



US005844146A

United States Patent [19]

[11] Patent Number: **5,844,146**

Murray et al.

[45] Date of Patent: **Dec. 1, 1998**

[54] FINGERPAD FORCE SENSING SYSTEM

FOREIGN PATENT DOCUMENTS

[75] Inventors: **Anne Marie Murray**, Onalaska, Tex.;
Richard M. Moore, Jr., Pittsburgh, Pa.;
David Alan Bourne, Pittsburgh, Pa.;
Melvin W. Siegel, Pittsburgh, Pa.

0301527 2/1989 European Pat. Off. .
0335314 10/1989 European Pat. Off. .
0355454 2/1990 European Pat. Off. .
3110018 5/1991 Japan .
3110022 5/1991 Japan .
4309414 11/1992 Japan .
9109696 7/1991 WIPO .
9503901 2/1995 WIPO .

[73] Assignees: **Amada America, Inc.**, Buana Park,
Calif.; **Amada Company, Ltd.**,
Kanagawa, Japan

OTHER PUBLICATIONS

[21] Appl. No.: **741,553**

Patent Abstracts of Japan, vol. 015, No. 298, Jul. 29, 1991,
& JP-A-03 110 022.

[22] Filed: **Oct. 31, 1996**

Patent Abstracts of Japan, vol. 015, No. 298, Jul. 29, 1991,
& JP-A-03 110 018.

Related U.S. Application Data

[63] Continuation of Ser. No. 338,095, Nov. 9, 1994, abandoned.

Patent Abstracts of Japan, vol. 018, No. 239, May 9, 1994,
& JP-A-06 031 345.

[51] Int. Cl.⁶ **G01L 1/24**

Patent Abstracts of Japan, vol. 015, No. 325, Aug. 19, 1991,
& JP-A-03 124 318.

[52] U.S. Cl. **73/862.043**; 73/862.624;
73/862.041

[58] Field of Search 73/862.042, 862.043,
73/862.044, 862.06, 862.644; 340/470.1,
470.2

Ichikawa et al., Y., "A Heuristic Planner And An Executive
For Mobile Robor Control", *IEEE Transactions on Systems,
Man and Cybernetics*, vol. SMC-15, No. 4, pp. 558-563,
New York, U.S.A. (Jul./Aug. 1985).

[56] References Cited

(List continued on next page.)

U.S. PATENT DOCUMENTS

3,438,251 4/1969 Kloss 73/862.624
3,654,616 4/1972 Dunne et al. .
3,890,552 6/1975 Devol et al. .
4,111,027 9/1978 Bottomley .
4,260,940 4/1981 Engelberger et al. .
4,309,600 1/1982 Perry et al. .
4,356,718 11/1982 Makino .
4,369,563 1/1983 Williamson .
4,455,857 6/1984 Salvagnini .
4,495,588 1/1985 Nio et al. .
4,501,135 2/1985 Chivens et al. .
4,509,357 4/1985 Zbornik .
4,517,653 5/1985 Tsuchihashi et al. .
4,521,685 6/1985 Rebman 250/229
4,571,694 2/1986 Inaba et al. .
4,602,345 7/1986 Yokoyama .
4,613,943 9/1986 Miyake et al. .

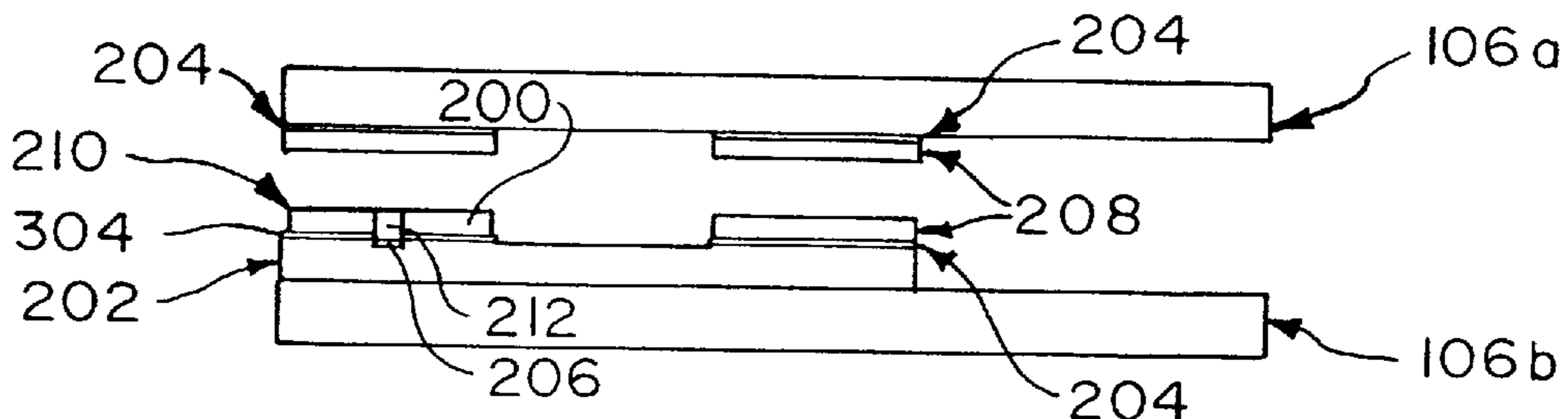
(List continued on next page.)

Primary Examiner—Ronald L. Biegel
Attorney, Agent, or Firm—Greenblum & Bernstein, P.L.C.

[57] ABSTRACT

A fingerpad force sensor system is disclosed which is useful
for detecting process variations during manufacturing pro-
cesses in which a plurality of force sensors are applied to the
gripper of a robot in order to monitor shear forces applied to
the workpiece held by the robot during, for example, sheet-
metal bending manufacturing processes. Each sensor is
encapsulated in rubber pads which are secured to the gripper
of the robot such that they monitor the status of the work-
piece during all phases of automated bending: material
acquisition, material handling, machine loading and unload-
ing.

17 Claims, 11 Drawing Sheets



U.S. PATENT DOCUMENTS

4,640,113	2/1987	Dieperink et al. .	
4,658,625	4/1987	Koyama et al. .	
4,745,812	5/1988	Amazeen et al.	73/862.04
4,802,357	2/1989	Jones .	
4,942,767	7/1990	Haritonidis et al. .	
4,947,666	8/1990	Hametner et al. .	
4,962,654	10/1990	Zbornik .	
4,979,385	12/1990	Lafrasse et al. .	
4,991,422	2/1991	Sartorio .	
5,005,394	4/1991	Sartorio et al. .	
5,007,264	4/1991	Haack .	
5,009,098	4/1991	van Merksteijn .	
5,012,661	5/1991	Catti et al. .	
5,031,441	7/1991	Jones .	
5,036,694	8/1991	Farney et al. .	
5,042,287	8/1991	Sartorio .	
5,058,406	10/1991	Sartorio et al. .	
5,081,763	1/1992	Jones .	
5,088,181	2/1992	Jeppsson .	
5,092,645	3/1992	Okada .	
5,146,670	9/1992	Jones .	
5,298,964	3/1994	Nelson et al.	73/862.624
5,307,282	4/1994	Conradson et al. .	
5,365,059	11/1994	Savage	73/862.624

OTHER PUBLICATIONS

Zussman et al., E., "A Planning Approach For Robot-Assisted Multiple-Bent Profile Handling", *Robotics and Computer-Integrated Manufacturing*, vol. 11, No. 1, pp. 35-40, Kidlington, Oxford, GB (Mar. 1994).

Huang et al., H., "Time-Optimal Control For A Robotic Contour Following Problem", *IEEE Journal of Robotics and Automation*, vol. 4, No. 2, pp. 140-149, New York, U.S.A. (Apr. 1988).

Bourne, David A., "Intelligent Manufacturing Workstations," which appeared in *Knowledge-Based Automation of Processes*, Session at the 1992 ASME Winter Annual Meeting, Nov. 1992.

Lozano-Perez, Tomas, "Automatic Synthesis of Fine-Motion Strategies for Robots," *The International Journal of Robotics Research*, vol. 3, No. 1, Massachusetts Institute of Technology (Spring 1984).

Stewart et al., David B., *Chimera II, Real Time Programming Environment*, Version 1.02, Carnegie Mellon University, Pittsburgh, PA (Oct. 1990).

Craig, John J., *Introduction to Robotics Mechanics and Control*, Second Edition, Addison-Wesley Publishing Company, Reading MA (1989).

Paul, R.G., "Problems and Research Issues Associated with Hybrid Control of Force and Displacement," *Proceedings of the IEEE International Conference on Robotics and Automation*, pp. 1966-1971 (1987).

Roger Allan, "Nonvision Sensors", *Electronic Design*, Jun. 27, 1985, pp. 103-115.

J.J. Carr, *Sensors and Circuits*, PTR Prentice Hall, Englewood, New Jersey, 1993, pp. 125-133.

Paolo Dario and Danilo De Rossi, "Tactile Sensors and the Gripping Challenge", *IEEE Spectrum*, vol. 22, No. 8, Aug. 1985, pp. 46-52.

P. Dario, M. Bergamasco, and A. Fiorillo, "Force and Tactile Sensing For Robots", NATO ASI Series, vol. F43, Sensors and Sensory Systems For Advanced Robots, Springer-Verlag, Berlin, 1988, pp. 153-185 No. 8, Aug. 1985, pp. 46-52.

Akira Nomura et al., "Two Dimensional Tactile Sensor Using Optical Method", *IEEE Transactions On Components, Hybrids, and Manufacturing Technology*, vol. 8, No. 2, Jun. 1985, pp. 264-268.

Patent Abstracts of Japan, vol. 017, No. 126, Mar. 17, 1993, & JP-A-04 309 414.

Hoermann, K., "A Cartesian Approach To Findpath For Industrial Robots", *NATO ASI Series*, vol. F29, pp. 425-450, Springer-Verlag Berlin Heidelberg, DE (1987).

Fink et al., B., "Schnelle Bahnplanung Fuer Industrieroboter Mit Veraenderlichem Arbeitsraum", *Automatisierungstechnik-At*, vol. 39, No. 6, pp. 197-200, 201-204, Munich, DE (Jun. 1991).

Shaffer et al., C.A., "A Real-Time Robot Arm Collision Avoidance System", *IEEE Transactions on Robotics and Automation*, vol. 8, No. 2, pp. 149-160, New York, U.S.A. (Apr. 1992).

Lee et al., C.T. "A Divide-And-Conquer Approach With Heuristics Of Motion Planning For A Cartesian Manipulator", *IEEE Transactions on Systems, Man and Cybernetics*, vol. 22, No. 5, pp. 929-944, New York U.S.A. (Sep./Oct. 1992).

O'Donnell et al., P.A., "Deadlock-Free And Collision-Free Coordination Of Two Robot Manipulators", *Proceedings of the 1989 IEEE International Conference on Robotics and Automation*, vol. 1, pp. 484-489, Scottsdale, AZ (May 1989).

Weule et al., V.H., "Rechnerintegrierte Fertigung Von Abkanteilen", *V.A.I.-Zeitschrift*, vol. 130, No. 9 pp. 101-106, Dusseldorf, W. Germany (Sep. 1988).

Reissner, V.J., "Innovationsschub Bei Rechnerintegrierten Umformsystemen", *Technische Rundschau*, vol. 85 No. 5, pp. 20-25, Bern, CH (Feb. 5, 1993).

Geiger et al., M., "Inferenzmaschine Fuer Ein Biegestadienplanungssystem", *Zwf Cim Zeitschrift Fur Wirtschaftliche Fertigung Und Automatisierung*, vol. 87, No. 5, pp. 261-264, Munich, DE (May 1992).

Database Dialog, Information Access Co., File 621, Access No. 0134529, *Communigraphics Inc*: "LVD Introduces New CNC/DNC/CAD/CAM Control System For Press Brakes At IMTS'86", & New Product Announcements, No. 0134529, Plainville, CT, U.S.A. (Jul. 1996).

An International Search Report for PCT/JP 95/02288.

An Invitation to Pay Additional Fees with a Partial International Search Report for PCT/JP 95/02289.

An International Search Report for PCT/JP 95/02290.

An International Search Report for PCT/JP 95/02291.

Murray, Anne M., A Fingerpad Force Sensor for Manipulating Sheet Metal, submitted to Dept. of Electrical and Computer Eng., Carnegie Mellon Univ., Pittsburgh, PA, (Aug. '93).

