



US006208093B1

(12) **United States Patent**  
**Truskalo**

(10) **Patent No.:** **US 6,208,093 B1**  
(45) **Date of Patent:** **Mar. 27, 2001**

(54) **SELECTABLE CLAMPERS FOR AN S-SHAPING VOLTAGE OF A VIDEO DISPLAY**

(75) Inventor: **Walter Truskalo, Indianapolis, IN (US)**

(73) Assignee: **Thomson Licensing S.A., Boulogne (FR)**

(\* ) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **09/246,281**

(22) Filed: **Feb. 8, 1999**

(51) Int. Cl.<sup>7</sup> ..... **G09G 1/04**

(52) U.S. Cl. .... **315/371; 315/370; 315/408**

(58) Field of Search ..... **315/364, 370, 315/371, 399, 408, 27, 395, 411; 348/746**

(56) **References Cited**

**U.S. PATENT DOCUMENTS**

|           |           |                     |         |
|-----------|-----------|---------------------|---------|
| 3,349,279 | 10/1967   | Schafft .....       | 315/27  |
| 3,767,963 | * 10/1973 | McArdle et al. .... | 315/27  |
| 4,019,093 | 4/1977    | Klein .....         | 315/370 |
| 4,130,783 | 12/1978   | de Hollander .....  | 315/371 |
| 4,232,254 | * 11/1980 | Haferl .....        | 315/408 |
| 4,423,358 | * 12/1983 | den Hollander ..... | 315/371 |
| 4,441,058 | * 4/1984  | Luz .....           | 315/371 |
| 4,533,855 | 8/1985    | Willis et al. ....  | 315/370 |
| 4,612,481 | 9/1986    | Storberg .....      | 315/370 |

|           |           |                     |         |
|-----------|-----------|---------------------|---------|
| 4,633,146 | * 12/1986 | Babcock .....       | 315/408 |
| 4,695,774 | 9/1987    | Gent et al. ....    | 315/408 |
| 4,707,640 | 11/1987   | Onozawa et al. .... | 315/408 |
| 4,761,586 | * 8/1988  | Wharton .....       | 315/408 |
| 4,761,587 | * 8/1988  | Wharton .....       | 315/408 |
| 5,043,637 | * 8/1991  | Gries et al. ....   | 315/371 |
| 5,182,504 | 1/1993    | Haferl .....        | 315/370 |
| 5,402,044 | 3/1995    | Haferl .....        | 315/371 |
| 6,114,817 | * 9/2000  | Fernsler .....      | 315/411 |

**OTHER PUBLICATIONS**

United States Patent Appln 09/130820 filed Aug. 7, 1998 (RCA 89042).

