US006370908B1

(12) **United States Patent**
James

(10) **Patent No.:** **US 6,370,908 B1**
(45) **Date of Patent:** **Apr. 16, 2002**

(54) **DUAL EVAPORATOR REFRIGERATION UNIT AND THERMAL ENERGY STORAGE UNIT THEREFORE**

(75) Inventor: **Timothy W. James**, Santa Barbara, CA (US)

(73) Assignee: **TES Technology, Inc.**, Ventura, CA (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **09/479,406**

(22) Filed: **Jan. 6, 2000**

Related U.S. Application Data

(60) Provisional application No. 60/047,064, filed on May 17, 1997, and provisional application No. 60/030,308, filed on Nov. 5, 1996.

(51) **Int. Cl.**[7] **F25D 17/02**
(52) **U.S. Cl.** **62/434**; 62/199; 165/104.11
(58) **Field of Search** 62/434, 430, 436, 62/439, 199; 165/104.11

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,641,109 A 6/1953 Muffly
2,763,132 A 9/1956 Jue
2,960,840 A 11/1960 Hosken et al.
3,537,274 A 11/1970 Tilney
4,122,892 A 10/1978 Delaporte
4,220,196 A 9/1980 Gawron et al.
4,341,262 A 7/1982 Alspaugh
4,416,119 A 11/1983 Wilson et al.
4,439,998 A 4/1984 Horvay et al.
4,474,026 A * 10/1984 Mochizuki et al. 62/157
4,494,382 A 1/1985 Raymond
4,655,050 A 4/1987 Aschberger
4,691,527 A * 9/1987 Ikeda 62/234
4,712,387 A 12/1987 James et al.
4,756,164 A 7/1988 James et al.
4,760,707 A 8/1988 Dennis et al.
4,779,425 A * 10/1988 Yoshihisa et al. 62/199
4,873,837 A 10/1989 Murray
4,910,972 A 3/1990 Jaster
4,918,942 A 4/1990 Jaster
4,928,493 A 5/1990 Gilbertson et al.
4,966,010 A 10/1990 Jaster et al.
5,056,328 A 10/1991 Jaster et al.
5,092,138 A 3/1992 Radermacher et al.
5,105,632 A 4/1992 Naruse
5,109,678 A 5/1992 Jaster et al.

(List continued on next page.)

FOREIGN PATENT DOCUMENTS

DE	1266770	7/1960
DE	3636254 A1	10/1986
EP	0109043 A1	11/1983
GB	2194651 A	3/1988
JP	60-175996	9/1985

OTHER PUBLICATIONS

Joe Minick, The Cold, Jun. 1995, pp. 54–62, Cruising World.

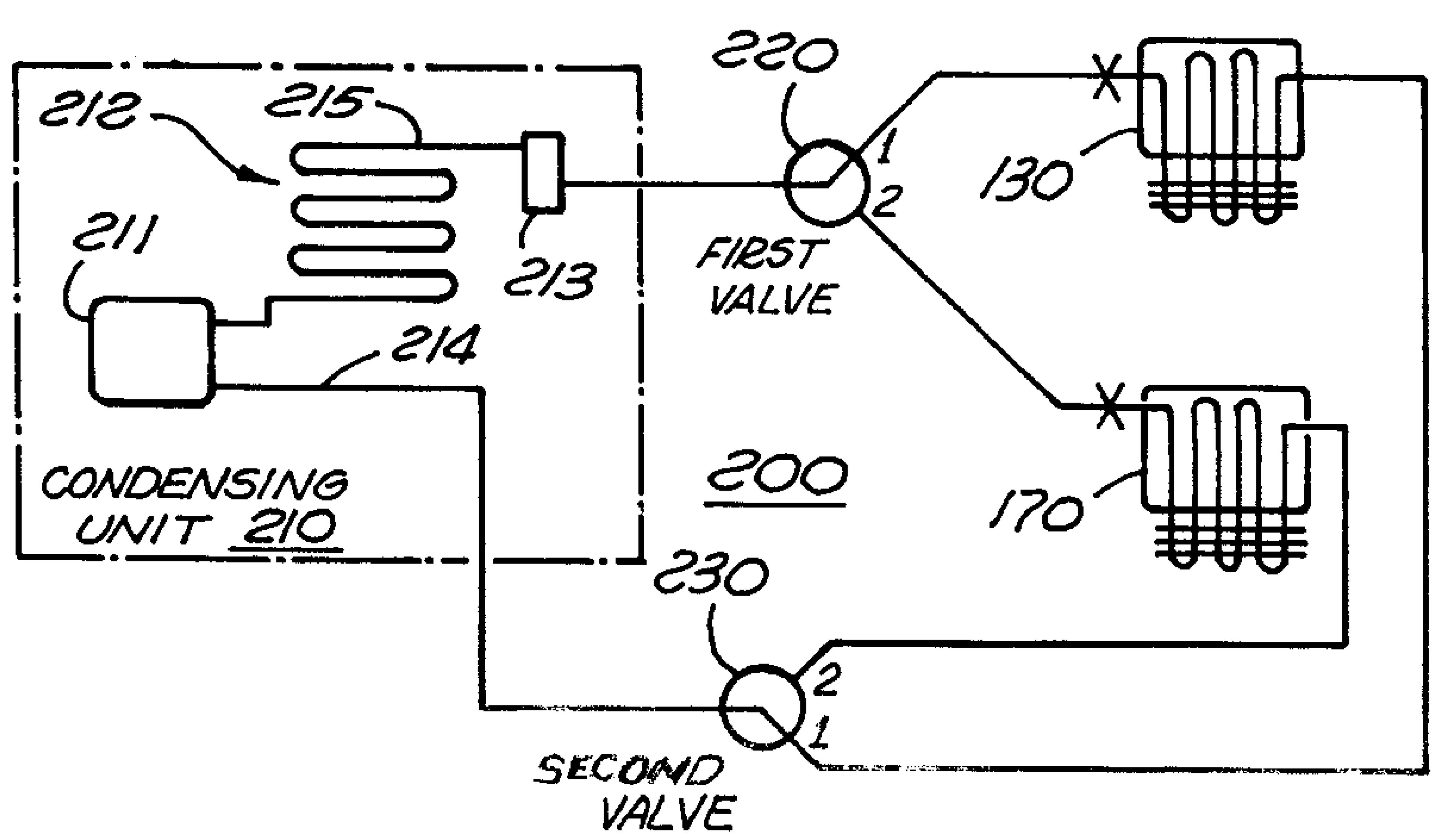
Enegess, Paquette and Elsherif; Spent Regenerant Processing System; Oct. 1975; 939 Official Gazette 8; T939,005.

Primary Examiner—Henry Bennett
Assistant Examiner—Melvin Jones
(74) *Attorney, Agent, or Firm*—Blakely, Sokoloff, Taylor & Zafman LLP

(57) **ABSTRACT**

A low-cost and thermodynamically efficient implementation of a two-stage refrigeration system applied to a retail refrigerator. The invention includes a simple and easily manufactured thermally efficient and low-cost evaporation unit. The invention further includes a thermal energy storage module and an energy efficient control protocol to maintain steady temperatures in the fresh and frozen food sections, to permit energy efficient defrosting of the heat exchange surfaces in the freezer section, and minimize losses associated with condensing unit on-and-off cycling.

18 Claims, 9 Drawing Sheets



U.S. PATENT DOCUMENTS

5,150,583	A	9/1992	Jaster et al.
5,207,077	A	5/1993	Radermacher et al.
5,220,806	A	6/1993	Jaster et al.
5,239,839	A	8/1993	James
5,431,026	A	6/1995	Jaster
5,465,591	A	11/1995	Cur et al.
5,524,453	A	6/1996	James

