



US006266257B1

(12) **United States Patent**
Geissler

(10) **Patent No.:** **US 6,266,257 B1**
(45) **Date of Patent:** **Jul. 24, 2001**

(54) **POWER CONVERTOR WITH LOW LOSS SWITCHING**

(75) Inventor: **Steven Geissler**, Little Chute, WI (US)

(73) Assignee: **Illinois Tool Works Inc.**, Glenview, IL (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **09/495,969**

(22) Filed: **Feb. 2, 2000**

5,414,613	5/1995	Chen .	
5,418,704	5/1995	Hua et al. .	
5,438,498	* 8/1995	Ingemi	363/132
5,477,131	12/1995	Gegner .	
5,563,777	10/1996	Miki et al. .	
5,570,279	10/1996	Venkataramanan .	
5,574,636	11/1996	Lee et al. .	
5,594,629	1/1997	Steigerwald .	
5,598,326	1/1997	Liu et al. .	
5,601,741	2/1997	Thommes .	
5,615,101	3/1997	Moriarty .	
5,636,114	6/1997	Bhagwat et al. .	
5,654,880	8/1997	Brkovic et al. .	
5,841,268	* 11/1998	Mednik	323/222
6,021,053	* 2/2000	Baskette et al.	363/40
6,061,253	5/2000	Igarashi et al. .	

Related U.S. Application Data

(62) Division of application No. 09/111,950, filed on Jul. 9, 1998, now Pat. No. 6,115,273.

(51) **Int. Cl.**⁷ **H02M 7/122**

(52) **U.S. Cl.** **363/56**

(58) **Field of Search** 363/55, 56, 97, 363/98, 131, 132, 56.02, 56.03, 56.05

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,375,077	2/1983	Williams .	
4,769,754	9/1988	Reynolds et al. .	
4,849,873	* 7/1989	Vandehelst	363/55
4,857,822	8/1989	Tabisz et al. .	
5,010,471	4/1991	Klaassens et al. .	
5,047,913	* 9/1991	De Doncker et al.	363/95
5,166,549	11/1992	Dedoncker .	
5,270,914	12/1993	Lauw et al. .	
5,307,005	4/1994	Ahladas et al. .	
5,313,382	5/1994	Farrington .	
5,321,348	6/1994	Vinciarelli et al. .	
5,343,016	8/1994	Davis et al. .	
5,343,140	8/1994	Gegner .	
5,412,310	5/1995	Wolk et al. .	

* cited by examiner

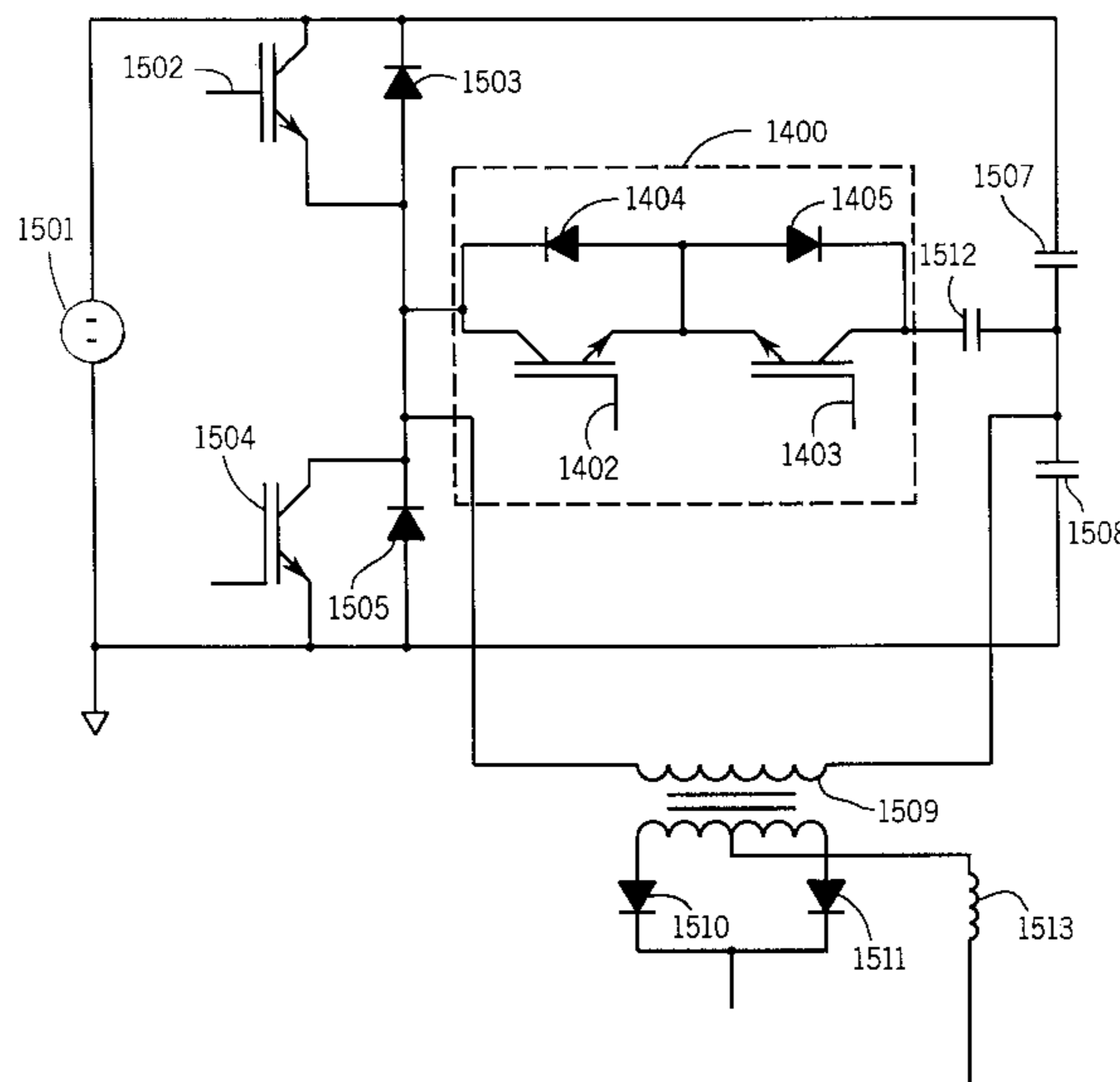
Primary Examiner—Matthew Nguyen

(74) *Attorney, Agent, or Firm*—George R. Corrigan

(57) **ABSTRACT**

A welding power supply includes an input rectifier that receives sinusoidal or alternating line voltage and provides a rectified voltage. A pre-regulator provides a dc bus and a convertor, such as a boost convertor, provides a welding output. The pre-regulator is an SVT (slow voltage transition) and an SCT (slow current transition) switched convertor. It may include a snubber circuit having a diode that is SVT switched. Also, the boost convertor may be SVT and SCT switched. The pre-regulator preferably includes a power factor correction circuit. The power source includes, in one embodiment, an inverter having a snubber circuit having a first switch in anti-parallel with a first diode, and a second switch in anti-parallel with a second diode. The first switch and first diode are connected in series with the second switch and the second diode, and the first and second switches are connected in opposing directions, to form a switched snubber.

11 Claims, 12 Drawing Sheets



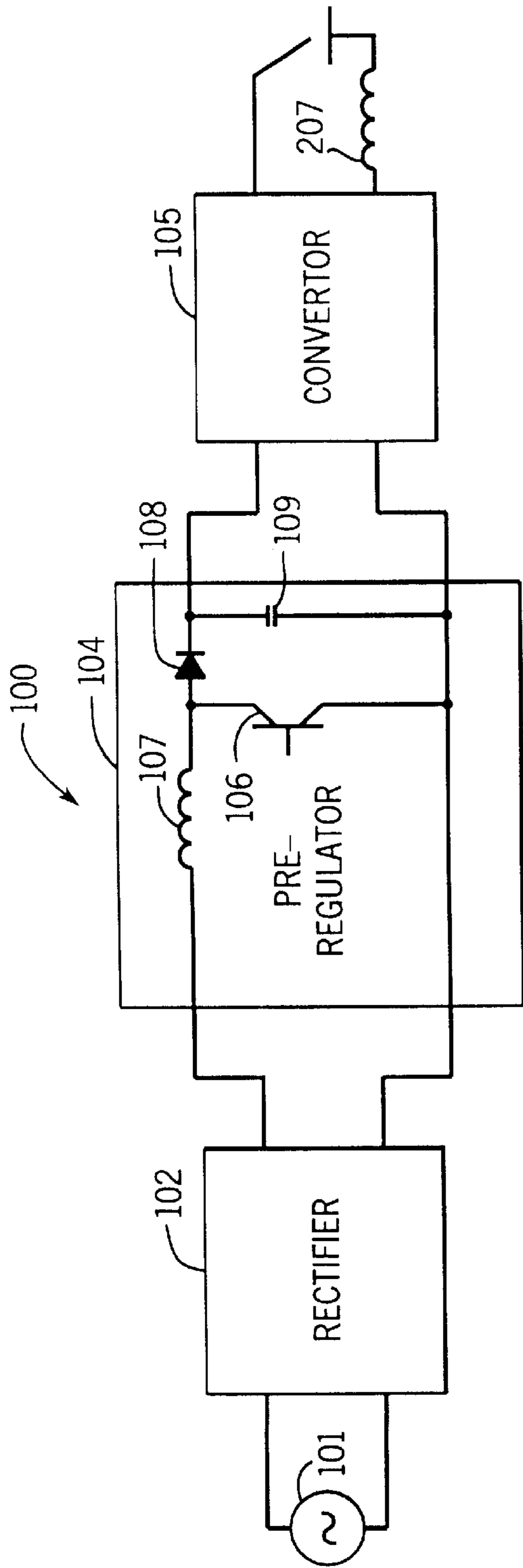


FIG. 1
PRIOR ART

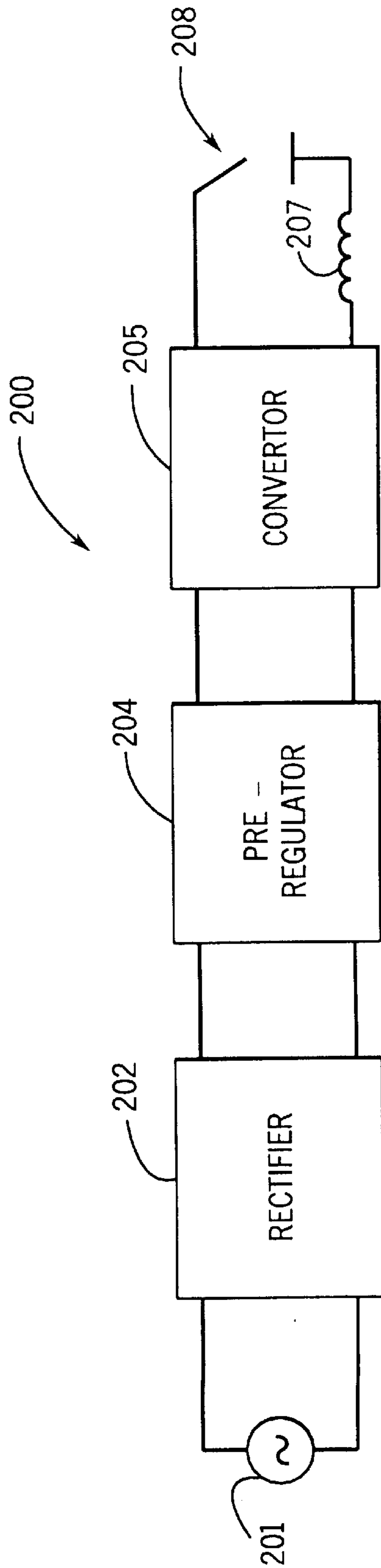
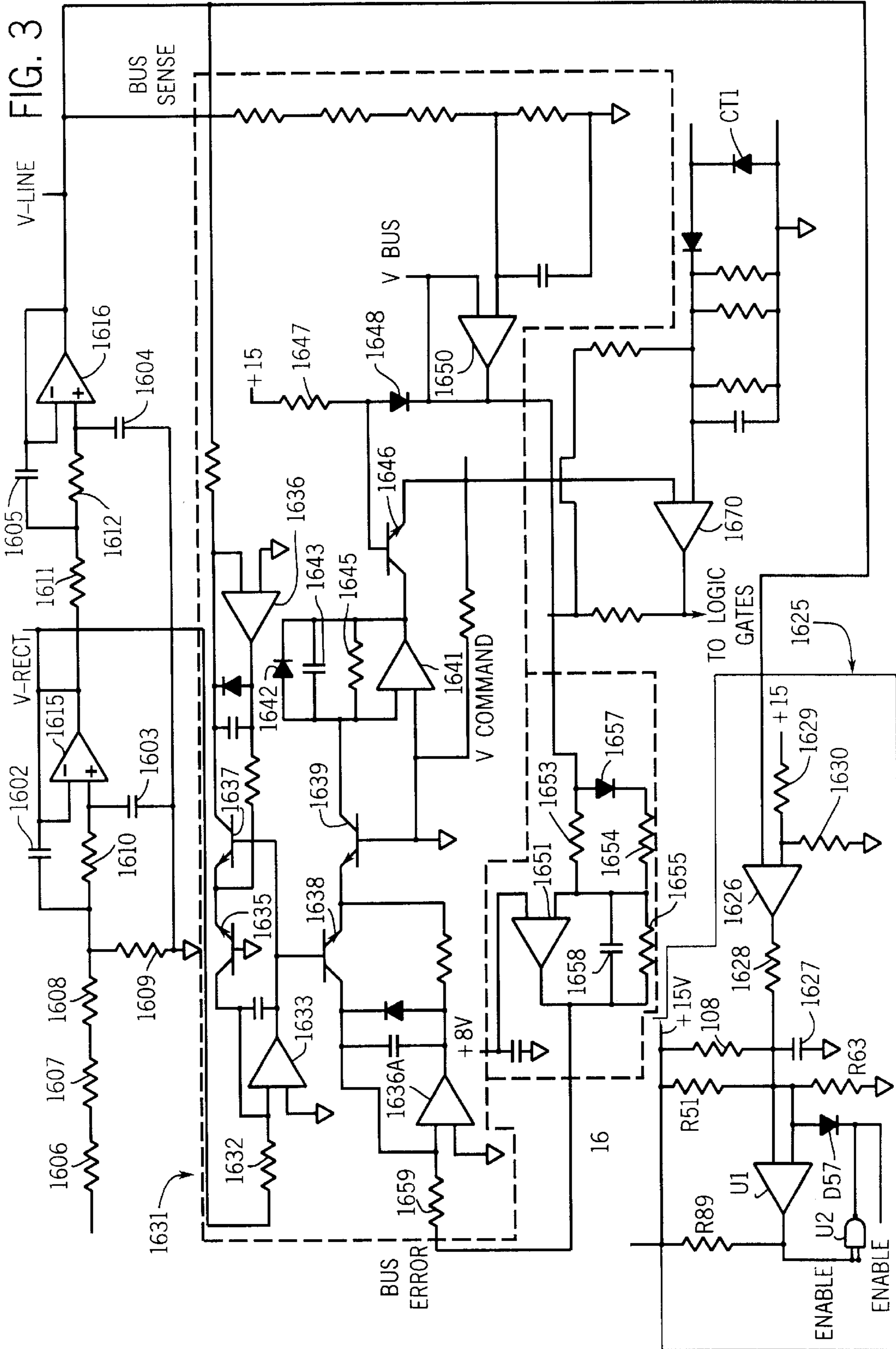


