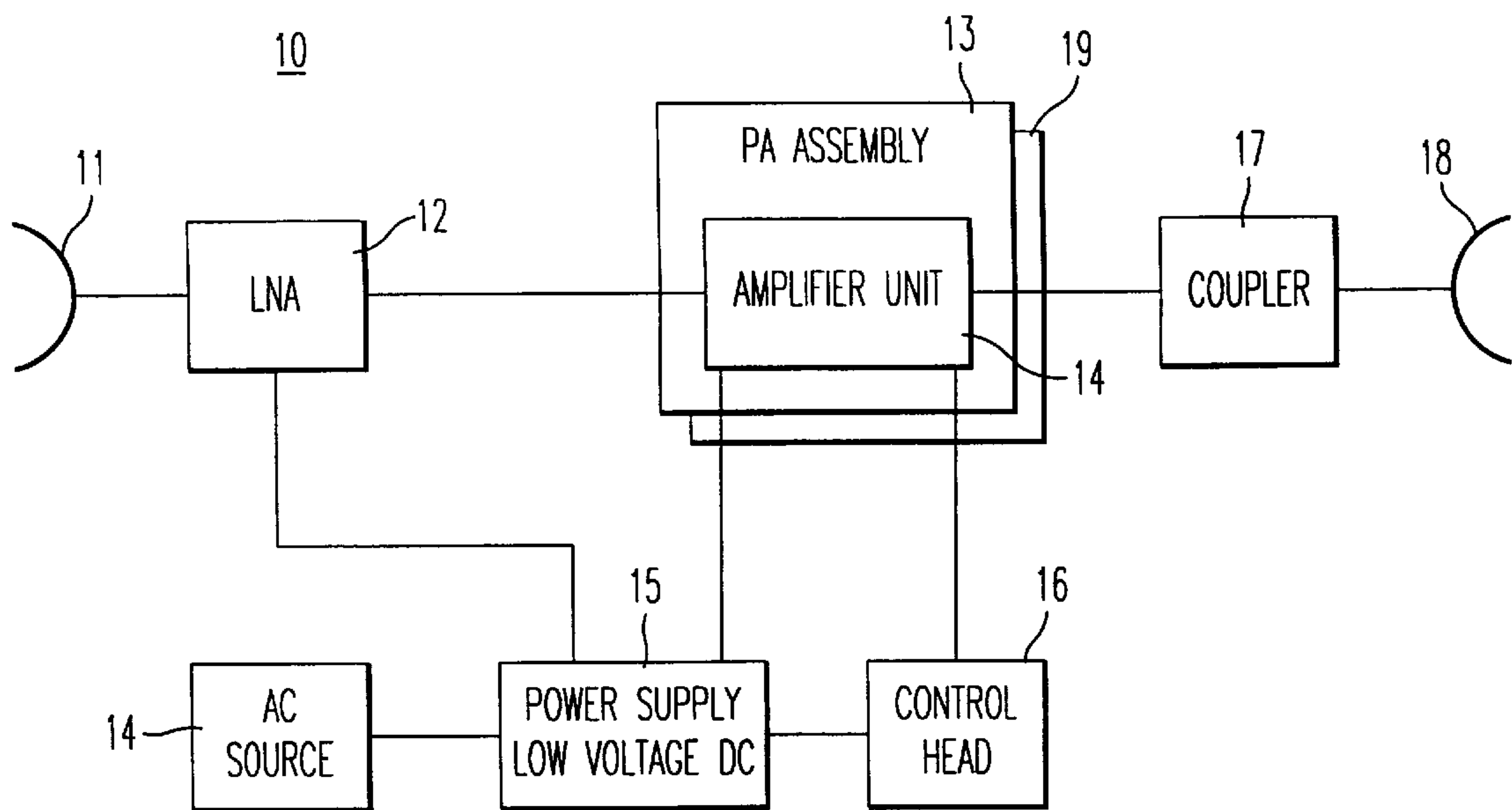


FIG. 4  
PRIOR ART

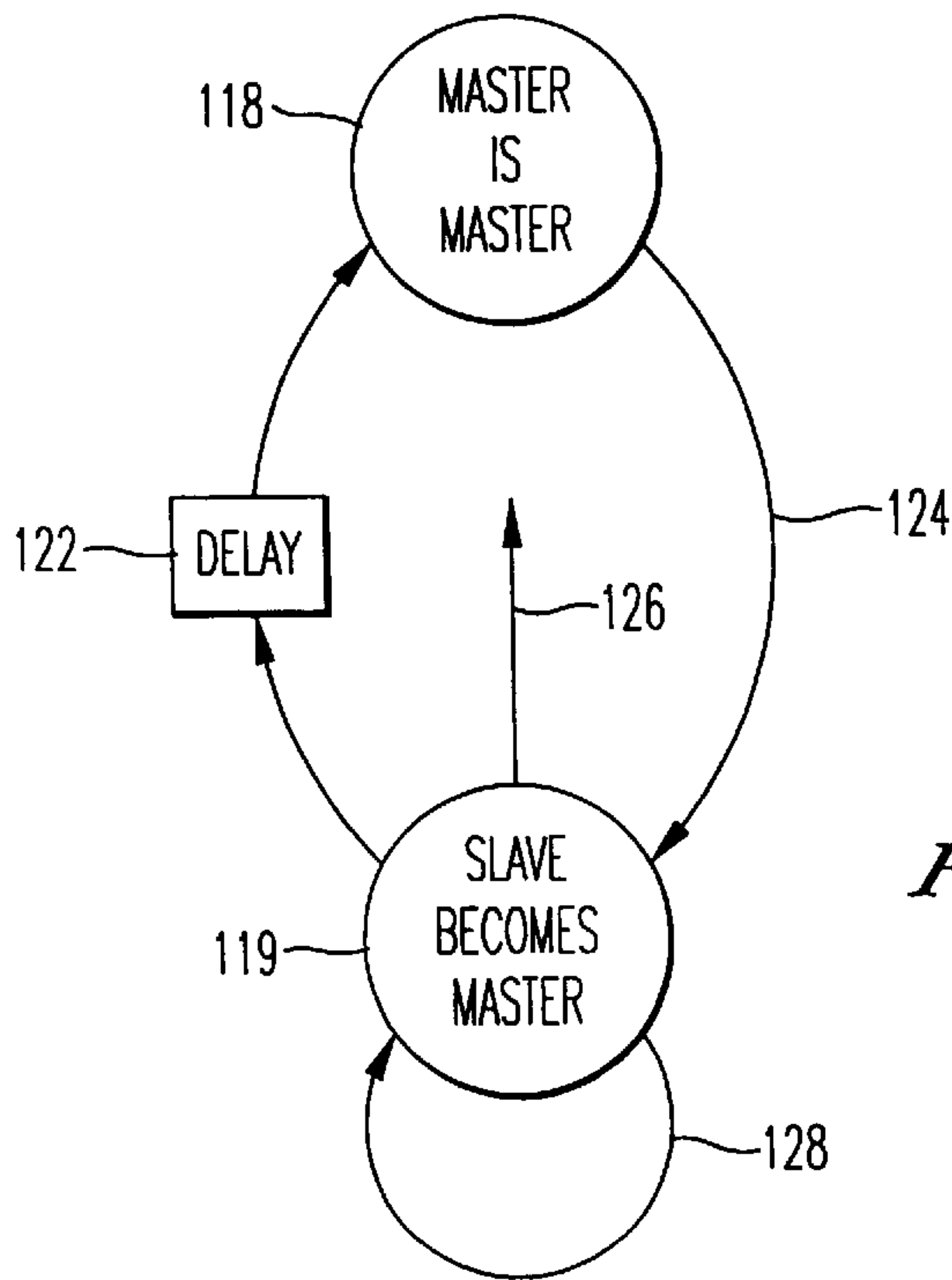


FIG. 9A

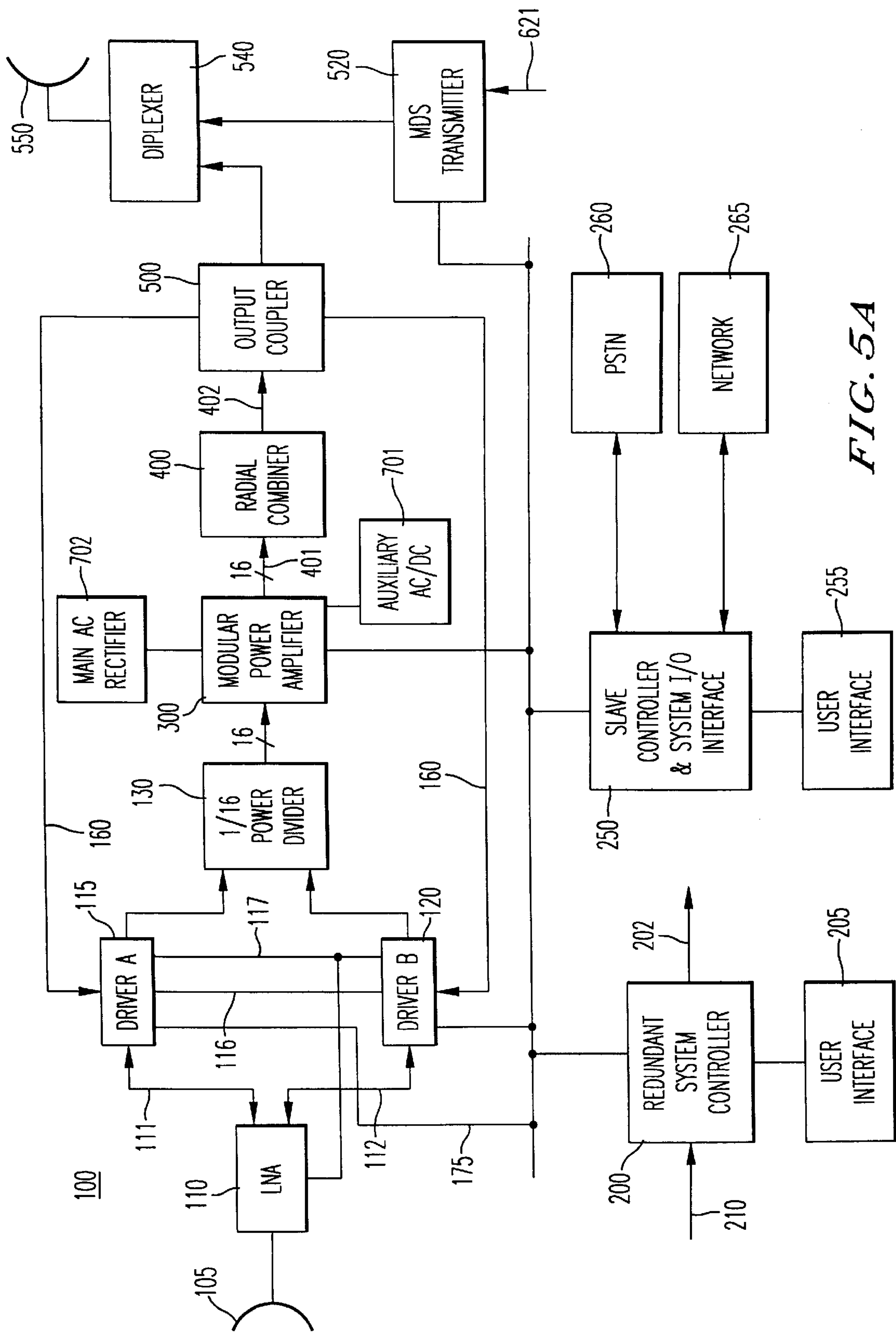


FIG. 5A

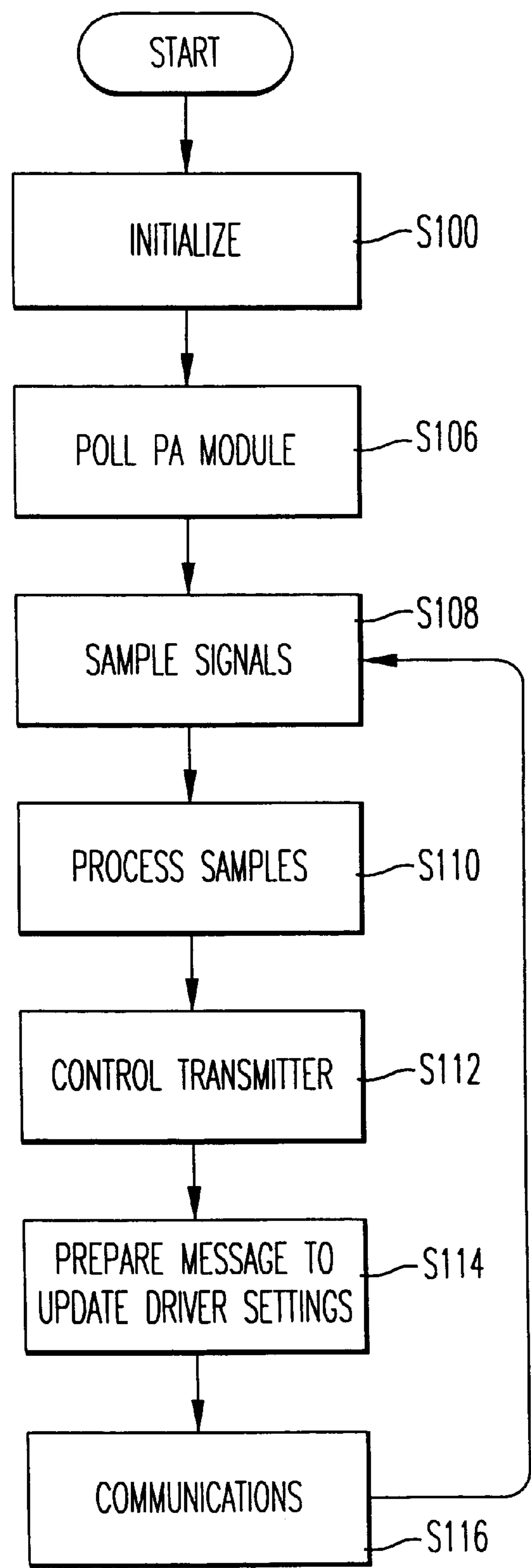


FIG. 5B

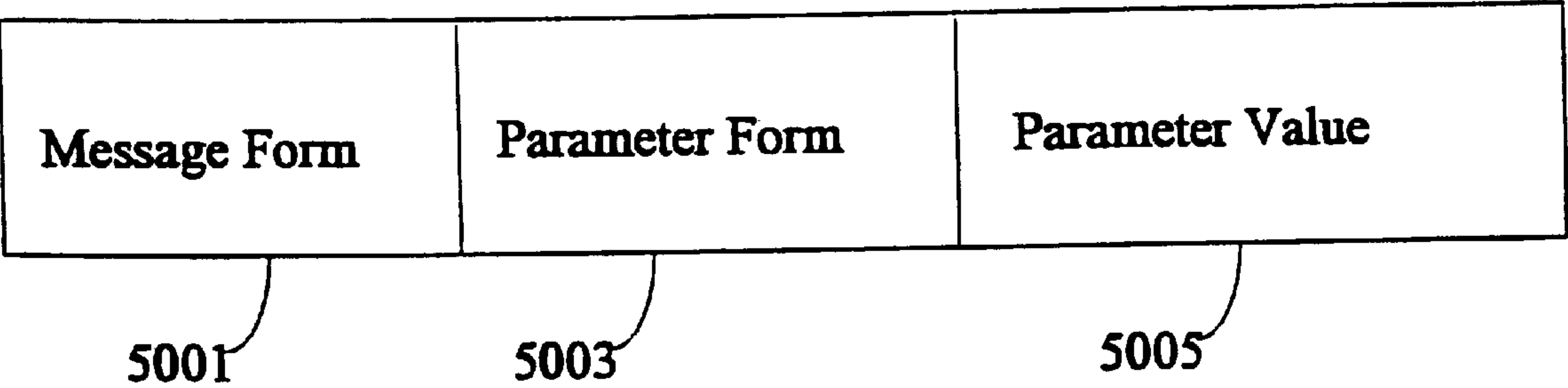


Figure 5C



FIG. 6

CHANNEL DESIGNATION	BANDWIDTH (MHz)	
MDS1	2150-2156	F1
MDS2	2156-2162	
ITFS A1	2500-2506	F2
ITFS A2	2512-2518	
ITFS A3	2524-2530	
ITFS A4	2536-2542	
ITFS B1	2506-2512	
ITFS B2	2518-2524	
ITFS B3	2530-2536	
ITFS B4	2542-2548	
ITFS C1	2548-2554	
ITFS C2	2560-2566	
ITFS C3	2572-2578	
ITFS C4	2584-2590	
ITFS D1	2554-2560	
ITFS D2	2566-2572	
ITFS D3	2578-2584	
ITFS D4	2590-2596	
MMDS E1	2596-2602	
MMDS E2	2608-2614	
MMDS E3	2620-2626	
MMDS E4	2632-2638	
MMDS F1	2602-2608	
MMDS F2	2614-2620	
MMDS F3	2626-2632	
MMDS F4	2638-2644	
ITFS G1	2644-2650	F3
ITFS G2	2656-2662	
ITFS G3	2668-2674	
ITFS G4	2680-2686	
OFS H1	2650-2656	F3
OFS H2	2662-2668	
OFS H3	2674-2680	



110

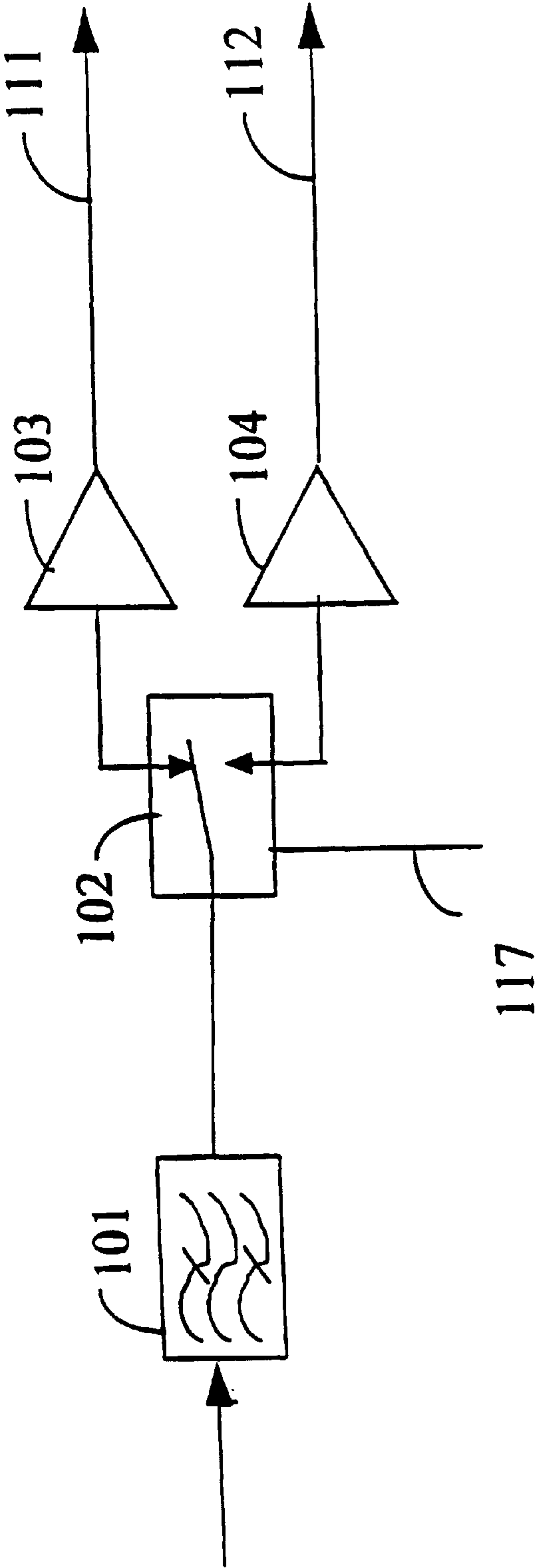


FIG. 7

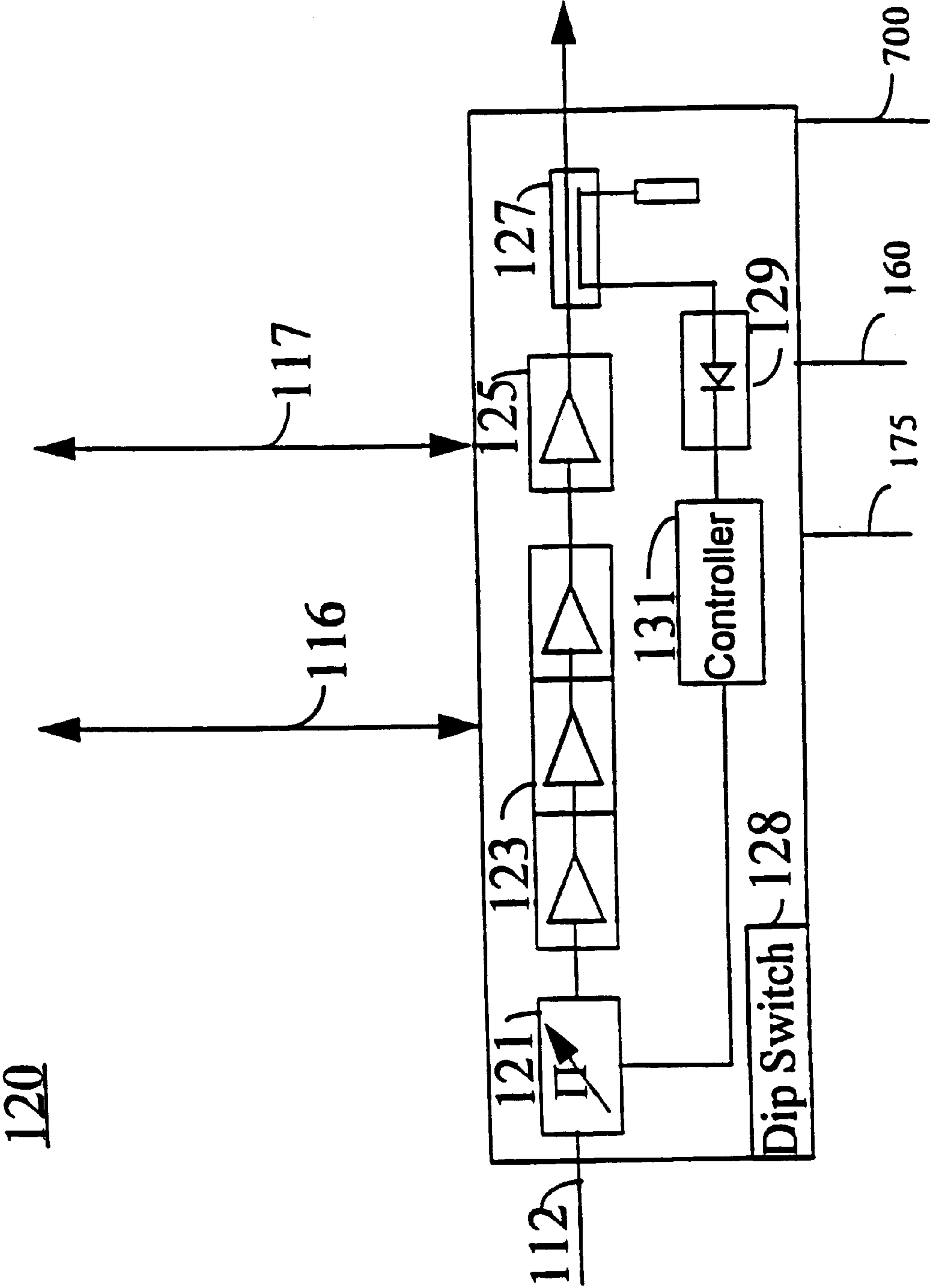
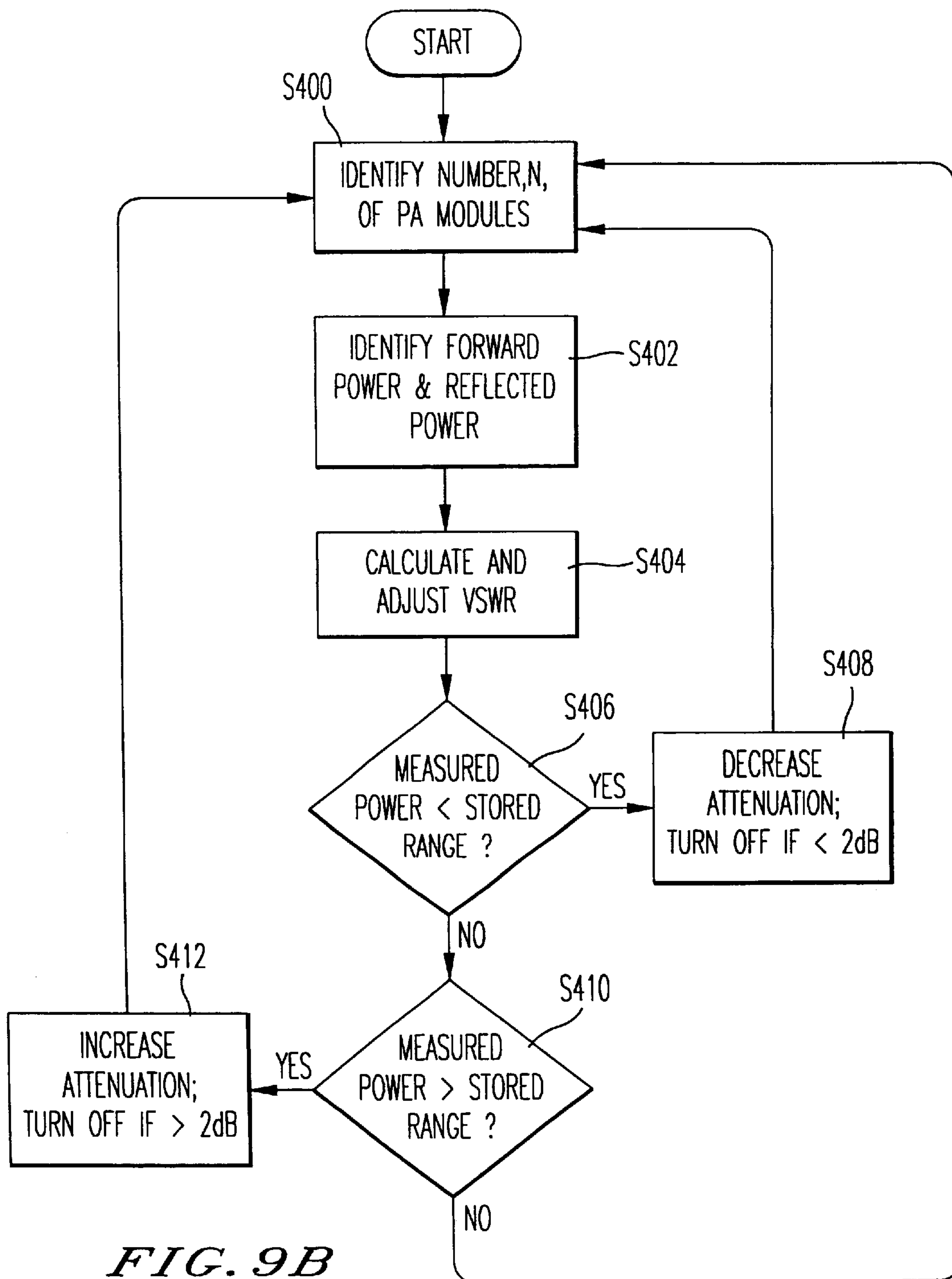
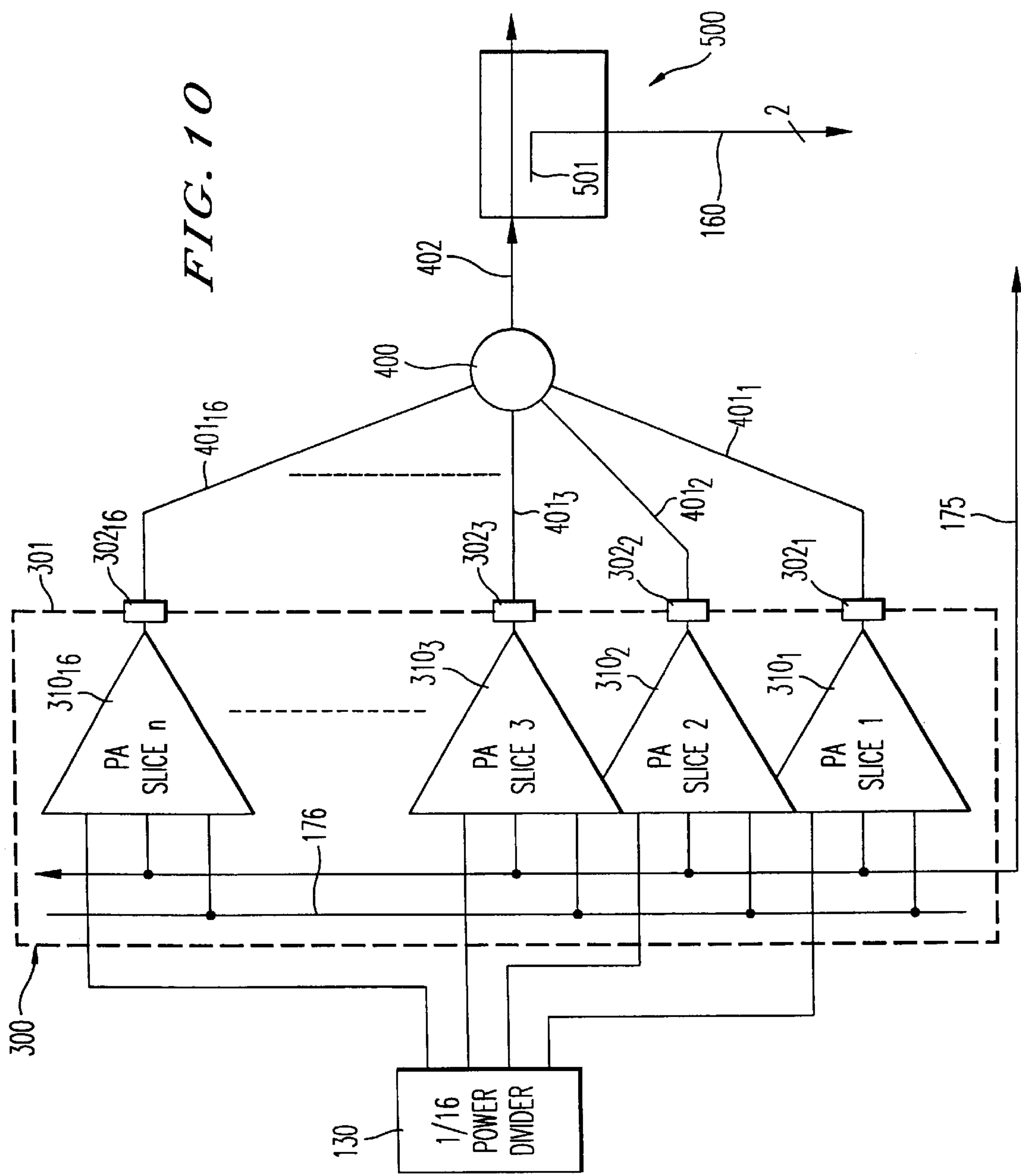