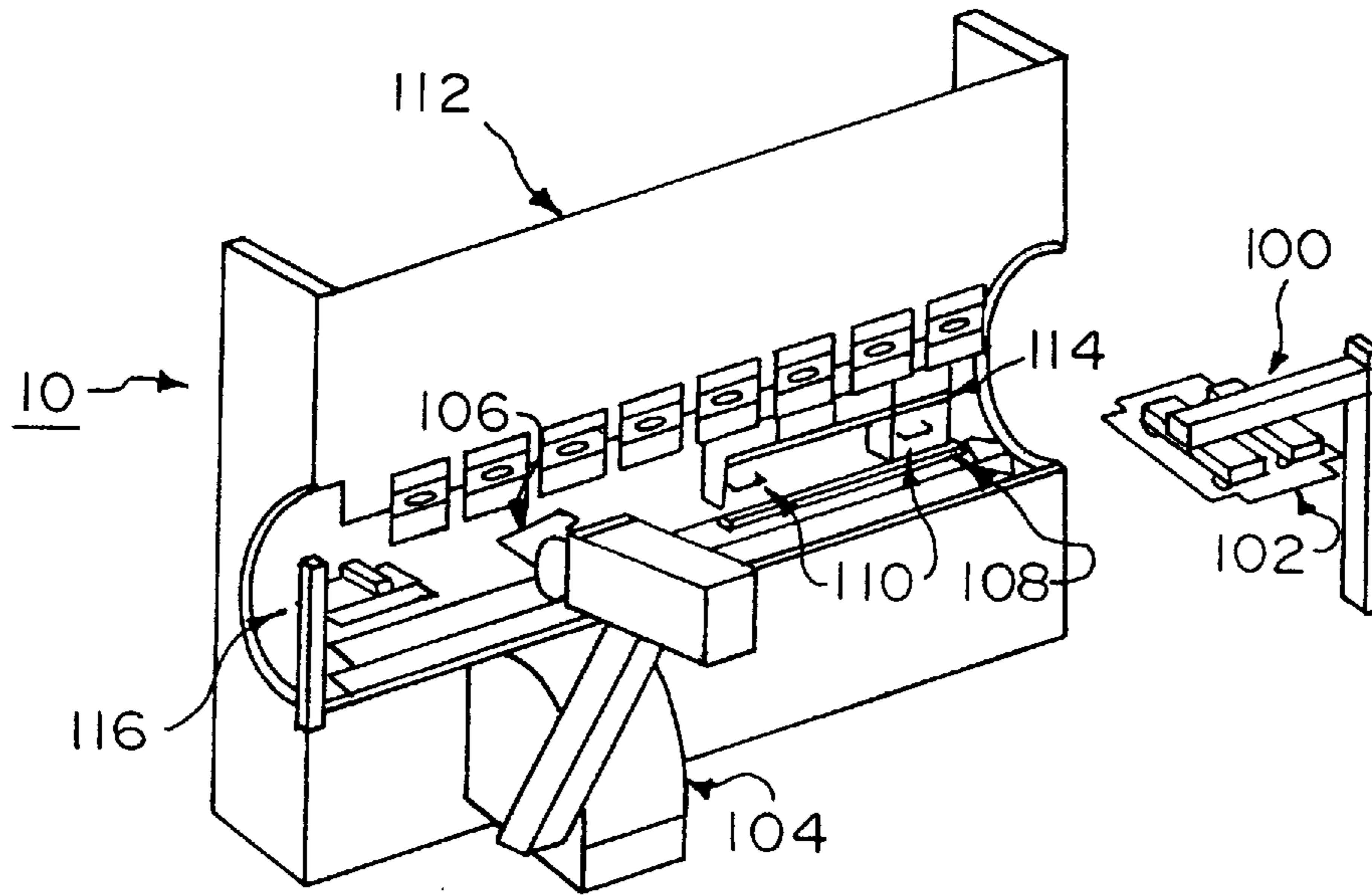


FIG. 1

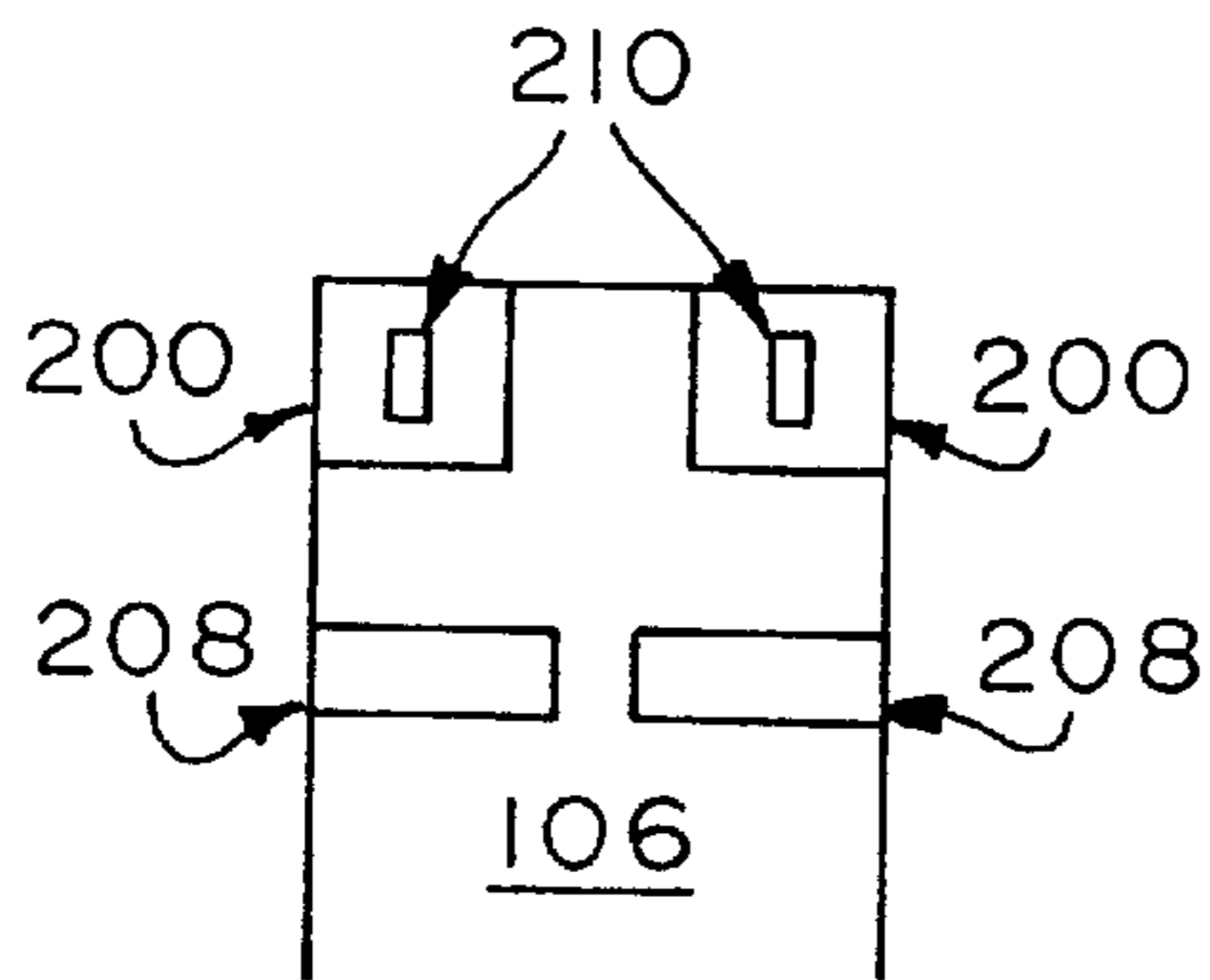


FIG. 6

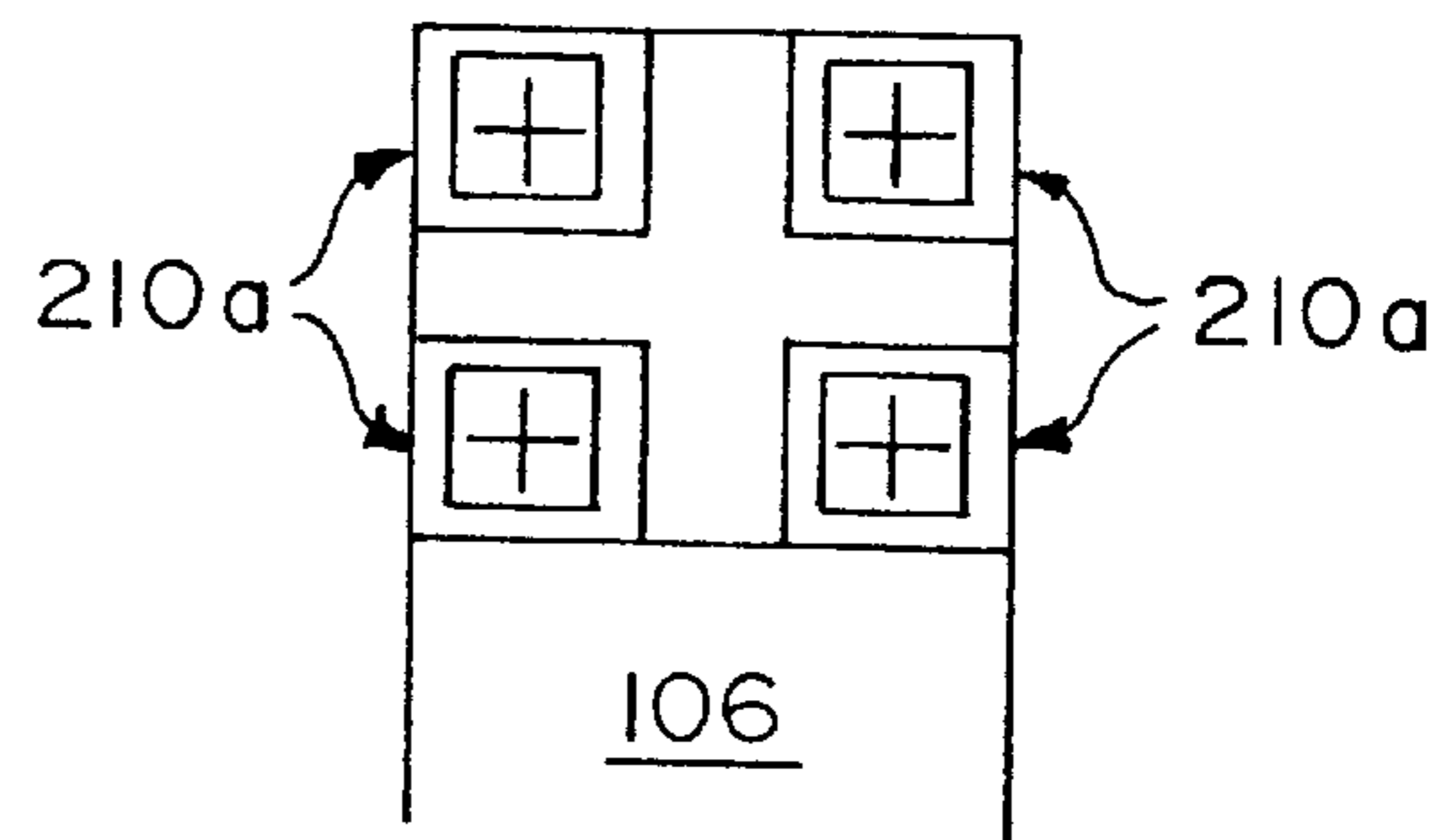


FIG. 7

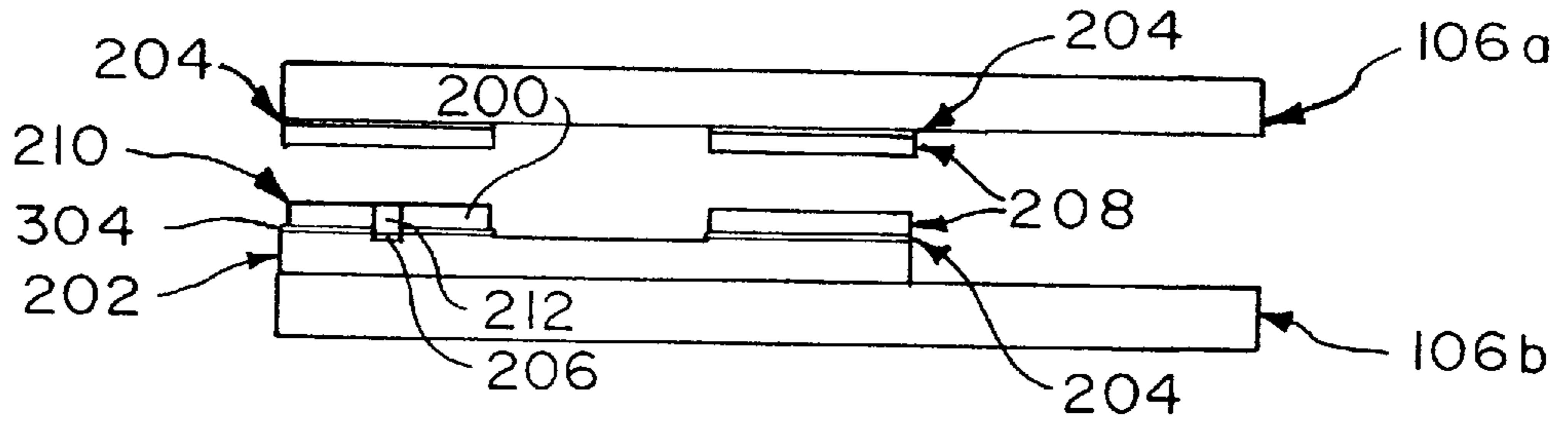


FIG. 2

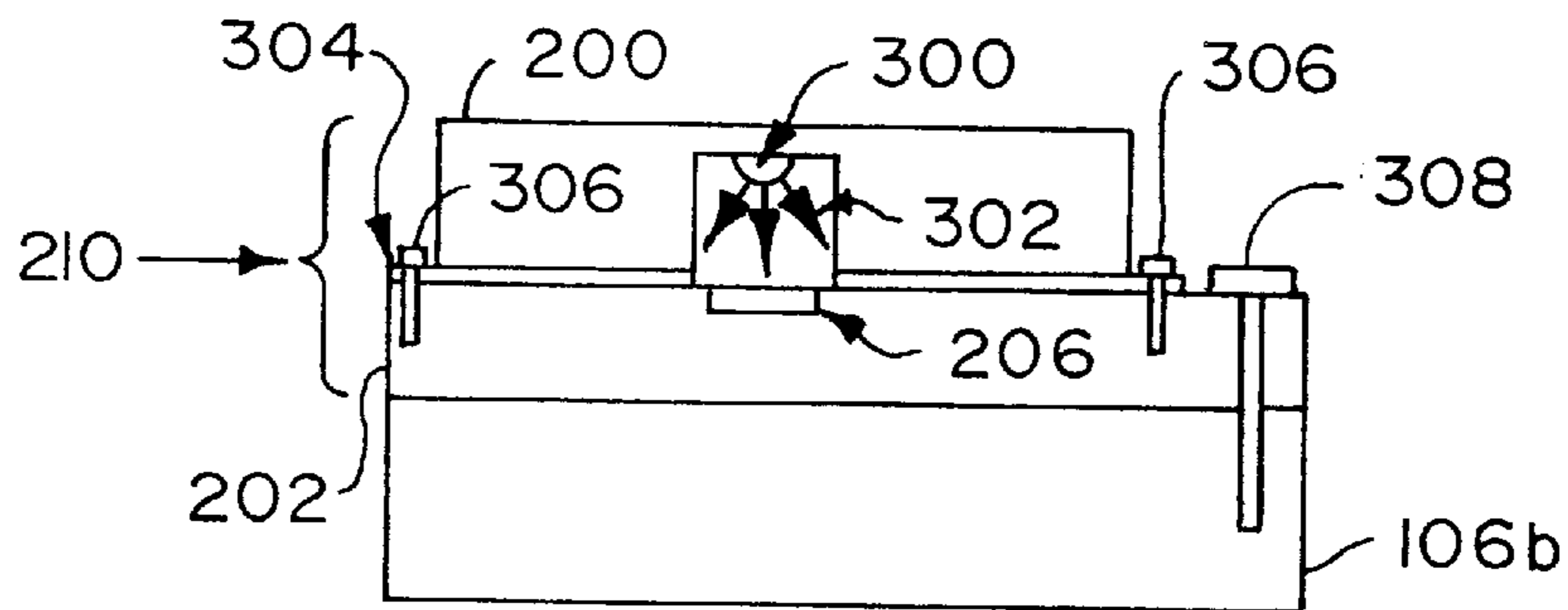


FIG. 3

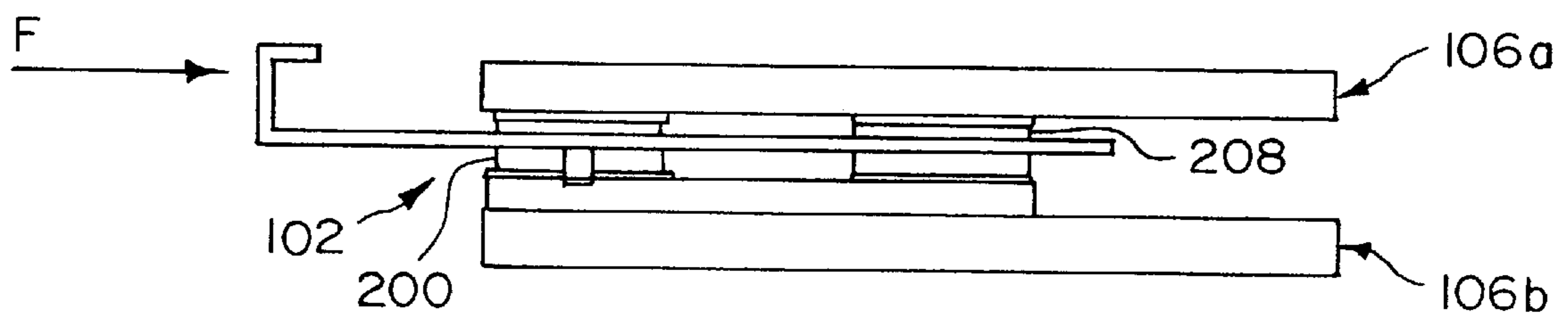


FIG. 4

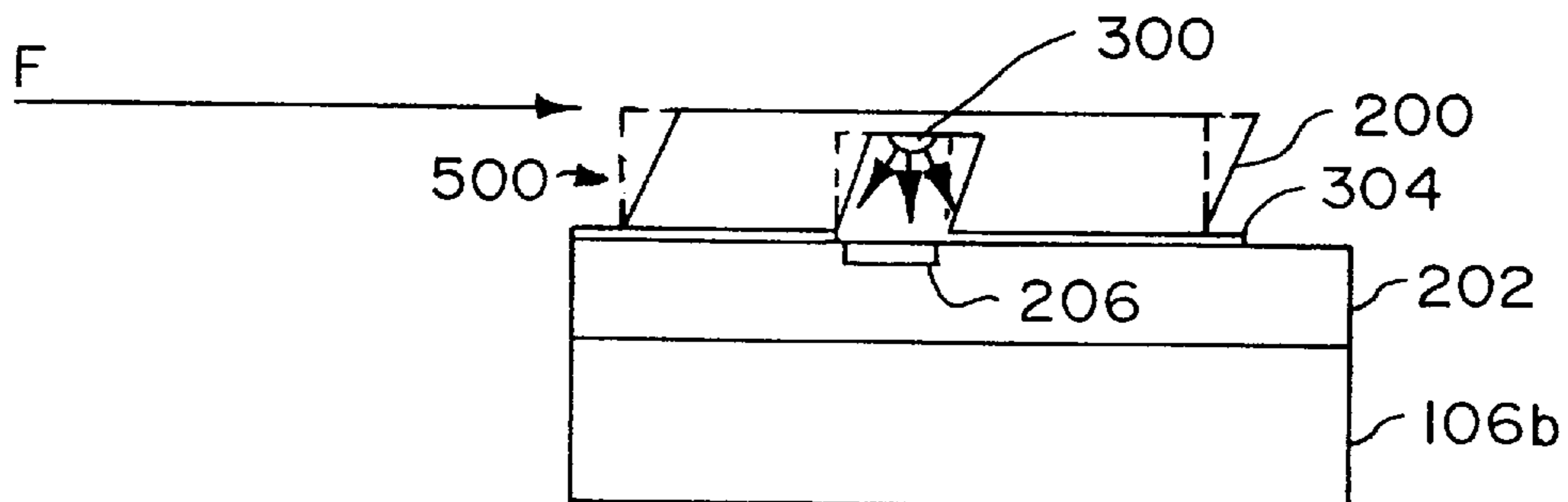


FIG. 5

FIG. 8A

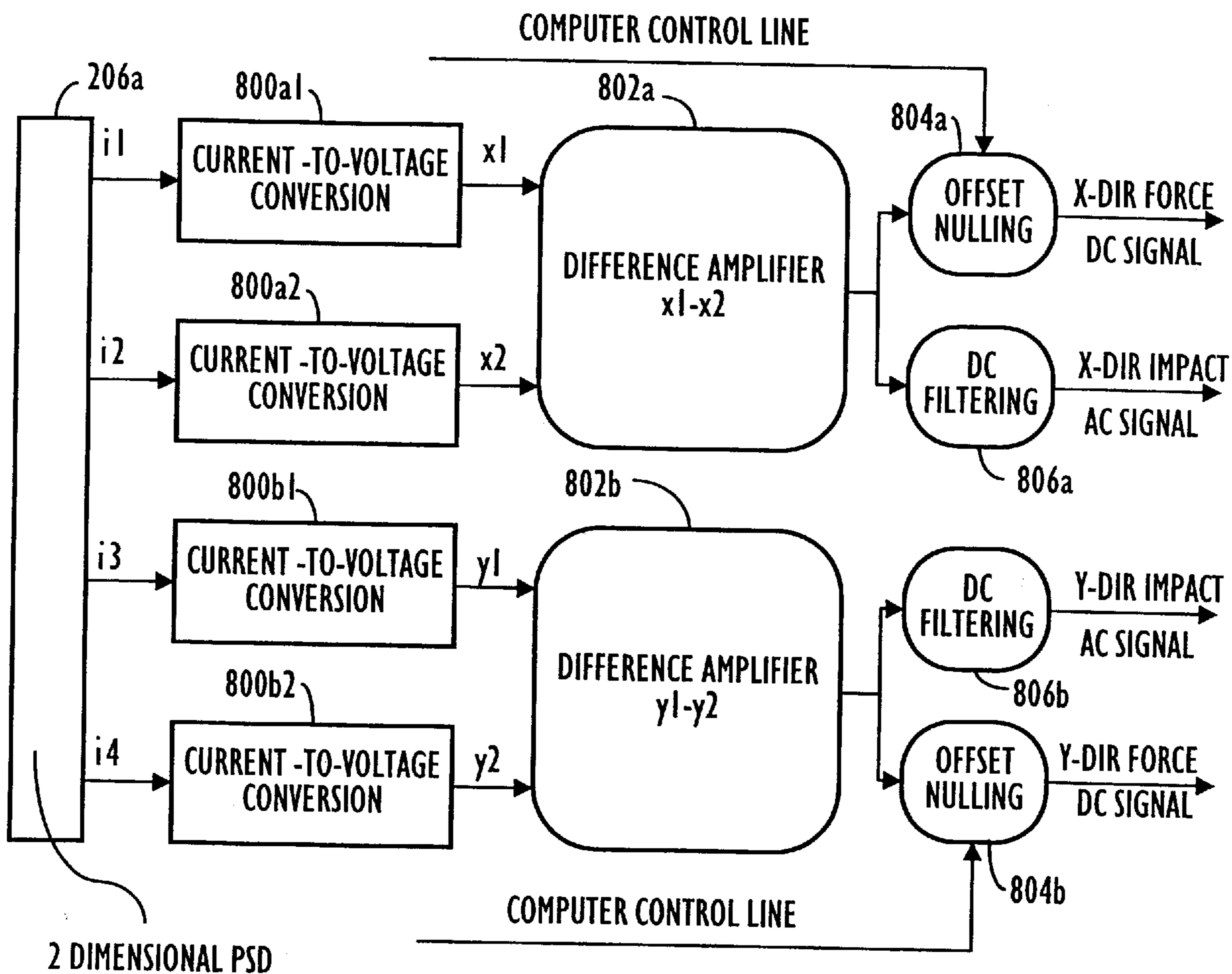
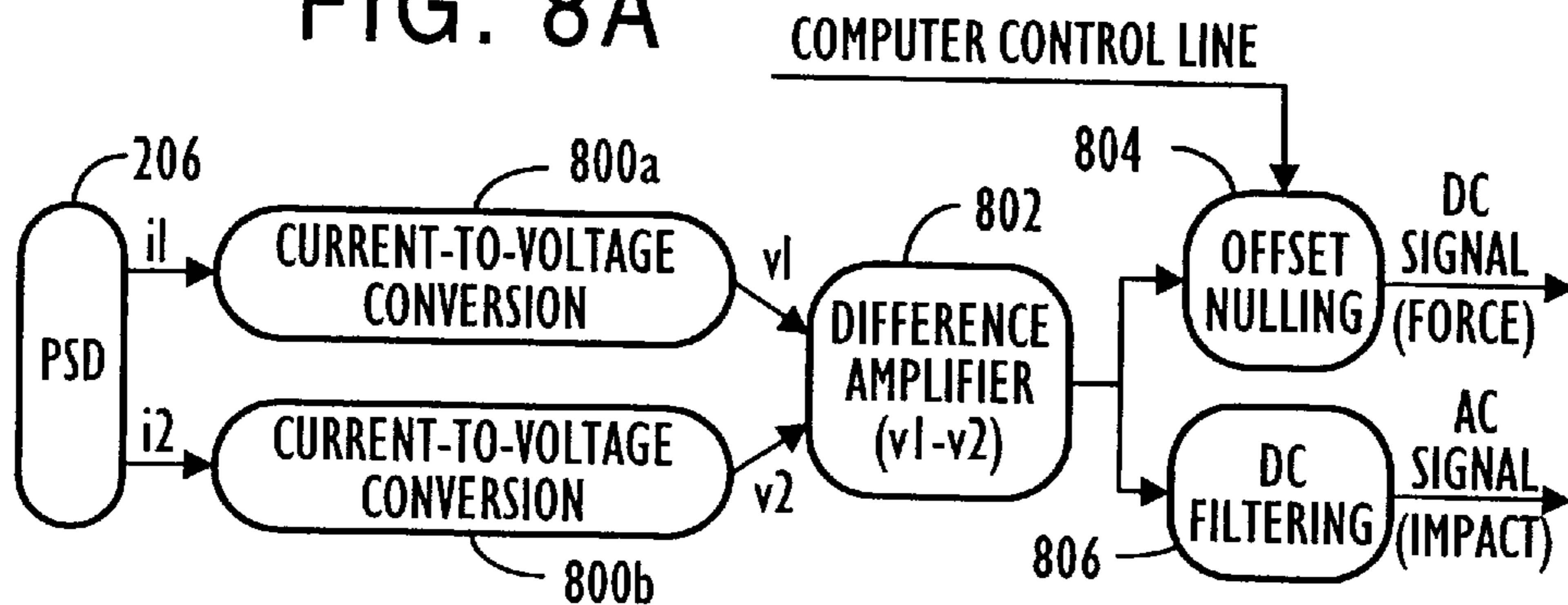