FIG. 2



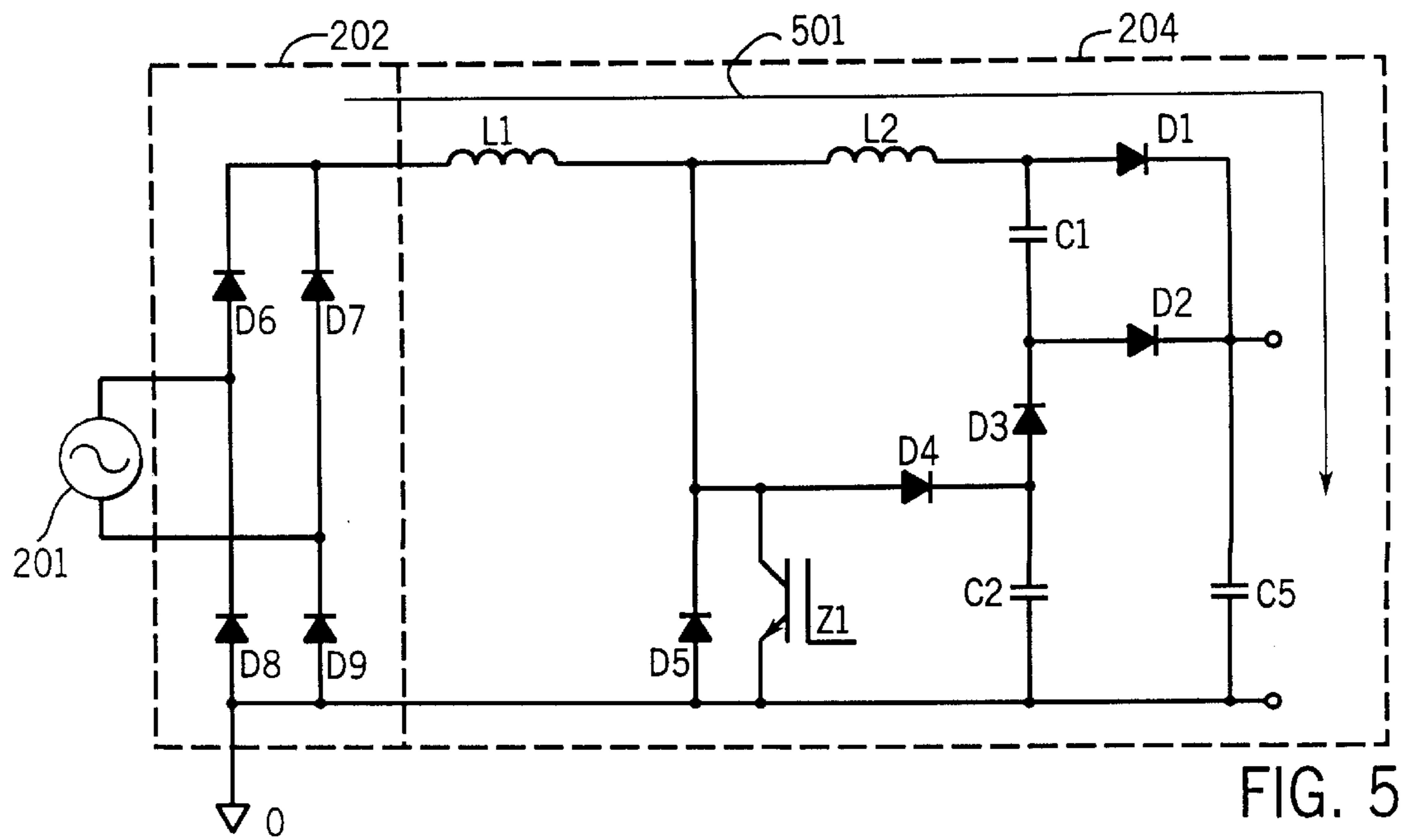
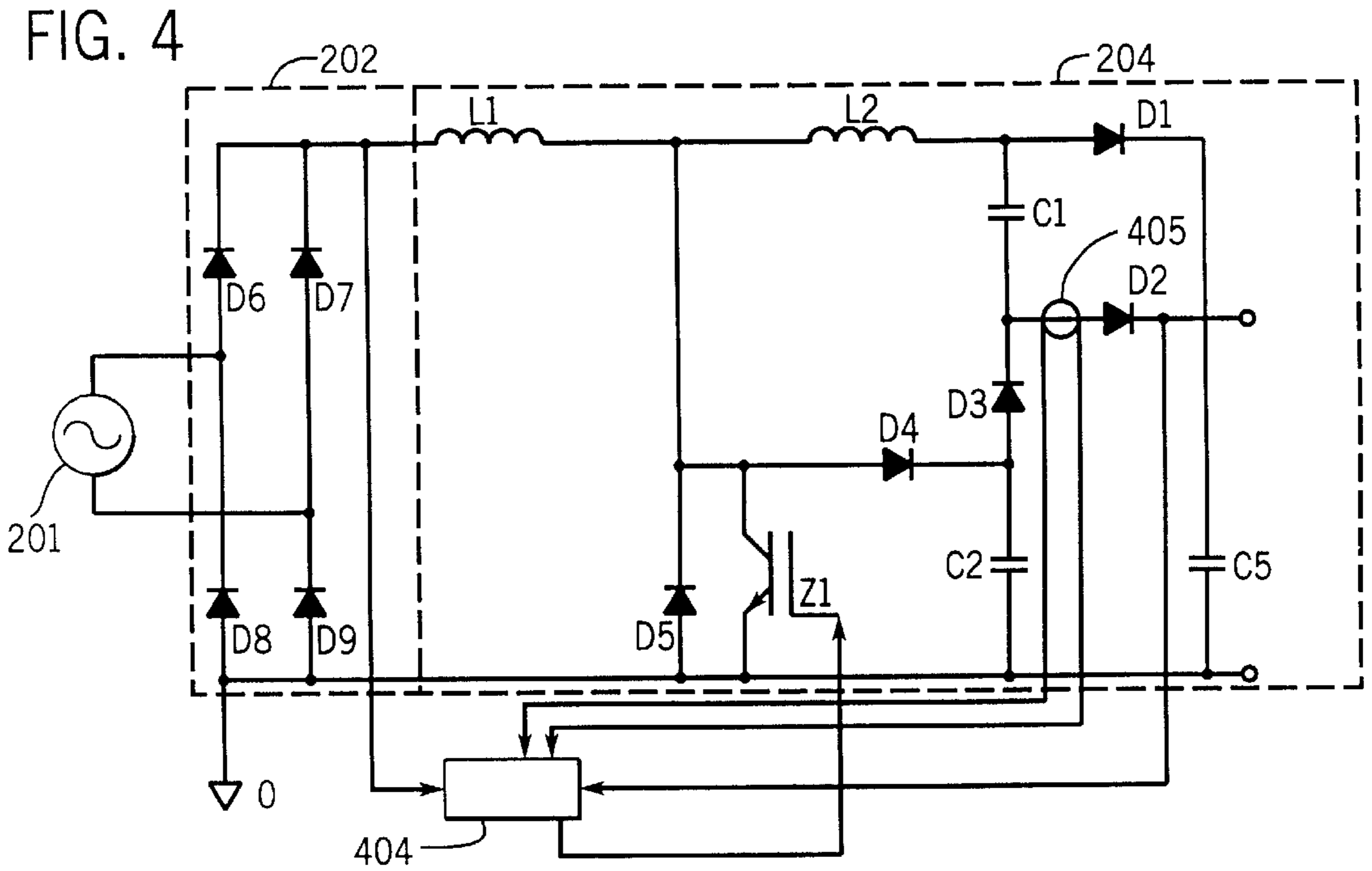


