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Tang

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[45] **Date of Patent: Dec. 16, 1986**

[54] CASCADE WAVEGUIDE TRIPLE-MODE FILTERS USEABLE AS A GROUP DELAY EQUALIZER

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[73] Assignee: **Com Dev Ltd.**, Cambridge, Canada

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[51] **Int. Cl.⁴** **H01P 1/208; H04B 3/14**
[52] **U.S. Cl.** .... **333/28 R**; 333/212
[58] **Field of Search** .... 333/208, 209, 212, 202, 333/227, 28 R

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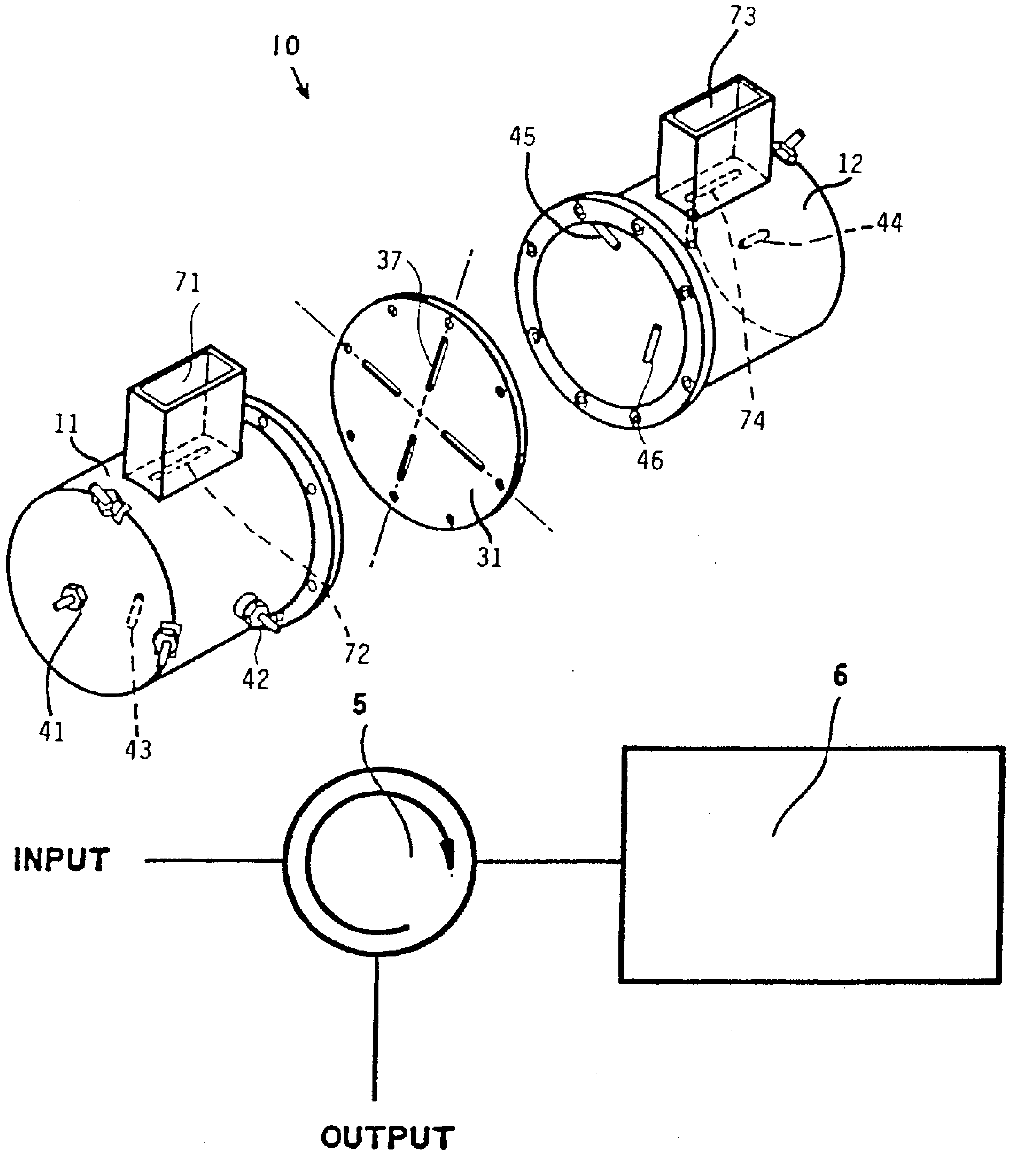
Assistant Examiner—Benny T. Lee
Attorney, Agent, or Firm—Daryl W. Schnurr

