United States Patent [19]

Leitch

[11] Patent Number:

4,816,783

[45] Date of Patent:

Mar. 28, 1989

[54]	METHOD AND APPARATUS FOR QUADRATURE MODULATION				
[75]	Inventor:	Clifford D. Leitch, Coral Springs, Fla.			
[73]	Assignee:	Motorola, Inc., Schaumburg, Ill.			
[21]	Appl. No.:	141,757			
[22]	Filed:	Jan. 11, 1988			
[58]	Field of Sea	rch			
[56] References Cited					
U.S. PATENT DOCUMENTS					
	3,082,296 3/1 3,511,936 5/1	960 Hodgson et al. 179/15 963 Caruthers 370/20 970 Saltzberg 370/20 970 Palatinus 370/20			

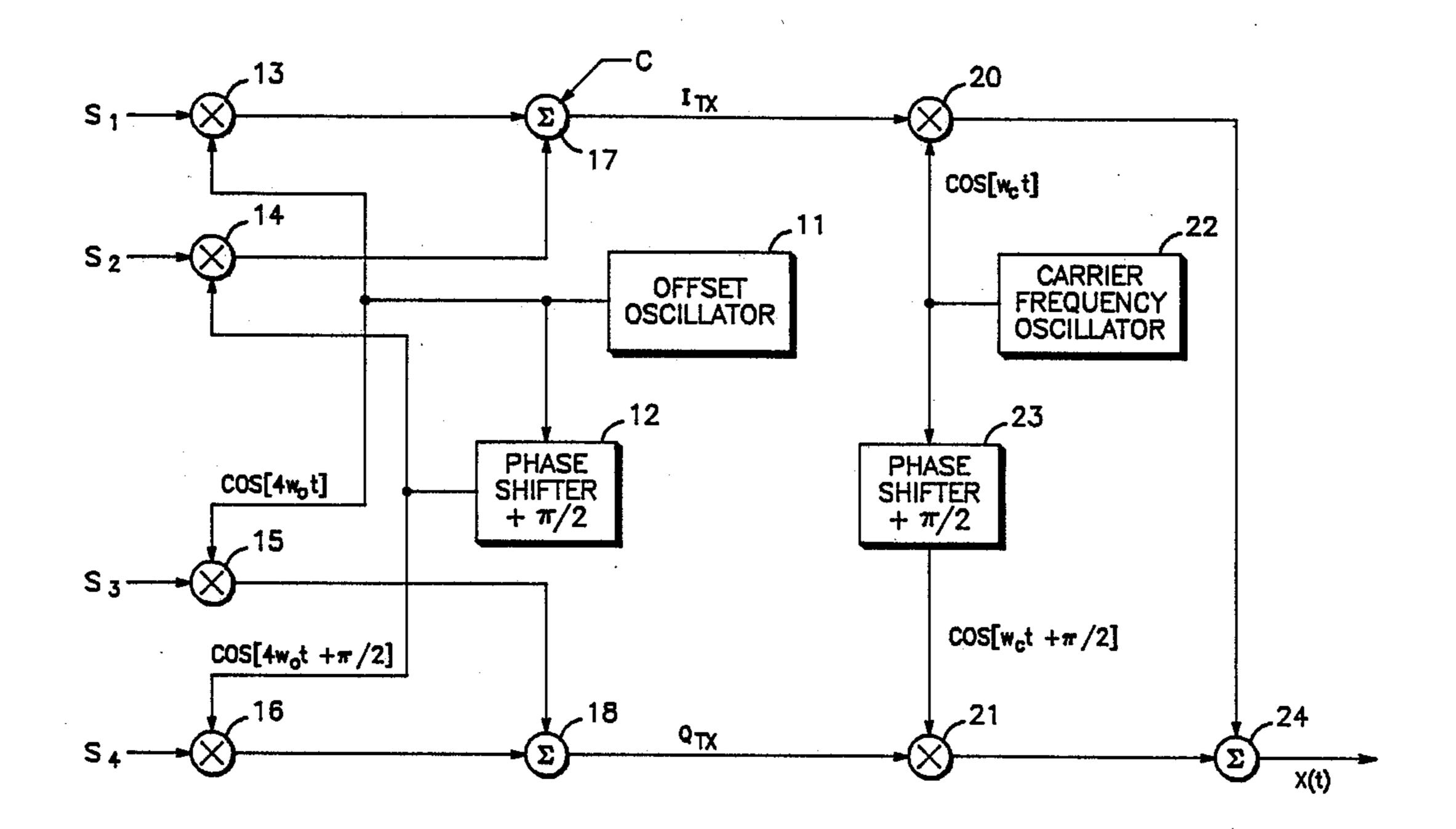
3,821,798	6/1974	Cannon	370/74
4,313,211		Leland	
4,398,216	8/1983	Field et al.	370/20
4,521,878	6/1985	Toyonaga	455/60 X
4,626,803		Holm	
4,675,619	6/1987	Uchibori et al	332/31 R
4,680,777	7/1987	Saha	375/53
4,696,017	9/1987	Masheff et al	375/60

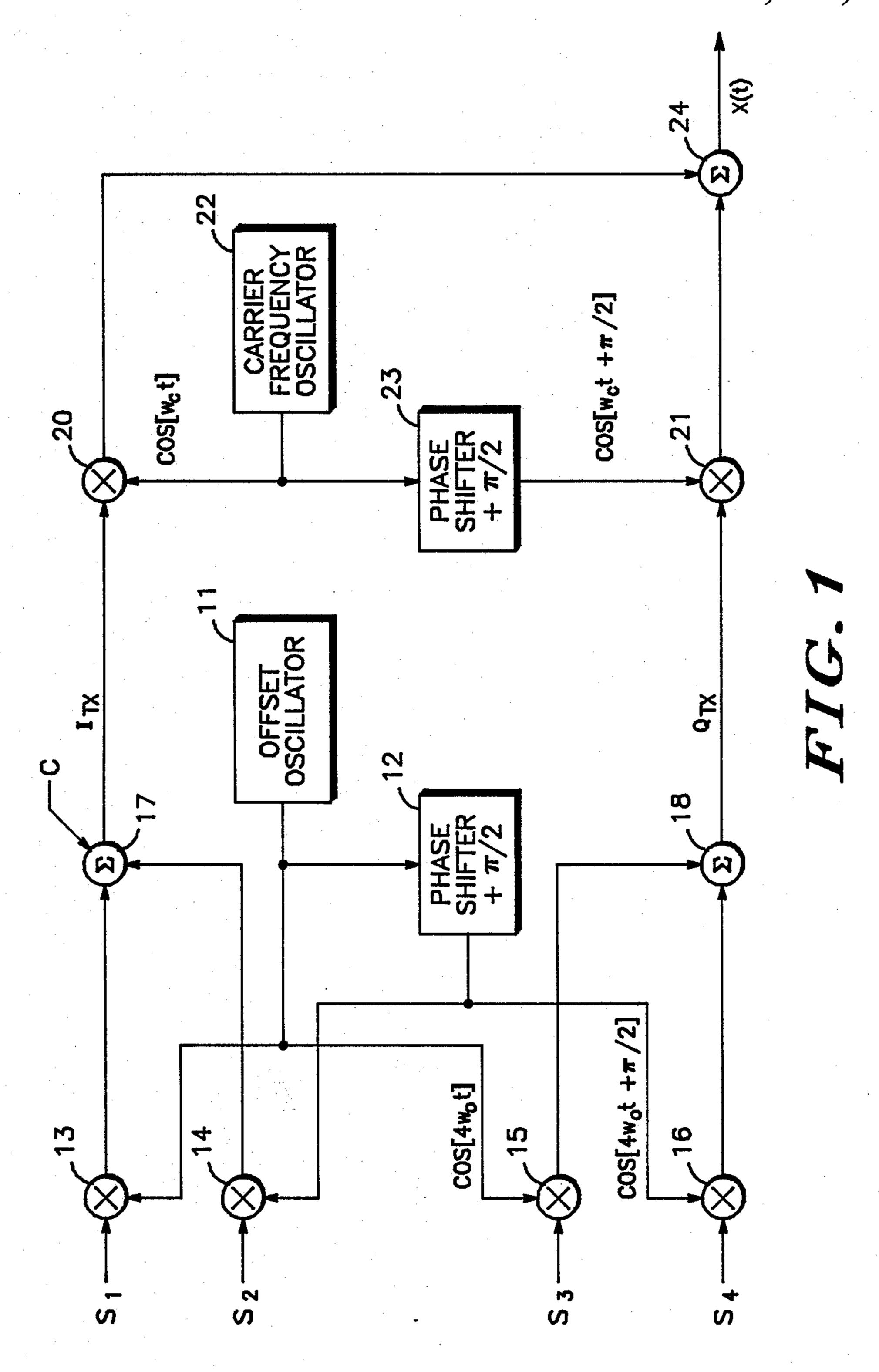
Primary Examiner—Eugene R. LaRoche Assistant Examiner—Robert J. Pascal Attorney, Agent, or Firm—Daniel K. Nichols