FIG. 6

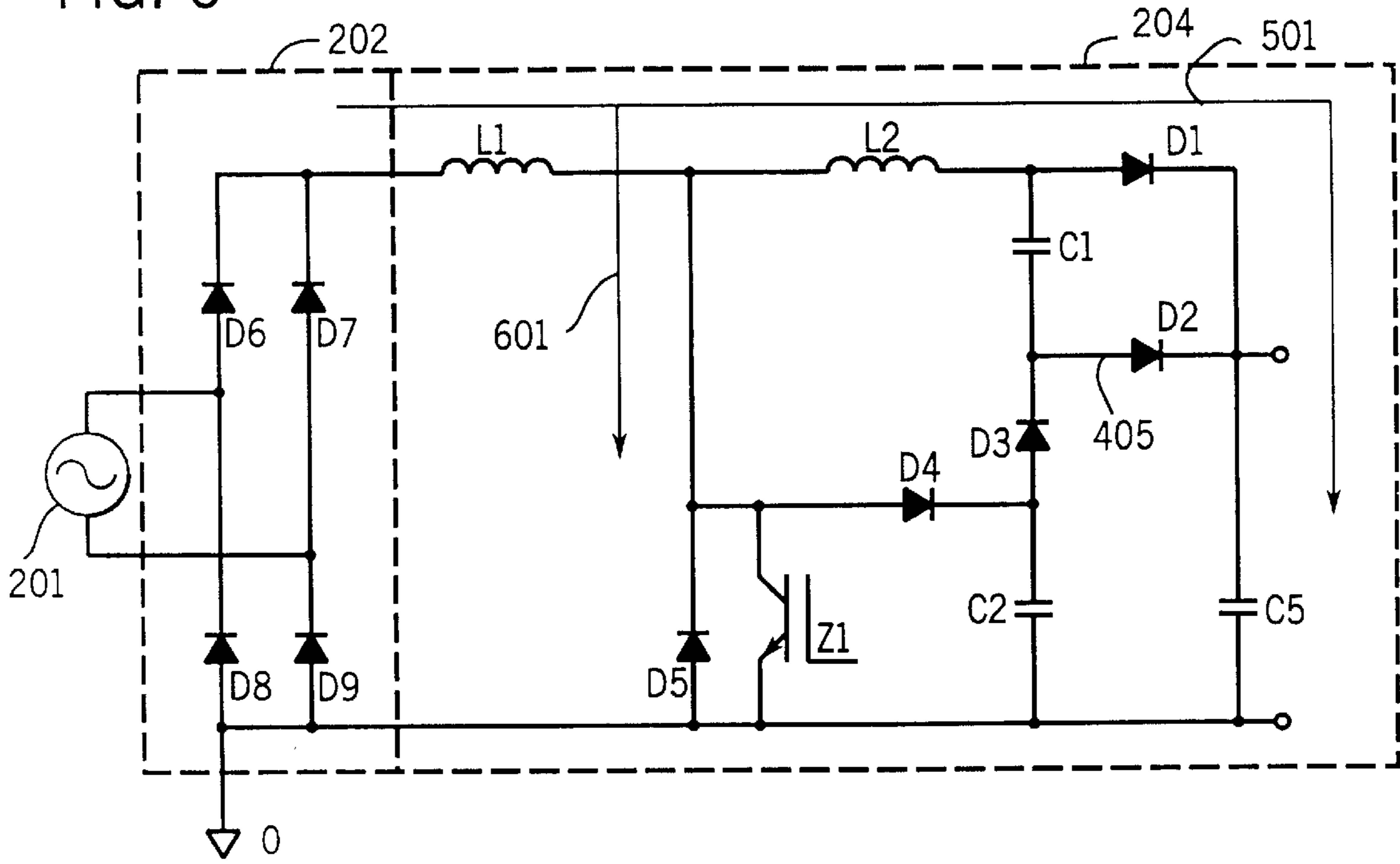


FIG. 7

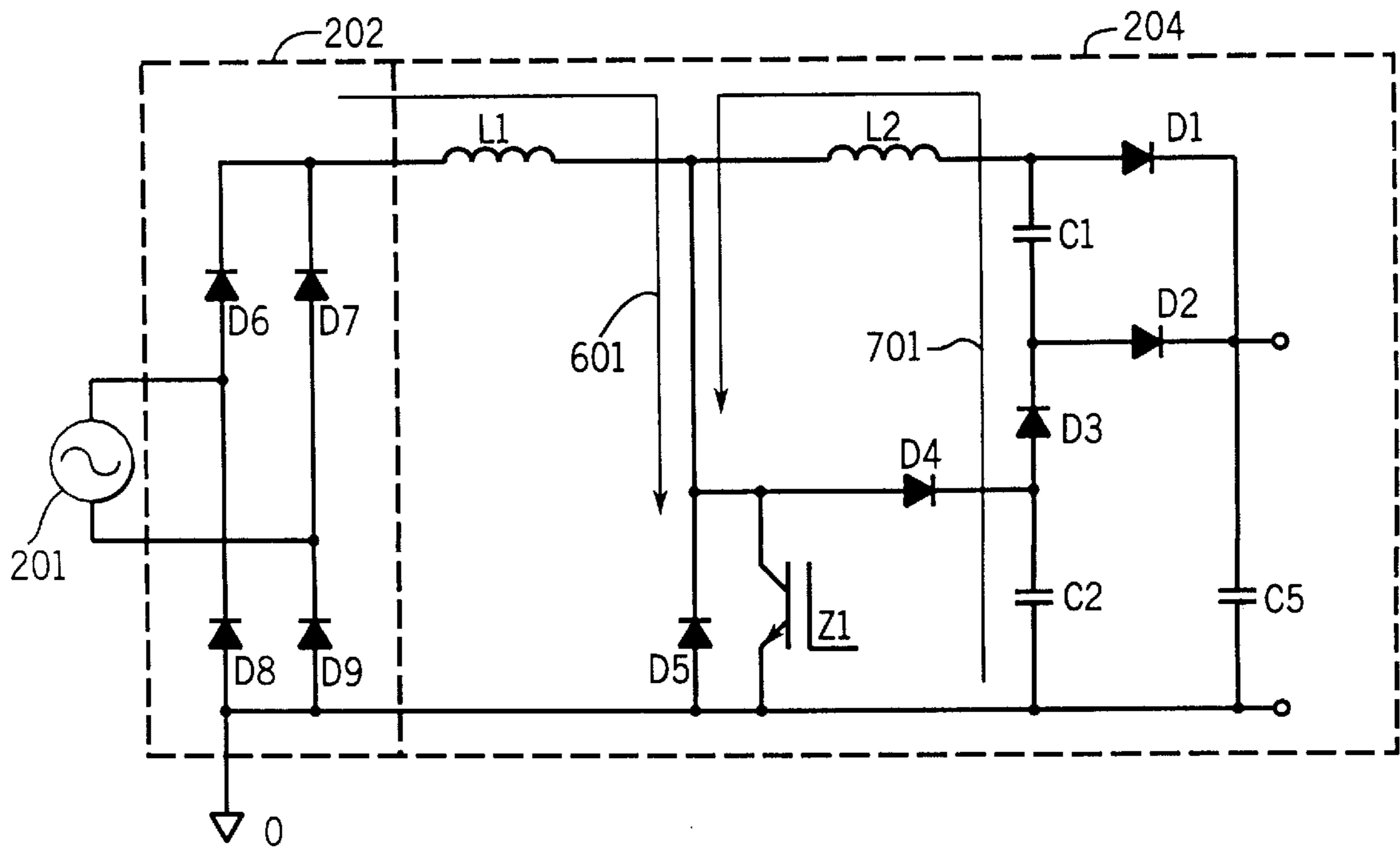


FIG. 8

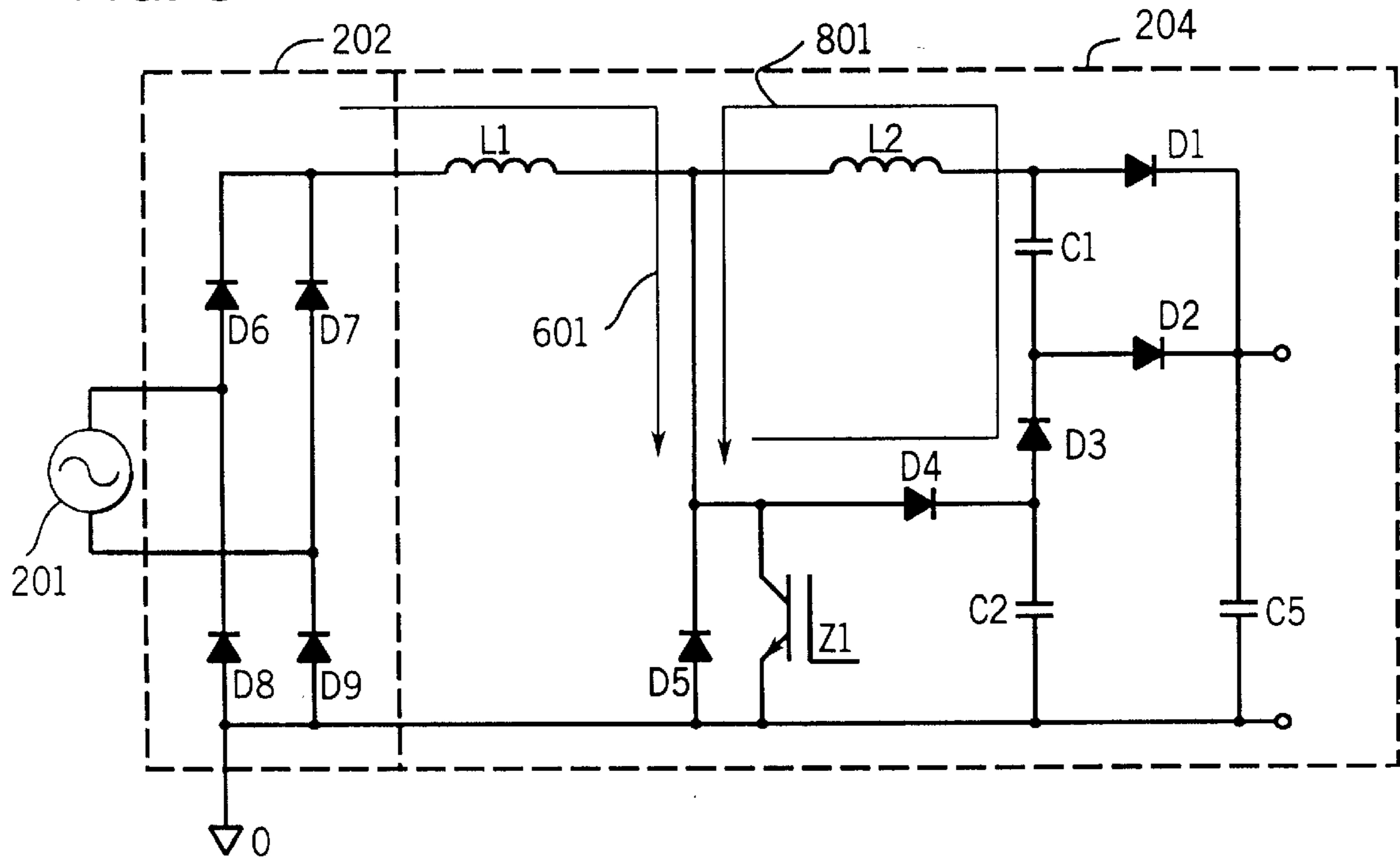


FIG. 9

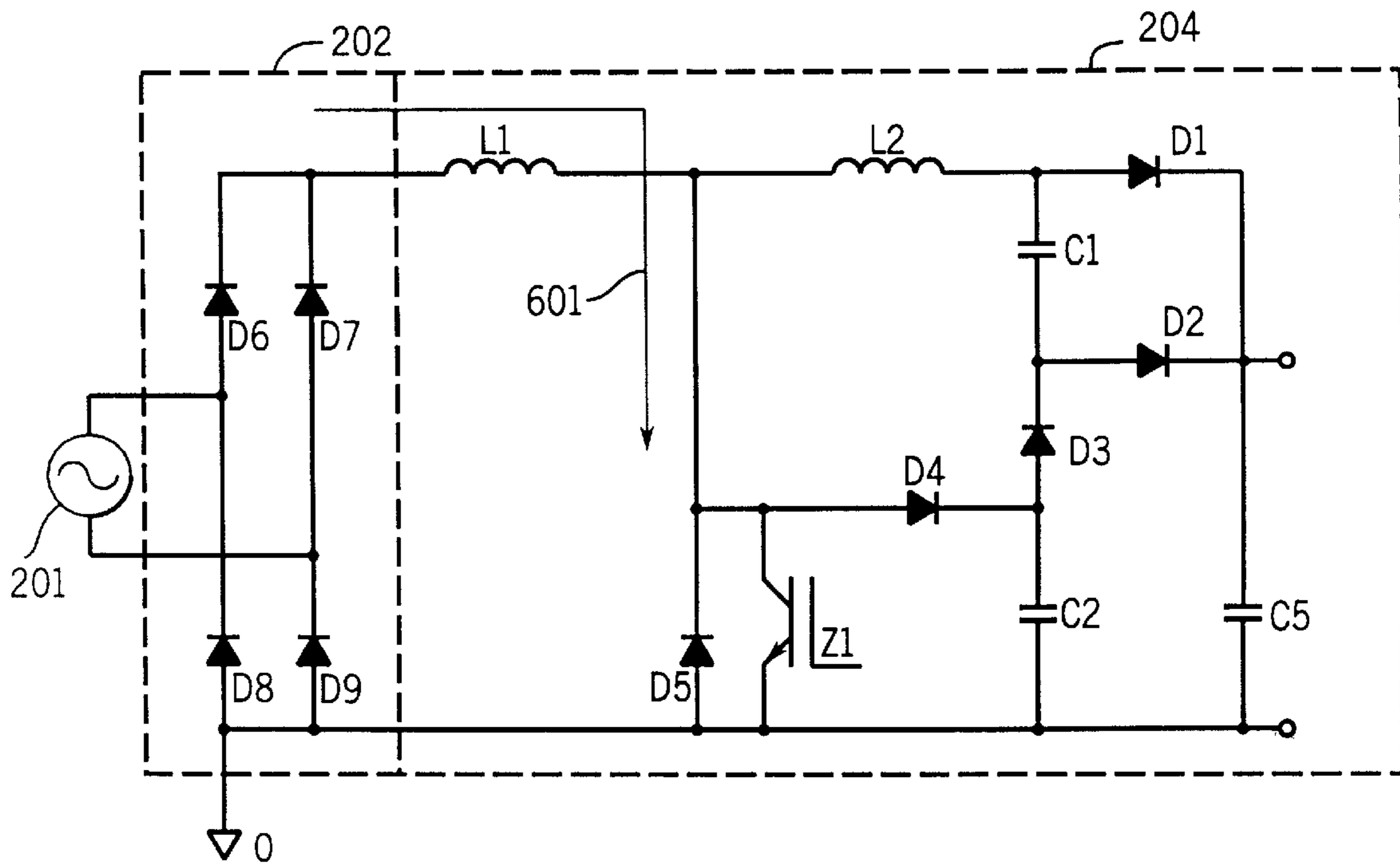


