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[54]	POWER-ON DETECTION CIRCUIT	
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[52]		
[58]		
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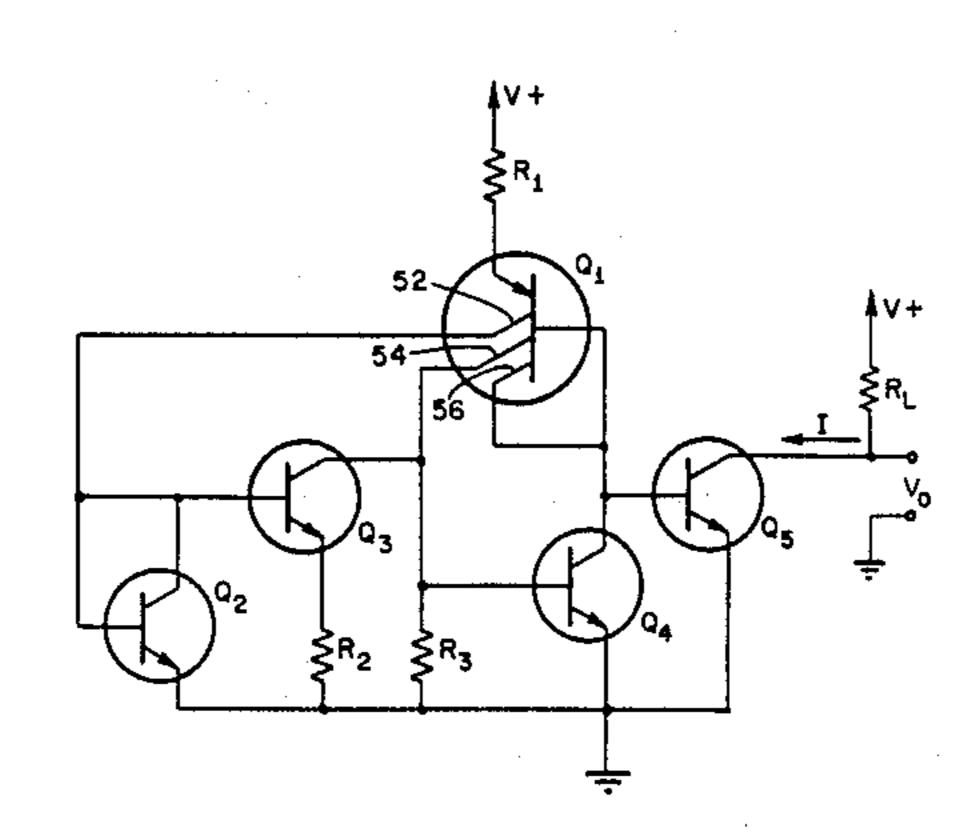
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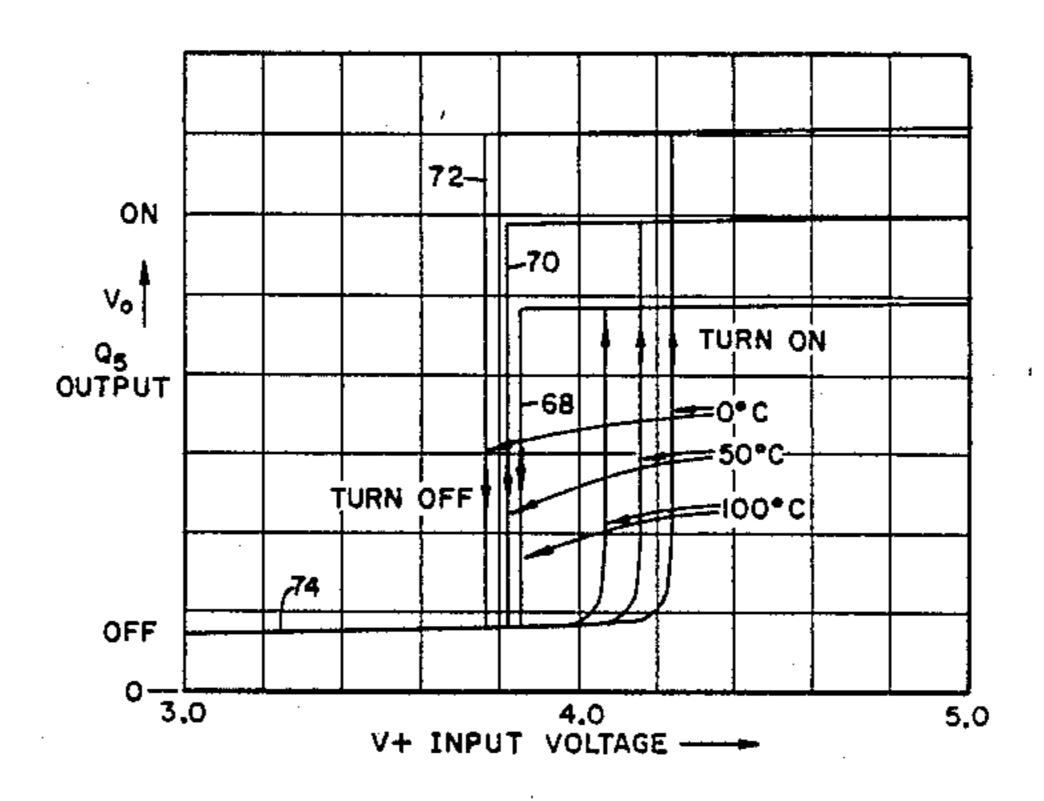
Primary Examiner—Stanley D. Miller Assistant Examiner—David R. Bertelson Attorney, Agent, or Firm—Weingarten, Schurgin, Gagnebin & Hayes