* cited by examiner

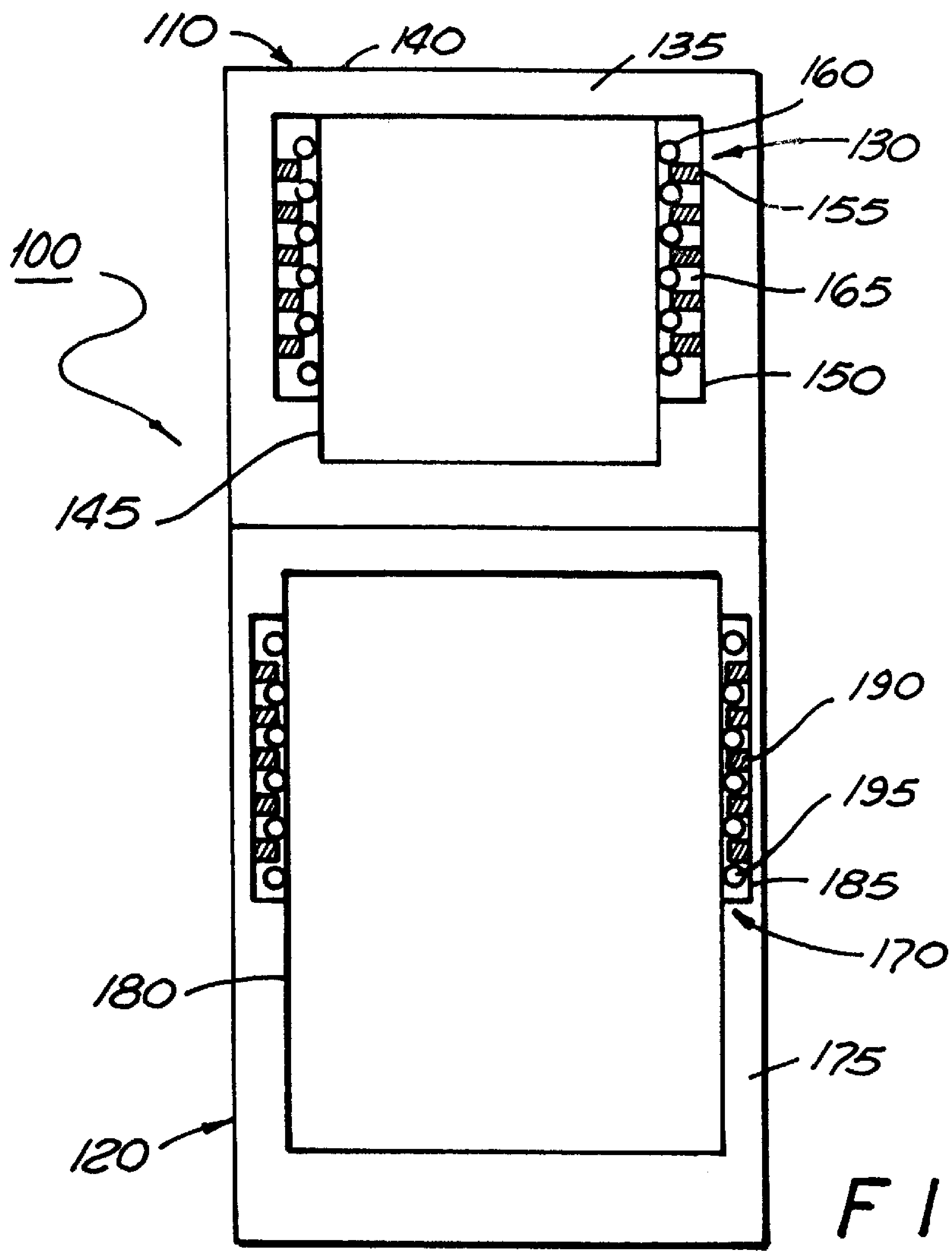

110
140
135
160
130
155
100
165
150
145
190
195
185
170
180
175
120

FIG. 1

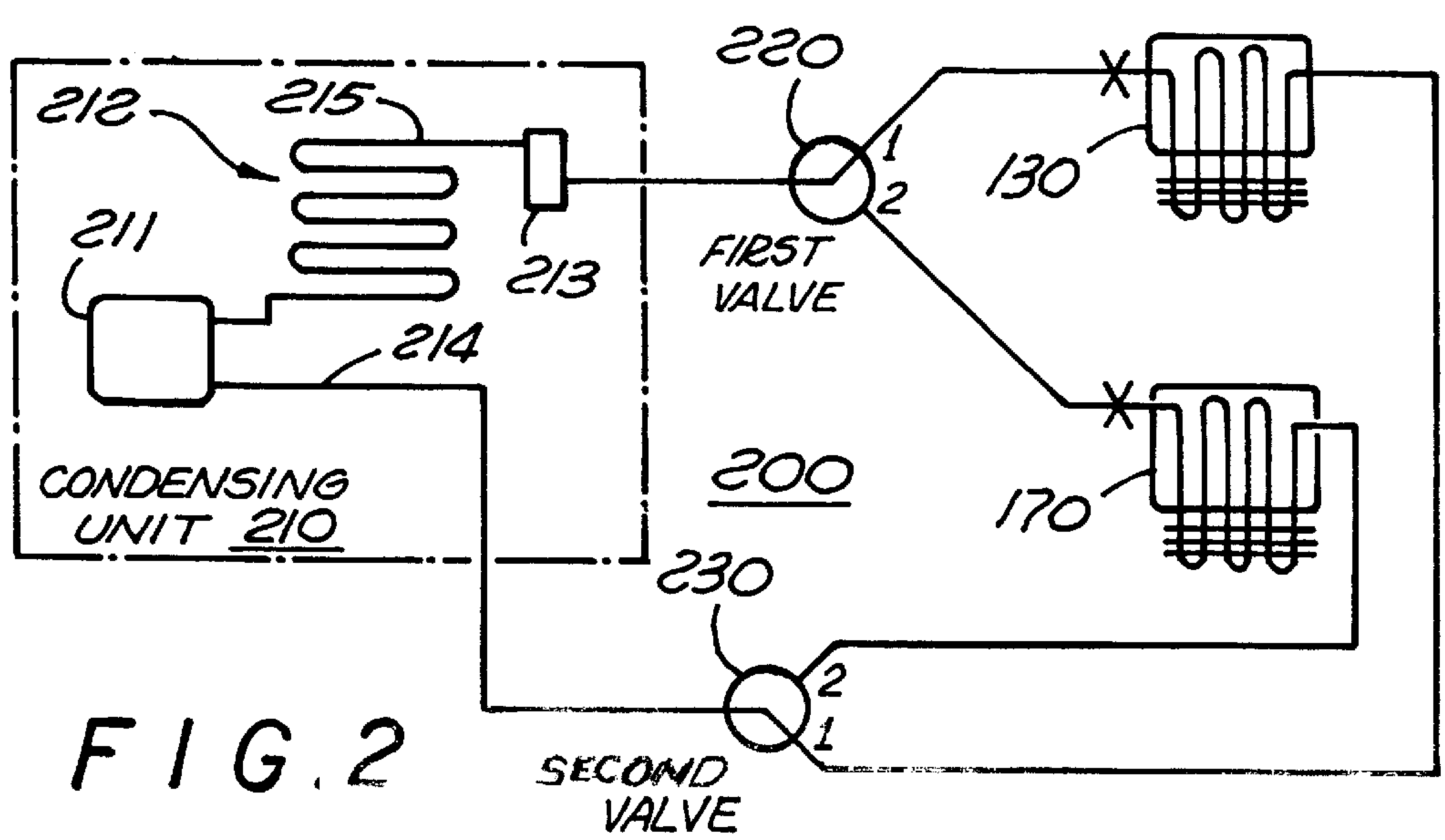

212
215
220
211
213
214
130
FIRST VALVE
1
2
CONDENSING UNIT 210
200
170
230
2
1
SECOND VALVE

FIG. 2

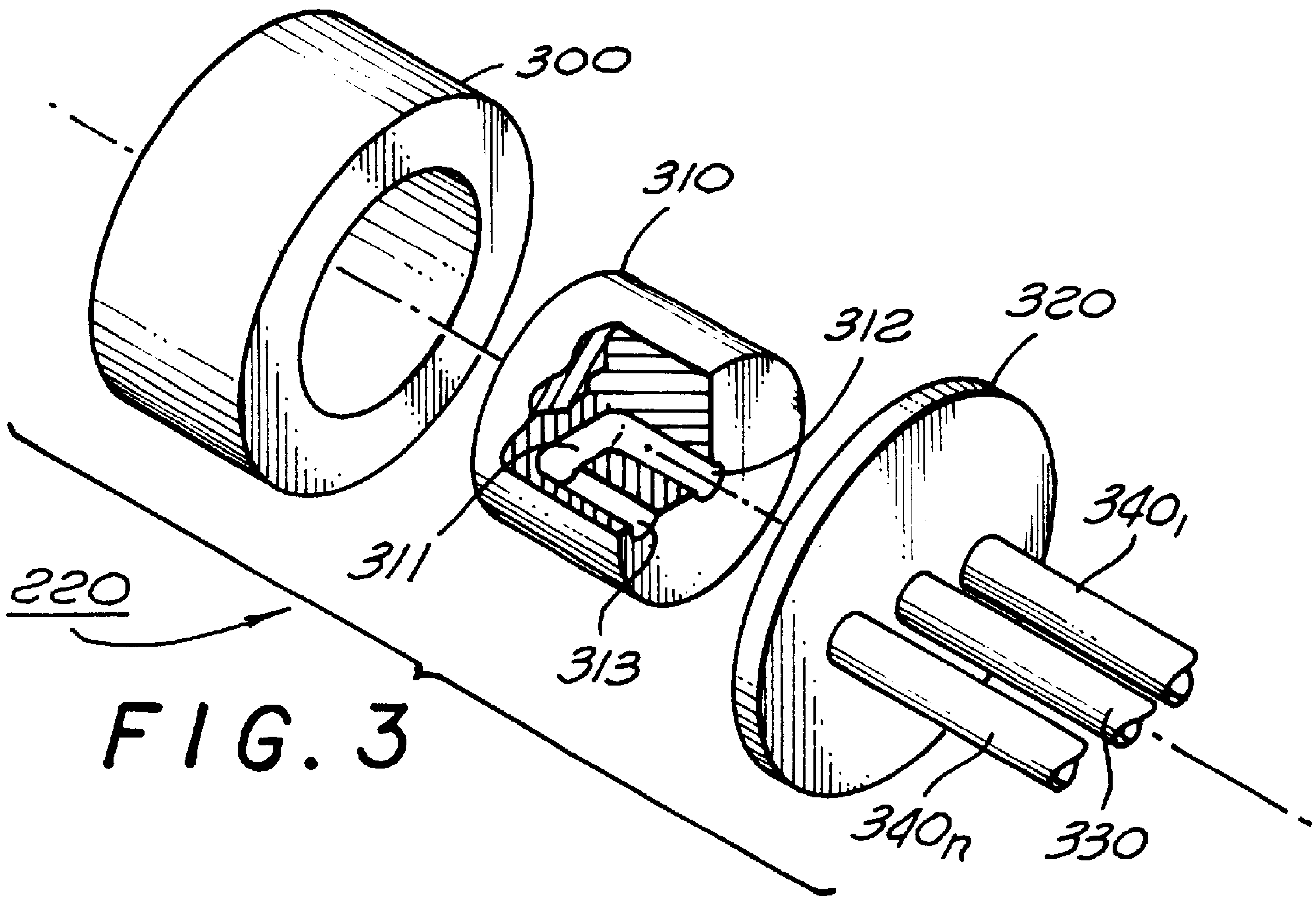

300
310
312
320
311
313
220
340₁
340n
330

FIG. 3

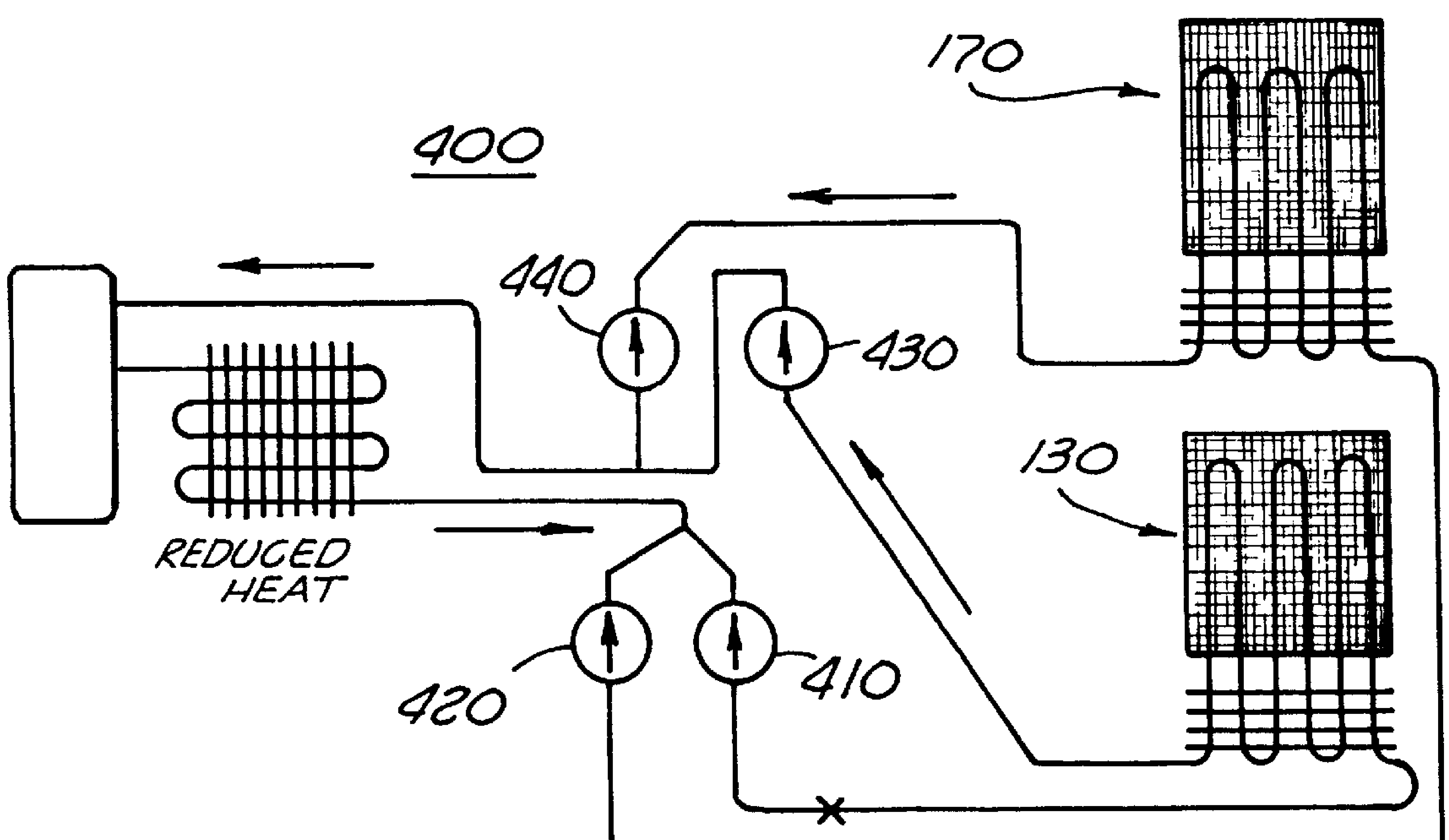

170
400
440
430