FIG. 10

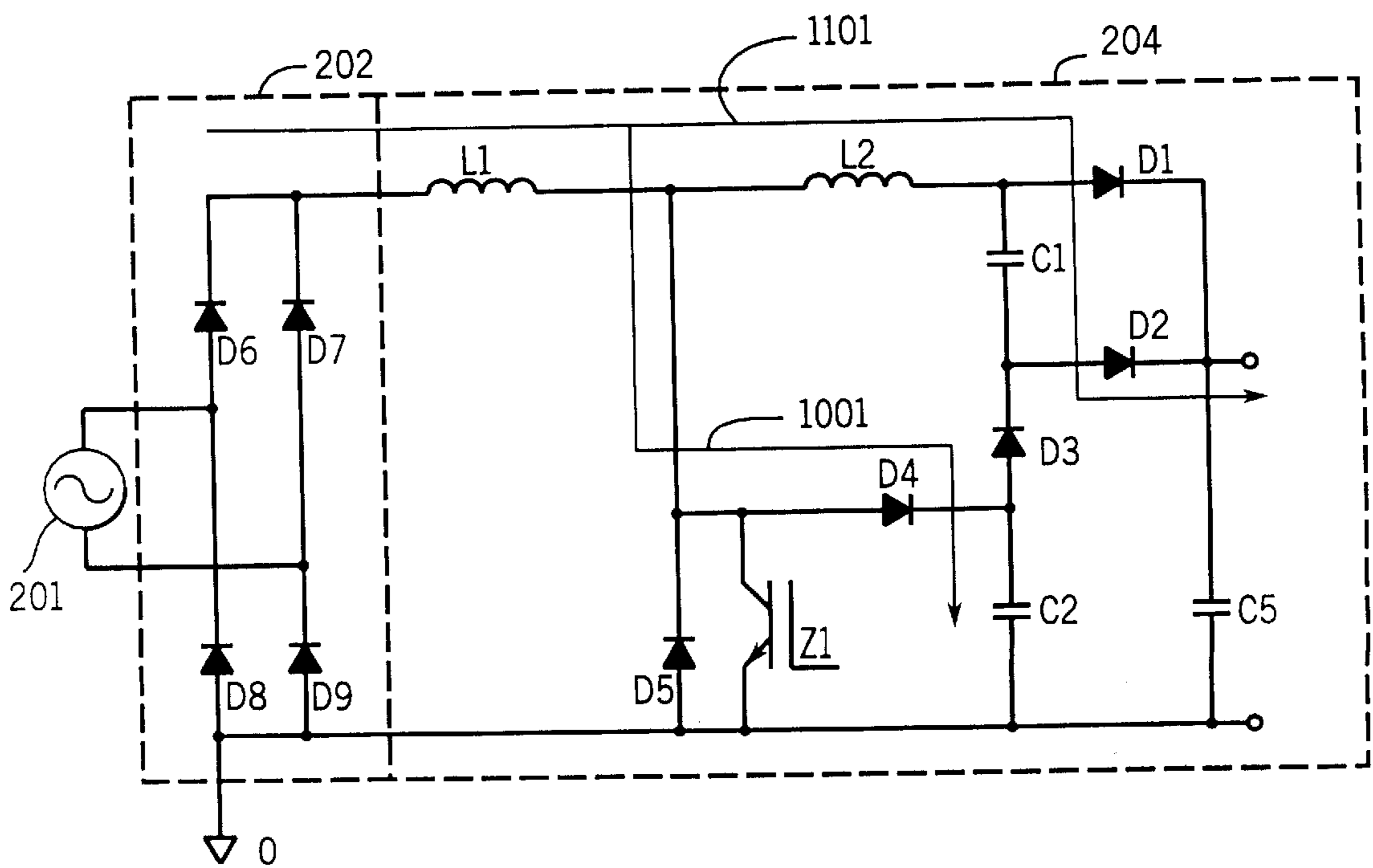
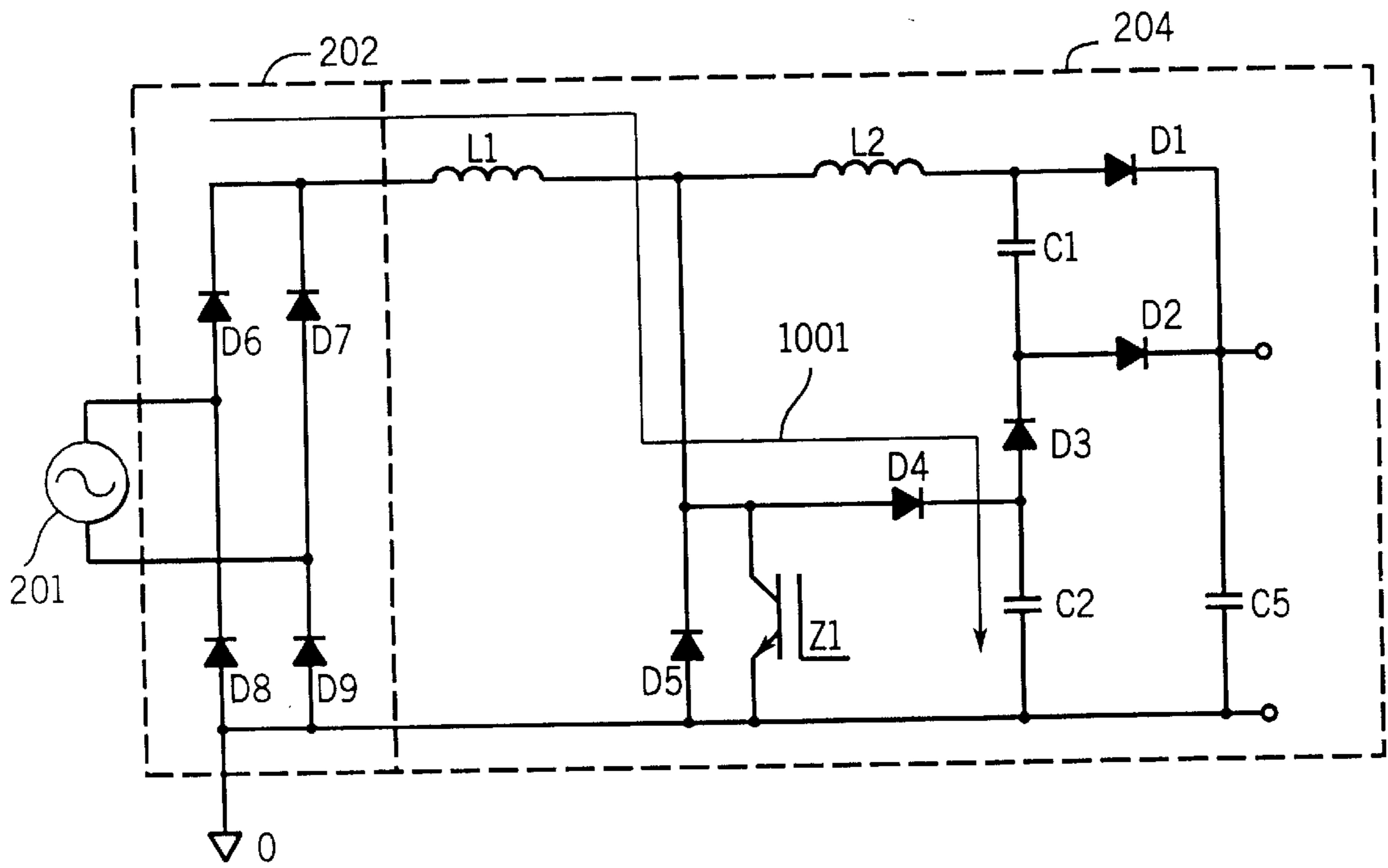


FIG. 11

FIG. 12

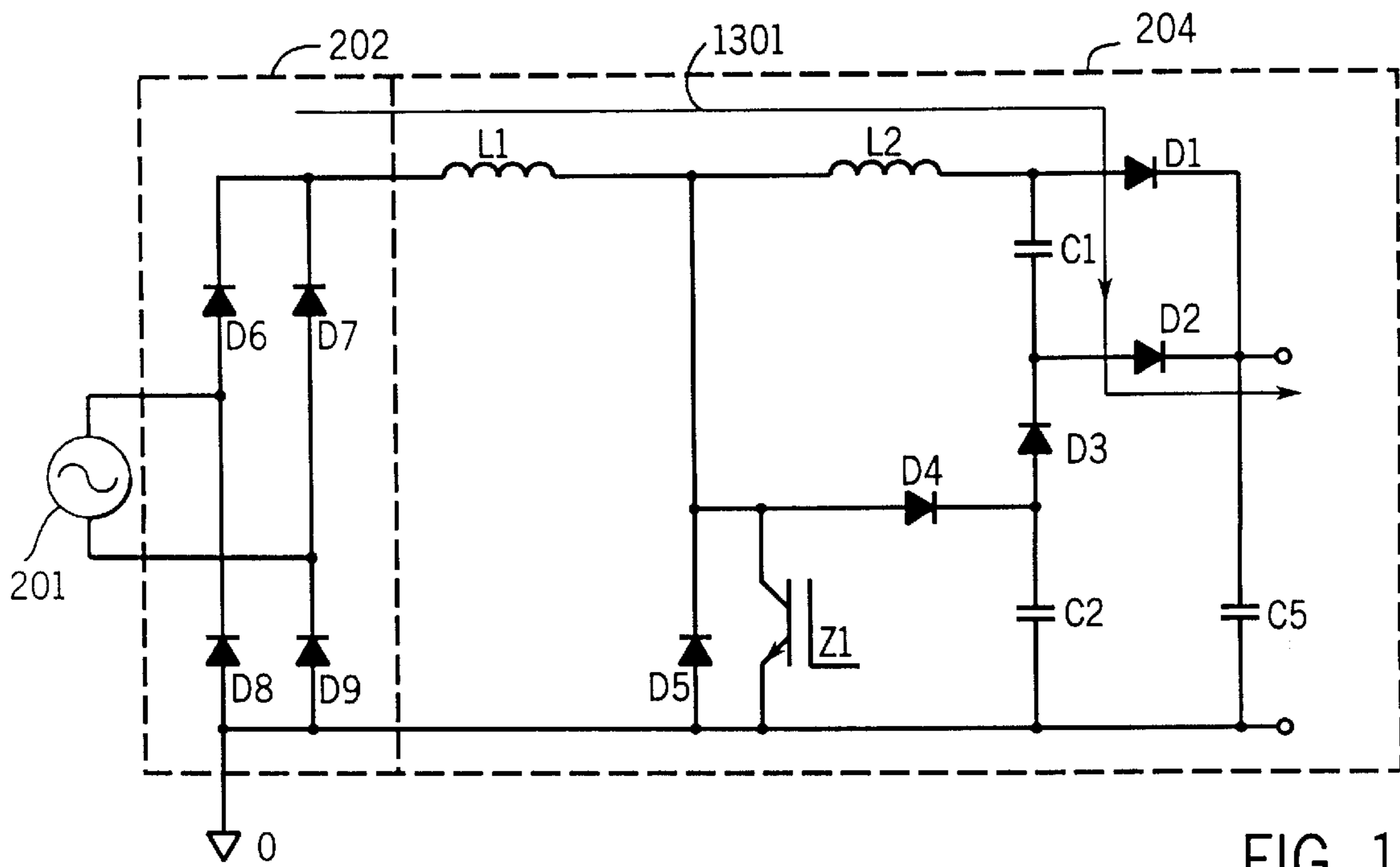
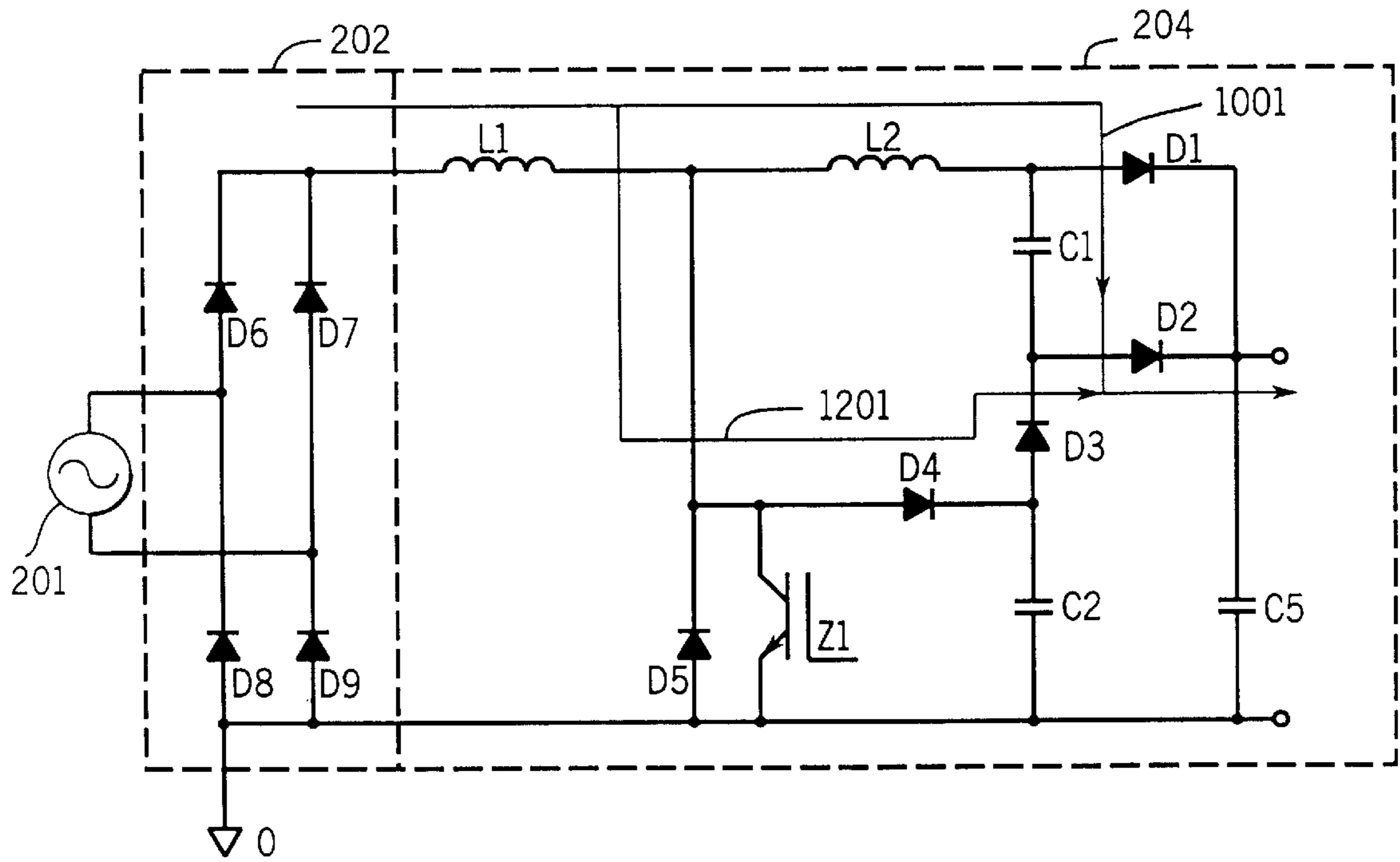