[57] ABSTRACT

A bandpass filter has a plurality of cascade wave-guide cavities each resonating in three independent orthogonal modes. The cavities can be cylindrical or have a square cross-section. Where the cavities are circular, each cavity resonates in TE_{111} or TE_{010} modes simultaneously. Where the cavities have a square cross-section, each cavity resonates in TE_{011} and TM_{110} modes simultaneously. Between each triple-mode cavity, there is located an iris having an aperture with four separate radial slots that are offset from a center of the iris. The filter is capable of producing an elliptic function response. In a variation of the invention, an allpass filter has an output that is short circuited and, when used in conjunction with a circulator, it functions as a group delay equalizer. Previous triple-mode filters are not capable of producing an acceptable result relative to dual-mode filters.

24 Claims, 17 Drawing Figures



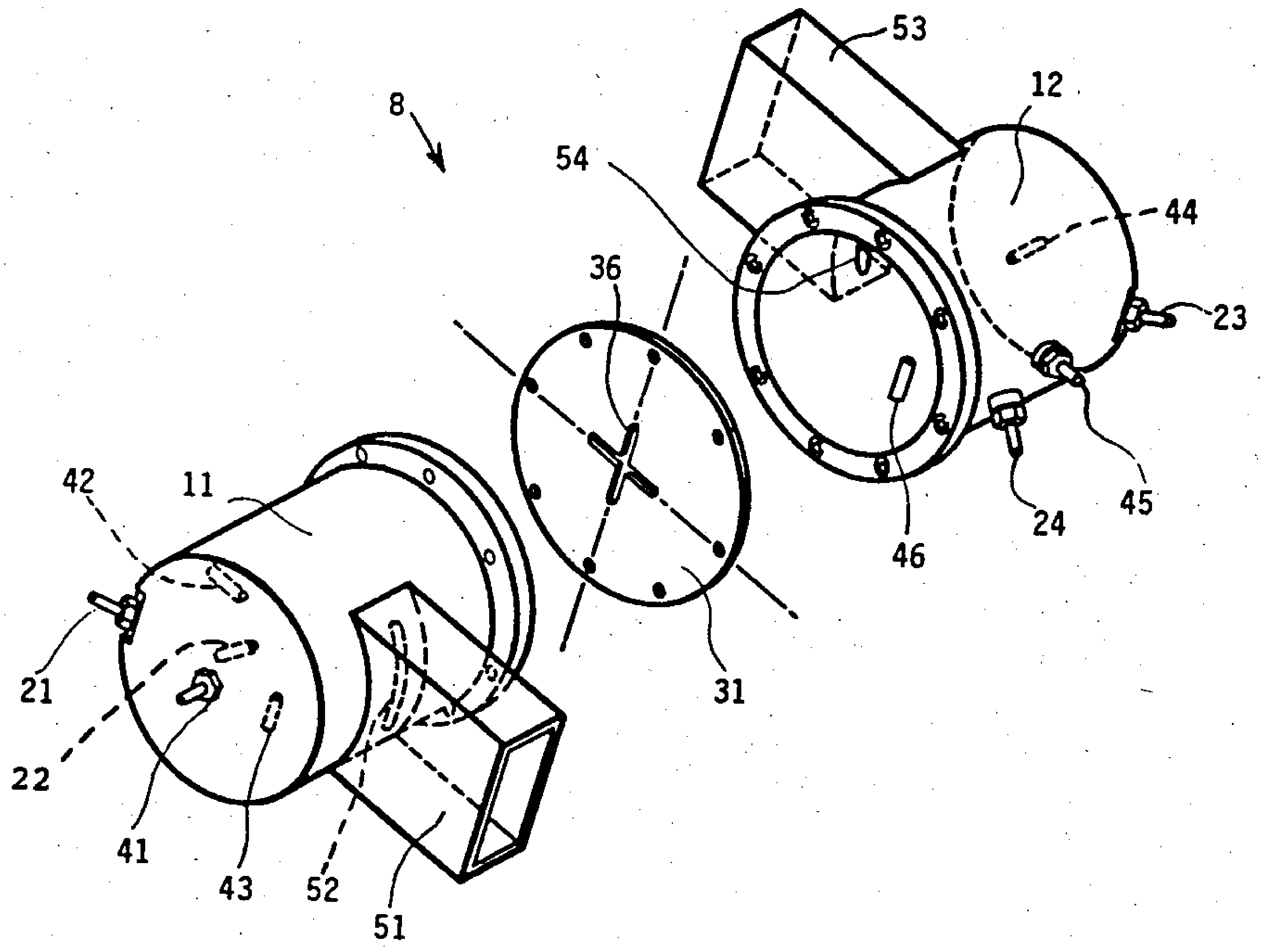


FIGURE 1.