FIG. 8

*FIG. 9B*



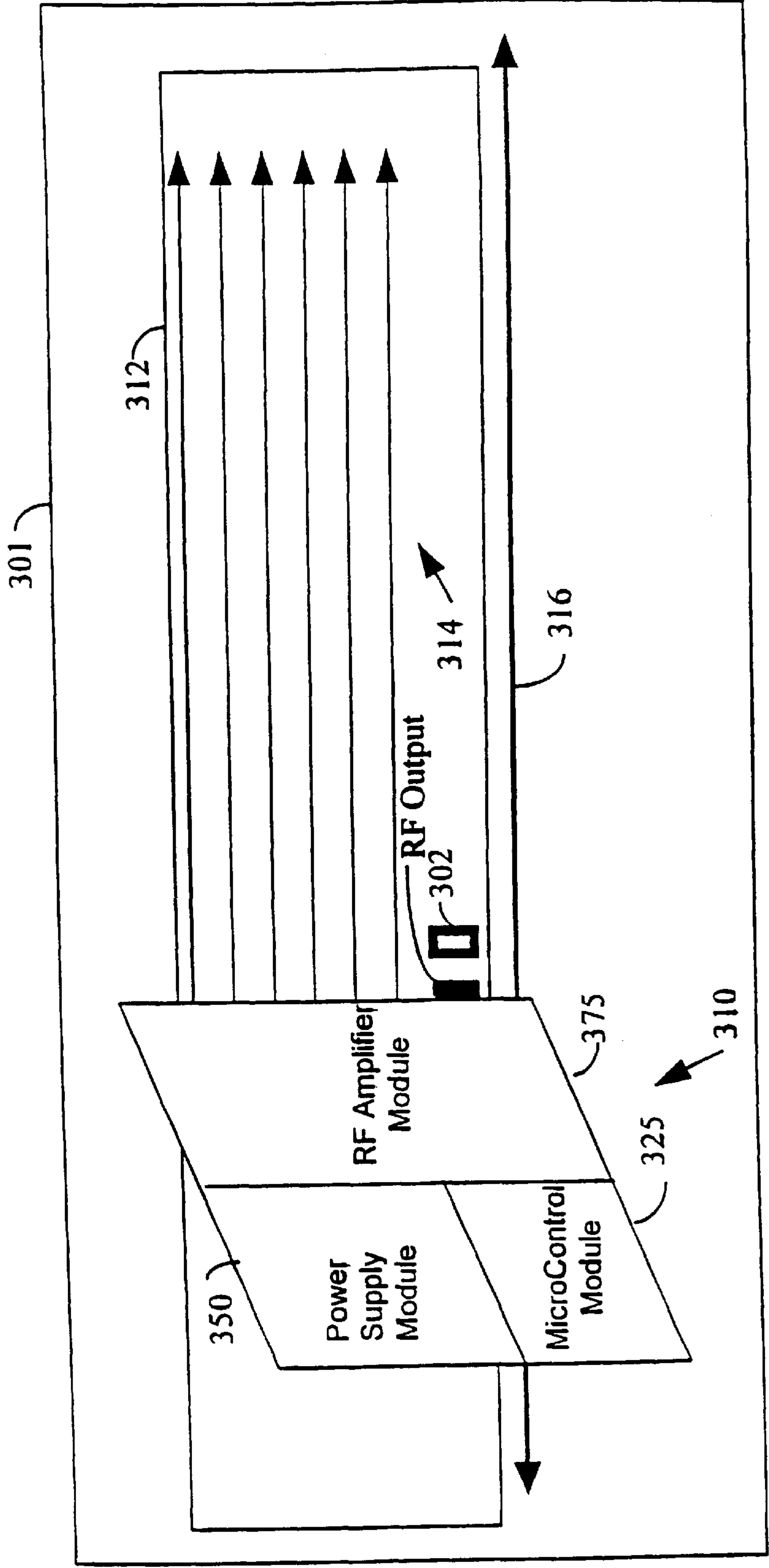


FIG. 11

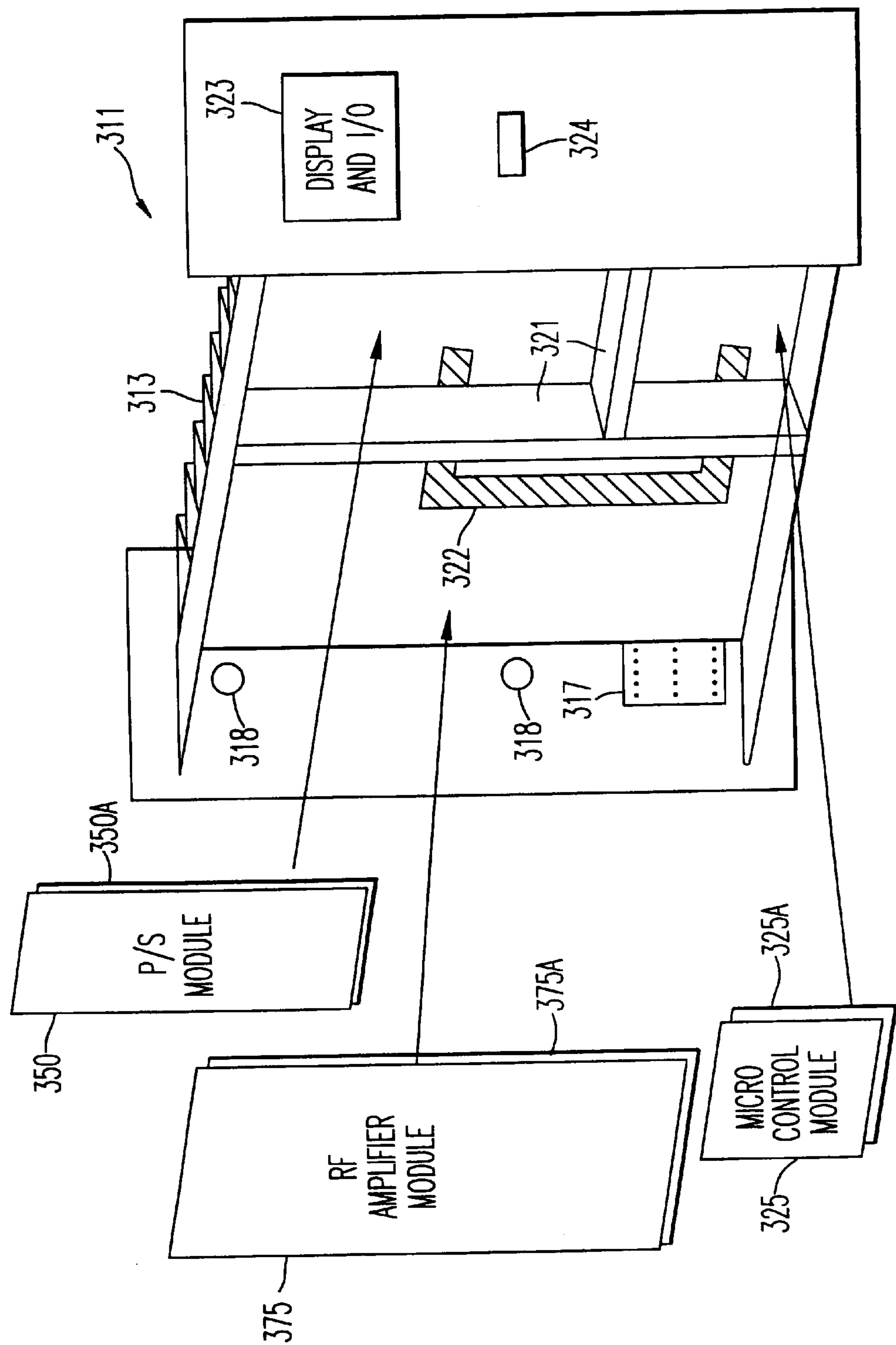


FIG. 12



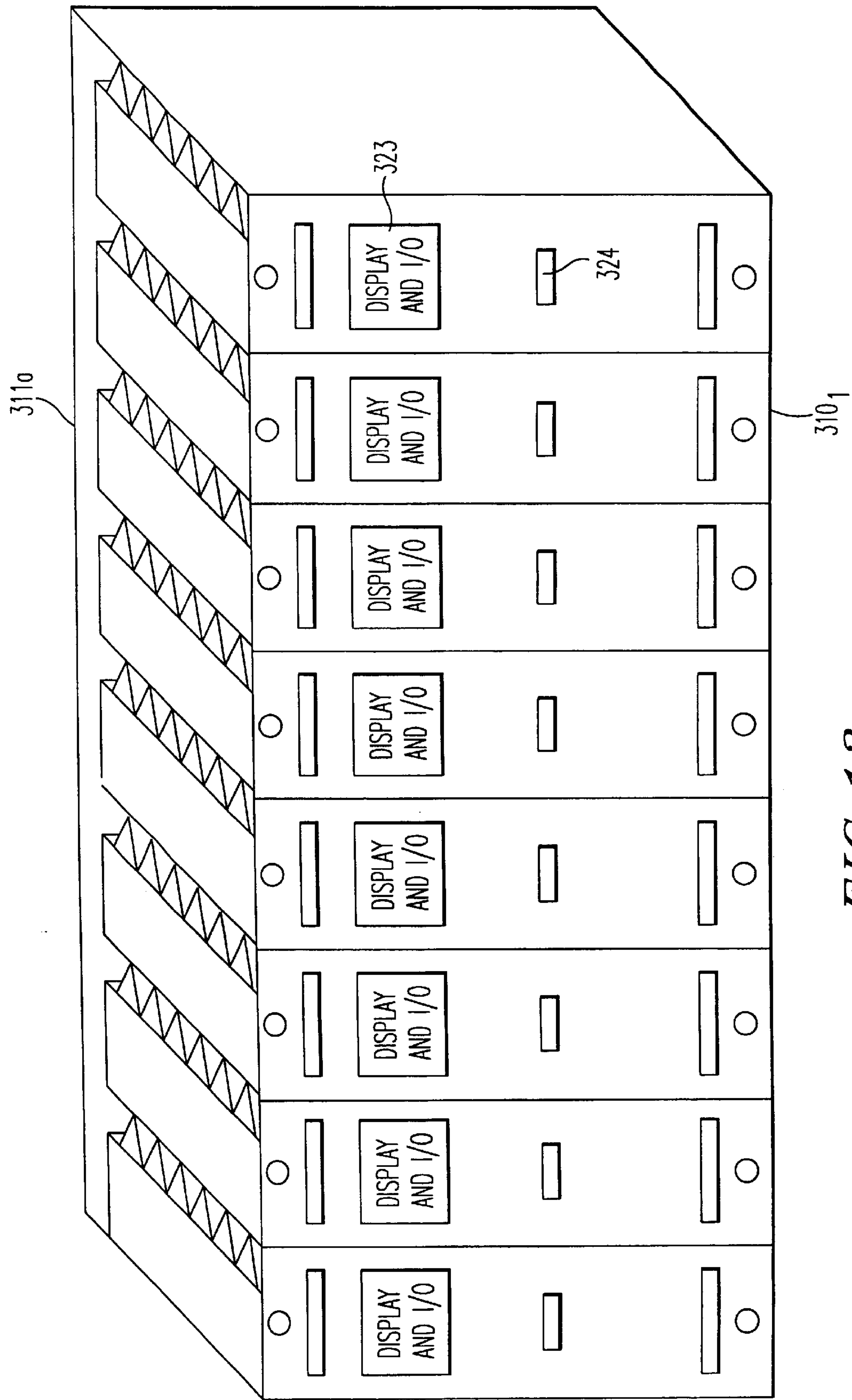


FIG. 13

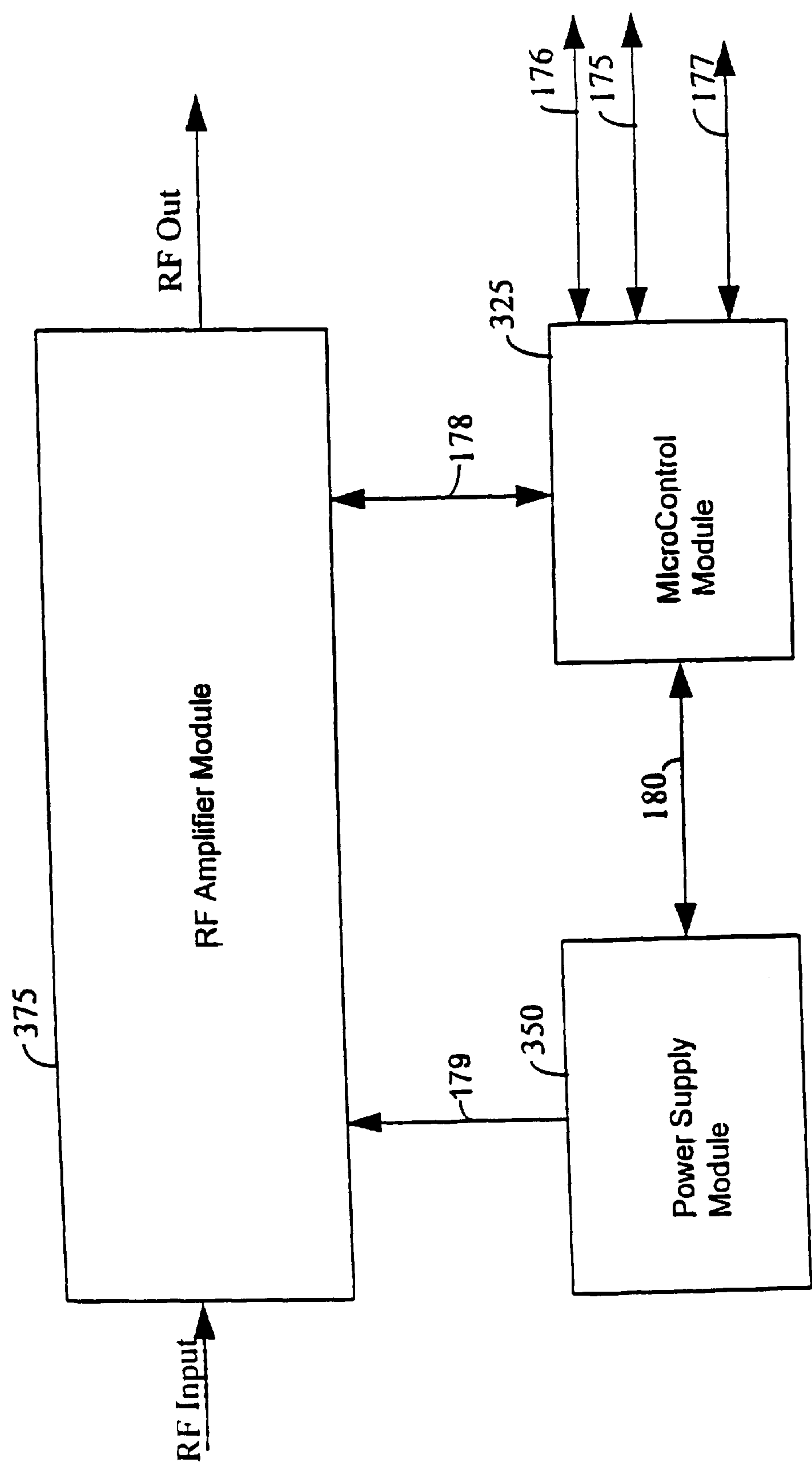


FIG. 14

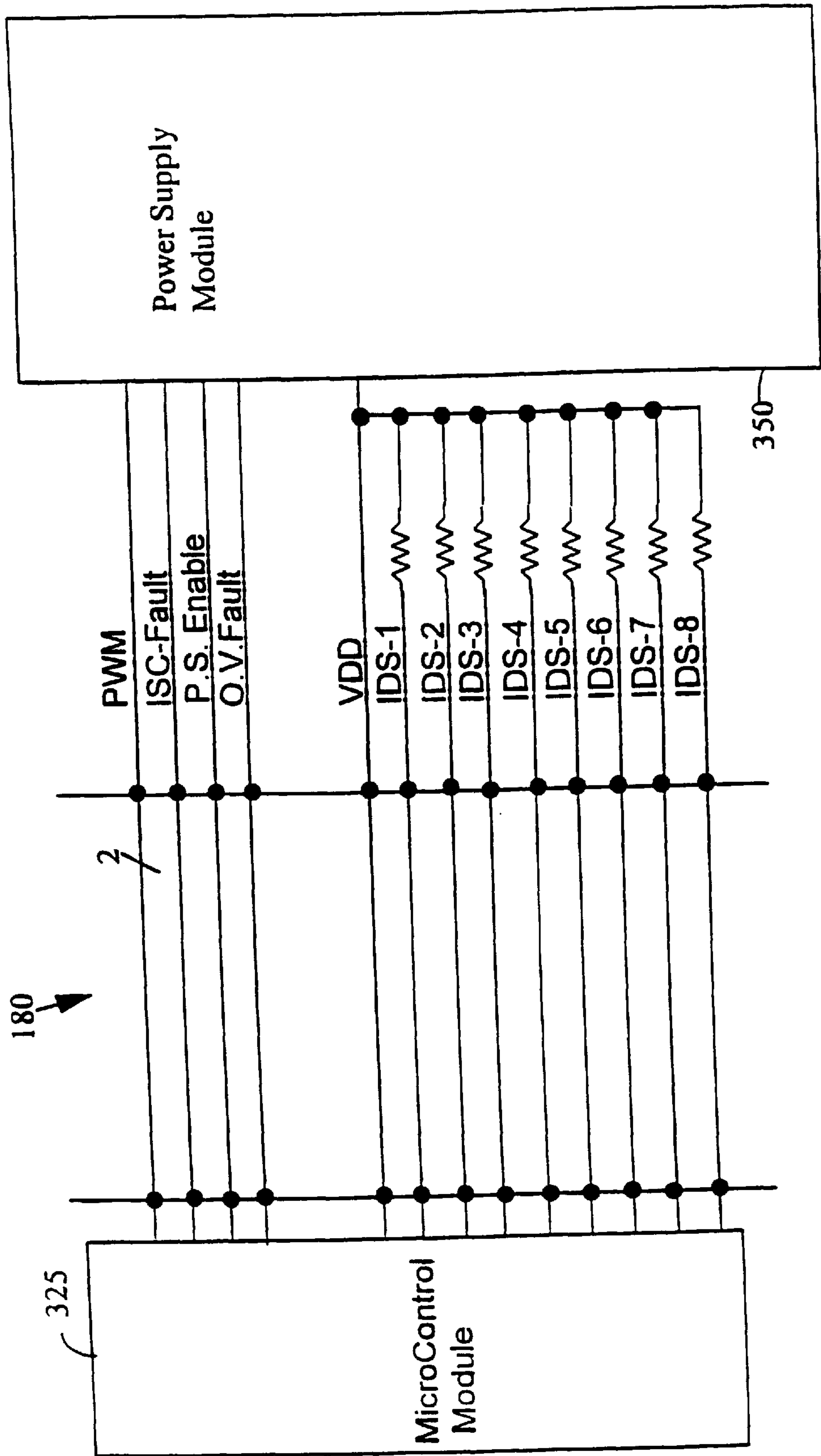


FIG. 15

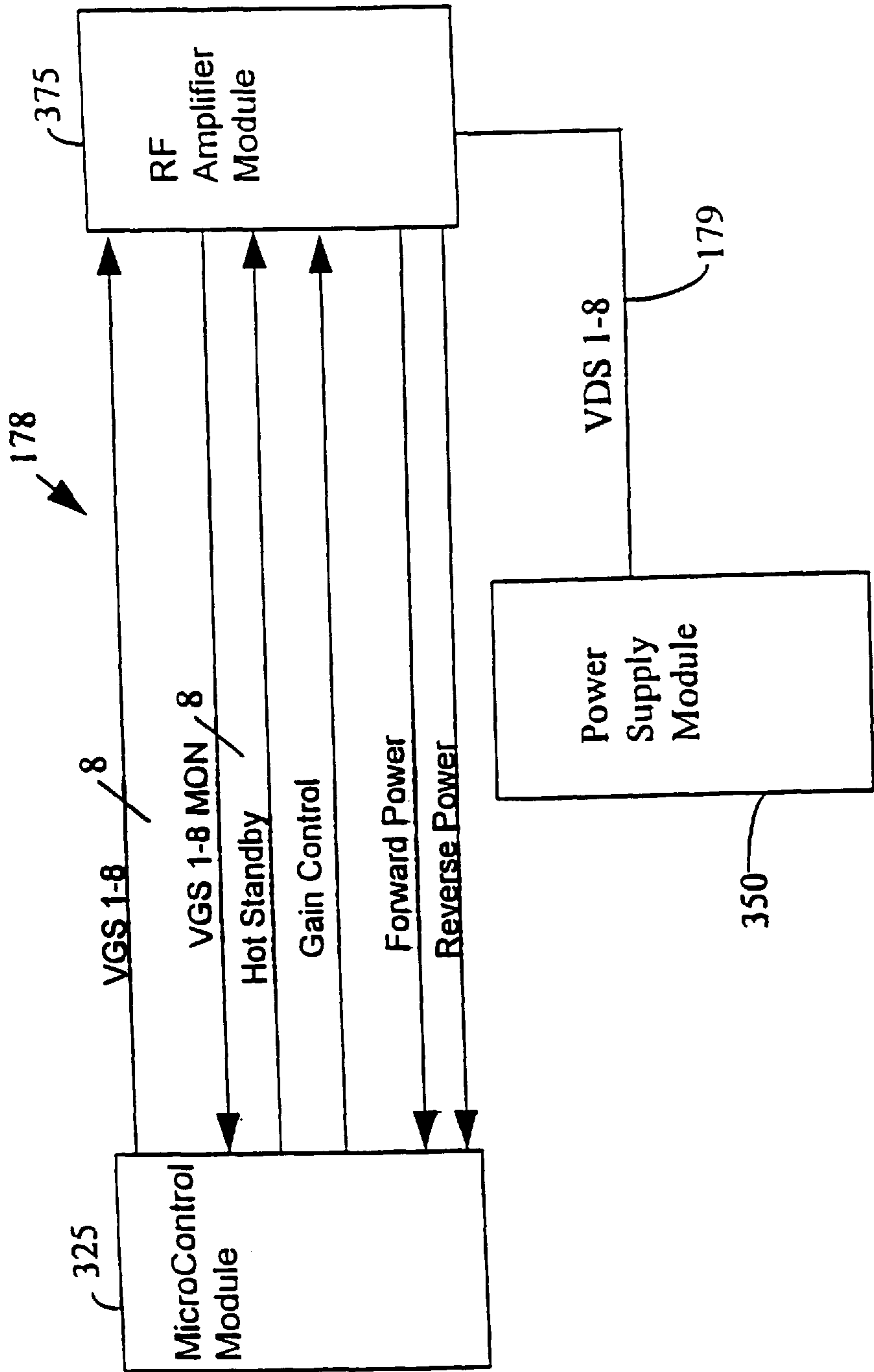


FIG. 16

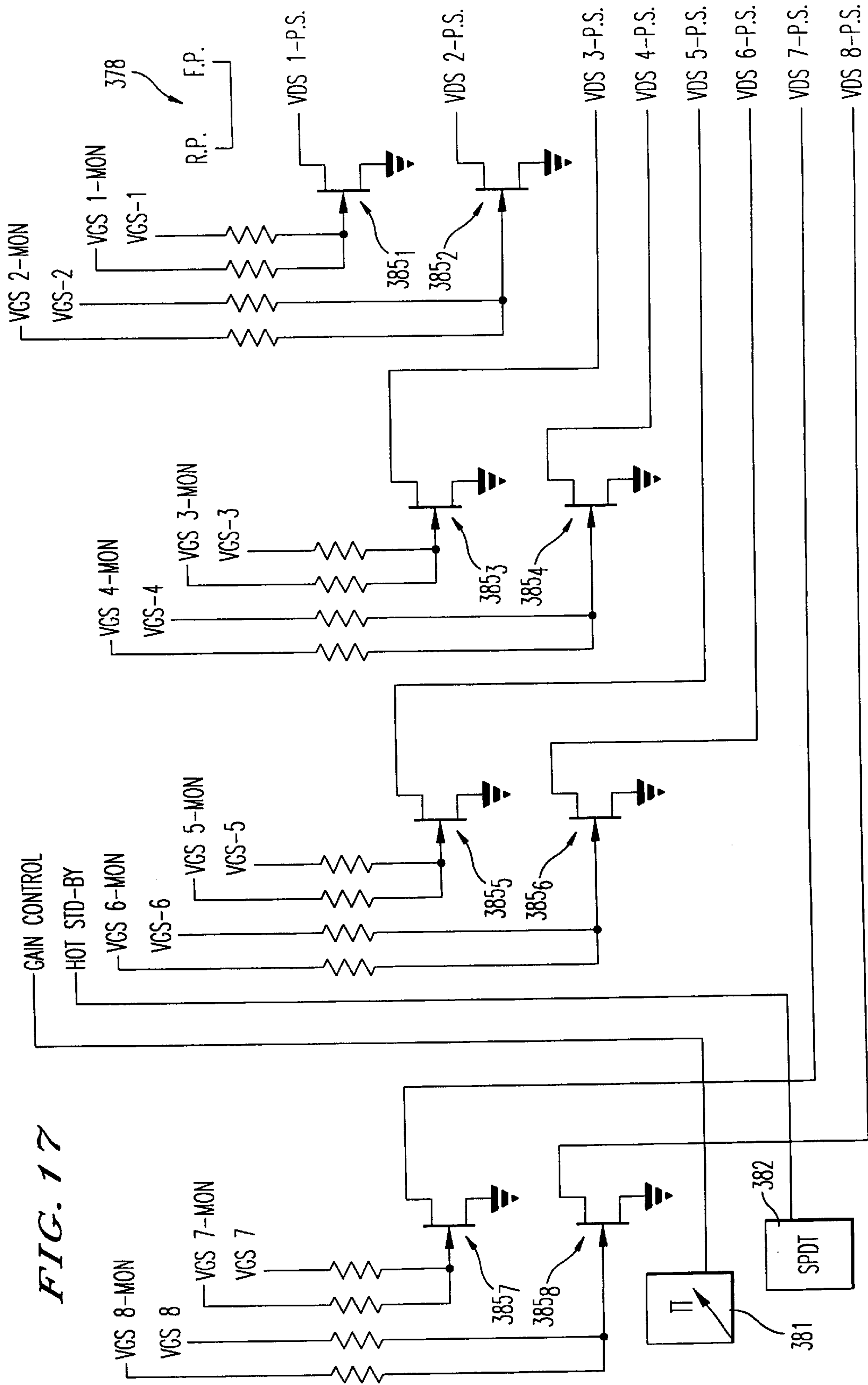
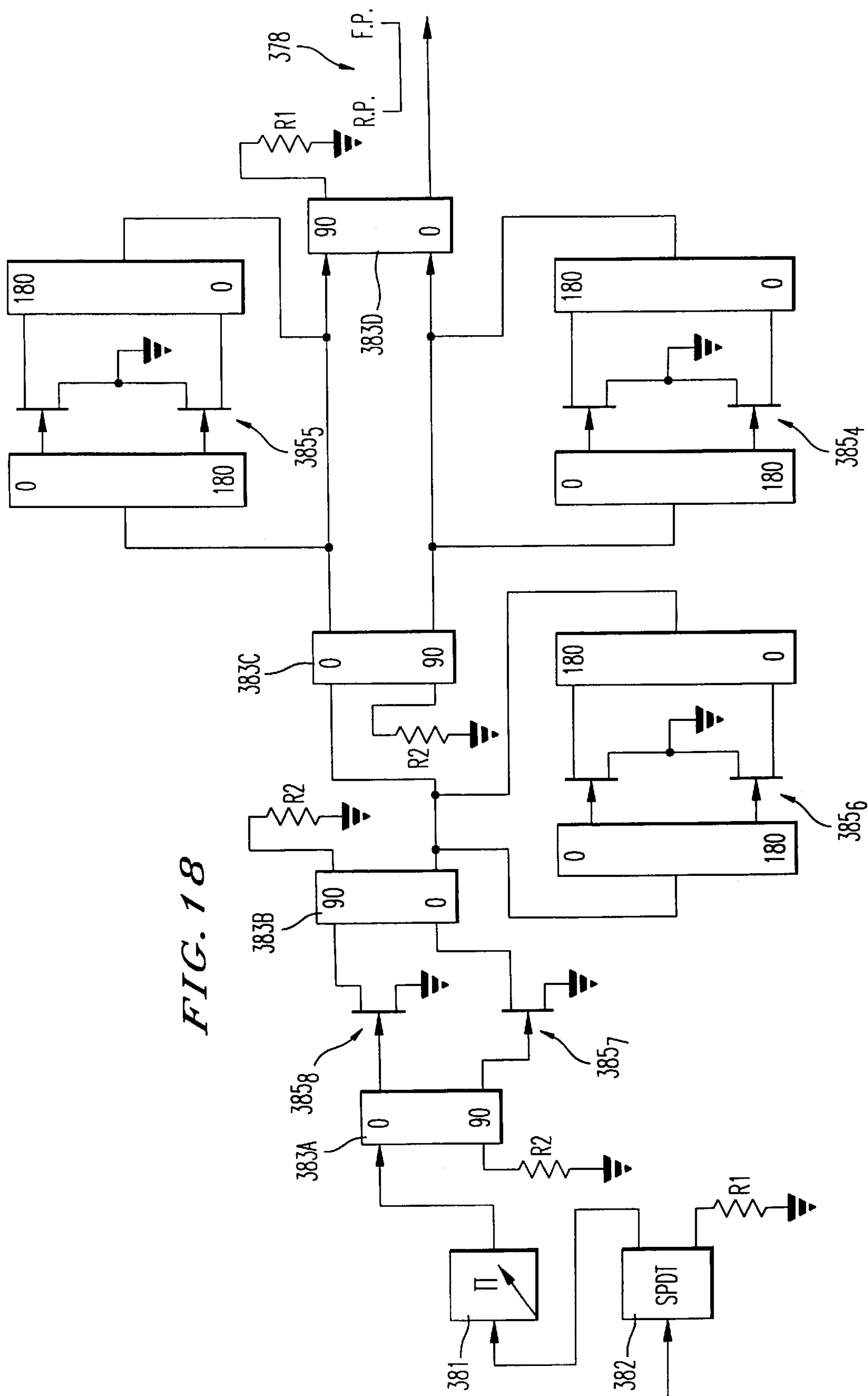


FIG. 17

FIG. 18





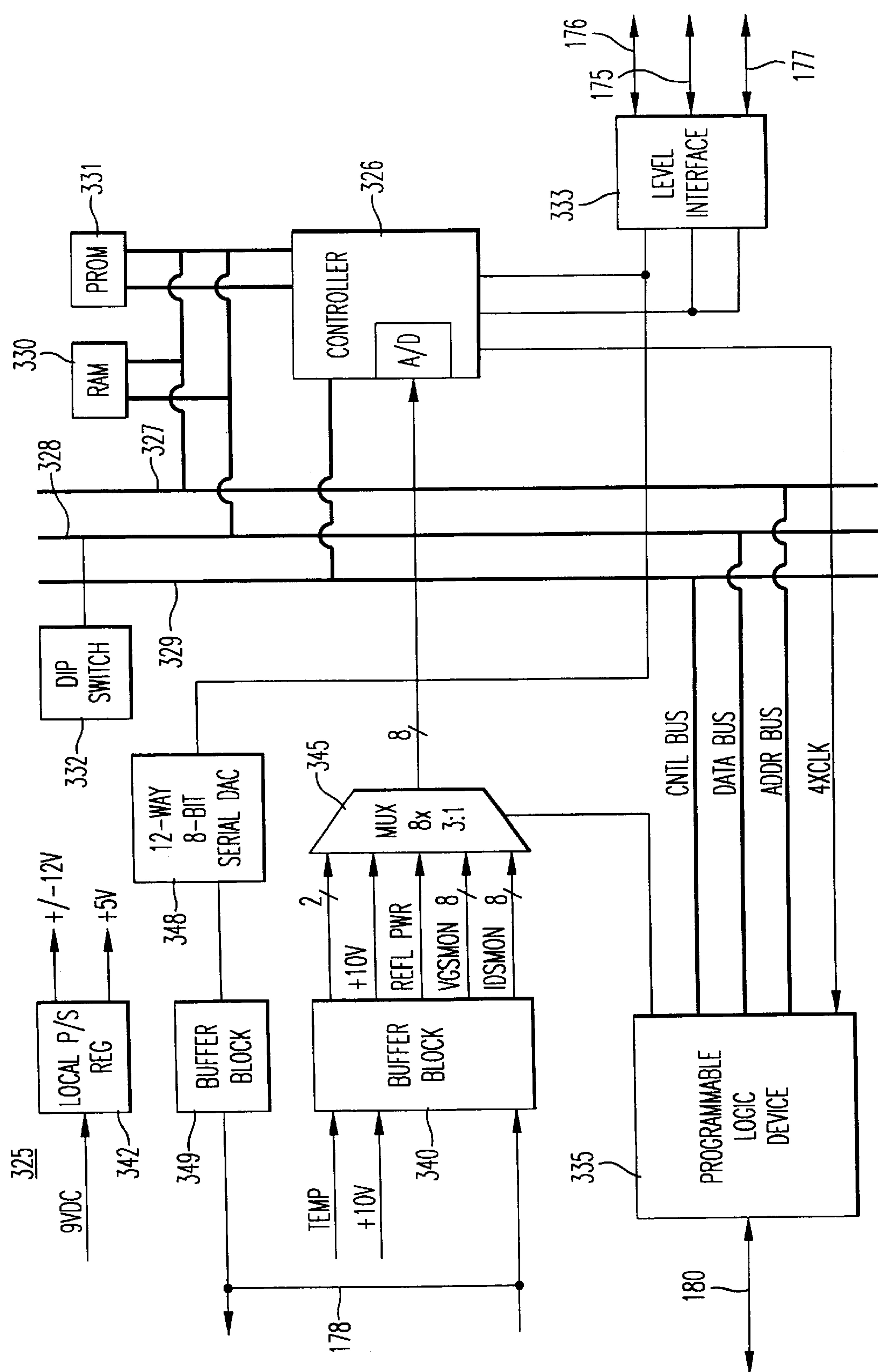


FIG. 19

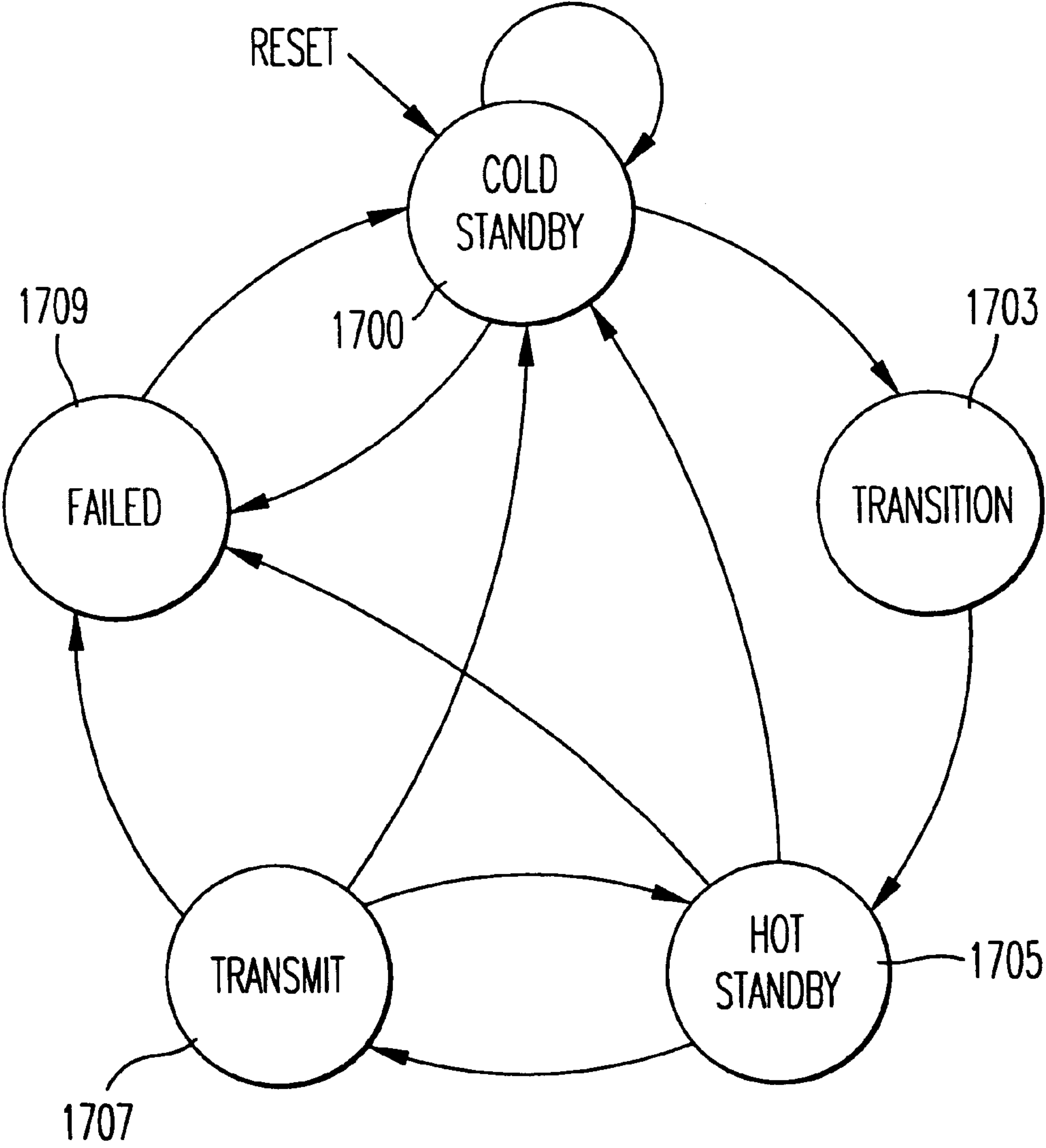


FIG. 20A

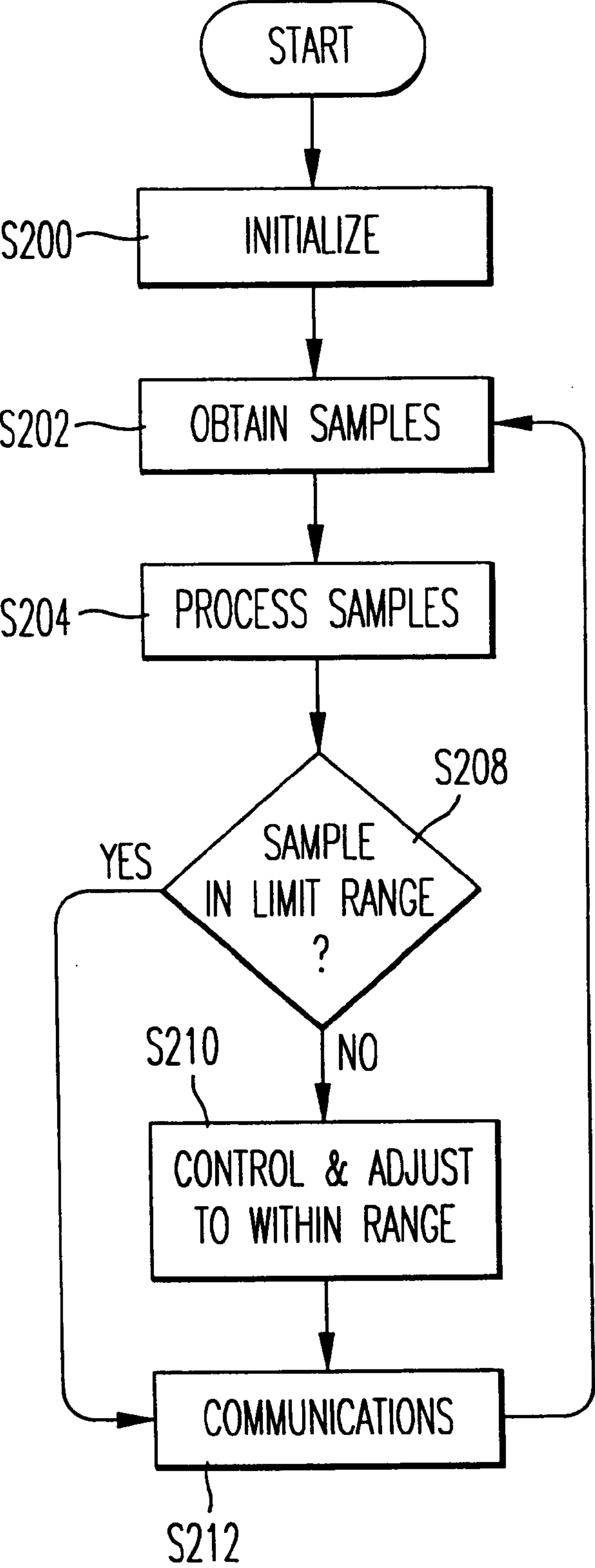
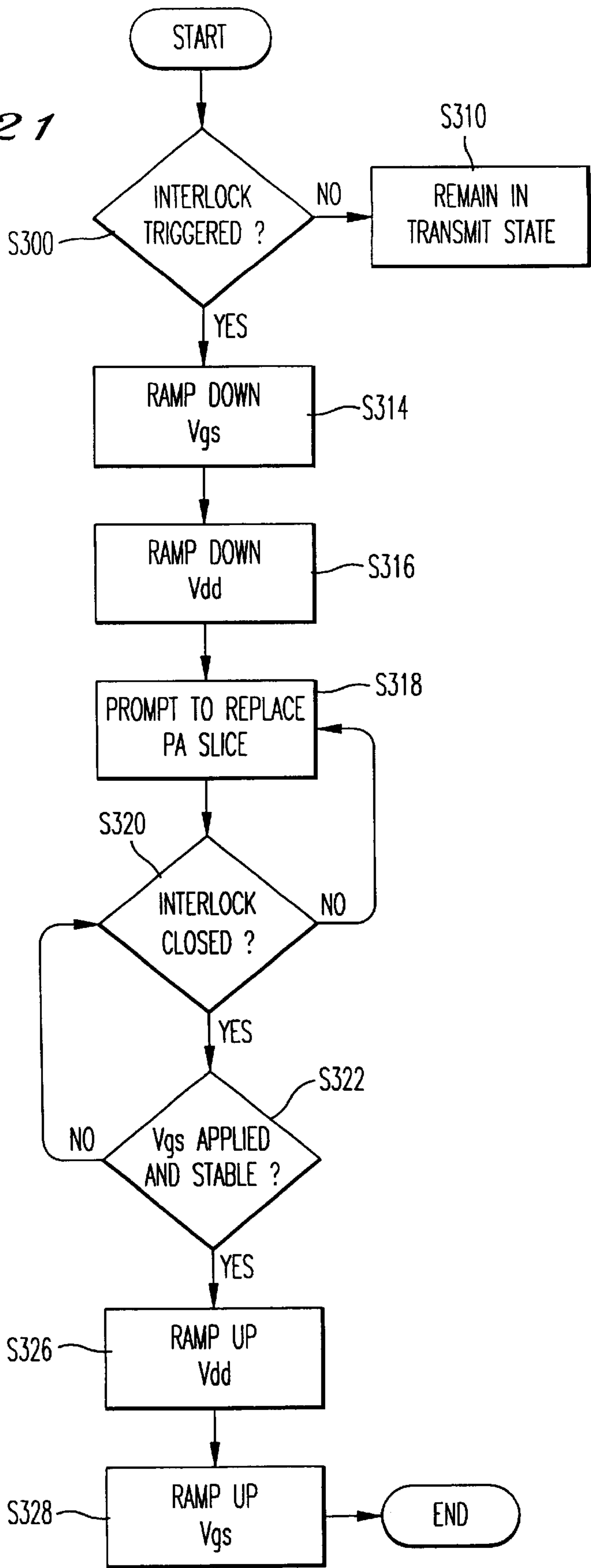