FIG. 13

FIG. 14

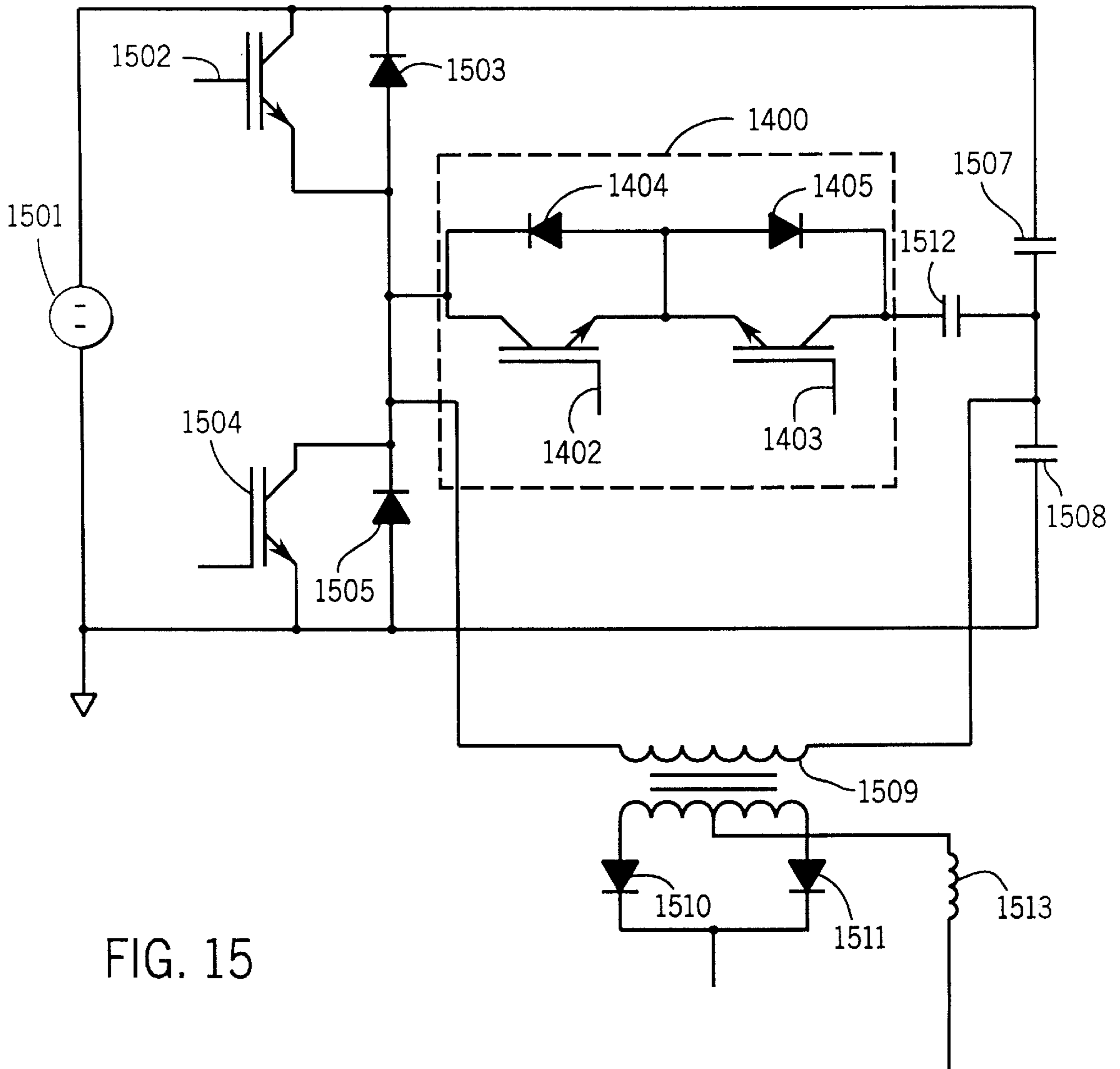
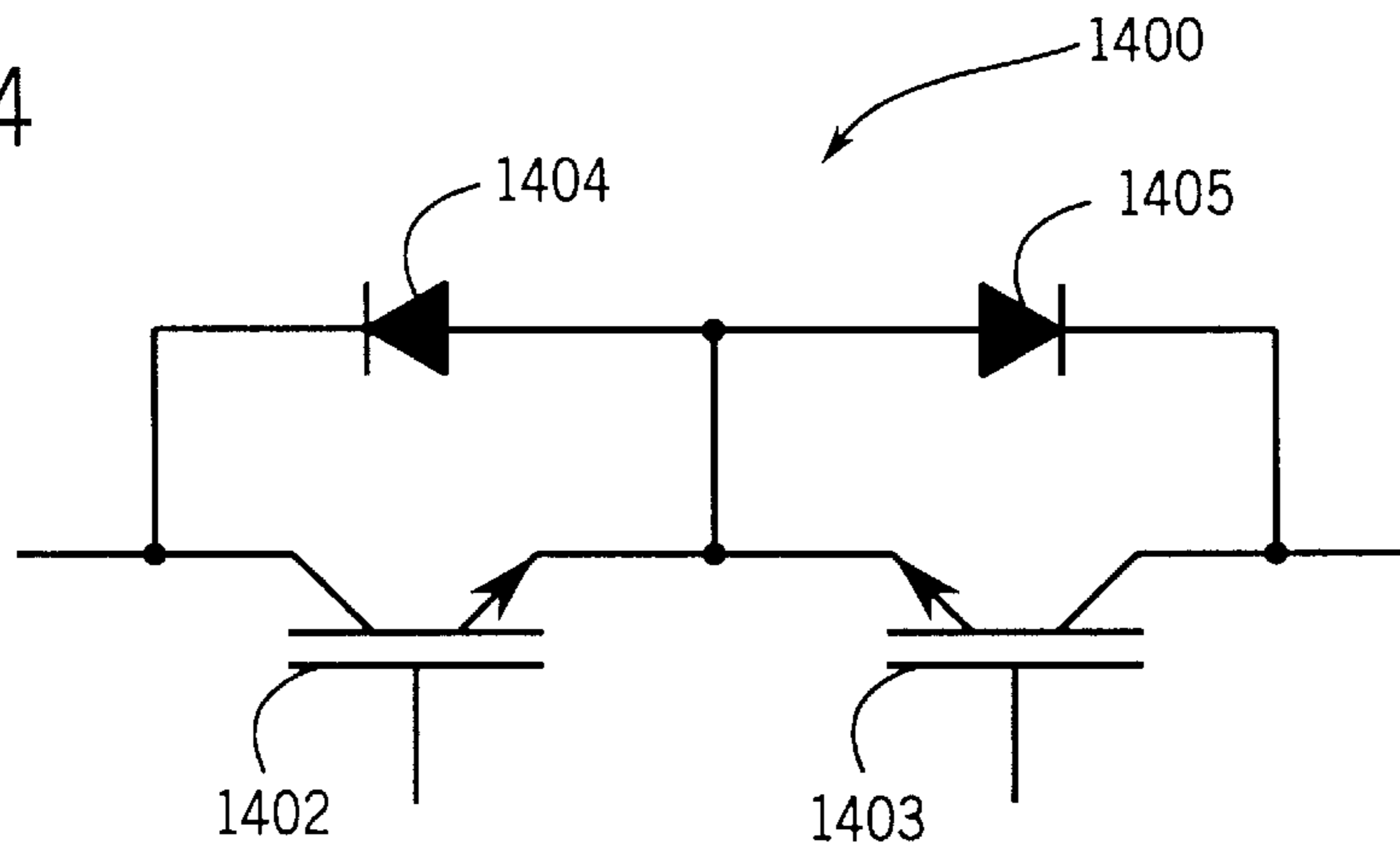
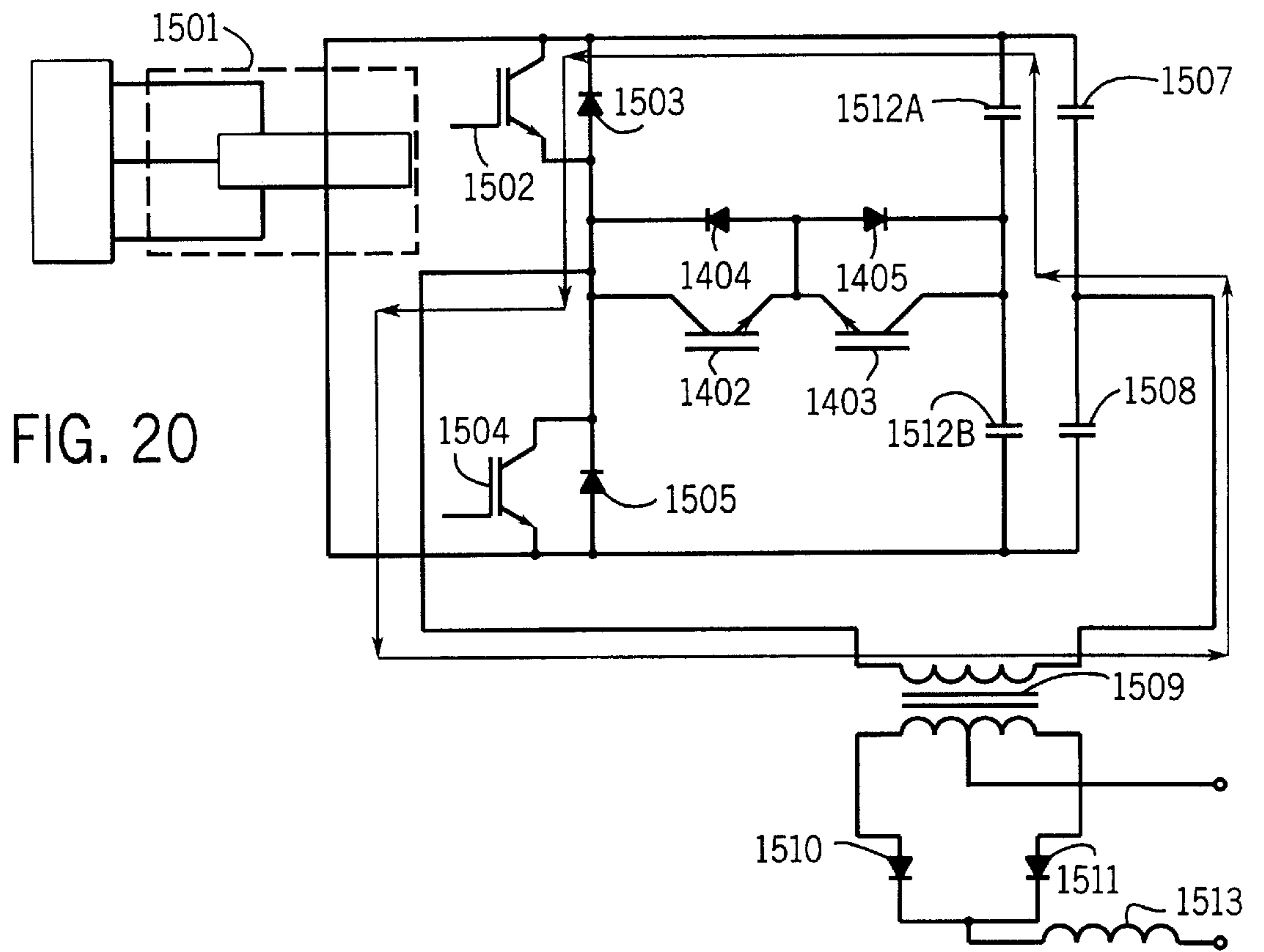
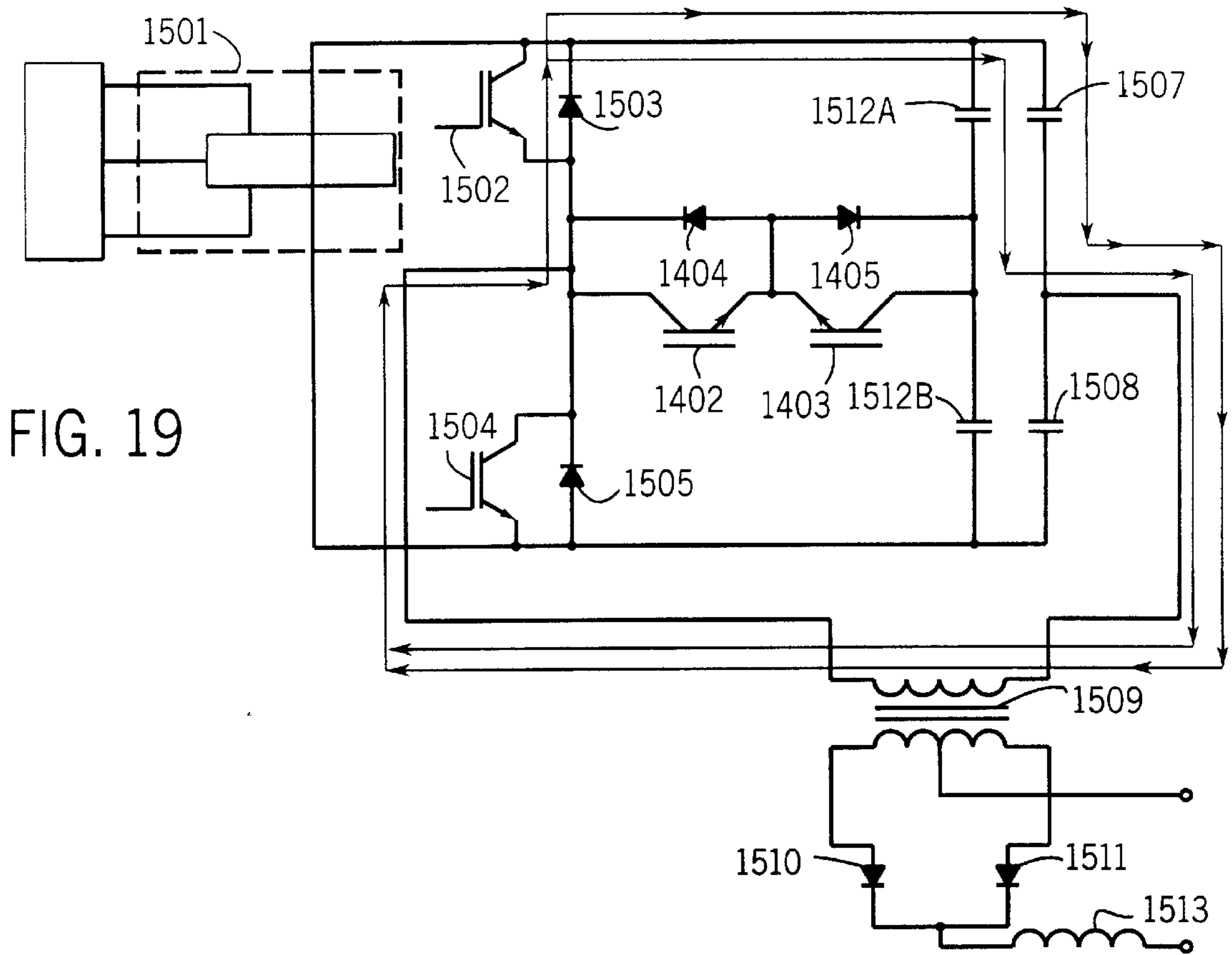


FIG. 15



POWER CONVERTOR WITH LOW LOSS SWITCHING

This new application is a divisional of, and claims the benefit of the filing date of, U.S. patent application Ser. No. 09/111,950, filed Jul. 9, 1998, entitled Power Converter With Low Loss Switching now U.S. Pat. No. 6,115,273.