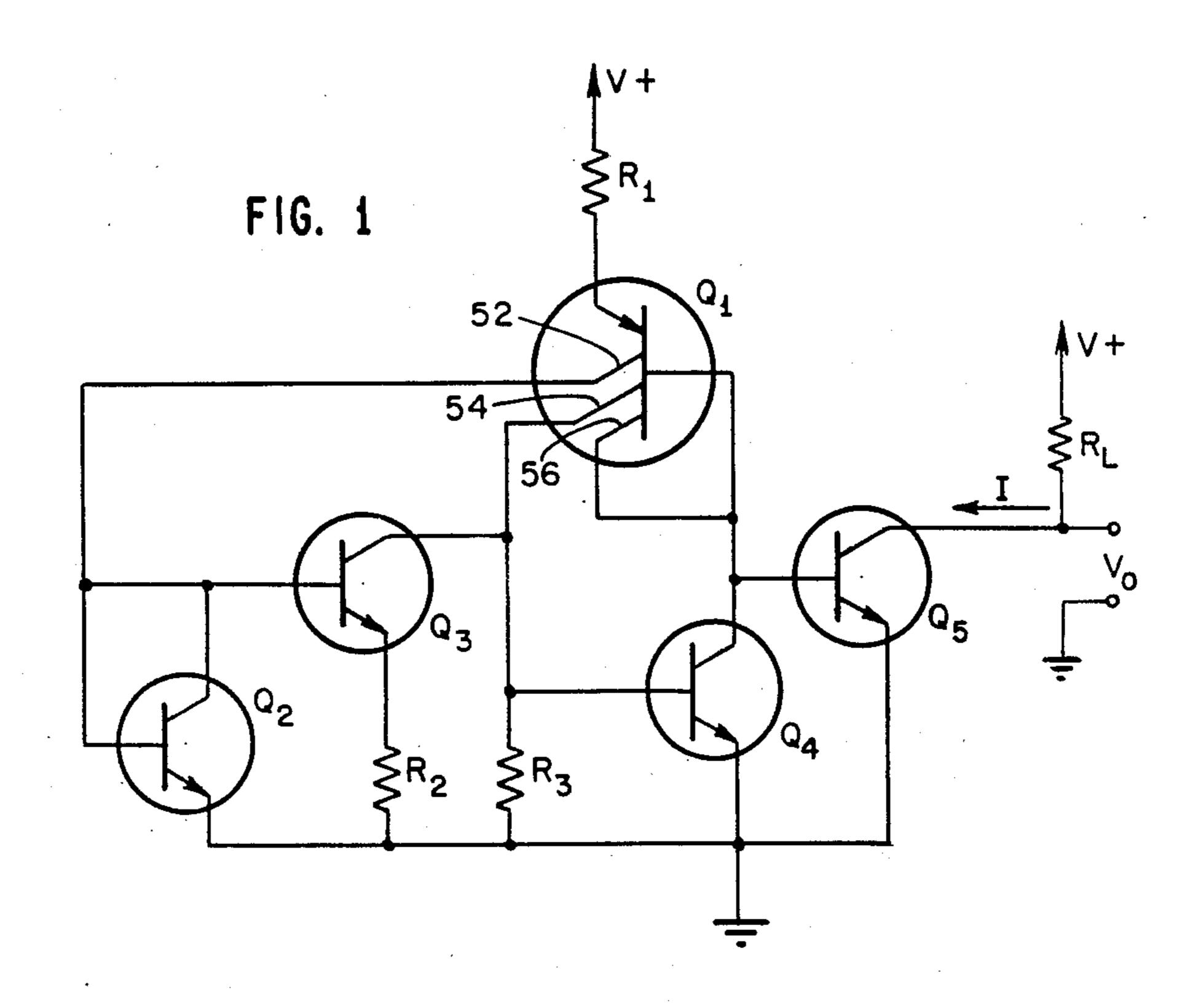
[57] ABSTRACT

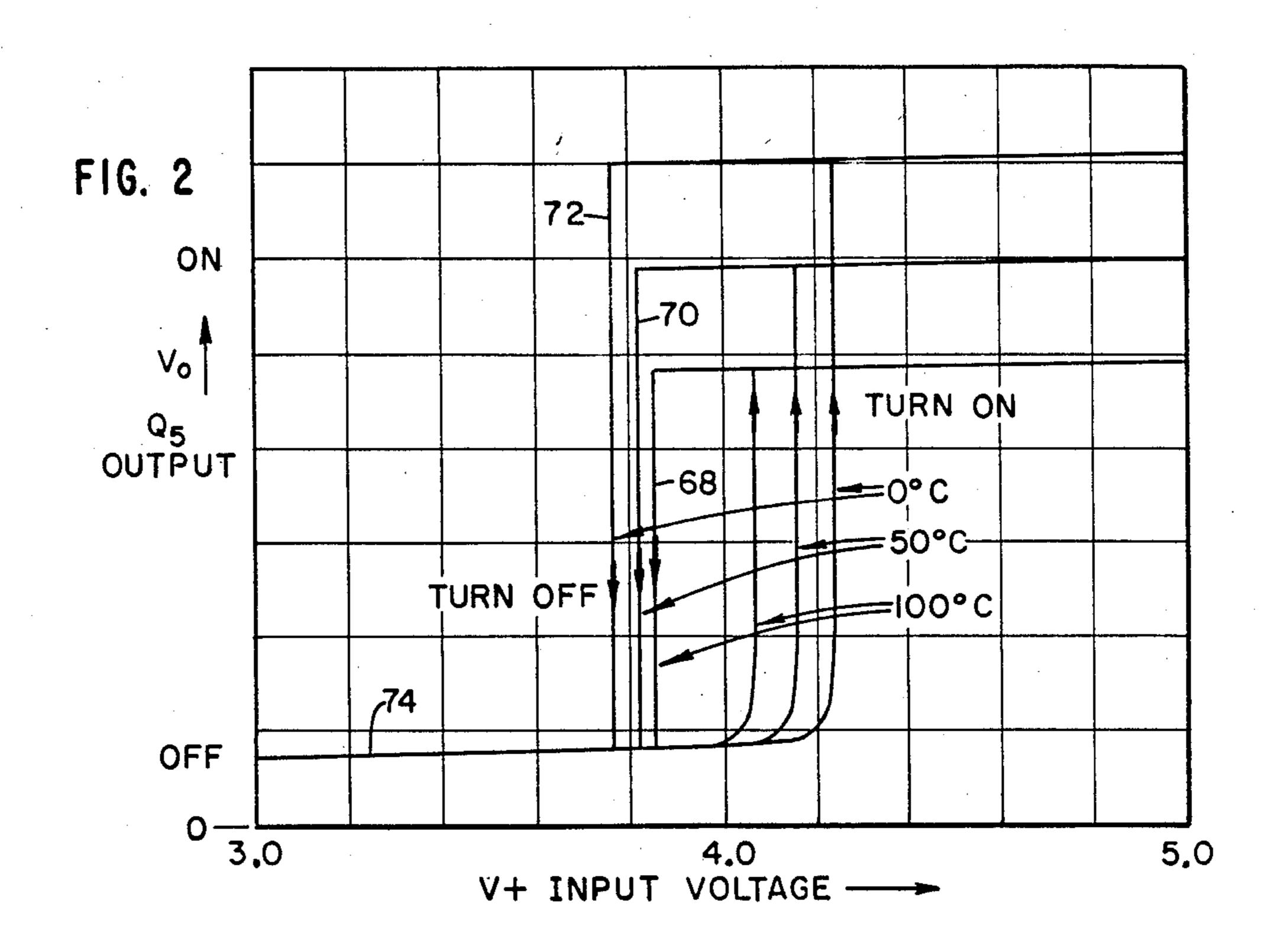
A threshold comparator having hysteresis wherein the repeatable threshold levels are established by multiple current paths and resistance ratios, which provides an under-voltage lock-out signal. The current paths are established by transistors fabricated on a common substrate and include a split collector P-N-P transistor that provides the distribution of the input signal to the various current paths. The turn-on and turn-off threshold points of the circuit according to the present invention are established by resistance ratios which are more easily maintained than are absolute resistance values. Similarly, when implemented on a common substrate, the remaining component values may be selected so that the thresholds values are nearly independent of temperature, providing an easily manufactured, high yield circuit.