FIG. 8B

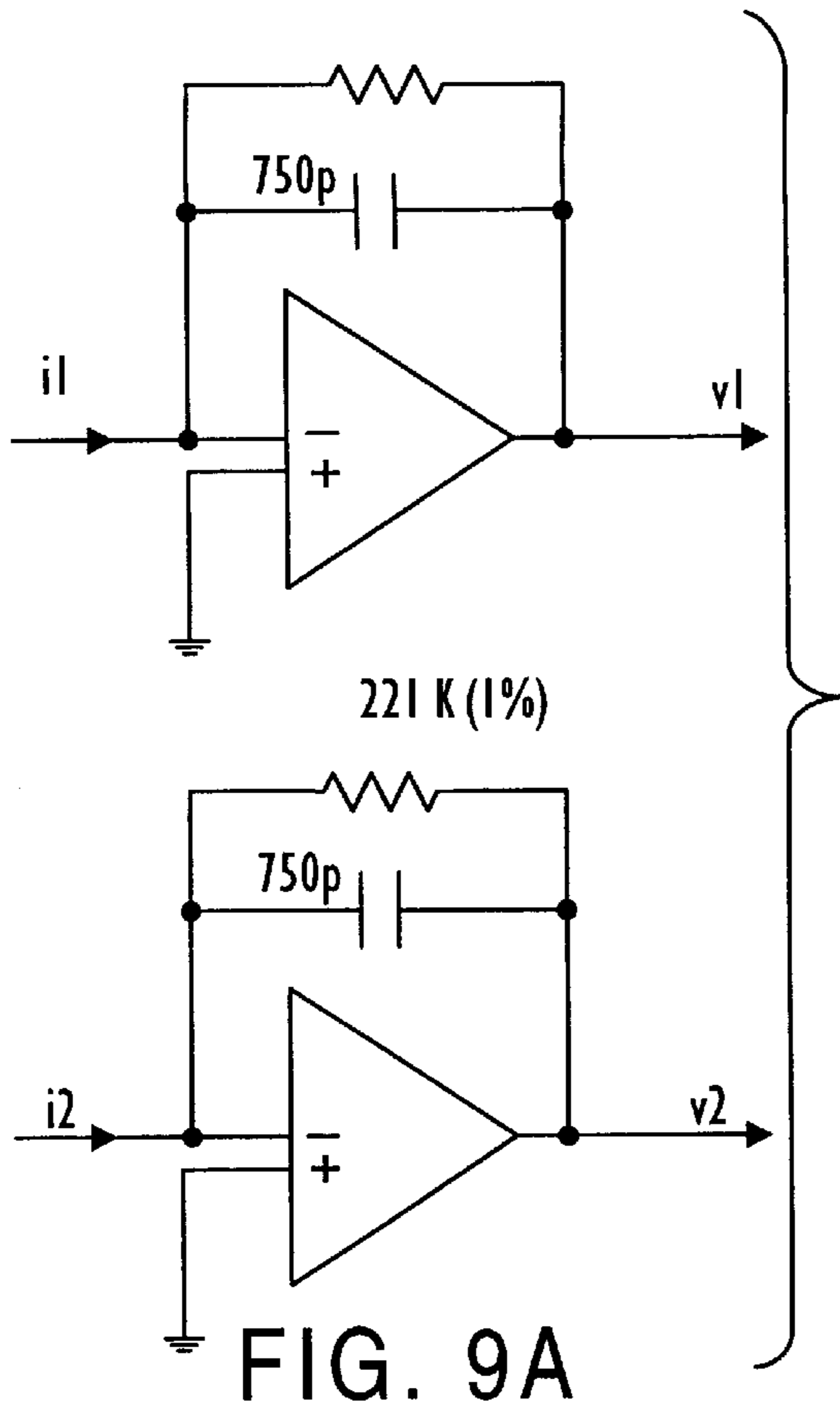


FIG. 9A

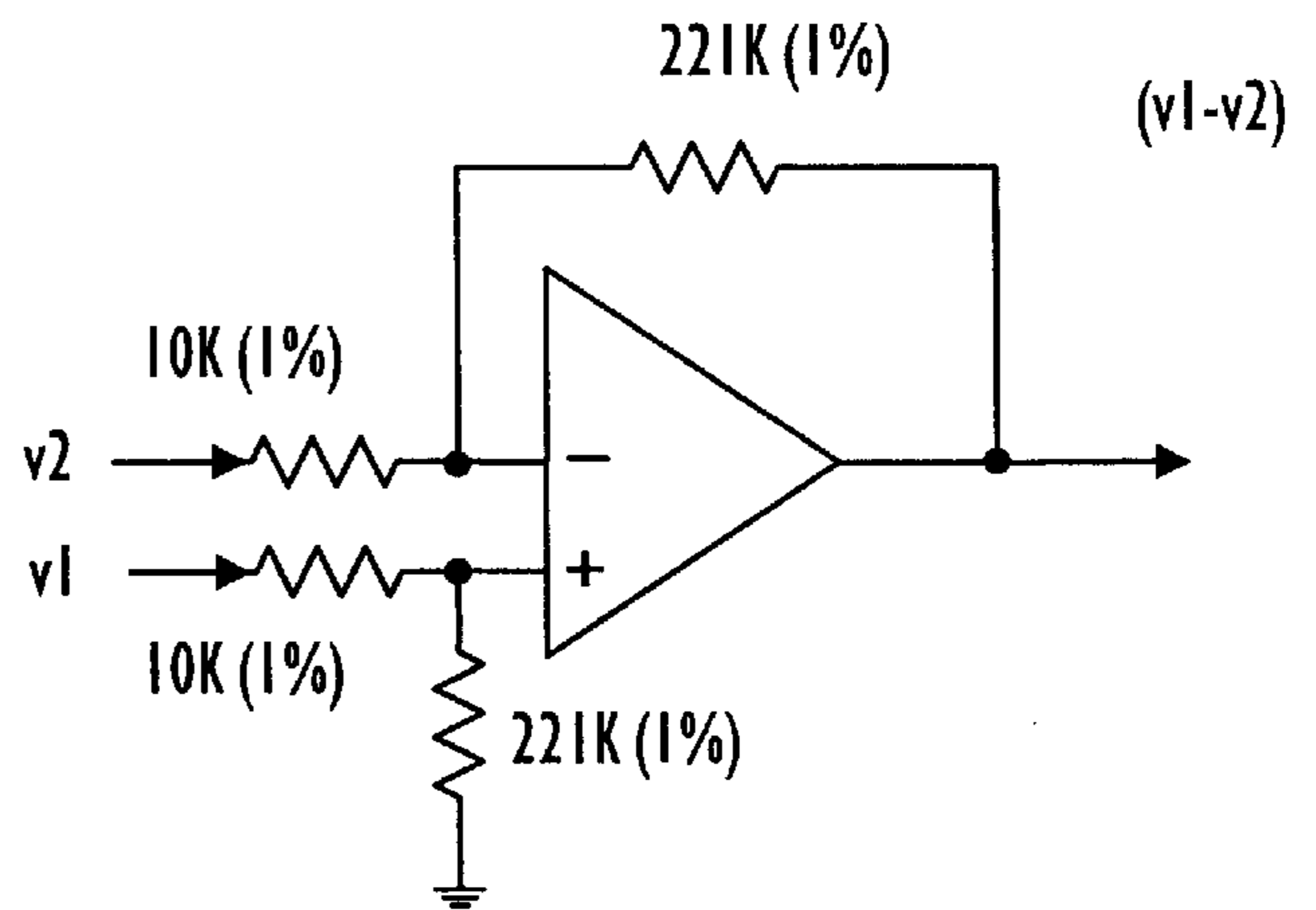


FIG. 9B

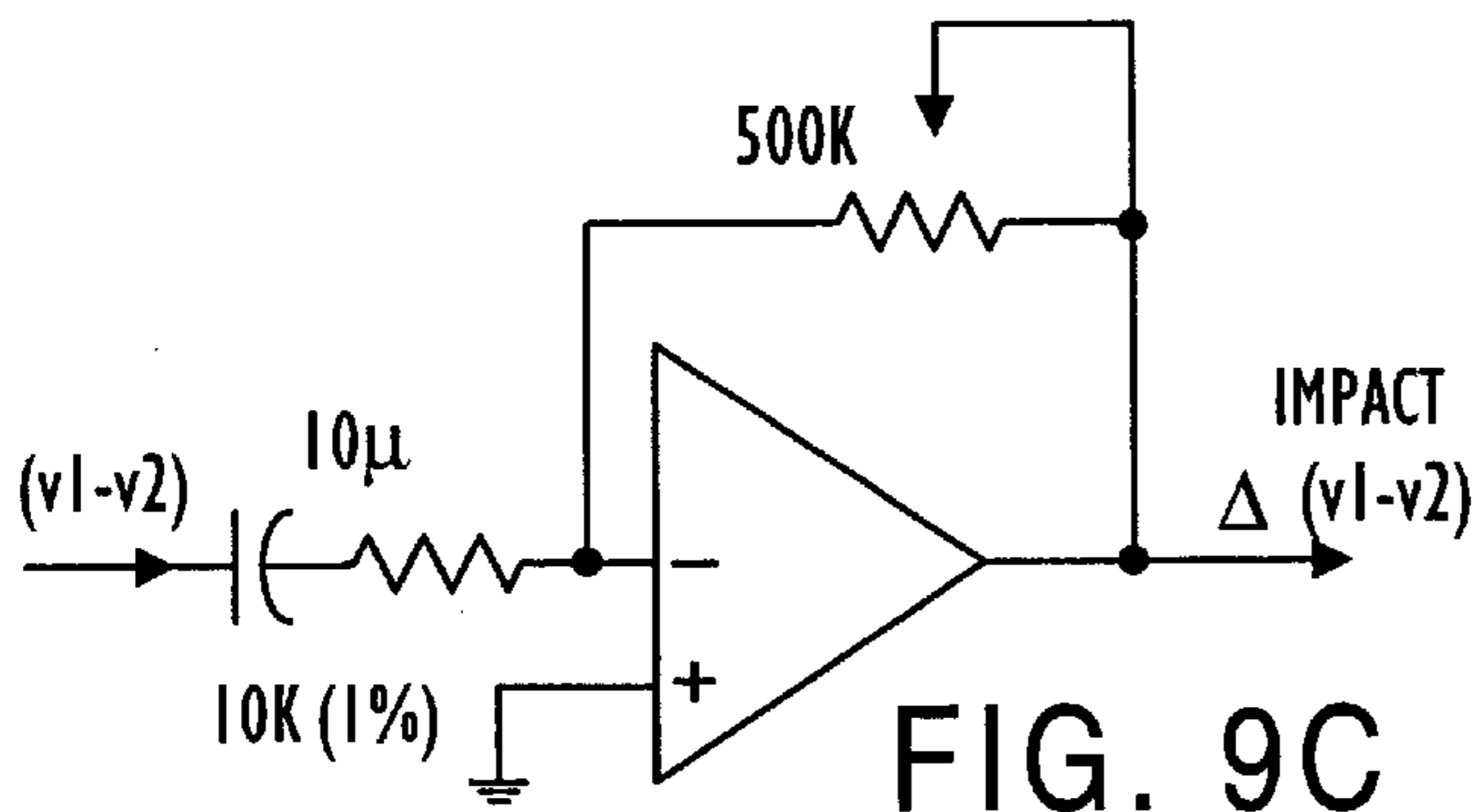


FIG. 9C

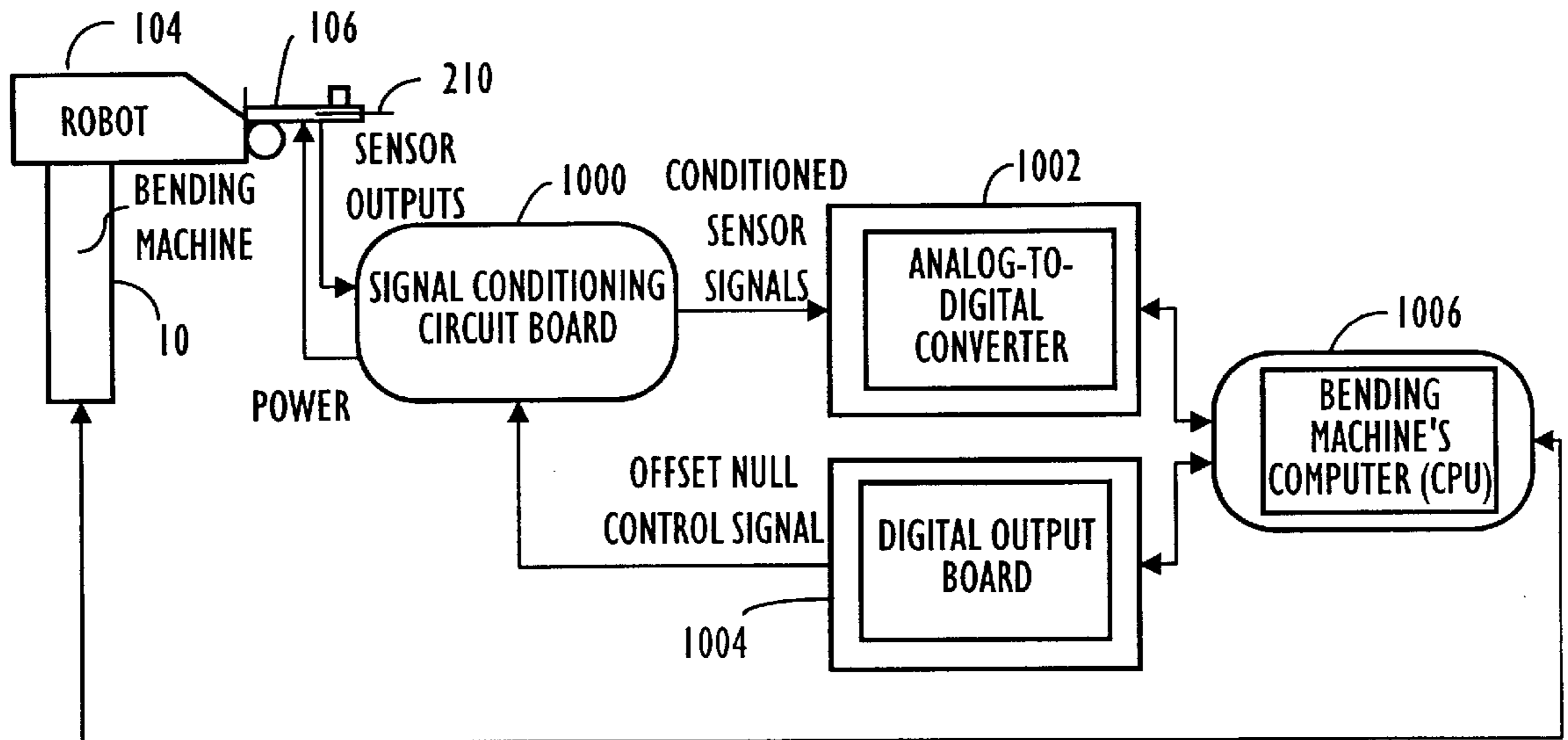


FIG. 10

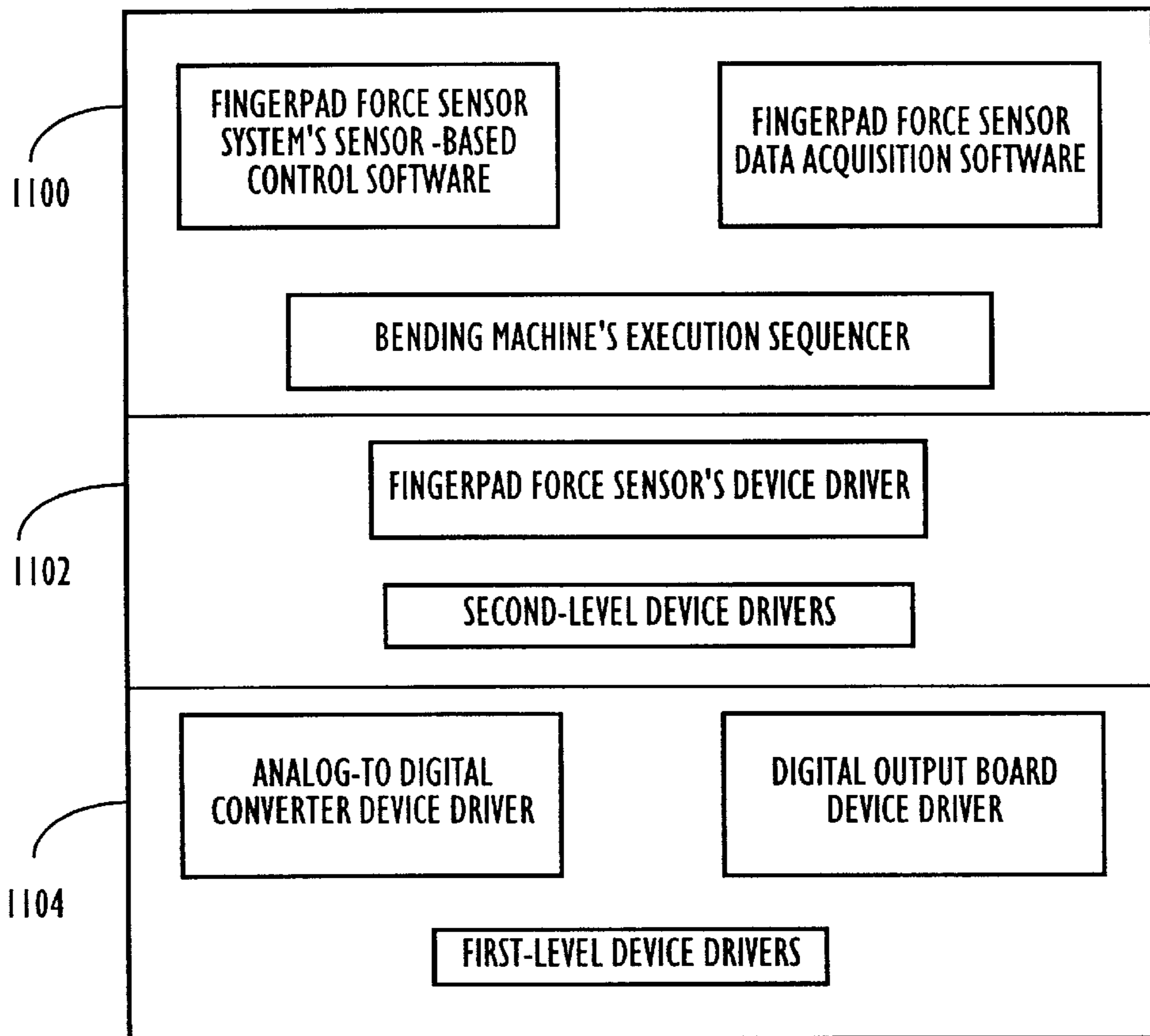


FIG. 11

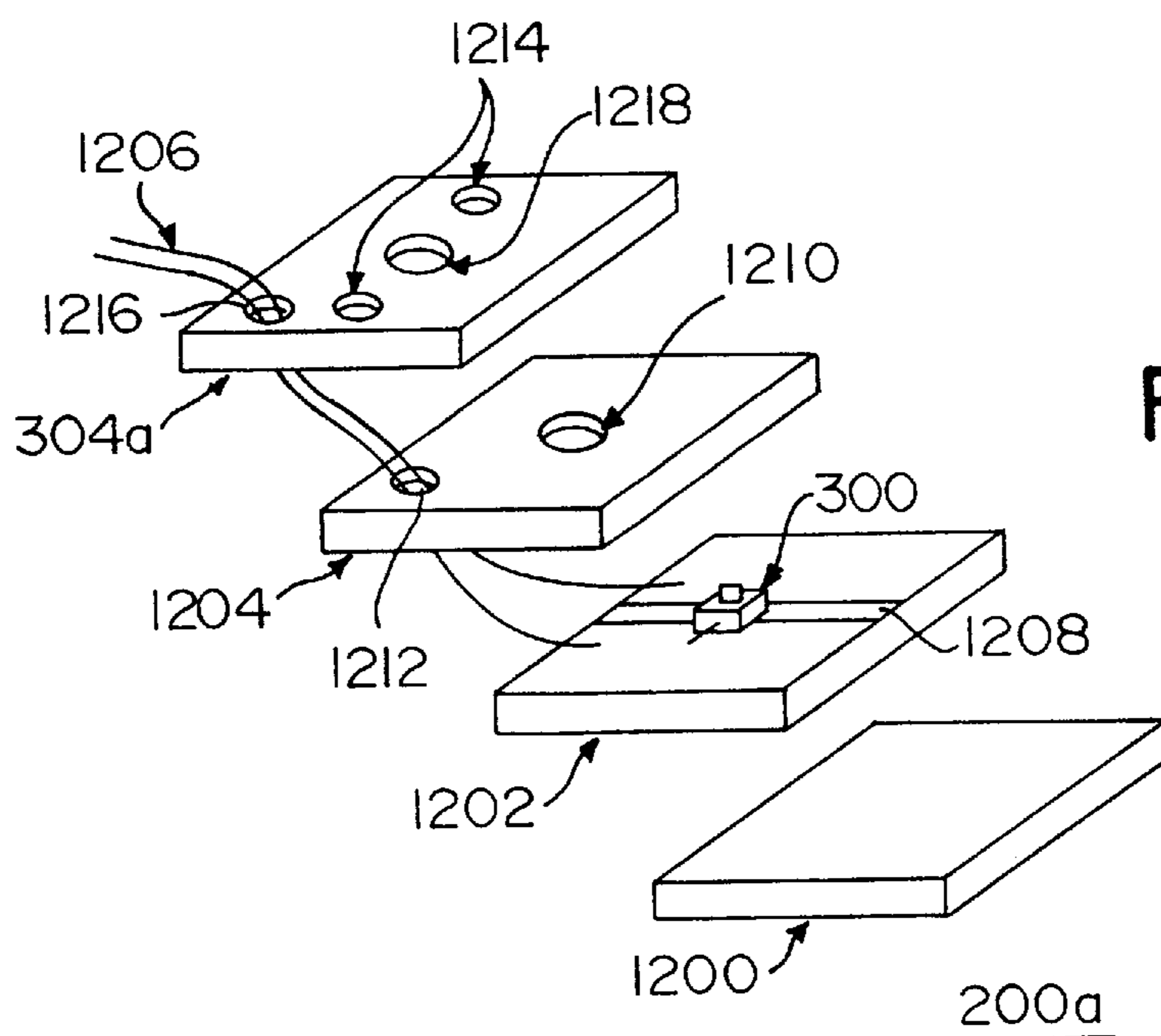


FIG. 12

FIG. 13A

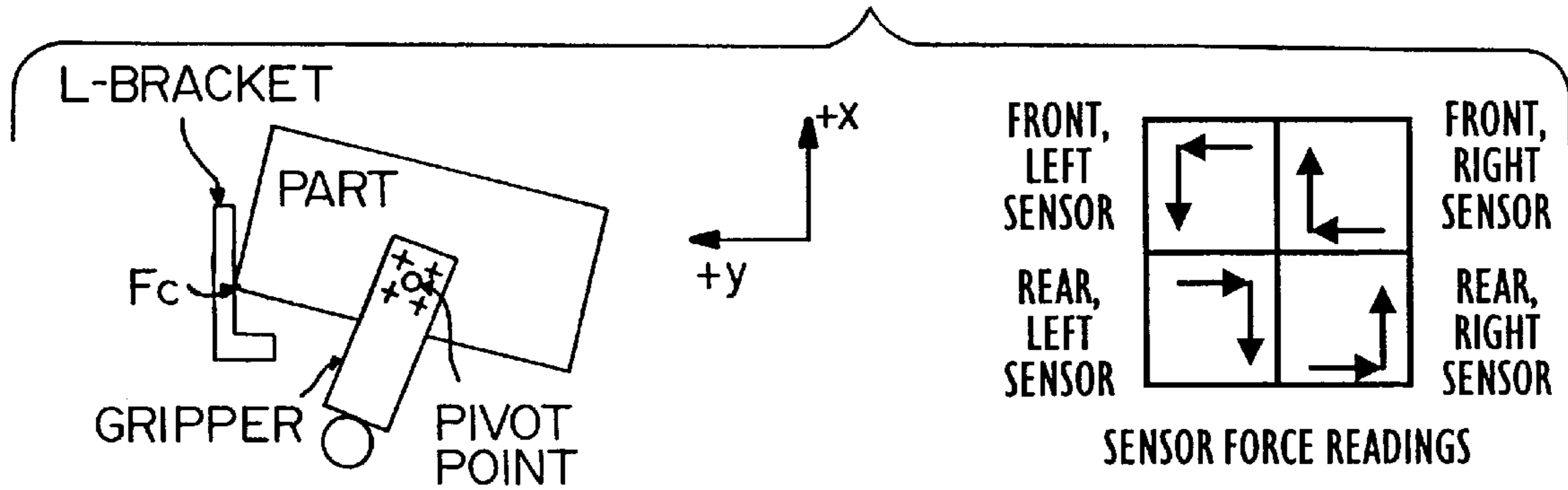


FIG. 13B

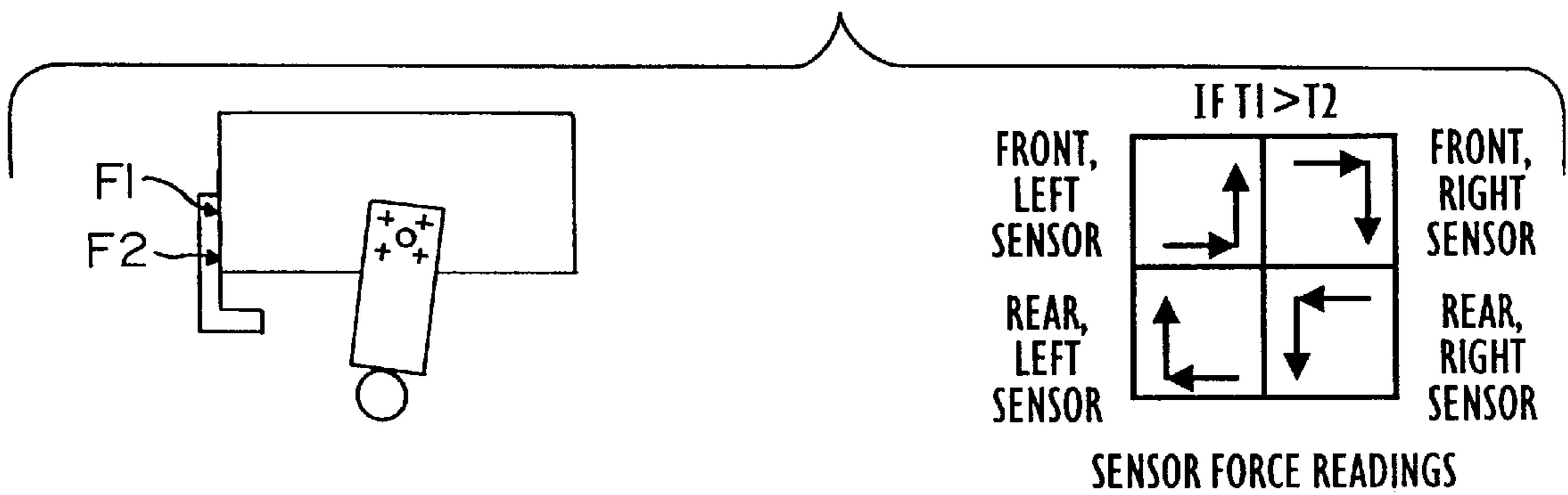


FIG. 13C

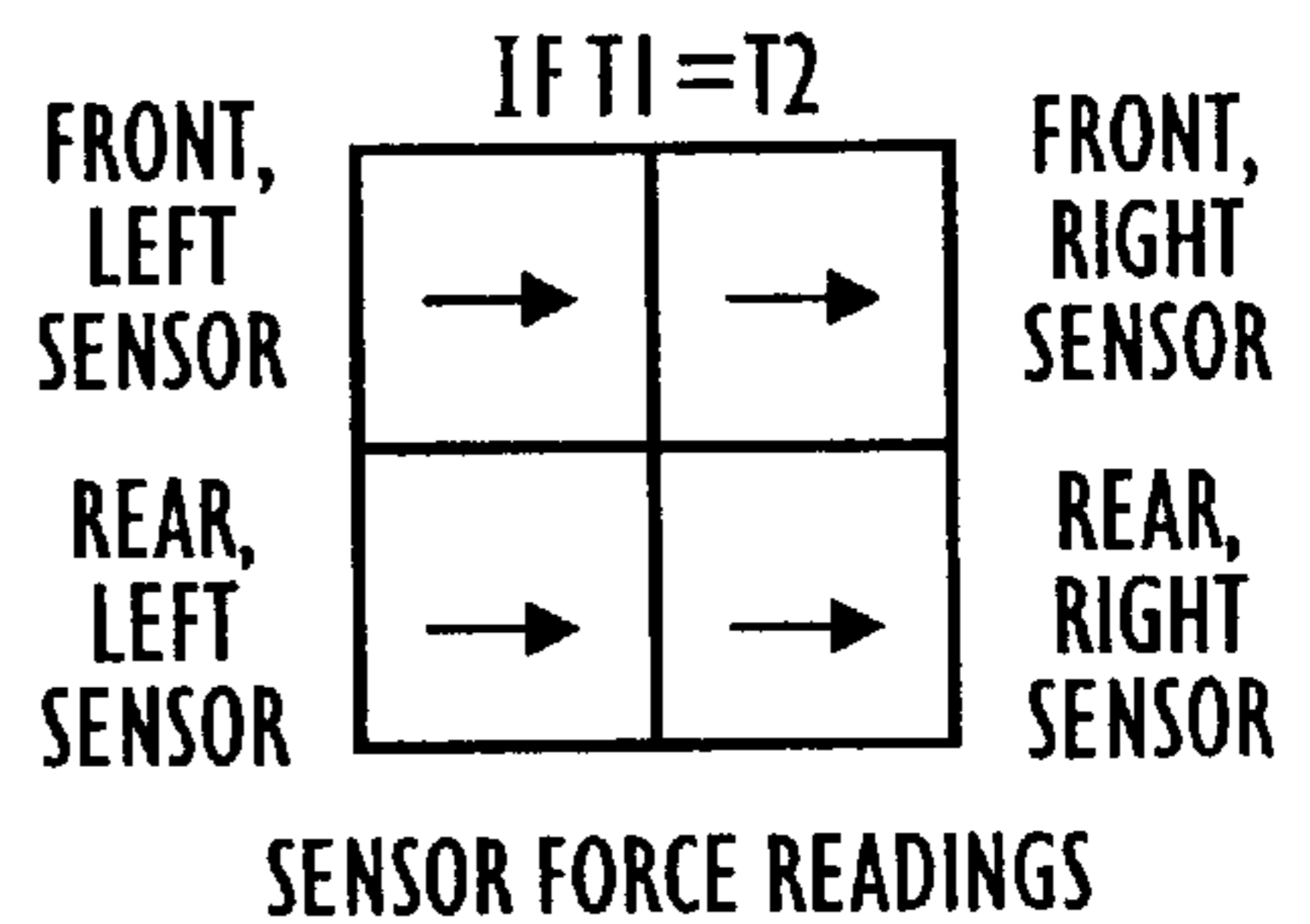


FIG. 13D

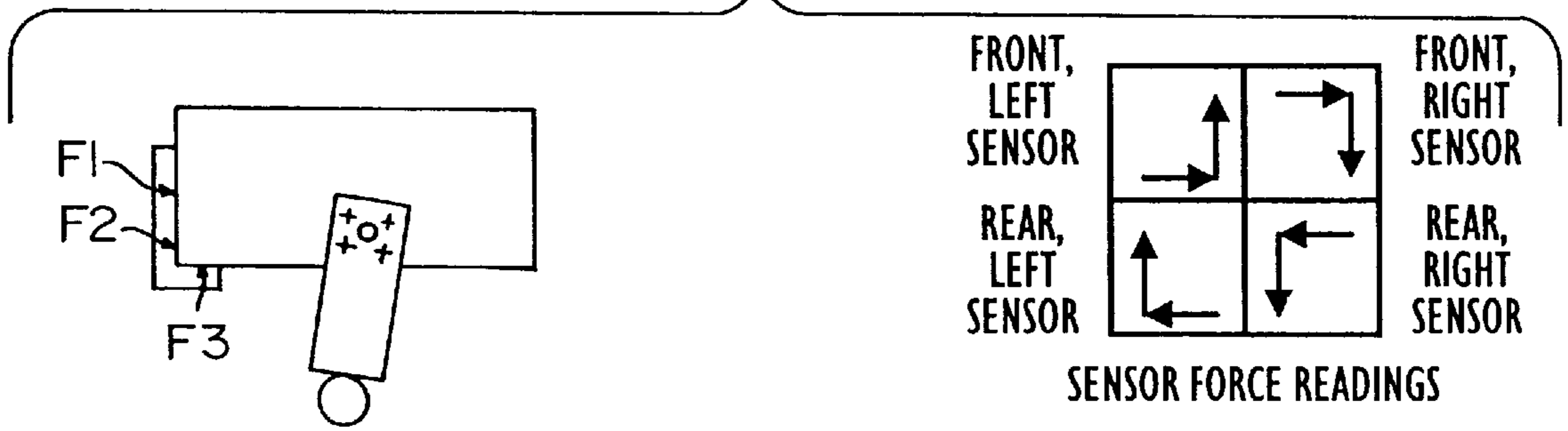


FIG. 13E

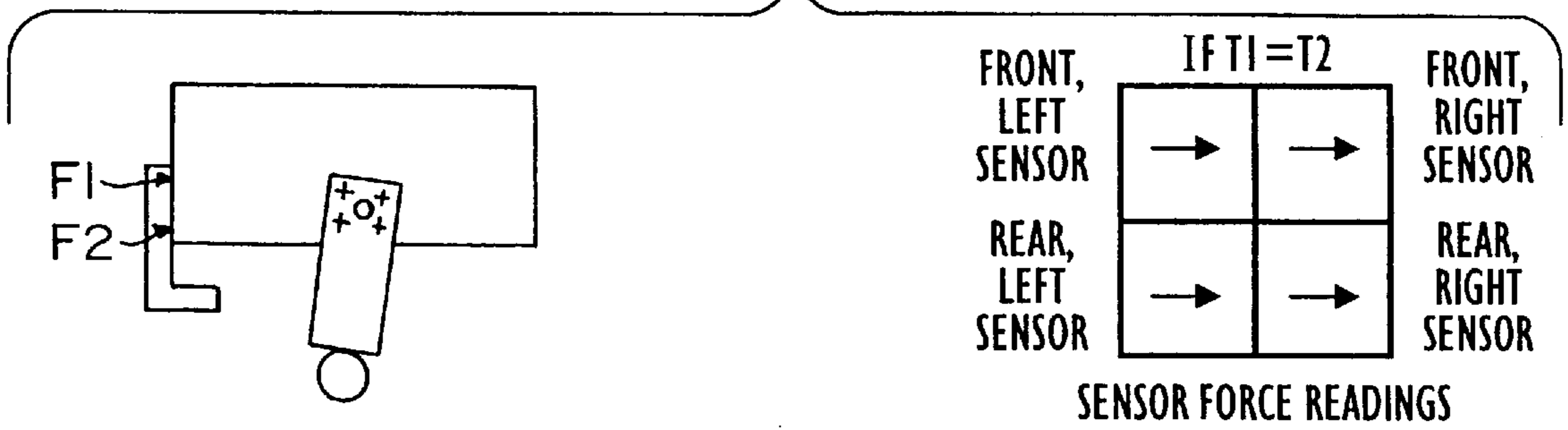


FIG. 14A

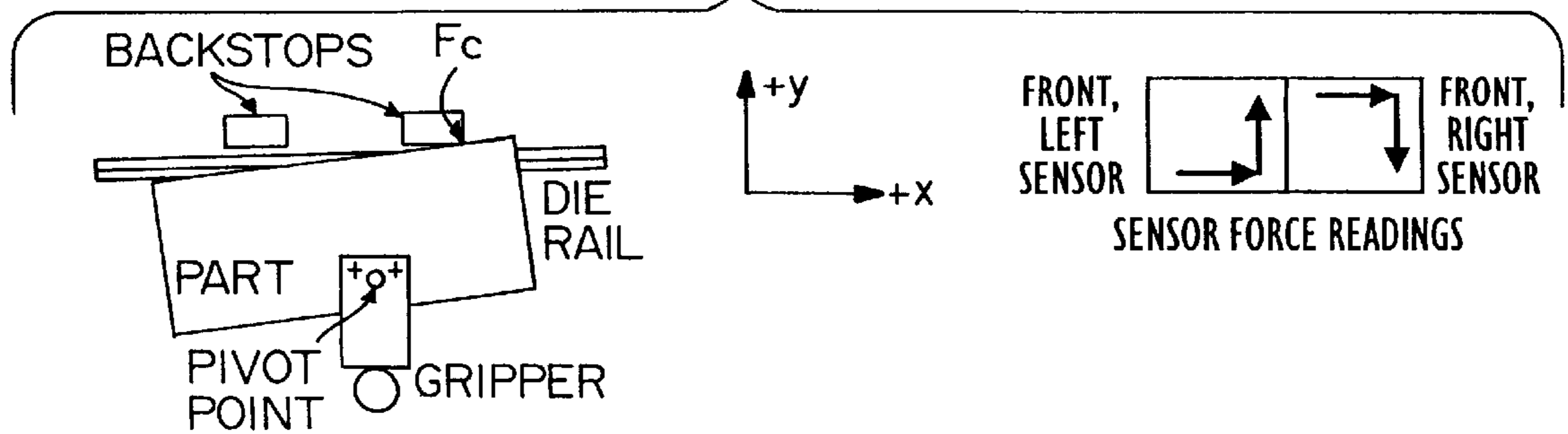


FIG. 14B

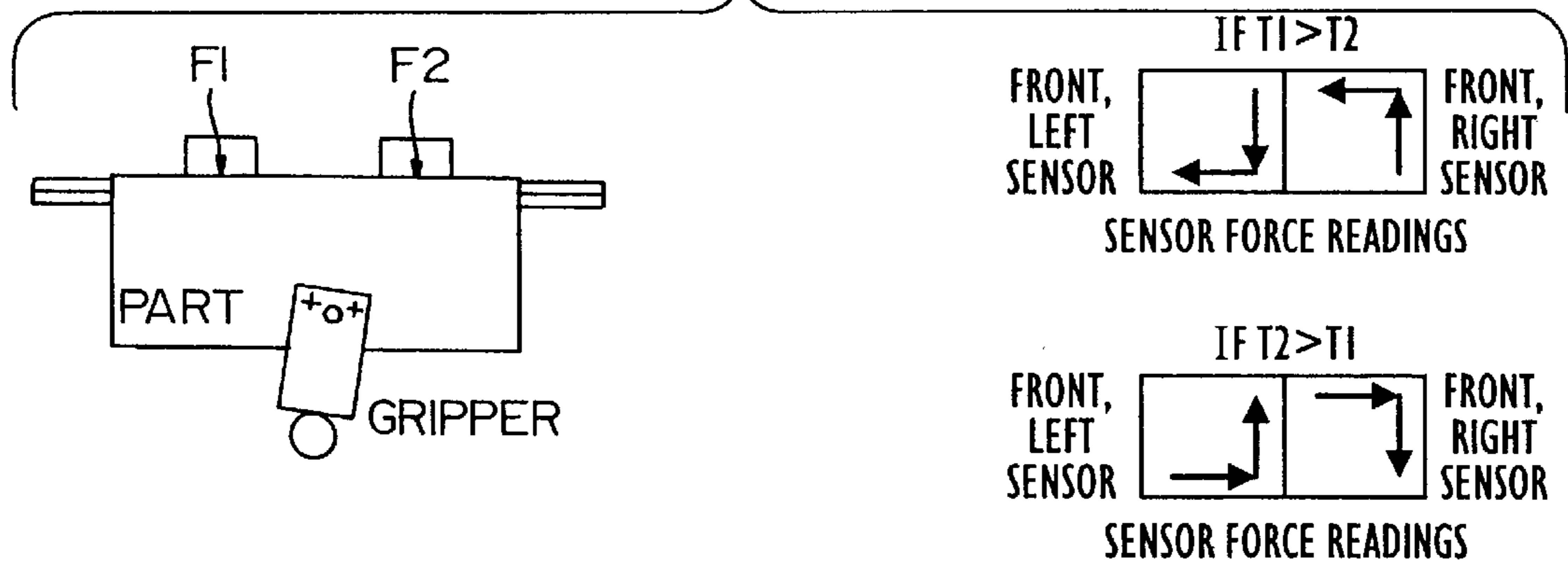


FIG. 14C

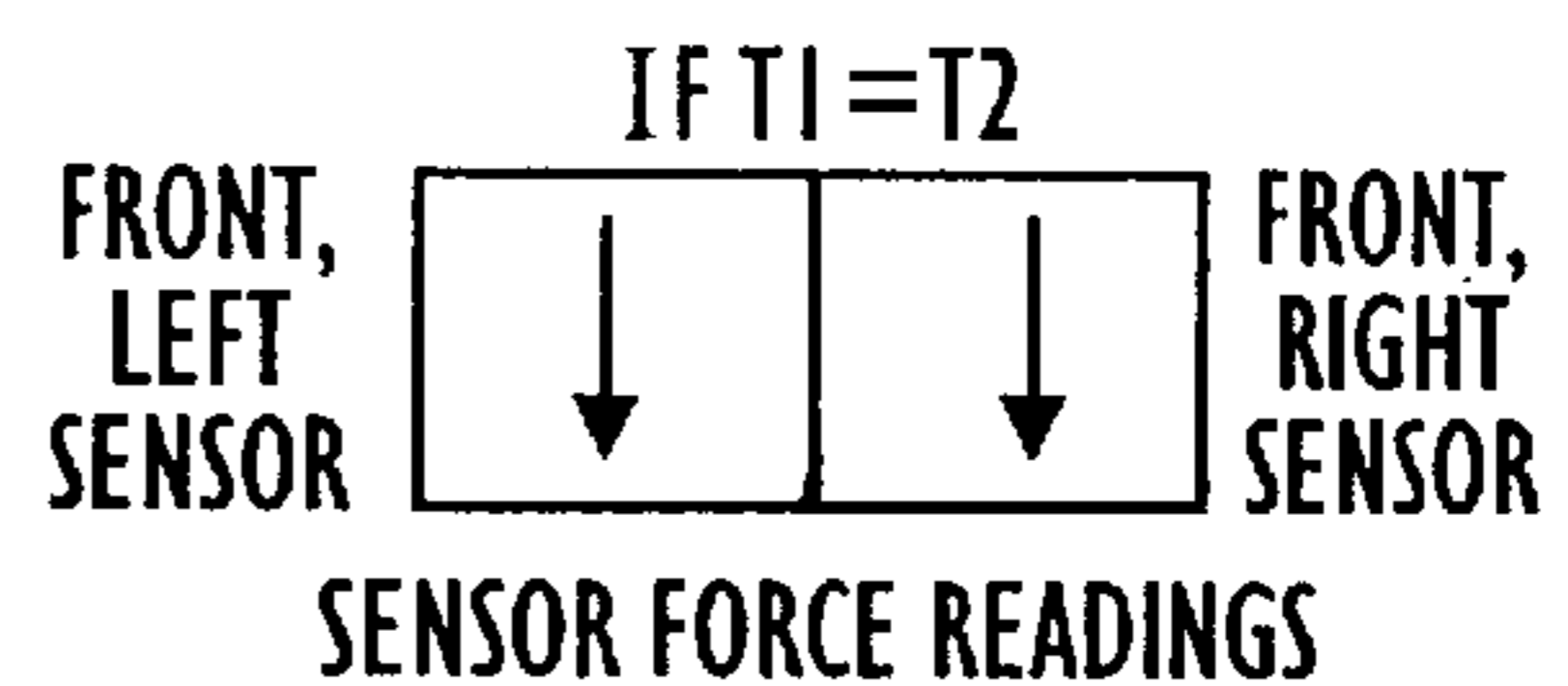


FIG. 16

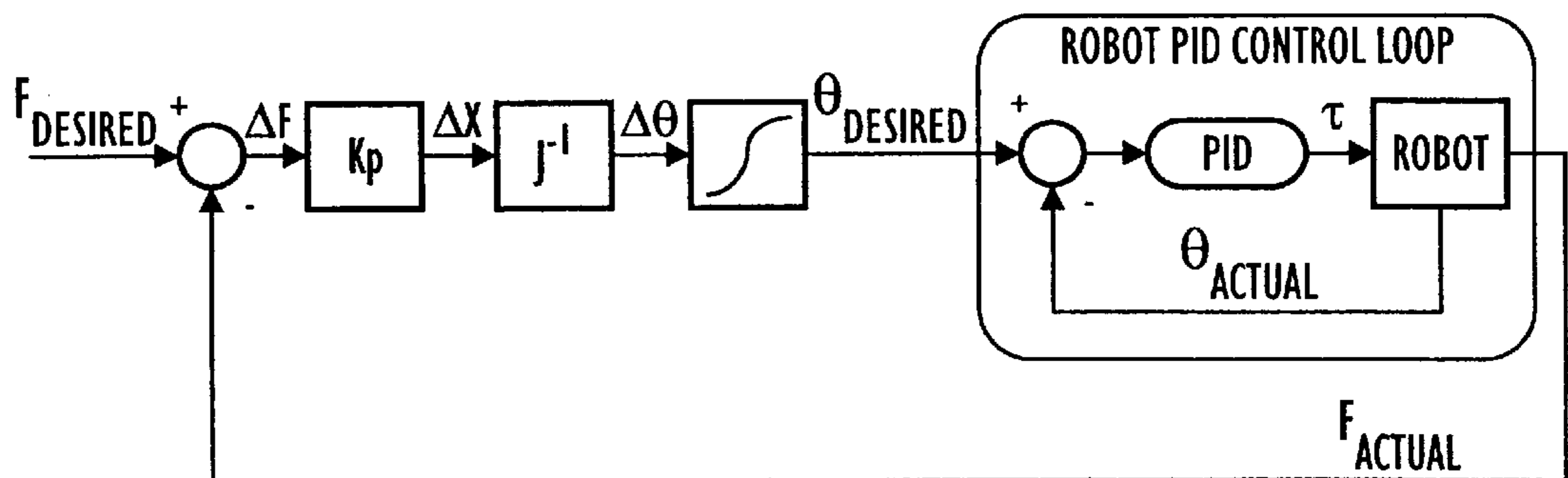


FIG. 14D

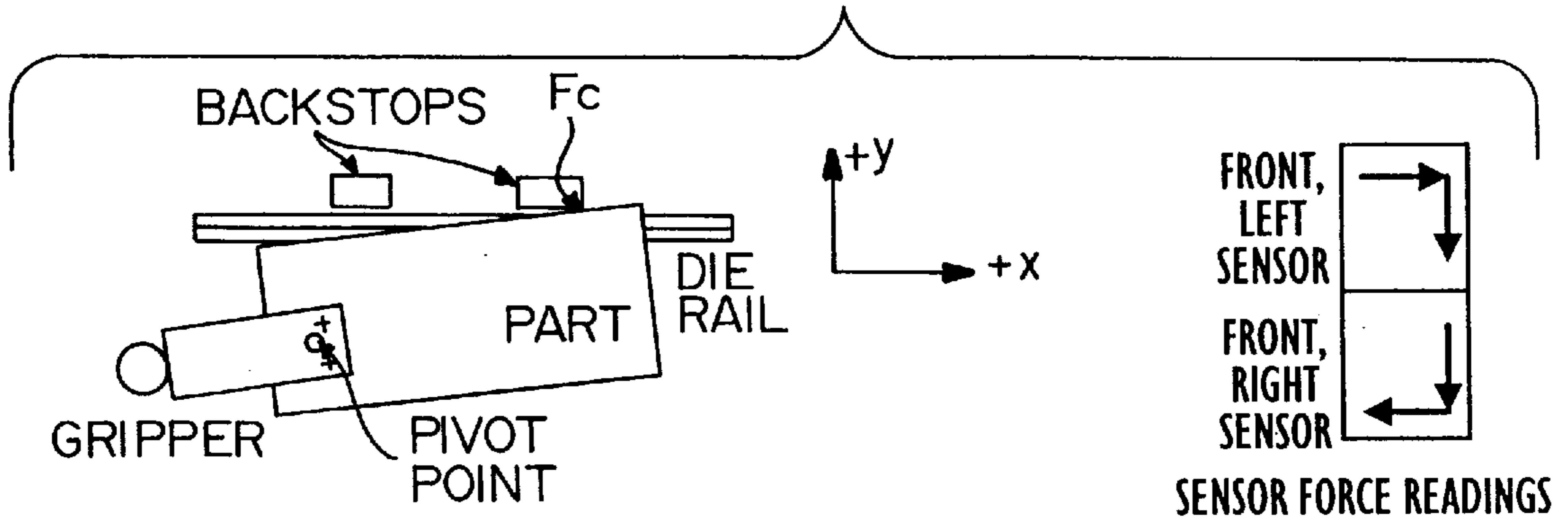


FIG. 14E

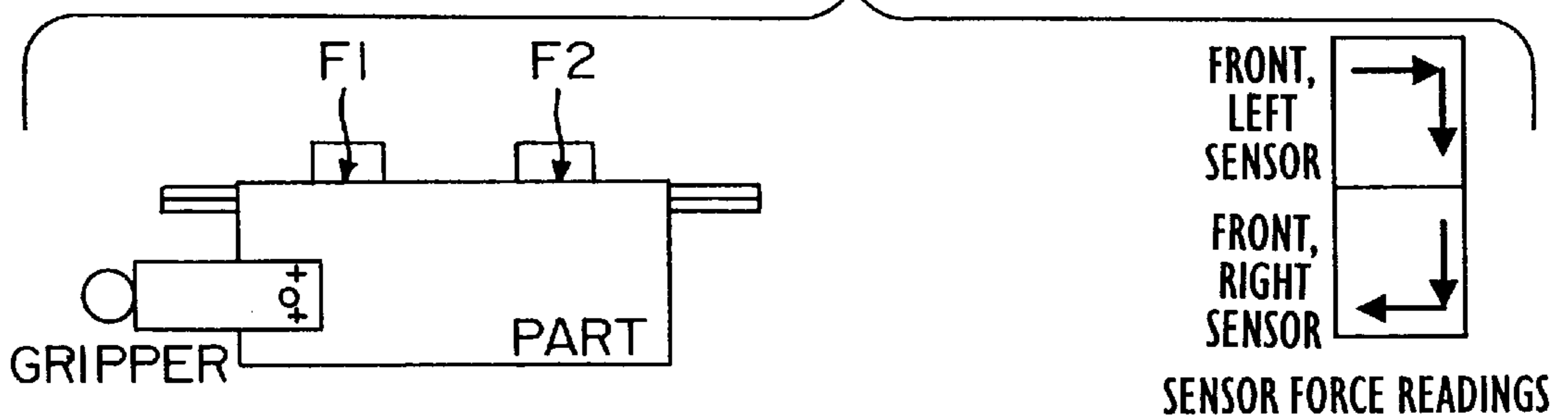
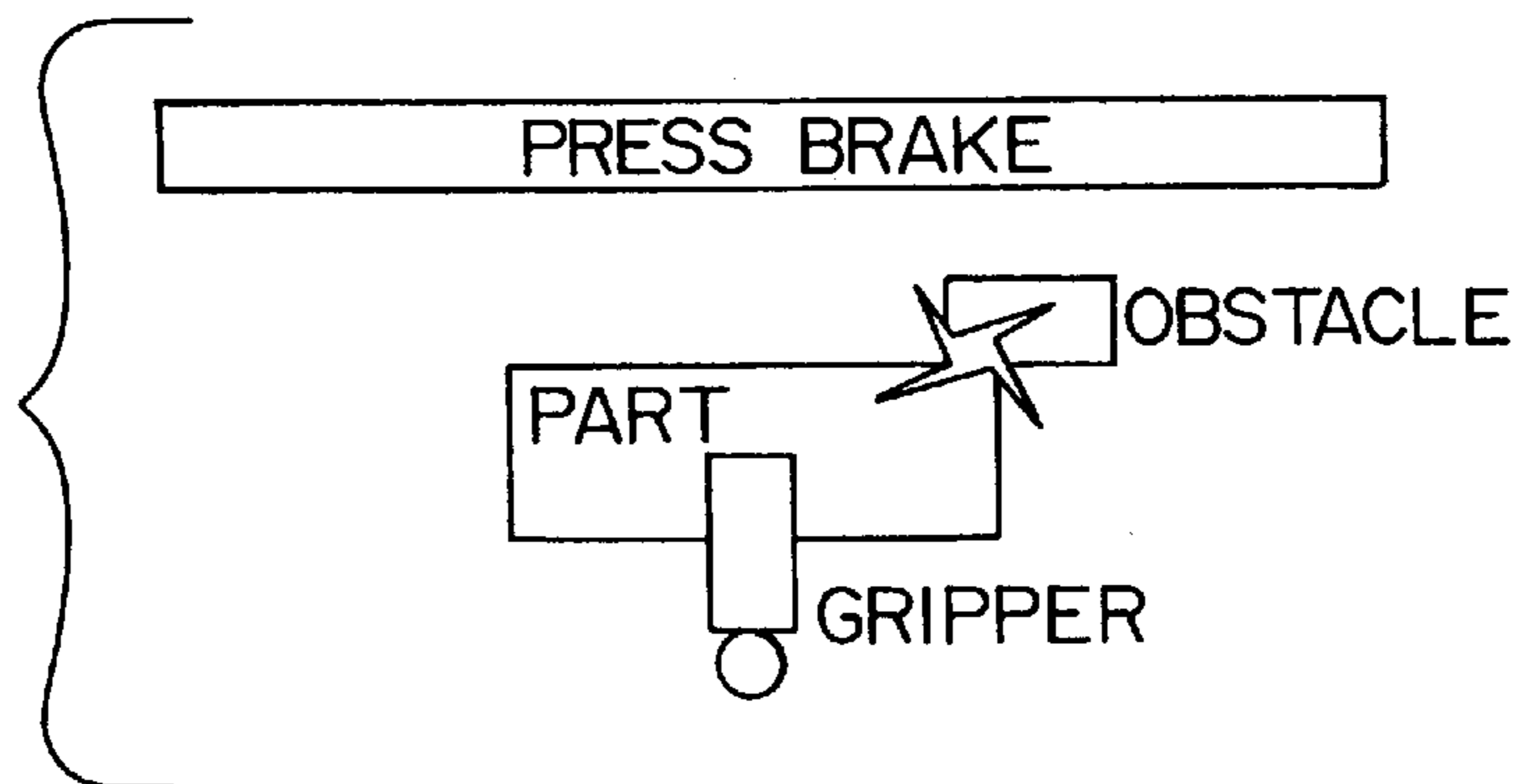


FIG. 15



FINGERPAD FORCE SENSING SYSTEM

This application is a continuation of application Ser. No. 08/338,095, filed Nov. 9, 1994, now abandoned.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present disclosure is related to the disclosures provided in the following U.S. applications filed concurrently herewith: "Intelligent System for Generating and Executing a Sheet Metal Bending Plan", filed in the names of David Alan Bourne et al. (U.S. Ser. No. 08/338,113); "Methods and Apparatuses for Backgaging and Sensor-Based Control of Bending Operations", filed in the names of Richard M. Moore et al. (U.S. Ser. No. 08/388,153); and "Method for Planning/Controlling Robot Motion", filed in the names of David Alan Bourne et al. (U.S. Ser. No. 08/338,115); and the disclosures of all of these applications are expressly incorporated by reference herein in their entireties.

The present invention relates to a fingerpad force sensing system for providing electrical signals representative of the force of material in contact with a fingerpad force sensor. More particularly, the present invention relates to a fingerpad force sensing system which is used to provide an indication of the force applied to a planar object which is in contact with the fingerpad force sensor of the system.

2. Background and Material Information

In mass-production systems for fabricating products made from planar materials, such as, for example, sheet metal, there is a need for manufacturing the desired products quickly, accurately and at the lowest possible cost. Mass-production systems which produce large batches of a product are able to distribute the cost of errors and the set-up and fine tuning of the fabrication machine such that the cost per product produced is relatively low. However, there is a continuing emphasis on producing a product at the lowest possible cost.

The cost per product produced is even more important in small-batch and custom part manufacturing systems which do not have the economies of scale of the mass-production systems and, therefore, cannot spread the cost of errors and mistakes over the same large product batch sizes as the mass-production systems. Therefore, such small-batch and custom part manufacturing systems must utilize automated machines which manufacture the desired product correctly the first time in order to be cost effective and to produce the product at a competitive cost to other producers. Errors should be corrected either before or during production of the product. Nevertheless, it would still be desirable to be able to eliminate errors as much as possible when manufacturing a product, whether using a mass-production system with large batch sizes or a small-batch and custom part manufacturing system.

Typically, a majority of production errors in automated mass-production manufacturing systems occur because the manufacturing system is not able to adequately compensate for variations in the manufacturing process. One such variation, which will be discussed in connection with the example of an automated mass-production manufacturing system described herein, is the thickness of the sheet metal used in connection with the fabrication of sheet metal products. Since the manufacturing process variations are difficult to model before the actual manufacturing system is operational, sensors are used to detect and compensate for such manufacturing process variations in real time.