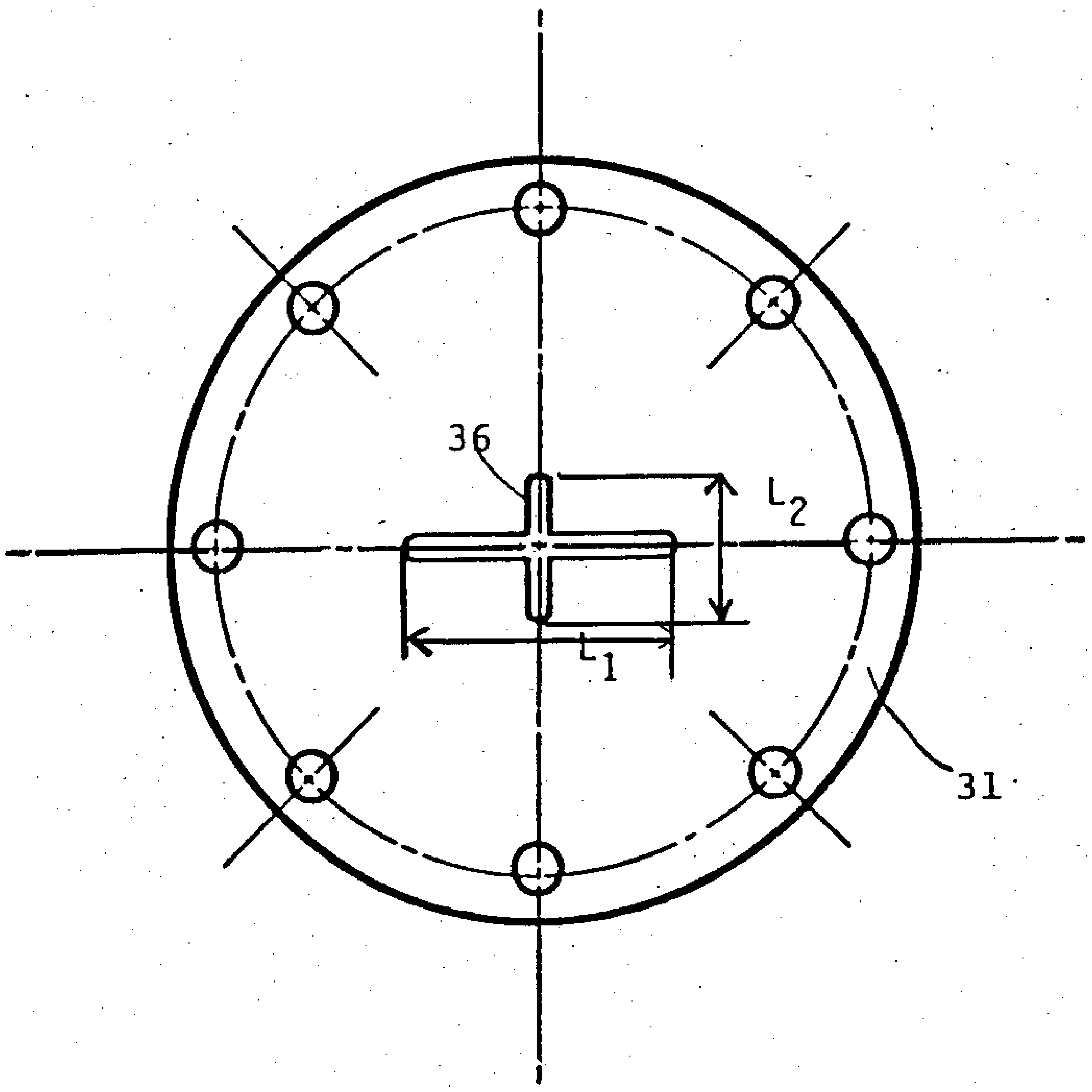


FIGURE 1A