\* cited by examiner

*Primary Examiner*—Haissa Philogene

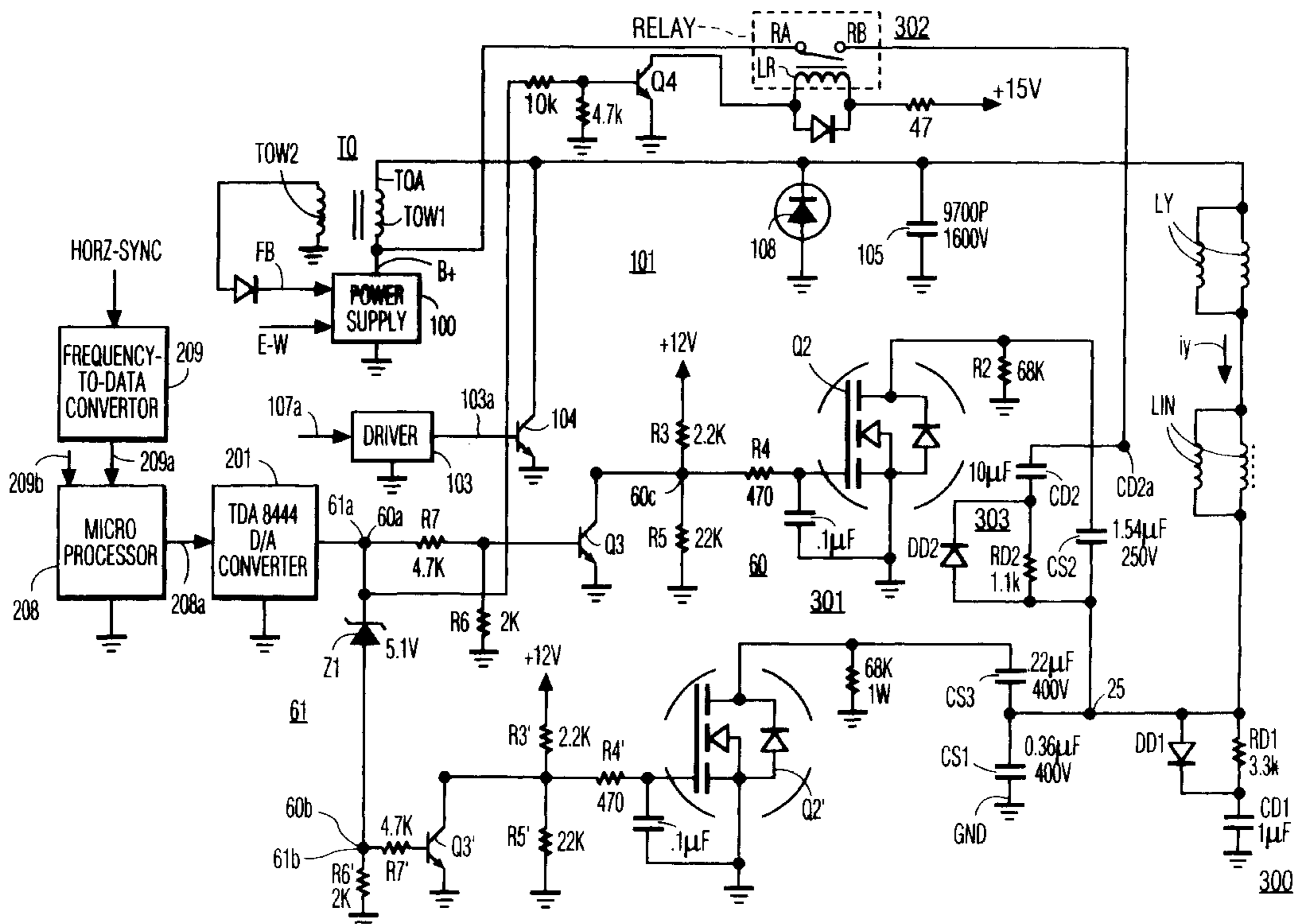
*Assistant Examiner*—Hoang Nguyen

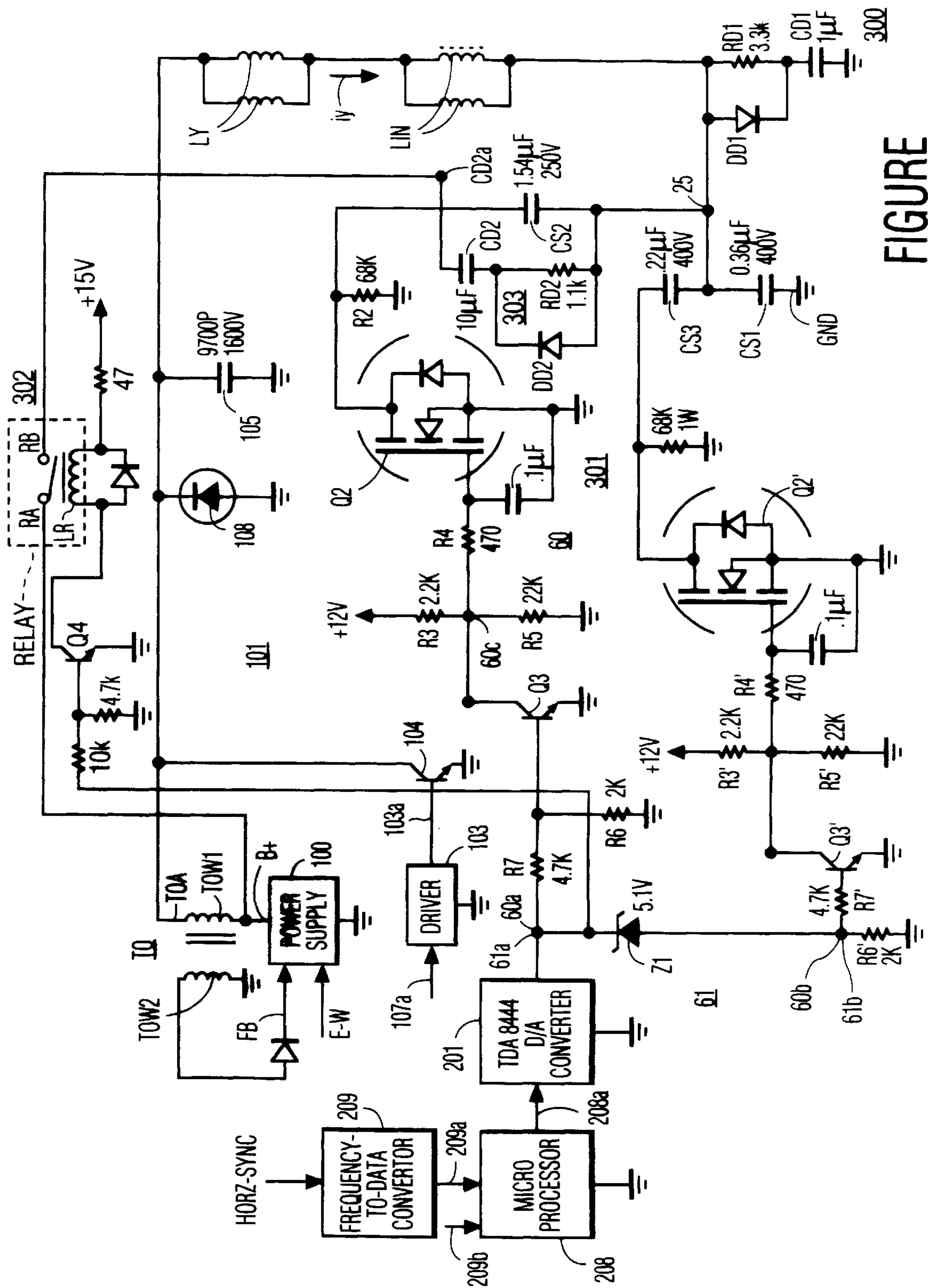
(74) *Attorney, Agent, or Firm*—Joseph S. Tripoli; Harvey D. Fried; Sammy S. Henig

(57) **ABSTRACT**

In a horizontal deflection circuit output stage of a video display monitor capable of operating at multi-scan rates, a given S-capacitor, selected from a bank of S-capacitors, provide S-correction at a corresponding range of frequencies. A resistor-capacitor-diode clamp selected from a bank of clamps is coupled to the selected S-capacitor for reducing ringing by causing critical damping. The in-circuit selected resistor-capacitor-diode clamp is selectable, in accordance with the selected horizontal deflection frequency.

**4 Claims, 1 Drawing Sheet**





FIGURE

## SELECTABLE CLAMPERS FOR AN S-SHAPING VOLTAGE OF A VIDEO DISPLAY

The invention relates to a dynamic clamping arrangement of a deflection circuit.

A television receiver, computer or monitor may have the capability of selectively displaying picture information in the same color cathode ray tube (CRT) using a deflection current at different horizontal scan frequencies. Typically, an S-capacitor is coupled to a horizontal deflection winding of a horizontal deflection circuit output stage to correct a deflection related beam landing error referred to as S correction.

A horizontal rate synchronizing signal that controls the horizontal deflection circuit may be subject to an abrupt phase change in a horizontal period that occurs, during the vertical blanking interval. Such abrupt phase change may be, for example, deliberately introduced to thwart unauthorized video recording of the video signal. Consequently, the stored energy in an inductance coupled to the supply voltage of the horizontal deflection circuit output stage may temporarily increase.