The fingerpad force sensor of the present invention can be used, in connection with, for example, an automated metal-

bending work station that efficiently manufactures small-batch sheet metal parts described by computer aided design systems. The automated work station may include a process planner that selects the necessary punches, dies, grippers and sensors, determines the fabrication sequence and then generates the appropriate data for the software which operates the bending machine. After the process plan is formulated, a work station-based system provides real-time sensor-based control of the bending machine during the manufacturing process, while also recording the process history for later review by operators.

Using such an automated metal-bending machine without the fingerpad force sensor of the present invention creates several drawbacks. For example, since the original bending machine is programmed through teach-playback methods, a considerable amount of time is required in order to fine tune and adjust the bending machine to produce the desired part. In addition, even after the system has been fine-tuned, failures still occur during the manufacturing of parts. Such failures include, for example, collisions with the punch tools and poor bends due to part misalignment. Generally, such failures occur because the bending machine does not have the intelligence to accurately know the position and orientation of the workpiece.

There are many reasons for the part position uncertainty in prior art systems. They include the mechanical slop present in the loading mechanism for the bending machine, the loss of part position information when the robot gripper releases the workpiece during bending operations, slippage of the workpiece in the robot gripper during handling and flexing of the workpiece during handling. The present invention addresses such workpiece position uncertainty by augmenting the sheet metal bending machine system with fingerpad force sensors.

The fingerpad force sensor system of the present invention overcomes the above-described shortcomings of the art by detecting process variations which occur in, for example, the automated sheet metal bending manufacturing system described above. Several of those fingerpad force sensors are embedded in the gripping pads of the robot which forms part of the automated sheet metal bending manufacturing system. When external forces are applied to the sheet metal workpiece being held by the robot gripper, the deformation of the rubber pads produces a change in the outputs of the sensors. The sensors are designed as an integral part of the robot's gripper and therefore travel with the workpiece. The instant design thus allows the manufacturing system to monitor the "status" of the workpiece at any time during all phases of automated bending: material acquisition, material handling, machine loading and unloading. In each of these areas, there are problems of dynamic forces between the sheet metal and the gripper that must be actively sensed and controlled. In that manner, the sensors used with the present invention enable the manufacturing system to align the workpiece at the loading station and the press brake, to detect unplanned collisions between the workpiece and the manufacturing system and to also detect imminent workpiece slippage. Such imminent workpiece slippage in the robot gripper occurs when the robot accelerates large parts too quickly.

SUMMARY AND OBJECTS OF THE INVENTION

In view of the foregoing, it should be apparent that there still exists a need in the art for a method of and apparatus for a force sensor system which can readily be used in both large and small batch automated manufacturing systems to detect

critical process variations which occur in such systems in order to correct deviations in, for example, the workpiece manipulation process based upon the data provided by the sensing system. It is, therefore, a primary object of this invention to provide a method of and apparatus for providing a force sensor system which detects process variations in automated manufacturing systems and which has particular application for automated sheet metal bending machine systems.

More particularly, it is an object of this invention to provide a fingerpad force sensor system which forms a part of the gripping pads of a robot and which detect variations in the forces acting on a workpiece during, for example, a metal-bending manufacturing process.