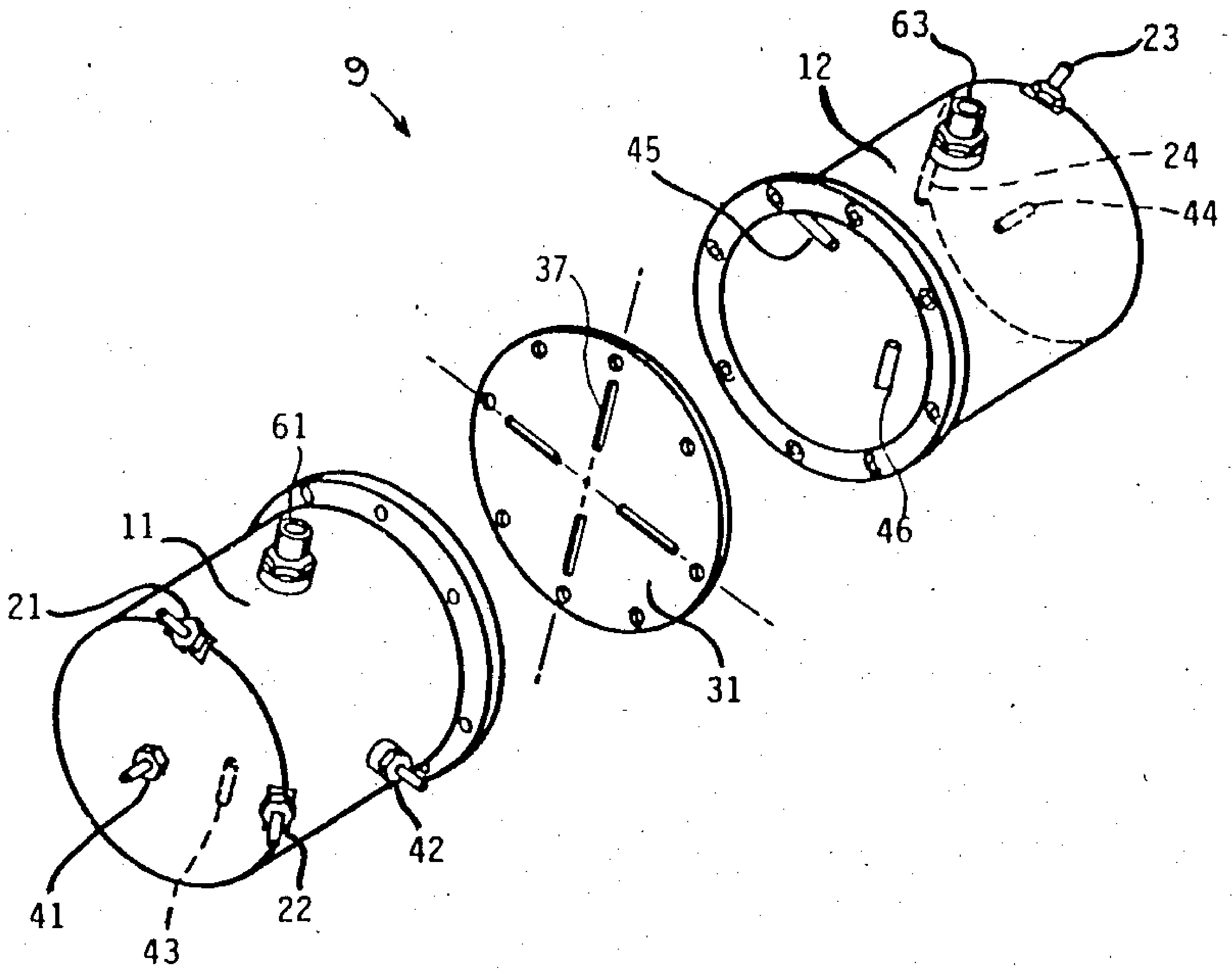


FIGURE 2.