130
REDUCED HEAT
420
410

FIG. 4A

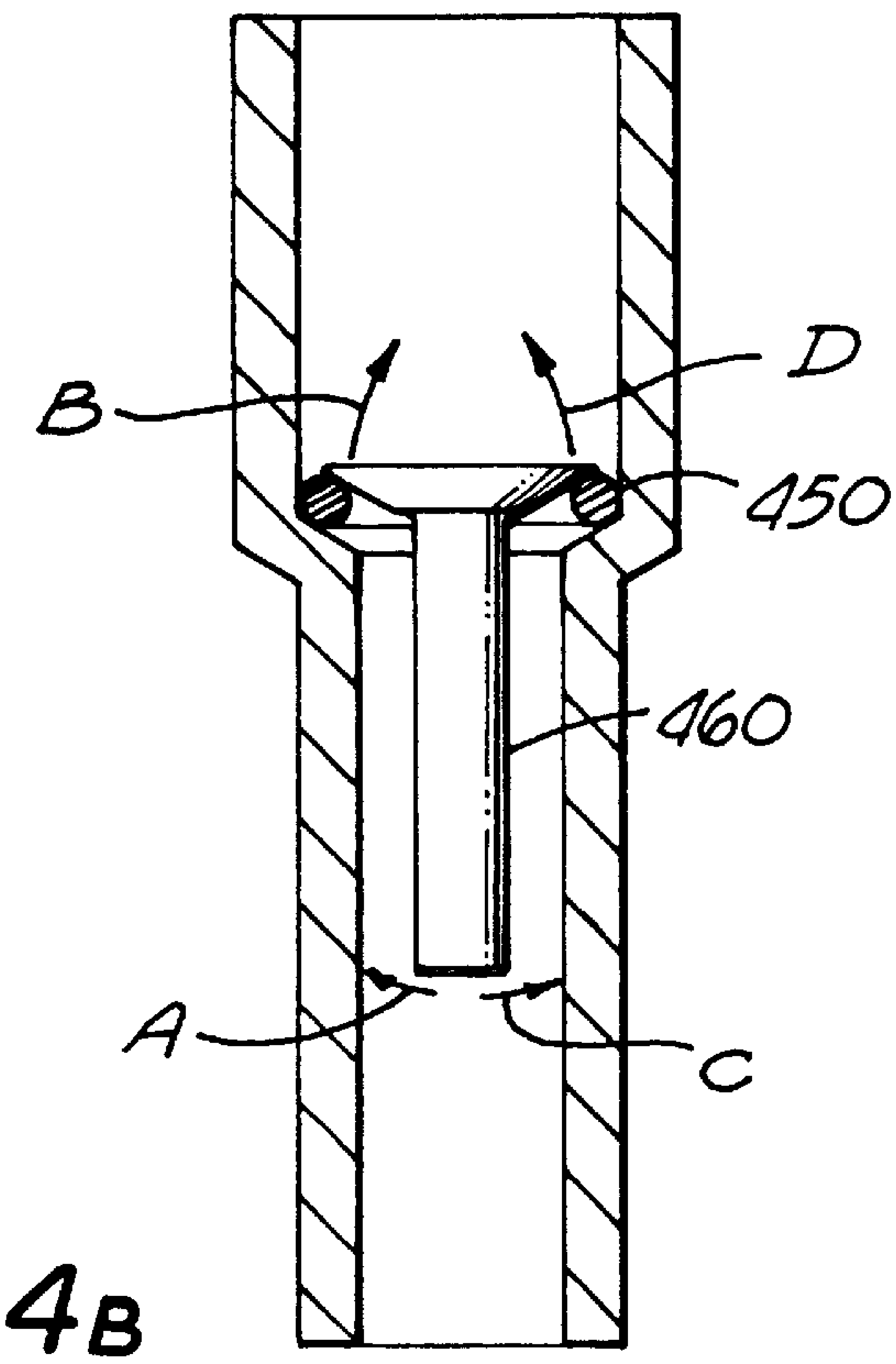


FIG. 4B

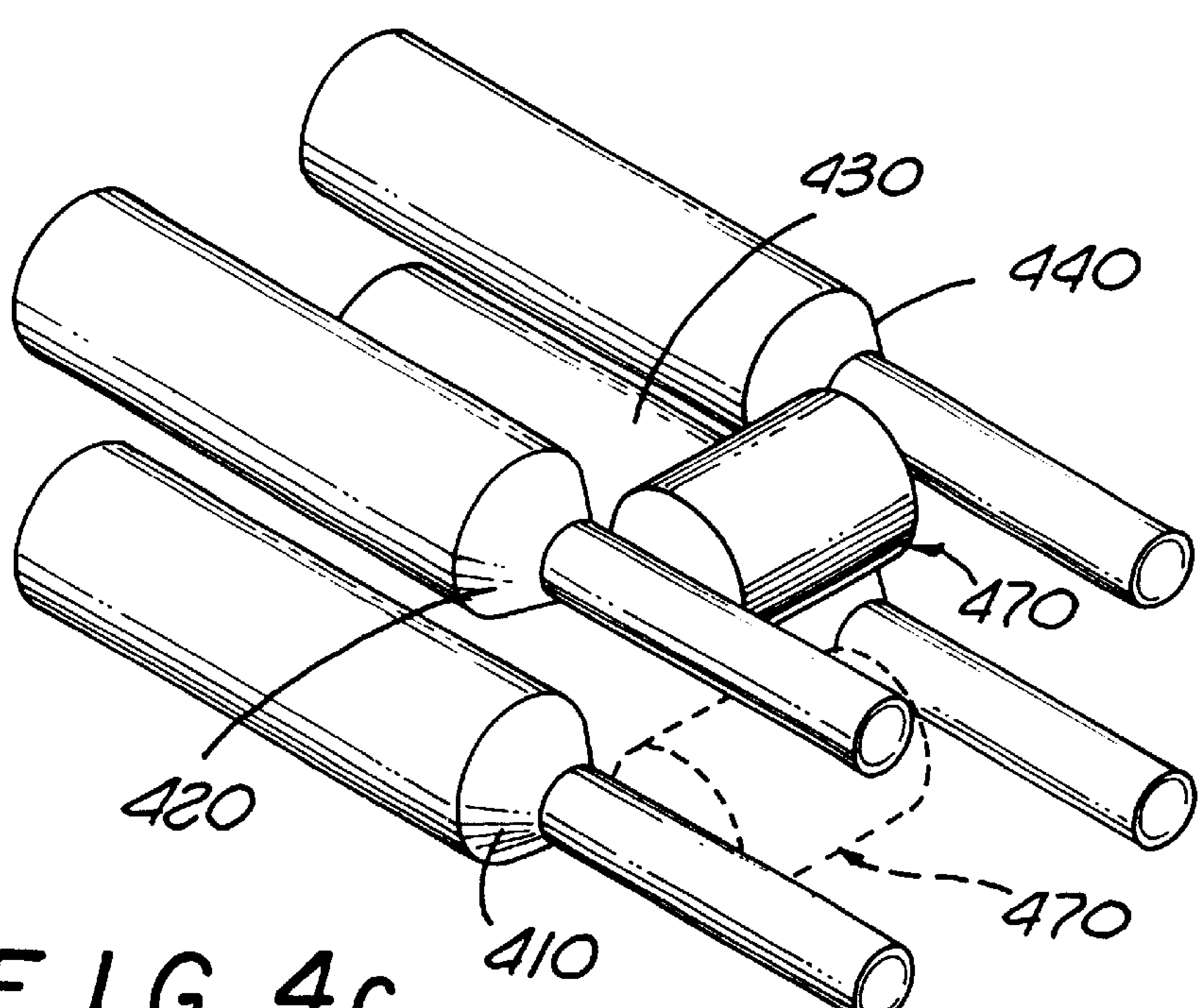


FIG. 4C

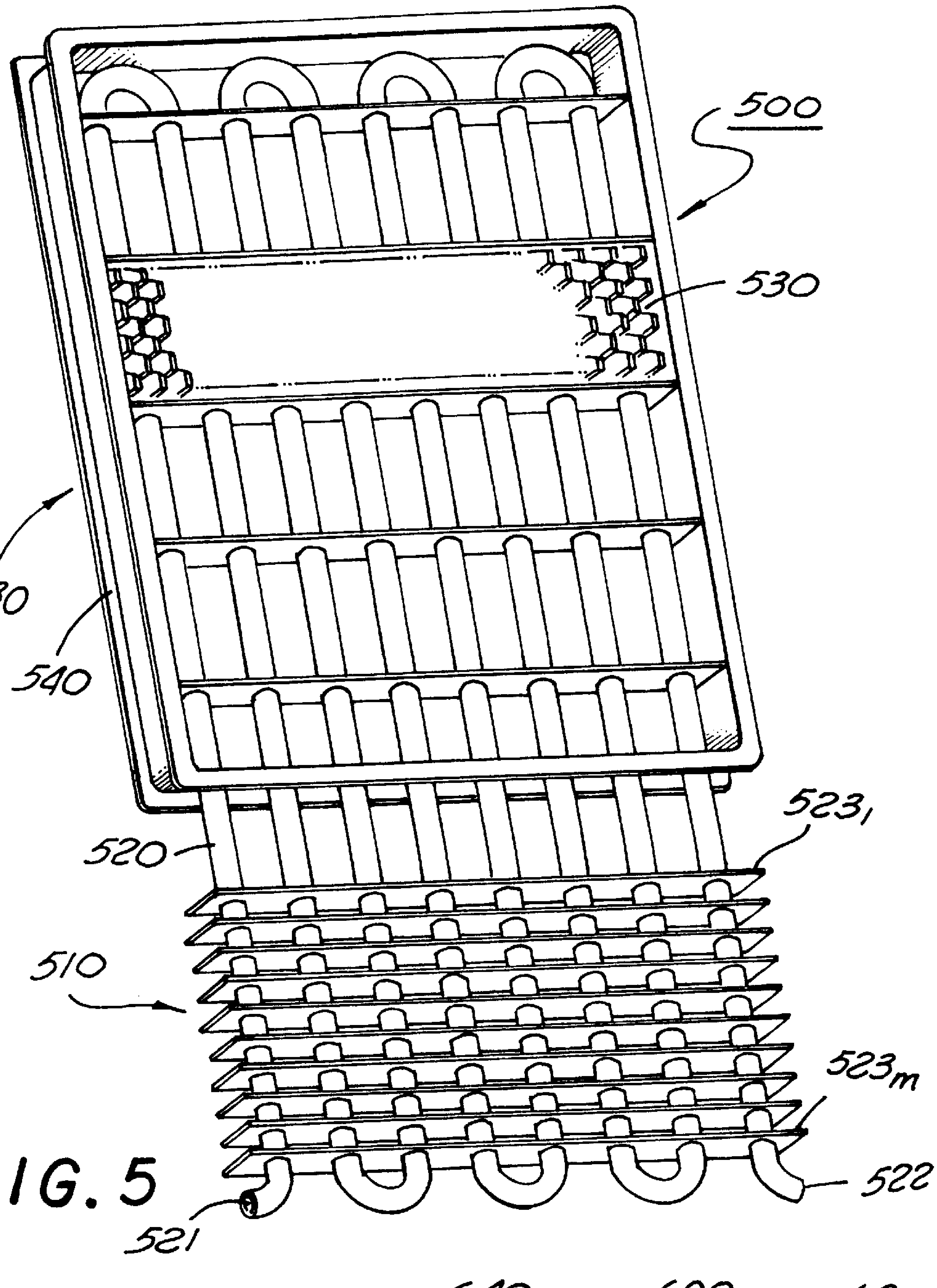

500
530
130
540
520
523₁
510
523m
522
521

FIG. 5

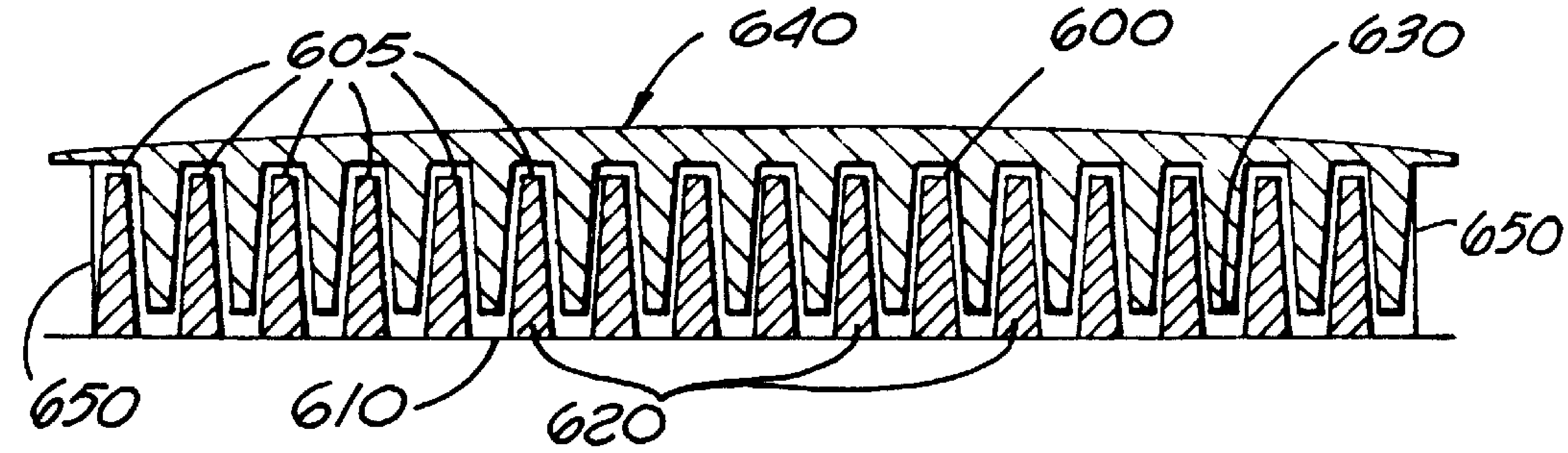

605
640
600
630
650
650
610
620

FIG. 6

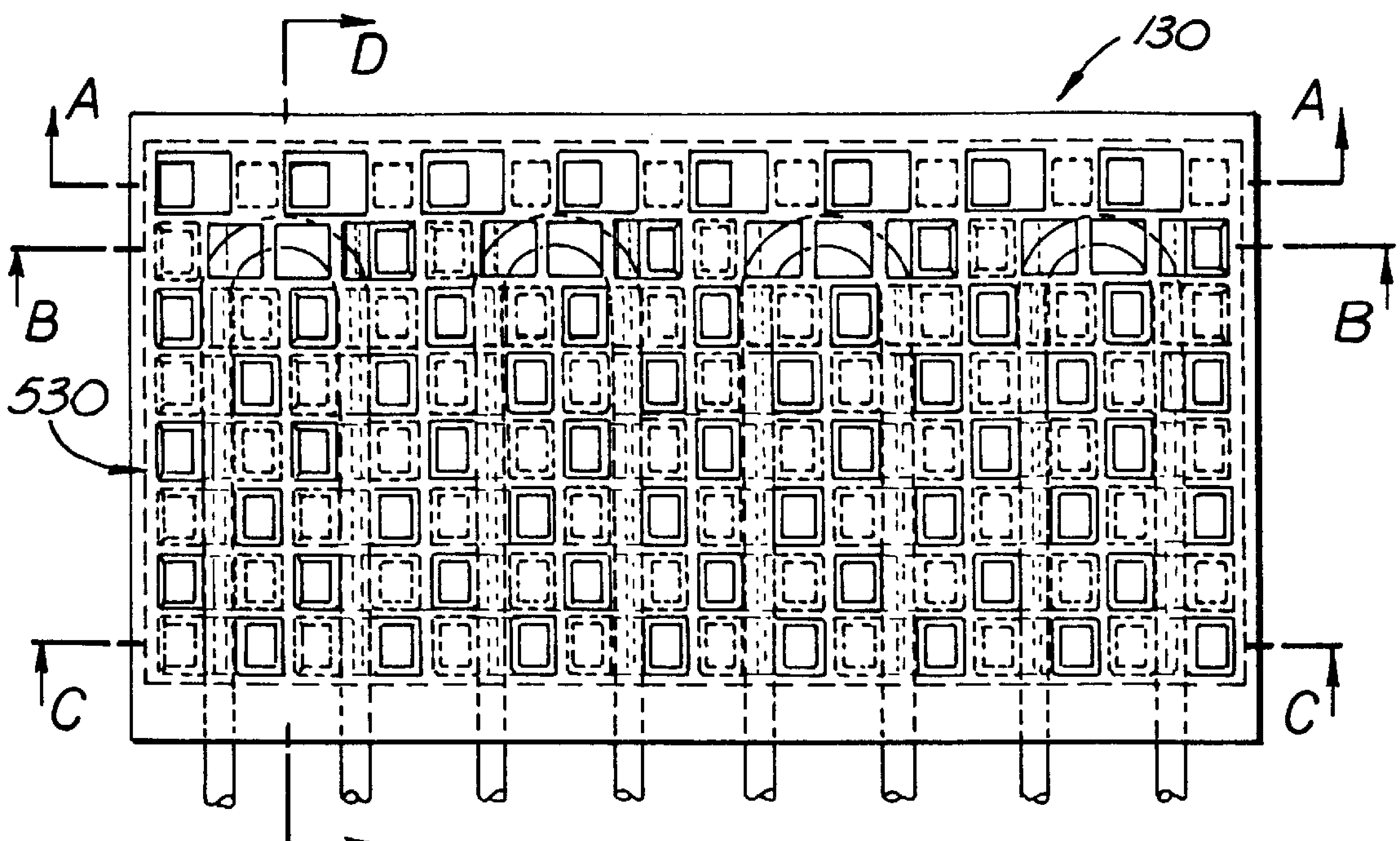


FIG. 7A

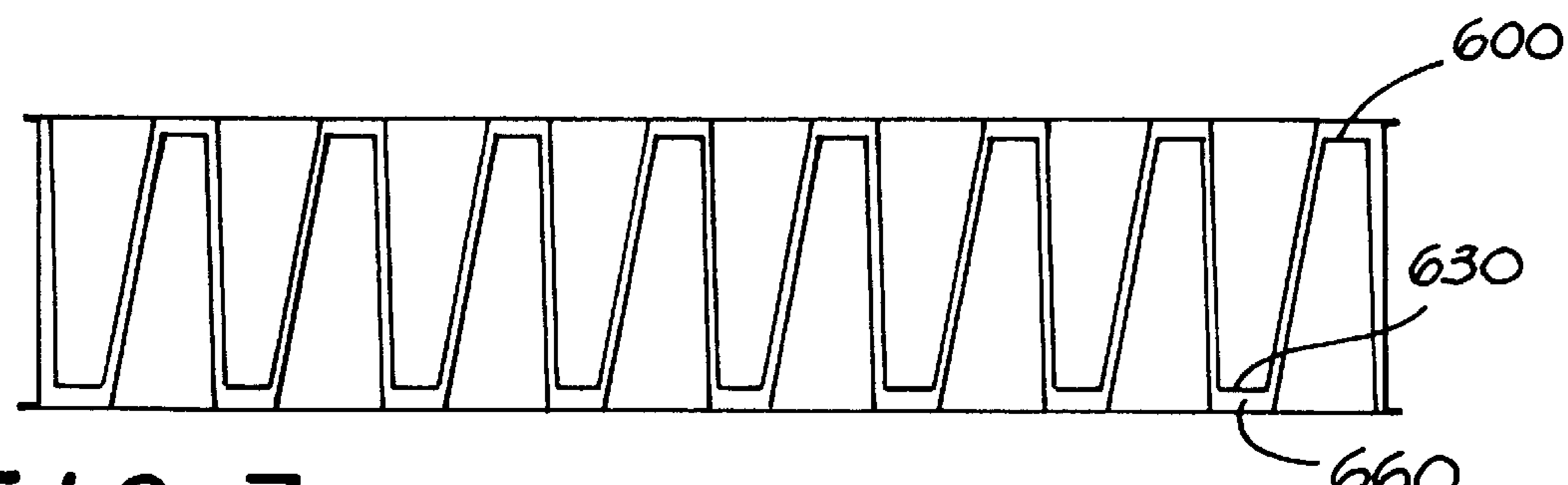


FIG. 7B