FIG. 20B

FIG. 21



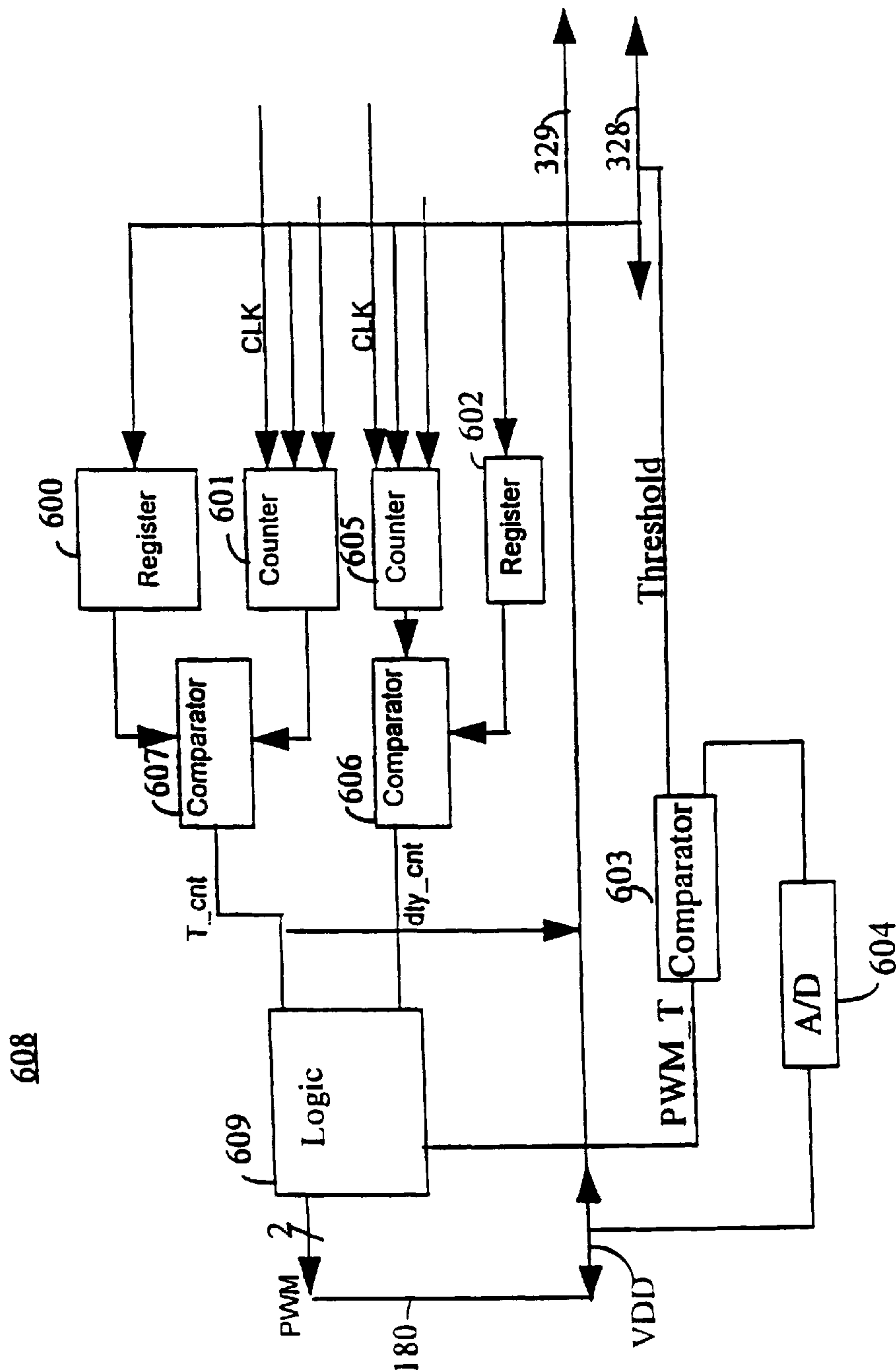


FIG. 22

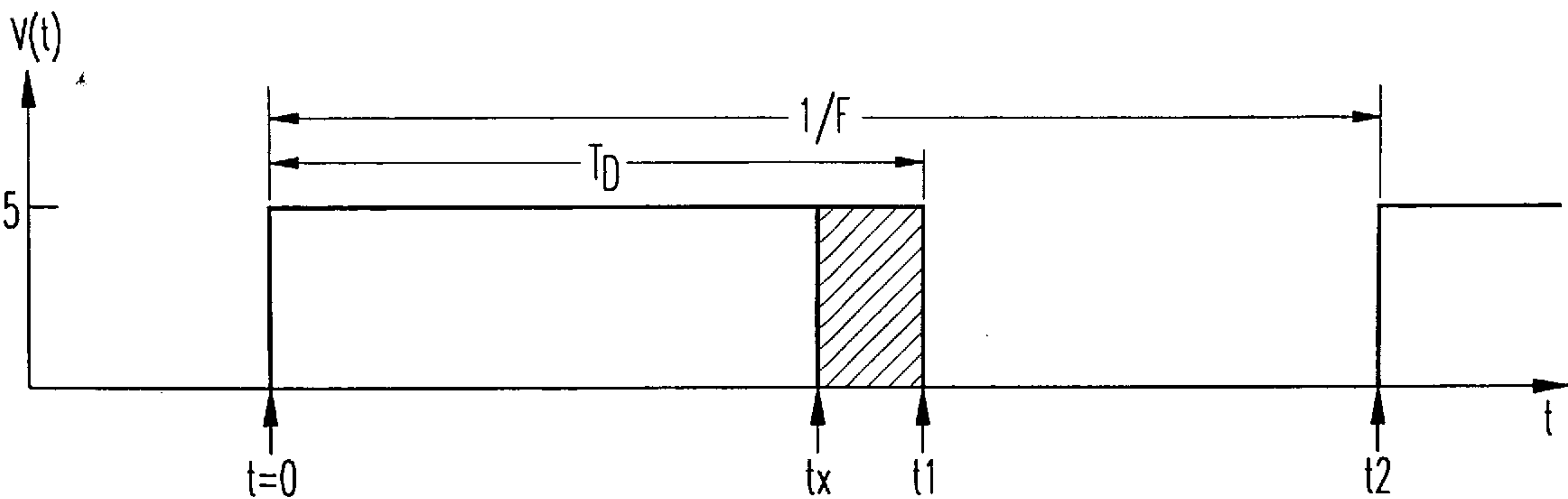


FIG. 23

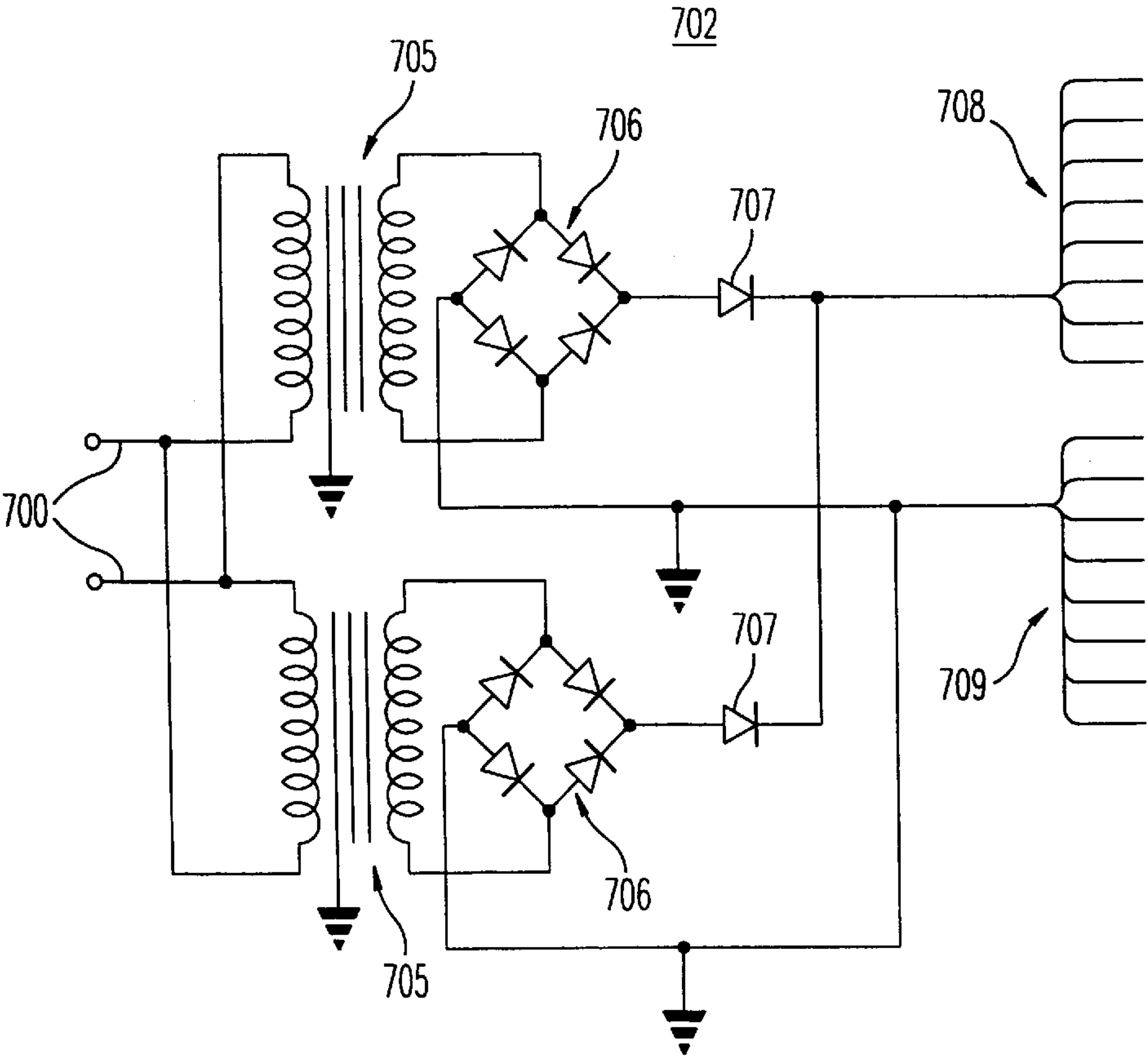


FIG. 26



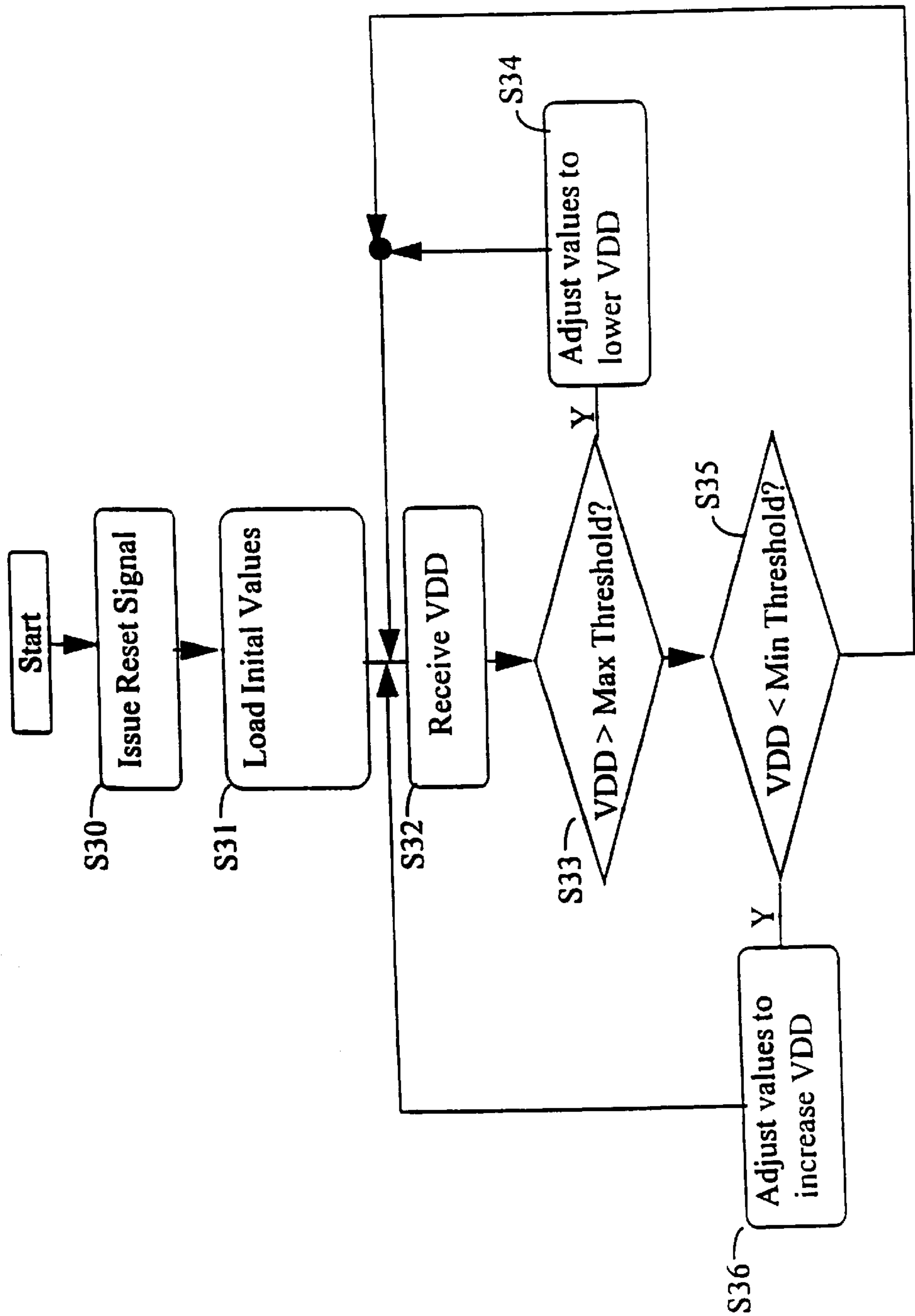
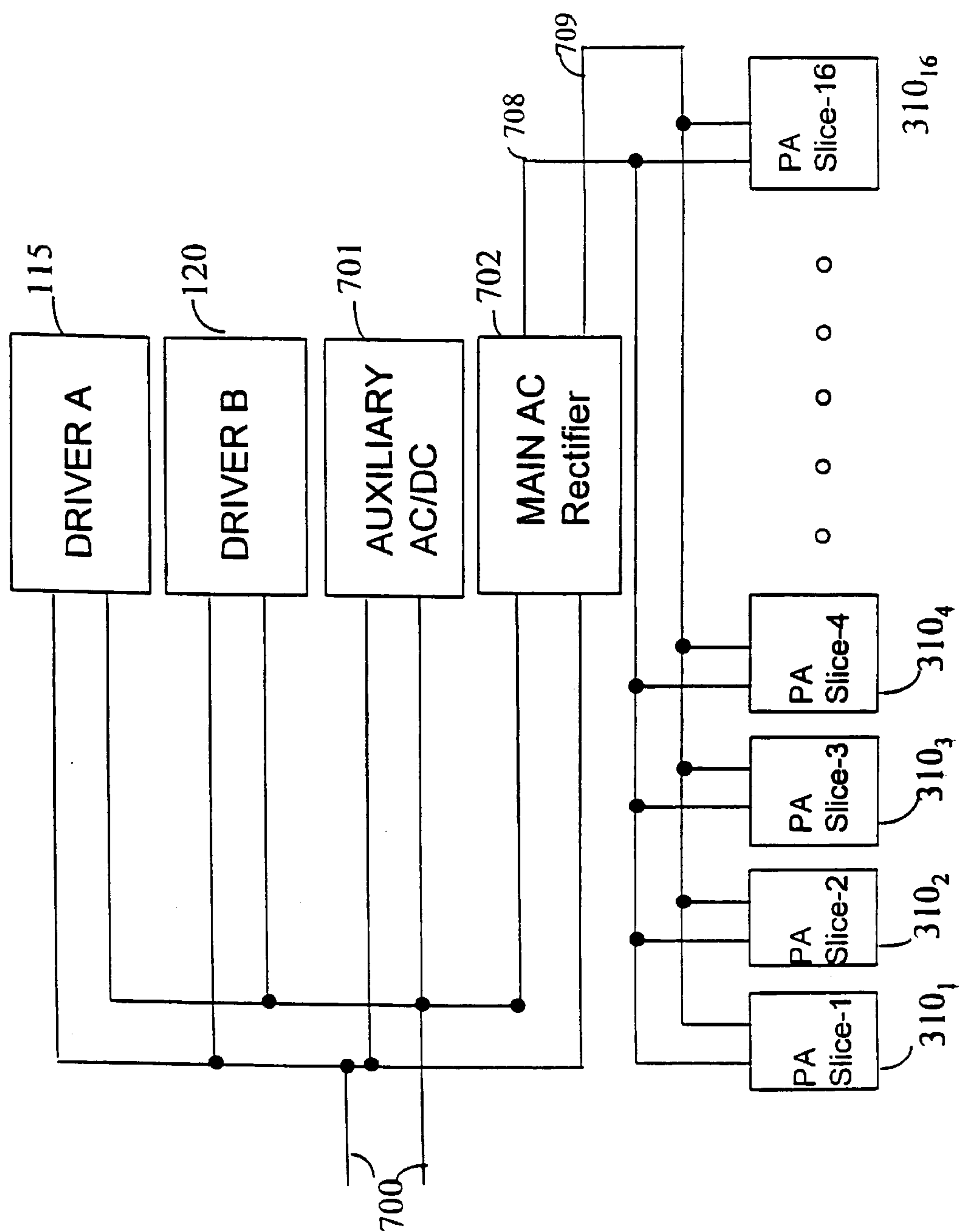
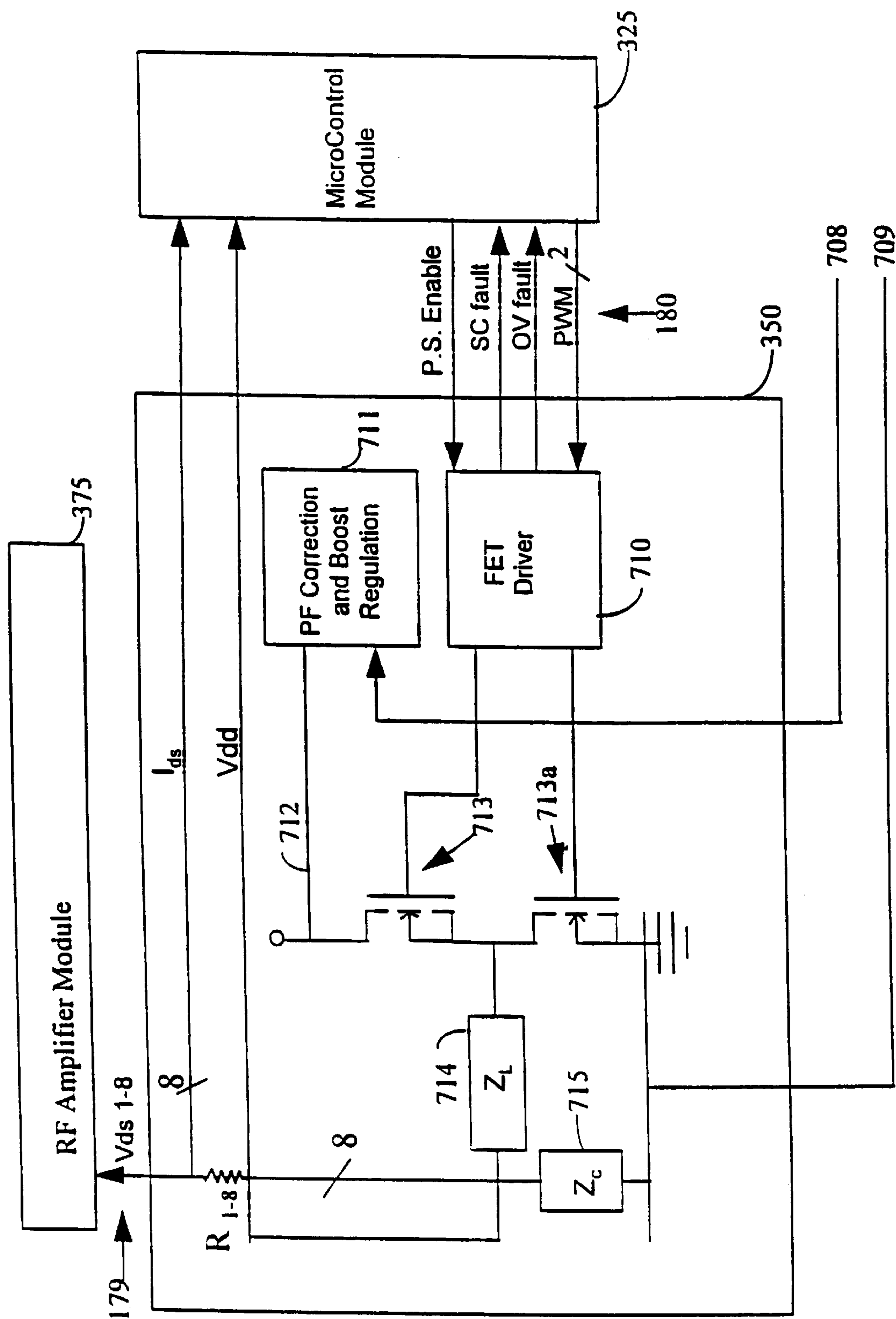


FIG. 24



**FIG. 25**



**FIG. 27**

400

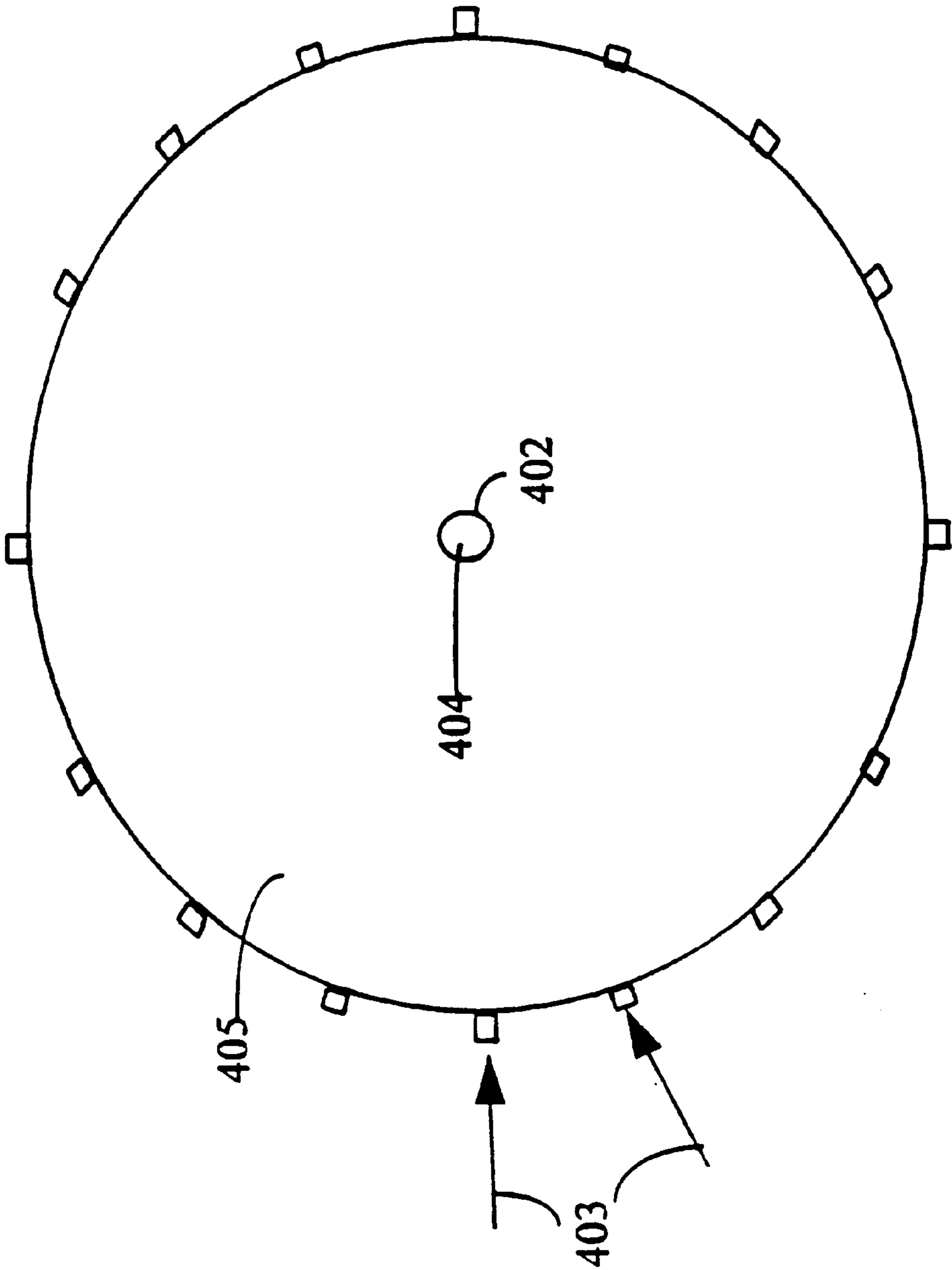


FIG. 28

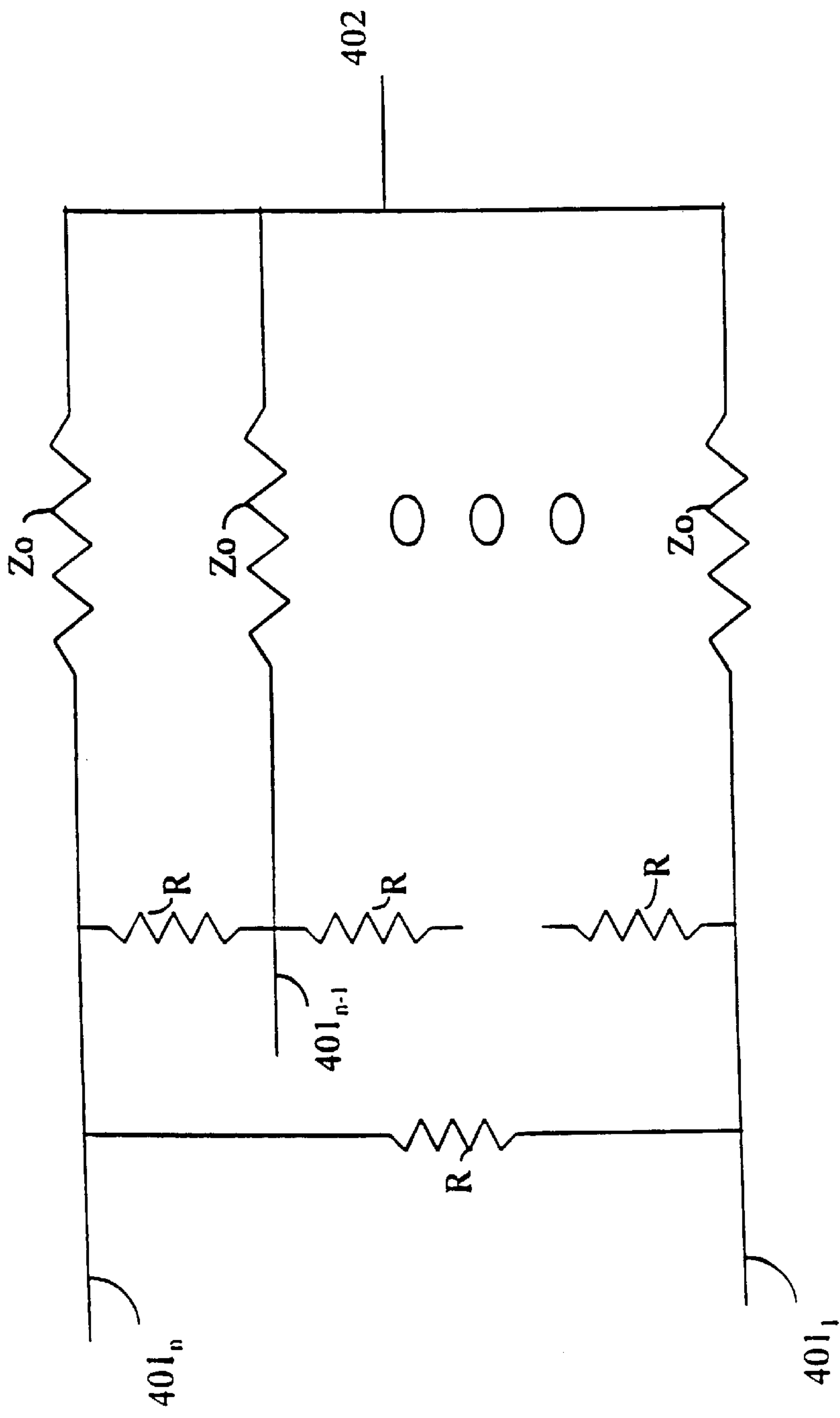
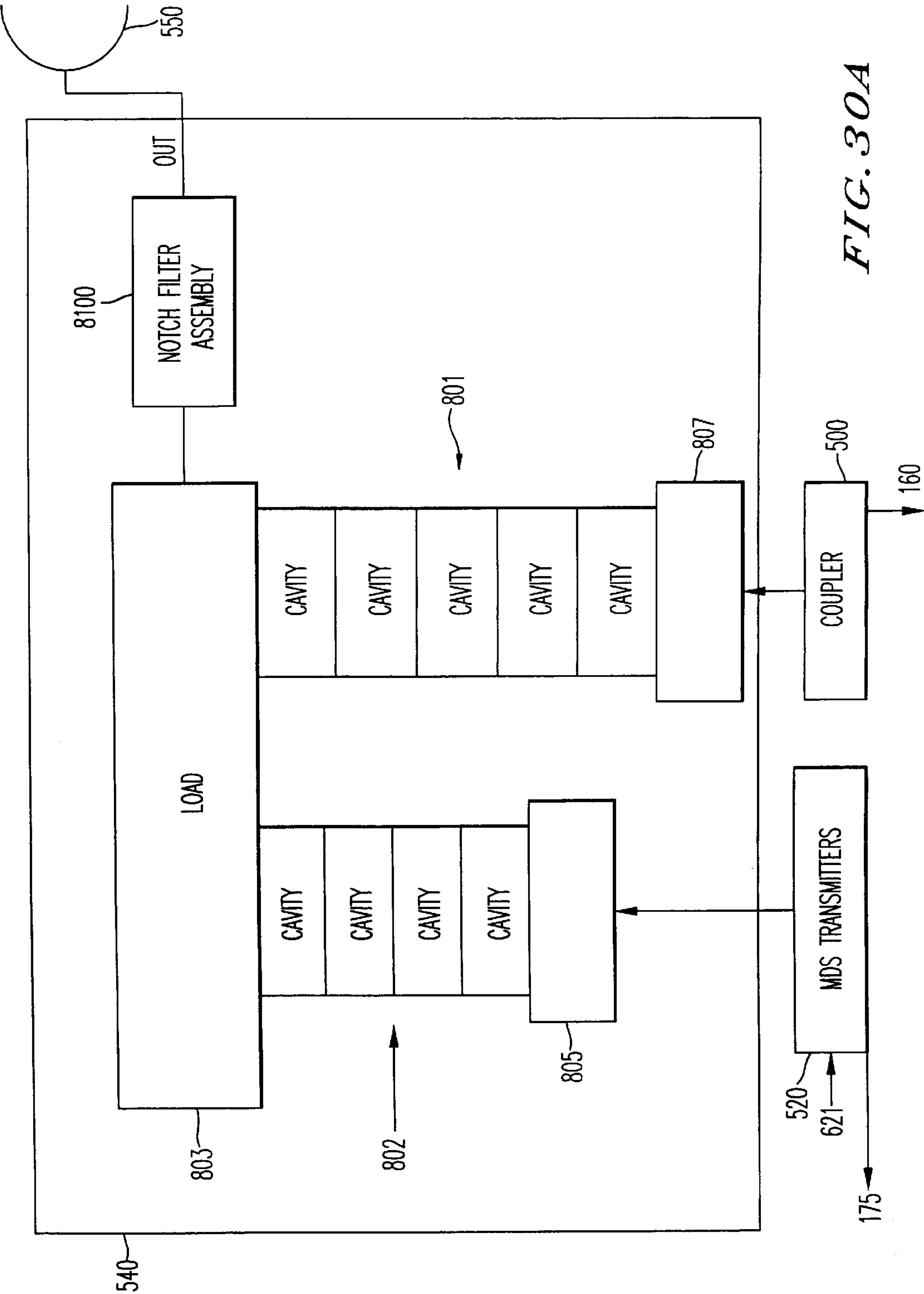