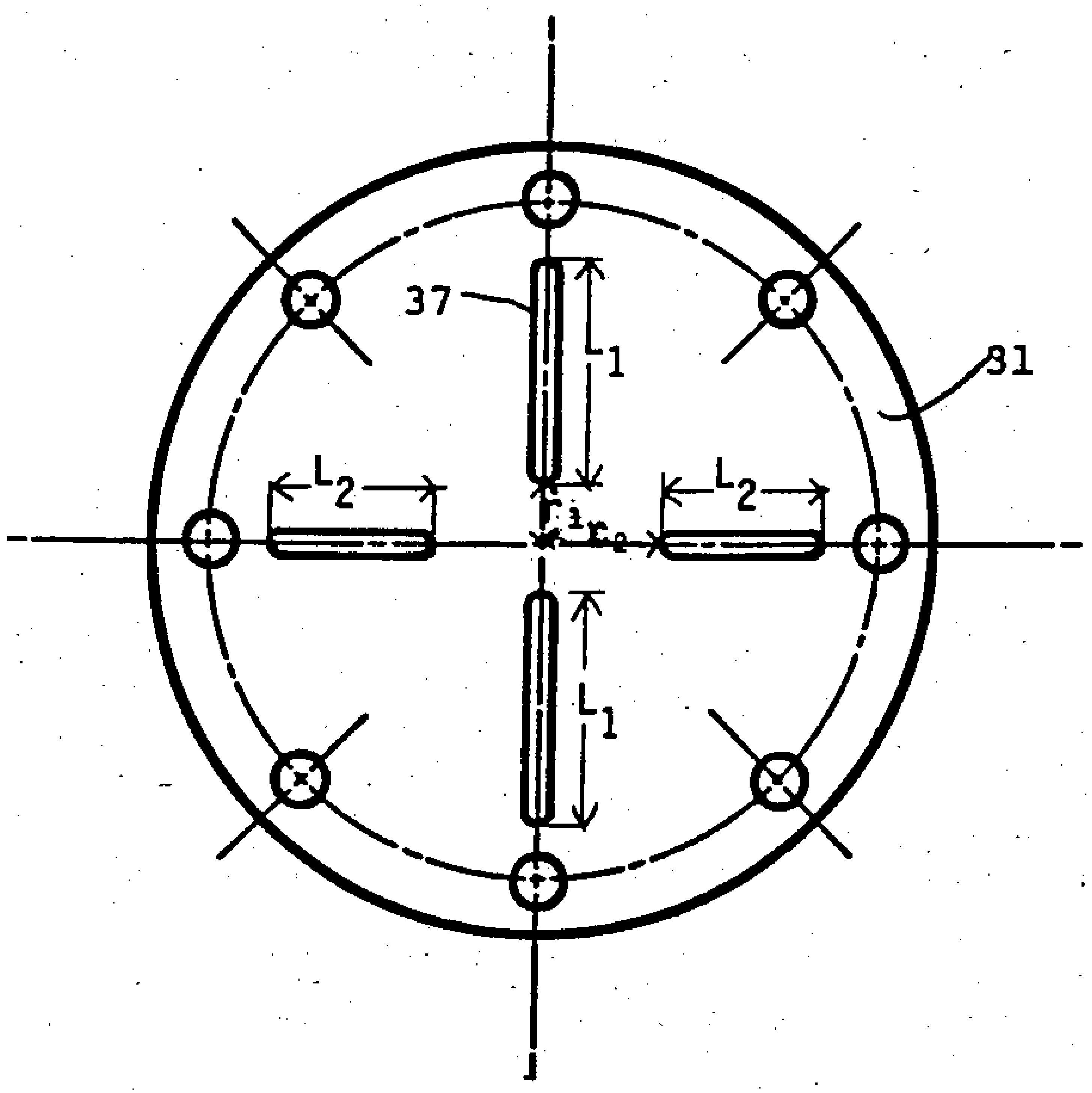


FIGURE 2A