9 Claims, 1 Drawing Sheet









POWER-ON DETECTION CIRCUIT

FIELD OF THE INVENTION

The present invention relates to power supply threshold detectors, and in particular power supply threshold detectors incorporated in integrated circuitry without Zener reference elements.

BACKGROUND OF THE INVENTION

The detection of adequate power supply voltage upon equipment power up requires an accurate and consistent determination of the earliest point of adequate power supply voltages, and minimization of false signals and changes the threshold at which a signal is 15 produced indicating the proper supply potential. Previous power-on detection circuits which produce undervoltage lock-out signals for inadequate power supply voltage have almost universally relied upon comparison of an input voltage to a Zener diode reference element. 20 However, the actual potential of the Zener diode reference is notoriously process and temperature dependent. As a result, the change in Zener potential due to manufacturing and temperature variances significantly affect product yield. Alternately, construction of discrete 25 under-voltage lock-out circuits having selected Zener diodes is both time consuming and expensive.

SUMMARY OF THE INVENTION

The power-on detection circuit according to the 30 present invention comprises a comparator having hysteresis, with an integral threshold circuit wherein the internal threshold is provided without a Zener reference element. The input signal to be measured is received by first transistor which in turn provides multi- 35 ple current signals therefrom from a split collector. Each collector current is received by separate current sinking elements including additional transistors and resistors which produce an under-voltage lock-out signal in response to changes in the input voltage. Changes 40 in input voltage cause corresponding changes in current in each of the various collector current paths. The threshold at which the under-voltage lock-out signal is produced is determined by resistance ratios in the various collector current paths and semiconductor band- 45 gap voltage (Vbg) of the semiconductor material.