FIG. 29





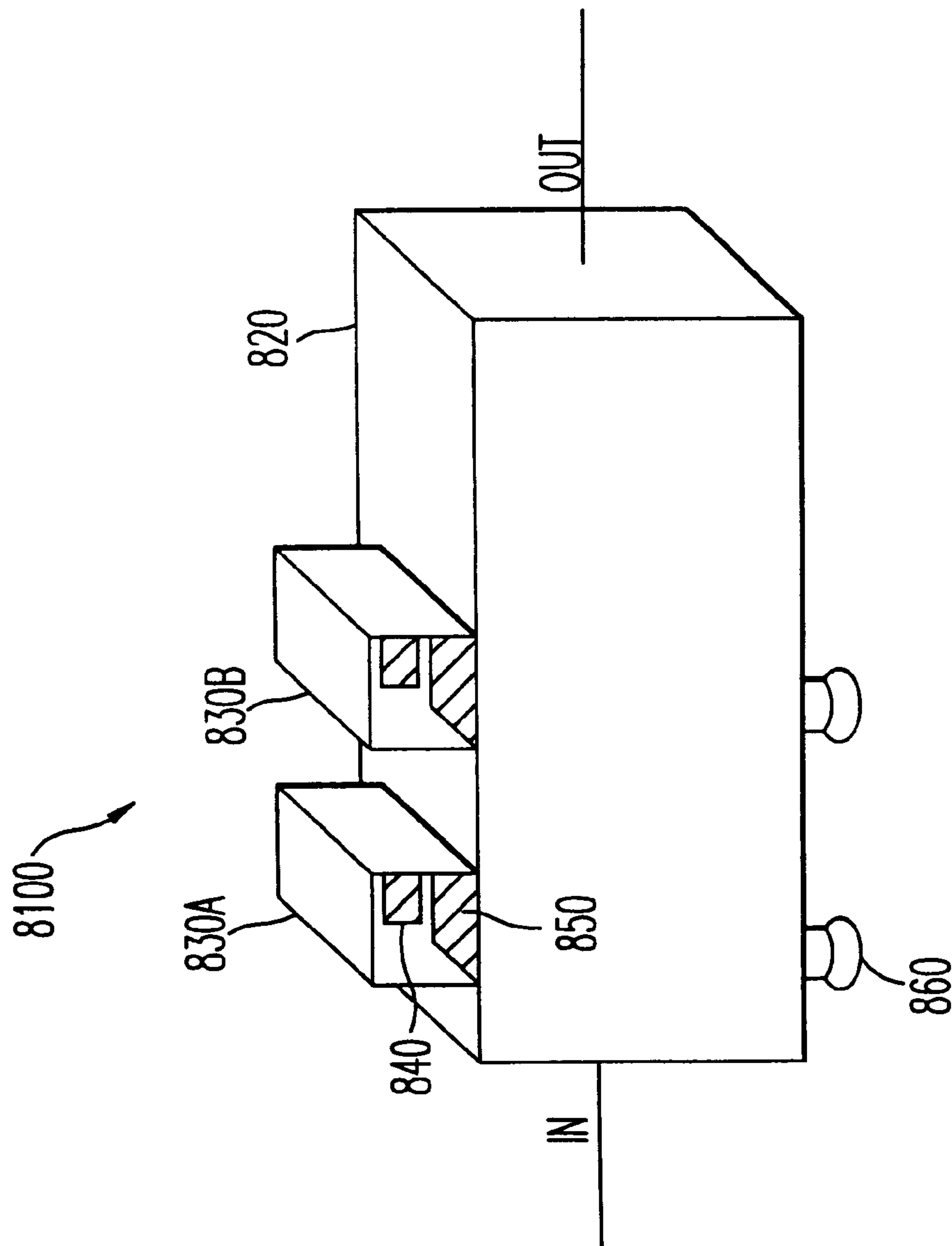


FIG. 30B

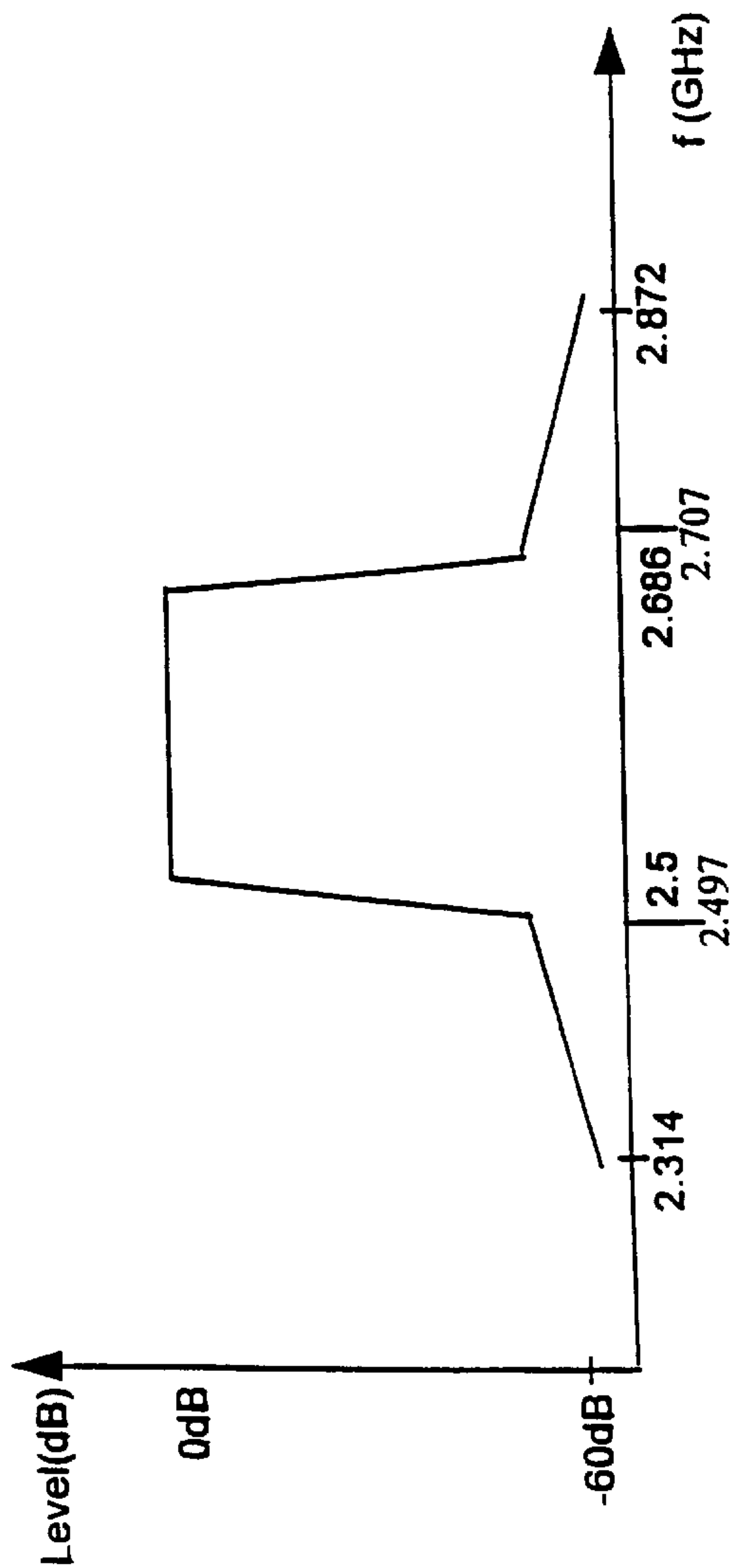


FIG. 31

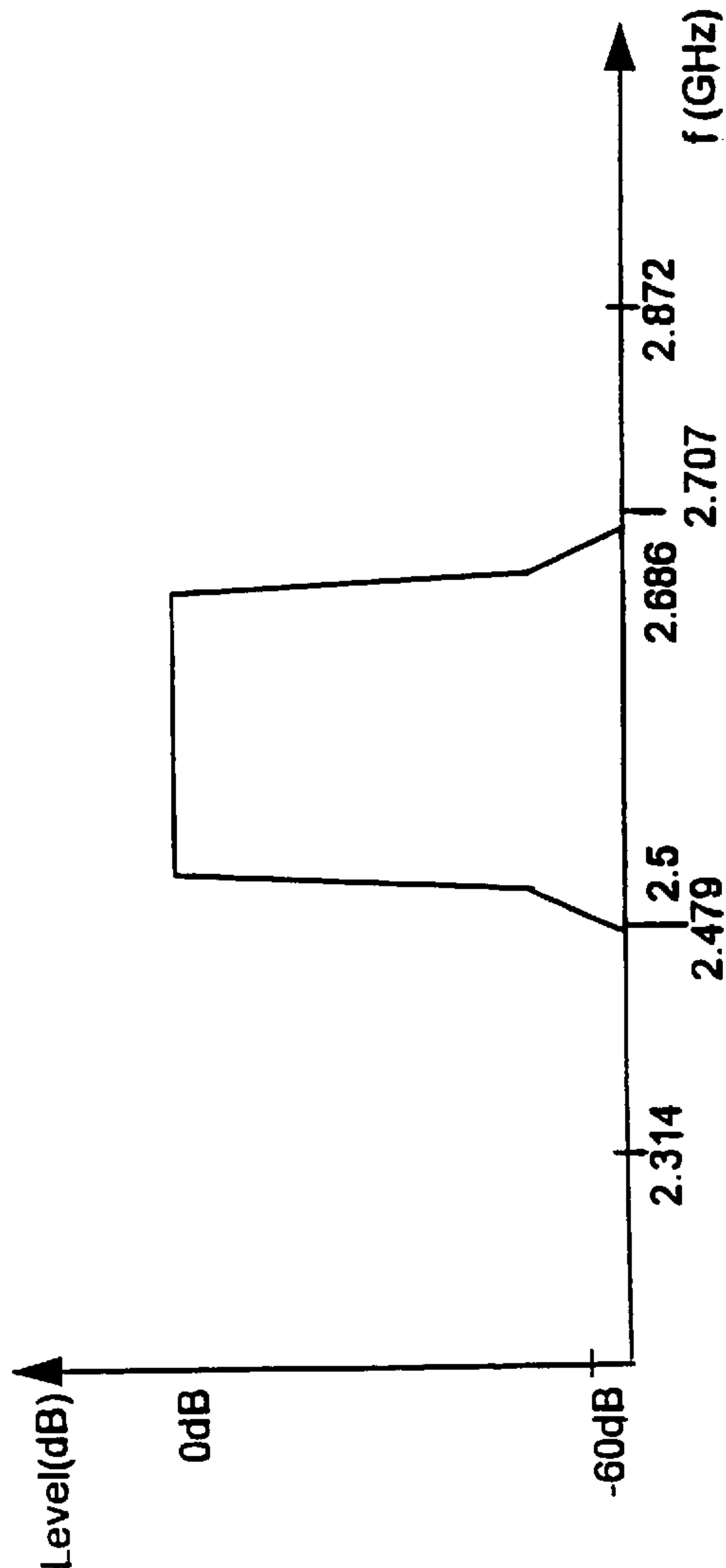


FIG. 32

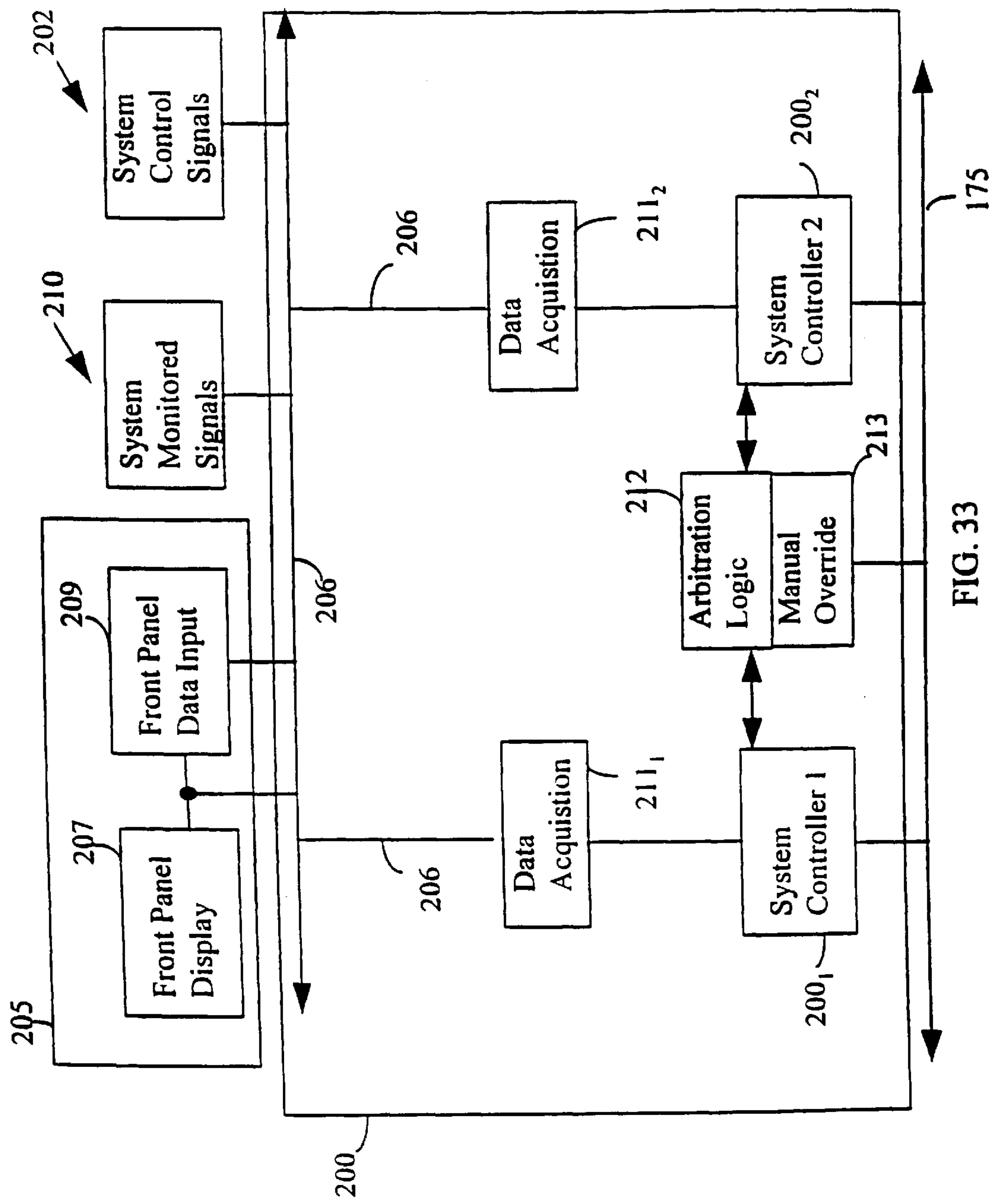


FIG. 33

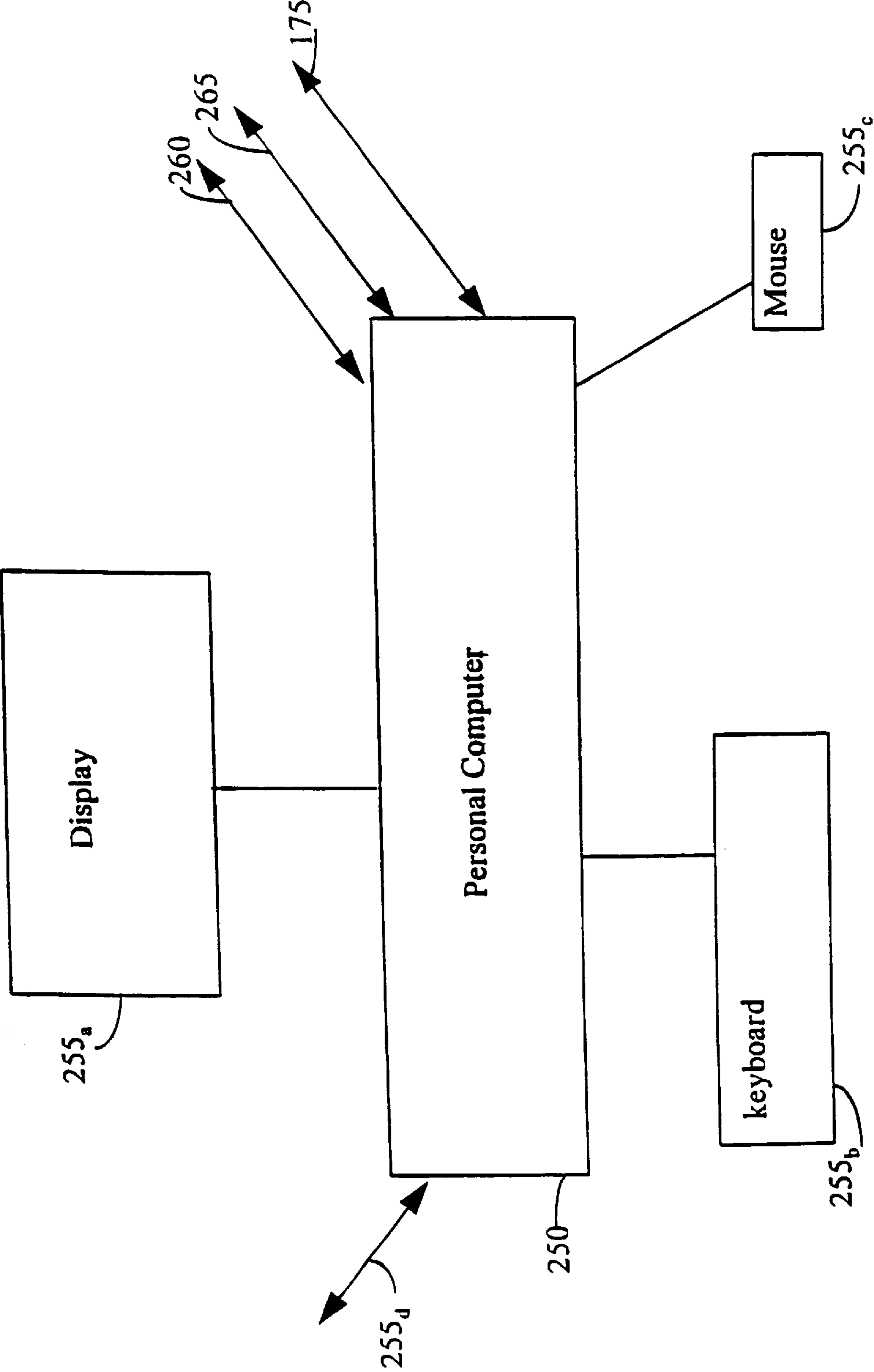


FIG. 34

266

TRAP No.	Object Class	Attribute 1=	Attribute 2 =	EOM
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FIG. 35a

267

000028	Slice	Saddr = 7	RefPStatus = high	END
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FIG. 35b

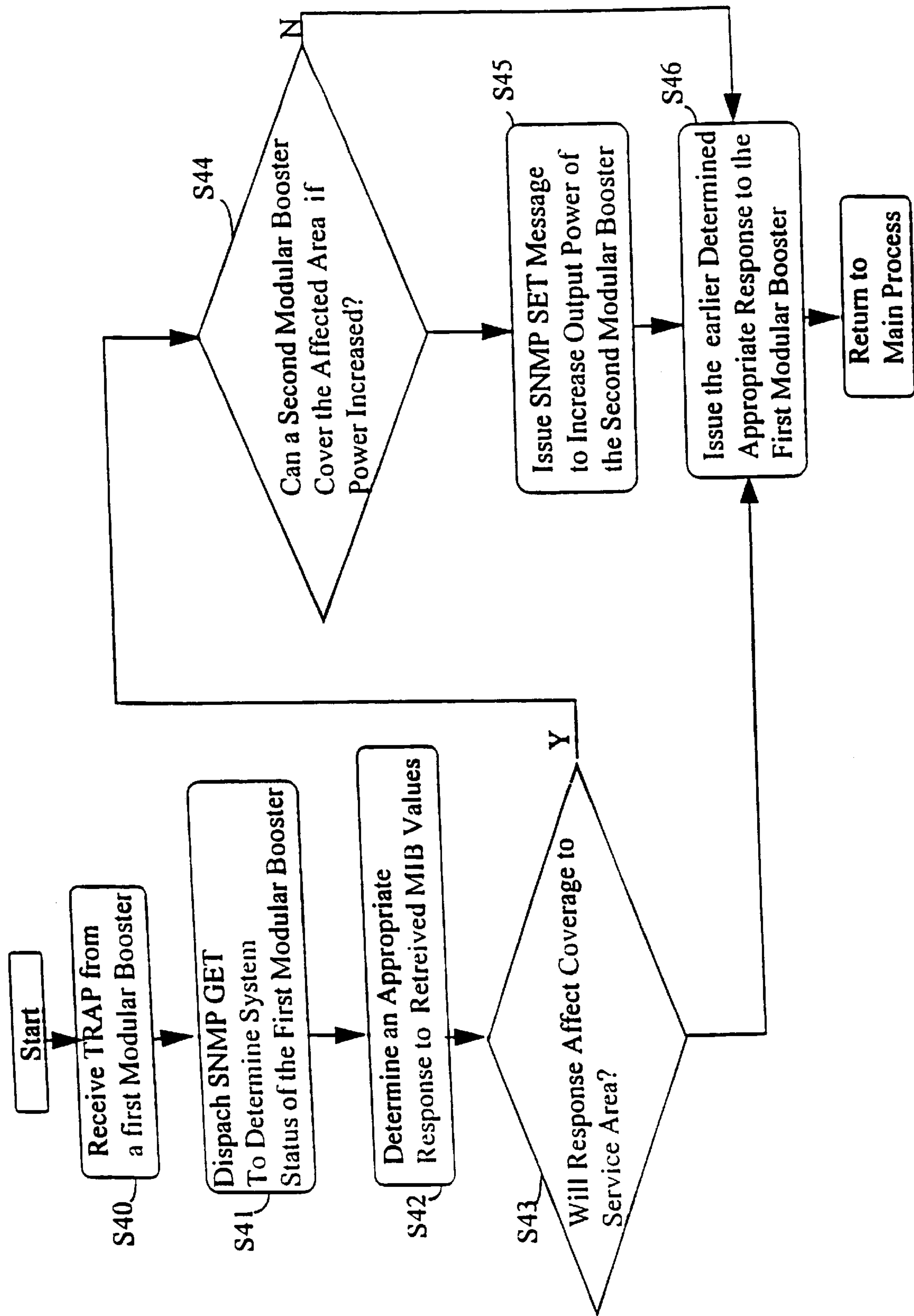


FIG. 36

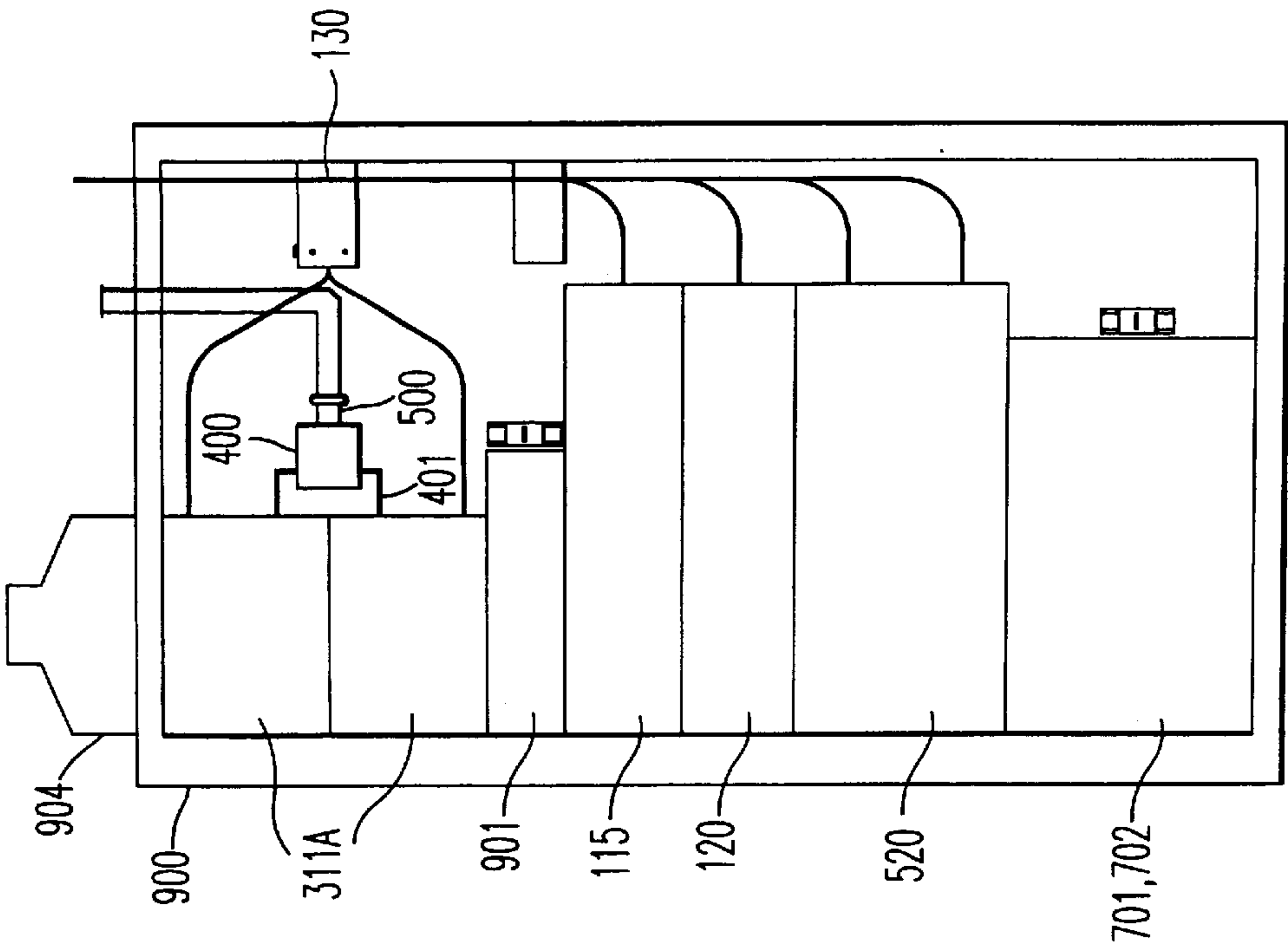


FIG. 37A

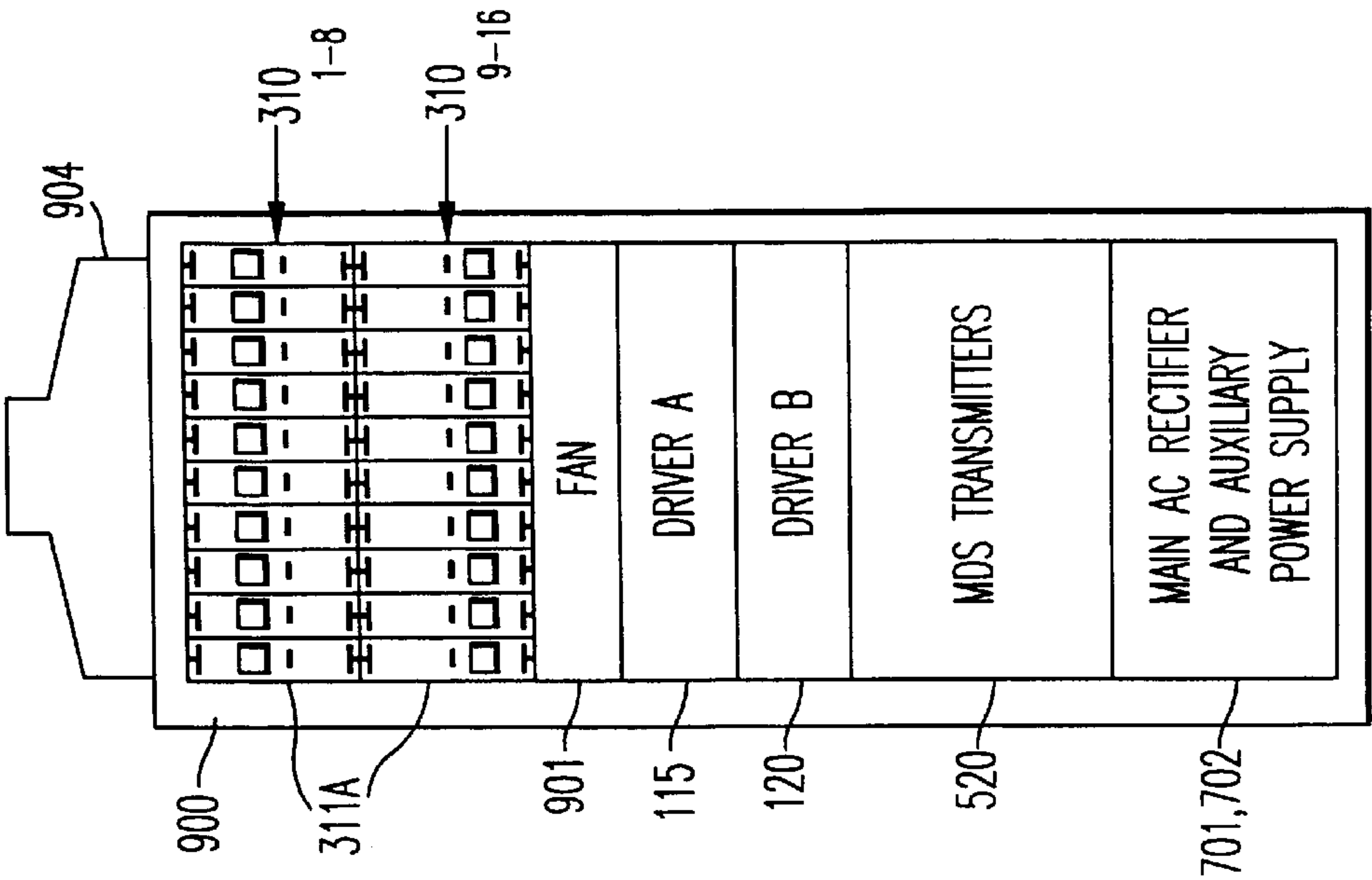


FIG. 37B

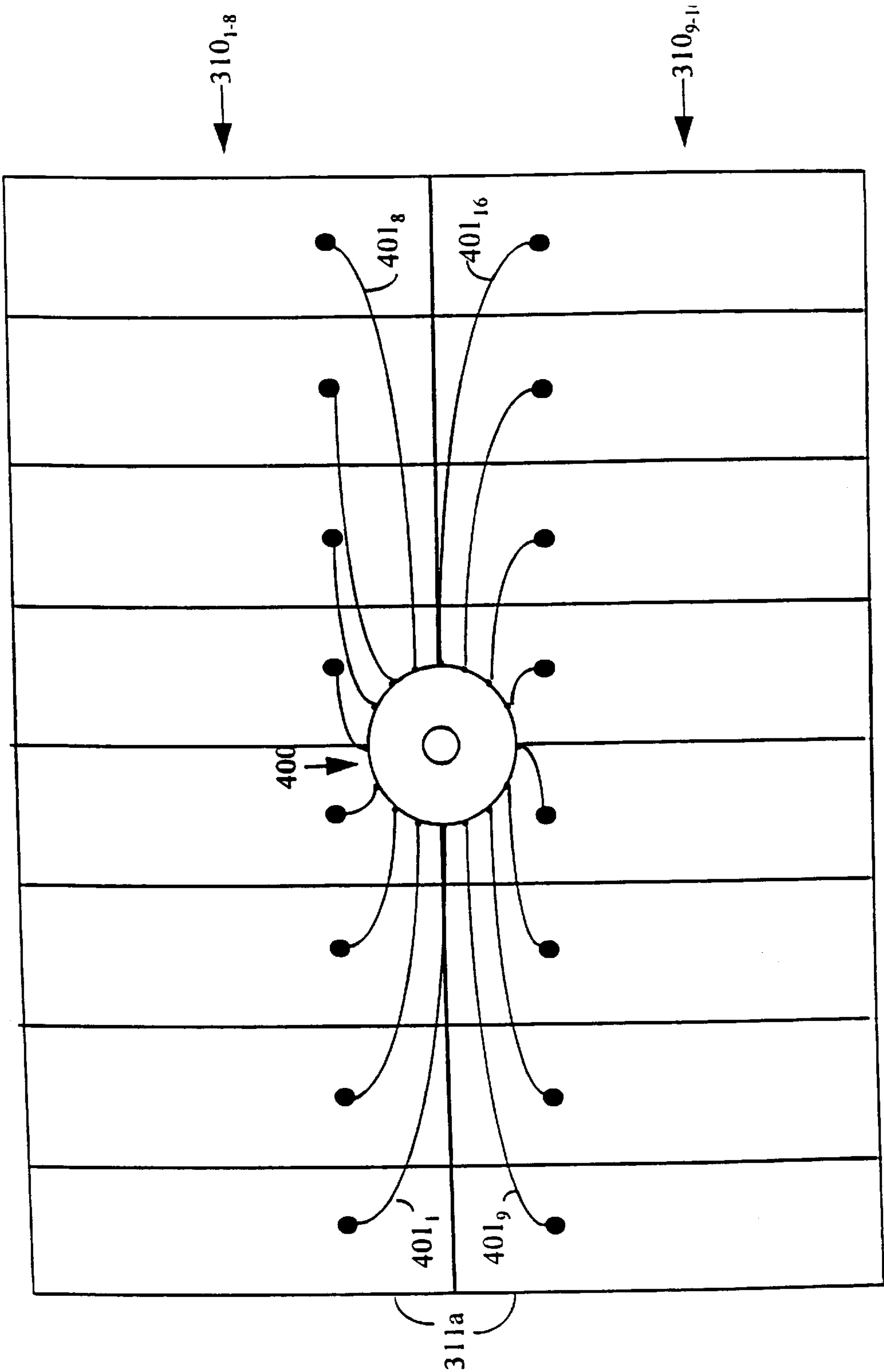


FIG. 37c



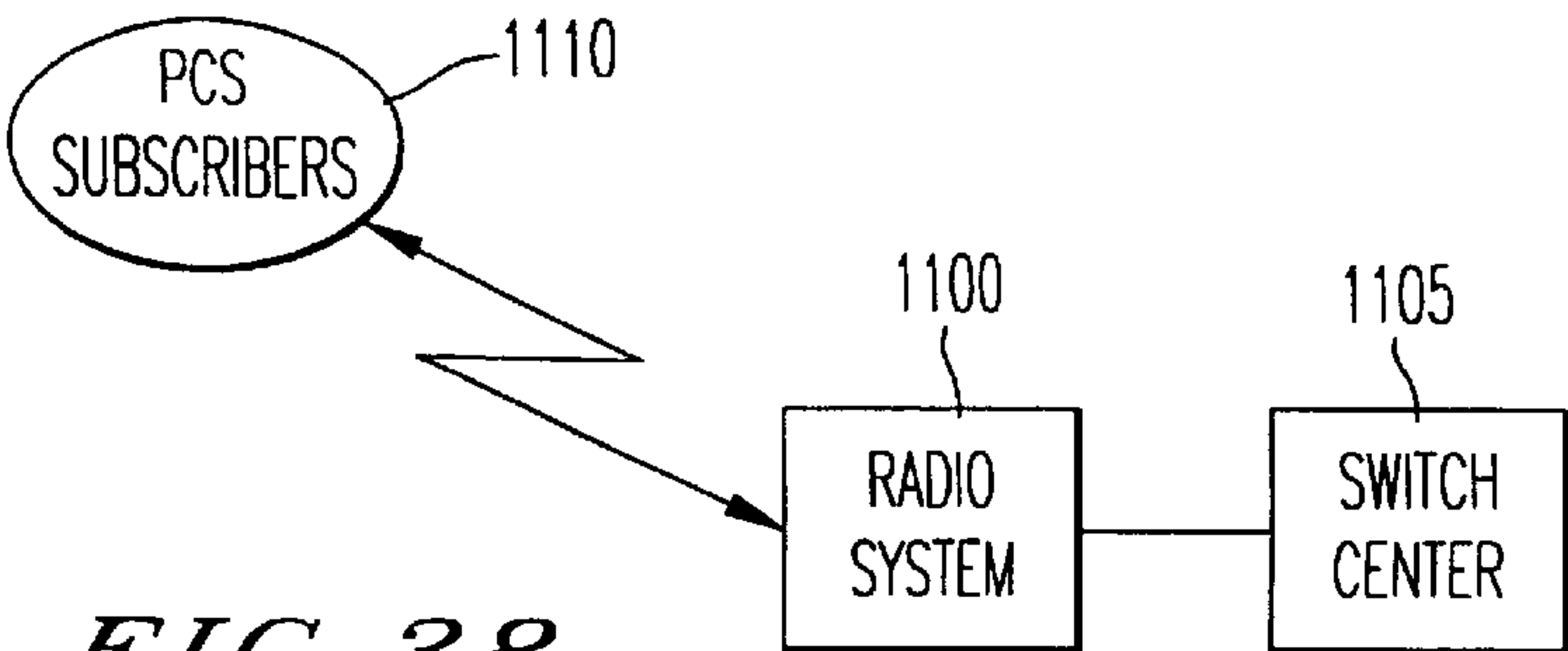


FIG. 38

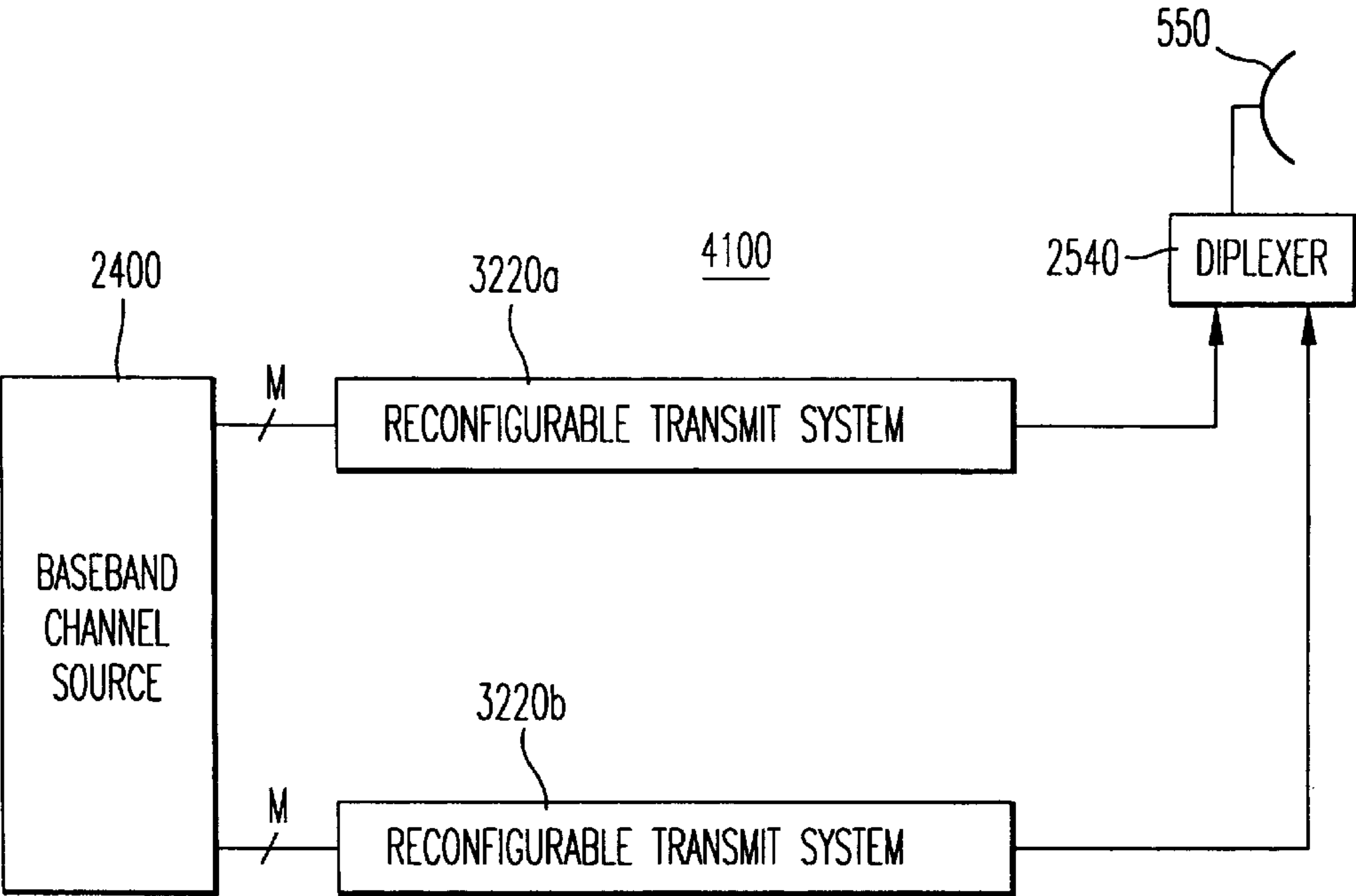


FIG. 42A

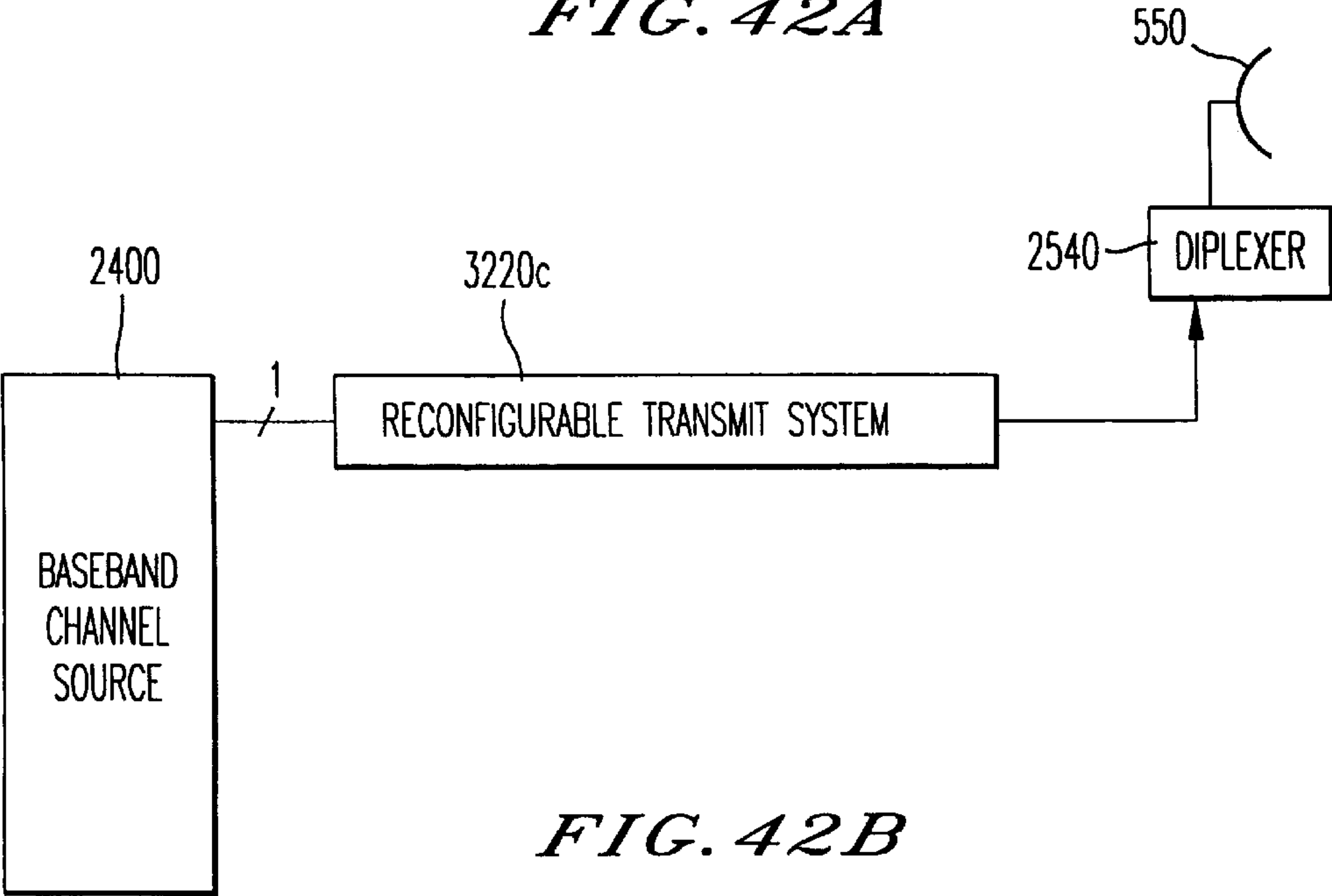
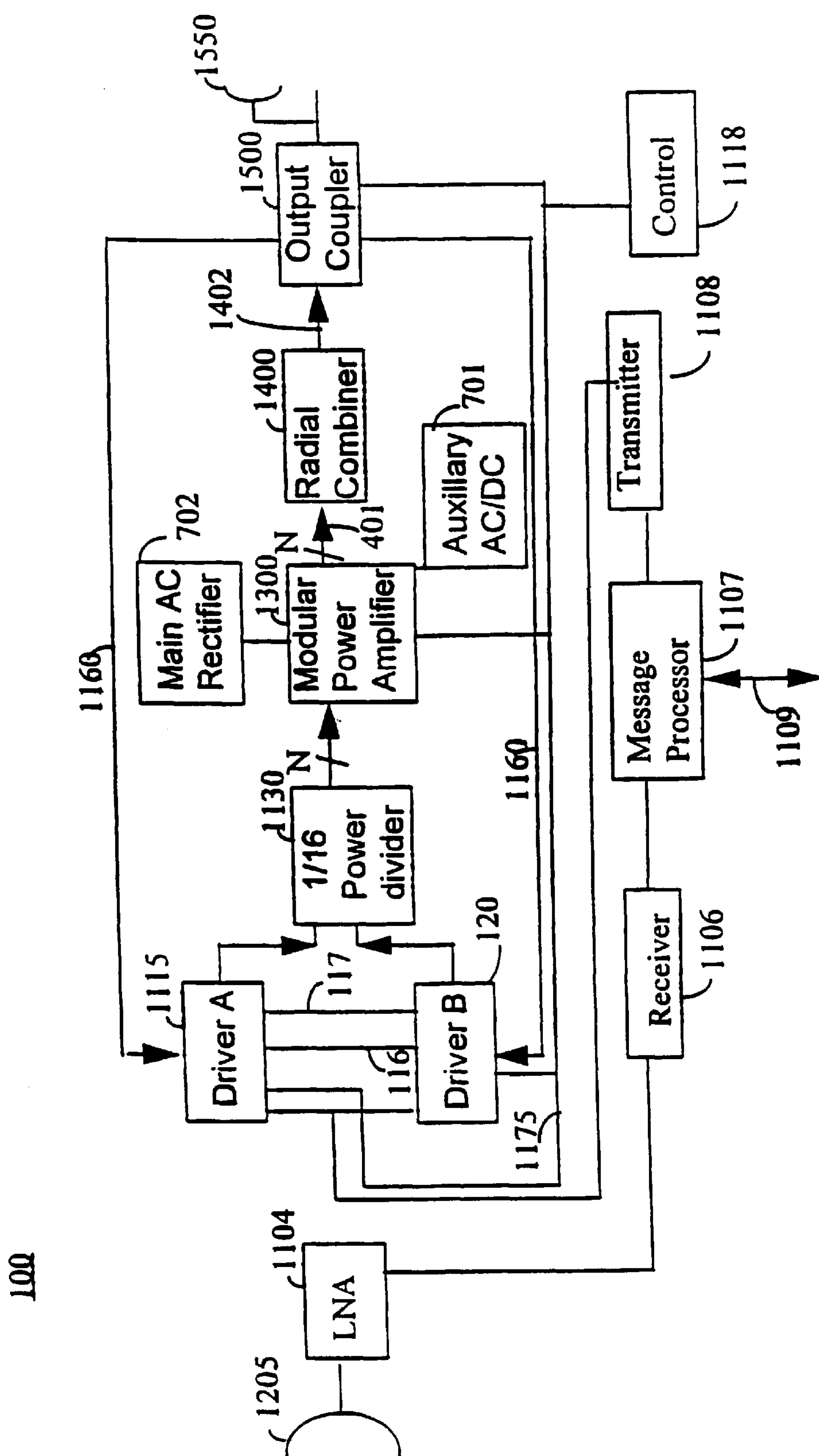