Still more particularly, it is an object of this invention to provide a fingerpad force sensor system for manipulating a workpiece which utilizes simple and reliable electronic circuitry which does not require frequent alignment nor costly components.

Another object of the present invention is to provide a reliable and relatively inexpensive process variation detector mechanism for use in detecting and overcoming various manufacturing process variations which occur in a metal-bending manufacturing process.

A still further object of the present invention is to provide a system for monitoring the forces acting on a sheet metal workpiece during a metal-bending manufacturing process so as to correct for various manufacturing process variations such as workpiece misalignment during the manufacturing process, workpiece collisions with various components of the manufacturing system and workpiece slippage in the robot gripper.

Briefly described, these and other objects of the invention are accomplished by providing a set of sensors which are secured to the gripper of a robot for providing force and impact information for the workpiece held by the gripper. Each of the sensors is formed from a deformable rubber pad which includes an LED aligned opposite a position-sensitive detector such that, when the rubber pad and LED combination is deformed by a shear force, the output of the position-sensitive detector changes, thus providing an output current which is proportional to the effect of the force applied to the workpiece.

The currents output by each of the position-sensitive detectors are separately converted to a voltage and the difference between the voltage calculated. That difference voltage signal is then applied to both a computer controlled offset nulling circuit and a DC filtering circuit to produce a DC signal representative of the amount of force experienced by the sensor and an AC signal representative of the impact of that force experienced by the sensor.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a diagram illustrating the various components which are typically utilized with an automated sheet metal bending machine;

FIG. 2 is a diagram showing a cross-section of the fingerpad force sensor of the present invention;

FIG. 3 is an enlarged view of a portion of the fingerpad force sensor of FIG. 2;

FIG. 4 is a cross-section of the fingerpad force sensor of the present invention under a shear load;

FIG. 5 is an enlarged view of a portion of the fingerpad force sensor of FIG. 4 under the same shear load;

FIG. 6 is a diagram illustrating a top view of the front-end of a robot gripper utilizing a fingerpad force sensor with one dimensional sensors;

FIG. 7 is a diagram illustrating a top view of the front-end of a robot gripper utilizing a fingerpad force sensor with two dimensional sensors;

FIGS. 8A-8B are schematic block diagrams of the signal conditioning electronics which may be used with the fingerpad force sensor of the present invention;

FIGS. 9A-9D are electrical schematic diagrams of circuitry suitable for use as the signal conditioning electronics shown in FIG. 8;

FIG. 10 is a block diagram illustrating the integration of the fingerpad force sensor of the present invention with an automated metal-bending machine;

FIG. 11 is a diagram showing the hierarchical support software for the fingerpad force sensor of the present invention;

FIG. 12 is a diagram illustrating a preferred embodiment of a pad for the fingerpad force sensor of the present invention shown upside down;

FIGS. 13A-13E illustrate, in accordance with an aspect of the invention, a five-step alignment procedure for aligning the corner of a workpiece with the corner of a bracket;

FIGS. 14A-14E illustrate loading procedures and the steps for aligning a workpiece with the backstops of a press brake, according to another aspect of the invention;

FIG. 15 illustrates an exemplary unplanned collision between a workpiece and an obstacle; and