The circuit can be easily implemented on a bipolar monolithic integrated circuit, consumes very little supply current, and consumes very little circuit space. The preferred embodiment comprises 5 transistors and 3 50 resistors, and is independent of resistor absolute value.

BRIEF DESCRIPTION OF THE DRAWING

These and other features according to the present invention will be better understood by reading the following detailed description taken together with drawing wherein:

FIG. 1 is a schematic diagram of one embodiment of the present invention; and

FIG. 2 is a graph of the characteristics of the circuits 60 $Vcc_1 = \left(2 + \frac{R_1}{R_3}\right)V_{bg} +$ according to FIG. 1.

DETAILED DESCRIPTION OF THE INVENTION

As shown in FIG. 1, the power supply voltage to be 65 monitored is received by the emitter of transistor Q_1 through resistor R_1 at input V+. The transistors Q_2 and Q_3 along with R_2 and R_3 form a temperature compensat-

ing current sink. Transistor Q₄ acts an error amplifier, which amplifies slight differences between the currents from Q₁ collector 54 and the temperature compensating current from the collector of Q₃ and R₃. Transistors Q₅ is the output driver providing the current flow exemplified by FIG. 2.

For V + less than Vbe, every transistor is off. For increasing monitored voltage above 2Vbe, current begins to flow through R1, the emitter-base junction of transistor Q₁ and through the emitter-base junction transistor Q₅, initially turning both Q₁ and Q₅ on. However, at the same time, a current equal to the base current of Q₅ flows into the base and collector of Q₂ and into the base of Q₃. Also, a current equal to the base current of Q₅ flows into R₃, the base of Q₄ and the collector of Q_3 . For V + below the turn-on threshold, the current in the collector of Q₃ plus the current in R₃ equals the current in the corresponding collector 54 of Q₁, providing no (or insufficient) base current to turn on transistor Q₄. However, as the monitored voltage V+ increases to the turn-on threshold, Q₄ will begin to turn on, causing an increasing current to flow through resistor R₁ and thus increasing current flow to the collectors of transistor Q₁. As Q₄ turns on, it pulls additional current from the base of Q_1 , which provides more current from Q₁ (and therefore collector 54), which turns on Q₄ harder. Transistor Q₄ turning on instantly turns off transistor Q₅, which provides an output signal shown by graph 60 curve portions 62, 64, 66, depending on device temperature. Thus, the turn-on threshold of the present apparatus is determined in part by the current resulting from the selection of resistor R₁ relative to the single base emitter voltage (Vbe) of transistor Q₁. For any voltage above that thershold the circuit state remains the same and Q₅ stays off.

As the monitored power supply voltage at V+ begins to decrease, such as in a power down sequence, transistors Q_1 and Q_4 initially stay on, but the current out of any Q_1 collector (52, 54, 56) decreases). When the current out of collector (54) of Q_1 drops below the current sinking through the collector of transistor Q_3 plus the current Vbe/ R_3 , transistor Q_4 will lose sufficient base drive and turn off, turning Q_5 on, shown by curve section 74 on FIG. 2.

The separate turn-off threshold which provides the hysteresis characteristic shown in FIG. 2 of the circuit of 1 is due to the fact that transistor Q_4 , no longer being saturated allows the Vbe of transistor Q_5 to be added to (in series with) the Vbe of transistor Q_1 , thereby affecting the current produced from collectors 52, 54 and 56 of transistor Q_1 (in response to the selected resistor R_1 and the monitored voltage V+). An approximation of the turn-on and turn-off thresholds are enumerated below in equations 1 and 2 respectively, where Vbg is the band-gap potential of the semiconductor material, such as silicon in the present invention:

$$Vcc_1 = \left(2 + \frac{R_1}{R_3}\right) V_{bg} + \tag{1}$$

$$\left[\frac{K}{q} \frac{R_1}{R_2} \ln M + .004 - .002 \frac{R_1}{R_3} \right] T$$

$$Vcc_2 = \left(2 + \frac{R_1}{R_3}\right) V_{bg} + \tag{2}$$

-continued

$$\left[\frac{K}{q} \frac{R_1}{R_2} \ln M + .004 - .002 \frac{R_1}{R_3} \right] T$$

Note that for a particular choice of components, the turn-on and turn-off thresholds can be made nearly independent of temperature. For instance, in the embodiment shown, $R_1 = 30K$ ohms, $R_2 = 3K$ ohms, and 10 $R_3 = 80k$ ohms to provide a voltage threshold of approximately 4.2 volts with ± 200 millivolts (mv) of hysteresis, FIG. 2.