FIG. 42B



**FIG. 39**

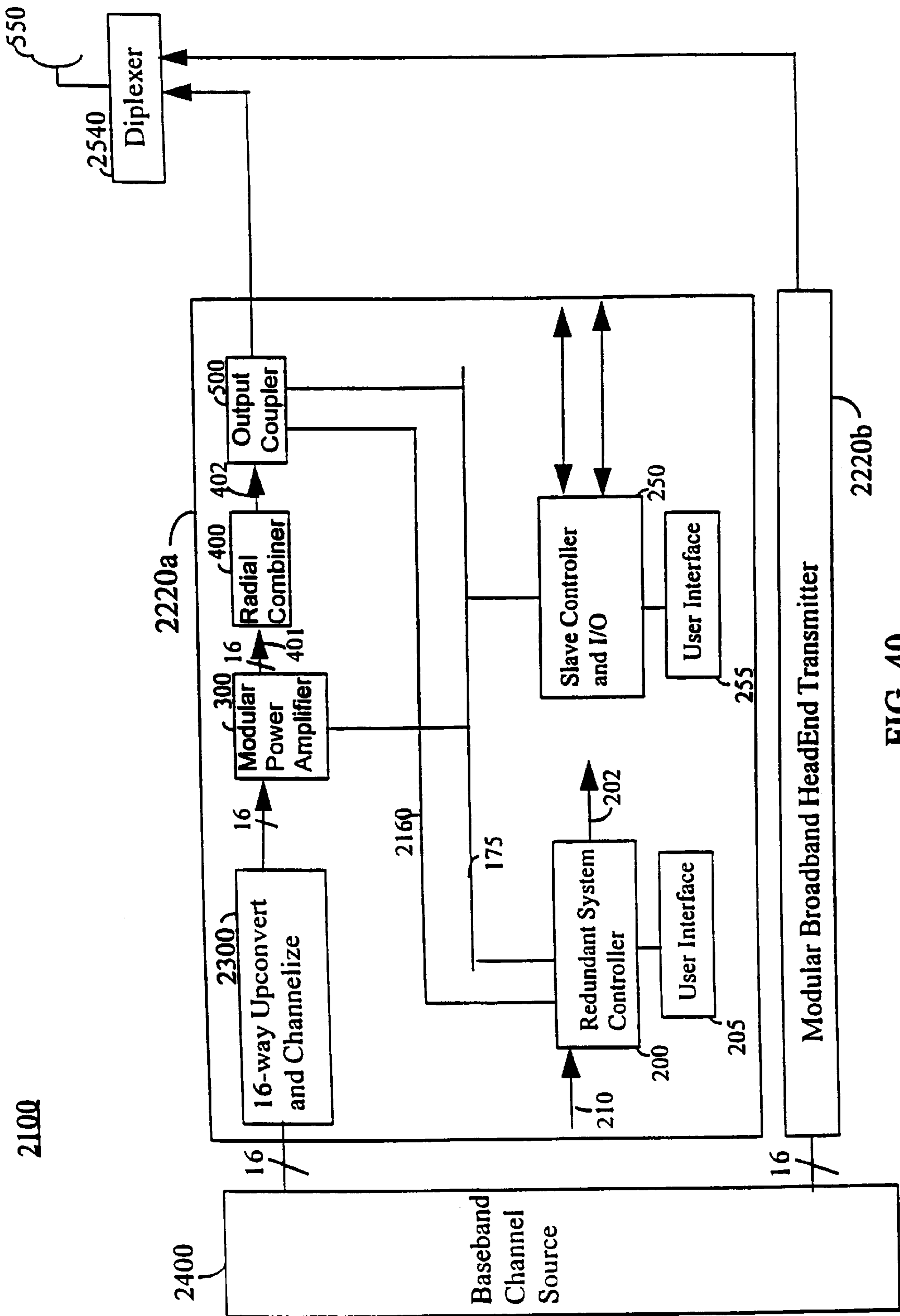
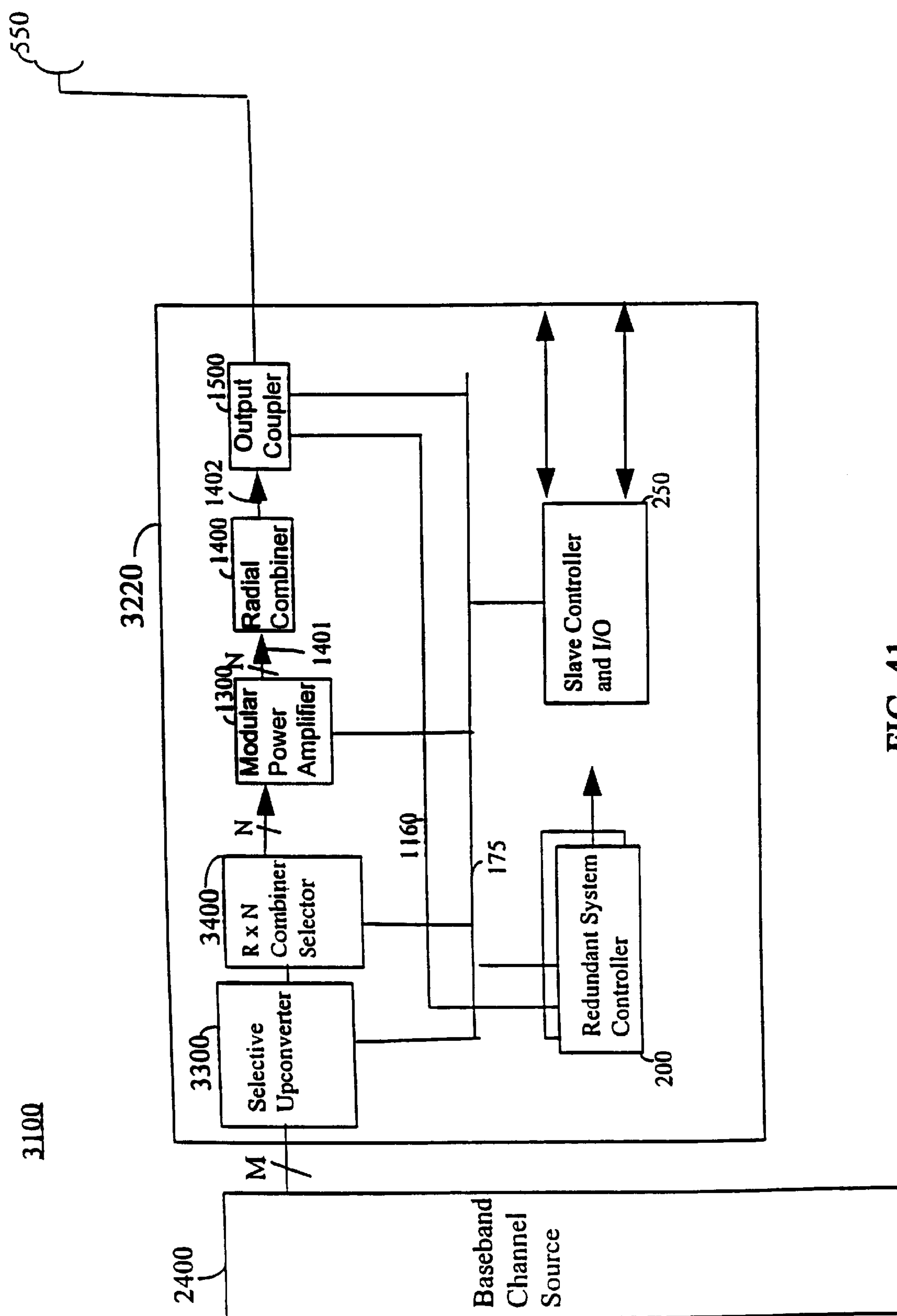
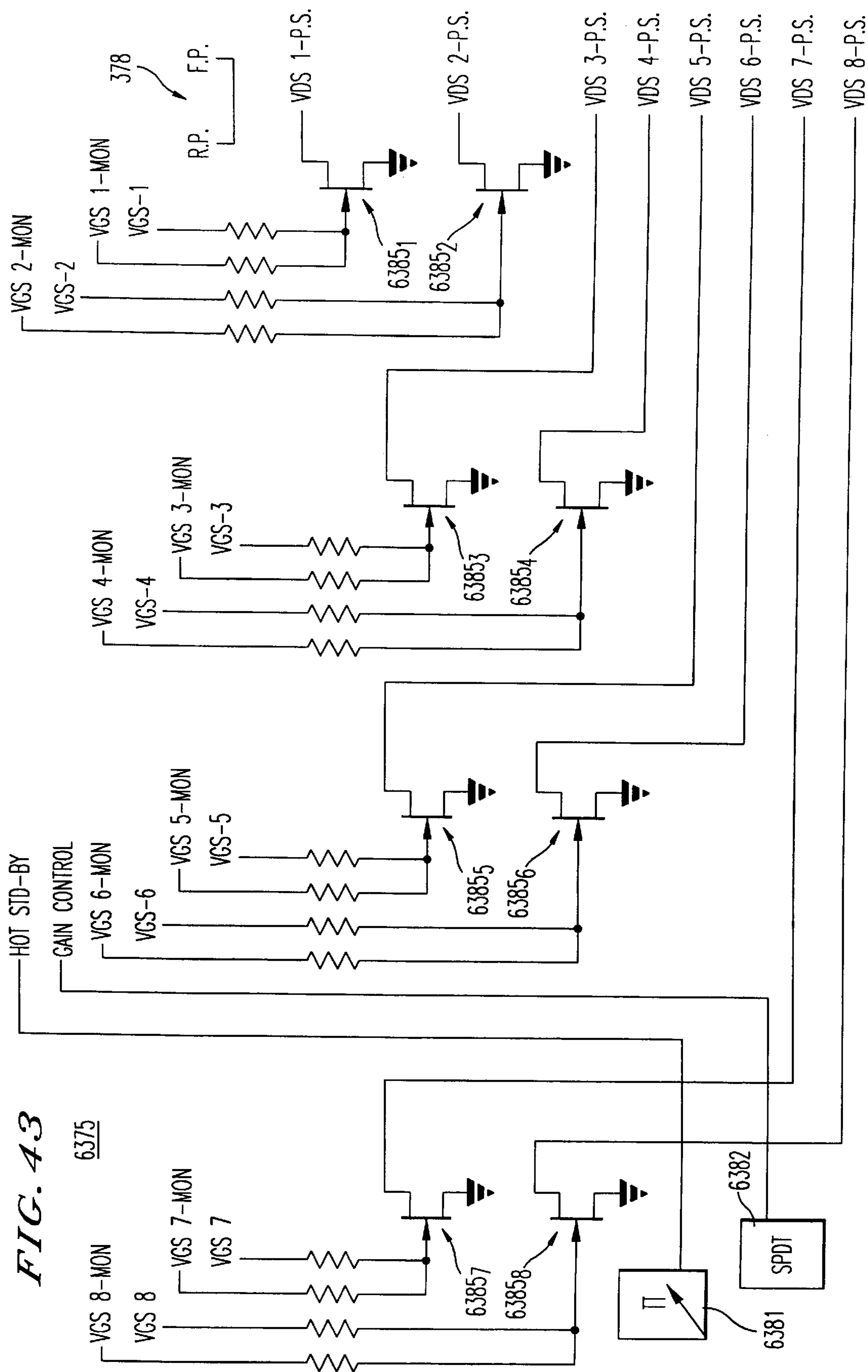


FIG. 40



**FIG. 41**



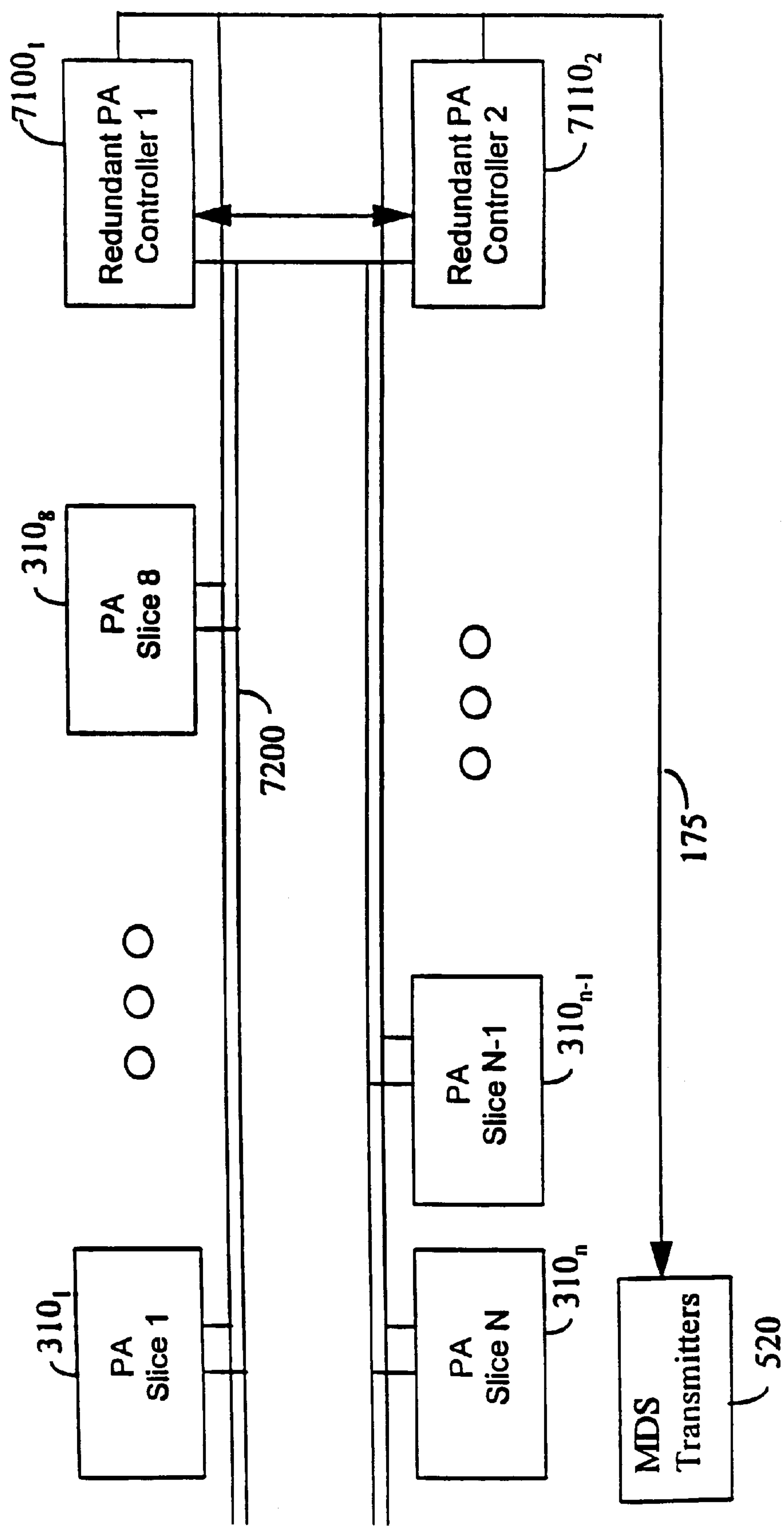


FIG. 44



## CONTROLLER-BASED RADIO FREQUENCY AMPLIFIER MODULE AND METHOD

### CROSS-REFERENCE TO RELATED APPLICATION

This application claims the benefit of U.S. Provisional Application No. 60/021,271, filed Jul. 5, 1996. This application is a continuation of 08/887,940 Jul. 3, 1997, now U.S. Pat. No. 6,078,222.

### BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

The present system and method pertains to communication systems and methods of the types used in communication networks and distribution services. More particularly the present invention relates to radio frequency (RF) transmission systems having modular architectures that accept an input signal(s), amplifies the signal(s) using modular components, and transmits the amplified signal(s) via radio waves to at least one receiver.

#### 2. Discussion of the Background

By their very nature wireless technologies do not require the same investment in infrastructure that originally motivated the United States (U.S.) to permit local telephone companies and cable operators to create "wired" service monopolies. However, in order to compete with "wired" technologies, wireless technologies have a number of unique obstacles that must be overcome. These obstacles include distributing radio waves to areas located in valleys, blocked by mountains, buildings, etc. as well as maintaining a network of high powered transmitters used to reliably broadcast the radio waves to service areas.

Multi-channel multi-point distribution service (MMDS) is generally referred to as "wireless cable," and is one of the wireless service industries that faces the inherent obstacles associated with wireless technologies. Although this document refers to MMDS and wireless cable synonymously, the following other channels of wireless cable when appropriate will be described individually: multi-point distribution service (MDS); Instructional Television Fixed Service (ITFS); and private operational fixed service (OFS).

One of the obstacles facing MMDS service providers is "blocking". In order to further illustrate blocking, FIG. 1 shows a conventional MMDS system where blocking is not a problem. A main transmitter 1 is capable of directly transmitting an analog signal to a receiver 2 without any intervening structures blocking the transmitted signal. When blocking does not occur, the receiver 2 couples the transmitted signal through an antenna 3 and to a home-unit 4. Once in the home-unit, a receiver 5 receives the signal and passes it to a set top 6 which descrambles and tunes the signal. A television 7 then displays a video image that was carried by the signal.

FIG. 2 illustrates a scenario where blocking is a problem. A MMDS signal 8 is blocked by an obstruction (e.g., a hill) 9 so that the receiver 2 cannot receive the MMDS signal. It is estimated that blocking reduces a service area of an MMDS service provider from a theoretical value of 100% to 40%.

FIG. 3 illustrates a conventional approach developed by the MMDS industry to counter the effects of blocking and improve the service area. A booster 10 is strategically placed such that it can receive the MMDS signal from the main transmitter 1 and rebroadcast the MMDS signal to the receiver 2. Thus, the booster 10 can improve service area

coverage because the booster 10 can cover areas that are outside of a line-of-sight of the main transmitter 1.

There are generally two types of MMDS boosters 10 used to improve service area coverage. A first type of MMDS booster is a single channel booster which receives 1 of 33 different MMDS channels (actually carriers which are capable of holding multiple audio/video programs) broadcast from the main transmitter 1, and amplifies and transmits that selected single channel to a receiver 2. Because the single channel boosters only process one channel, they do not provide service for the remaining 32 channels. A second type of MMDS booster is a broadband booster, which amplifies all of the channels (typically 33) transmitted from the main transmitter 1 and rebroadcasts the channels to the receiver 2. The broadband boosters require power amplifiers having greater power than those of the single channel boosters because the broadband boosters must amplify up to 33 MMDS channels while single channel boosters amplify only one channel.

As a practical matter, boosters 10 (single channel and broadband boosters) are expensive because they contain a single-unit power amplifier as well as supporting electronics. The expense of the boosters 10 is further escalated by the operational need to have two power amplifiers, or more often, a back-up booster system 10 in order to improve booster reliability. When only redundant power amplifiers are used, one amplifier serves as the operational amplifier and the other is used as a spare. However, aside from the high expense, the use of two single-unit amplifiers is not optimum because if one of the amplifiers fails, service to the service area will cease until the back-up amplifier can be brought on-line. Similarly, when two booster systems 10 are used to improve reliability, the back-up booster system 10 will not begin to broadcast until the operational booster system 10 fails. A gap in service to the service area will exist during the period when the operational booster system 10 fails and the back-up booster system 10 is brought on-line.

Co-channel interference is a second obstacle facing the MMDS industry and limits the effectiveness of current MMDS boosters. Co-channel interference occurs when a stray signal (say from a neighboring one of the boosters 10) interferes with an intended signal by acting as a coherent noise source. Co-channel interference has been particularly problematic with analog MMDS signals, preventing the boosters 10 from being placed close to one another for fear their respective signals would cause co-channel interference. However, with digital MMDS signals, digital signal processing techniques have been developed that effectively combat co-channel interference so more boosters 10 may be used to cover greater percentages of the MMDS service area.

Even though more of the MMDS boosters 10 may be used in a given service area, the single-unit amplifier architecture of the MMDS boosters 10 (single channel and broadband boosters) is problematic in that when the single unit amplifier fails, service from that MMDS booster 10 is interrupted until a spare amplifier can be brought on-line. Similarly, when a back-up booster 10 is used, service is interrupted until the back-up booster 10 is brought on line. Thus, the MMDS boosters 10 do not degrade gracefully, but rather, fail with little notice, making the MMDS boosters 10 difficult to maintain. When individual ones of the boosters 10 fail, other neighboring boosters are not equipped to increase their transmission powers in order to compensate for the failed booster 10. While some MMDS boosters 10 are equipped to communicate with a network manager, the communication is generally "reactive", in that the failed booster 10 reports its failure, but is incapable of reconfiguring itself in order to restore service.



FIG. 4 illustrates an exemplary conventional broadband MMDS booster 10 which may or may not be supported by a back-up booster 10 (not shown). MMDS signals received through a receive antenna 11 are passed through a low noise amplifier 12, where they are amplified. From the LNA 12, the RF signals are passed through a power amplifier assembly 13, which includes a single-unit amplifier, where the RF signals are amplified and passed to a conventional antenna coupler 17. The antenna coupler 17 couples the output signal from the PA assembly 13 and passes the signal to the transmit antenna 18. The amplifier unit 14 is typically powered by a system power supply 15 that distributes low voltage direct current (DC) voltage to all of the components of the booster 10. A control head 16, which is placed in a separate housing than either the power supply 15, the PA assembly 13, or a coupler 17, provides system control functions such as turning on and off the PA assembly.

The amplifier unit 14 is a single-unit amplifier and is not simultaneously operated with one or more of the power-amplifiers for several reasons. First, conventional combining networks for combining output powers from multiple power amplifiers may become damaged when one of the amplifier units 14 fails and in any event would result in several dB of lost output power when one amplifier fails. Second, combining losses are appreciable, and it is less expensive to increase broadcast power by using a larger single-unit amplifier. Third, MMDS booster operators would have to take the second amplifier off-line before removing the failed amplifier unit 14 because conventional MMDS amplifiers are not "hot-swappable". Fourth, maintaining constant output power from each of the single-unit amplifier assemblies 14 would be necessary in order to avoid significant combining and matching problems in a combiner, but conventional single-unit amplifiers are not well suited to provide constant, matched output power.

Because of all the economic, reliability, and performance limitations on the conventional booster 10, the conventional boosters serve a more limited role in MMDS networks than desired by MMDS service operators. Furthermore, due to their specialized architectures, conventional boosters 10 are not used in other applications such as a main MMDS transmitter (single channel or multi-channel), a Personal Communications Services (PCS) base station, or a general purpose reconfigurable transmitter.

#### SUMMARY OF THE INVENTION

Accordingly, one object of this invention is to provide a novel power amplifier module and method that overcomes the above-mentioned problems.

It is another object of the invention to provide a power amplifier module for amplifying an input signal applied thereto and providing an amplified output signal to a N-way radial combiner that combines the amplified output signal with other amplified output signals from other power amplifier modules, where the power amplifier module includes a processor submodule configured to control a level of the amplified output signal.

It is another object of the invention to provide a power amplifier module that includes a controller configured to monitor and adjust specific input, output, and control voltages of discrete amplifiers contained in the amplifier module.

It is another object of the invention to provide an amplifier module that is controllably configured to operate in one of a cold standby mode of operation, a transmission mode of operation, a hot-standby mode of operation, a transmit mode of operation and a failed mode of operation.

It is yet a further object of the invention to suppress electromagnetic interference within the power amplifier module.

It is still a further object of the invention to be connected to, and removed from, a system in which other power amplifier modules are presently operating so as to provide a hot-swapping capability.

Another object of the invention is to provide a power amplifier module that may be used with other power amplifier modules in a modular system where the respective power amplifier modules communicate data and status information to a system controller.

Yet another object of the invention is to provide a method for controlling discrete amplifiers in a power amplifier module by monitoring and adjusting specific voltages in the power amplifier module.

These and other objects are accomplished by a novel modular transmission system, that has multiple power amplifier modules, that receives an input signal which may be a single carrier or multiple carriers. The signal is passed to a one-by-N divider which divides the signal N ways. Each of the N divided signals are independently amplified by the separate power amplifier (PA) modules or "slices" (i.e., PA modules) that includes an RF amplifier module, a microcontroller module, and a power supply module, all of which are tightly coupled via a plurality of signal, power, control, and status connections. Each the PA slices amplifies its respective input signal and outputs a respective radio frequency output signal at a predetermined power level as controlled by the microcontroller module, the driver, and a redundant system controller, or a network manager via a system input/output interface. The N amplified output signals are passed via semirigid lines to a N-way radial combiner which combines the energy from the N PA slices such that the entire broadband amplifier system does not shut down if an individual PA slice fails. Furthermore, output power drops by only a few tenths of a dB when a single PA module fails, as opposed to at least several dB in conventional transmitters.

#### BRIEF DESCRIPTION OF THE DRAWINGS

A more complete appreciation of the invention and many of the attendant advantages thereof will be readily obtained as the same becomes better understood by reference to the following detailed description when considered in connection with the accompanying drawings, wherein:

FIG. 1 is a block diagram of a conventional wireless cable system;

FIG. 2 is an example wireless cable scenario with blockage due to a hill;

FIG. 3 is an example wireless cable system with blockage due to a hill and a booster to overcome the blockage problem;

FIG. 4 is a block diagram of a conventional broadband MMDS booster;

FIG. 5A is a block diagram of a modular broadband booster system of a first embodiment of the present invention;

FIG. 5B is a flowchart of a control process performed by a redundant system controller according to the first embodiment;

FIG. 5C is an illustrative diagram of a data structure of a transmission frame used to hold and convey message information within the modular broadband booster system;

FIG. 6 is a segmented table of channels used in wireless cable;



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FIG. 7 is a block diagram of a redundant low noise amplifier;

FIG. 8 is a block diagram of a driver circuit;

FIG. 9A is a state diagram illustrating transfer of master and slave control between two driver circuits;

FIG. 9B is a flowchart of a system level automatic level control process that controls an amount of RF output power based on a number of operational power amplifier modules;

FIG. 10 is a detailed block diagram of a power divider, modular power amplifier, radial combiner, and output coupler of the first embodiment;

FIG. 11 is a perspective view of a PA slice interfacing to a backplane;

FIG. 12 is an exploded diagram of a PA slice;

FIG. 13 is a perspective view of several PA slices in a chassis;

FIG. 14 is a block diagram of a PA slice;

FIG. 15 is a block diagram showing an interconnection harness between a microcontroller module and a power supply module on a PA slice;

FIG. 16 is a block diagram illustrating a wiring control harness between a microcontroller module and an RF amplifier module, and a control harness between the RF amplifier module and a power supply module;

FIG. 17 is a block diagram of signal and control lines in a power amplifier module;

FIG. 18 is a block diagram of a signal flow path in a power amplifier module;

FIG. 19 is a block diagram of a microcontroller module;

FIG. 20A is a state diagram implemented in computer software in respective controllers of individual power amplifier modules;

FIG. 20B is a flowchart of an automatic level control process performed at the module level on respective of the power amplifier modules;

FIG. 21 is a flowchart of a hot-swap process used to replace selected of the power amplifier modules while other the power amplifier modules remain in a transmitting state;

FIG. 22 is a block diagram of a pulse width modulation signal generating circuit;

FIG. 23 is an illustrative pulse width modulation signal diagram;

FIG. 24 is a flowchart of a process for monitoring and adjusting an output of a power supply module;

FIG. 25 is a block diagram illustrating a distributed power architecture;

FIG. 26 is a schematic diagram of a main alternating current/direct current converter circuit;

FIG. 27 is a block diagram of a power supply module interfacing with a microcontroller module and a RF amplifier module on a PA slice;

FIG. 28 is a schematic diagram of a radial combiner;

FIG. 29 is a schematic diagram of an equivalent circuit for a radial combiner;

FIG. 30a is a block diagram of a diplexer;

FIG. 30b is a perspective view of a waveguide and notch filter assembly of the diplexer;

FIG. 31 is a spectral occupancy graph of an output signal not passed through a diplexer;

FIG. 32 is a spectral occupancy graph of an output signal passed through a diplexer;

FIG. 33 is a block diagram of a redundant system controller;

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FIG. 34 is a perspective view of a slave controller and system input/output interface;

FIG. 35a is a data structure diagram of a generic TRAP message;

FIG. 35b is a data structure of an example TRAP message;

FIG. 36 is a flowchart illustrating a process for reconfiguring selected ones of modular boosters used in a network of modular boosters;

FIG. 37a is front view of a rack for holding components of a modular transmission system;

FIG. 37b is a side view of a rack holding components of a modular transmission system;

FIG. 37c is a back view of sixteen rack-mounted PA slices and a radial combiner;

FIG. 38 is a block diagram of a modular transmitter system used as a personal communication system base station in a second embodiment of the present invention;

FIG. 39 is a detailed block diagram of the radio system of the second embodiment;

FIG. 40 is a block diagram of a head-end transmitter system of a third embodiment of the present invention;

FIG. 41 is a block diagram of a head-end transmitter system of a fourth embodiment of the present invention;

FIG. 42A is a block diagram of a head-end transmitter system of a fifth embodiment of the present invention;

FIG. 42B is a block diagram of a single channel head-end transmitter system of the fifth embodiment;

FIG. 43 is a block diagram of signal monitoring and control lines for an RF power amplifier module of a sixth embodiment of the present invention; and

FIG. 44 is a block diagram of a differential bus and a redundant controller architecture of a seventh embodiment of the present invention.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring now to the drawings wherein like reference numerals designate identical or corresponding parts throughout the several views, and more particularly to FIG. 5A thereof, there is illustrated a modular transmit system 100 configured as a broadband booster. In reference to FIG. 5A, each of the components of the modular broadband booster system 100 will be described briefly and selected ones of the components will be described in more detail (where noted) in reference to other figures.

An input antenna 105 couples radio frequency (RF) energy in the MMDS frequency band (see FIG. 6 for a description of the various frequency bands used in MMDS, wireless cable) transmitted from a main MMDS transmitter 1 (FIG. 1). The antenna 105 is a two meter parabolic reflector antenna having a gain of 30 dBi (decibels relative to an isotropic radiator). This size antenna helps to spatially isolate the modular broadcast booster system 100 such that undesired energy from other transmitters, boosters, and reflections off objects arriving from directions other than a direction in which the main transmitter 1 is located are not picked-up. The input antenna 105 focuses the RF energy from the main transmitter 1 and provides the RF energy to a redundant low noise amplifier (LNA) 110.

The redundant LNA 110 (shown in more detail in FIG. 7) preselects and amplifies the input signal provided from the antenna 105. While redundant drivers are shown, in the interest of cost and time-to-market, a single driver may also be used. The output of LNA 110 is provided to a driver A 115



via a connection **111** and to a driver B **120** via a connection **112**. The output of the LNA **110** is provided to both of the drivers **115**, **120** so as to enhance system reliability.

The driver A **115** and the driver B **120** (which are described in more detail in reference to FIGS. 8–9) perform similar functions in that they provide variable attenuation, provide power to the redundant LNA **110**, and provide level control for the modular broadband booster system **100**. The drivers A and B **115**, **120** do not simultaneously process the signal provided by the redundant LNA **110**, but rather only one of the drivers **115**, **120** drives (i.e., provides an amplified signal to) the remainder of the modular broadband booster system **100**, while the other driver **120**, **115** drives a load impedance (i.e., is not used to process the signal). The drivers **115**, **120** are arranged in a master/slave architecture which they use to determine which of the drivers **115**, **120** will drive the modular broadband booster system **100** and which will drive the load.

Assuming the driver A **115** is active (master), the output of the driver A **115** is passed to a  $\frac{1}{16}$  power divider **130** (see FIG. 10). the power divider **130** divides the incoming signal in 16 ways by using a sixteen way splitter. However, more generally, the modular broadband booster system **100** may be configured to divide the input signal in N ways and subsequently process the divided signal in N corresponding signal paths. Nonetheless, in the illustrative embodiment, the signal from the driver A is divided by the power divider **130** in 16 ways, such that each of the 16 output signals of the  $\frac{1}{16}$  power divider **130** have a proportionate  $\frac{1}{16}$ th, not accounting for approximately 13 dB of insertion loss, of the input signal power. The  $\frac{1}{16}$  power divider **130** is a  $0^\circ$  hybrid splitter of a Wilkinson splitter structure.

A modular power amplifier **300** (described in more detail in reference to FIGS. 10–27) receives each of the 16 divided signals from the  $\frac{1}{16}$  power divider **130** and individually amplifies the divided signals on 16 separate signal paths. Each signal path normalizes a respective input signal to 20 dBm, amplifies the respective signal by 27 dB, and outputs one of 16 output signals at a level of 47 dBm. The input level and output levels, however, are adjustable by an automatic level control (ALC) process.

An N-way (16-way in the present embodiment) radial combiner **400** (described in more detail in reference to FIGS. 28, 29 and 37c) accepts the 16 amplified signals as fed by 16 respective semi-rigid lines **401** (also discussed in reference to FIG. 10) having a length of 25.4 cm and in the range of 21 cm to 30 cm, and spaced at increments of  $\frac{1}{2}$  of the wavelength of a center of the MMDS band, such that each of the respective lines are isolated from one another. The radial combiner **400** combines the 16 respective input signals and provides a single output **402** which is preferably a  $\frac{7}{8}$  inch rigid copper transmission line (i.e., a tube-like waveguide) via an EIA bullet connector. The radial combiner **400** provides a uniformly matched input impedance for each the respective 16 inputs. Accordingly, if an individual one of the 16 PA modules or (“PA slices **310**”) in the power amplifier **300** fails, the failed modules are removed and the radial combiner **400** remains stable and reflections from the active N-1 power amplifier modules does not damage either the radial combiner or the power amplifier **300**. Furthermore, when an individual power amplifier module fails, the total output power of the modular broadband booster drops only by 0.3 dB relative to the power when all 16 power amplifier modules PA slices are functioning.

The amplified signal output from the radial combiner **400** is input to an output coupler **500**, via single output **402**,

which couples the energy and prepares the amplified output energy for transmission from the modular broadband booster system **100** to the receiver **2** (FIG. 1). The output coupler **500** also samples (as discussed in reference to FIG. 10) the total energy (forward and reflected power) provided by the radial combiner **400** and respectively provides the sampled total energy to the driver **115**, **120** in the form of a DC voltage (e.g., 1.4 VDC) via a pair of sample lines **160**. The samples provided on the sample lines **160** provide information about whether there is mismatch between the output coupler **500** and the radial combiner **400**, and also whether the drivers **115**, **120** should adjust their output powers as part of the ALC process so as to control the output power level for the broadband booster system **100**.