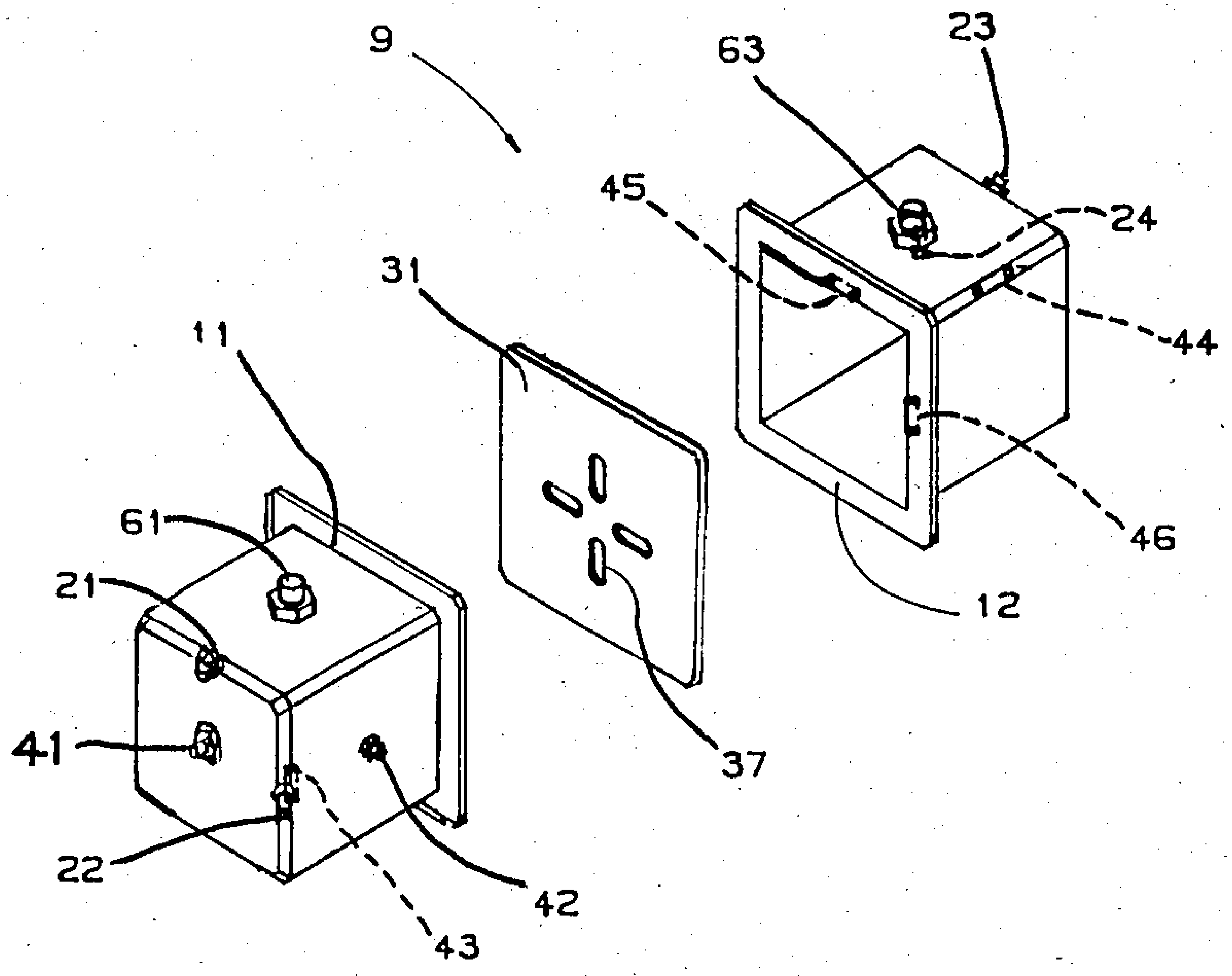


FIGURE 2B

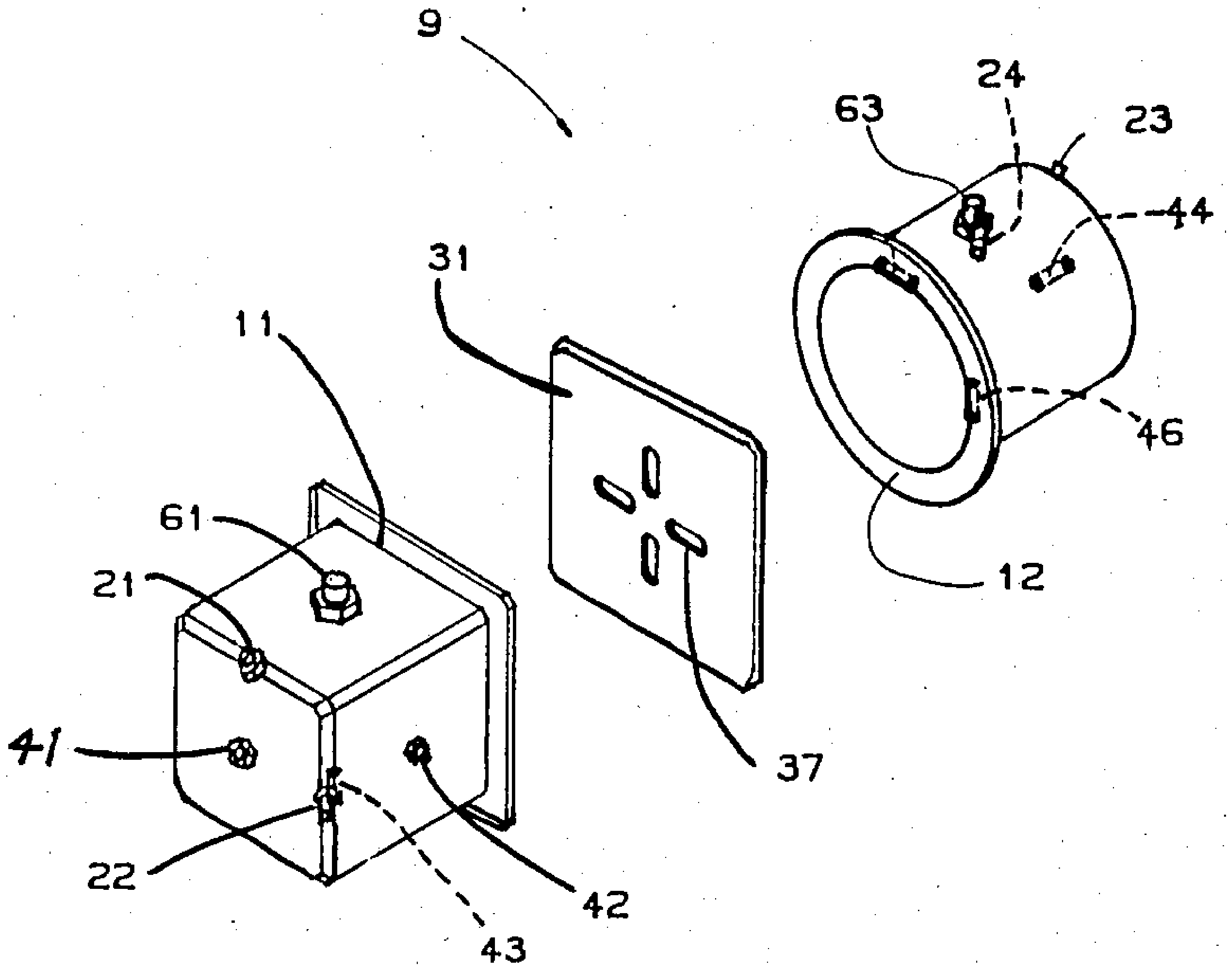