The increased stored energy is subsequently dissipated. However, disadvantageously, the return to steady state operation may be accompanied with ringing in currents and voltages produced in the horizontal deflection circuit output stage. A resistor-capacitor-diode (RCD) clamp coupled across the S-capacitance has been used to reduce such ringing by forcing the horizontal deflection circuit output stage to operate near critical damping.

When displaying the picture information of a television signal defined according to a broadcasting standard, it may be more economical to utilize a horizontal deflection current at a rate of approximately 16 KHz, referred to as the  $1f_H$  rate. Whereas, when displaying the picture information of a high definition television signal or a display monitor data signal, the rate of the horizontal deflection current may be equal to or greater than 32 KHz, referred to as  $2nf_H$ . The value  $n$  is equal to or greater than 1.

In a horizontal deflection circuit output stage of a video display monitor capable of operating at multi-scan rates, it is known to vary the number of in-circuit S-capacitors using switched S-capacitors. The selection of the S-capacitors is made via selectable switches, in accordance with the selected horizontal deflection frequency.

In a TV receiver-monitor, which operates at the different horizontal scanning frequencies, a single RCD clamp may not be able to provide the required damping for the entire range of the horizontal scanning frequency. It may be desirable to provide the required damping for the entire frequency range.

In carrying out an inventive feature, the number of in-circuit RCD clamps varies using switched RCD clamps. The selection of the RCD clamps is made via a selectable switch, in accordance with the selected horizontal deflection frequency.

A video display deflection apparatus operating at multi-scan horizontal frequencies, embodying an inventive feature, includes a source of an input signal at a frequency related to a selected horizontal deflection frequency. A first switch, responsive to the first input signal and coupled to a horizontal deflection winding and to a retrace capacitance, is used for generating a horizontal deflection current in the horizontal deflection winding at the selected horizontal deflection frequency. The horizontal deflection winding is coupled to an S-shaping capacitance for generating an S-shaping voltage that provides horizontal linearity distortion correction.

A pair of clamp circuits is selectable in accordance with the selected horizontal deflection frequency for clamping the S-shaping voltage, during a portion of a horizontal period. A second switch is responsive to the input signal and coupled to one of the clamp circuits for selecting the one clamp circuit, when the selected horizontal deflection frequency is within a first range, and for de-selecting the one clamp circuit, when the selected horizontal deflection frequency is within a second range.

The sole FIGURE illustrates a clamp, embodying an aspect of the invention, coupled across a switched S-capacitor of a horizontal deflection circuit output stage.

The sole FIGURE illustrates a horizontal deflection circuit output stage **101** of a television receiver having multi-scan frequency capability. Stage **101** is energized by a regulated power supply **100** that generates a supply voltage  $B+$ . A conventional driver stage **103** is responsive to an input signal **107a** at the selected horizontal scanning frequency  $nf_H$ . Driver stage **103** generates a drive control signal **103a** to control the switching operation in a switching transistor **104** of output stage **101**. By way of example, a value of  $n=1$  may represent the horizontal frequency of a television signal according to a given standard such as a broadcasting standard. The collector of transistor **104** is coupled to a terminal **T0A** of a primary winding **T0W1** of a flyback transformer **T0**. The collector of transistor **104** is also coupled to a retrace capacitor **105**. The collector of transistor **104** is additionally coupled to a horizontal deflection winding **LY** to form a retrace resonant circuit. The collector of transistor **104** is also coupled to a conventional damper diode **108**. Winding **LY** is coupled in series with a linearity inductor **LIN** and a non-switched trace or S-capacitor **CS1**. Capacitor **CS1** is coupled between a terminal **25** and a reference potential, or ground **GND** such that terminal **25** is interposed between inductor **LIN** and S-capacitor **CS1**.