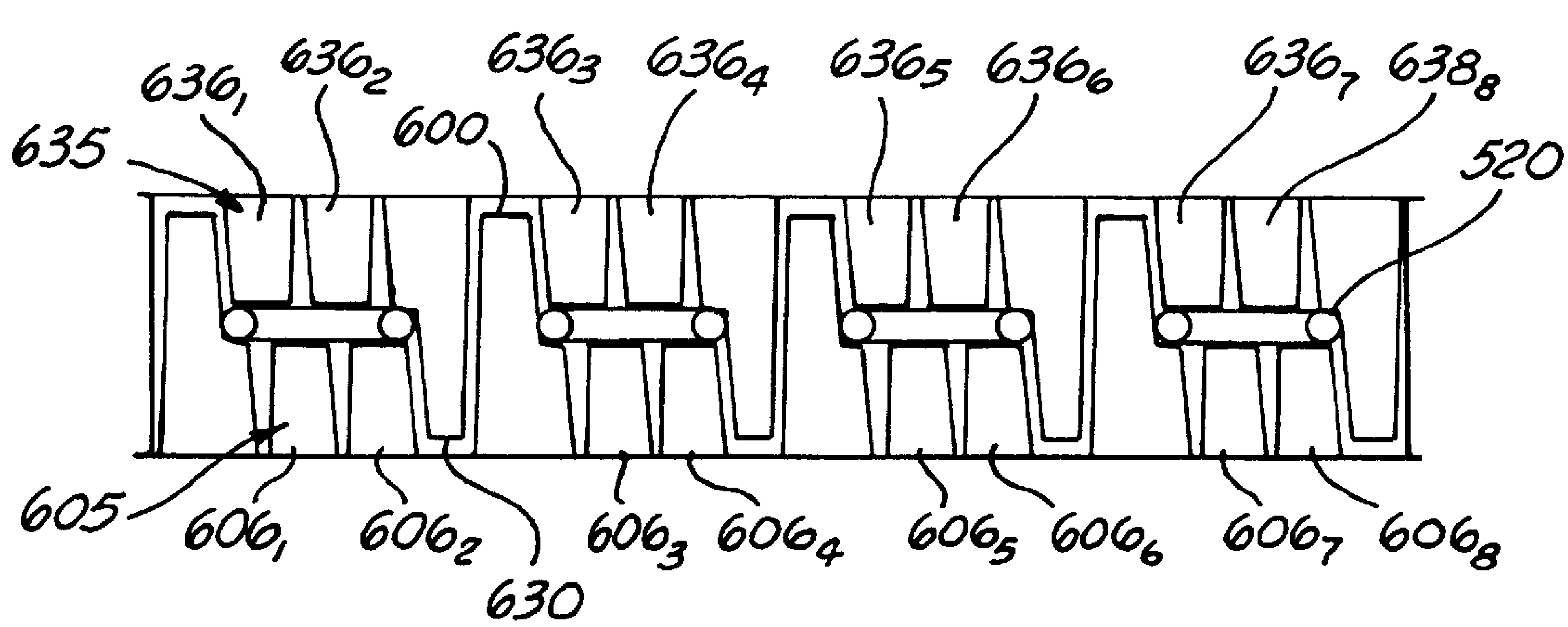


FIG. 7C

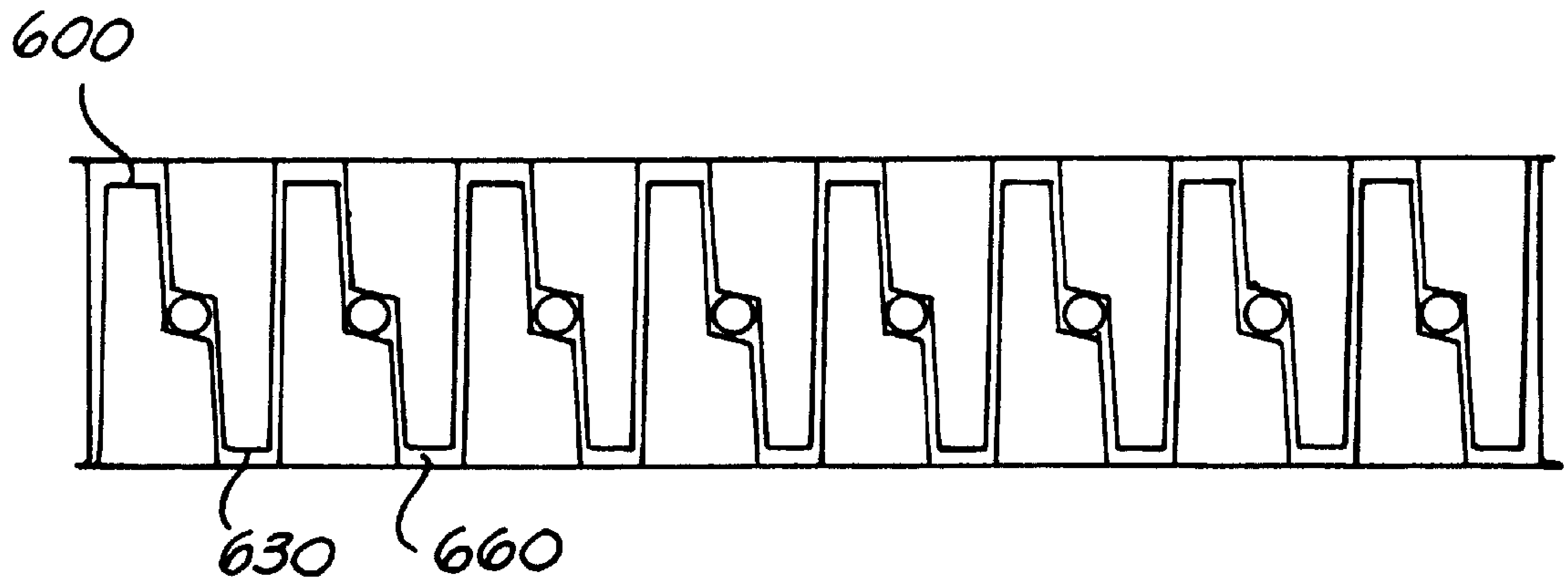


FIG. 7D

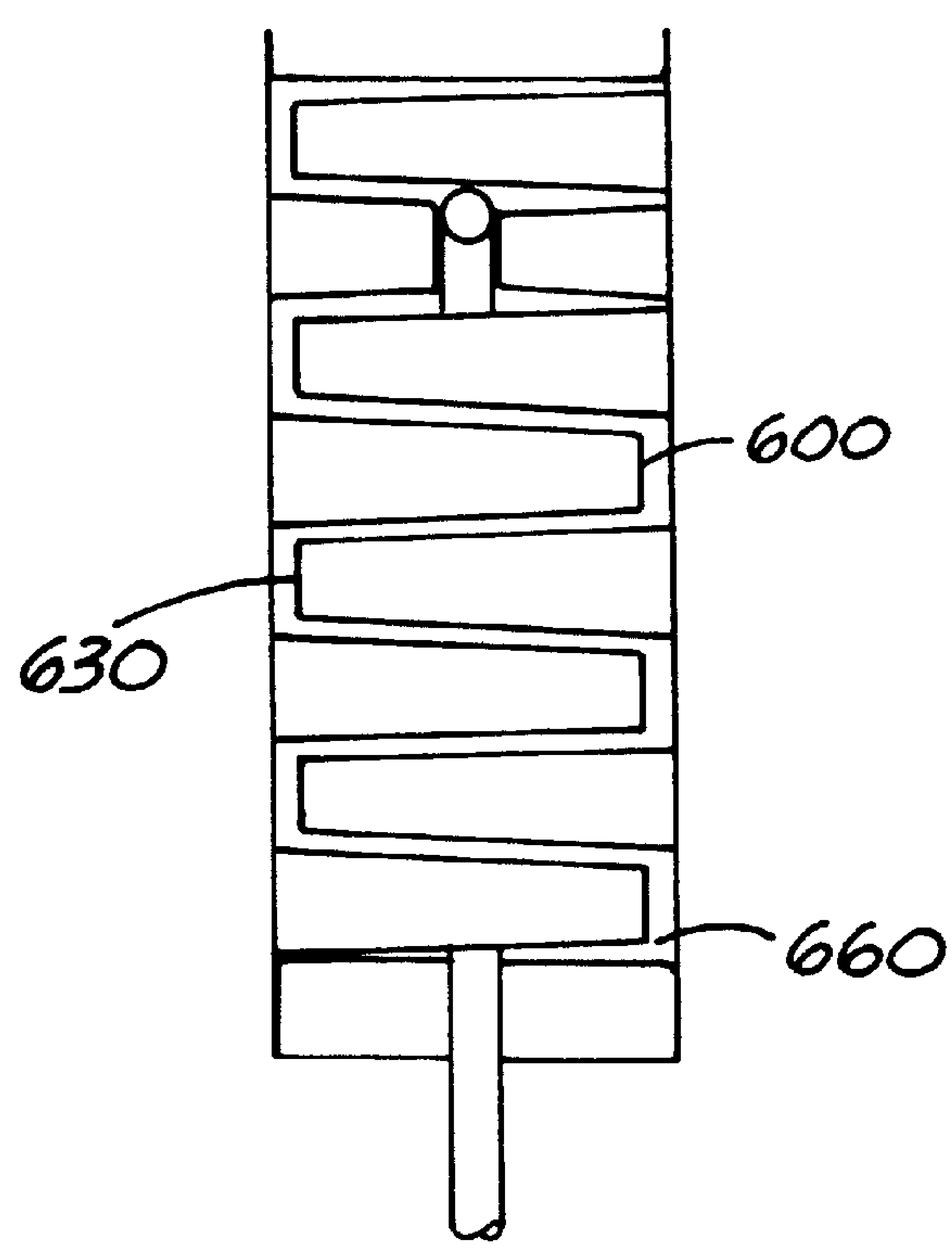


FIG. 7E

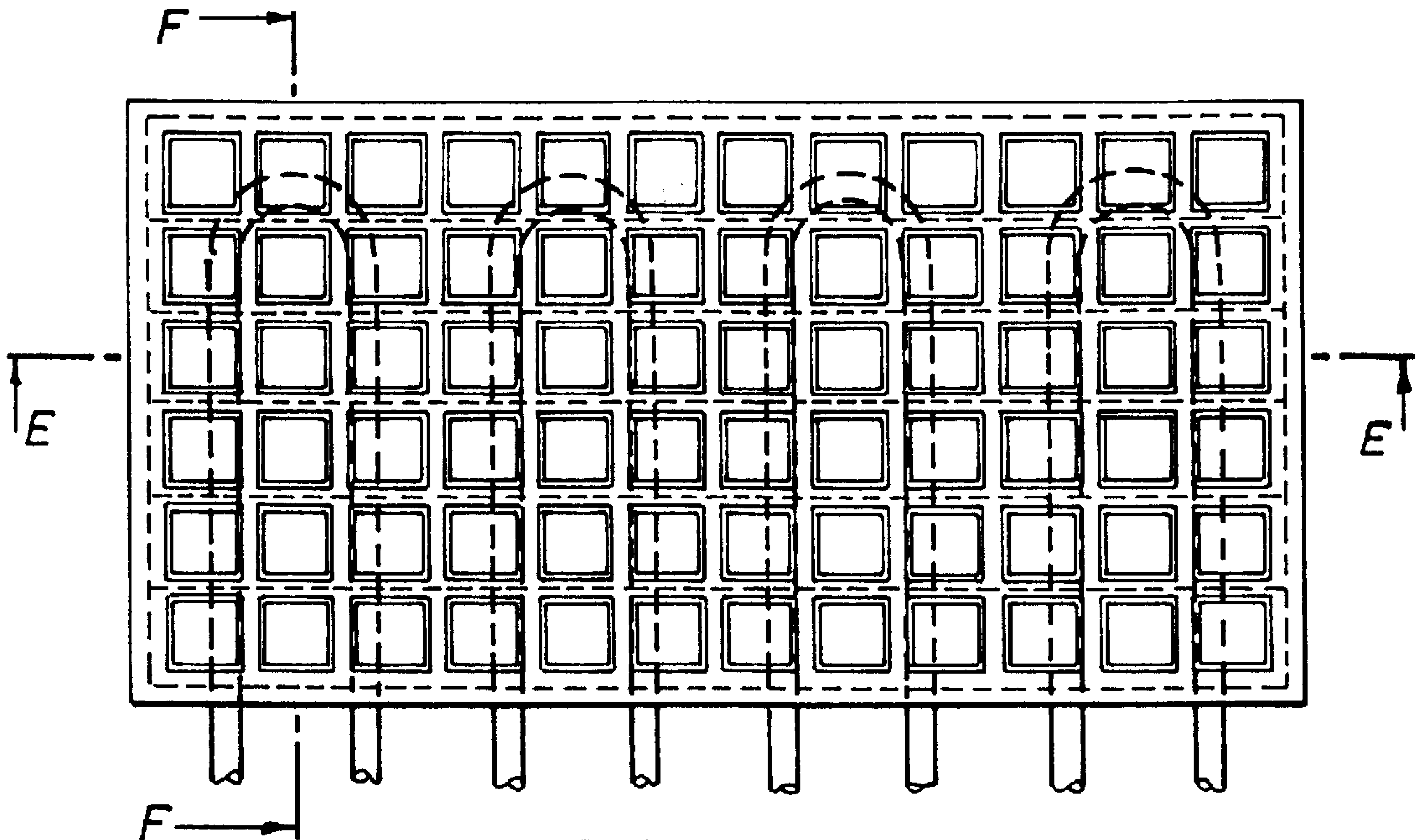


FIG. 8A

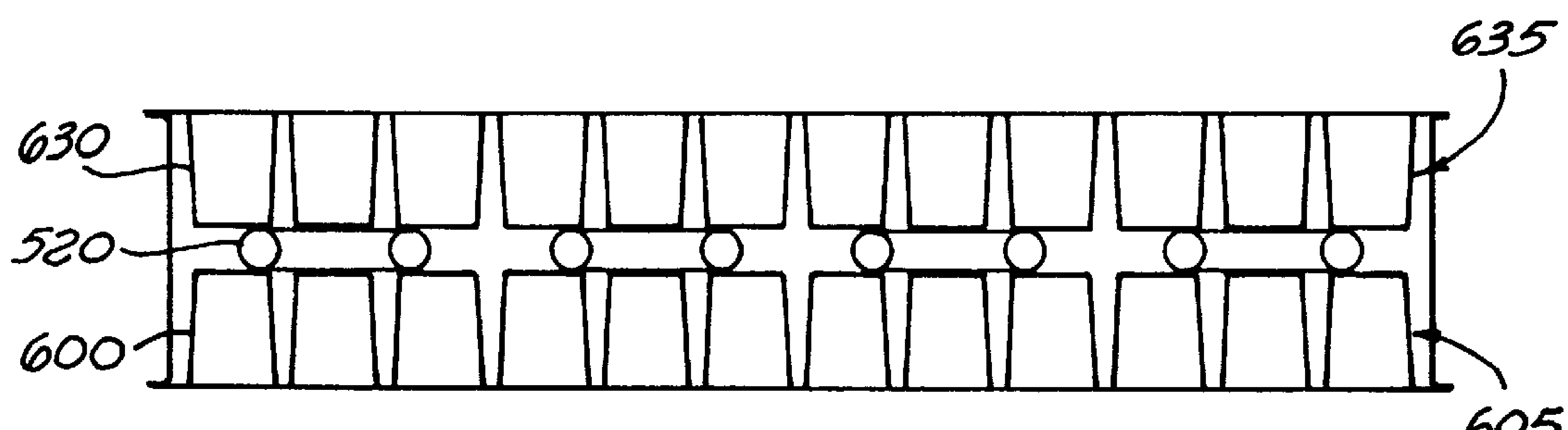


FIG. 8B

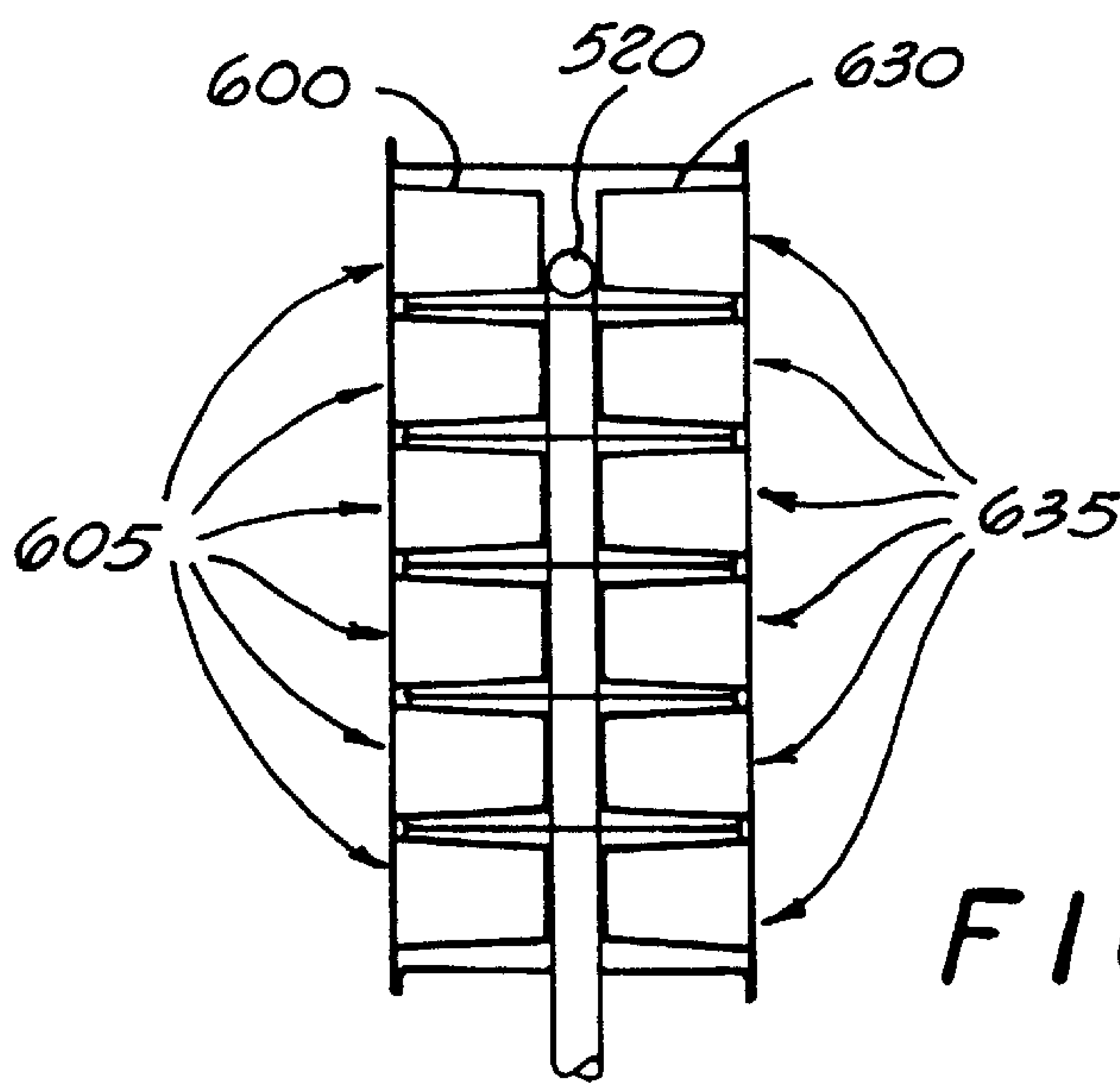


FIG. 8C

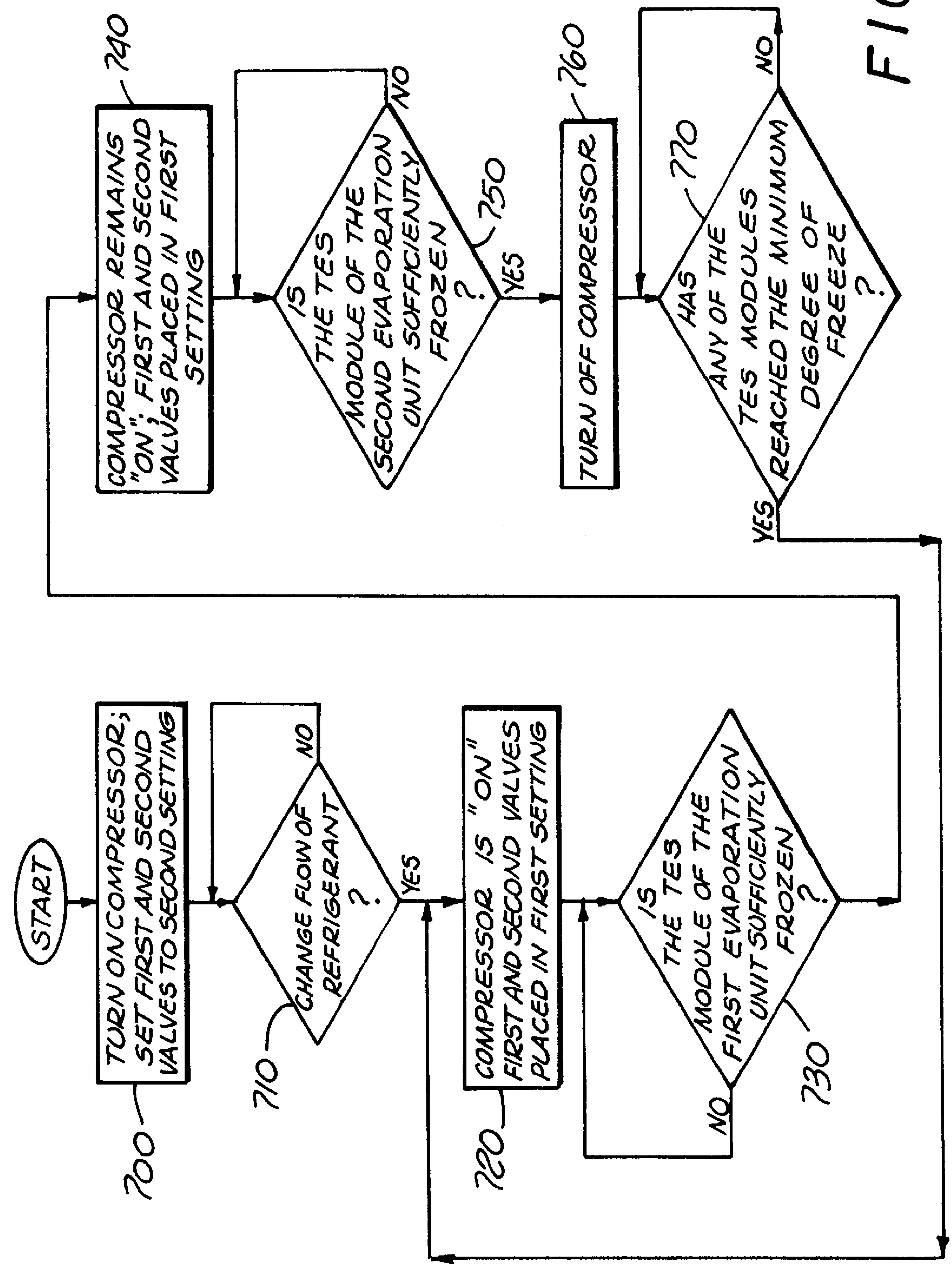

START
TURN ON COMPRESSOR; SET FIRST AND SECOND VALVES TO SECOND SETTING
700
CHANGE FLOW OF REFRIGERANT ?
710
NO
YES
COMPRESSOR IS "ON" FIRST AND SECOND VALVES PLACED IN FIRST SETTING
720
IS THE TES MODULE OF THE FIRST EVAPORATION UNIT SUFFICIENTLY FROZEN ?
730
NO
COMPRESSOR REMAINS "ON"; FIRST AND SECOND VALVES PLACED IN FIRST SETTING
740
IS THE TES MODULE OF THE SECOND EVAPORATION UNIT SUFFICIENTLY FROZEN ?
750
NO
YES
TURN OFF COMPRESSOR
760
HAS ANY OF THE TES MODULES REACHED THE MINIMUM DEGREE OF FREEZE ?
770
NO
YES