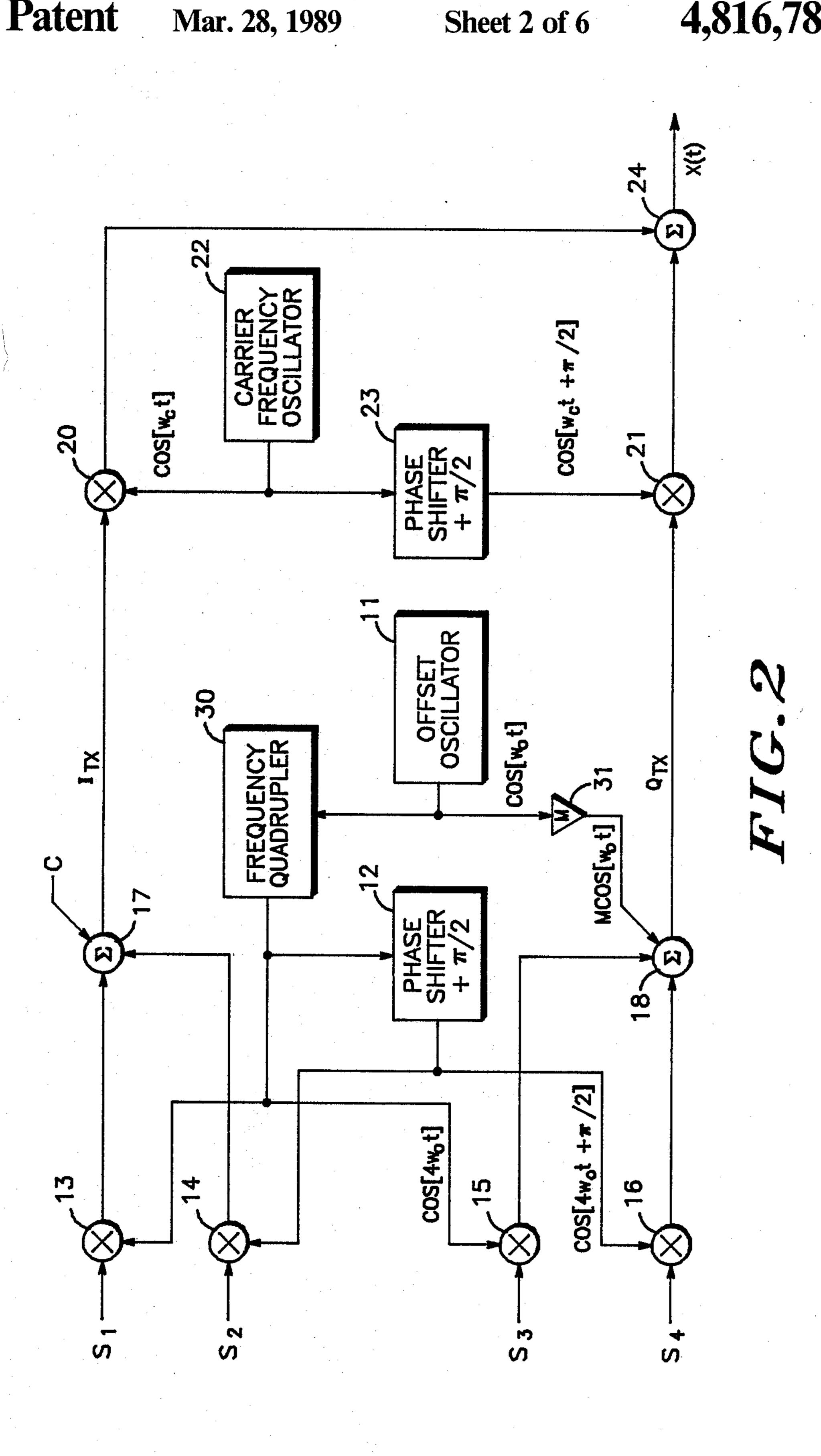
[57] ABSTRACT

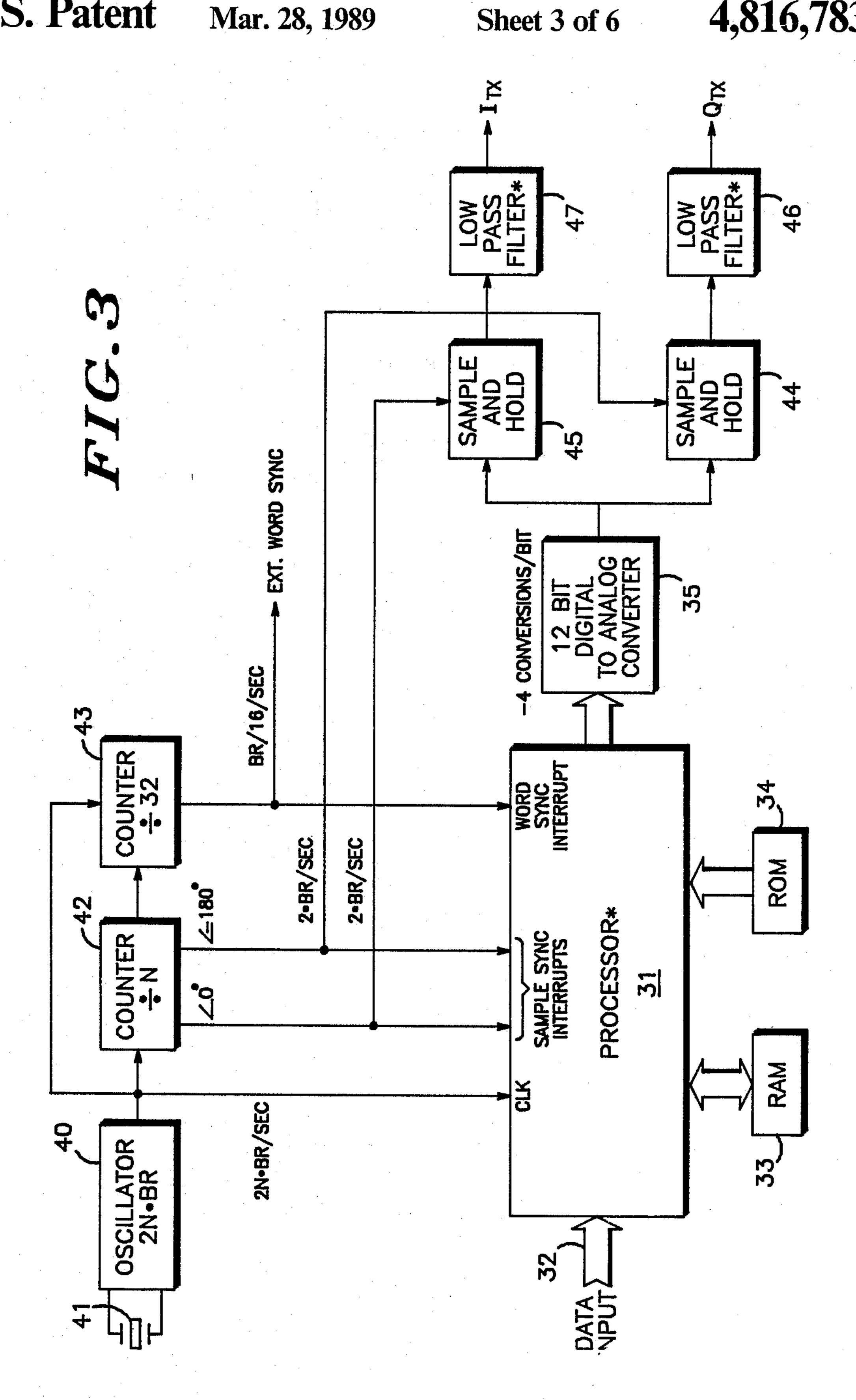
A quadrature amplitude modulation system utilizes two subcarrier signals, each quadrature modulated with information signals which are quadrature modulated onto the RF carrier. This provides a hole in the center of frequency spectrum, permitting carrier and bit sync signals can be provided in the center area of the signal spectrum.