A graph showing the turn-on and turn-off points of the embodiment shown in FIG. 1 of the present inven- 15 tion shows the response of a circuit for 0° C., 50° C. and 100° C., wherein it can be appreciated that the hysteresis characteristics is repeatable in the manufacturing process and maintained under a wide temperature variation and the threshold points are sufficiently consistent 20 to eliminate the necessity of Zener reference elements in circuitry embodying the present invention. Thus the apparatus according to the present invention provides a repeatable accuracy significantly exceeding that achievable with standard process Zener diodes, and is applica- 25 ble to various devices such as linear and switching voltage regulators, and inductive load drivers and in complex control systems.

Modifications and substitutions of the present invention by one skilled in the art is considered to be within 30 the scope of the present application, which is not to be limited except by the claims which follows.

What is claimed is:

- 1. A power-on detection circuit, comprising:
- magnitude in response to a supply potential and a first transistor base-emitter voltage drop;
- means for receiving a selected portion of current from said means for providing a source of current; and
- means for sensing when the selected portion of current exceeds a selected magnitude, reducing said first transistor base-emitter drop voltage and providing an output signal indicating a selected supply potential corresponding to an on condition.
- 2. The power-on detection circuit of claim 1, wherein said means for providing comprises a transistor having a plurality of collectors,
- said means for receiving being connected to one of said plurality of collectors, and
- said means for sensing being connected to a second of said plurality of collectors.
- 3. A power-on detection circuit, comprising:

means for providing a source of current at a first magnitude in response to a supply potential and a 55 first transistor base-emitter voltage drop;

- temperature compensated means for receiving a selected portion of current from said means for providing a source of current; and
- means for sensing when the selected portion of current exceeds a selected magnitude, reducing said first transistor base-emitter drop voltage and providing an output signal indicating a selected supply potential corresponding to an on condition; wherein
- said temperature compensated means for providing a source of current comprises
 - a multiple collector first transistor having a series connected emitter resistor,
 - a diode connected second transistor connected to one of said multiple collectors and a common terminal, and
 - a third transistor having a base junction connected to said second transistor, an emitter junction connected to said common terminal through an emitter resistor, a collector connected to a second collector of said first transistor and a resistor to said common terminal, and wherein
- said resistor connected to said first, second and third transistors are selected to provide the hysteresis turn-on and turn-off thresholds.
- 4. The power-on detection circuit of claim 3, wherein said means for sensing comprises a fourth transistor having a base junction connected to the collector of said third transistor, and wherein
- the current in excess of the current sunk by the collector of the third transistor and the resistor connected thereto is received by said fourth transistor to be made conductive.
- 5. The power-on detection circuit of claim 1, wherein means for providing a source of current at a first 35 at least one of said means for receiving and means for providing a source of current includes temperature compensation means.
 - 6. A threshold detector for sensing a predetermined voltage level of a voltage source, comprising:
 - means for providing a source of current at a first magnitude in response to a supply potential and a first transistor base-emitter voltage drop; and
 - means for sensing when said source of current exceeds a selected magnitude, reducing said first transistor base-emitter voltage drop and providing on output signal indicating said voltage source has attained said predetermined voltage level.
 - 7. The threshold detector of claim 6, further including
 - current limiter means connecting said means for providing a source of current and said voltage source.

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- 8. The threshold detector of claim 7, wherein said current limiter means comprises a resistor.
- 9. The threshold detector of claim 6, wherein said current limiter means comprises a resistor.

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