FIG. 9

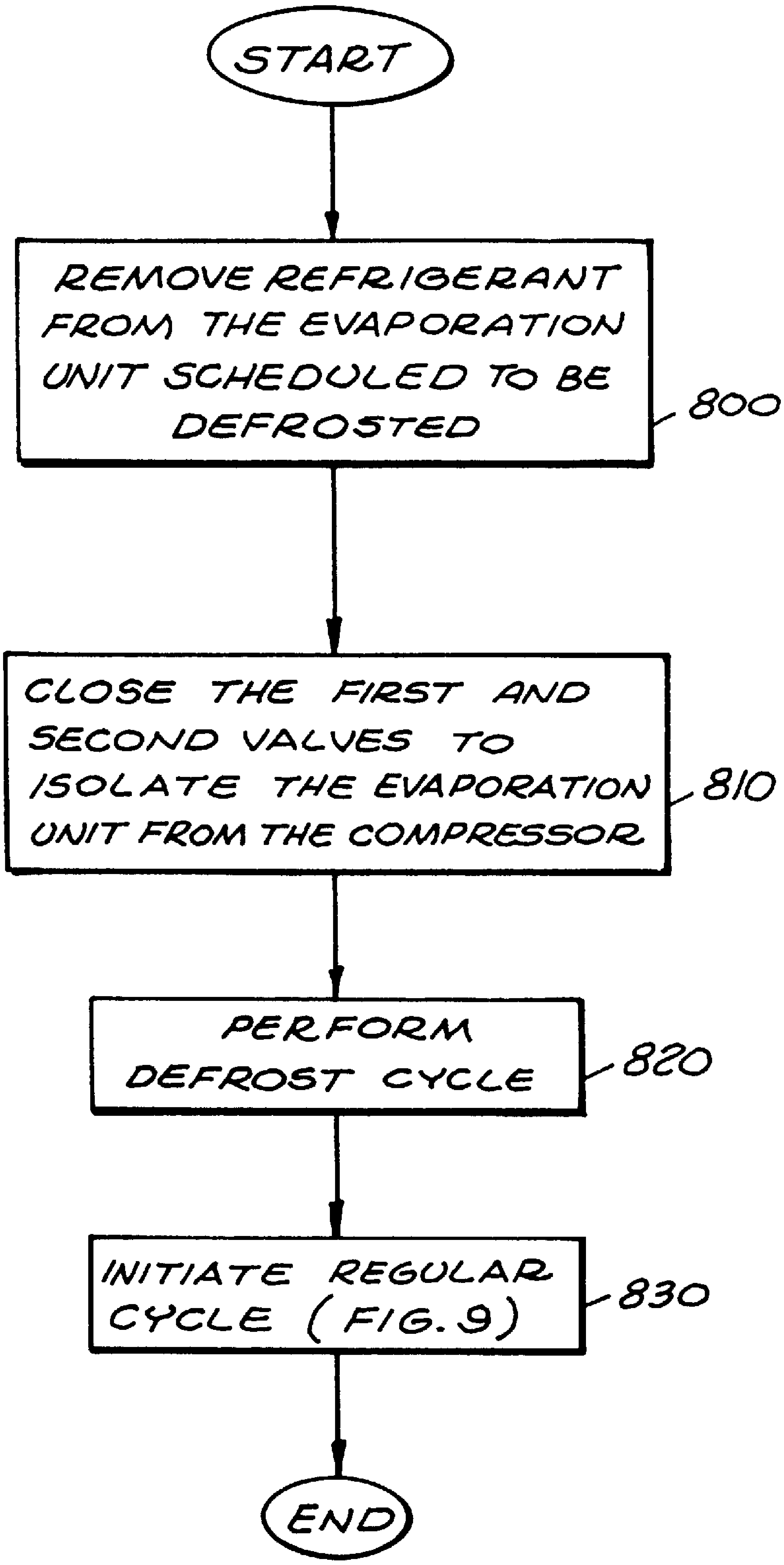

START
REMOVE REFRIGERANT FROM THE EVAPORATION UNIT SCHEDULED TO BE DEFROSTED
800
CLOSE THE FIRST AND SECOND VALVES TO ISOLATE THE EVAPORATION UNIT FROM THE COMPRESSOR
810
PERFORM DEFROST CYCLE
820
INITIATE REGULAR CYCLE (FIG. 9)
830
END

FIG. 10

DUAL EVAPORATOR REFRIGERATION UNIT AND THERMAL ENERGY STORAGE UNIT THEREFORE

This is a non-provisional U.S. (U.S.) patent application based on two provisional U.S. patent applications including (i) a first provisional U.S. patent application entitled "Cost and Energy Efficient Implementation of a Dual Evaporator Refrigerator Using Thermal Energy Storage" (App. No. 60/030,308); filed Nov. 5, 1996 and (ii) a second provisional U.S. patent application entitled "Cost and Energy Efficient Implementation of a Dual Evaporator Refrigerator Using Thermal Energy Storage" (App. No. 60/047,064); filed May 17, 1997.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to the field of refrigeration. More particularly, one embodiment of the present invention relates to a two-stage refrigeration system utilizing an evaporator integrated with an encapsulated thermal energy storage module.

2. Background of Art Related to the Invention

For many decades, domestic refrigerators have included a freezer section and a fresh food section. The fresh food section is maintained at a significantly higher temperature than the freezer section. While the basic laws of thermodynamics provide empirical evidence that it is increasingly more difficult to cool (i.e., remove heat from) an item as its temperature decreases, domestic refrigerators typically have been designed with more consideration focused on cost than thermodynamics. For example, many domestic refrigerators use a one-stage refrigeration system including a single evaporator located in the freezer section. Since the total heat load dissipation is through this single evaporator, this one-stage refrigeration system possesses less than optimal energy efficiency.

Recently, in order to increase system efficiency, some refrigerators have been constructed with two separate refrigeration systems; namely, one refrigeration system is responsible for cooling the freezer section while the other refrigeration system is responsible for cooling the fresh food section. Consequently, this dual refrigeration system includes repetitive condensing units, each featuring a compressor and a condenser. This repetition of equipment increases the cost and size of the refrigerator. Also, these repetitive condensing units produce a greater amount of noise.

Another example involves yacht refrigerators which have been implemented with refrigeration systems having valves to sequentially, but not simultaneously, connect a single, high-capacity condensing unit to multiple evaporators operating at differing temperatures. The refrigeration system may use thermal energy storage (TES) material to provide stable temperatures during the period between evaporator operations.

Preferably, TES material is an aqueous solution such as a salt solution having water and sodium chloride (NaCl). This composition provides high heat storage capacity, emits a large amount of heat isothermally upon changing phase from a liquid to a solid, is non-toxic and can be produced for a low cost. Unfortunately, this TES material is highly corrosive to most metals, tends to expand when frozen which would damage the thin wall of the heat exchanger and tends to freeze first on the heat exchange surfaces which would hamper further heat transfer. This requires the TES material to be separated from the thin-walled metal tubing of the heat exchanger. One technique of separation involves encapsulating TES material into separate expandable capsules as described in U.S. Pat. No. 5,239,839 by the named inventor. However, such encapsulation is costly and difficult to produce.

Additionally, the use of TES material adversely affects the efficiency of conventional defrosting cycles. The reason is that conventional defrost methods, if implemented, would require the entire TES material to melt before actual defrosting could begin.

U.S. Pat. Nos. 4,712,387 and 4,756,164 by the named inventor describe a heat pipe based method for efficiently transferring heat into and out of TES material and a method for thermally de-coupling the TES material from the cooled space to enable simple and efficient defrosting of the evaporator. These methods fail to provide any suggestion of the multi-stage refrigeration system and/or control protocol used to control this refrigeration system.

In contrast to the prior techniques and refrigeration systems, the present application describes a cost-effective evaporation unit and an energy efficient control protocol to maintain steady temperatures for each section of a refrigeration unit. An additional element of this disclosure is the use and design of a simple sensor for determining the frozen fraction of a TES module in order to control on-and-off cycling of the compressor for temperature stabilization.

SUMMARY OF THE INVENTION

The present invention describes a low-cost and thermodynamically efficient implementation of a multi-stage refrigeration system utilized by a refrigeration unit such as a retail refrigerator. This multi-stage refrigeration system includes a condensing unit and at least two evaporation units connected to the condensing unit through tubing and a plurality of valves. These valves may include a pair of selector valves, four check valves or any combination or type of valves necessary to control liquid and vapor flow through the refrigeration system.

The present invention further features a simple and easily manufactured thermally efficient and low-cost evaporation unit, a thermal energy storage module of the evaporation unit and an energy efficient control protocol to maintain steady temperatures of a freezer and fresh food section of the refrigeration unit. This control protocol permits energy efficient defrosting of the heat exchange surfaces in the freezer section and minimize losses associated with condensing unit on-and-off cycling.

BRIEF DESCRIPTION OF THE DRAWINGS

The features and advantages of the present invention will become apparent from the following description of the present invention in which:

FIG. **1** is an illustrative embodiment of a refrigeration unit implemented with the present invention.

FIG. **2** is an illustrative embodiment of a multi-stage refrigeration system utilizing selector valves.

FIG. **3** is an illustrative embodiment of a selector valve of the refrigeration system of FIG. **2**.

FIG. **4A** is another illustrative embodiment of a multi-stage refrigeration system utilizing check valves.

FIG. **4B** is an illustrative embodiment of a check valve of the refrigeration system of FIG. **4A**.

FIG. **4C** is an illustrative embodiment of a plurality of check valves whose operation is controlled by an external magnetic field.

FIG. **5** is an illustrative embodiment of an evaporation unit implemented in refrigeration systems of FIGS. **2** and **4**A.

FIG. **6** is an illustrative embodiment of a thermal energy storage (TES) module implemented within the evaporation unit of FIG. **5**.

FIG. **7**A is a more detailed illustrative embodiment of the TES module implemented in refrigeration systems of FIGS. **2** and **4**A.

FIGS. **7**B–**7**E are illustrative cross-sectional views of the TES module of FIG. **7**A taken along lines A—A, B—B, C—C and D—D, respectively.

FIG. **8**A is another detailed illustrative embodiment of the TES module implemented in refrigeration systems of FIGS. **2** and **4**A.

FIGS. **8**B and **8**C are illustrative cross-sectional views of the TES module of FIG. **8**A taken along lines E—E and F—F, respectively.

FIG. **9** is an illustrative flowchart of the operations of the multi-stage refrigeration system during a regular operation cycle.

FIG. **10** is an illustrative flowchart of the operations of the multi-stage refrigeration system during a defrost cycle.

DESCRIPTION OF THE PREFERRED EMBODIMENT

The present invention relates to a thermodynamically efficient multi-stage refrigeration system, a thermal energy storage module and its corresponding method of operation. In the following detailed description, specific details are set forth for illustration purposes in order to ensure understanding of the present invention. Of course, it would be apparent to one skilled in the art that the present invention may be practiced while still deviating from these specific details. Furthermore, it should borne in mind that the present invention should not be limited solely in connection with refrigerators, but may be utilized for other type of appliances.

In the following description, some terminology is used to generally describe certain features of the refrigeration system. For example, a "refrigeration unit" may include a refrigerator, a stand-alone freezer, an air conditioner, cryogenic equipment or any other equipment that provides refrigeration. A "refrigerant" may include any refrigerant such as those used domestically as well as in foreign countries like Europe. A "tube" (and related tenses such as "tubing") is defined as a partially enclosed region which is capable of transferring material in various forms from a source to a destination. The tube may be constructed of any non-soluble material such as metal or plastic.

1. Multi-stage Refrigeration System

Referring to FIG. **1**, an illustrative embodiment of a refrigeration unit (e.g., refrigerator) implemented with a multi-stage refrigeration system is shown. Refrigeration unit **100** includes a first section **110** and a second section **120**. In this embodiment, the first section **110** is a freezer which is maintained at a lower temperature than the temperature of the second (fresh food) section **120**. It is contemplated, however, that these sections **110** and **120** may be maintained at generally equivalent temperatures.

The first section **110** includes a first evaporation unit **130** placed adjacent to (i) insulation **135** surrounded by an outer wall **140** of the first section **110**, and (ii) a liner **145** creating a compartment for item storage. As described above, first evaporation unit **130** includes the containment vessel **150** including TES module **155** having one or more protrusions spaced between segments of an evaporation tube **160**. The containment vessel **150** is filled with freely convecting thermal coupling solution **165** (not shown). The thermal coupling solution is any liquid supporting freely convecting heat transfer such as an alcohol and water composition. Other characteristics of the thermal coupling solution may include, but are not limited or restricted to low viscosity, low cost and low toxicity. First evaporation unit **130** may be constructed to be adjacent to multiple sides of the first section as shown or a single side.

Similarly, second section **120** includes a second evaporation unit **170** placed adjacent to both insulation **175** and a liner **180** creating another compartment. The second evaporation unit **170** includes a containment vessel **185** enclosing TES module **190** having protrusions spaced between segments of its evaporation tube **195**. The containment vessel **185** is also filled with freely convecting thermal coupling solution (not shown).

Referring to FIG. **2**, one embodiment of a thermodynamically efficient, multi-stage refrigeration system **200** utilized by refrigeration unit **100** is shown. This embodiment of multi-stage refrigeration system **200** includes a condensing unit **210**, a first valve **220**, at least two evaporation units **130** and **170** and a second valve **230**. As further described below, each evaporation unit **130** and **170** includes an evaporator integrated with one or more expandable container(s) filled with thermal energy storage "TES" material such as an aqueous solution such as water and sodium chloride (NaCl). Other types of aqueous solutions may include, for example, different combinations of alkali metals (Group 1*a*) or alkaline earth elements (Group 2*a*) with halogen elements (Group 7*a*). Of course, a variety of non-aqueous solutions may be used as TES material. Each expandable container may be referred to as a "TES module".

The collective, simultaneous operations of valves **220** and **230** place refrigeration system **200** in one of two modes of operation. In general, the first mode of operation is a regular cycle where the TES module of the evaporation units **130** and **170** are sufficiently frozen to maintain the first and second sections **110** and **120** generally at their targeted temperatures. The second mode of operation is a defrost cycle in which the refrigerant from first evaporation unit **130** is removed in order to melt frozen water from the heat exchange surface of the first evaporation unit **130**. The particular state (or setting) of these valves **220** and **230** during these regular and defrost cycles are shown in Tables 2 and 3 and are described below.

Referring still to FIG. **2**, condensing unit **210** includes a compressor **211**, a condenser **212** and a reservoir **213** interconnected by tubes **214** and **215**. During operation, compressor **211** receives refrigerant as vapor from second valve **230** via tube **214** and compresses the vapor refrigerant to a selected pressure. Next, condenser **212** cools the compressed, refrigerant vapor to produce a liquid refrigerant which is subsequently supplied to reservoir **213** through tube **215**. The throughput of the liquid refrigerant is controlled by first valve **220** as well as an expansion device which is normally situated at an inlet of each evaporation unit **130** and **170**. The expansion device X may include a capillary tube or any mechanical device used to control flow rate between two areas having different levels of pressure such as an expansion valve well-known in the art.