Output stage **101** is capable of producing a deflection current  $i_y$ . Deflection current  $i_y$  has substantially the same predetermined amplitude for any selected horizontal scan frequency of signal **103a** selected from a range of  $2f_H$  to  $2.4f_H$  and for a selected horizontal frequency of  $1f_H$ . The horizontal frequency of  $1f_H$  is at, for example, approximately 16 KHz. Controlling the amplitude of deflection current  $i_y$  is accomplished by automatically increasing voltage  $B+$  when the horizontal frequency increases, and vice versa, so as to maintain constant amplitude of deflection current  $i_y$ . Voltage  $B+$  is controlled by a conventional regulated power supply **100** operating in a closed-loop configuration via a feedback winding **T0W2** of transformer **T0**. The magnitude of voltage  $B+$  is regulated, in accordance with a rectified, feedback flyback pulse signal **FB** having a magnitude that is indicative of the amplitude of current  $i_y$ . A vertical rate parabola signal **E-W** is generated in a conventional way, not shown. Signal **E-W** is conventionally coupled to power supply **100** for producing a vertical rate parabola component of voltage  $B+$  to provide for East-West distortion correction.

A switching circuit **60** is used for correcting a beam landing error such as linearity. Circuit **60** selectively couples none, only one or both of a trace capacitor **CS2** and a trace capacitor **CS3** in parallel with non-switched trace capacitor **CS1**. The selective coupling is determined as a function of the range of frequencies from which the horizontal scan frequency is selected. In switching circuit **60**, capacitor **CS2** is coupled between terminal **25** and a drain electrode of a field effect transistor (FET) switch **Q2**. A source electrode of transistor **Q2** is coupled to ground **GND**. A protection resistor **R2** that prevents excessive voltage across transistor **Q2** is coupled across transistor **Q2**.

A control signal **60a** is generated in a digital-to-analog (D/A) converter **201**. Control signal **60a** is coupled via a voltage divider that includes a resistor **R7** and a resistor **R6** to a base electrode of a threshold determining transistor **Q3**. An intermediate terminal **60c** disposed between a resistor **R3** and a resistor **R5**, forming a pull-up voltage divider, is coupled to the collector of transistor **Q3** and, via a protection resistor **R4** to a gate electrode of transistor **Q2**. When control signal **60a** is sufficiently large to turn on transistor **Q3**, the gate voltage of transistor **Q2** is zero and transistor **Q2** is turned off. On the other hand, when control signal **60a** is not sufficiently large to turn on transistor **Q3**, the gate voltage of transistor **Q2** is pulled up by the voltage produced via resistors **R3** and **R5** and transistor **Q2** is turned on.

Signal **60a** is coupled via a threshold determining arrangement of a zener diode **Z1** coupled in series with resistor **R6'** to develop switch control signal **60b** at a terminal **61b**. Signal **60b** is developed between diode **Z1** and resistor **R6'**. Signal **60b** is coupled to the base of transistor **Q3'** via a base resistor **R7'**.

In switching circuit **60**, capacitor **CS3** is coupled between terminal **25** and a drain electrode of a FET switch **Q2'**. FET switch **Q2'** is controlled by control signal **60b** in a similar way that FET switch **Q2** is controlled by control signal **60a**. Thus, resistors **R3'**, **R4'** and **R5'** and transistor **Q3'** are coupled to one another and perform similar functions as resistors **R3**, **R4** and **R5** and transistor **Q3**, respectively.

When the frequency of horizontal deflection current  $i_y$  is  $1f_H$ , signal **60a** is at a minimum level of zero volts such that the base voltage of transistor **Q3** does not exceed the forward voltage of transistor **Q3**. Consequently, both transistors **Q3** and **Q3'** are turned off and transistors **Q2** and **Q2'** are turned on. The result is that both S-capacitors **CS2** and **CS3** are in-circuit S-capacitors that are coupled in parallel with non-switched S-capacitor **CS1** and establish a maximum S-capacitance value.

When the frequency of horizontal deflection current  $i_y$  is equal to or greater than  $2f_H$  and less than  $2.14 f_H$  signal **60a** is at an intermediate level of 5V such that the base voltage of transistor **Q3** exceeds the forward voltage of transistor **Q3**. However, the level of signal **60a** does not exceed the breakdown voltage of zener diode **Z1**. Consequently, transistor **Q3** is turned on, transistor **Q3'** is turned off, transistor **Q2** is turned off and transistor **Q2'** is turned on. The result is that S-capacitor **CS2** is decoupled from non-switched S-capacitor **CS1** and S-capacitor **CS3** is coupled to S-capacitor **CS1** to establish an intermediate S-capacitance value.