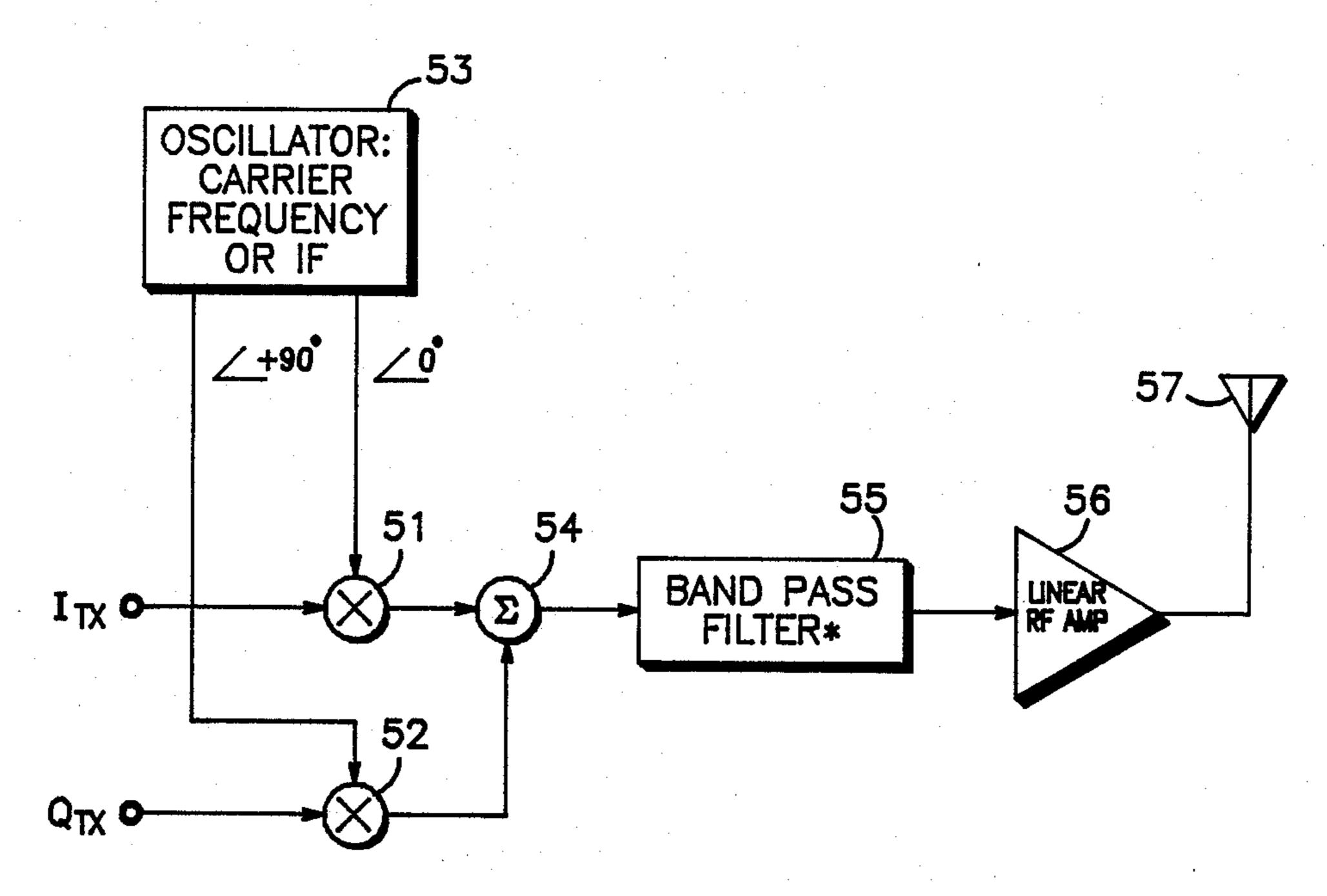
11 Claims, 6 Drawing Sheets











Mar. 28, 1989

FIG. 4

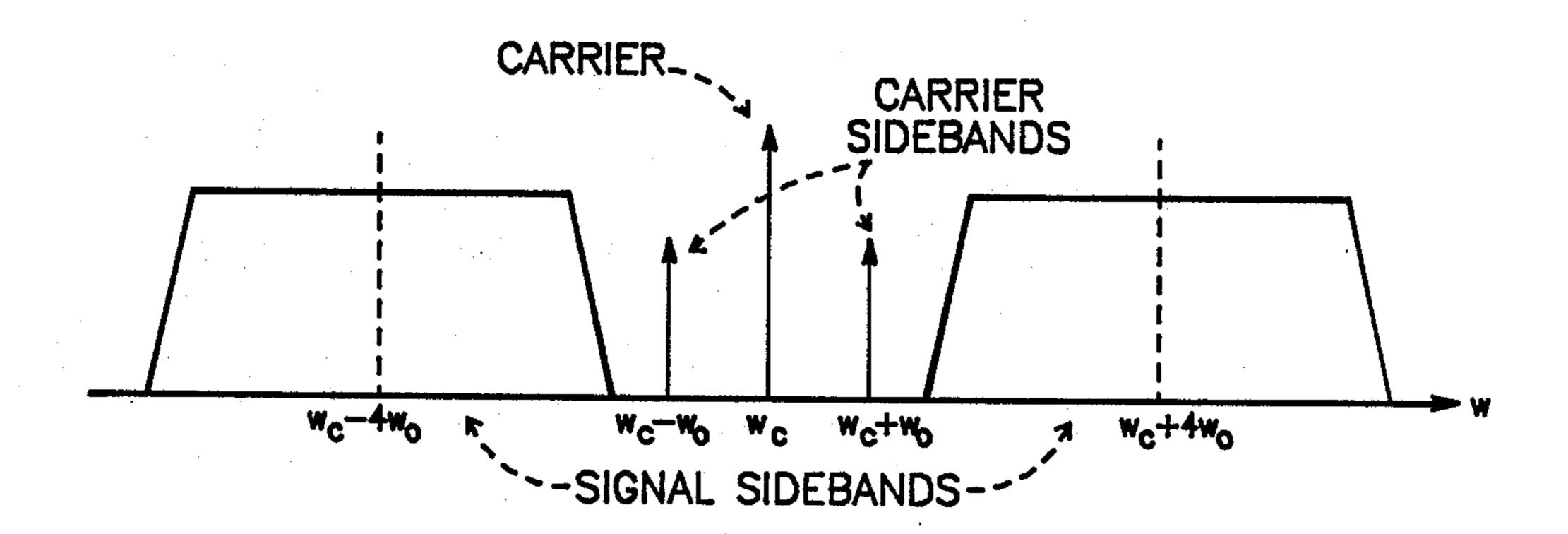
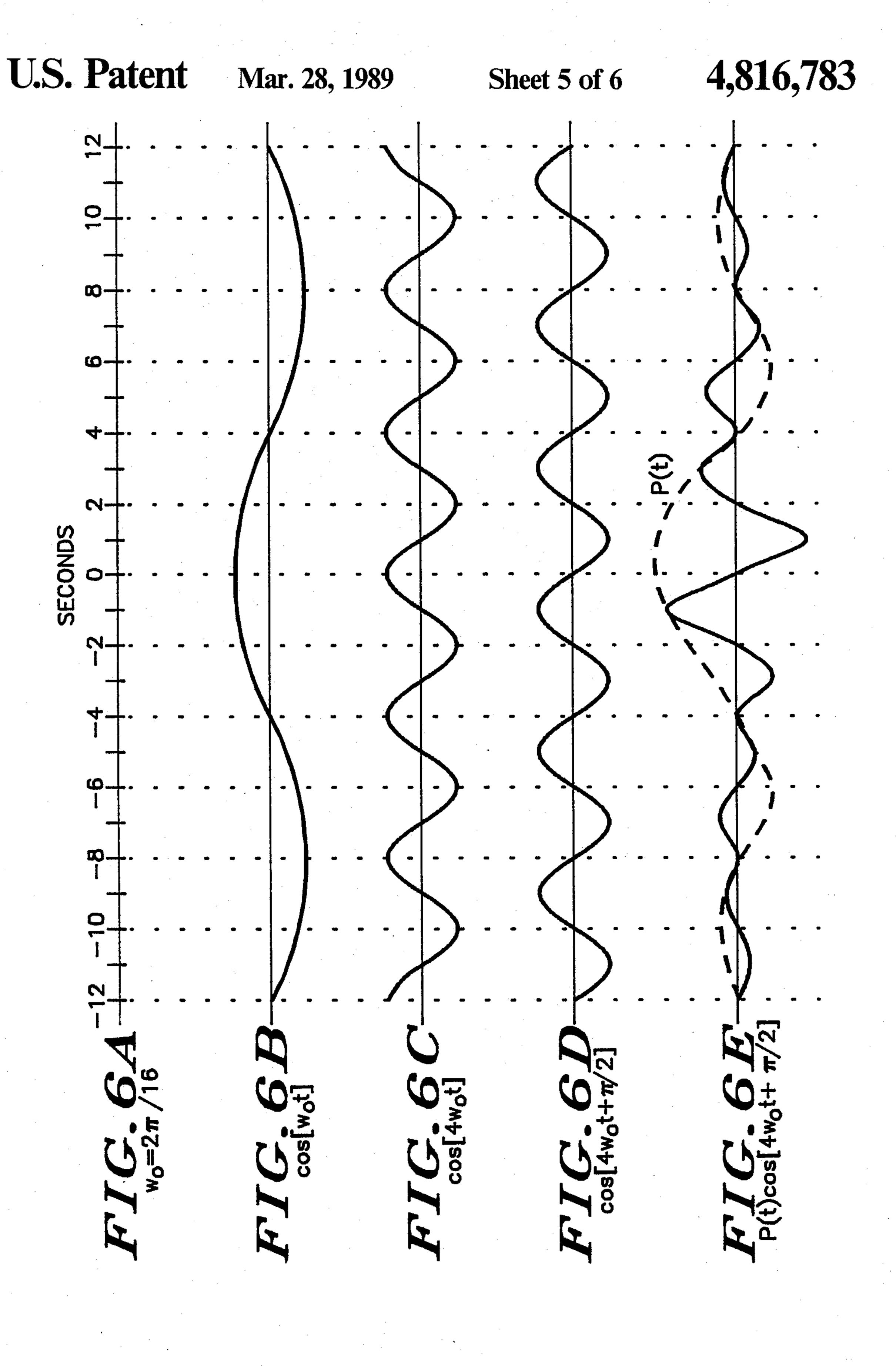
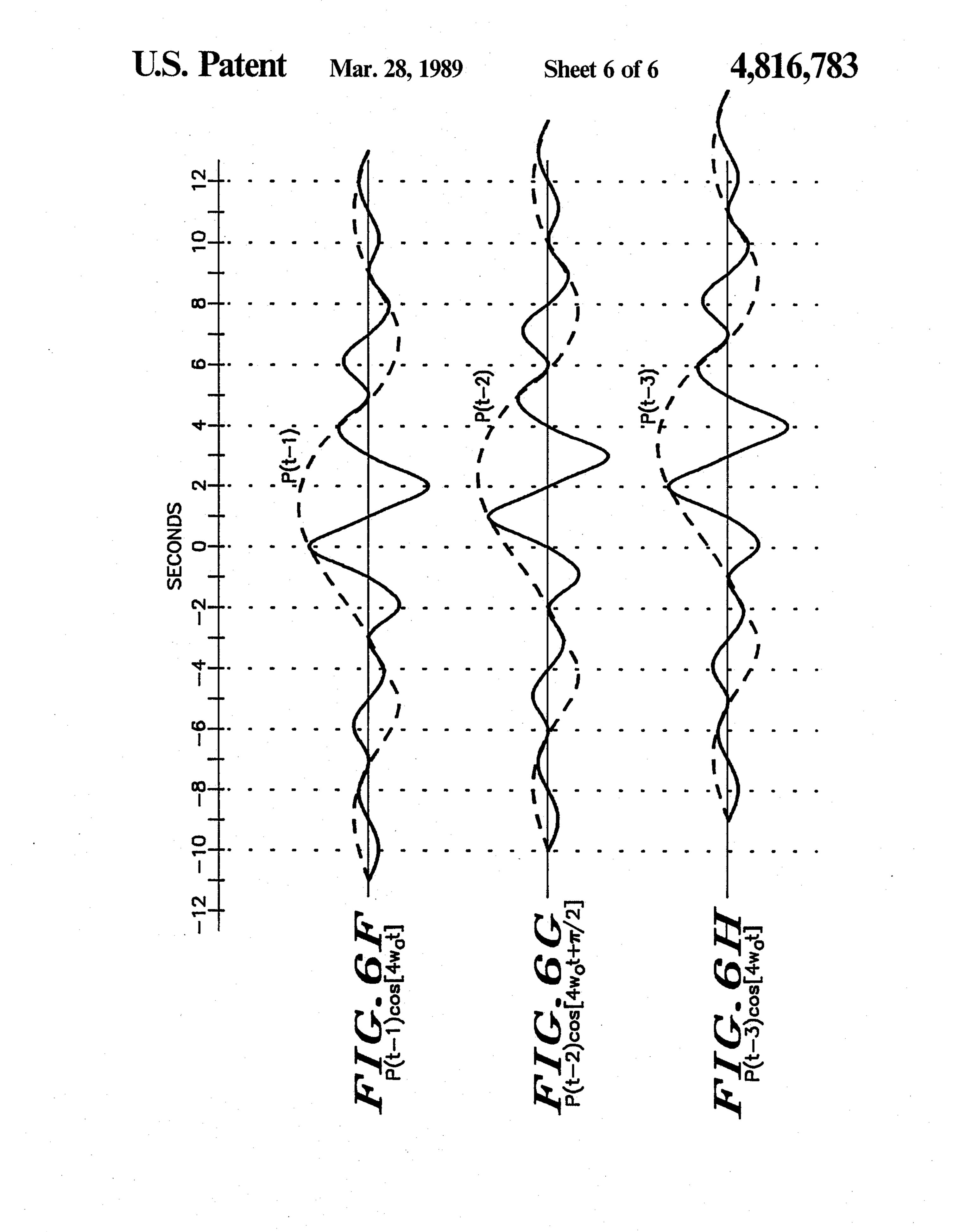


FIG. 5





METHOD AND APPARATUS FOR QUADRATURE MODULATION

BACKGROUND OF THE INVENTION

A portion of the disclosure of this patent document contains material which is subject to copyright protection. The copyright owner has no objection to the facsimile reproduction by anyone of the patent document or the patent disclosure, as it appears in the Patent and Trademark Office patent file or records, but otherwise reserves all copyright rights whatsoever.