The output coupler **500** forwards the coupled signal to a diplexer **540** (also discussed in reference to FIGS. 30–32) which combines a first signal from an MDS transmitter **520**, which provides two 6 MHz channels (as shown in FIG. 6), with a second signal which is provided from the output coupler **500**. The diplexer **540** first bandpass filters the first signal and the second signal, and then combines the two signals to provide a single output (which contains signal energy in the MDS and ITFS/MMDS/OFS frequency bands) to an output antenna **550**.

The MDS transmitter **520** receives its input signals from a line **621** which is connected to an external source, but alternatively can be provided from the LNA **110** (coupling connection not shown) because the antenna **105** will also couple the MDS frequency band.

The driver A **115**, driver B **120**, modular power amplifier **300**, and MDS transmitter **520** are all connected via a GNET serial multidrop network **175** conforming to an RS-485 standard and following a protocol developed and marketed by Coactive Aesthetics Inc. A selected data structures used by the modular broadband booster system **100** to communicate over the GNET **175** are discussed with respect to FIG. 5C. While this GNET RS-485 network **175** is preferred, other buses including VMEbus, VXIbus, etc., could be used as well. The GNET provides a system bus within the Modular Broadband Booster System **100** and is used for passing control signals, sensor signal and monitoring signals to the several components of the modular broadband booster system **100**.

Connected to and controlling the GNET **175** is a redundant system controller **200** (also discussed in reference to FIG. 33), which is a circuit board based on a Motorola MC68HC11F4FN micro-controller. Like the drivers **115**, **120**, the system controller need not have redundant features. The redundant system controller **200** has a plurality of inputs **210** for receiving signals from scaling amplifiers used in monitoring various system parameters. The redundant system controller **200** also includes a plurality of outputs **202** for providing control signals to the various components of the modular broadband booster system **100**.

A user interface **205** (also discussed in reference to FIG. 33) connects to the redundant system controller **200** and is used by local operators of the modular broadband booster system **100** to view the status of the booster system **100**, and to input specific control commands to the booster system **100**. More particularly, the user interface **205** permits a user to input data into the system for adjusting control parameters, maintenance parameters, controlling the system for turning the system on/off) and for printing data if desired.

A slave controller and system I/O interface device **250** connects to the GNET **175** and provides a second system monitoring station, ancillary to the redundant system con-



troller **200**, and provides remote accessing control through a network **265** and a public switched telephone network (PSTN) **260**. Alternatively, the slave controller and I/O **250** could perform the functions of the redundant system controller **200**, or vice versa. The remote accessing control feature allows the modular broadband booster system **100** to report status information, fault information, sensor information and system related information to a central network management system (e.g., a Sun Microsystems Sparc **20** Workstation operating a Hewlett Packard HP Openview® application) which controls a number of different broadband booster systems **100** which make up a MMDS network. Accordingly, through the slave controller and system I/O interface **250**, the central network management system (located at the main transmitter **1**, FIG. **1**) controls various features of the modular broadband booster system **100** (such as incrementally increasing or decreasing power, monitor system health, etc.), thereby enabling dynamic network resource reallocation and reconfiguration, and negating a conventional need for provided on-site operations personnel.

The slave controller and system I/O interface **250** also discussed in reference to FIGS. **34–35b** is a Packard Bell 120 MHz Pentium™ computer using the Microsoft Windows NT operating software, although other CPU-based systems and operating system would be adequate in light of the present description. The slave controller and system I/O interface **250** includes a network port for connecting to a network **265**, examples of which include a fiber distributive data interconnect (FDDI), an Ethernet, an integrated-services digital network (ISDN, which is preferred), asymmetrical digital subscriber line (ADSL), Firewire (IEEE 1394), Universal Serial Bus (USB), and an RJ-11 jack for connection to a public switched telephone network (PSTN) **260**.

A central network manager (also discussed in reference to FIG. **36**) is located at the main transmitter **1** (FIG. **1**) and employs a Sun Microsystems Sparc **20** Workstation operating a Hewlett Packard HPOpenview® network management application. Additionally, an authorized user employing a conventional personal computer can remotely access the booster system **100** via the PSTN **260**. The slave controller and system I/O interface **250** recognizes the entry of the network manager and the remote user and permits them to receive information as contained in a management information base (MIB), which is unique to the particular MMDS network that uses the booster systems **100**. Accessing MIB information and remotely controlling the booster system **100** is accomplished via simple network management protocol (SNMP) “GET,” “SET,” and “TRAP” commands.

The slave controller and system I/O interface **250** includes a user interface **255** which is a cathode ray tube (CRT) display, a keyboard, a mouse or the like for a data entry device (see FIG. **34**).

FIG. **5B** is a flowchart of a process implemented by the redundant system controller **200** (FIG. **5A**) that is one component of the system-level automatic level control of the system **100** (FIG. **5A**). The process starts in Step **S100** where the redundant system controller **200** is initialized by retrieving specific initialization values and initializing other processors in the system **100**. The process then proceeds to Step **S106** where the redundant system controller **200** polls respective PA modules in the modular power amplifier **300** as to determine the operational status of each of the PA modules. Based on the results of the polling step **S106**, the redundant system controller **200** identifies a number “N” of operational PA modules that will be used later for determining a system output power range in which the system **100**

should operate. While the process illustrated in FIG. **5B** shows the control flow for a power-up sequence, the step **S106** may also be performed in response to an interrupt request or a message from an individual PA module indicating that a change in an operational status has occurred.

The process subsequently proceeds to Step **S108** where samples are obtained from respective components of the system **100** (such samples of fan speed, open door status, respective states of the PA modules, etc.). The process then proceeds to Step **S110** where processes are performed on the respective samples in order to determine respective operational states of the respective components in the system. Based on the results of Step **S110**, the process proceeds to Step **S112**, where the redundant system controller **200** executes control over the transmitter system based on the results of the Step **S110**. Sequential to Step **S112**, or coincident therewith, the redundant system controller **200** prepares a message to be sent to the driver **115**, **120**, reporting the results of the polling step **S106**. In particular, the redundant system controller **200** forms a message held in a register implemented in semiconductor (or the like) that indicates the number of operational PA modules and later sends the message, in step **S116**, to the driver **115**, **120**, where the number “N” is used to adjust a system output power according to the number of operational PA modules. The structure of the message will be described with respect to FIG. **5C**.

After Step **S112**, the process proceeds to Step **S114** where the redundant system controller **200** prepares a message that contains the number “N” of operational power amplifier modules. Subsequently, in Step **S116**, the process sends the message and additional messages to other system components so as to exert control and monitor the status of the respective components. The process then returns to Step **S108** where additional samples are taken. Consequently, the redundant system controller performs a main loop that includes Steps **S108**, **S110**, **S112**, **S114**, and **S116**, and continues in the main loop until an interrupt or priority message is received that requires the redundant system controller **200** to temporarily exit the main loop.

FIG. **5C** shows a data structure of a message in the form of a transmission frame that is formed by the redundant system controller **200** and other processors for communicating information amongst the respective processors in the system **100**. In the illustrated data structure, each transmission frame includes a first data field **5001** that is one byte in length and defines a form of a message that is to be transmitted from one element in the system **100** to another element. Adjacent to the first field **5001** is a second data field **5003** that is one byte in length and defines a form of a parameter conveyed by the message. At the end of the transmission frame, a two-byte third data field **5005** is formed and includes a parameter value that is associated with the form of the parameter held in the second data field **5003**. While the data structure described above defines a transmission frame that is four bytes in length and having three fields, other message conventions may be used. A first alternative includes a transmission frame having two data fields defining the message type and parameter in the first field and the parameter value in the second field. A second alternative includes a first transmission frame that defines a type of message to be received followed by one or more additional frames that carry one or more updated parameter values.

The transmission frame illustrated in FIG. **5C** is used by the redundant system controller **200** to convey the polling result of Step **S106** (FIG. **5B**) to driver **115**, **120**. In this case,



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the redundant system controller **200** forms the transmission frame of FIG. 5C in a semiconductor memory register. The first data field **5001** indicates the message is of a “set parameter” type; the second data field **5003** indicates that the parameter to be set is the number “N” of operational PA modules that are active in the modular power amplifier **300**; and the third data field includes a value indicative of the number “N” of operation PA modules. The driver **115**, **120** receives and stores the message in memory, and analyzes the contents of the respective data fields **5001**, **5003**, **5005** so as to determine the number of operation PA modules. As will be discussed with respect to FIG. 9B, the driver **115**, **120** determines the expected system output power that should be observed based on the number of operation PA modules and, if necessary, adjust an input power so as to keep the system output power within a predetermined range. The data structure of FIG. 5C is similarly used to convey status messages, control message and other messages between any of the processors in the system **100**.

FIG. 6 shows the frequency bands processed by the modular broadband booster system **100**. Channels within the MMDS (wireless cable) structure are divided generally into three groups, F1, F2, and F3. The first group, F1, includes two 6 MHZ channels identified as MDS1 and MDS2 which provide a multi-point distribution service. The channels in the F1 frequency band are processed and amplified by the MDS transmitters **520** (FIG. 5A). The second group of channels F2 are non-contiguous with the frequency band F1 and includes 20 ITFS 6 MHZ channels and 8 MMDS 6 MHZ channels. The third group of channels, F3, include three 6 MHZ channels that are interspersed between ITFS channels G1–G4, and identified as OFS H1, H2, and H3. The frequency bands F2 and F3 are amplified by the drivers **115**, **120**, the  $\frac{1}{16}$  power divider **130**, the modular power amplifier **300**, the radial combiner **500** and the output coupler **500**, as shown in FIG. 5A. Each of the 33 channels shown in FIG. 6 is capable of holding a single 6 MHZ National Television System Committee (NTSC) analog television signal or several digital television signals. If desired, the invention may be specifically constructed for the above-frequencies and NTSC signal, although the invention may also be constructed for other frequencies and types of signals, as desired (e.g., personal communication system, PCS, head-end transmitter applications and the like).

FIG. 7 is a block diagram of the redundant low noise amplifier (LNA) **110**. Signals input through the input antenna **105** (FIG. 5A) are passed through a preselection filter **101** which is centered around the MMDS frequency band (see FIG. 6) and excludes out-of-band interference. An output of the preselection filter **101** is passed through a switch **102** which is controlled by a line **117**, originating from the drivers **115**, **120**. Toggling the switch **102** enables/disables, respectively, a first amplifier **103** and a redundant second amplifier **104** (although only one amplifier is required in the present embodiment). The amplifiers **103** and **104** are LNAs which boost the input RF signal by several dB and set a noise figure of the broadband booster system **100** to a low level such that the input RF signal will not become corrupted by noise produced within the broadband booster system **100**. Because only one of the drivers **115**, **120** is a master, at any given time, and has authority to control the LNA **110**, there is no risk of the drivers **115**, **120** sending conflicting signals over the line **117** (as will be discussed with respect to FIG. 9A). The two LNA amplifiers **103**, **104** provide an additional level of redundancy in the booster system **100** architecture. Redundancy is desired because the LNA **110** is located at a top of a support pole, adjacent to the

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antenna **105** (FIG. 1), and thus is not easily accessible and repairable. Furthermore, unlike conventional booster systems, the booster system **100** not need to go off the air if an LNA amplifier **103**, **104** fails because the other LNA amplifier **104**, **103** is available on hot-standby status.

FIG. 8 shows the driver B **120** in more detail, which has the same structure as the driver A **115** although not shown in FIG. 8. An input **112** provided by the redundant LNA **110** (FIG. 5A) is input to a variable attenuator **121** which cooperates with a first gain stage **123** and a second gain stage **125** to provide a fixed gain setting of about 25 dB when combined with the LNA **110** assembly. An output of the gain stage **125** is fed through a sense port **127** which senses the output signal level and feeds the output signal level back through an envelope detector **129**. The envelope detector **129** detects the output power from the driver B **120** and provides it to a MC68HC11F4FN controller **131** on a microcontroller board. The controller **131** adjusts the variable attenuator **121** by comparing the output of the envelope detector **129** with a stored threshold value held in memory on the microcontroller board, thereby allowing the driver B **120** to output a signal at a constant power level. The controller **131** also adjusts the variable attenuator **121** in response to information about a number of operational PA modules sent from the redundant system controller **200** (FIG. 5A) via the GNET serial bus **175**, and feed back line **160**, such that the output power of the modular broadband booster system **100** is controlled at the system level. A sampled signal (including forward and reflected power information) is fed back from the output coupler **500** (FIG. 5A) on line **160** so that if the sampled output power is less than a minimum threshold, which is held by the controller **131**, the driver B **120** can adjust its attenuation and output a higher level (as will be discussed with respect to FIG. 9B, for example). Power is supplied to the drivers **115**, **120** through line **700**.

A control line **116** is used to coordinate master/slave status between the driver B **120** and the driver A **115**. A set of signals corresponding to which of the drivers **115**, **120** becomes the master and which becomes the slave are passed over the line **116** as well as other information including a remote turnoff capability which allows each of the drivers **115**, **120** to turn off the other driver **120**, **115**. The line **116** is used to transfer fault information between the drivers **115**, **120**, RF output power measurements and an input power detection signal which is used to determine whether or not the LNA **110** is operating properly. Each of the input power detection and RF power monitoring and fault indicator signals are “cross-couple” in that the signals are shared between the two drivers **115**, **120**.

The drivers **115**, **120** include a dip switch **128** used to set one of the two drivers **115**, **120** to be designated as the master upon initialization and the other designated as the slave. On power-on, reset, or another initialization event, the controller **131** checks a setting on the respective dip switch **128** to determine whether that driver **115**, **120** is a master or a slave. When one of the drivers **115**, **120** determines it is the master it begins performing a role of sending control signals to the LNA **110** and to the divider **130**.

Because the drivers **115**, **120** are redundant and coupled to one another, they are capable of switching from a slave state to a master state when the slave determines the master has failed. If, for example, the driver B **120** is initially the slave, but later determines that the driver A **115** has in some way failed, the driver B **120** issues a turn-off command through line **116** which turns off the master state of the driver A **115**. Thus, the driver B **120** becomes the master and is capable of controlling the LNA **110** and dividing the divider **130**.



FIG. 9A illustrates a control flow between the driver A 115 and the driver B 120. It is first noted, however, that the state diagram and the drivers 115, 120 will function to arbitrate master and slave status regardless of whether the GNET 175 network serial bus is functioning properly or not. In FIG. 9A, an initial state upon power reset is shown as state 118, where the respective driver 115, 120 (FIG. 8) which has been designated (by the dip switch, FIG. 8) as being the master, recognizes that it is the master. Once the selected driver determines it is the master, it is free to select one of the amplifiers 103, 104 in the LNA 110 (FIG. 5A) to amplify the input signal provided by the antenna 105.

Also in the state 118, the designated slave executes a software process which effectively monitors an RF power, an input power detection signal, and all fault signals issued by the respective master. Provided that the slave determines that each of the signals coming from the master is normal, the slave will remain the slave. However, suppose that the RF power fails in the master as evidenced by an input detection signal dropping below a given threshold. Under these circumstances, the slave will determine, upon detecting this drop, that the master driver has failed in some way. In response, the slave will turn off the master by issuing a turnoff signal 126 through the line 116. The master status then transfers (as indicated by arrow 124) to the former slave and the state of the drivers 115, 120 changes to state 119. In essence, this transfer of status from master to slave becomes a slave "revolt" and will occur when any combination of the three signals (RF power, input power detection, and fault signals) are determined by the slave to be abnormal. The slave will continue to monitor its own input signal 128 until it determines that the input signal is absent. If the slave does determine the input signal is absent, the slave will relinquish control back to the original master (i.e., return to state 118). However, in returning the master status to the original master, the slave will first be delayed by a delay 122 for a certain predetermined amount of time in order to prevent a rapid transfer of master and slave status between the drivers 115, 120 when no RF signal is present. Suppose there is actually no RF signal present, perhaps because the transmitter 1 of FIG. 1 is damaged, the delay 122 prevents the respective drivers 115, 120 from endlessly transferring the master status back and forth between the drivers 115, 120 as they attempt to diagnosis why no signal is being input from the antenna 105 and LNA 110. The delay 122 prevents the master status from rapidly transferring between the drivers 115, 120, but rather requires a fixed period of time (e.g., 0.5 seconds) before transferring master status back to the original master.

FIG. 9B is a flowchart illustrating a process implemented in the driver controller 131 (FIG. 8) which adjusts an overall power of the transmit system, based on a number of functioning PA modules, and an amount of forward and reflected power observed by a power sampler 501 in the output coupler 500. While the process of FIG. 9B is performed by the drivers 115, 120, the process may alternatively be implemented on another controller such as the redundant system controller 200. The process begins in Step S400, where the controller 131 analyzes a message sent from the redundant system controller 200, where the message contains an indication of the number "N" of operational PA modules. Alternatively, the controller 131 may itself identify which of the respective PA modules are operating by polling the respective PA modules or monitoring respective status conditions of the PA modules. In Step S400, the controller 131 analyzes a third data field 5005 (FIG. 5C) of the message and identifies the number "N" of PA modules that

are presently in a transmit state and otherwise contribute to the total system output power.

After Step S400, the process proceeds to Step S402 where the forward and reflected power from the output coupler 500, as detected by a power sampler 501 (FIG. 10), are monitored. The power sampler 501 (FIG. 10) is calibrated by a factory calibration procedure, or another suitable calibrating technique, so as to provide a 1.4 VDC signal when all of the PA modules are functioning. For example, when 16 PA modules are functioning, a composite single carrier output power is 200 W, which in turn produces a 1.4 VDC signal from the power sampler 501. If less than 16 PA modules are functioning, then a less than 1.4 VDC signal will be produced. The process then proceeds to Step S404, where the VSWR is calculated by the controller 131 based on the forward and reflected power measurements provided by the power sampler 501. If the calculated VSWR exceeds a predetermined threshold (e.g., 20%) for a predetermined amount of time (e.g., 1 minute), the controller 131 sends a fault message to the redundant system controller 200 (FIG. 5A), notifying the redundant system controller 200 that a potentially damaging amount of reflected power has been observed so that the redundant system controller 200 may take corrective action.

After Step S404, the process proceeds to Step S406 where an inquiry is made regarding whether the measured forward power is less than a range that is stored in memory (internal or external to the controller 131). A separate range of output power is stored in the memory for different numbers of N, such that the range of acceptable output powers associated with N=16 will be greater than the range associated with N=15, 14 . . . If the response to the inquiry in Step S406 is affirmative, the process proceeds to step S408, where the controller 131 sends an adjustment signal to the adjustable attenuator 121 so as to decrease the attenuation (which is normally about 3 dB within a range of 0 dB to about 15 dB) by an amount that will bring the measured output power into a middle of the range associated with the number N of operational PA modules. However, if the measured power is more than 2 dB below the middle of the range, the controller 131 sends a fault signal to the redundant system controller 200, so that redundant system controller can take corrective action and turn the entire system off, if necessary. After Step S408, the process returns to Step S400 where the controller once again checks for the number of operation PA modules.

If the response to the inquiry in Step S406 is negative, another inquiry is made in Step S410 regarding whether the measured forward power is greater than a predetermined number in the stored range associated with the number N of operational PA modules. If the response to the inquiry in Step S410 is affirmative, the process proceeds to Step S412 where the controller 131 causes the amount of attenuation imparted by the attenuator 121 to be adjusted by an amount that makes the measured power fall in the middle of the range associated with the number N of operational PA modules. Similarly, if the output power exceeds a predetermined amount, e.g., 2 dB, the controller 131 issues a fault message to the redundant system controller 200 to take corrective action and perhaps power-down the system. Subsequently the process returns to Step S400.

FIG. 10 illustrates the modular, reconfigurable architecture of the modular power amplifier 300 and its interconnection with the  $\frac{1}{16}$  power divider 130, the radial combiner 400, and the output coupler 500. Preferably 16 signals are output from the  $\frac{1}{16}$  power divider 130 and accepted by the modular power amplifier 300. While 16 signals are preferred, the modular broadband booster system 100 is



capable of employing a N-way divider **130**, a N-way modular power amplifier **300**, and a N-way radial combiner **400**. The modular power amplifier **300** includes a power amplifier housing assembly **301** which is two chassis, although one housing or more than two housing would be sufficient, and 16 power amplifier “slices” (PA slices), **310<sub>1</sub>-310<sub>16</sub>**. The inventors coined the term “slice” because when placed next to one another in a chassis, the PA modules resemble slices of bread in a bread loaf.

Each of the PA slices **310<sub>1</sub>-310<sub>16</sub>** are constructed identically, and provide independent amplification paths for input signals applied thereto. The PA slices **310<sub>1</sub>-310<sub>16</sub>** communicate with other components of the booster system **100** via the GNET serial bus **175** which provides two-way communication between the individual PA slices **310<sub>1</sub>-310<sub>16</sub>** and other components of the modular broadband booster system **100**. A local bus **176** provides an internal communication path within the modular power amplifier **300**. The local bus **176** is a serial peripheral interface (SPI) bus because the SPI bus is closely associated with Motorola Corporation’s MC68HC11F4FN microcontrollers, which are the preferred microcontroller (FIGS. 14 and 19) used in each of the PA slices **310<sub>1</sub>-310<sub>16</sub>**. However, other local bus structures and microprocessors would be suitable. The local bus **176** and the GNET serial bus **175** connect to the individual PA modules **310<sub>1</sub>-310<sub>16</sub>** via circuit board connectors used for connecting boards to buses and backplanes.

The amplified output signals from the PA slices **310<sub>1</sub>-310<sub>16</sub>** are passed through the power amplifier housing assembly **301** and provided to a set of respective connectors **302<sub>1-16</sub>**, which are mounted on the power amplifier housing assembly **301**. Connecting to each of the respective connectors **401<sub>1</sub>-402<sub>N</sub>** is a corresponding semi-rigid line **401<sub>1</sub>-401<sub>16</sub>** which connect the respective PA slices **310<sub>1</sub>-310<sub>16</sub>** to the radial combiner **400**. Each of the semi-rigid lines **401<sub>1</sub>-401<sub>16</sub>** is preferably a Teflon dielectric cable and having a specified length corresponding to the MMDS frequency range, MMDS bandwidth and mechanical packaging constraints for packaging the PA slices **310<sub>1</sub>-310<sub>16</sub>** proximate to the radial combiner **400**. The length of each of the semi-rigid lines **401<sub>1</sub>-401<sub>16</sub>** is set such that individual PA slices **310<sub>1</sub>-310<sub>16</sub>** may be removed from the power amplifier housing assembly **301** if for some reason that particular PA slice fails. Accordingly, each of the semi-rigid lines **401<sub>1</sub>-401<sub>16</sub>** is desirably within the range of 21 cm to 30 cm in length and preferably 25.4 cm.

The low end of the semi-rigid line length range is primarily based on mechanical considerations where, each of the PA slices **310** are mounted in an equipment rack **900** (discussed with respect to FIGS. 37a, 37b, and 37c), and the radial combiner **400** is mounted behind the PA slices **310** in the rack **900** (FIGS. 37b and 37c). The length of the semi-rigid lines **401<sub>1</sub>-401<sub>16</sub>** must be sufficiently long in order to connect the radial combiner to the individual PA slice modules. In order to reduce the length of the semi-rigid lines **401<sub>1</sub>-401<sub>16</sub>**, PA slices **310<sub>9-16</sub>** are mounted “up-side down” in the rack **900**, as shown in FIGS. 37a, 37b and 37c. This permits semi-rigid lines **401<sub>9-16</sub>** to be placed closer to the radial combiner **400** than if PA slices **310<sub>9-16</sub>** were mounted “right-side up”. When the PA slices **310<sub>1-16</sub>** are positioned as shown in FIGS. 37a-37c, the length of 25.4 cm for the semi-rigid lines **401<sub>1-16</sub>** is sufficient to connect each of the PA slices **310** to the radial combiner **400**.

The upper end of the desirable range of the semi-rigid line lengths is established by a phase length restriction of each of the semi-rigid lines **401** such that a maximum output power is delivered by each of the semi-rigid lines **401**. In order to

deliver a maximum output power, a phase length of 1.86 cm in each of the Teflon dielectric cables should be set to correspond with a center of the MMDS band (2.593 GHz). Because 1.86 cm is too short of a length to connect each of the PA slices **310** to the radial combiner **400**, a phase length of each of the cables must be increased in increments of the phase length of each of the semi-rigid lines **401**, where the phase length at 2.593 GHz is 3.93 cm, and is ½ of the wavelength at 2.593 GHz. Thus, the desired length of each semi-rigid line **401** is set to 6 wavelengths plus the offset of 1.86 cm so as to provide maximum output power from each line. If the cable lengths were made too long, a phase rotation of frequencies at an upper end of the MMDS frequency band (i.e., 2.686 GHz) and at the low end of the MMDS frequency band (2500 MHz), would be offset from optimal power matching conditions and create a risk of high VSWR developing at the connections between the PA lines **310** and the corresponding semi-rigid lines **401**. Because each of the semi-rigid lines **401** is optimized for the center frequency 2.593 GHz, as the length of the semi-rigid lines **401** increases, the absolute amount of phase offset at the high frequency (2686 MHz) and the low frequency (2500 MHz) also increases by a proportional amount. It is undesirable for the absolute amount of phase offset for the upper frequency and the lower frequency to be significant because an observed voltage standing wave ratio (VSWR) will become substantial for significant phase offsets and thus will create the possibility of a voltage breakdown at a connection between each of the PA slices **310** and the semi-rigid lines **401**.

The combination of the fixed input impedance of the radial combiner **400**, the modularity of the power amplifier **300** and semi-rigid lines **401**, and an ability to control power level and number of modules, via a local system controller or a remote network controller, allows the booster system **100** to be reconfigured for various applications. In particular, the above combination permits the booster system **100** to degrade gracefully, such that should one of the respective PA slices **310<sub>1</sub>-310<sub>16</sub>** fail, the booster system **100** can operate with only 15 or fewer of the PA slices **310<sub>1</sub>-310<sub>16</sub>** operating, which in the case of N=16, results in a loss of about 0.3 dB in output power. For example, suppose the PA slice **1** (**310<sub>1</sub>**) fails, its failure will be detected at the module level (i.e., the PA slice **1** will detect a fault condition), at the system level (i.e., the Redundant System Controller **200**, FIG. 5A, will detect the fault condition), and at the network level (i.e., the MMDS network controller that controls the booster system **100** via the Network **265**, FIG. 5A, will detect the failure). The initial fault condition will be transmitted as a fault signal and issued through the GNET serial bus **175** where the redundant system controller **200** (FIG. 5A) will, for example, turn off the PA slice **1** (**310<sub>1</sub>**). Alternatively, a technician by viewing a front panel display and I/O (FIG. 13) on PA slice **1** (**310<sub>1</sub>**) showing that the PA slice has failed (e.g., perhaps by producing an abnormally low output power as a result of one of several power field effect transistors failing), can locally turn off PA slice (**310<sub>1</sub>**) and remove the failed slice while each of the other PA slices **310<sub>2</sub>-310<sub>16</sub>** are still functioning. Furthermore, the network manager can detect and control the status of the PA slice **310<sub>1</sub>** via the network **265**. The ability to support “hot-swapping” of PA slices **310** is a direct result of the arrangement of the radial combiner **400**, lengths of the semi-rigid line **410**, addition of a processor on each PA module and positioning of the PA slices **310<sub>1-16</sub>** with respect to the radial combiner **400**, which combine to minimize VSWR to each of the functioning PA slices **310** when a failed PA slice is removed.



In contrast to conventional combiners, such as Wilkinson combiners, the present system permits individual ones of the PA slices **310**<sub>1-16</sub> to be removed from the chassis **301** while the other PA slices **310** are still functioning (i.e., the PA slices **310** are “hot swappable”). With conventional combiners combining two or more high power amplifiers, all of the high power amplifiers must be turned off in order to replace a failed high power amplifier. Furthermore, in the conventional combiner, there would be a substantial risk of personal injury and risk of damaging the other power amplifiers and the combining network due to a development of high, breakdown-level voltages on respective connections to the power amplifiers and the Wilkinson combiner. In contrast, the modular shown in FIG. 10 will not develop breakdown voltages at the radial combiner **400** and a set of connectors **302**<sub>1-16</sub>, and thus, damage results to other components in the power amplifier module **300** or the radial combiner **400**, when one or more of the PA slices **310** are removed from the power amplifier housing assembly **301**. Accordingly, the length and number of the semi-rigid lines **401**, the number of inputs to the radial combiner cavity **400**, will be specific, in this particular embodiment, to the MMDS frequency range (FIG. 6).

The output coupler **500** accepts a single high power (about 800 W peak envelope power) input from the radial combiner **400** and prepares a high power output signal for transmission from an output antenna **550** (FIG. 5A) after first matching an output impedance of the radial combiner **400** with the output antenna **550**. The output coupler **500** includes a power sampler **501** which samples the total available power and reflected power at the output coupler, although a bidirectional coupler may be used to sense reflected power and forward power and provide the forward and reflected power measurements to the drivers **115**, **120**. The output of the power sampler **501** is divided and distributed to the drivers **115**, **120** through the feedback lines **160**.

FIG. 11 illustrates how an individual one of the PA slices **310** connects to a backplane **312**, both of which reside in the power amplifier housing assembly **301** (FIG. 10). The backplane **312** provides both structural and electrical connections for the PA slice **310**. The PA slice **310** plugs into the backplane **312** by an operator inserting the PA slice **310** into the power amplifier housing assembly **301** and pressing the PA slice **310** onto backplane connectors (not shown). Once connected, the PA slice **310** is electrically interfaced with the backplane **312**. Other slices (see FIG. 13) will attach to the backplane **312** in a similar manner as the slice **310** shown in FIG. 11.

The backplane **312** includes a plurality of signal, control, power, and ground lines **314** which include: differential SPI serial communication lines; differential SPI address lines; GNET RS-485 serial lines; control master reset and standby lines; digital ground lines; analog ground lines; and +25 volts and +9 volts direct current (DC) voltages. Each of the signal, control, power and ground lines **314** are available to each of the PA slices **310** that connect to the backplane **312**. The slice **310** also connects to line **316** which provides 220 volts rectified alternating current (AC) from which the slice **310** derives its own power used to perform the amplification process.

The slice **310** includes three modules: a RF amplifier module **375**, a microcontroller module **325**, and a power supply module **350** which includes a switching power supply. Combining a RF amplification circuit (e.g., the RF amplifier module **375**) with digital logic (microcontroller module **325**) and switching power supply on a single circuit board is contrary to conventional RF amplifier design prac-

tice because it is very difficult to prevent the RF signals from becoming corrupted by electromagnetic interference (EMI) created by the switching power supply and digital logic, as preventing the high power RF signals from disrupting digital logic circuitry. However, in order to provide the reconfigurability, reliability, and modularity offered by the booster system **100**, the inventors determined it was preferable to combine the power supply module **350**, microcontroller module **325**, and RF amplifier module **375** in a single PA slice **310** assembly. However, to preserve the integrity of digital signals passed along the backplane **312**, the output high power output from the RF amplifier module **375** is not passed through the backplane **312**, but rather is received by I/O connectors **302** (e.g., push-on semi-rigid SMA-type connectors) formed in the power amplifier housing assembly **301**. Each of the PA slices **310** amplifies the frequency range of 2500 MHZ to 2686 MHZ (F2 and F3 from FIG. 5A) of the MMDS frequency band.

FIG. 12 shows the mechanical and electromagnetic interference (EMI) structural architecture for the PA slice **310**. A housing assembly **311** includes a front panel display and I/O **323** which is used by an operator as a local user interface. A display portion of the front panel display and I/O **323** is a LED, although an LCD, plasma, CRT and other displays would be suitable for providing more detailed information about the specific PA slice **310**. An I/O portion of the front panel display and I/O **323** is a 12 position flexible membrane touch panel used to input data and control signals to the specific PA slice **310**. The housing assembly **311** also includes an interlock enable/disable switch **324**, which is used by a local operator to disable the PA slice **310** before removing or inserting the PA slice **310** into the power amplifier housing assembly **301** (FIG. 10). The interlock enable/disable switch **324** prevents an operator from inadvertently being injured or damaging the PA slice module by removing the module from the power amplifier housing assembly **301** while power is applied to the PA slice module. The housing assembly **311** also includes a heat sink **313** formed on a back portion of the assembly **311** for dissipating heat from the PA slice **310**. As an additional feature, a front metallic cover plate covers the assembly **311** such that the modules **325**, **350**, and **375** are enclosed.

The housing assembly **311** includes EMI isolation shields **321**, preferably aluminum, but other materials are possible, which divide an internal space of the housing assembly **311** into three compartments for respectively hosting the RF amplifier module **375**, the power supply module **350**, and the microcontroller module **325**. The EMI isolation shields **321** provide electromagnetic shielding between the respective modules and thus help reduce contamination of the RF signal when passed through the RF amplifier module **375**. Likewise, radiated emissions of digital and power supply noise are confined within their respective compartments. A pair of I/O connectors **318** and a backplane connector **317** are provided on a back portion of the assembly **311** for providing RF, digital and power connections to other system components.

As an added measure of EMI protection, within a surface of the assembly **311**, a milled EMI isolation channel **322** is formed for receiving intermodule wiring harnesses. The milling is approximately 2–3 mm deep and has approximately the same width as the wiring harnesses (which varies in the preferred range of 0.1 cm to 2.1 cm) which fit therein. Each of the respective modules **350**, **375**, and **325** include a flexible EMI isolation shield (preferably made from a Kapton flex material) which is laminated to a back portion of each of the respective modules **325**, **350**, **375**. The lamina-



tion portions **350A**, **375A**, and **325A**, as shown in FIG. 12, are made of the KAPTON flex material and provide a high amount of EMI isolation from the digital signals passed between the respective modules and sent through the wiring harnesses disposed in the milled EMI isolation channels **322**. In addition to the EMI advantages, the milled EMI isolation channels **322** allow the harness to be recessed into the assembly **311** such that the modules **325**, **350**, and **375** have respective flat surfaces on which to lie. This arrangement provides a stronger mechanical connection between the modules **325**, **350**, and **375** and the assembly **311**, as well as a flat surface for positioning the EMI isolation shields **321** so as to prevent gaps in which EMI can leak between respective module compartments.

FIG. 13 shows the PA slice **310<sub>1</sub>** next to seven other of the PA slices **310<sub>2-8</sub>**. Each of the respective PA slices are placed within a subchassis **311A** which is suitable for holding 6U (i.e., "U" being an industry standard measurement of circuit board size) circuit boards. From FIG. 13 it is clear that if one of the PA slices **310** fail, and a fail (or fault) message is displayed on its corresponding display **323** (e.g., by illuminating an LED), a service technician is provided with a clear indication of which of the failed PA modules has failed. Once the technician identifies the PA slice which has failed, the technician will first press the interlock switch **324** which removes power from the PA slice **310<sub>1</sub>**. Once the power is turned off, the technician may easily slide the respective failed assembly **310** from the subchassis **311A** and replace the failed PA slice **310<sub>1</sub>** with a new PA slice **310**. This maintenance operation can be performed while each of the other PA slices **310** continue to function. Thus the modular broadband booster system **100** need not be turned off in order to replace an individual PA slice **310**. A similar subchassis **311** is utilized with the PA slices **310<sub>9-16</sub>**. In order to minimize the length of the semi-rigid lines **401**, the up/down orientation of one subchassis **311A** is opposite to that of the other rack (see FIGS. 37a-37c). However, if the length of the lines **401** is not an issue, (e.g., for other frequency bands) it will not be necessary to have one rack upside-down as compared to the other.

FIG. 14 is a block diagram showing respective control and signal interconnections between the RF amplifier module **375**, the power supply module **350**, and the microcontroller module **325** for a particular PA module **310**. The RF amplifier module **375** accepts an RF input signal and outputs an amplified RF output signal (RF out), and the power supply module **350** and the microcontroller module **325** do not directly process the RF input signal. Rather, the RF amplifier module **375** communicates with the microcontroller module **325** through an amplifier control harness **178** (see FIG. 16). Similarly, the RF amplifier module **375** communicates with the power supply module **350** via an amplifier power supply harness **179** (see FIG. 16). Communications between the microcontroller module **325** and the power supply module **350** are performed via a power supply control harness **180** (see FIG. 15).

As shown in FIG. 14, the microcontroller module **325** is also configured to communicate to other modules in the modular broadband booster system **100** via the SPI bus **176** and the GNET serial bus **175**. Operation of the display and I/O **323** (FIG. 13) is performed through a RS-232 bus **177**, although illuminating a LED in response to a fault condition is achieved by a hardwired connection to the microcontroller module **325**.

FIG. 15 shows a more detailed diagram of the power supply control harness **180**. Individual lines within the power supply control harness **180** includes a pair of comple-

mentary pulse width modulation lines (PWM), a short circuit current fault indication lines (ISC-Fault), a power supply enable line (P.S. Enable), and an open voltage (O.V. Fault) fault line. The PWM lines are used by the microcontroller module to send complementary controllable PWM signals to the power supply module **350** in order to control a switching frequency and a duty cycle of (which determines on/off times) for switching on and off the field effect transistors (FETs) used the power supply module **350**. The ISC-fault line sends a status message to the microcontroller module **325** informing the microcontroller module **325** of a perceived short circuit in the power supply module **350** or a load connected to an output of the power supply module **350**. Similarly, the O.V. fault line is used to relay a status message to the microcontroller module informing the microcontroller module **325** of a perceived overvoltage condition in the control module **325**. The P.S. Enable line is used enable/disable the power supply at the board level (via the control module **325**), at the system level (via the redundant system controller **200**, FIG. 5A), or at the network level (via the network **275**).