FIG. 16 illustrates an exemplary position-based proportional force control scheme, in accordance with an aspect of the invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring now in detail to the drawings wherein like parts are designated by like reference numerals throughout, there is illustrated in FIG. 1 an automated sheet metal bending machine system 10 in which a material loader/unloader 100 is used to pick up a workpiece 102. The workpiece 102 is then taken from the material loader/unloader 100 by a five degree of freedom robot 104. More specifically, the gripper 106 of the robot, to which the fingerpad force sensor system of the present invention is secured, as will be discussed later herein, is used to grip the workpiece 102 and move it into position along the die rail 108 and against the backstops 110 of the press brake 112. Once properly positioned, the punch tools 114 are used to process the workpiece 102. In the event that the robot 104 needs to adjust its grip on the workpiece, the repositioning gripper 116 may be utilized.

As has been discussed previously in detail, various manufacturing process variations occur when utilizing the automated sheet metal bending manufacturing system 10 and other such similar types of manufacturing systems. For example, the workpiece 102 may be misaligned when acquired by the robot 104 at the material loading and unloading station 100 or when the robot 104 places the workpiece 102 into the press brake 112 for bending. Also, collisions occasionally occur between the workpiece 102 and the press 112, the robot 104 or other obstacles. An additional common manufacturing process variation is the slippage between the workpiece 102 and the gripper 106 of the robot 104, which can occur when the robot 104 accelerates too quickly while gripping a large workpiece 102.

Therefore, the fingerpad force sensor of the present invention as shown, for example, in FIGS. 2 and 3, has been developed in order to provide real time compensation for those manufacturing process variations. In particular, the

fingerpad force sensor system of the present invention will assist the robot **104** in properly aligning the workpiece **102**, detecting and/or recovering from a collision between the workpiece and various components of the automated sheet metal bending system **10** and to prevent slippage of the workpiece **102** while in the gripper **106** of the robot **104**.

The foregoing goals can be achieved by integrating the fingerpad force sensing system hardware and software with that of the automated sheet metal bending machine **10**. The hardware of the fingerpad force sensor system, that is, the fingerpad force sensors **210** and the associated signal condition circuit board **1000**, interface with the computer **1006** of the sheet metal bending machine by means of an analog-to-digital converter board **1002** and a digital output board **1004**. The digital output board **1004** allows the bending machine's computer **1006** to control the offset nulling functionality of the force sensor's signal conditioning circuit board **1000**. The integration of the fingerpad force sensor system of the present invention with an automated metal bending machine is shown in FIG. **10**.

The fingerpad force sensor's software includes routines that permit the bending machine's computer **1006** to read the sensor output values, to convert the sensor output voltage values to equivalent force units, to control the offset nulling module of the signal conditioning circuit board **1000**, and to perform sensor-based control strategies. As illustrated in FIG. **11**, the sensor software consists of a three-level hierarchy. At the lowest level is the first-level device drive software **1104** for the analog-to-digital board **1002** and the digitable output board **1004**. The first-level device drivers define the commands that allow the bending machine's computer **1006** to communicate with the analog-to-digital board **1002** and the digital output board **1004**. The next level **1102**, called the second-level device driver software, contains the device driver for the fingerpad sensor system. The sensor system's second-level device driver embodies the routines that allow the bending machine's computer **1006** to communicate with the signal conditioning circuit board **1000** of the fingerpad force sensor, including routines to read and convert the sensor outputs and to activate the offset nulling module of the signal conditioning board **1000**. The second-level device driver builds upon the commands defined by the first-level device driver. The third level of software **1100** contains the real time application routines that are embedded in the bending machine's overall application software (e.g., the execution sequencer).