FIELD OF THE INVENTION

This invention relates generally to power sources used in welding and, more particularly, to welding power sources that have a pre-regulator.

BACKGROUND OF THE INVENTION

Power sources typically convert a power input to a necessary or desirable power output tailored for a specific application. In welding applications, power sources typically receive a high voltage, alternating current, (VAC) signal and provide a high current welding output signal. Around the world, utility power sources (sinusoidal line voltages) may be 200/208 V, 230/240 V, 380/415 V, 460/480 V, 500 V and 575 V. These sources may be either single-phase or three-phase and either 50 or 60 Hz. Welding power sources receive such inputs and produce an approximately 10–75 volt, DC or AC high current welding output.

There are many types of welding power sources that provide power suitable for welding, including inverter-based welding power sources. As used herein, an inverter-type power supply includes at least one stage where DC power is inverted into ac power. There are several well known inverter type power sources that are suitable for welding. These include boost power sources, buck power sources, and boost-buck power sources.

Traditionally, welding power sources were designed for a specific power input. In other words, the power source cannot provide essentially the same output over the various input voltages. More recently, welding power sources have been designed to receive any voltage over a range of voltages, without requiring relinking of the power supply. One prior art welding power supply that can accept a range of input voltages is described in U.S. Pat. No. 5,601,741, issued Feb. 11, 1997 to Thommes, and owned by the assignee of the present invention, and is hereby incorporated by reference.

Many prior art welding power supplies include several stages to process the input power into welding power. Typically stages include an input circuit, a pre-regulator, an inverter and an output circuit that includes an inductor. The input circuit receives the line power, rectifies it, and transmits that power to the pre-regulator. The pre-regulator produces a dc bus suitable for conversion. The dc bus is provided to the inverter of one type or another, which provides the welding output. The output inductor helps provide a stable arc.

The pre-regulator stage typically includes switches used to control the power. The losses in switches can be significant in a welding power supply, particularly when they are hard switched. The power loss in a switch at any time is the voltage across the switch multiplied by the current through the switch. Hard switching turn-on losses occur when a switch turns on, with a resulting increase in current through the switch, and it takes a finite time for the voltage across the switch to drop to zero. Soft switching attempts to avoid turn-on losses by providing an auxiliary or snubber circuit with an inductor in series with the switch that limits the current until the transition to on has been completed, and the

voltage across the switch is zero. This is referred to as zero-current transition (ZCT) switching.

Similarly, hard switching turn-off losses also occur when a switch turns off, with a resultant rise in voltage across the switch, and it takes a finite time for the current through the switch to drop to zero. Soft switching attempts to avoid turn-off losses by providing an auxiliary or snubber circuit with a capacitor across the switch that limits the voltage across the switch until the transition to off has been completed, and the current through the switch is zero. This is referred to as zero-voltage transition (ZVT) switching.

There are numerous attempts in the prior art to provide soft-switching power converters or invertors. However, these attempts often either transfer the losses to other switches (or diodes) and/or require expensive additional components such as auxiliary witches and their control circuits. Thus, an effective and economical way of recovering (or avoiding) switching losses in power converters or invertors is desirable. Examples of various attempts at soft switching are described below.

U.S. Pat. No. 5,477,131, issued Dec. 19, 1995 to Gegner discloses a ZVT type commutation. However, a controlled auxiliary switch and a coupled inductor are needed to implement the ZVT. Also, the primary current is discontinuous.

Some prior art designs require discontinuous conduction mode for diode recovery. One such design is found in U.S. Pat. No. 5,414,613. This is undesirable because of excessive high frequency ripple in the power lines.

Gegner also disclosed a ZVS converter that operated in a multi-resonant mode in U.S. Pat. No. 5,343,140. This design produced relatively high and undesirable RMS current and RMS voltage.

Another multi-resonant converter is disclosed in U.S. Pat. No. 4,857,822, issued to Tabisz. This design causes undesirable high voltage stress during ZVS events and undesirable high current stress during ZCS events.

U.S. Pat. No. 5,307,005 also requires an auxiliary switch. Losses occur when the auxiliary switch is turned off. This merely shifts switching losses, rather than eliminating them. Other designs that “shift” losses are shown in U.S. Pat. Nos. 5,418,704 and 5,598,318.

A circuit that requires an auxiliary controlled switch but does not “shift” losses to the auxiliary switch is shown in U.S. Pat. No. 5,313,382. This is an improvement over the prior art that shifted losses, but still requires an expensive controlled switch.

Another design that avoided “loss shifting” is shown in U.S. Pat. No. 5,636,144. However, that design requires a voltage clamp for recovery spikes, and 3 separate inductors. Also, the voltages on the inductors is not well controlled.

A zero-current, resonant boost converter is disclosed in U.S. Pat. No. 5,321,348. However, this design requires relatively complex magnetics and high RMS current in the switches and magnitudes. Also, a high reverse voltage is needed for the boost diodes.

When it is not practical or cost effective to use a true ZCT and ZVT circuit, an approximation may be used. For example, slow voltage/current transitions (SVT and SCT) as used herein, describe transitions where the voltage or current rise is slowed (rather than held to zero), while the switch turns off or on.

A typical prior art welding power supply **100** with a pre-regulator **104** and an output convertor or inverter **105** is shown in FIG. 1. An input line voltage **101** is provided to a

rectifier **102** (typically comprised of a diode bridge and at least one capacitor). Pre-regulator **104** is a hard-switched boost converter which includes a switch **106** and an inductor **107**. A diode **108** allows a capacitor **109** to charge up by current flowing an inductor **107** when the switch **106** is turned off. The current waveform in inductor **107** is a rectified sinusoid with high frequency modulation (ripple).

The amount of ripple may be reduced by increasing the frequency at which switch **106** is switched. However, as the frequency at which a prior art hard switched boost converter is switched is increased to reduce ripple, the switching losses can become intolerable.

Another drawback of some prior art power supplies is a poor power factor. Generally, a greater power factor allows a greater power output for a given current input. Also, it is generally necessary to have more power output to weld with stick electrodes having greater diameters. Thus, a power factor correction circuit will allow a given welding power supply to be used with greater diameter sticks for a given line power. A prior art inverter that provided a good power factor is disclosed in U.S. Pat. Nos. 5,563,777. Many prior art convertors with power factor correction suffer from high switching losses. Examples of such prior art designs are found in U.S. Pat. Nos. 5,673,184; 5,615,101; and 5,654,880.

One type of known output convertor is a half-bridge, transformer isolated, inverter. However, such output invertors often have high switching losses and/or require passive snubber circuits (which increases losses) because each snubber must operate in both directions overall, but only in one direction at a time. Also, known snubber circuits generally have a limited range of acceptable loads and will not snub proportional to the load, thus the losses are relatively high for lower loads.

Accordingly, a power circuit that provides little switching losses and a high (close to unity) power factor is desirable. Also, the pre-regulator should be able to receive a wide range of input voltages without requiring relinking. A desirable output convertor will include a full wave, transformer isolated, inverter, that is soft switch and has full range, full wave, low loss snubber.

SUMMARY OF THE PRESENT INVENTION

According to a first aspect of the invention a welding power supply includes an input rectifier that receives sinusoidal or alternating line voltage and provides a rectified sinusoidal voltage. A pre-regulator receives the rectified input and provides a dc bus. An inverter connector across the bus provides a welding output. The pre-regulator is an SVT (slow voltage transition) and an SCT (slow current transition) switched inverter.

In one embodiment the pre-regulator includes a snubber circuit having diode that is SVT switched.

In another embodiment the inverter is a boost converter with a switch. The pre-regulator includes a snubber circuit having a capacitor and an inductor. The capacitor is connected to slow the switch voltage rise while the switch is turning off, and the inductor is connected to slow the switch current rise when the switch is turning on. The boost converter includes a boost inductor, a switch, and an output capacitor in another embodiment. Also, the snubber includes a snubber capacitor, a snubber inductor, a first snubber diode, a second snubber diode, a third snubber diode, a fourth snubber diode, and first and second snubber capacitors. The snubber inductor, switch, an fourth diode are connected such that current may flow from the boost induc-

tor to any of the snubber inductor, switch, and fourth diode. Current flowing through the fourth diode can flow through either the third diode or the second capacitor. Current flowing from the boost inductor through the snubber inductor can flow through either the first diode or the first capacitor. The fourth diode and the second capacitor are connected across the switch and current flowing through the third diode can flow through either the first capacitor and the snubber inductor or through the second diode. Current flowing through the first and second diodes flows to the output. A fifth diode is connected in anti-parallel to the switch in one embodiment.

A second aspect of the invention is a method of providing welding power by rectifying a sinusoidal or alternating input line voltage and pre-regulating the sinusoidal input line voltage to provide a dc bus. The method further includes SVT and SCT switching a boost convertor. The bus is converted to a welding output.

Pre-regulating includes, in one embodiment, maintaining a boost converter switch off, and allowing current to flow through a boost inductor, a snubber inductor, and a first diode, to the dc bus, and turning the switch on and diverting current from the snubber inductor to the switch. Current is reversed in the snubber inductor and a second capacitor is discharged through a first capacitor, a third diode, and the snubber inductor, thereby transferring energy from the second capacitor to the snubber inductor. Current is diverted through a fourth diode, the third diode and the first capacitor when the second capacitor is discharged, thereby transferring energy from the snubber inductor to the first capacitor. The switch is turned off and current diverted through the fourth diode and into the second capacitor. Voltage on the second capacitor is allowed to rise until current begins to flow from the snubber inductor to the first capacitor and then current is diverted from the second capacitor through a third diode to the second diode. The current from the boost inductor to the snubber inductor increases until all of the current from the boost inductor flows into the snubber inductor. Then current is diverted from the first capacitor to the first diode. This process is repeated.

One embodiment includes SVT turning off a diode in a snubber circuit. Another includes slowing the switch voltage with a capacitor rise while the switch is turning off, and slowing the switch current rise with an inductor while the switch is turning on to SVT and SCT switching a boost convertor.

A third aspect of the invention is a welding power supply having an input rectifier that provides a rectified voltage. A pre-regulator receives as an input the rectified signal and provides a dc bus. An inverter converts the bus to a welding output and the pre-regulator includes a power factor correction circuit.

Yet another aspect of the invention is a welding power supply having an input rectifier and a preregulator, and an inverter. The pre-regulator includes a snubber circuit having a first switch in anti-parallel with a first diode, and a second switch in anti-parallel with a second diode. The combination of the first switch and first diode are connected in series with the combination of the second switch and the second diode, and the first and second switches are connected in opposing directions.

Another aspect of the invention is a welding power supply having an inverter with first and second current paths through a transformer, each in a unique direction. The first current path includes at least a first switch with an anti-parallel first diode and the second current path through the

transformer in a second direction, the second current path including at least a second switch with an anti-parallel second diode. A snubber includes a current path having a third switch with an anti-parallel third diode, a fourth switch with an anti-parallel fourth diode. The third switch and anti-parallel diode are in series with, and oppositely directed from, the fourth switch and anti-parallel diode. The snubber also has at least one snubber capacitor.

In alternative embodiments the first and second switches are in a half-bridge configuration or full bridge configuration. Also, the snubber capacitor may be split into two capacitors.

Another aspect of the invention is a method of providing welding power by turning on a first power switch and a first snubber switch, and allowing current to flow through the first power switch, an first dc bus, a first power capacitor, and in a first direction through a transformer. Then the first power switch is turned off and current flows through the first snubber switch, a second snubber diode, a snubber capacitor, and through the transformer in the first direction, while the first power switch is turning off, to provide a slow voltage transition off. Then current flows through a second anti-parallel power diode, a second DC bus, a second power capacitor, and through the transformer in the first direction, while the first power switch is continuing to turn off, to continue providing a slow voltage transition off. The first snubber switch is also turned off. After the system is at rest a second power switch on and a second snubber switch are turned after the first power switch is off, and current flows through the second power switch, the transformer in a second direction, the second power capacitor, and the second bus. The second power switch is turned off and current flows through the second snubber switch, a first snubber diode, the transformer in the second direction, and a snubber capacitor, while the second power switch is turning off, to provide a slow voltage transition of. Then current flows through a first power diode, the transformer in the second direction, and the first power capacitor, while the second power switch is turning off, to provide a slow voltage transition off. The second snubber switch is also turned off, and the process is repeated.