In addition to the above mentioned control and status lines, the power supply control harness **180** includes monitoring signal lines. The respective current drain to source lines (IDS-1 . . . IDS-8) are used by the microcontroller module **325** to monitor a current draw from individual amplifier FETs in the RF amplifier module **375** (see, FIG. 17). While eight current drain to source lines are preferred, others may be added or subtracted according to the number amplifiers used in the RF amplifier module **375**. The IDS 1-8 lines provide information to the microcontroller module **325** which enable the microcontroller module **325** to directly manipulate eight corresponding VGS 1-8 control lines (discussed in more detail with respect to FIG. 16). Each of the respective IDS 1-8 lines include a resistor therein which is used to sense the respective current flow through a corresponding one of the IDS 1-8 lines. Thus the microcontroller module **325** is capable of monitoring the voltage supplied by the power supply module **350** and respective current drawn on each of the lines IDS-1 . . . IDS-8, which will be used by the microcontroller module **325** to automatically adjust the respective output levels of individual amplifier FETs in the RF amplifier module **375**.

FIG. 16 is a more detailed diagram of the amplifier control harness **178** and the power supply control harness **179**. The amplifier control harness **178** includes eight control signal lines VGS1-8 for controlling, respectively, a voltage between a gate and a source of amplifiers in the RF amplifier module **375** (see FIG. 17 and FIG. 18). Each of the lines VGS1-8, is used to send a control signal from the control module **325** to the RF amplifier module **375** in order to independently control up to eight independently controlled amplifiers used within the RF amplifier module **375**. (Of course, other techniques such as multiplexing control signals will reduce the number of lines required). Furthermore, eight other signal paths, VGS1-8 MON, carry to the microcontroller module **325** monitoring signals for each of the voltage gate to source signals for the amplifiers in the RF amplifier module **375**.

The amplifier control harness **178** also includes a hot standby line, and a gain control line. The hot standby line carries a control signal from the control module **325** to the RF amplifier module **375** in order to place the RF amplifier module in a hot standby state (as will be discussed with respect to FIG. 20A), or to turn the RF amplifier module **375** on or off. When the RF amplifier module **375** is in the hot standby state, no RF energy is output from the RF amplifier



module 375. VDS voltages (discussed in more detail with respect to FIG. 17) are applied to the respective amplifiers in the RF amplifier module 375, each of which provide a corresponding output that is monitored by the microcontroller 325 and used to bias the respective VGS 1–8 signals (see FIG. 17 for more detail) in order to automatically adjust an output signal level at each of the amplifiers in the RF amplifier module 375. Once each of the respective output levels is adjusted, the RF amplifier module is brought “on-line” without risk that its respective output power level will be inconsistent with the output signal levels provided by the other PA slices 310 (assuming the other PA slice 310 are functioning properly).

The amplifier control harness 178 also includes a gain control signal line that is used by the control module 325 to control an overall amount of gain applied to the input RF signal by the RF amplifier module 375. Controlling the gain amongst the PA slices 310 enables each slice 310 to output signals having powers consistent with the other PA slices. The consistent output power from each PA slice suppresses intermodulation distortion (which is a problems when non-linear amplifiers amplify plural signals at different frequencies), and avoids signal compression which would be present if all of the PA slices 310 did not output the same power levels.

The amplifier control harness 178 further includes a forward power signal line and a reverse power signal line which are used by the microcontroller module 325 to monitor the output signal from the RF amplifier module 375. The microcontroller module 325 uses the forward power and the reverse power to determine the coupling efficiency of the RF amplifier module to the radial combiner 400 (FIG. 5A), measure voltage standing wave ratio (VSWR), and other figures-of-merit.

The power supply module 350 provides eight VDS lines (VDS1–8) in the power supply control harness 179. Each of the VDS1–8 lines provides an independent voltage path to individual amplifiers used in the RF amplifier module 375. By providing independent voltage paths, risk is minimized of one failed amplifier within the RF amplifier module 375 affecting the performance of the other amplifiers in the RF amplifier module 375. Also, the insertion of sense resistors (see FIG. 15) permit the respective IDS values for individual amplifiers in the RF amplifier module 375 to be monitored.

FIG. 17 illustrates how each of the voltage gate to source lines (VGS1–8) respectively, are used to bias individual ones of amplifiers 385, as shown in FIG. 17. FIG. 17 shows an embodiment where five amplifiers 385<sub>3-4</sub> and 385<sub>6-8</sub> are used as part of a three-stage amplification chain. Three other amplifiers (which would be labeled 385<sub>1-2</sub> and 385<sub>5</sub> in FIG. 17, although not expressly shown) could be added to supplement performance if desired. Each Ids (i.e., each amplifier’s drain to source current) is adjustable by adjusting a voltage gate to source control signal VGS<sub>1-8</sub>, which is controlled by the microcontroller module 325 as applied through a bias circuit (shown as a resistor in FIG. 17). A corresponding set of monitoring signals lines VGS1–8 MON are used by the microcontroller module 325 to monitor the bias voltage on each of the amplifiers 385<sub>1-8</sub> present in the RF amplifier module 375. Each of the voltage supply lines VDS 1–8 is applied to respective ones of the eight amplifiers 385<sub>1-8</sub> as shown in FIG. 17. Thus, should one of the amplifiers fail, power is not necessarily removed from the other amplifiers 385.

The microcontroller module 325 monitors each of the respective VGS1–8 lines with VGS 1–8 MON lines, as well

as the reflected power (R.P.) and the forward power (F.P.) through a pair of monitoring lines R. P. and F. P. as shown in FIG. 17. The monitoring lines R. P. and F. P. are provided by the directional coupler 378 (e.g., a surface mount microstrip coupler manufactured by Mid-Atlantic Corp.) which is placed at the RF signal output of the amplifier module 375.

The overall output level of the RF amplifier module 375 is adjusted by varying a signal level on a gain control line, as applied from the microcontroller module 325. The signal level on the gain control line adjusts an attenuation setting on a variable attenuator 381 such that an input signal level is normalized to 20 dBm before passing through the fixed gain amplifiers 385 which output an output signal at 47 dBm.

On/off and hot standby modes of the RF amplifier module 375 may be controlled from the microcontroller module 325 by sending a signal to the single pole double through (SPDT) switch 382 via the hot standby control signal line. When in the hot standby mode (as will be discussed with respect to FIG. 21), the individual amplifiers 385 have their VGS and signals varied so as to avoid damaging the FETs in the PA module. During the hot-standby mode, no energy is output from the RF power amplifier 375.

FIG. 18 shows a three-stage amplifier/coupling architecture used in the RF amplifier module 375. The five amplifiers 385<sub>4-8</sub> are configured in three stages. The amplifier pair 385<sub>7-8</sub> provides a first stage of amplification that cooperates with the amplifier 385<sub>6</sub>, which provides a second stage of amplification. These two stages of amplification provide 18 db of gain. Amplifiers 385<sub>4-5</sub> provide an additional 10 dB of gain to provide a system gain of about 28 dB. In contrast to single stage amplifiers, this tri-stage amplification architecture provides both broad bandwidth and constant linearity over 300 MHz bandwidth with a 0.1 dB to 0.2 dB ripple through the band. By driving each of the amplifiers 385<sub>4-8</sub> well beneath its specified operational range, linearity throughout the amplification process is preserved and intermodulation distortion products are suppressed. For example, the second stage amplifier 385<sub>6</sub> is a FLL310 GaAs amplifier manufactured by Fujitsu which is rated for 30 watts. However, by backing-off the output power of the amplifier 385<sub>6</sub> to 5 watts, exceptional linearity is preserved. Amplifiers 385<sub>7-8</sub> are of the type 2XFLL171, and in contrast to conventional design practice, these two amplifiers are used together in the first stage of amplification in order to get a large bandwidth (e.g., 300 MHz) and flat ripple through the pass band. This is accomplished by sharing the first stage of amplification between two amplifiers 385<sub>7-8</sub>, which are each backed off by over 5 dB from their maximum operational rating and combining the outputs of the respective amplifiers using a 90° hybrid 383B. The Amplifiers 385<sub>4-5</sub> are of a type 2XFLL310, which are push-pull GaAs amplifiers manufactured by Fujitsu. These amplifiers are preferred for the third amplification stage because when configured to provide a fixed gain of about 10 dB, they can provide an output signal power of 47 dBm (peak power) in the frequency range of 2 GHz and higher, with only ±1.0 dB of gain flatness, and third order intermodulation products that are down –43 dBc.

The first stage amplifiers 385<sub>7-8</sub> are fed from a 20 dBm input signal passed through a first 90° hybrid 383A. The first 90° hybrid 383A receives an input signal from the variable attenuator 381 which in turn is fed from the switch 382. The first 90° hybrid 383A appropriately divides the input signal into two isolated component parts which are then amplified by the first stage amplifiers 385<sub>7-8</sub>. Aside from the signal splitting function, the first 90° hybrid 383A provides a fixed input and output impedance of 50 Ω such that input imped-



ances are consistently matched in each of the three stages of amplification in the RF amplifier module **375** for each of the PA slices **310**<sub>1-16</sub>. Consistent 50  $\Omega$  matching between successive amplifier stages minimizes reflections in the signal path such that consistent signal coupling efficiency is exhibited for each amplifier stage in each of the PA slices **310**. Resistor **R2** connects to the 90° hybrid in order to provide isolation between the two signals output from amplifiers **385**<sub>7-8</sub>.

A second hybrid **383B** combines the respective outputs from the first stage amplifiers **385**<sub>7-8</sub> and provides a 50  $\Omega$  output to the second stage amplifier **385**<sub>6</sub>, which amplifies the signal to provide a constant level output of about 37 dBm at the second stage of amplification.

A third 90° hybrid **383C** accepts and splits the signal output from the second stage amplifier **385**<sub>6</sub> into two separate signals. These two separate signals are passed to the third stage push-pull amplifiers **385**<sub>4-5</sub> which further amplify the RF signal by about 10 dB (accounting for hybrid losses) and provide two respective inputs to a fourth 90° hybrid **383D**. The fourth 90° hybrid **383D** combines these respective amplified output signals into a single RF output signal having a power level of 47 dBm and a source impedance of 50  $\Omega$ .

The RF output signal is sensed by the directional coupler **378** which is a surface mount strip-line directional coupler manufactured by Mid-Atlantic Corporation and used to sense a forward power and reflected power at the output of the RF amplifier module **375**.

During normal operation, when the RF amplifier module **375** is placed in a transmit state, the microcontroller module **325** will continue to monitor the respective output power levels by comparing the respective measured  $I_{ds}$  signals from the amplifiers and **385**<sub>4-8</sub> with ideal  $I_{ds}$  values stored in memory in the microcontroller module **325**. By performing these measurements and adjustments concurrent with normal transmit operations, the microcontroller module **325** can compensate for signal level variations caused by temperature variation and amplifier aging in each of the respective amplifiers **385**<sub>4-8</sub>.

The adjustable attenuator **381** is set at a specific value during manufacturing and predelivery evaluation where each of the gain stages in the drivers **115**, **120** and RF amplifier module are characterized. The value is set such that the output of the adjustable attenuator is 20 dBm when provided with a signal from the respective drivers **115**, **120** (FIG. 5A) which typically provide signals of 32 dBm. By normalizing the input signal to 20 dBm for each of the PA slices **310**, the output of each PA slice **310** will also be normalized because the output levels of each stage of amplification will constantly be monitored and adjusted by the microcontroller module **325**.

Thus, for the modular broadband booster embodiment, when the respective outputs of 16 PA slices **310** are combined, the modular broadband booster system **100** provides a minimum of 800 watts peak envelope power (PEP) and typically 1 kw PEP.

FIG. 19 shows a detailed architecture of the microcontroller module **325** for a given one of the PA slices **310**. The microcontroller module **325** is based on a controller **326** which is preferably a Motorola MC68HC11F4FN microcontroller, having eight analog to digital (A/D) converters. The controller **326** interfaces with a random access memory (RAM) **330** used for holding dynamic program variables such as flags used for program status, state variables, management information base (MIB) values, etc.

The controller **326** also includes a programmable read only memory (PROM) **331** which is used to store program variables such as a setting value for the adjustable attenuator **381** (see FIG. 17), and ideal  $I_{ds}$  values which will be used to compare with the  $I_{ds}$  MON signals from the respective amplifiers **385** (FIG. 18) in the RF amplifier module **375** (FIG. 18). The microcontroller module **325** includes a dip switch **332** which holds initial switch settings used by the controller **326** in order to determine its respective state during initialization. More particularly, the dip switch **332** holds a controller "address" which allows the controller **326** to identify itself while communicating over the local bus **176**, and over the GNET serial bus **175**. During pre-delivery evaluation, the dip switch **332** will be initially set to have an address setting of, for example, "1" if used in the PA slice **310** assigned a first slot in a chassis **311A** (see FIG. 13).

Signals communicating over the local bus **176**, the GNET serial bus **175**, as well as the RS-232 bus **177**, which connects the controller **326** with the display and IO **323** (FIG. 13), have their voltage levels adjusted by a TTL level interface **333** to normal TTL logic levels.

The controller **326** communicates with the power supply module **350** (FIG. 16) via a programmable logic device (PLD) **335**. Signals communicated over the amplifier control harness **180** are passed through the PLD **335** and routed through a control bus **329**, a data bus **328** and an address bus **327** of the microcontroller module **325**. The controller **326** also communicates with the RF amplifier module **375** (FIG. 16) through a buffer block **340** and a buffer block **349**. Signals received from the amplifier control harness **178** are passed through the buffer block **340** which appropriately scales and buffers the respective signals received from the amplifier control harness **178**. In addition, the buffer block **340** accepts other signals such as a 10 volt monitoring signal and various sensor signals such as temperature sensor signals (TEMP). Each of the signals input to the buffer block **340** is buffered, using tri-state buffers, then forwarded to a multiplexer **345** which multiplexes the respective input signals onto eight separate lines under the control of the PLD **335**. Once multiplexed, the signals distributed on the eight line are passed to the eight A/D converters in the controller **326** where they are digitized and subsequently analyzed by the controller **326**.

Signals output from the controller **326** and sent through the amplifier control harness **178** are passed through a 12-way, 8-bit serial digital-to-analog converter (DAC) **348**, which converts each of the digital signals output from the controller into an analog format and passes them through the buffer block **349**, which then sends the buffered analog signals to the amplifier control harness **178**.

Power for the microcontroller module **325** is derived from the 9 volt DC power line received from the backplane **312** (FIG. 11). A local power supply regulator **342** converts the input 9 volt DC power signal into a  $\pm 12$  volt DC regulated power source and a +5volt DC regulated power source, each of which are used to power the components on the microcontroller module **325**.

FIG. 20A illustrates a state diagram implements by the controller **326** (FIG. 19) and defining five active states in which the respective PA modules **310** may operate. Upon receiving a reset signal, the controller **326** enters a cold standby state **1700**. In this cold standby state, the PA module has its respective FET amplifiers turned off and  $V_{dd}$  set near 0 V (i.e., turned off). The controller **326** will remain in the cold standby state **1700** until it receives a transition signal, indicating that an interlock for the PA module has been



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closed and the PA module is to move into a hot standby state **1705**, via a transition state **1703**. Accordingly, in the transition state **1703**, the respective FETs are configured to follow a specific power up sequence, as will be discussed with respect to FIG. 21. Once powered up and stabilized, the controller **326** transfers the PA module **310** from the transition state **1703** to the hot standby state **1705**. The hot standby state **1705** is defined as the respective FET amplifiers being powered on (i.e., Vdd being 10.6 V and Vgs set so as not to pinch off the FET), although an input switch **382** (FIG. 18) being placed in an open position. Accordingly, in the hot standby state **1705**, the PA module does not contribute to the RF power that is output from the output coupler **500**.

If while in hot standby state the PA module receives a transmit signal, the PA module transfers from the hot standby state **1705** to a transmit state **1707** by closing the switch **382** so that the PA module does contribute to the total RF output power. Similarly, if in the transmit state **1707**, the PA slice module receives an instruction to return to the hot standby state **1705**, the switch **382** will open and the PA module will return to the hot standby state **1705**. Also, while in the hot standby state **1705**, the PA module will return to the cold standby state **1700** if instructed to do so, or enter a failed state **1709** if the controller **326** identifies a fault condition. Similarly, while in the transmit state **1707**, the controller **326** may detect a failure and enter the failed state **1709**, or transfer back to cold standby state **1700** if instructed to do so.

While in the failed state **1709**, the processor **326** recognizes that a fault condition has occurred and can only transfer out of the failed state **1709** by correction of the fault condition. While in the failed state **1709**, the processor will attempt to transition to the cold standby state **1700** a predetermined number of time at predetermined intervals. However, if while in the cold standby state **1700**, the fault condition continues to exist, the PA module will return to the failed state **1709**. The PA module will remain in the failed state and a fault light will be illuminated on the front panel of the failed PA module if the PA module is unsuccessful in transitioning to the cold standby state **1700** after a predetermined number of attempts.

FIG. 20B is a flowchart of a process implemented by the controller **326** in the PA module **310** for performing automatic level control at the board level. The process begins in Step **S200** where the controller **326** is initialized (which also may be implemented with an interrupt routine, for example). As part of the initialize Step **S200**, the control voltages for the respective FETs are ramped-up in a predetermined manner by first lowering Vgs (to about -3.2 V) so as to pinch-off the FETs, and while pinched-off ramping up Vdd to about 10.6 V. Subsequently, Vgs is increased to about -0.9 V after Vdd is ramped-up and stable. The process then proceeds to Step **S202** where samples from the monitored signals, such as VGS 6-MON, as shown in FIG. 17, are obtained. The controller **326** then processes the respective samples in Step **S204** by converting the samples into digital values so as to facilitate comparing them with stored digital values. The process then proceeds to Step **S208** where an inquiry is made for each digital value regarding whether the digital value is within a predetermined range of values stored in memory that correspond to the sample under investigation. If the response to the respective inquiries in step **S208** are affirmative, then the process proceeds to Step **S212** where any appropriate communication from the PA module (such as a message containing the measured value) is formed and transmitted from the PA module, and then the

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process returns to Step **S202** after all of the samples have been evaluated. However, if the result in Step **S208** is negative, the controller **326** controls and adjusts the respective adjustable parameter (e.g., respective Vdd or Vgs) to within the predetermined range of values and then the process proceeds to Step **S212** and the Step **S202**.

FIG. 21 is a flowchart of a "hot swap" process which is enabled by the presence of the respective controllers **326** in the PA modules. The process begins in Step **S300** where an inquiry is made regarding whether a normally closed interlock on a PA module that hosts the subject controller **326** is triggered (i.e., change close to open status or a message indicated a status has changed). If the response to the inquiry in Step **S300** is negative, the PA module remains in an transmit state as indicated in Step **S310**. However, if the response in Step **S300** is affirmative, the process proceeds to Step **S314**, where the respective values Vgs are ramped down so as to pinch-off the FETs and thereafter, in Step **S316**, Vdd is ramped down so as to turn off the respective transistors. Subsequently, the process proceeds to Step **S318** where a prompt message is sent to the redundant system controller **200** (FIG. 5) and the front panel of the PA module, prompting a technician to replace the PA module. Because the RF power has now been removed from the PA module and due to the structure of the modular power amplifier **300** and radial combiner **400**, this PA module may safely be removed/replaced even though the other PA modules remain in a transmit state.

After Step **S318**, the process to Step **S320** where the same controller on the PA module (or another controller if a new PA module has been inserted) inquiries whether the interlock for the PA module is closed. If the response in **S320** is negative, the process returns to Step **S318** where the technician is prompted to replace the PA module. However, if the response to Step **S320** is affirmative, the process proceeds to Step **S322** where an inquiry is made regarding whether the Vgs has been set to pinch off the respective FETs. Thus, if the response in Step **S322** is negative, the PA module remains in a transition state and the process returns to Step **S320**. However, if the response in Step **S322** is affirmative, Vdd is ramped up to 10.6 volts and the process then proceeds to Step **S328** where the Vgs may then be increased from about -3.5 volts to about -0.9 volts so as to activate the FET.

FIG. 22 is a block diagram of a pulse width modulation (PWM) circuit **608** embodied within the programmable logic device **335** (FIG. 19) and controlled by a computer-based software process implemented in the controller **326** (FIG. 19). An output of the PWM circuit **608** provides an adjustable complementary pair of PWM signals that are passed over the power supply control harness **180** to the power supply module **350**. The PWM signals are used by the power supply module **350** to control a switching frequency and duty cycle of a switching power supply that employs switching power FETs resident within the power supply module **350**. Alternatively, in the interest of simplifying the system architecture, a power supply using commercial off-the-shelf components may be used.

The PWM circuit **608** receives the data bus **328** and the control bus **329** from the controller **326** (FIG. 20A). The PWM circuit **608** outputs the PWM signals on the power supply control harness **180**, and receives from the power supply module **350** a VDD feedback signal on the power supply control harness **180**.

The PWM circuit **608** includes a first register **600** used to hold a terminal count value loaded over the data bus **328** from the controller **326** (FIG. 19). This terminal count value



will determine a lower bound on the switching frequency of the PWM signals (about 60 kHz). A first counter 601 receives a frequency seed value from the data bus 328, which is used to define an upper bound on the switching frequency of the PWM signals produced by PWM circuit 608. The counter 601 also receives from the controller 326 a clock input (CLK).

At the beginning of a PWM cycle, the counter 601 will sequentially count from its initial frequency seed value (e.g., 0) at a rate determined by the CLK signal (e.g., a 14.7 MHz clock). The counter 601 outputs its accumulated value to a comparator 607 which compares the terminal count value, 245, stored in register 600 with the accumulated output of the counter 601. When the accumulated value in counter 601 equals or exceeds that of the stored value in register 600 the comparator 607 will output a signal T\_CNT as a logic high (i.e., +5V). The T\_CNT signal is provided to a logic block 609 and to the control bus 329. When the T\_CNT signal is a logic high, it resets the accumulated count value in the counter 601. Thus, the time duration between successive logic high pulses on the T\_CNT signal line defines the switching frequency of the PWM output signals from the circuit 608.

The PWM circuit 608 also includes a second counter 605, a register 602, and a comparator 606, combined to provide a "dty\_cnt" (duty count) signal which defines a duty cycle of the PWM signals. The register 602 is initially provided with a duty cycle seed value, 32, via the data bus 328 as provided from the controller 326. The duty cycle seed value will determine an upper bound on the duty cycle of the PWM signals output from the PWM circuit 608. Updating the duty seed cycle value is accomplished by overwriting the old value stored in the register 602. The counter 605 receives an initial duty cycle value, 0, from the databus 328. In response to an external clock signal (CLK), the counter 605 will sequentially count from the initial duty cycle value.

At the beginning of a PWM signal period, the counter 605 will begin counting from the initial duty cycle value and output its accumulated value to a second comparator 608 which compares the accumulated count value from counter 605 with the duty cycle seed value stored in the register 602. The comparator 606 outputs a logic high dty\_cnt signal when the accumulated count value in the counter 605 is equal to or greater than the stored duty cycle seed value from the register 602. The comparator 606 will continue to output a logic high dty\_cnt signal until the counter 605 is reset to its initial value, as triggered by the T\_cnt logic high signal. Thus, when the comparator 607 outputs a logic high T\_cnt signal, both the counter 601 and the counter 605 are reset to their initial value. The controller 326 may also initialize a reset event independent of the T\_cnt value by issuing a reset signal over the control bus 329.

The PWM circuit 608 also includes a comparator 603 which compares a threshold voltage, 10.7 volts, set by the controller 326 (FIG. 19) to a fed-back VDD voltage from the power supply control harness 180 (FIG. 20A), which is digitized by an A/D converter 604. An output of the comparator 603 is a signal PWM\_T which is applied to the logic block 609. The logic block 609 derives the complementary PWM signals in response to receiving the PWM\_T signal, the dty\_Cnt signal and the T\_Cnt signal. The PWM\_T signal is used by the logic block 609 to truncate the duty cycle of the PWM signals, as discussed below and also with respect to FIG. 23.

The logic block 609 uses combinatorial logic (although a software process may be used) to produce the PWM output

signals based on the T\_cnt, dty\_cnt and PWM\_T input signals. A first one of the PWM output signals will have a logic high value when the T\_cnt signal, the dty\_cnt signal, and the PWM\_T signal are at a logic low. The first PWM output signal will have a logic low value whenever the PWT\_T signal is high, whenever the dty\_cnt signal is a logic high and the T\_cnt is a logic low, or whenever the T\_cnt is a logic high. The other PWM output signal will have logic levels that are complementary to that of the first PWM output signal.

The controller 326 will use the fed-back VDD signal provided by the power supply module 350 as an indicator for whether and how to adjust the terminal count value in register 600, the frequency seed value in counter 601, the duty cycle seed value in register 602 in the initial duty cycle value in the counter 605 in order to provide a constant VDD output. The PWM\_T signal provides control for reducing the PWM duty cycle and thus, reducing the level of VDD output from the power supply module 350.

FIG. 23 provides a description of how the PWM signals are shaped by the respective T\_cnt, dty\_cnt, and PWM\_T signals. FIG. 23 is a time diagram showing the time-based characteristic of the first PWM signal output from the PWM circuit 608. The x-axis of the graph represents time and the y-axis represents voltage. At a time  $t=0$  a reset signal has just been issued and each of the counters 601, 605 has been just been reset to their initial values. Accordingly, the first PWM signal transitions to a logic high state (+5V) because both the dty\_cnt and the T\_cnt will return to a logic low after a reset event, and it is presumed that the measured Vdd value does not exceed the threshold value. Assuming the value of Vdd does not exceed the threshold voltage, the first PWM signal will remain in the logic high state for a time duration  $T_D$ . Then, at a time  $t_1$ , the dty\_cnt signal transitions to a logic high and the logic block 609 responds by changing the output to a logic low. The first PWM signal will remain at a logic low until a time  $t_2$  which signifies the beginning of the next cycle of the first PWM signal in response to the T\_cnt signal resetting the counters 601, 605.

Assuming the value of Vdd does not exceed the threshold voltage, the PWM\_T signal will truncate the duty cycle of the PWM signals output from the logic block 609. More particularly, for the exemplary PWM signal shown in FIG. 23, the first PWM signal is truncated for a duration of time  $T_1-t_x$  where  $t_1$  is a time when the dty\_Cnt signal transitioned to a logic high and  $t_x$  is a time when the PWM\_T signal transitioned to a logic high. The PWM\_T signal will normally be at a low voltage because the VDD signal will be beneath the threshold signal, set at 10.7V. However, when the VDD signal raises above the threshold signal, the comparator 603 will output a logic high signal at a time  $t_x$ , which will cause the logic block 5609 to truncate the PWM signal.

FIG. 23 shows the first PWM signal after having been truncated at time  $t_x$ . As shown in FIG. 23, the normal duty cycle of a time duration  $T_d$  has now been reduced to a time duration equivalent to  $t_1-t_x$ . The overall period ( $1/F$ ) is not affected by the truncation of the duty cycle.

FIG. 24 illustrates a process for controlling and adjusting the output power from the power supply module 350. The process begins in a Step S30 where the microcontroller module 325 issues a reset signal to reset each of the stored values in the PWM circuit 608. The process then flows to a Step S31 where an initial terminal count value is loaded into the register 600, and the initial frequency seed value is loaded into the counter 601, the initial duty cycle seed value



is loaded into the register **602**, and the initial duty cycle value is loaded into the counter **605**. Once each of the initial values have been respectively loaded, the process flows to Step **S32** where a value of VDD is received from the VDD feedback line.

The received VDD signal is compared in a Step **S33** against a stored maximum threshold voltage value. If the received VDD signal is greater than the maximum threshold value, the process proceeds to a Step **S34**, but if not, the process proceeds to a Step **S35**. In the Step **S34**, respective ones of the terminal count value, the frequency seed value, the duty cycle seed value, and the initial duty cycle value are adjusted in order to lower the VDD. For example, the VDD value can be lowered by placing a larger duty cycle seed value into the register **602** because the larger duty cycle seed value lowers the duty cycle. The VDD value can be increased by placing a lower duty cycle seed value into the register **602** because it lengthens the duty cycle of the first PWM signal. The value of VDD is affected by the duty cycle because the duty cycle determines the duration for which switching transistors used in the power supply will remain active. The longer the transistors stay active the more current they will pass to a charging capacitor. If the process flows from the Step **S33** to the Step **S35**, the Step **S35** inquires whether VDD is less than a minimum threshold. If an affirmative response is received, the process flows to Step **S36** where selected ones of the terminal count value, the frequency seed value, are adjusted in order to increase the VDD signal. The duty cycle seed value will be decreased by 10% in order to increase the resulting duty cycle of the first PWM signal output from the PWM circuit **608**. If a negative response is received from the inquiry in Step **S35**, the process returns to Step **S32** where VDD is monitored once again.

FIG. **25** is a block diagram that illustrates the distributed power supply architecture for the modular broadband booster system **100**. A power source of single phase 220 volts alternating current (AC) is available from an input **700** to each of the driver A **115**, the driver B **120**, an auxiliary AC/DC converter **701**, and a main AC rectifier circuit **702**. The driver A **115** and the driver B **120** derive their own power from the input **700**. The auxiliary AC/DC converter **701** produces the +9V and +12V power lines supplied on the backplane **312** (FIG. **11**) of the modular power amplifier **300** (FIG. **5A**). The main AC rectifier circuit **702** converts the 220 volt AC input into a 200 volt Haversign pulses that are distributed to each of the PA slices **310**<sub>1-16</sub> (FIG. **10**).

It is preferable to distribute power to each of the PA slices **310**<sub>1-16</sub> in this way because it allows distributed power factor correction between the PA slices **310** in order to minimize harmonic disturbances that the modular broadband booster system **100** imparts to a commercial power grid that supplies power to the modular broadband booster system **100**. Also, because each of the PA slices **310**<sub>1-16</sub> include their own housing assembly **311** (FIG. **12**) with cooling fins **313** serving as heat sinks, there is no single dominant heat source which may effect negatively the reliability of the system. Additionally, if one of the individual power supplies on the PA slices **110**<sub>1-16</sub> fails, the entire system does not fail. Moreover, if one of the power supply modules **350** on a given PA slice **310** fails, the overall system output power (RF power) is only reduced by 0.3 dB because the radial combiner **400** (FIG. **10**) is still capable of accepting inputs from N-1 functioning PA slices **310**.

FIG. **26** is a schematic diagram of the main AC rectifier circuit **702**. The input **700** provides 220 volt AC at 32 amps to a pair of one-to-one isolation transformers **705**. Each of

the respective isolation transformers **705** are provided for redundancy such that if one should fail the other is available as a hot standby. A pair of rectifier assemblies **706** accepts the 220 VAC and produce rectified 200 volts at 2.5 amps respectively. The rectified 225 volt signals are passed through the respective cross coupled diodes **707**, which further block AC signals as well as reflected waves. The output of cross coupled diodes **707** is are Haversign pulses which are then provided by a terminal **708** to the respective PA slices **310** (FIG. **25**). Similarly, the main AC rectifier circuit **702** provides grounds terminals **709** to the PA slices **310** (FIG. **25**).

FIG. **27** is a schematic diagram of the power supply module **350** used in each one of the PA slices **310**. The power supply **350** includes a field effect transistor (FET) driver circuit **710**, a power factor correction and boost regulation circuit **711**, a pair of power switching FETs **713**, **713a**, a load resistor **714** and a load capacitor **715**. The Haversign pulses are provided via connector **708** from the main AC rectifier circuit **702** (FIG. **26**) and passed to the power factor correction and boost regulation circuit **711**. In response, the power factor correction and boost regulation circuit **711** adjusts the power factor (i.e., active power to apparent power ratio) of the input power to 0.95. Once corrected, the input power is then boosted to a level of 300 volts unregulated DC provided to a source of the switching FET **713**. A gate of the switching FET **713** is controlled by the FET driver circuit **710** which receives and forwards the PWM signals provided by the microcontroller module **325**. The first PWM signal switches the switching amplifier **713** on and off such that small pulses of the 300 VDC unregulated power are provided to the capacitor load **715** through the load resistor **714**. The second PWM signal switches a low-side FET **713a**. The capacitor load **715** accumulates the charge from the small pulses such that 10.5 volts are developed with respect to ground, **709**. An FET **713a** serves to protect the power supply module **350** from an overvoltage condition by providing a drain of FET **713** a path to ground during an overvoltage condition.

The voltage developed on the capacitor **715** is provided as a feedback signal VDD which is passed to the microcontroller module **325** through the power supply control harness **180** so the VDD can be monitored and adjusted by the microcontroller module **325**.

Each of the eight lines connecting to load capacitor **715** include a set of respective sense resistor  $R_{1-8}$  used to measure the current drain to source ( $I_{ds}$ ) of each of the currents drawn from the respective GaAs FET amplifiers **385** (FIG. **17**). The output of each of the respective resistors  $R_{1-8}$  correspond to the voltage lines VDS 1-8 P.S., as shown in FIG. **17**.

In order to further promote the reliability of the power supply module **350**, the microcontroller module **325**, upon being notified of the fault in the power supply module **350**, can alert a local operator through a front panel display and I/O device **323** (FIG. **13**) so appropriate maintenance action may be taken.

Additionally, the microcontroller module **325** can also alert remote terminals by sending an error message over GNET **175** to the redundant system controller **200** (FIG. **5A**). The redundant system controller will then issue an SNMP trap message (described in more detail with respect to FIG. **35a** and FIG. **35b**) informing the network manager, via the network **265** (FIG. **5A**) precisely what is the nature of the perceived problem and which power supply module is failing or failed. Accordingly, the remote network manage-



ment system may then place the PA slice **310** in a hot standby mode, turn the failed module off, or require that it continue to operate until it fails completely.

FIG. **28** is a plan view of the radial combiner **400** (FIG. **5A**). The radial combiner includes a set of 16 inputs **403**, e.g., SMA female connectors which receive the 16 semi-rigid lines **401** (FIG. **5A**). However, if N PA slice modules **310** are used in the modular power amplifier **300** (FIG. **5A**) then an N-way radial combiner **400** having N inputs **403** would be used. The function of the radial combiner is to provide a matched summing network for each of its N inputs and offer a graceful degradation feature such that the combiner network will not fail even if driven with only a subset of N input signals.

Each semi-rigid line **401** connects to corresponding inputs **403** of the radial combiner **400** (as shown in FIGS. **37b** and **37c**). The radial combiner is configured so each semi-rigid line **401** sees a  $50 \Omega$  impedance. Adjacent ones of the semi-rigid lines **401** are input to corresponding adjacent inputs of radial combiner inputs **403**. Each of the semi-rigid lines are isolated from one another by fixed resistance R (not shown) in accordance with the inherent impedance characteristics of the radial combiner **400**.

Energy coupled into a given input **403** of the radial combiner **400** is passed through a waveguide section formed between two opposing radial plates **405** (only the top plate is visible in FIG. **28**), which are separated by 3.11 inches and have an outer diameter of 4 inches, into a central cavity portion **404** formed in a central portion of radial combiner **400**. At the central cavity portion **404**, each of the N signals input through the inputs **403**, are summed in power and jointly exit as a single RF output signal through an output **402**.

The respective size of the outputs port **402**, the opposing plates **405**, the inputs **403**, and the waveguide portions, are made consistent with the disclosures of U.S. Pat. No. 5,128,628 (Marks et al.), which is incorporated herein by reference; U.S. Pat. No. 4,956,614 (Baril), which is incorporated herein by reference and U.S. Pat. No. 4,812,782 (Ajioka), which is incorporated herein by reference; and made to support the preferred frequency range of 2.5 GHz to 2.686 GHz.

Because of the unique structure and electrical integration of the radial combiner **400** into the modular broadband booster system **100**, an individual one of the PA slices **310** may be turned off using switch **324** and extracted from the chassis **311A** without fear of damaging adjacent PA slices **310<sub>2-n</sub>**. Furthermore, as a further guard against unforeseen potential reflections from the radial combiner **400** to an individual PA slice **310** output, the directional coupler **378** (FIG. **17**) on each PA slice **310**, and the sample port **501** (FIG. **10**) after the radial combiner output are capable of sensing an impedance mismatch between the slice module **310**, semi-rigid line **401**, and radial combiner **400**. When a mismatch is detected in response to the signals provided by either the directional coupler **378** or the sample port **501**, the microcontroller modules **325** in the respective PA slices **310** and or drivers A, B **115**, **120** will terminate operation when the amount of forward power or reverse power reflection from the PA slice output is greater than a certain predetermined threshold. Alternatively, the redundant system controller **200** (FIG. **5A**) will detect the mismatch and shut down the problematic PA slice **310**. Furthermore, the network manager may shut down the problematic PA slice when the network manager checks the modular broadband booster system's MIB (see discussion regarding FIGS. **35a**, **35b** and

**36**) and sees an attribute value indicating the particular PA slice **310** is experiencing extraordinary forward or reverse power reflections.

When an individual PA slice **310** fails, or is moved off-line for any reason, the redundant system controller **200** (FIG. **5A**) issues a command to the driver controller **131** via the GNET data bus **175**. The drivers **115**, **120** adjust a required output power in order to compensate for a lower level of performance necessitated by the failure or removal of the PA slice **310**. If an adjustment were not made, the automatic level correction function provided by the drivers **115**, **120** in response to the sampled output single fed back from the output coupler **500** on the line **160** would attempt to over-drive the modular power amplifier **300** even though one of the PA slices **310** failed. Thus, when the drivers **115**, **120** recognize that one of the PA amplifier slices **310** have failed or have been taken off-line, the ALC control provided by the drivers **115**, **120** strive to provide an output power commensurate with a modular power amplifier **300** having only 15 PA slices **310**.

FIG. **29** shows an equivalent circuit for the radial combiner **400**. Each semi-rigid line **401<sub>1-n</sub>** observes an input impedance  $Z_o$  ( $50 \Omega$ ). The signals provided through the respective semi-rigid lines **401<sub>1-n</sub>** are summed at the output port **402** (also shown in FIG. **28**). Because each of the individuals semi-rigid lines **401** are appropriately sized (i.e., within a range of 21 cm to 30 cm), a fixed resistance exists between adjacent ones of the lines **401<sub>1-n</sub>**. If, however, each of the semi-rigid lines **401** are not appropriately sized (e.g., perhaps the semi-rigid lines are too lengthy such that the RF energy at 2686 MHz is rotated in phase by  $0.25 \lambda$  from the center frequency 2593 MHz) a voltage developed on R will become excessively large. Thus, there will be a substantial risk of a short circuit (e.g., arcing) developing between the outputs of adjacent PA slice modules **310** and their corresponding connections **302** (FIG. **10**) to the semi-rigid lines **401** when an individual one of the PA slice modules **310** is either removed from the chassis **311A** or for some reason develops an impedance mismatch with the radial combiner **400**.