The first valve **220** is a liquid selector valve that regulates the flow of liquid refrigerant from reservoir **213** into either first evaporation unit **130** or second evaporation unit **170**. As shown, first valve **220** selects a flow path to first evaporation unit **130** when placed in a first setting (outlet **1**-on; outlet **2**-off) and selects a flow path to second evaporation unit **170** when placed in a second setting (outlet **1**-off; outlet **2**-on). The flow of liquid refrigerant through valve **220** is automatically changed by adjusting the setting of valve **220** in accordance with the control protocol described below. It is contemplated, however, that the valves **220** and **230** may be construed with additional settings in which the flow path is disconnected from either of the evaporation units. In this case, for example, the control protocol may be slightly altered to possibly select that setting when the compressor is turned off.

One embodiment of first valve **220** features an electromagnetic selector valve such as a rotary face seal valve as shown in FIG. **3**. This valve includes a housing and rotary actuator **300**, a rotary valve element **310** and a stationary base plate **320** supporting a single inlet **330** and one or more outlets $\mathbf{340_1}$–$\mathbf{340_n}$ ("n" is a positive whole number). Rotary valve element **310** features an internal flow passage **311** including an input **312** and a single output **313**. Input **312** is always in alignment with inlet **330**. However, output **313** may be aligned with output $\mathbf{340_1}$ or output $\mathbf{340_n}$ based on the rotational orientation of rotary valve element **310**. This orientation is selected through rotational adjustment of housing and rotary actuator **300** in which one flow path is selected when actuator **300** is energized and the other flow path is selected when actuator **300** is not energized.

Referring back to FIG. **2**, second valve **230** may be implemented as a suction selector valve that selects to receive refrigerant vapor from either first evaporation unit **130** or second evaporation unit **170**. As shown, second valve **230** selects a flow path from first evaporation unit **130** when placed in a first setting (inlet **1**-on; inlet **2**-off) and selects a flow path from second evaporation unit **170** when placed in a second setting (inlet **1**-off; inlet **2**-on). The selected construction of second valve **230** may be similar to the embodiment described for first valve **220** with exception in substitution of a single outlet and multiple inlets. Of course, other embodiments for these valves may be utilized (e.g., mechanical, electrical, magnetic and/or electro-magnetically controlled valves) besides those illustrated.

Referring to FIG. **4A**, another embodiment of a thermodynamically efficient, multi-stage refrigeration system **400** utilized by refrigeration **100** unit is shown. Similar to the embodiment shown in FIG. **2**, multi-stage refrigeration system **400** includes a condensing unit **210**, a plurality of check valves **410**, **420**, **430** and **440** and at least two evaporation units **130** and **170** as described below. Each evaporation unit **130** and **170** includes an evaporator integrated with one or more TES modules.

The collective, simultaneous operations of valves **410**, **420**, **430** and **440** place refrigeration system **400** in one of three modes of operation. In general, the first mode of operation (Mode A) is where a first valve **410** and a third valve **430** are functioning as normal check valves while a second valve **420** and a fourth valve **440** are "overridden" such that they do not impede liquid or vapor flow in either direction. The second mode of operation (Mode B) is where the first and third valves **410** and **430** are overridden while second and fourth valves **420** and **440** are functioning as normal check valves. The third mode of operation (Mode C) is where all of the check valves function as normal one-way check valves which provides a defrost capability. The check valve operation protocol to support the above-described operations are set forth in Table 1.

TABLE 1

State of Valves/Compressor of the Refrigeration System of FIG. 4A

Sequence	Valve 1	Valve 2	Valve 3	Valve 4	Compressor	Mode
Start	check⇒	open⇔	check⇒	open⇔	On	A
Low Temp Run (TES Freezing)	open⇔	check⇒	open⇔	check⇒	On	B
High Temp Run (TES Freezing)	check⇒	open⇔	check⇒	open⇔	On	A
Passive Cooling (TES melting)	check⇒	check⇒	check⇒	check⇒	Off	C
Defrost: Low Temp Liquid Removal	check⇒	check⇒	check⇒ (passes flow)	check⇒	On, briefly	C
Defrost	check⇒	check⇒	check⇒	check⇒	Off	C

Each of the check valves **410**, **420**, **430** or **440** may be constructed with any check valve embodiment such as a tilt-type check valve as shown in FIG. **4B**. The tilt-type check valve includes an o-ring valve seat **450** and a valve stem **460** placed in tubing. Made of magnetic material, valve stem **460** is attached to o-ring valve seat **450**. Normally, valve stem **460** is applying a force against o-ring valve seat **450** caused by gravity or possibly by a mechanical element (e.g., spring). This provides sufficient closure of the o-ring valve seat **450**.

When an external magnetic field is applied, the normal check valve action of valve stem **460** can be overridden by magnetically repositioning valve stem **460** as shown by arrows A and B or arrows C and D. This small amount of lateral and/or vertical movement by valve stem **460** opens the valve. Both lateral and vertical movement of valve stem **460** may allow the valve to be opened easier by mitigating back pressure associated with tube. The external magnetic field may be applied by an external electromagnet or even a permanent magnet positioned by any mechanical means in order to override one or more check valves.

As an illustrative example, FIG. 4C shows a condition where a magnet **470** is placed in a first position which overrides the second and fourth check valves **420** and **440** while allowing the first and third check valves **410** and **430** to operate as normal. This condition usually occurs at the start a regular cycle and in freezing TES material associated with the second (higher temperature) evaporation unit. FIG. 4C also shows another condition where the magnet **470** is placed in a second position (denoted by dotted lines) which overrides the first and third check valves **410** and **430** while the second and fourth check valves **420** and **440** function as normal.

Referring now to FIG. **5**, an embodiment of an evaporation unit (e.g., the first evaporation unit **130**) is shown. Of course, the second evaporation unit **170** possess a similar (if not identical) implementation. The first evaporation unit **130** includes an evaporator featuring an upper heat exchanger **500** and a lower heat exchanger **510**, both of which are formed by segments from a single evaporation tube **520**. Shaped in a serpentine pattern or bent and manipulated in any direction so that liquid refrigerant will flow freely, evaporation tube **520** also operates as heat pipes to transfer heat to a TES module **530** described below. The lower heat exchanger **510** features a plurality of U-shaped segments of evaporation tube **520** including an inlet **521** to receive liquid refrigerant and at least one outlet **522** to output refrigerant vapor. The lower heat exchanger **510** further features a plurality of evaporator fins $\mathbf{523_1}$–$\mathbf{523_m}$ ("m" is a positive whole number) placed adjacent to evaporation tube **520** for enhanced heat transfer from air to the refrigerant.

The TES module **530** is placed adjacent to segments of evaporation tube **520** located in upper heat exchanger **500**. Both TES module **530** and upper heat exchanger **500** are collectively enclosed in a containment vessel **540** filled with thermal coupling solution (not shown). There are several options for sealing the penetrations of segments of evaporation tube **520** into containment vessel **540**. A foamed sealant can provide both the required sealing and provide insulation for evaporation tube **520**. This will help prevent ice build-up on a portion of evaporation tube **520** adjacent to containment vessel **540** and minimize the heating required for defrosting lower heat exchanger **510**.

The "TES module" **530** is TES material encapsulated within an expandable container to avoid direct contact (physical or chemical) with evaporation tube **520** in upper heat exchanger **500**. The "thermal coupling solution" is an liquid that does not freeze at normal operating temperatures of the refrigeration unit and provides thermal coupling between TES module **530** and upper heat exchanger **500**.

In one embodiment, TES module **530** is formed by two sheets of material **600** and **610** such as thermal formed plastic as generally shown in FIG. **6**. A first sheet **600** includes an array of closely spaced, high aspect ratio protrusions **605** which form cavities for TES material; namely, some of these protrusions **605** have a substantial amount of surface area situated adjacent to segments of evaporation tube associated with upper heat exchanger in order to remove heat from refrigerant passing therethrough. These protrusions **605** are tapered to simplify their manufacture and to ensure that ice blocks do not cause localized pressure. If freezing occurs so that a region of liquid TES material remains trapped in the end of a protrusion, the tapered shape permits the ice plug to relieve pressure generated when the remaining liquid freezes.

A backing sheet **610**, which is normally flat, is sealed to first sheet **600** around its perimeter in order to form an enclosed area **620**. The enclosed area **620** is filled with TES material. Alternatively, backing sheet **610** may be sealed around the base of each protrusion. The sealing may be accomplished through heat or ultrasonic welding to prevent leakage. It is contemplated, however, that backing sheet **610** may be patterned in a manner similar to first sheet **600** and sealed to first sheet **600** so that the protrusions of both sheets protrude outward.

It is contemplated that TES module **530** may further include a second pair of sheets **630** and **640** which are constructed in a similar manner in order to substantially occupy a substantial amount of the volume of containment vessel **540**. The second pair of sheets **630** and **640** are constructed to interlock with the first pair of sheets **600** and **610** and with the protrusions generally perpendicular to the evaporation tube and parallel to the fins, but leaving well-defined passages for the thermal coupling solution to flow between sheets **600** and **630**. U-shaped flanges **650** of containment vessel **540** are sealed to sheets **600** and **610** to form one side of the containment vessel for the thermal coupling solution.

More specifically, FIG. **7**A provides a detailed view of an embodiment of evaporation unit (e.g., first evaporation unit **130**) having TES module **530**. Various cross-sectional views of the evaporation unit along lines A—A, B—B, C—C and D—D are shown in FIGS. **7**B, **7**C, **7**D and **7**E, respectively.

Referring now to FIG. **7**B, a cross-sectional view (along lines A—A and perpendicular to a layout of evaporation tube **520**) of an embodiment of TES module **530** of FIG. **7**A is illustrated. As shown, this portion of TES module **530** is not in a region having any segment of evaporation tube **520** of evaporation unit. Thus, the array of protrusions formed by the second sheet **630** of TES module **530** interlock with cavities associated with the first sheet **600**. This leaves a well-defined passage **660** for the thermal coupling solution to flow between sheets **600** and **630**.

Referring to FIG. **7**C, a cross-sectional view (along lines B—B) of the embodiment of TES module **530** of FIG. **7**A is illustrated. Herein, the sizing and/or positioning of various protrusions associated with the first and second sheets **600** and **630** of TES module **530** is influenced by the presence or absence of segments of evaporation tube **520**. In particular, the protrusions associated with the first and second sheets **600** and **630** usually is made of material which is more flexible than the material forming evaporation tube **520**. Thus, a few protrusions $\mathbf{606_1}$–$\mathbf{606_8}$ associated with the array of protrusions **605** and protrusions $\mathbf{636_1}$–$\mathbf{636_8}$ associated with an array of protrusions **635** of second sheet **630** are compacted or adjusted to conform with evaporation tube **520**. The passage **660** still remains between the first and second sheets **600** and **630**. Alternatively, provisions can be made to ensure that the protrusions remain adjacent to evaporation tube, but at a distance so as to not contact a surface of evaporation tube **520**.

Referring to both FIGS. **7**D and **7**E, a cross-sectional view (along lines C—C and lines D—D) of the embodiment of TES module **530** of FIG. **7**A is illustrated. As set forth in FIG. **7**C, FIGS. **7**D and **7**E illustrate other cross-sectional views which indicate that the sizing and/or positioning of various protrusions associated with the first and second sheets **600** and **630** of TES module **530** are influenced by the presence or absence of segments of the evaporation tube

520. The passage **660** still remains between the first and second sheets **600** and **630**.

Referring to FIGS. **8**A–**8**C, another embodiment of the TES module is shown along with cross-sectional views along lines E—E and F—F. In this embodiment, first sheet **600** includes array of protrusions **605** while second sheet **630** includes array of protrusions **635** as set forth in FIG. **8**B. In contrast with the embodiment in FIGS. **6** and **7**A–**7**E, these protrusions **605** and **635** are not sized to support an interlocking configuration. Instead, the protrusions **605** and **635** are sized to provide a separation spacing therebetween. The separation spacing is generally equivalent to the width of evaporation tube **520**. As a result, the protrusions **605** and **635** are adjacent to (and in contact with) evaporation tube **520**.

A further innovation involves adding a small amount of metal or other thermal conduction material to the TES material. Since water/ice has less than one percent (1%) of the conductivity of copper or aluminum, the addition of small amounts of metal fibers will enhance heat transfer from the freezing TES material.

Because TES is very effective at stabilizing temperatures in a refrigeration system, the conventional means of using temperature change to control on-and-off cycling of condensing unit **210** of FIGS. **2** and **4**A has limitations. This would require the TES material to fully melt before the TES module temperature is used to generate a signal to turn-on the condensing unit is initiated because TES material necessarily has a lower melting temperature than the frost. Likewise, the TES material would be required to fully freeze before signaling the condensing unit to turn-off.

With respect to the present invention, a small reserve of frozen TES material is maintained by a "degree of freeze indicator" which may include a sensor that detects a change of dimension, volume or any other characteristic associated with the TES modules when the TES material freezes. There are many techniques for the degree of freeze indicator to detect characteristic changes. One technique is to construct containment vessel **540** of rigid material and incorporate some gas therein. A change volume can be calculated by the indicator measuring the pressure within containment vessel **540**. A second technique is to construct containment vessel **540** of flexible material (or even only a localized area) and subsequently incorporating a degree of freeze indicator that can measure the dimension or change in dimension (i.e., deflection or inflection) of that material. The use of this degree of freeze indicator eliminates the need (and cost) of a conventional thermostat.

2. Control Protocol

The multi-stage refrigeration systems operate in accordance with a control protocol which is designed to minimize losses associated with on-and-off cycling of the condensing unit **210** and to maintain close temperature control in both sections **110** and **120** of refrigeration unit **100** of FIG. **1**. This protocol also accommodates simple and thermally efficient defrosting of the evaporation unit located in the section **110** of refrigeration unit **100**.