Other principal features and advantages of the invention will become apparent to those skilled in the art upon review of the following drawings, the detailed description and the appended claims.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a circuit diagram of a prior art welding power supply having a boost convertor pre-regulator;

FIG. 2 is a block diagram of a welding power supply constructed in accordance with the present invention;

FIG. 3 is a circuit diagram of a power factor correction circuit used in the preferred embodiment;

FIG. 4 is a circuit diagram of the pre-regulator of FIG. 2;

FIGS. 5–13 are a circuit diagram of FIG. 4, showing various current paths;

FIG. 14 is a circuit diagram of a switching circuit;

FIG. 15 is a full wave inverter using the switching circuit of FIG. 14;

FIG. 16 is a control circuit; diagram; and

FIGS. 17–22 are the circuit diagrams of FIG. 15 showing various current path.

Before explaining at least one embodiment of the invention in detail it is to be understood that the invention is not limited in its application to the details of construction and

the arrangement of the components set forth in the following description or illustrated in the drawings. The invention is capable of other embodiments or of being practiced or carried out in various ways. Also, it is to be understood that the phraseology and terminology employed herein is for the purpose of description and should not be regarded as limiting. Like reference numerals are used to indicate like components.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

While the present invention will be illustrated with reference to a welding power supply using a boost converter for a pre-regulator and particular circuitry, it should be understood at the outset that other circuit topologies may be used, and the power supply may be used for other purposes, and still be within the intended scope of this invention.

A block diagram of a welding power supply constructed in accordance with the preferred embodiment is shown in FIG. 2. Source 201 represents the input line voltage used to provide power to the welding power supply. The input line voltage may be anywhere between 90 and 250 volts in the preferred embodiment. The voltage typically operates at a frequency of 60 hertz (in the United States) and is single phase in the preferred embodiment (although alternative embodiments used a three phase input). Other voltages may also be used.

The input voltage is provided to a rectifier 202, which may be a simple bridge rectifier. The output of rectifier 202 is a rectified sinusoid.

A pre-regulator 204 receives the rectified sinusoid from rectifier 202 and provides a dc bus output to an output inverter 205. Pre-regulator 204, in the preferred embodiment is a soft-switched boost convertor which provides close to a unity power factor. Other convertor and inverter configurations may be used. Pre-regulator 204 also allows the input voltage to be anywhere within a range of input voltages in the preferred embodiment.

Convertor 205 is preferably a half-bridge, transformer isolated, soft (or slow) switched inverter. Such an output circuit will be described in detail below. Output convertor 205 may alternatively be a typical forward convertor (generally a buck convertor and a transformer), and other output converters may be used in other embodiments. A circuit including an output buck convertor is described in U.S. patent application entitled Auxiliary Open Circuit Voltage Power Supply, invented by Vogel and Geissler, filed on even date herewith, (hereby incorporated by reference) and assigned to the assignee of this invention. The output of convertor 205 is provided through an inductor 207 to welding output 208.

The circuit used in the preferred embodiment to implement pre-regulator 204 is shown in FIG. 4 (along with rectifier 202 and voltage source 201). The embodiment of FIG. 4 uses a 90–250 volt ac power line as input voltage 201. Rectifier 202 is comprised of diodes D6, D7, D8, and D9, which rectify the input voltage to provide a single polarity sinusoidal input voltage.

The power factor correction portion (described below) of pre-regulator 204 functions best when the input voltage is sinusoidal, although it could be another alternating input. Thus, a small (10 μ F) capacitor (not shown) is provided across input rectifier 202 in one embodiment to smooth the input line voltage.

The rectified input voltage is applied to a boost inductor L1 (750 μ H) which is connected with a boost switch Z1

(preferably an IGBT) to form a boost convertor. An anti-parallel diode D5 is connected across switch Z1 to protect switch Z1 during transitions. The portion of the circuit which provides the lossless switching includes a snubber inductor L2 (3.9 μ H) a pair of capacitors C1 (1 μ F) and C2 (0.068 μ F), and diodes D1, D2, D3, and D4. Switch Z1 is switched in a known manner such that the output of pre-regulator 204 is a desired voltage, no matter what the input voltage is. The output is provided across a capacitor C5 (2000 μ F) that provides a stable voltage source (400 volts in the preferred embodiment) for the downstream convertor. Also, capacitor C5 prevents the voltage from being dangerously high and damaging switch Z1.

The soft switching of pre-regulator 204 is best understood with reference to FIGS. 5–11, which show the circuit with various current paths (states). The first state (FIG. 5) is when switch Z1 is off, and the current (arrow 501) is in a steady state condition through inductors L1 and L2, and diode D1, to charge output capacitor C5 (arrow 501).

Then, switch Z1 is turned on, and current from inductor L1 begins to be directed through switch Z1 (arrow 501 of FIG. 6). Switch Z1 applies a reverse voltage to inductor L2, causing its current to fall. Thus, the current (in this state) is decreasing through inductor L2 and increasing through switch Z1. Inductor L2 effectively limits or slows the current in switch Z1 at turn on until the switch voltage drops (to close to zero). Thus, the turn on has been a slow-current transition (SCT).

Eventually all of the current from inductor L1 flows through switch Z1, and current in inductor L2 drops until it becomes zero, and then reverses. Capacitor C2 discharges through capacitor C1, diode D3, and inductor L2, as shown in FIG. 7, by arrow 701. Capacitors C1 and C2 allow diode D1 to turn off with a SVT, thus reducing losses. The discharge occurs at a resonant frequency determined by the time constant of the inductance of inductor L2 and the series capacitance of capacitors C1 and C2 ($f=1/(2\pi\sqrt{L2*(C1*C2/(C1+C2))})$). The time it takes for capacitor C2 to discharge is the SVT time for diode D1.

Capacitor C2 discharges to about zero volts, and diode D4 begins to conduct, as shown by arrow 801 in FIG. 8. When diode D4 conducts, inductor L2 releases the energy stored therein to capacitor C1 at a resonant frequency determined by inductor L2 and capacitor C1 ($f=1/(2\pi\sqrt{L2*C1})$). The voltage energy on capacitor C1 is transferred to current in inductor L2, and then to voltage on capacitor C1. The ratio of voltage transfer is nearly equal to the capacitance ratio.

When the charge transfer is complete, and current ceases to flow in snubber inductor L2, the snubber is reset, and current in inductor L1 increases through switch Z1, as shown in FIG. 9. The circuit remains in this state until the switch is turned off.

Next, switch Z1 is turned off, (FIG. 10) and current is diverted through diode D4 and into capacitor C2 (arrow 1001). Capacitor C2 provides the SVT time for switch Z1, thus a soft switching off is provided. The voltage on capacitor C2 continues to rise and eventually reaches the bus voltage (the voltage on capacitor C5) less the voltage on capacitor C1.

When this happens the voltage on capacitor C1 begins to reestablish the current in inductor L2 (FIG. 11 and arrow 1101). The voltage on capacitor C2 continues to rise until it reaches the bus voltage plus two diode drops. At that time current from inductor L1 not taken by inductor L2 is diverted through diode D3 FIG. 12 and arrow 1201). The voltage on capacitor C1 continues to increase the current in inductor L2.

Eventually all of the current from inductor L1 flows through inductor L2, and current through diodes D3 and D4 ceases (FIG. 13). Capacitor C1 continues to give energy to the bus.

When all of the energy on capacitor C1 is expended (to the bus) current flows from inductor L1 to inductor L2, and through diode D1. This is the state initially described, with respect to FIG. 5, and the cycle repeats.

Thus, the voltage rise across switch Z1 was slowed by capacitor C2 to allow the current to drop when switch Z1 was turned off. The current rise in switch Z1 was slowed by inductor L2 to allow the voltage to drop, when switch Z1 was turned on. Moreover, diode D1 was soft-switched by capacitors C1 and C2.

The portion of pre-regulator 204 that provides power factor correction is a power factor correction circuit 404 (FIG. 4), and generally senses the input voltage waveform, and conforms the shape of the current waveform to be that of the line voltage waveform. This provides a power factor of very close to 1, 0.99 in the preferred embodiment. Power factor correction circuit 404 may be implemented using an integrated circuit, such as a UC3854 or an ML4831, or with discrete components. Power factor correction circuit 404 receives as inputs the output voltage from rectifier 202, the output voltage from pre-regulator 204, and the output current of pre-regulator 204 (using a CT 405). Because the frequency of pre-regulator 204 (25 KHz) is much higher than that of the line (60 Hz) the pre-regulator current can be made to track the input line voltage shape by sensing the shape of the input voltage, and controlling the input current in response thereto.

An embodiment of power factor correction circuit 404 having discrete components is shown in FIG. 3 controls the switches so that the input current is shaped to match the input voltage, as well as regulates the DC bus.

The input voltage is rectified and provided to a 2 pole Bessel filter which removes switching frequencies. The Bessel filter includes capacitors 1602 (0.0022 μ F) and 1603 (0.001 μ F), resistors (1606–1608 (1M ohms), resistors 1609–1610 (39.2K ohm), and an op amp 1615. The output of the Bessel filter (V-RECT) is provided to a low pass filter (approximately 2 Hz), which includes resistors 1611 and 1612 (68.1K ohms), capacitor 1604 (0.22 μ F), capacitor 1605 (47 μ F), and op amp 1616. The output of op amp 1616 gives an average of the input line voltage (V-LINE).

V-LINE is provided to a typical precharge circuit 1625 which sets a delay before the electrolytic capacitors in the power supply precharge. An op amp 1626, and resistors 1629 (100K ohms) and 1630 (10K ohms), don't allow a capacitor 1627 (10 μ F) to charge through a resistor 1628 (100 ohms) until the line voltage reaches a threshold. After the line voltage reaches the threshold capacitor 1627 charges to a level where it turns on a relay (not shown) through associated components including a resistor R63 (200K ohms), a resistor R51 (100K ohms), a resistor R108 (619K ohms), an op amp U1, a diode D57, a NAND gate U2, and a resistor R89 (4.7K ohm). These components operate in a typical fashion. The relay energizes and fires an SCR that precharges the electrolytic capacitors.

A multipliers/divider 1631 of receives the rectified line voltage signal, and divides that by the average input (typically either 230 or 460) so that a scaled rectified voltage is provided. Then the scaled, is rectified voltage is multiplied by an error signal from the bus to produce a reference command. Specifically, V-RECT, the output of op amp 1615 which corresponds to the rectified input voltage, is provided

through a resistor **1632** (100K ohms) and an op amp **1633** as one channel input to the multiplication. The other channel input to the multiplication is a BUS-ERROR signal provided through an op amp **1636A**.

The output of op amp **1633** is provided through a log transistor **1635**, and the average line voltage (V-LINE) is provided through an op amp **1636** and to a log transistor **1637**. The common junction between transistors **1635** and **1637** is a subtraction, so the base of transistor **1637** is the result of the subtraction. That difference is added through a transistor **1638** to the bus error. The sum is provided to a transistor **1639**, which takes the anti-log of that value. Thus, a division and multiplication are performed. The output is scaled by an op amp **1641** and associated circuitry including a diode **1642**, a capacitor **1643** (0.001 μF), and a resistor **1645** (20K ohms).

A transistor **1646** limits the output current of op amp **1641**, and is controlled by a resistor **1647** (20K ohms) and a diode **1648**. The input to op amp **1650** is a scaled bus voltage, and sets the maximum output command. The output command (VCOMM) is used to force the current shape to match the input voltage shape.

The BUS-ERROR signal is provided by a typical error circuit which includes an op amp **1651** and associated circuitry resistors **1653** (20K ohms), **1654** (11K ohms), and **1655** (499K ohms), a diode **157** and a capacitor **1658** (0.047 μF). An 8 volt reference signal is compared to the divided down (and scaled) 800 volt bus. An error signal is provided through a resistor **1659** (82.5K ohms) to op amp **1636A** commanding an increase or decrease in the current to increase or decrease the bus voltage. Also, the current command is adjusted by the shape of the input signal as provided through V-RECT to mimic the shape of input rectified signal. Therefore, the current needed to result in a desired bus voltage is provided, but in such a shape that a power factor very close to one is obtained.

The command signal is summed with a current feedback signal from a CT1 by an op amp **1670** and provided to a boost drive circuit through logic gates (not shown) to turn on and off the IGBT in the preregulator. A CT is used to provide current feedback (rather than an LEM for example) because if a LEM fails it will call for unlimited current.

The boost drive signal is a digital signal of either zero (IGBT ON) or fifteen volts (IGBT OFF). The boost drive input is provided to the base of a pair of transistors because the logic gates output do not provide enough current to drive the IGBT's. Thus the transistors provide sufficient current. A transistor level shifts. The gates of a pair of transistors are tied together by a capacitor (0.1 μF).

Another aspect of this invention is implemented with a half-bridge, transformer isolated, inverter that is SVT switched. The inverter uses a switch circuit **1400**, shown in FIG. 14, that includes a pair of switches or IGBT's **1402** and **1403**, and a pair of diodes **1404** and **1405**. Diode **1404** is an anti-parallel diode for switch **1402**. Diode **1405** is an anti-parallel diode for switch **1403**. The two switch/diode parallel combinations are in series, but reversed, i.e. in opposing directions. This configuration provides a diode-type switch whose direction can be reversed.