FIG. **30a** illustrates the diplexer **540** which excepts inputs from the MDS transmitters **520** (FIG. **5A**) and the output coupler **500** and produces a combines, bandpass filtered output to the output antenna **550**. The diplexer **540** combines the RF energy from the MDS frequency band (i.e., the F1 band from FIG. **6**) with the RF energy from the ITFS/MMDS/OFS frequency band (i.e., the F2 and F3 band in FIG. **6**, which is non-contiguous with the MDS frequency band). The MDS transmitter **520** inputs its MDS RF energy into an input **805** which couples the MDS RF energy into a plurality of resonant cavities **802** (e.g., four), each of which is optimized in size (i.e., capable of supporting transmission modes) MDS frequency band and thus bandlimits RF energy outside of the MDS frequency band. Stacking the cavities **802** one after another, sharpens a pair of bandstop skirts (e.g., at high and low edges of the MDS band), thereby further suppressing out-of-band emissions, including intermodulation products. A filter such as that disclosed in co-pending U.S. patent application Ser. No. 08/818,896, entitled "Dielectric Resonator Filter Configured to Filter Radio Frequency Signals in a Transmit System," filed Mar. 17, 1997, the contents of which is incorporated herein by reference, may be used as well.

The diplexer **540** also includes a second cavity stack **801**, optimized for the ITFS/MMDS/OFS frequency band, which couples and bandpass filters the RF energy from the coupler **500** through a second input **807** and to the second cavity



stack **801** (which includes 6 resonant cavities). The cavity stack **801** couples the energy into the load **803**, such that the RF energy from the coupler **500** combines with the RF energy from the MDS transmitters **520**.

The load **803** outputs the combined RF energy to a notch filter assembly **8100** (discussed in more detail in reference to FIG. **30b**). The notch filter assembly **8100** further bandlimits the RF energy by notch filtering the RF energy at frequencies slightly below the MMDs band and slightly above the MMDs band. The RF energy from the notch filter assembly is then output to the antenna **550**.

FIG. **30b** is a perspective view of the notch filter assembly **8100** embodied within the diplexer **540**. RF energy from the load **803** (FIG. **30a**) is input to a waveguide portion **820**, which couples the RF energy to be output to the antenna **550** (FIG. **5A**). A dielectric resonator **830a** serves as a notch filter assembly and includes a window **850** and a stub **840**. The window **850** and the stub **840** cooperate with the waveguide **820** to further suppress the spectral occupancy of the diplexer **540** at specific frequencies. Tuning screws **860** tune the discontinuity of the dielectric resonators such that if the screws **860** protrude into the waveguide by more than one-quarter of a wavelength, the apparent load will become inductive and thus further suppress signals at the low end of the MMDS band near 2.5 GHz. If the screw is turned to less than one-quarter of a wavelength, the load appears to be capacitive and thus the notch filter dielectric resonators **830a** and **830b** suppress RF energy just above the upper MMDS band at 2.686 GHz. Two dielectric resonator notch filters **830a-b** are used, one turned capacitively and one turned inductively, to further suppress the out-of-band signals below the 2.5 GHz range and above the 2.686 GHz range. However, additional dielectric resonator notch filters may be used as well to further suppress out-of-band signals emissions.

FIG. **31** is a graph of frequency versus signal power level for the combined RF signal output from the Diplexer **540** (FIG. **30a**) to the antenna **550**. More particularly, the graph illustrates the spectral occupancy of the radiated emissions from the antenna **550** because U.S. Federal Communications Commission requires out-of-band emission for MMDS boosters to be 60 dB down from the average power spectral density at band edge 2.5 GHz and 60 dB down at 2.707 GHz relative to the 2.686 GHz band edge. Without the diplexer **540** (FIG. **30a**) emissions from the MMDS transmitters **520** and output coupler **500** would exceed the FCC spectra occupancy requirements, primarily due to intermodulation products generated in the signal combining process. The intermodulation emissions problem is seen in FIG. **31** where output emissions at frequency 2,497 GHz are greater than the -60 dB requirement. Furthermore the emissions at 2.707 GHz are above the -60 dB requirement.

FIG. **32** shows the spectral occupancy of the combined MDS and ITFS/MMDS/OFS energy when the diplexer **540** is used to filter and combine the MDS energy with the ITFS/MMDS/OFS energy. As seen in FIG. **32**, the spectral occupancy at 2.497 GHz is about 64 dB below the average power spectral density at the 2.5 GHz band edge. Similarly, the spectral occupancy at 2.707 GHz is about 64 dB down from the average power spectral density at the 2.686 GHz band edge. Thus, the independent bandpass filtering of the MDS RF energy and the independent bandpass filtering of the ITFS/MMDS/OFS energy respectively provided by the diplexer **540** brings the combined output signal of the modular broadband booster system **100** within the FCC requirements.

FIG. **33** describes the redundant system controller **200** (FIG. **5A**) and its interconnection with the GNET serial bus

**175**, the user interface **205**, the system monitored signals **210**, and the system control signals **200**. The redundant system controller **200** includes a first system controller **1 200<sub>1</sub>** which includes a Motorola MC68HC11F4FN microcontroller-based circuit board. A system controller **2 200<sub>2</sub>** is identical in construction to system controller **1 200<sub>1</sub>** although for cost or time-to-market reasons, only one system controller may be used. An arbitration logic block **212**, which is implemented in a programmable array logic (PLA), is equipped with software switchable I/O functions and communicates with both the system controller **1 200<sub>1</sub>** and the system controller **2 200<sub>2</sub>** as a slave controller), or assigns the system controller **2 200<sub>2</sub>** initially as the master (and thus system controller **1 200<sub>1</sub>** as the slave). Assuming, for example, that the system controller **1 200<sub>1</sub>** is initially assigned by the arbitration logic **212** as the master controller, the system controller **1 200<sub>1</sub>** will control the GNET serial bus **175** and thus all message traffic over the GNET serial bus **175** will pass through and be controlled by the system controller **1 200<sub>1</sub>**. Under these conditions, the system controller **2 200<sub>2</sub>**, acting as a slave, will continually monitor the "health" of the system controller **1 200<sub>1</sub>** via the arbitration logic **212** and the GNET serial bus **175** in order to determine if the system controller **1 200<sub>1</sub>** is functioning properly. If the system controller **2 200<sub>2</sub>** determines that the system controller **1 200<sub>1</sub>** is not functioning properly, the system controller **2 200<sub>2</sub>** will revolt (in a similar manner that which was discussed in reference to FIG. **9A** for the driver **115** and the driver **120**) and send a control signal through the arbitration logic **212** which will set a software switch in the arbitration logic **212**, thereby reassigning the master and slave status of the respective system controllers **200<sub>1-2</sub>**.

Even though the respective system controllers **200<sub>1-2</sub>** automatically detect and switch respective master and slave roles, a manual override **213** allows an operator or a remote network management system to positively assign the respective master and slave roles of the system controllers **200<sub>1-2</sub>**. The manual override function can be performed over the GNET serial bus **175** or through a front panel data input device **209** which is part of the user interface **205**. An operator local to the modular broadband transmission system **100** can assert the master and slave status by observing a front panel display **207**, which is part of the user interface **205**, and informs the user of the relative roles and health of the system controllers **200<sub>1-2</sub>**.

Each of the system controllers **200<sub>1-2</sub>** has access to respective data acquisition devices **211<sub>1-2</sub>** which include a DAC circuits, an A/D circuit, memory and a level shifting circuit. The respective data acquisition circuits **211<sub>1-2</sub>** connect to a system controller local bus **206** which in turn connects to the front panel **205**, a set of system monitored signals **210**, as well as a set of system control signals **202**. The connection of the data acquisition devices **211<sub>1-2</sub>** to the user interface **205** permits the redundant system controller **200** to both accept input from a user, via the front panel data input device **209**, but also can display information on a front panel display that is a liquid crystal display. Each of the respective data acquisition devices **211<sub>1-2</sub>** receive system monitored signals **210** which include signals such as status of doors and system **100**, thermal status of the booster system **100**, ON/OFF states of the fans, a functional status of the main AC rectifier circuit **702**, a functional status of an auxiliary AC/DC converter **701**, health and status signals regarding the respective drivers (**115** and **120**), etc. Based on each of these received monitored signals **210**, the redundant system controller **200** issues text and graphics-based message displays to be displayed on the front panel display **207**.



and will set appropriate flags in a MIB. Furthermore, based on the system monitored signals **210**, the redundant system controller **200** will issue appropriate system control signals **202** in order to provide power on/power off, hot standby, sound audible alarms, as well as other control signals.

FIG. **34** illustrates in more detail the slave controller and system I/O interface (personal computer) **250** and the user interface **255** (a-d) shown earlier in FIG. **5A**. Alternatively, the slave controller and system I/O interface **250** may be adapted perform the functions of one of the redundant system controllers **200**. The slave controller and system I/O interface **250** is a personal computer of a Packard Bell 120 MHz Pentium<sup>SM</sup> type using the Microsoft Windows NT operating system software. A CRT display **255a** displays data output from the slave controller and system I/O interface **250** (although other displays such as LCD displays, plasma displays and other displays may be used). Data is input by a local user by a mouse **255c**, a keyboard **255e**, a local area network **255d**, which is a Novell Ethernet or other local connection such as a USB or fire wire connection. The slave controller and system I/O interface **250** also connects to the GNET serial bus **175**, but serves as the "slave" on the GNET serial bus **175** because the GNET bus **175** recognizes only one master at a time, and the redundant system controller **200** (FIG. **5A**) is the master. However, the slave controller and system I/O interface **250** is the primary external interface of the modular broadband booster system **100** (FIG. **5A**), and thus, communicates with external sources through the PSTN **260** and the remote network **265** (a SNMP compliant network connecting to an Internet), although other networks such as wireless networks, cellular networks, ASDL networks, etc. may be used as well.

The slave controller and system I/O interface **250** serves as the primary system interface to the MMDS network management central facility (network manager) connected through the network **265**. The network manager is centrally located at the main transmitter **1** (FIG. **1**), operated by the MMDS service provider, and manages a number of modular broadband booster systems as part of an MMDS distribution network. The network manager is SNMP compliant such that SNMP "GET", "SET", "TRAP" messaging conventions are supported.

The slave controller and system I/O interface **250** manages the MIB for the modular broadband message booster system **100** (FIG. **5A**). The MIS maintains selected status information about the modular broadband message booster system **100** (FIG. **5A**) which is used by the MMDS network manager to remotely monitor and control the operation of the modular broadband message booster system **100** (FIG. **5A**).

An enterprise portion of a MIB employed by the modular broadband booster system (MBBS) **100** (FIG. **5A**) defines a superior object class "Comwave\_Transmitter" which includes the attributes "Name" and "IPaddress". An example attribute value corresponding to the attributes to the superior object class "Comwave\_Transmitter" would be "Name=MBBS1" which refers to a specific modular broadband booster system **100** that is part of the MMDS distribution network.

Subobject classes for the above identified superior object class "Transmitter" of the MIB include the following:

- Master;
- Slice;
- MDS;
- System Alarms;
- Drivers;

Coupler; and

Power Supply.

Each of the above-identified subobject classes inherits the attributes of the superior object class

5 "Comwave\_Transmitter".

Attributes of the "Master" subobject class with attribute values include:

Maddr=<address of the master>

Failure detected=<description of failure>

10 My\_Mn=Master yes/Master no; and

Status=ON/OFF.

The above attributes within the above subobject class "Master" allows the network manager to remotely detect and correct failures in the redundant system controller **200** (FIG. **5A**), as well as control master/slave status.

Attributes of the "Slice" subobject class with example attribute values include:

Saddr=<address of the slice>

20 Failure detected=<description of failure>

Status=ON/OFF/hot standby/cold standby/transmit/reset;

VDDtolerance= $VDD \leq 10.5/VDD \geq 10.5/VDD = 10.5$ ;

IDS#low=IDS\_1\_low/ . . . /IDS\_8\_high;

25 IDS#high=IDS\_1\_high/ . . . /IDS\_8\_high;

PS reset=yes/no

OV fault=<description of fault>

PSstatus=enable/disable;

30 ISC fault=<description of fault>

PWM=increase/decrease;

VGS#MonLow=VGS1MONlow/ . . . /VGS8MONlow;

VGS#MonHigh=VGS1MONhigh/ . . . /VGS8MONhigh;

35 VGS#IncrUp=VGS1incrementup/ . . . /VGS8incrementup;

VGS#IncrDown=VGS1incrementdown/ . . . /VGS8increment down;

VDS#PSLow=VDS1/ . . . /VDS8;

40 VDS#PSHigh=VDS1/ . . . /VDS8;

RefPStatus=low/normal/high; and

ForPStatus=low/high.

The above attributes within the above subobject class "Slice" allows the network manager to remotely control the ON/OFF status of individual slices (i.e., PA modules) as well placing an individual slice in a hot standby state or a cold standby state, a transmit state or receive state. In addition, the network manager will have access to the following status values within a given PA slice, VDD, IDS, reflected power and forward power, and various power supply fault signals and power supply PWM signals. In addition, each of the attributes for the object class "Slice" will allow the network manager to monitor and control each of the respective GaAs FET amplifiers used in the RF amplifier module **375** (FIG. **16**).

The subobject class "MDS" will include the following attributes with attribute values:

MDSaddr=<address of MDS>; and

60 Status=ON/OFF/standby/health.

The above-identified attributes will allow the network manager to remotely monitor and control each of the two MDS transmitters **520** (FIG. **5A**). Furthermore, the network manager will be able to monitor the health and status of the respective MDS transmitters.

The subobject class "System\_Alarms" includes the following attributes with attribute values:



ThermalAlarm=high/low;  
 System overtemp=<temperature of system>;  
 FanStatus=ON/OFF; and  
 OpenDoor=Yes/No.

The above-identified attributes of the subobject class “System\_Alarms” allows a network manager to remotely monitor various system features including thermal overtemp conditions and sounding alarms therefore, notifying operators of the operational ON/OFF status of a system fan, and an open door condition.

The “Drivers” subobject class of the MIB includes the following attributes with attribute values:

Daddr=<address of driver>;  
 Master=Yes/No;  
 For.P=high/normal/low;  
 Power=increment/decrement;  
 RefP=low/normal/high; and  
 Driver=ON/OFF.

The above-identified attributes within the subobject class “Drivers” allows a network manager to individually monitor and alter a respective Master status of the driver modules **115, 120** (FIG. 9A). In addition, the network manager will be able to monitor the forward and reflected powers in increments, the respective driver **115, 120** gains in order to provide appropriate output power for the respective drivers **115, 120**. In addition, the network manager will be able to control an ON and an OFF status of each of the individual drivers **115, 120**.

The subobject class “Coupler” includes the following attributes with attribute values:

RefP=low/normal/high; and  
 ForP=low/normal/high.

The above-identified attributes of the subobject class “Coupler” allow the network manager to monitor and adjust the respective reflected and forward powers as measured at the output of the radial combiner **400** (FIG. 5A).

The subobject class “Power Supply” of the MIB includes the following attributes with attribute values:

MainAddr=<address of main power supply>;  
 AuxAddr=<address of auxiliary power supply>; and  
 Health=<ON/OFF>.

The above-identified attributes of the subobject class “Power Supply” will allow the network manager to remotely monitor and control the health of the respective main AC rectifier circuit **702** (FIG. 25) and auxiliary power supply **701** (FIG. 25).

The slave controller and system I/O interface **250** employs an expert system which gathers and maintains an updated table of the respective attribute values for each attribute in the MIB for the modular broadband booster system **100** (FIG. 5A). Upon detection of an individual failure or detection of an abnormal reading of any of the system monitored signals **210** (FIG. 33), the expert system will alert the slave controller and system I/O interface **250** to initiate an SNMP TRAP signal which will report the detection of a potential failure within the modular broadband booster **100** (FIG. 5A) to the network manager via the network **265**. Unique SNMP TRAP messages will be provided for each of the potential faults or perceived abnormal readings in the modular broadband booster system **100**. By providing unique TRAP messages, the network manager precisely determines the nature of the perceive fault merely by looking at the unique number assigned to the TRAP message.

In response to receiving an SNMP trap message, the network manager issues an SNMP GET signal in order to

retrieve various attribute values that the network manager believes correspond to the reported TRAP message. By employing the expert system to maintain a current table of attribute values for the MIB, the slave controller and system I/O interface **250** is consistently prepared to provide an updated response to the network manager’s SNMP GET request.

The slave controller and system I/O interface **250** is also capable of dispatching, within the modular broadband booster system **100**, a control signal received from the network manager via the network **265** corresponding to whatever values are included in a SNMP SET signal from the network manager. For example, if the network manager detects that a given PA slice **310** has failed, the network manager may issue an SNMP SET message which sets the Slice status attribute to hot standby.

FIG. 35a shows the trap message data structure for reporting messages to the network manager. A trap message data structure **266** includes the following subfields: Trap No., Object Class, Attribute 1=, Attribute 2=, EOM. The Trap No. subfield contains a unique number for each of TRAP message in the vocabulary of the slave controller and system I/O interface **250**. Each unique TRAP message number will correspond to a given perceived problem or a status value within the MIB. The object class, attribute 1=, attribute 2=, subfields are included to successively report the respective values of first and second attributes within a given object class. The EOM subfield reports to the network manager that it marks an end of the TRAP message.

FIG. 35b is an example TRAP message which is assigned a number “000028”. This exemplary TRAP message reports to the network manager that a “reflected power” is reported as being “high” on a “slice” module assigned the “address 7”. Given the information that the PA slice **7** has a reflected power that is high, the network manager could now reasonably conclude that an impedance mismatch has been detected between the given PA slice **310** and the radial combiner **400** (FIG. 5A). In response, the network manager can either defer the system control to the redundant system controller **200** and respective microcontroller **326** on the individual slice, or can take action by issuing a SNMP SET function which may perhaps set PA slice **7** (**310<sub>7</sub>**) in a standby state or an OFF state. Suppose the SNMP network manager chooses to get additional information by polling the MIB and obtaining other system information. Based on the system information, the network manager may make other adjustments to the modular broadband booster system **100** (FIG. 5A) based on other perceived system problems.

The structure of the TRAP messages is defined such that a network manager may instantly be apprised of problems as they arise. Because the issuance of a TRAP message from the modular broadband booster **100** is proactive, the system **100** promptly alerts the network manager of an early problem so that the network manager can adapt its polling scheme from amongst the several booster systems in the MMDS network and provide immediate attention to what the respective modular broadband booster system **100** perceives as a problem.

In order to temporarily cure a problem, the network manager may, for example, decide to reallocate network resources. For example, the network manager may increase transmit power from neighboring modular broadband booster systems **100**, in order to provide coverage to a service area that is typically covered by a modular broadband booster system **100** (FIG. 5A) that is down for maintenance. While conventional receivers **2** (FIG. 1) would not benefit from the increased transmit power from the neigh-



boring booster system **100** (FIG. 5A) because of the spatial isolation offered by the high-gain antenna employed by the receiver **2**, receivers **2** that are configured to provide diversity reception of a plurality transmit sources would benefit from the neighboring broadcasts. Because of the modular architecture and graceful degradation characteristics of the modular broadband booster system **100**, the network manager may compensate for reduced power conditions at adjacent booster sites by reallocating the respective output powers of individual ones of the broadband booster system **100**.

FIG. 36 illustrates an exemplary process flow diagram employed by a network manager as part of an MMDS network **265** (FIG. 5A) in order to dynamically control network resources. The specific example process flow set forth in FIG. 36 illustrates how a plurality of modular broadband booster systems **100** may be dynamically controlled and reconfigured by a central network management controller (or even self controlled amongst the several ones of modular broadband booster systems **100**) such that service areas will not be affected in the event any particular one of the plurality of modular broadband booster systems **100** detects a fault that will limit its output power. The process begins in step **S40** when the network manager via network **265** (FIG. 5A) receives a TRAP message from a first modular broadband booster system **100**. Once received, the process flows to step **S41** where the network manager in network **265** dispatches a SNMP GET message to the first modular broadband booster system **100** in order to retrieve the status data in the MIB of the first modular booster **100**. The process then flows to step **42** where the network manager uses the MIB values obtained via the SNMP GET message in order to determine an appropriate response to the initial TRAP message from the first modular booster. Once an appropriate response is determined, the process flows to step **43** where the network manager queries whether the determined appropriate response will effect coverage to a respective service area covered by the first modular booster. If the response to the inquiry in step **S43** is negative, the process flows to step **S46** where the network manager issues the earlier determined appropriate response to the first modular booster; however, if the response to the inquiry in step **43** is affirmative, the process flows to step **S44** where the network manager queries whether a second modular booster is present such that an increase in the effective radiated power from the second modular booster (perhaps because the second modular booster has some spare PA slices that are either off or in hot standby mode) could compensate for the decrease in coverage area from the first modular booster. If the response to the inquiry in step **S44** is negative, the process flows to step **S46** and the earlier determined appropriate message is dispatched to the first modular booster; however, if the response to the inquiry in step **S44** is affirmative, the network manager issues an SNMP SET message to the second modular booster in order to increase the output power of the second modular booster (perhaps by bringing on-line spare PA slices). By increasing the output power of the second modular booster, no gap in coverage occurs in the effected (or what would have been the effected) area. After the SNMP SET message is sent in step **S45**, the process flows to step **S46** where the earlier determined appropriate message to the first modular booster is dispatched by the network manager.

The process disclosed in FIG. 36, is made possible by the modular architecture of the modular broadband booster system **100** on the presence of a microcontroller module **325** on respective of the PA modules **310**. Because each of the

modular boosters **100** are N-way modular boosters, each modular broadband booster system **100** may reserve selected ones of the N PA slices **310** to be used only in the even when extra service area or coverage area is required. Thus, in normal operations perhaps only 50% of the N PA slices **310** are used, however, when extra service area is required, additional ones of the PA slice modules **310** may be brought on line by the network manager in order to provide seamless coverage within the service area of the network.

FIGS. 37a and 37b respectively show a front view and side view of the component parts of the modular broadband booster system **100**. In FIG. 37a, a rack **900** that is 40 rack units in height (RU, rack unit=1.75 inches) houses the PA slice modules **310**<sub>1-8</sub> in one of the chassis **311a**, the PA slice modules **310**<sub>9-16</sub> in a second of the chassis **311a**, the driver **A 115**, the driver **B 120**, the MDS transmitters **520**, and the main AC rectifier circuit **702** and the auxiliary power supply **701**. In addition, a chimney unit **904** is included in order to exhaust air forced through the rack **900** by the fan **901**.

FIG. 37b is a side view of the rack **900** shown in FIG. 37a. FIG. 37b shows, in addition to the components shown in FIG. 37a include the radial combiner **400**, the semi-rigid lines **401**, the coupler **500**, and the N-way splitter **130**. The chassis **311a** are each of a size 6U. The fan unit **901** of a size 3U. The driver **A 115** and the driver **B 120** are both of a size 4U and the respective 2 MDS transmitters **520** are of a size 8U. The main AC rectifier circuit **702** and auxiliary power supply **701** occupy 9Us.

FIG. 37c is a back view of the PA slices **310**<sub>1-16</sub> and the radial combiner **400** as mounted in the rack **900** (FIGS. 37a and 37b). The PA slices **310**<sub>1-8</sub> are mounted above the PA slices **310**<sub>9-16</sub> in the respective chassis **311a**. Each of the PA slices **310**<sub>9-16</sub> connect to the radial combiner **400** via corresponding semi-rigid lines **401**. In order to support "hot-swapping" of individual PA slices **310**, the lengths of each of the semi-rigid lines **401** are minimized by connecting the outermost PA slices **310** (e.g., PA slices **310**<sub>1</sub>, **310**<sub>8</sub>, **310**<sub>9</sub>, and **310**<sub>16</sub>) with the corresponding semi-rigid lines **401**<sub>1</sub>, **401**<sub>8</sub>, **401**<sub>9</sub>, and **401**<sub>16</sub> to the nearest one of the 16 inputs to the radial combiner **400**. As shown in FIG. 37c, the PA slices **310**<sub>9-16</sub> are positioned "up-side down" with respect to the PA slices **310**<sub>1-8</sub> so that the lengths of semi-rigid lines **401**<sub>9</sub>, and **401**<sub>16</sub> are less than what would be required if the PA slices **310**<sub>9-16</sub> were not mounted up-side down.

#### Second Embodiment

FIG. 38 shows a radio system **1100** which is similar to the modular broadband booster system of the first embodiment although optimized for use as a radio system (RS) (i.e., base station), as an element of a personal communication service (PCS) system. The radio system **1100** is used in a personal access communication system (PACS) PCS system which receives frequencies between 1850.1 MHZ to 1909.9 MHZ and transmits within the band 1930.1 MHZ to 1989.9 MHZ. However, the radio system **1100** may also be used with other PCS systems.

In the PCS system, PCS subscribers **1110** communicate with a RS **1100** (shown in more detail in FIG. 39) over a radio link. The RS **1100** receives incoming messages from individual PCS subscribers **1110** and passes them to a switch center **1105**. This switch center then routes the given messages to an appropriate destination location. If the destination location is within the area covered by the RS **1100**, the switch center **1105** will forward the message to the RS **1100** which permits the RS **1100** to establish a broadcast connection to an intended recipient of the original message.

FIG. 39 shows the RS **1100** as used in the PCS system. A receive antenna **1205** is optimized to receive in the fre-



quency band of 1805.1 MHZ to 1909.9 MHZ. Energy coupled to the receive antenna **1205** is forwarded to a low noise amplifier **1104**, which amplifies the coupled energy and forwards it to a receiver **1106**. The receiver **1106** downconverts the received energy and provides an output to a message processor **1107**. The message processor **1107** detects and decodes the received energy in order to reconstruct the original message and then forwards the message to the switch center **1105** for channel assignment. Messages coming from the switching center **1105** are passed to the message processor **1107**. The message processor **1107** then forwards an outgoing channel assignment and control message to a transmitter **1108** which combines the assignment and control message with other outgoing messages and up-converts the composites message to the PCS frequency band based on the respective channel assignments for the outgoing messages.

The transmitter **1108** outputs the composite messages to a driver A **1115** and a driver B **1120**, each optimized for the PCS frequency band. The drivers **1115**, **1120** output the respective signals (depending on which is the Master) to a 1/N power divider. The value N is appropriately selected based on the budget and power demands of the hosting RS facility. If more power is required, the value N is increased or if less power is required, the value of N is decreased. The output of the 1/N power divider **1130** is provided to a modular power amplifier **1300** which contains at least N PA slice modules **310**, each optimized for use in the PCS band. The modular power amplifier **1300** outputs a corresponding set of N amplified signals via lines **1401** to a radial combiner **1400** which combines the N amplified signals. The respective size of the lines **1401** and radial combiner **1400** are adjusted to be optimized for the PCS band. The radial combiner **1400** outputs a single summed output through line **1402** (optimized for the PCS band) to an output coupler **1500** which is optimized for the PCS band. The output coupler then outputs the RF energy into a transmit antenna **1550** which is optimized for the PCS band.

A network **1175** interconnects the respective drivers **1115**, **1120**, the modular power amplifier **1300**, and the output coupler **1500**. The network **1175** operates under control of the control device **1118** which provides similar features to the redundant system controller **200**, and the slave controller I/O **250** with their corresponding user interfaces **205**, **255** of the first embodiment.

#### Third Embodiment

FIG. **40** illustrates a third embodiment of the invention which is directed to a modular broadband head-end transmitter having a first modular broadband head-end transmitter **2220a** combined with a second modular broadband head end transmitter **2220b**. Each of the respective broadband head-end transmitters **2220** receives 16 separate MMDS channels (or more generally N) from a baseband channel source **2400**. The baseband channel source **2400** provides the separate MMDS channels to each of the respective modular broadband head-end transmitters **2220**. Each of the respective modular broadband head-end transmitters **2220** employs a 16-way up-convert and channelizing device **2300**, which maintains isolation between the respective input signals while simultaneously up-converting each of the signals to a separate MMDS channel. The output of the 16-way (N-way) up-convert and channelizing device **2300** is provided on 16 (N) separate lines, each feeding a separate PA slice **310** (see FIG. **5A**) which independently amplifies each of the 16 (N) channels and outputs the respective output on one of 16 (N) channels semi-rigid lines **401**. Each of the semi-rigid lines **401** feeds an independent port of the radial

combiner **400** which combines the separate amplified RF signals into a single output **402**, and subsequently provided to the output coupler **500**. A directional coupler output **2160** monitors the output signal and feeds a forward and a reflected power signal to the redundant system controller **200**.

Sixteen (N) other channels are processed in a similar manner through the modular broadband head end transmitter **2220b**.

The respective outputs of the modular broadband head-end transmitters **2220a** and **2220b** are provided to a diplexer **2340** which is optimized for the MMDS frequency band. The diplexer **2340** provides a single output to the transmit antenna **550**.

#### Fourth Embodiment

FIG. **41** shows a reconfigurable head-end transmit system **3100** that includes a baseband channel source **2400** and a reconfigurable modularized transmit system **3220**. Under control of a redundant system controller **200**, a selective up-converter **3300** accepts a set of M inputs (where M can be as small as 1) from the baseband channel source **2400** and up-converts a selected set of R of the signals to the specific channels based on control signals from the redundant system controller to be broadcast from the output antenna **550**. Once each of the selected R signals is up-converted to its appropriate channel, the R signals are output to an R×N ("R by N") combiner selector circuit **3400**, which is connected to the GNET serial bus **175** and controlled by the redundant system controller **200**. The R×N combiner selector **3400** appropriately combines or divides the respective R signals to produce N outputs. Although the operator can adjust a number of separate power amplifier paths through which an individual signal will pass, normally, if R is less than N, the operator will designate which of the R signals is to be broadcast at a higher power than the other channels. Suppose the operator selects a "signal 1" of the R signals to be broadcast at a higher power than the other signals, the signal 1 will be divided and power scaled within the R×N combiner selector **3400** and passed through two separate amplification paths within the modular power amplifier **1300**. Thus the signal 1 will be transmitted at twice the power (3 dB) than the other signals. When the value R is equal to N, each of the respective R signals is amplified to a common level. When the value R is greater than the value N, the redundant system controller determines which of the R signals will be paired with one another and passed through an individual one of the N amplification paths in the modular power amplifier **1300**. Each signal that is paired with another signal and passed through one path of the modular power amplifier **1300** will be broadcast with less effective radiative power than a signal that was not paired with another signal.

#### Fifth Embodiment

FIG. **42A** illustrates a fifth embodiment of the present invention where the reconfigurable head-end transmit system **3220** of the fourth embodiment is combined with the baseband channel source **2400** and diplexer **2540** of the third embodiment. The baseband channel source **2400** provides M signals to the reconfigurable head-end transmit system **3220a** and a different M signals to the reconfigurable head-end transmit system **3220b**. Under control of the respective redundant system controllers **200** (FIG. **41**), a selected set of R of the M signals are combined and/or selected with one another in order to form N respective signal paths through each of the reconfigurable transmit system **3220**. Each of the signal paths is independently amplified and output through the reconfigurable head-end transmit system **3220** and provided to the diplexer **2540** which filters and combines the



respective outputs of the reconfigurable transmit systems **3220** and provides a single input to the transmit antenna **550**.

While the two reconfigurable head-end transmit systems **3220a** and **3220b** are shown in FIG. **42**, other reconfigurable head-end transmit systems could be included as well in order for individual ones of the selected input signals to be broadcast from the output antenna **550** with a greater effective radiated power. One such example of this latter configuration is shown in FIG. **42B**, where the baseband channel source **2400** provides a single channel (which may carry, for example, between 1 to 6 digital programs) to a reconfigurable transmit system **3220c**. The reconfigurable transmit system **3220** optionally includes the R×N combiner selector **3400** and the diplexer **2540**, for example, and other components (e.g., redundant system controller **200**, slave controller and I/O **250**) that are not necessary for head end operation. PA Slice fault detection may be performed at the module level and communication of the detected fault may be achieved by a “wired OR” reporting scheme as monitored by driver controller **131** (FIG. **8**). Once one of the PA Slices reports a fault condition, the driver controller **131** issues a fault detection message, and a technician may then identify the location of the failed PA Slice module by observing which of the N PA Slice modules has an illuminated LED on its front panel.

A benefit with the structure shown in FIG. **42B** is that a head end operator may configure the system to broadcast a single channel at a desired power level simply by adding the appropriate number of PA slice modules to the modular power amplifier. As with the other embodiments, this simplified architecture offers (1) graceful degradation when one or more PA slice modules fail, (2) “hot swap” capability, and (3) a defined upgrade path if more than one channels are later to be transmitted from the head end transmitter. Similarly, the simplified architecture of FIG. **42B** is reconfigurable to allow for a change in desired output power according to a change in concept of operations for the subject head end transmit facility. Moreover, the number of PA modules may be increased so as to meet an increase in output power requirements and decreased so as to meet a decrease in output power requirements.

#### Sixth Embodiment

FIG. **43** illustrates an alternative amplifier architecture **6375** that is similar to the RF amplifier module **375** of the first embodiment, but FET amplifiers **6385<sub>5</sub>**, **6385<sub>2</sub>** and **6385<sub>1</sub>** are added to the architecture. Furthermore, a set of amplifiers **6385<sub>1-4</sub>** are of a type 4×FLL **200**, a pair of amplifiers **6385<sub>7-8</sub>** are of the 2×FLL **171** type, and a pair of amplifiers **6385<sub>5-6</sub>** are of the 4×FLL **200** type. While this architecture requires additional amplifiers as compared to the first embodiment, each of the several amplifiers are readily available.

#### Seventh Embodiment

FIG. **44** shows a SPI bus **720** which interconnects each of the respective PA slices **310<sub>1</sub>–310<sub>n</sub>** for sharing data monitoring and control signals between each other. The SPI bus **720** is particularly well suited for each of the microcontroller modules **325** on each of the respective PA slice modules **310<sub>1-n</sub>**. The GNET serial bus **175** also connects to each of the individual PA slices **310<sub>1-n</sub>**, as well as to the MDS transmitters **520**. Separate redundant PA controllers **1** and **2**, **7100<sub>1-2</sub>**, are provided to arbitrate the use of the SPI bus. The redundant PA controller **1** **7100<sub>1</sub>** and the redundant PA controller **2** **7100<sub>2</sub>** will assert master and slave control using the same process described with respect to the redundant system controllers **200** of the first embodiment.

The processes set forth in the present description may be implemented using a conventional general purpose micro-

processor programmed according to the teachings of the present specification, as will be appreciated to those skilled in the relevant art(s). Appropriate software coding can readily be prepared by skilled programmers based on the teachings of the present disclosure, as will also be apparent to those skilled in the relevant art(s).

The present invention thus also includes a computer-based product which may be hosted on a storage medium and include instructions which can be used to program a computer to perform a process in accordance with the present invention. The storage medium can include, but is not limited to, any type of disk including floppy disk, optical disk, CD-ROMS, and magneto-optical disks, ROMS, RAMs, EPROMs, EEPROMs, flash memory, magnetic or optical cards, or any type of media suitable for storing electronic instructions.

Obviously, numerous modifications and variations of the present invention are possible in light of the above teachings. It is therefore to be understood that, within the scope of the appended claims, the invention may be practiced otherwise than as specifically described herein.

What is claimed as new and desired to be secured by Letters Patent of the United States is:

1. A computer implemented high power transmitter controller, comprising:

a processor; and

an interface to a communication link, wherein

said interface is configured to receive message data produced by a high power transmitter, said message data being descriptive of an operational status of the high power transmitter, said processor and said interface being located remotely and in a different facility from said high power transmitter,

said processor is configured to receive said message data and generate a control instruction and send said control instruction to said high power transmitter via said interface so as to control the high power transmitter, and

said high power transmitter is operated at a power level of 12.5 watts or greater.

2. The controller of claim 1, wherein said interface is configured to receive said message data and transmit said control instruction over the Internet.

3. The controller of claim 1, wherein said communication link is a wireless communications link.

4. The controller of claim 1, wherein said communication link is a cellular communications link.

5. The controller of claim 1, wherein said communication link is a telephony communications link.

6. The controller of claim 1, wherein said communication link is an asymmetric digital subscriber line (ADSL) communications link.

7. The controller of claim 1, wherein said controller is configured to remotely control a plurality of high power transmitters over said communications link.

8. The controller of claim 1, wherein said controller comprises a personal computer.

9. The controller of claim 1, wherein said controller comprises a computer work station.

10. The controller of claim 1, wherein said controller is configured to one of remotely turn off said transmitter and remotely place said transmitter in standby mode.

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11. The controller of claim 1, wherein said message data comprises at least one of status information, fault information, sensor information and system related information of said transmitter.

12. The controller of claim 1, wherein said controller is configured to remotely reconfigure said transmitter. 5

13. The controller of claim 1, wherein said controller is configured to at least one of remotely monitor thermal over temperature conditions, remotely sound alarms, remotely notify of an operational status of cooling fan and remotely notify of an open door condition of said transmitter. 10

14. The controller of claim 1, wherein said controller is configured to at least one of remotely monitor an AC rectifier circuit, remotely monitor a power supply, remotely control an AC rectifier circuit, and remotely control a power supply of said transmitter. 15

15. The controller of claim 1, wherein said controller is configured to one of remotely increase power of said transmitter and remotely decrease power of said transmitter.

16. The controller of claim 1, wherein said controller is configured to remotely monitor at least one of VDD, IDS, 20

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reflected power, forward power, power supply fault signals, power supply PWM signals and amplifier gains of said transmitter.

17. The controller of claim 1, wherein said controller is configured to at least one of remotely monitor amplifiers and remotely control amplifiers of said transmitter.

18. The controller of claim 1, wherein said controller is configured to at least one of remotely monitor master and slave status of modules of said transmitter and remotely reconfigure master and slave status of modules of said transmitter.

19. The controller of claim 1, wherein said controller is configured to one of remotely turn on drivers of said transmitter and remotely turn off drivers of said transmitter.

20. The controller of claim 1, wherein said interface is configured to receive said message data and transmit said control instruction using a simple network management protocol (SNMP).

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