It has been realized that cycling losses in conventional refrigeration units constitute a substantial percentage of total energy consumption. Typically, this percentage ranges from five percent (5%) to as high as fifteen percent (15%) of the total energy consumed. These cycling losses may be incurred during the transitory start-up period of the condensing unit because the compressor of the condensing unit needs to operate for some time before steady-state operating pressures and temperatures are reached. Operations performed before reaching steady-state are less efficient than if performed during steady-state.

In addition, the cycling losses may be incurred during a thermal siphoning condition as experienced by the multi-stage refrigeration system of FIG. **2**. A "thermal siphoning" condition is where refrigerant vapor flows back into an evaporation unit when the condensing unit is turned off. This refrigerant vapor condenses and deposits heat in the evaporation unit which increases the total system heat load associated with the evaporation unit. This additional heat load causes a reduction in system efficiency. It is contemplated that no thermal siphoning condition is present for the multi-stage refrigeration system of FIG. **4**A due to the nature of the check valves.

Referring now to FIGS. **2** and **9** and Table 2, the control protocol associated with the multi-stage refrigeration system of FIG. **2** minimizes the start-up transient and thermal siphoning losses described above by initiating cooling with the second (higher temperature) evaporation unit; namely, an evaporation unit associated with the fresh food section. This is accomplished by turning on the compressor and placing the first and second valves **220** and **230** in the second setting (Step **700**). As a result, refrigerant is circulated between the condensing unit **210** and the second evaporation unit **170** is shown in FIG. **2**. This minimizes the amount of time to reach steady-state.

Next, one or more degree of freeze indicators are used to control the flow of refrigerant through the first and second valves **220** and **230** into evaporation units **130** and **170** based on a measured degree of freeze of the TES modules located in evaporation units **130** and **170**. For example, after a predetermined time period or after a selected amount of the TES module of second evaporation unit **170** has been frozen, first and second valves **220** and **230** are placed in the first setting where refrigerant is circulated between first evaporation unit **130** and condensing unit **210** (Steps **710** and **720**).

When the TES module in first evaporation unit **130** is determined to be sufficiently frozen as detected by one or more degree of freeze indicators of the first evaporation unit **130** (e.g., one or more position sensors), first and second valves **220** and **230** are again placed in the second setting where refrigerant is circulated between second evaporation unit **170** and condensing unit **210** (Steps **730** and **740**). Thereafter, when the TES module in second evaporation unit **170** is determined to be sufficiently frozen, compressor **211** of condensing unit **210** is turned off and first and second values **220** and **230** remain in the first setting (Steps **750** and **760**).

When either of the TES modules reach a "minimum degree of freeze" which represents a predetermined amount of TES material being frozen (Step **770**), compressor **211** of condensing unit **210** is turned on and repeats the sequence described above and listed in Table 2. The completion of this cycle freezes the TES modules to a predetermined degree of freeze, as determined by the degree of freeze indicator(s), to generally maintain a stable, constant temperature. By maintaining sections of a refrigeration unit at stable temperatures, the degradation rate of the food is significantly improved (i.e., slower).

TABLE 2

State of Valves and Compressor for the Regular Cycle

Regular Cycle stages (in execution sequence)	First Valve	Second Valve	Compressor	Stage complete when:
Compressor start, initiated by degree of freeze indicator(s) reaching minimum in one TES mechanism	1-off, 2-on	1-off, 2-on	on	Start up transient ended
First evaporation unit on	1-on, 2-off	1-on, 2-off	on	TES in evaporator #2 frozen
Second evaporation unit on	1-off, 2-on	1-off, 2-on	on	TES in evaporator #1 frozen
Compressor shut down	1-off, 2-on	1-off, 2-on	off	Condensing unit power off
Quiescent state, cooling by TES	1-off, 2-on	1-off, 2-on	off	Cooling until sensor detects that a TES module has reached a minimum degree of freeze

For the regular cycle presented in Table 2, the use a condensing unit smaller than the size required for a conventional single-stage refrigeration system is permitted. This smaller condensing unit is less costly as well as produces less noise and occupies less volume than the larger or multiple condensing units associated with conventional refrigeration systems. Also, the implementation of TES modules can provide enhanced cooling.

Referring now to FIG. **2**, FIG. **10** and Table 3, an illustrative embodiment of the control protocol used to support an energy efficient defrost cycle for the multi-stage refrigeration system of FIG. **2** is shown. The defrost cycle is performed prior to the regular cycle. In addition, the defrost cycle is not performed immediately prior to the quiescent state because refrigerant is removed from evaporation tubes of the first evaporation unit.

For the defrost cycle, the compressor is turned on while the first valve is placed in the second setting and the second valve is placed in the first setting (Step **800**). This causes refrigerant to be removed from the first evaporation unit, namely the evaporation tube **520** of FIG. **5**. Next, the compressor is turned off and the second valve is placed in the second setting to avoid unwanted material from passing through the second valve (Step **810**). As a result, evaporation tube **520** of FIG. **5** no longer acts as a heat pipe when heated by a heater as described by U.S. Pat. Nos. 4,756,164 and 4,712,387, both of which are incorporated by reference herewith. Thereafter, defrosting proceeds and when completed, the regular cycle of FIG. **9** is initiated (Steps **820** and **830**).

TABLE 3

State of Valves and Compressor for the Defrost Cycle.

Defrost cycle stages	First Valve	Second Valve	Compressor	Must be run prior to Regular cycle and not immediately prior to quiescent state because the first evaporation unit is left with no refrigerant
Defrost cycle initiation	1-off, 2-on	1-on, 2-off	on	Refrigerant is removed from the first evaporation unit

TABLE 3-continued

State of Valves and Compressor for the Defrost Cycle.

Defrost cycle stages	First Valve	Second Valve	Compressor	Must be run prior to Regular cycle and not immediately prior to quiescent state because the first evaporation unit is left with no refrigerant
Defrost, (Frost removed by heater, heat from fresh food section, or other source)	1-6ff, 2-on	1-off, 2-on	off	Allow frost to melt from heat exchange surface.

Referring back to FIGS. **4A–4C** and Table 1, the control protocol of the multi-stage refrigeration system of FIG. **4A** minimizes the start-up transient losses described above. This is accomplished by turning on the compressor and overriding the second and fourth valves **420** and **440**. As a result, refrigerant is circulated between the condensing unit and the second evaporation unit **170** as shown in FIG. **4A**. This minimizes the amount of time to reach steady-state.

Next, one or more degree of freeze indicators are used to control the flow of refrigerant through the second and fourth valves **420** and **440** into evaporation units **130** and **170** based on a measured degree of freeze of the TES modules located in evaporation units **130** and **170**. For example, after a predetermined time period or after a selected amount of the TES module of second evaporation unit **170** has been frozen, the second and fourth valves **420** and **440** operate as normal check valves and the first and third valves **410** and **430** are overridden so that refrigerant is now circulated between first evaporation unit **130** and the condensing unit.

When the TES module in first evaporation **130** unit is determined to be sufficiently frozen as detected by an degree of freeze indicator (e.g., one or more position sensors), the first and third valves **410** and **430** are again set to operate as normal check valves to prevent refrigerant flow while the second and fourth valves **420** and **440** are overridden so that refrigerant is circulated between second evaporation unit **170** and the condensing unit. Thereafter, when the TES module in second evaporation unit **170** is determined to be sufficiently frozen, the compressor of the condensing unit is turned off while all of the valves **410**, **420**, **430** and **440** return to their normal operations in preventing refrigerant flow.

When either of the TES modules reach a "minimum degree of freeze" which represents a predetermined amount of TES material being frozen, the compressor of the condensing unit is turned on and the sequence described above and listed in Table 1 is repeated.

With respect to undergoing a defrost cycle prior to the regular cycle as set forth in Table 1, the compressor is briefly turned on and whereupon the third valve **430** allows refrigerant to be removed from the evaporation tubes of the first evaporation unit **130** of FIG. **4A**. Next, the compressor is turned off and the third valve returns to its normal check valve operations. As a result, evaporation tube **520** of FIG. **5** no longer acts as a heat pipe to allow defrosting to proceed. When defrosting has completed, the regular cycle is initiated.

While this invention has been described with reference to illustrative embodiments, this description is not intended to be construed in a limiting invention pertains, are deemed to lie within the spirit and scope of the invention. Thus, the invention should be measured in terms of the claims which follow.

What is claimed is:

1. A refrigeration system comprising:

a condensing unit;

a first valve connected to the condensing unit;

a second valve connected to the condensing unit;

a first evaporation unit connected to the first valve and the second valve, the first evaporation unit receiving a refrigerant for cooling when the condensing unit is turned on, the first valve is set to a first setting and the second valve is set to the first setting; and

a second evaporation unit connected to the first valve and the second valve, the second evaporation unit receiving the refrigerant for cooling when the condensing unit is turned on, the first valve is set to a second setting and the second valve is set to the second setting.

2. The refrigeration system of claim **1**, wherein both the first and second valves are selector valves, each selector valve is capable of being automatically adjusted from the first setting to the second setting.

3. The refrigeration system of claim **1**, wherein the condensing unit includes

a compressor directly connected to the second valve in which the condensing unit is considered turned on when the compressor is operational;

a condenser connected to the compressor; and

a reservoir connected to the condenser and the first valve in which the condensing unit is turned on when the compressor is operational.

4. The refrigeration system of claim **1**, wherein the first evaporation unit includes

a containment vessel;

a first evaporator enclosed within the containment vessel, the first evaporator formed with at least one evaporation tube; and

a first expandable container enclosed within the containment vessel, the first expandable container containing thermal energy storage (TES) material placed adjacent to a portion of the at least one evaporation tube.

5. The refrigeration system of claim **4**, wherein the containment vessel of the first evaporation unit is filled with a thermal coupling solution.

6. The refrigeration system of claim **4**, wherein the first evaporator includes

a lower heat exchanger formed by a first segment of the at least one evaporation tube, the lower heat exchanger including an inlet and an outlet for the refrigerant; and

an upper heat exchanger formed by a second segment of the at least one evaporation tube, the upper heat exchanger having the first expandable container placed adjacent to a portion of the upper heat exchanger.

7. The refrigeration system of claim **4**, wherein the first expandable container includes

a first sheet including an array of closely spaced, high aspect ratio protrusions which form a plurality of cavities, the array of protrusions of the first sheet are situated adjacent and generally perpendicular to the at least one evaporation tube; and

a first backing sheet sealed to the first sheet to prevent leakage of the TES material.

8. The refrigeration system of claim **4**, wherein the first expandable container further includes

a second sheet including an array of closely spaced, high aspect ratio protrusions, the array of protrusions of the second sheet are situated to interlock with the plurality of cavities associated with the first sheet; and

a second backing sheet sealed to the second sheet to prevent leakage of the TES material.

9. The refrigeration system of claim **4** further comprising a degree of freeze indicator to monitor at least one characteristic of the first expandable container.

10. The refrigeration system of claim **5**, wherein the second evaporation unit includes

a containment vessel filled with the thermal coupling solution;

a second evaporator enclosed within the containment vessel, the second evaporator including a lower heat exchanger having evaporator fins and an upper heat exchanger, the lower heat exchanger and the upper heat exchanger are formed by at least one evaporation tube; and

a second expandable container enclosed within the containment vessel, the second expandable container containing the TES material is placed adjacent to the upper heat exchanger.

11. A refrigeration system comprising:

a condensing unit;

a first set of valves connected to the condensing unit;

a second set of valves connected to the condensing unit;

a first evaporation unit connected to the first set of valves, the first evaporation unit receiving a refrigerant for cooling when the condensing unit is turned on and each valve of the first set of valves is overridden to provide a first flow path for the refrigerant; and

a second evaporation unit connected to the second set of valves, the second evaporation unit receiving the refrigerant for cooling when the condensing unit is turned on and each valve of the second set of valves is overridden to provide a second flow path for the refrigerant.

12. The refrigeration system of claim **11**, wherein each valve of the first and second sets of valves is a check valve.

13. The refrigeration system of claim **11**, wherein the first evaporation unit includes

a containment vessel;

a first evaporator enclosed within the containment vessel, the first evaporator formed with at least one evaporation tube; and

a first expandable container enclosed within the containment vessel, the first expandable container containing thermal energy storage (TES) material placed adjacent and generally perpendicular to a portion of the at least one evaporation tube.

14. The refrigeration system of claim **13** further comprising a degree of freeze indicator to monitor a characteristic of the first expandable container.

15. A method for refrigeration comprising the steps of:

turning on a compressor;

placing a plurality of valves in a first state to provide refrigerant to a first evaporation unit of a plurality of evaporation units, the first evaporation unit having a higher steady-state temperature than a second evaporation unit of the plurality of evaporation units; and

placing the plurality of valves in a second state when a thermal energy storage (TES) material contained in the first evaporation unit has reached a minimum degree of freeze.

16. The method of claim **15** further comprising the steps of:

placing the plurality of valves in the first state when the TES material contained in the second evaporation unit has achieved a predetermined degree of freeze; and

shutting off the compressor when the TES material contained in the first evaporation unit has reached the predetermined degree of freeze.

17. A method for defrosting a first evaporation unit of a multi-stage refrigeration system including (i) a first valve connecting a condensing unit to the first evaporation unit and a second evaporation unit and (ii) a second valve connecting the first evaporation unit and the second evaporation unit to the condensing unit, the method comprising the steps of:

placing the first valve at a second setting to establish a flow path between the condensing unit and the second evaporation unit;

placing the second valve at a first setting to establish a flow path between the condensing unit and the first evaporation unit;

turning on the condensing unit to remove a refrigerant from the first evaporation unit;

placing the second valve at a second setting to establish a flow path between the second evaporation unit and the condensing unit; and

shutting off the condensing unit.

18. A method for defrosting a first evaporation unit of a multi-stage refrigeration system including (i) a first set of check valves connecting a condensing unit to the first evaporation unit, the method comprising the steps of:

turning on a compressor of the condensing unit to override a check valve by opening the check valve of the first set of check valves in order to remove a refrigerant from the first evaporation unit; and

turning off the compressor to close the check valve.

* * * * *