FIGURE 2C

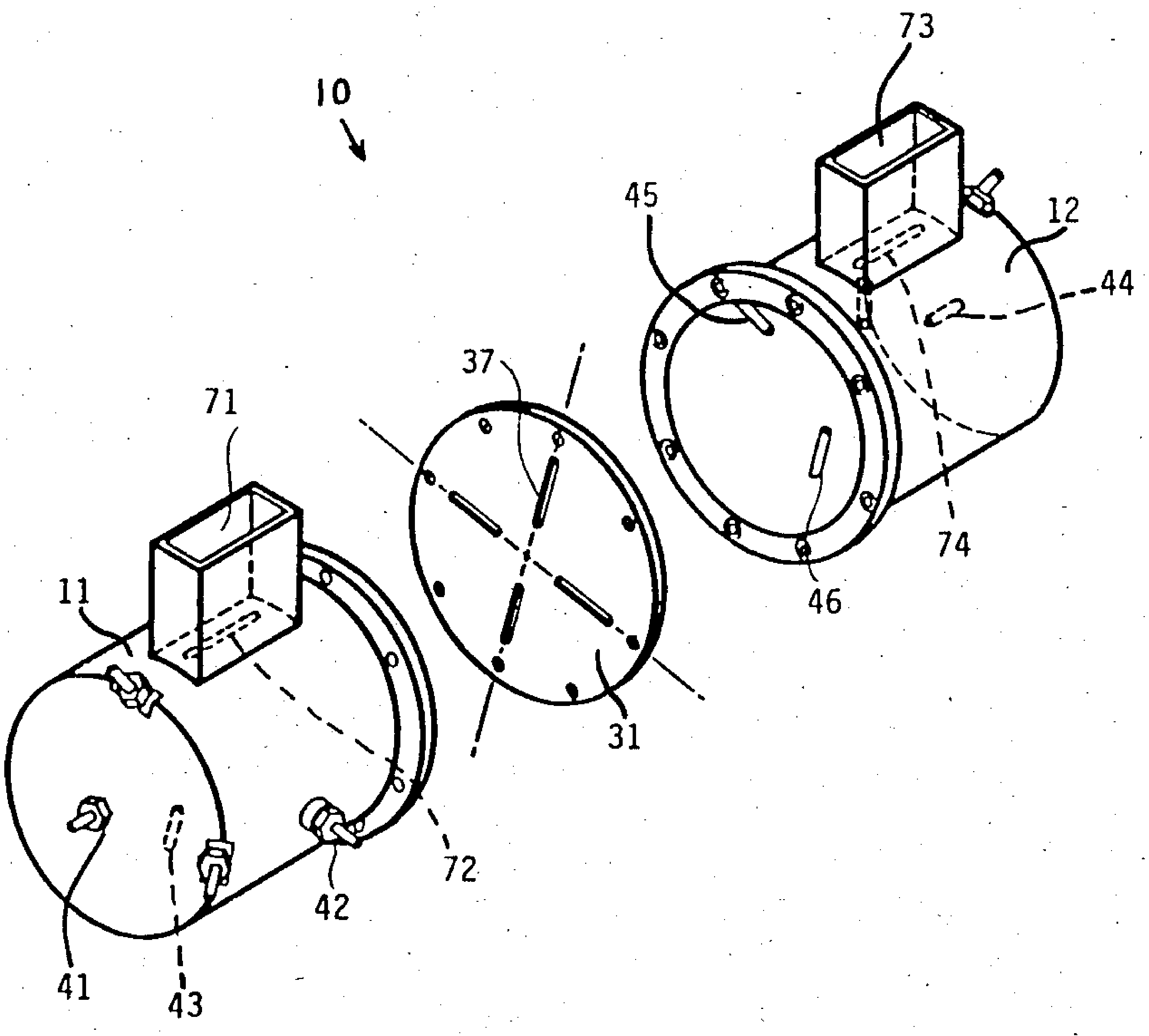


FIGURE 3.