This invention relates to quadrature amplitude modulation systems in general and particularly to a system in which signal components are modulated unto a subcar- 15 rier to allow for inclusion of carrier and bit sync information at the center of the transmitted frequency spectrum. In a quadrature modulation system, designed for radio transmission, it is desirable to transmit a pilot carrier in order to facilitate reception and decoding of ²⁰ the transmitted information. While it is known to transmit a pilot carrier, such carriers have been added as a side frequency to the quadrature amplitude modulated signal. There are, however, limitations and disadvantages to this approach. Due to selectively fading, such 25 as can occur on a radio path, problems can result where the pilot carrier is spaced from the signal information. Additionally, problems can occur due to limitations in the passband of receivers i that the pilot carrier signal may fall too close to or outside of receiver's passband 30 filter edge. Consequently, it is desirable that such a pilot carrier be located more centrally to the transmitted frequency spectrum.

Where digital information is to be transmitted in a synchronous manner, channel fading and noise can 35 prevent the maintenance of bit sync. In such a system it is therefore desirable to transmit a bit sync signal with the synchronous digital information. Like the pilot carrier, the bit sync signal should be provided as close to the center of the transmitted frequency spectrum as 40 possible.

SUMMARY OF THE INVENTION

This method and apparatus for a quadrature amplitude modulation permits the inclusion of both the car- 45 rier pilot and bit sync signals at and adjacent to the center of the signal spectrum.

A method of transmitting a quadrature amplitude modulated signal including the steps of: quadrature modulating first and second signals onto a subcarrier; 50 quadrature modulating third and fourth signals onto a subcarrier; quadrature modulating the first and second quadrature modulated subcarriers onto a carrier; and tranmitting the quadrature modulated carrier.

In one aspect of the invention, the method includes 55 the further step of providing a DC component with one of the quadrature modulated subcarrier to produce a pilot carrier. In another aspect of the invention, the method includes the further step of providing a bit sync signal with one of said quadrature modulated subcarriers. In still another aspect of the invention, the signals are digital signals having a predetermined bit rate and the bit sync signal has a frequency that is an integral submultiple of the bit rate.

In still another aspect of the invention, a method of 65 transmitting a quadrature amplitude modulated signal includes the steps of reading from memory first and second prototype pulses each including a subcarrier

component, summing the first and second prototype pulses to produce a first quadrature modulated subcarrier, reading from memory third and fourth prototype pulses each including a subcarrier component, summing said third and fourth prototype pulses to produce a second quadrature modulated subcarrier, quadrature modulating a carrier with said first and second quadrature modulated subcarriers and transmitting the quadrature modulated carrier.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of a quadrature amplitude modulation system in accordance with the present invention, particularly suitable for the transmission of analog signals.

FIG. 2 is a block diagram of another quadrature amplitude modulation system in accordance with the present invention, particularly suitable for the transmission of digital signals.

FIG. 3 is a schematic block diagram of another quadrature amplitude modulation system in accordance with the present invention, which utilizes predetermined pulse waveforms.

FIG. 4 is a schematic block diagram of a the transmitter backend for use with the system of FIG. 3.

FIG. 5 is a graphical representation of the frequency spectrum of a quadrature modulated signal with a pilot carrier and bit sync signals in accordance with the present invention.

FIG. 6A is a time line normalized for 1 bit per second. FIG. 6B is a graphical representation of the offset oscillator output cos (w₀t).

FIG. 6C is a graphical representation of the frequency quadrupler output or subcarrier cos (4w₀t).

FIG. 6D is a graphical representation of the phase shifter output or quadrature subcarrier cos (4w₀t+Pi/2).

FIG. 6E is a graphical representation of the S2 channel pulse P(t) modulated on the quadrature subcarrier of FIG. 6D.

FIG. 6F is a graphical representation of the S1 channel pulse P(t-1) modulated on the subcarrier of FIG. 6C.

FIG. 6G is a graphical representation of the S4 channel pulse P(t-2) modulated on the quadrature subcarrier of FIG. 6D.

FIG. 6H is a graphical representation of the S3 channel pulse P(t-3) modulated on the subcarrier of FIG. 6C.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now by characters of reference to the drawings and first to FIG. 1, a quadrature modulation system is shown which is capable of providing a pilot carrier signal in the center of the signal spectrum. Four input signals S1-S4 which can be independent analog and/or digital signals are combined. This particular system is most suitable for analog signals as no provision is made for insertion of bit sync information.

An offset oscillator 11 is used to provide a subcarrier signal $\cos[w_0t]$. Its output is also provided to a 90 degree phase shifter 12 which provides a quadrature subcarrier signal $\cos(w_0t+Pi/2)$. The four input signals S1-S4 are applied to mixer or multiplier circuits 13-16 respectively. The subcarrier signal from oscillator 11 is applied to mixers 13 and 15 while the quadrature sub-

3

carrier signals, from phase shifter 12 is applied to mixers 14 and 16. The outputs of mixers 13 and 14 are combined at summer 17, while the outputs of mixer 15 and 16 are combined at summer 18. The output of summer 17 is the I_{tx} or in-phase signal for modulation on the RF 5 carrier and the output of summer 18 is the Q_{tx} or quadrature signal for quadrature modulation on the RF carrier. Mixers 13 and 14 and summer 17 constitute means for quadrature modulating first and second signals on a first subcarrier while mixers 15 and 16 and summer 18 10 constitute means for quadrature modulating third and fourth signals on a second subcarrier.

When it is desired to provide a pilot carrier signal for transmission with the quadrature modulated signals, a DC offset voltage, having a magnitude C, is applied to 15 one of the summers 17 and 18. In this embodiment, DC voltage is applied to the summer 17. The outputs of summers 17 or 18 are provided to mixer or multipliers 20 and 21 respectively. A carrier frequency oscillator 22 provides an in phase carrier signal cos(w_ct) which is 20 applied to the mixer 20 and to the input of a 90 degree phase shifter 23. The output of phase shifter 23, which is the quadrature carrier signal cos(w_ct+Pi/2), is applied to the mixer 21. The outputs of mixers 20 and 21 are provided to a summing circuit 24 to produce the 25 combined transmit signal X(t). The X(t) signal can then be applied as through a bandpass filter and amplifier to an antenna, which constitute means for transmitting the quadrature modulated carrier, for radio transmission as is discussed subsequently in regard to FIG. 4. The mix- 30 ers 20 and 21 and summer 24 constitute means for quadrature modulating the subcarriers onto a carrier.

When digital signals are to be transmitted, it is desirable to provide a bit sync signal. The bit sync signal can be provided as sideband signals to the carrier signal and 35 be located in the frequency spectrum between the quadrature signals. A system suitable for digital communication is illustrated in FIG. 2. The parts of FIG. 2 which are identical to the parts of FIG. 1 are indicated with the same reference numeral. The principal difference 40 involves the offset oscillator arrangement. In this case, the offset oscillator 11 provides an output frequency wo which is one quarter of the oscillator frequency of FIG. 1. The frequency wo is chosen as an integer submultiple of the bit rate and in the preferred embodiment is one- 45 fourth of the bit rate of each of the subchannels (one-sixteenth of the total bit rate). The output of offset oscillator 11 of FIG. 2 is applied to a frequency quadrupler 30 for application to the phase shifter 12 and mixers 1314 16 in a manner identical to FIG. 1. However, the lower 50 frequency signal of offset oscillator 11 is also applied to a amplifier 31 having an amplification factor equal to M. Its output is applied, in this case, to the summer 18 constituting means for summing a sync signal with one of the subcarriers. It will be understood that the output 55 of amplifier 31 could be applied to the summer 17 and the carrier signal C applied to the summer 18 if desired or both to the same summer. The I_{tx} and Q_{tx} signals are then quadrature modulated on the carrier frequency as in FIG. 1. The output signal X(t) includes not only the 60 quadrature modulated signal components but also a carrier and bit sync sidebands as illustrated in FIG. 5. The S1-S4 signals are preferably predetermined pulses P(t) read from a memory ROM, such as it is disclosed in co-pending U.S Pat. No. 4,737,969, issued Apr. 12, 65 1988, and owned by the assignee of this invention, the disclosure of which is incorporated by reference as if fully set out herein.

4

When using stored pulses, the mixing or multiplication step of mixers 13-16 can be eliminated by reading from memory pulses representative of the product of the multiplication or mixing, provided the bit rate and subcarrier frequency are related by an integer ratio.