The fingerpad force sensor's application routines include sensor-based control strategies for force sensing, as well as data acquisition routines. As shown in FIG. **11**, the application program uses the software routines defined in the second-level device drivers as building blocks for the more elaborate application routines. This is a common software paradigm which is described, for example, in *CHIMERA II Real Time Programming Environment: Program Documentation*, by David B. Stewart, Donald E. Schmitz, and Pradeep K. Khosla, released in 1991 by Carnegie Mellon University, at pages 154-167.

During the manufacturing process, it is possible that a bent workpiece **102** may collide with the punch tool **114** when the robot **104** tries to remove it from the press brake **112**. That collision causes a large and abrupt change in the sensor signals, which can be used to initiate a sensor-based control routine to help the bending machine recover from the collision. The sensor routine can also be used to interrupt the robot program such that the robot **104** moves away from the punch tool **114**. That prevents damage to the workpiece **102**, the robot **104**, the punch tool **114** and the sensors **210**. The

sensor routine may then notify the process planner of the error and can then be used to adjust the path of the robot **104** by utilizing the sensor's information concerning the impact force direction in order to recover from a collision between the punch tool **114** and a bent workpiece **102**. Also, the robot **104** can be instructed to move along the newly adjusted path using feedback obtained from the sensors **210** in order to "feel" its way out of the press brake **112**. Thus, the fingerpad force sensor system of the present invention uses both the detection of the error during the manufacturing process and a sensor-based control scheme for compensating for a sensed error in order to prevent such an error from recurring.

The fingerpad force sensor of the present invention, as discussed above, is mounted to the gripper **106** of the robot **104**. In that manner, one set of sensors can be utilized for numerous force sensing applications. The gripper **106** of the robot **104** is an ideal place of the mounting of the force sensors since forces are transferred from the workpiece **102** to the gripper **106** when the workpiece **102** interacts with its environment. Also, the set of the force sensors **210** travels with the workpiece **102** and is always present to measure the forces which affect the workpiece **102**, and especially those which occur during the procedure of loading the workpiece **102** into the press brake **112** for bending.

Each of the force sensors **210** is formed as integral component of the robot's parallel-jaw gripper **106** and forms, in effect, a fingerpad for the robot **104**. As shown in FIGS. **2** and **3**, the fingerpad force sensor of the present invention is fabricated by mounting one or more position-sensitive detectors **206** (only a single position-sensitive detector is shown for purposes of clarity) in an aluminum mounting plate **202**. The aluminum mounting plate **202** is then secured to the bottom half **106b** of the gripper **106** of the robot **104** using the existing screw holes (not shown) of the gripper **106**.

A rubber pad **200** having a recess **212** cut in it is mounted to a thin sheet metal base plate **304** by, for example, an adhesive. The base plate **304** has a hole cut in it to allow the light from the LED **300** to reach the position-sensitive device **206**. The rubber pad **200** and its base **304** are secured to the top surface of the aluminum mounting plate **202** with screws **306**. In addition, another rubber pad **208** may be likewise mounted to the aluminum plate to make the gripping surface even. In a similar manner, a number of other rubber pads **208** may be mounted with an adhesive to the sheet metal base plates **204** which are in turn fastened to the gripper top **106a** by any suitable means, such as with screws (not shown). The light from the LED **300** of the rubber pad **200** can be centered on the position-sensitive detector **206** by moving the rubber pad **200** and its base plate **304** within the confines of enlarged screw through holes by which the rubber pad base-plate is attached to the aluminum plate **202**. Alternatively, the aluminum mounting plate **202** can be designed in such a way that small set screws can be inserted into its sides to push the position-sensitive device **206** into a centered position relative to the sensor pad LED **300**. The aluminum mounting plates **202** are mounted to the bottom gripper **106b** by suitable devices, such as the screw **308** shown in FIG. **3**.

Using the foregoing construction, access to the sensors **210** is readily obtained, since the mounting plate **202** can be quickly removed from the gripper bottom **106b**. Therefore, the gripper **106** of the robot **104** need not be removed from service for long periods of time in order to repair the sensors **210**.

FIG. **3** shows an enlarged portion of FIG. **2** which includes the rubber pad **200** having a recess **212** formed

therein, as well as the position-sensitive detector **206** mounted on its aluminum plate **202**. The force sensor **210** is formed from, for example, a one-dimensional position sensitive detector having a sensitive area of preferably 1 mm×3.5 mm. Preferably, a two-dimensional position-sensitive detector is utilized. The one-dimensional position-sensitive detector may be Part No. S3274-01 available from Hamamatsu Photonics KK of Japan. The two-dimensional position-sensitive detector may be Part No. S4744, also available from the same company.

The infrared light emitting diode (LED) **300** which is embedded in the rubber pad **200** in that portion of the rubber pad **200** which bridges the recess **212** may preferably be a miniature 2 mm wide LED Part No. LD261-5 for use with the one-dimensional sensor and a miniature 1 mm wide LED, Part No. SFH405-3, for use in the two-dimensional sensor. Both of those components are available from Siemens Components, Inc. of Cupertino, Calif.

The sensor **210** is designed such that when an external force acts on a workpiece **102** held by the gripper **106**, the rubber pad deforms, thus causing LED **300** to shift along the sensitive area of the position-sensitive detector **206**. The position-sensitive detector **206** detects the shifting the light source, as shown in FIGS. **4** and **5**, and the electrical output from the position-sensitive detector **206** is affected. FIG. **4** is a diagram of a cross-section of the instant force sensor **210** under a shear load F which is applied to the left-hand side of the workpiece **102** which is gripped by the rubber pads **208** and **200**. For purposes of simplicity, not all of the remaining components shown in FIG. **2** are shown in FIG. **4**.

FIG. **5** is an enlargement **500** of a portion of FIG. **4**, including the rubber pad **200** which carries the LED **300**, showing the skewed relationship between the LED **300** and the position-sensitive detector **206** when the shear load F is applied to workpiece **102** as shown in FIG. **4**. The changes in the output from the position-sensitive detector **206** can then be utilized to determine the amount of force experienced by the workpiece **102** and its direction of application. It is preferred that the sensors **210** have a measurement resolution of at least 1 pound and a range of at least 10 pounds in each sensing direction.

A typical rubber pad **200** may preferably measure $\frac{1}{2}$ in.×1 in.× $\frac{3}{8}$ in. in size for the 1-D sensors (and $1 \times 1 \times \frac{3}{8}$ for 2-D sensors) and have a recess **212** cut into it for the LED **300** as well as a channel **302** for the wires connected to the LED **300**. An epoxy adhesive may be utilized to embed the LED **300** into the rubber pad **200**. The process of embedding the LED **300** into the rubber pad **200** involves removing as little rubber material as possible from the pad **200** and utilizing only a small amount of epoxy cement such that the mechanical properties of the rubber pad **200** do not change substantially. Preferably, at least two one-dimensional sensors **210** are utilized on the front end of the gripper **106**.

FIG. **6** shows a diagram of a top view of the front end of the gripper **106**. While the instant invention is described with the sensors **210** being secured to the gripper bottom **106b** and the rubber pads **208** being secured to the gripper top **106a**, it should be understood that the sensors **210** could alternatively be secured to the gripper top **106a** while the rubber pads **208** could be secured to the gripper bottom **106b** or the sensors **210** could be secured to both the top and bottom of the gripper **106**.

FIG. **7** shows a diagram of a top view of the front end of the gripper **106** illustrating the location and orientation of four two-dimensional force sensor **210a**. The four two-

dimensional sensors **210a** are mounted to a mounting plate in a similar manner described in connection with the mounting of the sensors **210** to the mounting plate **202** in FIG. **2**. By using the four two-dimensional sensors **210a** and measuring the differences between the outputs from the top and bottom sets of sensors **210a** it may be possible to distinguish between shear and normal forces being applied to the workpiece **102**. The direction and magnitude of the forces detected by the top and bottom sensors is similar when shear forces are applied in the plane of the sensors **210a**, while the magnitude and direction differs when a normal force is applied to the workpiece **102**. The typical shear forces monitored by the sensors **210** and **210a** assure 1 lb to 10 lbs.

The rubber used to form the pads **200** and **208** may preferably be made from neoprene rubber having a 45 Shore A hardness rating. It has been found that such rubber pads exhibit both hysteresis and a creep characteristic, which effect the response time and recovery time of the sensor. The creep characteristic of the rubber pad **200** also results in a slow settling time for the sensor's output when the gripper **106** of the robot **104** first closes. The slow settling time of the sensor output can be reduced by pre-loading the sensor with a compression force greater than the typical nominal gripping force of 300 psi. Alternatively, a look-up table can be developed which contains the average change in the sensor's output for each different applied load. Such a table would include the changes that occurred during both the loading and unloading of the sensor, that is, changes due to both creep and recovery. Such a look-up table could be utilized with software used in connection with the output signals produced by the instant fingerpad force sensor system.

The hysteresis and creep characteristics of the rubber pad also affect the bandwidth of the sensor. Such undesirable characteristics can be minimized by utilizing a rubber material made with more natural rubber and few reinforcing fillers. For example, a rubber pad can alternatively be made from castable urethane, also having a 45 Shore A hardness rating, by pouring liquid urethane into a mold into which the LED **300**, its associated wires and the pad base-plate **304** have already been fixed in place. The rubber pad is then formed as the urethane cures. That method of manufacturing the sensor **210** minimizes the variability between LED-embedded rubber pads and ensures that the LED is located in the center of the rubber pad and is perpendicular to the position-sensitive detector **206**. Liquid urethane is available from, for example, Conap, Inc., of Olean, N.Y. under the Part No. CONATHANE TU-500.

FIG. **12** shows an alternative and preferred sensor pad design for use with the fingerpad force sensor system of the present invention (shown upside down). This design offers several improvements over the previously described LED-embedded rubber pad. Its improvements include easier fabrication, more accurate placement of the LED **300** in the sensor pad, and better shear displacement under a load. Instead of placing LED **300** in one solid piece of rubber as with the sensor pad **200** of FIG. **2**, this alternative approach uses three layers of material to form the sensor pad **200a**. The three layers are formed from a cork-rubber pad **1200**, a copper surface printed circuit board (PCB) **1202**, and a rubber pad **1204** made of natural gum rubber.

The cork-rubber pad **1200** provides a good gripping surface and absorbs the oils used on the sheet metal parts moved by the robot **104**. The dimensions of the cork-rubber pad are preferably $1 \times 1 \times \frac{1}{16}$ ". The copper surface printed circuit board **1202** holds the LED **300** and connects the LED

300 to power and ground sources through the wires **1206**. A line **1208** is etched away from the copper surface of the PCB **1202** in order to electrically isolate the board into two copper sections (one section for power and other for ground). The LED **300** is then snugly fitted into a hole on the copper side of the printed circuit board **1202**. The leads of the LED **300** are then soldered to the copper board one lead to each side. The wires **1206** are soldered to each copper section to supply the power and ground signals for the operation of the LED **300**. The dimensions of the copper PCB **1202** board are preferably 1"×1"× $\frac{1}{16}$ ".

The third layer consists of a natural gum rubber pad **1204** of 45 Shore A hardness having a hole **1210** cut out of its center to allow the light from the LED **300** to pass through to the position-sensitive detector **206**, **206a** and a second hole **1212** near the corner of the pad **1204** for the wires **1206** to feed through to the copper PCB **1202**. The dimensions of the rubber pad **1204** are preferably 1"×1"× $\frac{1}{8}$ ".

The sensor pad **200a** is formed by placing the three layers **1200–1204** together using a suitable adhesive. More specifically, the cork rubber pad **1200** is attached to the non-copper side of the printed circuit board layer **1202** and the rubber pad **1204** is attached to the copper side of the printed circuit board layer **1202**. The natural gum rubber side of the layered sensor pad **200a** is then attached to a sheet metal base plate **304a** with suitable adhesive. The base plate **304a** has a hole **1218** cut in its center to allow the light from the LED **300** to pass through to position-sensitive detector **206**, **206a**, screw holes **1214** on each end for attaching the base plate **304a** to the sensor's aluminum mounting plate **202**, and a fourth hole **1216** near its corner for the wires **1206** to feed through to copper plate **1202**.

FIG. **8A** shows a schematic diagram of a one-dimensional force sensor signal conditioning circuit which may be used to convert the photo-current output signals of the position-sensitive detectors **206** into voltage signals. The force sensor signal conditioning circuit produces two signals for each sensor, a DC-level signal for measuring forces applied to the sensor and an AC signal for detecting collisions.

Each of the one-dimensional sensitive detectors produces two output currents i_1 and i_2 which are fed respectively to first and second current-to-voltage converters **800a** and **800b**, which convert those currents to voltage values v_1 and v_2 . Those output voltages v_1 and v_2 are fed to a difference amplifier **802** which, by subtracting the voltage v_2 from the voltage v_1 , determines the relative light position of the LED **300** on the photo-sensitive detector sensitive area **206**. The output from the difference amplifier **802** is fed to both an offset nulling module **804** and to a DC filtering module **806**. The offset nulling module **804** is connected to be controlled by the bending machine computer. The offset nulling module **804**, under computer control, functions to remove the large DC component of the difference output (v_1-v_2) which occurs when the gripper **106** closes and compresses the rubber pads **200**. The DC filtering module **806** functions to pass only the transitions in that difference voltage for purposes of collision detection. All of the stages **800–806** also function to amplify the signals which are input to them. Each of the force sensors **210** utilizes a respective force sensor signal conditioning circuit such as that shown in FIG. **8**.

Where two-dimensional sensors **210a**, as shown in FIG. **7** are utilized, then the circuitry shown in FIG. **8A** is modified accordingly. The modifications to the circuit shown in FIG. **8A** are minimal for the two-dimensional (2-D) position-sensitive device (PSD) **206a** since its operational properties

are similar to the one-dimensional (1-D) PSD **206**. For this type of 2-D PSD, the circuitry in FIG. **8A** is duplicated two times (once for each sensing direction) and for each module the amplification gains and capacitor values are adjusted. Such circuitry is shown in FIG. **8B**.

Specific circuitry which can be used with the current-to-voltage converters **800** is shown in FIG. **9A**; circuitry for use as the differential amplifiers **802** is shown in FIG. **9B**; circuitry for use as the DC filtering modules **806** is shown in FIG. **9C**; and circuitry for use as the computer-controlled offset nulling models **804** is shown in FIG. **9D**.

As discussed above, the fingerpad force sensing system of the present invention is useful for correcting workpiece misalignment at the loading station and press brake, for detecting unplanned workpiece collisions and for detecting imminent workpiece slippage. Each of those applications and a suggested sensing strategy is described below and illustrated in Tables 1–3. In each of the descriptions which follow, the gripper **106** of the robot **104** is equipped with four two-dimensional force detectors **210a**, as shown and described in connection with FIG. **7**.

The first application which will be discussed is that of the alignment of the workpiece at the loading station. The loader/unloader **100** picks up an unbent workpiece **102** with its suction cups and feeds sheet workpiece **102** to the robot **104** for bending, in a known manner. Although the workpieces **102** are usually aligned in their bin before the loader/unloader **100** picks them up, positional information may be lost due to mechanical imperfections in the loading mechanism. The workpiece **102** thus passed to the robot **104** will be skewed. If the misalignment of the workpiece is not corrected, then a crooked bend will result and the workpiece **102** will have to be discarded as scrap material.

By correcting the mechanical imperfections in the loader/unloader **100**, workpiece position uncertainty can be corrected. Alternatively, an L-shaped bracket, as shown in Table 1, can be used to align the workpiece **102** at the loading station **100**. By using the force feedback information of the fingerpad force sensor system, the robot **104** can fit a corner of the workpiece **102** into the corner of the alignment bracket, whose position is accurately known by the bending machine **112**. After matching the corners, the degree of misalignment is determined by calculating the difference between the robot's position and orientation before and after aligning the workpiece **102**. A position and orientation offset value is then added to all other robot moves throughout the manufacturing process in order to correct for the initial workpiece misalignment. Correction of the workpiece misalignment at the loading station thus minimizes or eliminates the necessity for realignment of the workpiece **102** at the press brake **112** for each bend.

FIGS. **13A–13E** illustrate a five-step alignment procedure and the forces indicated by the sensors **210a** during the procedure while accomplishing the alignment of a corner of the workpiece **102** with the corner of the alignment bracket. After the robot **104** acquires the workpiece **102** from the loader **100**, it rotates the workpiece **102** in a clockwise direction and then moves the workpiece in the +y direction until contact is made with the bracket (see, e.g., FIG. **13A**). The robot **104** initially rotates the workpiece **102** clockwise to ensure that the lower left corner of the workpiece **102** touches the bracket. The x-direction and y-direction force signals generated by each of the four sensors **210a** indicate that contact has occurred. Specifically, the resultant force signals for each of the four sensors **210a** will be in a clockwise orientation when the lower left corner of the workpiece **102** first contacts the alignment bracket.

It should be noted that in the discussion of this task, it is assumed that the pivot point for the force moment is located in the center of the mounting plate of the force sensors **210a**. That also assumes that the compressive force acting on the four rubber pads which form part of those four sensors **210a** is the same and that the rubber pads all have the same contact surface area. In the event that the gripper **106** used with the fingerpad force sensor system of the present invention has a compressive force which is greater for the rear pad than for the front pads, because of the gripper design, the pivot point would be further back towards the center of the two rear sensors, but the overall results as described herein are the same.