When the frequency of horizontal deflection current  $i_y$  is equal to or greater than  $2.14 f_H$ , signal **60a** is at a maximum level of 10V such that the base voltage of transistor **Q3** exceeds the forward voltage of transistor **Q3**. Also, the level of signal **60a** exceeds the breakdown voltage of zener diode **Z1** by a sufficient amount to produce a base voltage of transistor **Q3'** that exceeds the forward voltage of transistor **Q3'**. Consequently, transistors **Q3** and **Q3'** are turned on and transistors **Q2** and **Q2'** are turned off. The result is that S-capacitors **CS2** and **CS3** are decoupled from non-switched S-capacitor **CS1** and establish a minimum S-capacitance value.

A control circuit **61** includes a microprocessor **208** that is responsive to a data signal **209a** generated in a frequency-to-data signal converter **209**. Signal **209a** has a numerical value that is indicative of the frequency of a synchronizing signal **HORZ-SYNC** or deflection current  $i_y$ . Converter **209** includes, for example, a counter that counts the number of clock pulses, during a given period of signal **HORZ-SYNC**

and generates word signal **209a** in accordance with the number of clock pulses that occur in the given period. Microprocessor **208** generates a control data signal **208a** that is coupled to an input of D/A converter **201**. The value of signal **208a** is determined in accordance with the horizontal rate of signal **HORZ-SYNC**. D/A converter **201** generates, in accordance with data signal **208a**, analog control signal **60a** at a single terminal **61a**. Signal **60a** is at a level that is determined by signal **208a**, in accordance with the frequency of signal **HORZ-SYNC**. Alternatively, the value of signal **208a** may be determined by a signal **209b** that is provided by a keyboard, not shown.

A non-switched, clamp circuit **300** includes a capacitor **CD1** coupled in series with a parallel arrangement of a rectifying diode **DD1** and a damping resistor **RD1**. Clamp circuit **300** is coupled between terminal **25** of capacitor **CS1** and ground or across S-capacitor **CS1**. Clamp circuit **300** is an in-circuit clamp at each horizontal scan frequency of signal **103a** selected from the range of  $1f_H$  to  $2.4f_H$ . Diode **DD1** of clamp circuit **300** rectifies peaks of the horizontal rate voltage component at terminal **25** of S-capacitor **CS1**. The rectification occurs mainly when vertical scanning is at approximately the top third of the display screen. The R-C component values of clamp circuit **300** are selected to provide optimized damping, when the frequency of horizontal deflection current  $i_y$  is equal to or greater than  $2 f_H$ . When the operation frequency is at the lower frequency,  $1f_H$ , the horizontal deflection supply voltage **B+** is reduced to 70V from a higher level in the vicinity of 140V. Therefore, the rectification provided by diode **DD1** of clamp circuit **300**, renders a lower voltage. The result is that the power dissipated in resistor **RD1** drops to about 25% of that at  $2f_H$ . Consequently, disadvantageously, at the lower frequency  $1f_H$  circuit **300** may not provide sufficient damping to prevent ringing.

Advantageously, a switched, clamp circuit **303** is coupled to terminal **25** and includes a capacitor **CD2** coupled in series with a parallel arrangement of a rectifying diode **DD2** and a damping resistor **RD2**. A terminal **CD2a** of capacitor **CD2** that is remote from terminal **25** is coupled to supply voltage **B+** via a relay contact **RB** and a relay contact **RA** of a relay **302**. Coil **LR** of relay **302** is coupled between a supply voltage of 15V and the collector terminal of a relay control transistor **Q4**. The base terminal of transistor **Q4** is coupled to terminal **61a**.