FIG. 3 illustrates a microprocessor based system for providing the I_{tx} and Q_{tx} signals. In this case a digital signal processor 31, constituting processor means, includes a data input 32 for receiving the digital data to be transmitted. The digital data can be four independent digital data stream or preferably a single data stream can be subdivided as the S1-S4 signals. The processor 31 includes RAM 33 and ROM 34. The ROM 34 includes the preprogrammed waveforms which are be summed to provide the I_{tx} and Q_{tx} signals. The I_{tx} signal is produced by adding an S1 stored pulse corresponding to P(t-1) cos (4w₀t) of FIG. 6F to an S2 signal corresponding to P(t) cos (4w₀t+Pi/2) of FIG. 6E along with the carrier amplitude constant C. Similarly for the Q_{tx} signal, the S3 signal P(t-3) cos (4w₀t) and the S₄ stored pulse P(t) cos $(4w_0t+Pi/2)$ of FIG. 6G are added along with the bit sync signal M cos (4wot). The process continues similarly for each successive set of 4 bits. It will be appreciated that for a binary system it is only necessary to store one prototype pulse. It is negated to represent the other binary signal. Also as illustrated in FIGS. 6E-6H, the same waveform is used on each channel S1-S4 differing only in phase or time. While the preferred embodiment utilizes binary or two level signals, multilevel (e.g. 8 level) signals could be provided on each channel to increase information throughput. It would then be necessary to store four pulses for an 8 level signal since their negatives would represent the other four levels which can be easily computed by the processor 31.

The output of processor 31 is applied to a 12 bit D/A converter 35. An oscillator circuit 40, having a crystal, 41 provides an output frequency equal to 2N×Bit Rate which is applied to the clock input of processor 31 and the clock inputs of counters 42 and 43. Counter 42, constituting a divide by N counter, provides 0 degree and a -180 degree outputs, which are applied to the processor 31 as a sample sync interrupts and are also applied to sample and hold circuits 44 and 45, respectively. These are at twice the bit rate to permit the single D/A converter 35 to be used for both the I_{tx} and Q_{tx} signals. The inputs of sample and hold circuits 44 and 45 are connected to the output of the D/A converter 35. Low pass filters 46 and 47 are connected to the outputs of the sample and hold circuits 44 and 45 with their outputs providing the Q_{tx} and I_{tx} transmit signals. These are then quadrature modulated on the carrier frequency w_c as in FIG. 1 and 2. In this embodiment, a Texas Instruments TMS 32020 Digital Signal Processor can be utilized. The object code including the prototype pulse information as stored in ROM 34 is given in Table 1, which is appended hereto.

Referring now to FIG. 4, the radio backend for quadrature modulation of the I_{tx} and Q_{tx} signals of FIG. 3 onto a carrier, is illustrated. The I_{tx} and Q_{tx} signals are applied to mixers 51 and 52 respectively which correspond to the mixers 20 and 21 of FIGS. 1 and 2. The carrier and 90 degrees quadrature carrier signals are provided to mixers 51 and 52 respectively, as by carrier frequency oscillator 53 which corresponds to the carrier frequency oscillator 22 and phase shifter 23. The output of mixers 51 and 52 are applied to a summer 54 whose output provides the transmit signal X(t).

5

The backend of the transmitter is identical to that to be used in the circuits of FIG. 1 and FIG. 2. The output of the summer 54 in this case, or the summer 24 of FIGS. 1 and 2, is applied to a bandpass filter 55 having its output applied to a linear RF amplifier 56, the output of which is transmitted via antenna 57. The transmitted signal includes the input signals modulated on subcarriers, the center carrier signal and the two carrier sideband bit sync signals as illustrated in FIG. 5. The carrier and bit sync signals are useful when demodulating the 10 received transmitted signal in order to compensate for selective fading that can occur over a radio path.

In operation, a first pair of signals are quadrature

modulated onto a first subcarrier while a second pair of signals are quadrature modulated onto a second subcarrier. The two quadrature modulated subcarriers are then quadrature modulated onto the carrier resulting in the information carrying components signal being spaced from the carrier frequency. A pilot carrier signal and bit sync signals can be inserted between sidebands carrying the twice quadrature modulated information signals. This provides a spectrally efficient signal capable of being successfully transmitted over an unstable channel. Consequently, it can be used in applications, such as land mobile radio where conventional quadrature amplitude modulation cannot be reliably applied.

TABLE 1

KOOOOXMT II.590000BFF80B0020BFF80B0599BFF80B059990020BCE02BCE077F187F BC800BCE08B5589BC103BD001BFFFFB60A0BD001BFFC1B60A0BCA00B6880BC8067F0E7F BCA01B604EB604FBB050B9F50BF880B014BBD001B07CFB604CBD001B00C5B604D7F130F B204EB104FB604EBF180B004FBCA19B604EBC104BD001BFFC2B60B0BCE00BCE1F7F0F1F BC104BD001BFFC2B60B0BFF80B0051BCE00BCE1FBD001B065DB604CBD001B01EE7F101F B604DBCE00BCE1FBD001B03EBB604CBD001B021BB604DBCE00BCE1FBD001B01357F10BF B604CBD001B00FDB604DBCE00BCE1FBD001BFF03B604CBD001BFECBB604DBCE007F0C2F BCE1FBD001BFDE8B604CBD001BFC15B604DBCE00BCE1FBD001BFE12B604CBD0017F0B9F BF9A3B604DBCE00BCE1FBD001BFF3BB604CBD001BF831B604DBCE00BCE1FBD0017F0B3F BOOC5B604CBD001BF831B604DBCE00BCE1FBD001B01EEB604CBD001BF9A3B604D7F0FBF BCE00BCE1FBD001B021BB604CBD001BFC15B604DBCE00BCE1FBD001B00FDB604C7F0E6F BD001BFECBB604DBCE00BCE1FBD001BFECBB604CBD001B00FDB604DBCE00BCE1F7F07FF BD001BFC15B604CBD001B0218B604DBCE00BCE1FBD001BF9A3B604CBD001B01EE7F104F B604DBCE00BCE1FBD001BFB31B604CBD001B00C5B604DBCE00BCE1FBD001BFB317F0EDF B604CBD001BFF3BB604DBCE00BCE1FBD001BF9A3B604CBD001BFE12B604DBCE007F0C9F BCE1FBD001BFC15B604CBD001BFDEBB604DBCE00BCE1FBD001BFECBB604CBD0017F097F BFF03B604DBCE00BCE1FBD0C1B00FDB604CBD001B0135B604DBCE00BCE1FBD0017F0E7F BO218B604CBD001B03EBB604DBCE00BCE1FBD001B01EEB604CBD001B065DB604D7F114F BCEOOBCE1FBDOO1BOOC5B604CBDOO1BO7CFB604DBCE00BCE1FBD001BFF3BB604C7FQC1F BDOO1BO7CFB604DBCE00BCE1FBD001BFE12B604CBD001B065DB604DBCE00BCE1F7F0CCF BD001BFDE8B604CBD001B03EBB604DBCE00BCE1FBD001BFF03B604CBD001B01357F0F3F B604DBCE00BCE1FBD001B0135B604CBD001BFF03B604DBCE00BCE1FBD001B03EB7F0E7F B604CBD001BFDE8B604DBCE00BCE1FBD001B065DB604CBD001BFE12B604DBCE007F0D7F XMT II23 BCE1FBD001B07CFB604CBD001BFF3BB604DBCE00BCE1FBFF80B0036BD100B02007F0DFF XMT 1124 BCB63BFCA0B059DBCE05BCB06BD100B0300BCB1FBFCA0B0601B9E50BF980B01707F0F0F XMT II25 BD100B0320BCB0ABFCA0B064DBD100B032BBCB0ABFCA0B0658BD100B0336BCB0A7F101F XMT 1126 BFCA0B0663BD100B0341BCB0ABFCA0B066EBFF80B0184BD1CJL)320BCB0ABFCA07F0EDF XMT II27 B0621BD100B032BBCB0ABFCA0B062CBD100B0336BCB0ABFC6. > 1637BD100B03417F131F XMT II28 BCBOABFCA0B0642BCA00BA000BD100B0329BCB09B5D90BFF5ABD100B0334BCB097F0FCF XMT II29 B5D90BFF46BCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF32BD100B034A7F0FBF OEII TMX BCB09B5D90BFF1EBCE15B0017B604DB204EB104FB604EBF1B0B01B4BCA19B604E7F0F1F BC104BD001BFFC2B60B0BCE00BCE1FBC104BD001BFFC2B60B0BFF80B01B6BCE007F0DBF SEII TMX BCE1FBCA00BA000BD100B0329BCB09B5D90BFF50BD100B0334BCB09B5D90BFF3C7F0E6F EEII TMX BCE 15B604CBCA00BA000BD100B033FBCB09B5D90BFF2BBD100B034ABCB09B5D907F0FBF XMT 1134 BFF 14BCE 15B0018B604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF467F0E4F XMT II35 BD100B0334BCB09B5D90BFF32BCE15B604CBCA00BA000BD100B033FBCB09B5D907F10EF **BEII TMX** BFF1EBD100B034ABCB09B5D90BFF0ABCE15B0019B604DBCE00BCE1FBCA00BA0007F0C1F XMT II37 BD100B0327BCB07B5D70BFF3CBD100B0334BCB07B5D70BFF28BCE15B604CBCA007F0E6F SEII TMX BA000BD100B033FPCB09B5C90BFF14BD100B034ABCB09B5C90BFF00BCE15B001A7F105F XMT II39 B604DB203AB6036B2045B6041BCE00BCE1FBCA00BA000BD100B0329BCB09B5D907F147F XMT II40 BFF32BD100B0334BCB09B5D90BFF1EBCE15B604CBCA00BA000BD100B033FBCB097F0EEF **XMT 1141** B5D90BFF5ABD100B034ABCB09B5D90BFF46BCE15B001BB604DBCE00BCE1FBCA007F0AEF XMT 1142 BA000BD100B0329BCB09B5D90BFF2BBD100B0334BCB09B5D90BFF14BCE15B604C7F10AF EPII TMX BCA00BA000BD100B033FBCB09B5D90BFF50BD100B034ABCB09B5D90BFF3CBCE157F0DBF XMT 1144 B001CB604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF1EBD100B03347F10DF XMT 1145 BCB09B5D90BFF0ABCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF46BD1007F0D6F XMT II46 BO34ABCB09B5D90BFF32BCE15B001DB604DBCE00BCE1FBCA00BA000BD100B03297F0F6F XMT 1147 BCB09B5C90BFF14BD100B0334BCB09B5C90BFF00BCE15B604CB2024B6020B202F7F120F XMT 1148 B602BBCA00BA000BD100B033FBCB09B5D90BFF3CBD100B034ABCB09B5D90BFF2B7F0EAF XMT 1149 BCE15B001EB604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF5ABD1007F0E7F XMT 1150 B0334BCB09B5D90BFF46BCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF327F0EDF XMT 1151 BD100B034ABCB09B5D90BFF1EBCE15B001FB604DBCE00BCE1FBCA00BA000BD1007F0DCF XMT 1152 B0329BCB09B5D90BFF50BD100B0334BCB09B5D90BFF3CBCE15B604CBCA00BA0007F0EFF BD100B033FBCB09B5D90BFF28BD100B034ABCB09B5D90BFF14BCE15B0000B604D7F0FEF XMT 1154 BCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF46BD100B0334BCB09B5D907F0FBF