An inverter using switch circuit **1400** is shown in FIG. 15, and includes a dc voltage source **1501**, a pair of switches **1502** and **1504**, with a pair of anti-parallel diodes **1503** and **1505**, a pair of capacitors **1507** and **1508** (1410 μF), a transformer **1509**, a capacitor **1512** (0.099 μF), an output rectifier including diodes **1510** and **1511**, and an output inductor **1513**.

Capacitor **1512** is switched across transformer **1509** by switches **1502** and **1504**. Switches **1402** and **1403** are used to soft switch switches **1502** and **1504**. Switches **1402** and **1403** do not need any special timing, and run with the main clock at effectively 50% duty cycle. For example, switches **1502** and **1402** turn on together, and switch **1502** delivers current to transformer **1509**, while switch **1402** does nothing. When switch **1502** turns off, switch **1402** remains on, and current is directed through switch **1402** and diode **1405** into capacitor **1512**, thus giving an SVT (Slow Voltage Transition) turn off. Switch **1402** is turned off after the transition and diode **1405** prevents the back flow of current from capacitor **1512**. This occurs in complimentary fashion with switches **1502** and **1402** and diode **1405**. Thus, this circuit provides full-wave transformer usage, PWM control, complete capacitor balance control with no extra circuitry, and efficient use of switches with SVT.

Referring now to FIGS. 17–24, the various current paths followed during a complete cycle are shown. The circuit in these Figures is an alternative embodiment that includes splitting capacitor **1512** into two capacitors, one connected to the upper bus, and one connected to the lower bus. This is done because the path through capacitors **1507** and **1508** can reduce the effectiveness of the snubber substantially.

Initially, all of the switches are off in the snubber, and capacitors **1512A** and **1512B** split the bus. The 800 volts bus is also split by capacitors **1507** and **1508** (for half bridge operation). Capacitors **1507** and **1508** should be large enough to keep the junction voltage between them substantially constant during operation. Switches **1504** and **1402** are turned on together. Switch **1504** delivers power to transformer **1509** while switch **1402** is blocked by diode **1404**. Thus, switch **1402** is in “standby” until switch **1504** turned off, as shown in FIG. 17.

Switch **1504** turns off, and the current through the transformer transfers to switch **1403**, diode **1404** and capacitor **1512** (which form the snubber path). The voltage across switch **1504** rises slowly giving a slow voltage transition. This current path is shown in FIG. 18.

When the voltage across switch **1504** reaches the bus voltage, the remaining energy from transformer **1509** is spilled back into the bus through diode **1503**. This current path is shown in FIG. 19. When the remaining energy and transformer **1509** has been provided to the bus the system comes to rest with snubber capacitor **1512** fully charged to completely soft switch **1502** (FIG. 15).

After the system comes to rest switches **1502** and **1403** are turned on together. Switch **1502** delivers power to transformer **1509** while switch **1403** is blocked by diode **1404**. Thus, switch **1403** is in standby until switch **1502** is turned off (FIG. 20).

Switch **1502** is turned off and current from transformer **1509** transfers to capacitor **1512** through the snubber path including diode **1404** and switch **1403** rises slowly, giving a slow voltage transition. This current path is shown in FIG. 21. The current continues in this path until the voltage across switch **1502** has reached the bus, and remaining energy in transformer **1509** is spilled into the bus through diode **1505** (FIG. 22). Capacitor **1512** fully charged so that switch **1504** may be soft switched. The process then repeats.

One feature of the switched snubber used in FIGS. 15–22 is that the main switches (**1504** and **1502**) do not incur actual losses if the output power is less than necessary to transition snubber capacitor **1512** from “rail to rail”. Thus, it is not necessary to fully transition the snubber. The reversible single direction switch prevents snubber interference on turn

on, and thus provides snubbing proportional to load. This feature allows very heavy snubbing without restricting the load range of the inverter.

An alternative embodiment includes using a full bridge version of the snubber.

FIG. 16 shows a control circuit for controlling the switching of the switched snubber in FIGS. 14–22. Four gates drives **1402A**, **1403A**, **1502A**, and **1504A** are used to provide the gate signals for switches **1402**, **1403**, respectively. These gate drives are not shown in detail and are conventional gate drives such as those found in the Miller XMT 304®. The gate drives are inverting in that a high input maintains the gates off and a low input maintains the gates on.

Gate drivers **1402A**, **1403A**, **1502A**, and **1504A** are controlled by a logic circuit **2301**. Logic circuit **2301** includes a plurality of NAND and OR gates in the preferred embodiment, however it's specific construction may be any of the designer's choosing. An enable signal is included as an input to logic circuit **2301**, in one embodiment. The enable signal is used only during power down.

An error amplifying circuit **2303** is also shown in FIG. 16. Error amplifying circuit **2303** may be a standard error circuit and is used, in the preferred embodiment, with a CT feedback signal. The output of error amplifier circuit **2303** is a PWM reference signal. The PWM reference signal control is provided through an opto-isolator **2305** to electrically isolate the remaining portion of the circuit from the error amp circuit. A pair of resistors **2306** (10K ohms) and **2307** (2K ohms) scale the PWM reference command for input into opto-isolator **2305**. The output of opto-isolator **2305** is scaled from a current to a voltage by a resistor **2308** (10K ohms).

Generally, the control circuitry implements a modified PWM control scheme. Above a minimum pulse width operation is a typical PWM scheme, and the pulse width is adjusted to increase or decrease current. However, for current less than that corresponding to the minimum pulse width the frequency of pulses is reduced (thus increasing the OFF time). The minimum pulse width is used because the gate drives have a limited speed.

The conventional pulse with modulation portion works with a ramp created by an op amp **2310**, resistors **2311** (10K ohms), **2312** (10K ohms), and **2313** (200K ohms). The PWM reference command is received by op amp **2310** through a diode **2314**. The appropriate switch is turned on at the start of the ramp. The ramp is initiated by an op amp **2315** and resistors **2316** (10K ohms), **2317** (611 ohms), **2318** (20K ohms), **2319** (200K ohms), **2321** (6.11K ohms) and **2322** (2K ohms).

The main power switches (**1502** and **1504**) are maintained on for 95% of the total ramp time. The 95% threshold is set by an op amp **2325** and a resistor **2326** (10K ohms). The switches are turned off by changing states on the set input of a flip flop **2327** (which is connected to op amp **2325**). The snubber switches (**1402** and **1403**) are switched off at 100% of the ramp.

A current source including transistors **2336** and **2331** and resistors **2333** (332 ohms), **2334** (100 ohms) and **2335** (9100 ohms). The current source sets the slope of the ramp. When a capacitor **2337** (100 pF) discharges to a threshold set by a diode **2338** the ramp is restarted. The ramp will continue up at the slope set by the current source until the capacitor voltage reaches the threshold set by op amp **2315** and its circuitry.

A flip flop **2328** is used to alternate between switches, and to receive an enable signal and a machine on/off signal.

Generally, the circuit operates as follows: the capacitor voltage is fully reset down to the minimum and then the ramp begins to ramp up and the voltage on the capacitor is increasing from the current source. As the capacitor charges the output of the opto-isolator is provided to op amp **2310**, which pulse width modulates the switches. When the capacitor voltage rises above the reference voltage set by the opto-isolator, op amp **2310** changes state, causing the switch to be turned off. Steering flip flop **2328** determines which one, and only one, of the main power switches are on in a conventional manner. If the capacitor voltage increases to the level set by op amp **2315** (95% of the peak), then the main power switch that is on is turned off.

The frequency adjust (for low current commands) operates as follows: the output of op amp **2315** (the ramp reset) is fed back through a NAND gate **2341** through a resistor **2342** (100K ohms) and a buffering transistor **2343**. The machine on/off signal is also provided to transistor **2343**. The output of NAND gate **2341** also causes flip flop **2328** to change state through the clock input.

A voltage divider including resistors **2342** and **2345** (68.1K ohms) is tied to a diode **2346**. If diode **2346** pulls down the voltage at one end of resistor **2345**, then the voltage across a resistor **2347** (5.11K ohms) is also pulled down. A current mirror including resistors **2349** and **2350** (100 ohms) and transistors **2351** and **2352** provide the rest current for the ramp. However, if the voltage through **2346** is low enough, then the voltage input to transistor **2343** will be ground, and transistor **2343** will not provide current to the current mirror to reset capacitor **2337**, thus allowing the ramp to continue upward.

The various aspects of this invention, while described in the context of a welding power supply has applications in many different areas. Generally, in applications where low loss switching is desirable using a boost convertor this arrangement may be used.

Numerous modifications may be made to the present invention which still fall within the intended scope hereof. Thus, it should be apparent that there has been provided in accordance with the present invention a method and apparatus for providing power with a high power factor and low switching losses that fully satisfies the objectives and advantages set forth above. Although the invention has been described in conjunction with specific embodiments thereof, it is evident that many alternatives, modifications and variations will be apparent to those skilled in the art. Accordingly, it is intended to embrace all such alternatives, modifications and variations that fall within the spirit and broad scope of the appended claims.

What is claimed is:

1. A welding power supply comprising:

- an input rectifier configured to receive an input line voltage and provide a rectified voltage on an output;
 - a pre-regulator connected to receive as an input the output of the rectifier and provide a dc bus as an output; and
 - an inverter, connected to receive the output of the pre-regulator and provide a welding output;
- wherein the inverter includes a snubber circuit having a first switch in anti-parallel with a first diode, and a second switch in anti-parallel with a second diode, and wherein the combination of the first switch and first diode are connected in series with the combination of the second switch and the second diode, and wherein the first and second switches are connected in opposing directions.

2. A welding power supply comprising:

a first current path through a transformer in a first direction, the first current path including at least a first switch with an anti-parallel first diode;

a second current path through the transformer in a second direction, the second current path including at least a second switch with an anti-parallel second diode;

a snubber, including a current path having a third switch with an anti-parallel third diode, a fourth switch with an anti-parallel fourth diode, wherein the third switch and an anti-parallel diode are in series with, and oppositely directed from, the fourth switch and anti-parallel diode, and at least one snubber capacitor.

3. The power supply of claim 2 wherein the first and second switches are in a half-bridge configuration.

4. The power supply of claim 2 wherein the at least one snubber capacitor includes a first snubber capacitor connected with a first bus line and a second snubber capacitor connected with a second bus line.

5. The power supply of 2 wherein the at least one snubber capacitor is in series with the third and fourth switches and anti-parallel diodes.

6. A method of providing welding power from a welding power supply including a first power switch a second power switch, a first snubber switch, a second snubber switch, a first dc bus, a second dc bus, a first power capacitor, a second power capacitor, a first snubber diode, a second snubber diode, a first snubber capacitor, a second snubber capacitor, a first anti-parallel power diode, a second anti-parallel power diode, and a transformer, comprising:

turning on the first power switch and the first snubber switch, and allowing current to flow through the first power switch, the first dc bus, the first power capacitor, and in a first direction through the transformer;

turning the first power switch off and allowing current to flow through the first snubber switch, the second snubber diode, the first snubber capacitor, and through the transformer in the first direction, while the first power switch is turning off, to provide a slow voltage transition off;

allowing current to flow through the second anti-parallel power diode, the second DC bus, the second power capacitor, and through the transformer in the first direction, while the first power switch is continuing to turn off, to continue providing a slow voltage transition off;

turning off the first snubber switch;

turning on the second power switch and the second snubber switch after the first power switch is off, and allowing current to flow through the second power switch, the transformer in a second direction, the second power capacitor, and the second dc bus;

turning the second power switch off and allowing current to flow through the second snubber switch, the first snubber diode, the transformer in the second direction, and the second snubber capacitor, while the second power switch is turning off, to provide a slow voltage transition off;

allowing current to flow through the first anti-parallel power diode, the transformer in the second direction,

and the first power capacitor, while the second power switch is turning off, to provide a slow voltage transition off;

turning off the second snubber switch;

and repeating these steps.

7. The method of claim 6, wherein turning on the first and second power switches includes soft switching on the first and second power switches.

8. A method of providing welding power from a welding power supply including a first power switch a second power switch, a first snubber switch, a second snubber switch, a dc bus, a power capacitor, a first snubber diode, a second snubber diode, as snubber capacitor, a first anti-parallel power diode, a second anti-parallel power diode, and a transformer, comprising:

turning on the first power switch and the first snubber switch, and allowing current to flow through the first power switch, the dc bus, the power capacitor, and in a first direction through the transformer;

turning the first power switch off and allowing current to flow through the first snubber switch, the second snubber diode, the snubber capacitor, and through the transformer in the first direction, while the first power switch is turning off, to provide a slow voltage transition off;

allowing current to flow through the second anti-parallel power diode, the DC bus, the power capacitor, and through the transformer in the first direction, while the first power switch is continuing to turn off, to continue providing a slow voltage transition off;

turning off the first snubber switch;

turning on the second power switch and the second snubber switch after the first power switch is off, and allowing current to flow through the second power switch, the transformer in a second direction, the second power capacitor, and the dc bus;

turning the second power switch off and allowing current to flow through the second snubber switch, the first snubber diode, the transformer in the second direction, and the snubber capacitor, while the second power switch is turning off, to provide a slow voltage transition off;

allowing current to flow through the first anti-parallel power diode, the transformer in the second direction, and the power capacitor, while the second power switch is turning off, to provide a slow voltage transition off;

turning off the second snubber switch;

and repeating these steps.

9. The method of claim 8, wherein turning on the first and second power switches includes soft switching on the first and second power switches.

10. The method of claim 9, wherein the power capacitor is comprised of first and second capacitors, and the dc bus is a split bus.

11. The method of claim 9, wherein the snubber capacitor is comprised of first and second capacitors, and the dc bus is a split bus.