When the horizontal frequency is equal or greater than  $2f_H$ , signal **60a** at terminal **61a** is at the higher level causing coil **LR** of relay **302** to be energized via transistor **Q4**. This results in decoupling contact **RA** from contact **RB**. On the other hand, when the horizontal frequency is equal to  $1f_H$ , signal **60a** is at the lower level and causes transistor **Q4** to turn off in a manner to couple capacitor **CD2** to the terminal where voltage **B+** is developed. Thus, clamp circuit **303** and trace capacitor **CS2** are in-circuit elements when the selected horizontal scan frequency is  $1f_H$ .

The component values of clamp circuit **303** are selected to supplement the damping provided by circuit **300** for providing the desired damping, when the frequency of horizontal deflection current  $i_y$  is equal to  $1 f_H$ . Advantageously, both clamp circuits **300** and circuit **303** provide together the required clamping for eliminating ringing, when the frequency of horizontal deflection current  $i_y$  is equal to  $1 f_H$ . Similarly to capacitor **CS2**, clamp circuit **303** has no effect at higher frequencies than  $1f_H$ .

Had capacitor **CD2** of clamp circuit **302** been coupled to ground as capacitor **CD1**, it would have differentiated the E-W pincushion correction parabolic voltage component

5

developed at terminal **25** of the in-circuit S-shaping capacitors. This is so because supply voltage B+ that determines the voltage at terminal **25** varies at a vertical rate parabolic manner. Such differentiation could have resulted in an undesirable sawtooth current component that varies at vertical rate in current  $i_y$  of horizontal winding Ly. Disadvantageously, the undesirable sawtooth current component could have caused the sides of the raster to tilt.

Advantageously, in contrast to clamp capacitor CD **1**, terminal CD**2a** of clamp capacitor CD**2** that is remote from terminal **25** is DC coupled to supply voltage B+ via relay contacts RB and RA, instead of to ground. Each terminal of capacitor CD**2** develops the same amplitude and phase of the vertical rate parabola component of voltage B+. Consequently, the voltage difference developed between the terminals of clamp capacitor CD**2** excludes any vertical rate parabola voltage difference. Thus, the rectified peaks of the voltage in S-capacitor CS**2**, for example, and the supply voltage B+ modulation are approximately equal in magnitude. Therefore, vertical rate variations in supply voltage B+, advantageously, have no effect on the damping function.

The extent of damping required is greater when the frequency of horizontal deflection current  $i_y$  is equal to  $1 f_H$ , than when the frequency of horizontal deflection current  $i_y$  is higher. Therefore, coupling capacitor CD**1** to voltage B+ is not as important as in the case of capacitor CD**2**.

What is claimed is:

**1.** A video display deflection apparatus operating at multi-scan horizontal frequencies, comprising:

- a source of an input signal at a frequency related to a selected horizontal deflection frequency;
- a first switch, responsive to said input signal and coupled to a horizontal deflection winding and to a retrace capacitance, for generating a horizontal deflection cur-

6

rent in said horizontal deflection winding at the selected horizontal deflection frequency, said horizontal deflection winding being coupled to an S-shaping capacitance for generating an S-shaping voltage that provides horizontal linearity distortion correction;

a first clamp circuit selectable in accordance with the selected horizontal deflection frequency for clamping said S-shaping voltage, during a portion of a horizontal period; and

a second switch responsive to said input signal and coupled to said first clamp circuit for selecting said first clamp circuit, when the selected horizontal deflection frequency is within a first range, and for de-selecting said first clamp circuit, when the selected horizontal deflection frequency is within a second range.

**2.** A video display deflection apparatus according to claim **1**, wherein said S-shaping capacitance comprises, a plurality of S-shaping capacitors for selecting one of said S-shaping capacitors, when the selected horizontal deflection frequency is within one of said first and second ranges, and for de-selecting said one S-shaping capacitor, when the selected horizontal deflection frequency is within the other one of said first and second ranges.

**3.** A video display deflection apparatus according to claim **1**, further comprising a second clamp circuit for clamping said S-shaping voltage, during a portion of said horizontal period.

**4.** A video display deflection apparatus according to claim **3**, wherein said second clamp circuit clamps both, when the selected horizontal deflection frequency is within the first range, and when the selected horizontal deflection frequency is within the second range.

\* \* \* \* \*