BFF32BCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF1EBD100B034ABCB097F0E0F 85D90BFF0ABCE15B0001B604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D907F0F4F I I 57 BFF3CBD100B0334BCB09B5D90BFF28BCE15B604CBCA00BA000BD100B033FBCB097F0E9F B5C90BFF14PD100B034ABCB09B5C90BFF00BCE15B0002B604DB203AB6036B20457F137F 1157 B6041BCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF32BD100B0334BCB097F117F 1160 P5D90BFF1EBCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF5ABD100B034A7F0DBF 1161 BCB09B5D90BFF46BCE15B0003B604DBCE00BCE1FBCA00BA000BD100B0329BCB097F0EDF XMT 1162 B5D90BFF28BD100B0334BCB09B5D90BFF14BCE15B604CBCA00BA000BD100B033F7F106F EAII TMX BCB09B5D90BFF50BD100B034ABCB09B5D90BFF3CBCE15B0004B604DBCE00BCE1F7F0B8F 1164 BCA00BA000BD100B0329BCB09B5D90BFF1EBD100B0334BCB09B5D90BFF0ABCE157F0EBF B604CBCA00BA000BD100B033FBCB09B5D90BFF46BD100B034ABCB09B5D90BFF327F0F8F XMT 1166 BCE15B0005B604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5C90BFF14BD1007F10AF XMT II67 B0334BCB09B5C90BFF00BCE15B604CB2024B6020B202FB602BBCA00BA000BD1007F151F 1148 B033FBCB09B5D90BFF3CBD100B034ABCB09B5D90BFF28BCE15B0006B604DBCE007F0D4F BCE1FBCA00BA000BD100B0329BCB09B5D90BFF5ABD100B0334BCB09B5D90BFF467F0E1F 1170 BCE 158604CBCA00BA000BD100B033F8CB09B5D90BFF32BD100B034ABCB09B5D907F100F BFF1EBCE15800078404DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF507F0DAF XMT 1172 BD100B03348CB09B5D90BFF3CBCE15B604CBCA00BA000BD100B033FBCB09B5D907F0FDF XMT II73 BFF28BD100B034ABCB09B5D90BFF14BCE15B0008B604DBCE00BCE1FBCA00BA0007F0DBF XMT 1174 BD100B0327BCB07B5D70BFF46BD100B0334BCB07B5D70BFF32BCE15B604CBCA007F0F7F XMT 1175 BA000BD100B033FBCB09B5D90BFF1EBD100B034ABCB09B5D90BFF0ABCE15B00097F0EAF XMT 1176 B604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF3CBD100B0334BCB097F0F3F XMT 1177 B5D90BFF2BBCE15B604CBCA00BA000BD100B033FBCB09B5C90BFF14BD100B034A7F0F9F XMT 1178 BCB09B5C90BFF00BCE15B000AB604DB203AB6036B2045B6041BCE00BCE1FBCA007F111F XMT 1179 BA000BD100B0329BCB09B5D90BFF32BD100B0334BCB09B5D90BFF1EBCE15B604C7F0FEF XMT IIBO BCA00BA000BD100B033FBCB09B5D90BFF5ABD100B034ABCB09B5D90BFF46BCE157F0D6F XMT IIB1 B000BB604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF28BD100B03347F11BF XMT 1182 BCB09B5D90BFF14BCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF50BD1007F0E7F EBII TMX BO34ABCBO9B5D90BFF3CBCE15B000CB604DBCE00BCE1FBCA00BA000BD100B03297F0E7F XMT IIB4 BCB09B5D90BFF1EBD100B0334BCB09B5D90BFF0ABCE15B604CBCA00BA000BD1007F0DCF XMT 1185 B033FBCB09B5D90BFF46BD100B034ABCB09B5D90BFF32BCE15B000DB604DBCE007F0D7F XMT 1186 BCE1FBCA00BA000BD100B0329BCB09B5C90BFF14BD100B0334BCB09B5C90BFF007F0FEF XMT 1187 BCE15B604CB2024B6020B202FB602BBCA00BA000BD100B033FBCB09B5D90BFF3C7F12BF XMT II88 BD100B034ABCB09B5D90BFF2BBCE15B000EB604DBCE00BCE1FBCA00BA000BD1007F0EAF XMT II89 B0329BCB09B5D90BFF5ABD100B0334BCB09B5D90BFF46BCE15B604CBCA00BA0007F0EAF XMT 1190 BD100B033FBCB09B5D90BFF32BD100B034ABCB09B5D90BFF1EBCE15B000FB604D7F0DCF XMT II91 BCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF50BD100B0334BCB09B5D907F100F XMT 1192 BFF3CBCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF28BD100B034ABCB097F0DBF EPII TMX B5D90BFF14BCE15B0010B604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D907F100F XMT 1194 BFF46BD100B0334BCB09B5D90BFF32BCE15B604CBCA00BA000BD100B033FBCB097F0FAF XMT 1195 B5D90BFF1EBD100B034ABCB09B5D90BFF0ABCE15B0011B604DBCE00BCE1FBCA007F0BBF BA000BD100B0329BCB09B5D90BFF3CBD100B0334BC709B5D90BFF28BCE15B604C7F0F9F XMT II97 BCA00BA000BD100B033FBCB09B5C90BFF14BD100B 134 ABCB09B5C90BFF00BCE157F0F3F XMT 1198 B0012B604DB203AB6036B2045B6041BCE00BCE1FBCA00BA000BD100B0329BCB097F166F XMT II99 B5D90BFF32BD100B0334BCB09B5D90BFF1EBCE15B604CBCA00BA000BD100B033F7F0FAF XMT 1100 BCB09B5D90BFF5ABD100B034ABCB09B5D90BFF46BCE15B0013B604DBCE00BCE1F7F0B3F XMT 1101 BCA00BA000BD100B0329BCB09B5D90BFF28BD100B0334BCB09B5D90BFF14BCE157F103F XMT 1102 B604CBCA00BA000BD100B033FBCB09B5D90BFF50BD100B034ABCB09B5D90BFF3C7F0ECF EOII TMX BCE15B0014B604DBCE00BCE1FBCA00BA000BD100B0329BCB09B5D90BFF1EBD1007F0FBF XMT 1104 B0334BCB09B5D90BFF0ABCE15B604CBCA00BA000BD100B033FBCB09B5D90BFF467F0E1F XMT I105 BD100B034ABCB09B5D90BFF32BCE15B0015B604DBCE00BCE1FBCA00BA000BD1007F0FEF XMT 1106 B0329BCB09B5C90BFF14BD100B0334BCB09B5C90BFF00BCE15B604CB2024B60207F12CF XMT 1107 B202FB602BBCA00BA000BD100B033FBCB09B5D90BFF3CBD100B034ABCB09B5D907F106F XMT 1108 BFF28BCE15B0016B604DBCE00BCE1FBFF80B0184BE54CBE64DBE74DBCE26B00007F0B6F XMT I109 BFFFEB000BBFFDDB0065BFD64BFF49B003DBFFEBB0005B000B0001BFFFEB00077F0ACF XMT 1110 BFFE7BFCC1B001BBFFF9B0002BFFFFB0000B0005BFFEDB0037BFF50BFE77B00787F095F XMT 1111 BFFD7B000DBFFFDB0000B0003BFFF5B001FBFF93B011BB0014BFFFBB0002B00007F10AF XMT 1112 BO001BFFFAB0016BFFBEB00E0B0285BFF89B0029BFFF3B0003B0002BFFF3B002E7F0EFF XMT 1113 BFF7CB0220B01E0BFF7AB002FBFFF3B0002B0002BFFF8B001ABFFB6B01D8B002B7F0D9F XMT 1114 BFFE4B0009BFFFEB0000BFFFFB0006BFFECB003ABFFC3BFF13B0043BFFE9B00077F07AF XMT I115 BFFFBFFFEB000BBFFDDB0065BFD64BFF49B003DBFFEBB0005B0000B0001BFFFE7F05BF BOOO7BFFE7BFCC1B001BBFFF9B0002BFFFFB0000BFFE5BFFD7BFFCABFFBFBFFB67EFF6F XMT I117 BFFB1BFFAEBFFAFBFFB2BFFB9BFFC3BFFCEBFFDCBFFEBBFFFBB000BB001BB00297EFB4F XMT 1118 B0036B0041B004AB004FB0052B0051B004EB0047B003DB0032B0024B0015B00057F214F XMT 1119 BFFF5BFFFB0001BFFFFB0001BFFFFB0001BFFFFB0001BFFFFB0001B0000B00017F0AAF XMT 1120 BFFFFBFFFB0001B0001BFFFFBFFFFB0001B0000B0001BFFFFB0001BFFFFB00017F099F XMT 1122 BFFFFB0001BFFFFB0001BFFFFB0000B0000BFFFFB0001BFFFFB0000BFFFFB00017F09BF ESII TMX BFFFFB0000BFFFFB0000B0001B0000BFFFFB0000B0001B0000BFFFFB0000B00017F14CF XMT 1124 B0000B0000B0000BFFFFB0001B0000B0000BFFFFB0001B0000B0000BFFFFB00007F1A5F XMT 1125 BFFFFB0001B0000B0001BFFFFB0001B0000B0001BFFFFB0001B00007F3A6F XMT 1126 XMT II.5 08-25-87 10:15:36 . ASM32020 PC 1.0 86.036 XMT 1127