As shown in FIG. **13B**, after contact of the workpiece **102** has been made with the bracket, the robot **104** rotates the workpiece **102** in a counter-clockwise direction around the contact point until the side of the workpiece **102** is in full contact with the left side of the bracket. After such contact has occurred, the sensor readings will indicate one of three possibilities. First, the moment forward of the pivot point is greater than the moment below the pivot point, such that the sensors **210a** read resultant forces in a clockwise direction. Second, the opposing moments about the pivot point are equal, so that all four of the sensors **210a** read a force in the $-y$ direction and possibly a small force in the $+x$ direction. The third possibility is that the moment behind the pivot point is greater than the moment in front of the pivot point, so that the sensors **210a** read a resultant force in the counter-clockwise direction greater than the initial contact forces. By making the initial contact point at the lower left hand corner of the workpiece **102**, the line contact forces with the workpiece and bracket sides can be differentiated, since the force readings generated by the fingerpad force sensing system of the present invention will change direction or will be in the same direction with an increased magnitude.

Once line contact is achieved, the robot **104** then rotates the workpiece **102** clockwise or counter-clockwise, as necessary, in order to cancel the opposing moments acting on the workpiece **102** (see, e.g., FIG. **13C**). This step establishes the orientation of the workpiece **102** and makes it easier to detect contact with the corner of the bracket in the next step. After the moments have been cancelled, the robot **104** moves the workpiece **102** back, while maintaining contact with the side of the bracket, until the workpiece **102** touches the corner of the bracket (see, e.g., FIG. **13D**). Contact between the bracket and the workpiece **102** is indicated by a clockwise resultant force reading generated by the sensors **210a**. This step establishes the position of the workpiece **102**. As previously discussed, an offset value corresponding to the position and orientation of the workpiece **102** is then used throughout the manufacturing process to compensate for the loading process variation.

As shown in FIG. **13E**, the final step in the alignment procedure, is to push the workpiece **102** away from the corner before the robot **104** executes its next move. This step removes any force moments acting on the workpiece and prevents the rubber pads which form part of the sensors **210a** from "springing back" when the robot **104** eventually moves the workpiece **102** away from the alignment bracket.

FIGS. **14A–14C** illustrate the three steps and the resultant sensor force readings which are used to align the workpiece **102** in the press brake **112** such that the robot **104** places the workpiece **102** snugly against the backstops **110** of the press brake **112**. Once the workpiece **102** is properly aligned in the press brake **112**, the workpiece is bent. A straight bend is desired. The steps for aligning the workpiece **102** to the

backstops **110** of the press brake **112** are similar to alignment task described above in connection with the loading station **100**. This task differs, however, because a workpiece **102** can be loaded into the press brake **112** in two ways. The first way to load a workpiece **102** into the press brake **112** is with the gripper **106** perpendicular to the desired bend line. That type of loading is called front loading. The second type of loading is that in which the gripper **106** is parallel to the bend line. That type of loading is termed side loading. The steps for accomplishing the front loading are shown in FIGS. **14A–14C**, while the steps for accomplishing side loading are shown in FIGS. **14D–14E**. Although each loading technique requires a slightly different sensing strategy, the goal is the same, that is, to place the side of the workpiece **102** against the backstops **110** of the press back **112**.

Since the gripper **106** of the robot **104** often holds the workpiece **102** to be bent over a flange, only the front two sensors of the four sensors **210a** shown in FIG. **7** can effectively be used to align the workpiece **102** against the backstops **110** since the workpiece **102** does not extend over the two rear most sensors. Therefore, the following description of the steps of aligning the workpiece **102** in the press brake **112** against the backstops **110** will be described utilizing only the information available from the front two sensors **210a** mounted on the gripper **106**.

Since the sensing strategy and force sensor readings for alignment of the workpiece **102** at the press brake **112** are similar to those at the loader/unloader **100**, such readings will not be discussed in detail again.

The front loading alignment procedure has three steps, which are illustrated in FIGS. **14A–14C**. First, the robot **104** moves the workpiece **102** forward into the press brake **112** until the workpiece touches the backstops **110**. If the workpiece is misaligned, it will either touch the right corner of the right backstop, thus producing a clockwise moment, or the left corner of the left backstop, thus producing a counter-clockwise moment. By analyzing the pattern of forces read by the sensors **210a**, the point of contact can be determined, since the position of the backstops **110** is known. The robot **104** then rotates the workpiece **102** about the point of contact until it touches both backstops **110**. Finally, the robot **104** adjust the position of the workpiece **102** until the opposing moments acting on workpiece **102** are within the desired tolerance. The workpiece **102** is thus aligned and the press brake **112** can then proceed to bend the workpiece.

The two steps for accomplishing the side loading of the workpiece **102** into the press brake **112** as shown in FIGS. **14D–14E**. First, the robot **104** rotates the workpiece **102** towards the press brake **112** in order to ensure that the workpiece strikes the backstop **110** farthest from the gripper **106**. The robot **104** then moves the workpiece **102** into the press brake **112** until the workpiece **102** touches the corner of the farthest of the two backstops **110**. Finally, the robot **104** rotates the workpiece **102** about the point of contact until the workpiece **102** touches the second backstop **110**. The robot **104** only manipulates the workpiece **102** until it touches both backstops **110**. The robot **104** does not attempt to balance the opposing moments applied to the workpiece **102**. Since contact of the workpiece **102** with both backstops **110** is indicated only by an increase in the measured force since there is no change in the force direction, supplementary contact sensors may also be utilized on each backstop **110**.

As discussed above, the fingerpad force sensing system of the present invention can also be utilized to detect impacts. That is desirable since such detection can prevent damage to

the robot **104**, the punch and die tools **108**, **114** and the workpiece **102**. In addition, the detection of an unplanned collision indicates that there is an error in the process planner software of an unanticipated process variation. Such errors, after being detected, can then be corrected before beginning the manufacturing process again with a new workpiece. It is therefore desirable to detect unplanned collisions with the workpiece **102** and, if possible, recover from those collisions by backing away from the impact.

FIG. **15** shows an example of an unplanned collision between the workpiece or part **102** and an obstacle. In order to detect such an unplanned collision, the information generated by the sensors **210a** in response to impact forces utilized. First, a threshold force value is set that is well above the noise level of the sensors **210a** and the nominal sensor readings produced by mechanical vibrations in the manufacturing system. If a force greater than the threshold is registered by the sensors **210a** during moves in free-space, then an impact has occurred. When an impact or collision occurs, the sensor-based plan overrides the current robot **104** motion plan and, using the impact direction information obtained from the sensors **210a**, moves the robot **104** away from the obstruction. Then, depending upon the robot motion in progress at the time of the collision, the sensors **210a** may or may not be used to finish the desired robot move.

As shown in FIG. **15**, the right corner of the workpiece **102** has incurred an unplanned collision with an unknown obstacle in what would normally be a "safe" or open space region with no known obstacles. The robot motion planner can then use the information generated by the sensors **210a** to move the workpiece **102** over further to the left and then to try the front loading procedure again. Alternatively, if the workpiece **102** collides with the punch tools **114** while the robot **104** tries to extract it from the press brake **112**, then the signals produced by the sensors **210a** can be used to help the robot **104** "feel" its way out of the press brake **112**.

Alternatively, another approach can be used to avoid severe damage to the robot **104** and then press brake **112** as shown and described in connection with FIGS. **8A** and **8B**, two types of signals are produced by each force sensor's signal conditioning circuit; namely a DC-level output for measuring forces and an AC signal that passes only the transitions in the force readings. That AC output can be used for impact detection by setting a threshold force value for a severe collision. When the AC signal generated by the sensors **210a** reaches preset thresholds, it can be used to trigger a system interrupt to stop the robot **104**. Thus, the AC signal can be used as a safeguard that generates a hardware interrupt to shut down the robot **104** and the bending machine **112** upon the detection of a severe collision.

The fourth detection application discussed above is that of detecting the workpiece **102** slipping within the gripper **106** of the robot **104** while the robot is rotating quickly. Such slippage occurs when the force acting on the workpiece **102** exceeds the frictional force between the rubber pads of the fingerpad force sensing system and the workpiece **102**. If a workpiece **102** slips in the gripper **106**, then information regarding the position of the workpiece **102** and its orientation is lost. The fingerpad force sensing system of the present invention can be used to prevent workpiece slippage by warning the robot system of an impending slippage condition. This warning mechanism can be used to control the speed or acceleration of the robot **104**. For example, in order to operate efficiently, the robot **104** may be instructed to move workpiece **102** as fast as it can until the sensors **210a** generate a signal which is used to instruct the robot to decrease its speed since the workpiece **102** may be about to slip.

The mechanism for detecting imminent workpiece slippage is similar to that discussed in connection with the detection of an impact. A force threshold that is below the nominal frictional force between the rubber pads and the sheet metal workpiece **102** may be used. When the sensors **210a** register a force at or above that threshold, the workpiece **102** is about to slip and the robot **104** is warned/instructed to slow down.

The information generated by the fingerpad force sensor system of the present invention may be used in an open-loop system within the position-based control system of the robot **104**. For example, during the alignment tasks as discussed above, the robot **104** is moved a small increment and then the values of the sensors **210a** are read. Based on the signals generated by the sensors **210a**, the next move of the robot **104** is determined. Alternatively, the information generated by the sensors **210a** can be tied into the control loop of the robot **104** in order to improve the effectiveness of the sensors **210a** and the response of the robot **104** to contact forces. For that purpose, a force-based control loop can be placed around the position controller of the robot **104**. That can be accomplished by relating the desired incremental force with the desired incremental robot position through a proportionality constant. Such a scheme is termed a position-based proportional force control scheme, an example of which is shown in FIG. **16**. This system operates as follows. When the motion of the robot **104** is constrained, for example, and the robot has pushed the workpiece **102** up against the backstops **110** of the press back **112**, the robot controller can switch over to the force control scheme to assist the robot **104** in adjusting its movements until the desired force reading is reached. Such a method is desirable because it provides a natural way of implementing the application tasks, minimizes the possibility of missing an important event, such as an impact, and also eliminates the possibility of applying excessive forces to the workpiece **102**.

It is also desirable to have the flexibility of simultaneously using a force controller in directions of constrained motion, that is, directions in which there is contact of the workpiece with a fixed structure, such as the backstops **110**, and a position controller in directions of free motion, that is, directions in which there is no physical contact between the workpiece **102** and any other structure except the gripper **106**. Such a scheme is called a hybrid position-force controller and is illustrated and described in *Introduction to Robotics: Mechanics and Control* by J. J. Craig, 2nd edition, published by Addison-Wesley of Reading, Massachusetts in 1989. However, as described in an article entitled "Problems and Research Issues Associated with Hybrid Control of Force and Displacement", *Proceedings of the IEEE International Conference on Robotics and Automation*, by R. P. Paul, Published in 1987, at pages 1966-1971, when using either control mode the force and position should be monitored for unexpected changes. Such changes could indicate a problem in the robot procedure.

Although only a preferred embodiment is specifically illustrated and described herein, it will be appreciated that many modifications and variations of the present invention are possible in light of the above teachings and within the purview of the appended claims without departing and intended scope of the invention.

What is claimed:

1. A fingerpad force sensor system for detecting shear forces applied to a workpiece, said system comprising:
 - a robot having a gripper for holding said workpiece;
 - at least one fingerpad force sensor affixed to said gripper such that it is positioned between said gripper and said

15

workpiece in order to experience a shear force experienced by said workpiece, each said at least one fingerpad force sensor including a two-dimensional position-sensitive detector, comprising a piece of deformable planar material and a light emitting source that is

attached to said piece of deformable planar material, said light emitting source emitting a light that is detected by the position-sensitive detector when said shear force is experienced by said workpiece; and

each said at least one fingerpad force sensor being constructed such that it produces at least two output signals representative of the magnitude and direction of said shear force.

2. The fingerpad force sensor system of claim 1, wherein four of said fingerpad force sensors are affixed on one side of said gripper, each approximately equidistant from a central point on said one side of said gripper.

3. A fingerpad force sensor system for detecting shear forces applied to a workpiece, said system comprising:

a robot having a gripper for holding said workpiece; at least one fingerpad force sensor affixed to said gripper such that it is positioned between said gripper and said workpiece in order to experience a shear force experienced by said workpiece; and

each said at least one fingerpad force sensor being constructed such that it produces at least two output signals representative of the magnitude and direction of said shear force,

wherein each said at least one fingerpad force sensor comprises a piece of deformable planar material having a recess formed therein, a light source affixed in said recess in such a manner that light is emitted primarily in a direction towards an opening of said recess, and a position-sensitive detector positioned to receive said light emitted by said light source.

4. The fingerpad force sensor system of claim 3, further including a base plate in which said position-sensitive detector is recessed and to which said piece of deformable planar material is affixed.

5. The fingerpad force sensor system of claim 4, wherein said piece of deformable planar material is affixed over said position-sensitive detector such that said at least two output signals of said position-sensitive detector vary when said shear force is applied to said piece of deformable planar material.

6. A method for sensing the application of a shear force to a workpiece held by a gripper of a robot, said robot having at least one fingerpad sensor affixed to said gripper such that said fingerpad force sensor is positioned between said gripper and said workpiece in order to experience a shear force experienced by said workpiece, said method comprising:

exerting a shear force on said workpiece held by said gripper; and

sensing deformation of said fingerpad force sensor in response to said shear force experienced by said workpiece by providing a deformable planar material carrying a light emitting source which is positioned to emit light to be received by a fixed position-sensitive detector which generates at least one output signal representative of a location on a surface of said fixed position-sensitive detector receiving said emitted light.

7. A force sensor for measuring shear forces applied to a sheet of planar material, said force sensor comprising:

a piece of deformable planar material;

a recess formed in said piece of deformable planar material;

16

a light source mounted in said recess of said piece of deformable material; and

a position-sensitive detector mounted adjacent to said recess such that light emitted by said light source impinges on said photo-sensitive detector,

whereby shear forces applied to said sheet of planar material cause deformation of said piece of deformable planar material, thus moving an impingement location of light on said position-sensitive detector.

8. The force sensor of claim 7, wherein said light source is an infrared light emitting diode.

9. The force sensor of claim 7, wherein said piece of deformable planar material is formed from a material having a hardness of Shore A 45.

10. The force sensor of claim 7, further including a base plate in which said position-sensitive detector is recessed and to which said piece of deformable planar material is affixed.

11. The force sensor of claim 10, wherein said piece of deformable planar material is affixed over said position-sensitive detector such that an output signal of said position-sensitive detector varies when said shear force is applied to said piece of deformable planar material.

12. The force sensor of claim 11, further including processing circuitry connected to receive said output signals from said position-sensitive detector and to generate signals representative of the magnitude and direction of force and the occurrence of an impact experienced by said force sensor.

13. The force sensor of claim 12, wherein said processing circuitry comprises:

a plurality of current-to-voltage converters for converting said output signals from said force sensor to output voltages;

a difference amplifier for receiving said output voltages and producing a difference signal therefrom;

a computer controlled offset null circuit for receiving said difference signal and for producing a DC signal representative of said shear force experienced by said force sensor; and

a filtering circuit for receiving said difference signal and for filtering out a DC component such that an AC signal representative of an impact experienced by said force sensor is produced.

14. The force sensor of claim 7, wherein said force sensor includes two-dimensional position-sensitive detectors.

15. A fingerpad force sensor system for detecting shear forces applied to a workpiece, said system comprising:

a robot having a gripper for holding said workpiece; at least one fingerpad force sensor affixed to said gripper such that it is positioned between said gripper and said workpiece in order to experience a shear force experienced by said workpiece, each said at least one fingerpad force sensor including a two-dimensional position-sensitive detector and a light emitting source that emits a light that is detected by the position-sensitive detector when said shear force is experienced by said workpiece; and

each said at least one fingerpad force sensor being constructed such that it produces at least two output signals representative of the magnitude and direction of said shear force,

wherein each of said at least one fingerpad force sensor further comprises:

a first piece of planar material having a first surface for contacting said workpiece and a second surface;

17

a second piece of planar material having a first portion of dielectric material and a second portion of electrically conductive material, said second piece of planar material being affixed to said second surface of said first piece of planar material by affixing said first portion of dielectric material to said first surface of said first piece of planar material, said light emitting source being affixed to said electrically conductive first portion of said second piece of planar material; and

a third piece of deformable planar material having an opening therein for allowing light emitted by said light emitting source to pass therethrough and to be detected by said position-sensitive detector, said third piece of deformable planar material being affixed to said first portion of said second piece of planar material.

16. The force sensor of claim 15, wherein said light emitting source is an infrared light emitting diode.

17. A fingerpad force sensor system for detecting shear forces applied to a workpiece, said system comprising:

a robot having a gripper for holding said workpiece;

at least one fingerpad force sensor affixed to said gripper such that it is positioned between said gripper and said workpiece in order to experience a shear force experienced by said workpiece, each said at least one fingerpad force sensor including a two-dimensional position-

18

sensitive detector and a light emitting source that emits a light that is detected by the position-sensitive detector when said shear force is experienced by said workpiece, and each said at least one fingerpad force sensor being constructed such that it produces at least two output signals representative of the magnitude and direction of said shear force;

processing circuitry connected to receive said at least two output signals from said fingerpad force sensor and to generate signals representative of the magnitude and direction of force and the occurrence of an impact experienced by said fingerpad force sensor; and

said processing circuitry comprising a plurality of current-to-voltage converters that convert said at least two output signals from said fingerpad force sensor to output voltages, a difference amplifier that receives said output voltages and produces a difference signal therefrom, a computer controlled offset null circuit that receives said difference signal and produces a DC signal representative of the magnitude and direction of said shear force experienced by said fingerpad force sensor, and a filtering circuit that receives said difference signal and filters out a DC component such that an AC signal representative of an impact experienced by said fingerpad force sensor is produced.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 5,844,146
DATED : December 1, 1998
INVENTOR(S) : Anne M. MURRAY et al.

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

At column 17, line 9 (claim 15, line 9) of the printed patent, "first" should be ~~—second—~~.

At column 17, line 16 (claim 15, line 16) of the printed patent, "first" should be ~~—second—~~.

Signed and Sealed this
Fifth Day of September, 2000

Attest:



Q. TODD DICKINSON

Attesting Officer

Director of Patents and Trademarks