I claim as my invention:

1. A method of transmitting a quadrature amplitude modulated signal comprising the steps of:

quadrature modulating first and second signals onto a first subcarrier, quadrature modulating third and 5 fourth signals onto a second subcarrier,

quadrature modulating said first and second quadrature modulated subcarriers onto a carrier, and transmitting said quadrature modulated carrier,

2. A method of transmitting a quadrature amplitude 10 modulated signal comprising the steps of;

quadrature modulating first and second signals onto a first subcarrier

quadrature modulating third and fourth signals onto a second subcarrier,

providing a DC component with one of said quadrature modulated subcarriers for producing a pilot carrier,

quadrature modulating said quadrature first and second quadrature modulated subcarriers onto a carrier, and

transmitting said quadrature modulated carrier.

- 3. A method of transmitting quadrature amplitude modulated signal as defined in claim 1, comprising the further step of providing a bit sync signal with one of 25 said quadrature modulated subcarriers.
- 4. A method as defined in claim 3, in which the signals are digital signals having a predetermined bit rate and the bit sync signal has a frequency that is an integral multiple of said bit rate.
- 5. A method of transmitting a quadrature amplitude modulated signal, comprising:

reading from memory first and second prototype pulses each including a subcarrier component,

summing said first and second prototype pulses to produce a first quadrature modulated subcarrier,

reading from memory third and fourth prototype pulses each including a subcarrier component,

summing said third and fourth prototype pulses to produce a second quadrature modulated subcarrier,

quadrature modulating a carrier with said first and second quadrature modulated subcarriers, and transmitting said quadrature modulated carrier.

6. A method of transmitting a quadrature amplitude modulated signal comprising:

reading from memory first and second prototype pulses each including a subcarrier component,

summing said first and second prototype pulses to produce a first quadrature modulated subcarrier,

reading form memory third and fourth prototype pulses each including a subcarrier component,

summing said third and fourth prototype pulses to produce a second quadrature modulated subcarrier,

quadrature modulating a carrier with said first and second quadrature modulated subcarriers,

summing an offset with one of said summed pulses prior to quadrature modulating said carrier, and transmitting said quadrature modulated carrier,

7. A method of transmitting a quadrature amplitude modulated signals defined in claim 5 including the further step of summing a sync signal with one of said summed pulses prior to quadrature modulating said carrier.

8. An apparatus for transmitting quadrature modulated signals comprising:

means for quadrature modulating first and second signals on a first subcarrier,

means for quadrature modulating third and fourth signals onto a second subcarrier,

means for quadrature modulating said first and second subcarriers onto a carrier, and

means for transmitting said quadrature modulated carrier.

9. An apparatus for transmitting quadrature modulated signals comprising:

means for quadrature modulating first and second signals on a first subcarrier,

means for quadrature modulating third and fourth signals onto a second subcarrier,

means for summing a sync signal with one of said subcarriers,

means for quadrature modulating said first and second subcarriers onto a carrier, and

means for transmitting said quadrature modulated carrier.

10. An apparatus as defined in claim 9, in which a processor means is used for quadrature modulating said first and second signals and said third and fourth signals.

11. An apparatus as defined in claim 10, in which said processor means includes a memory means containing a prototype pulse having a subcarrier component, and said first and second subcarriers produced by summing prototype pulses in said microprocessor means.

50

55

60