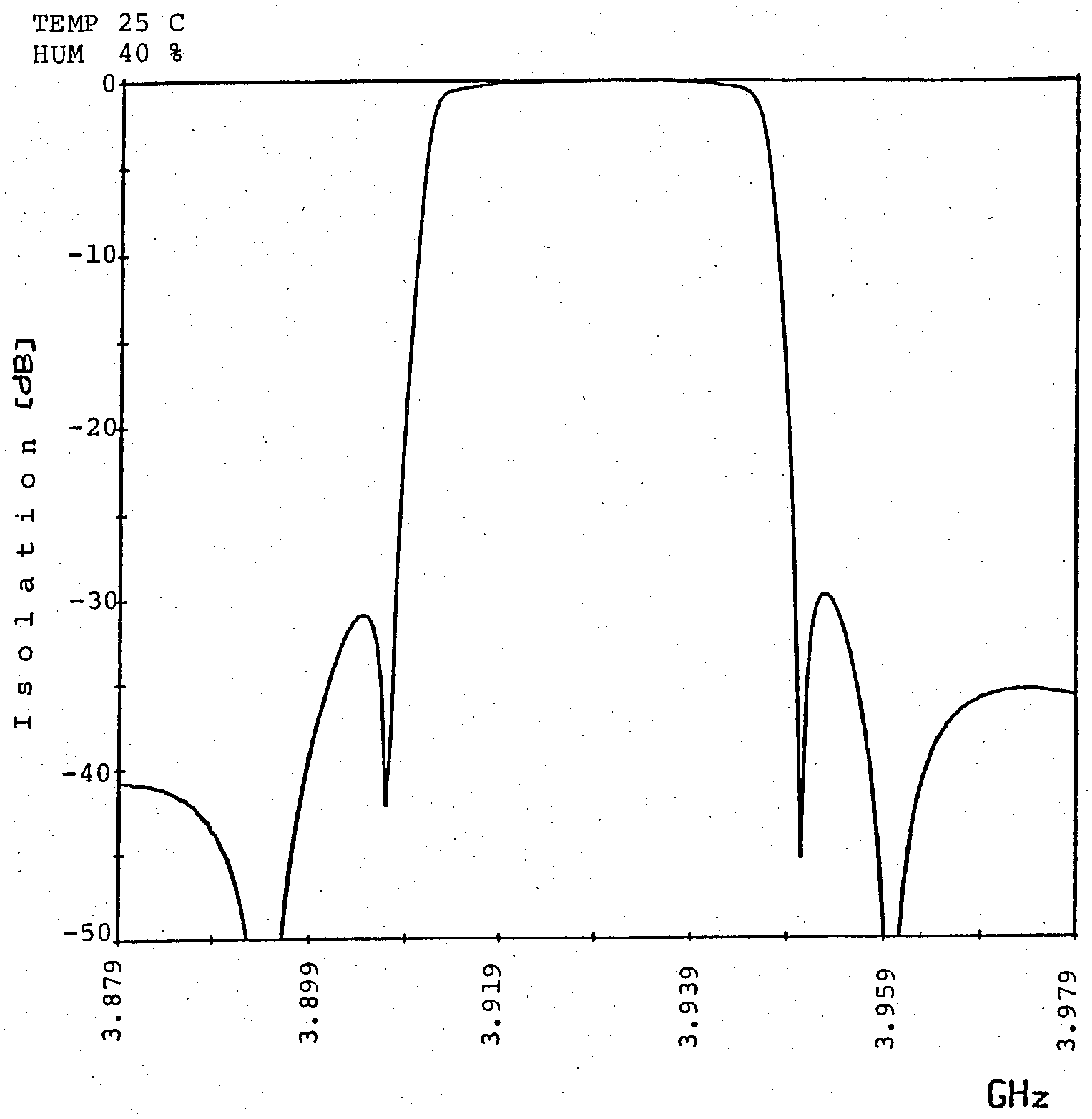

TEMP 25 C
HUM 40 %
0
-10
-20
-30
-40
-50
Isolation [dB]
3.879
3.899
3.919
3.939
3.959
3.979
GHz

FIGURE 4A

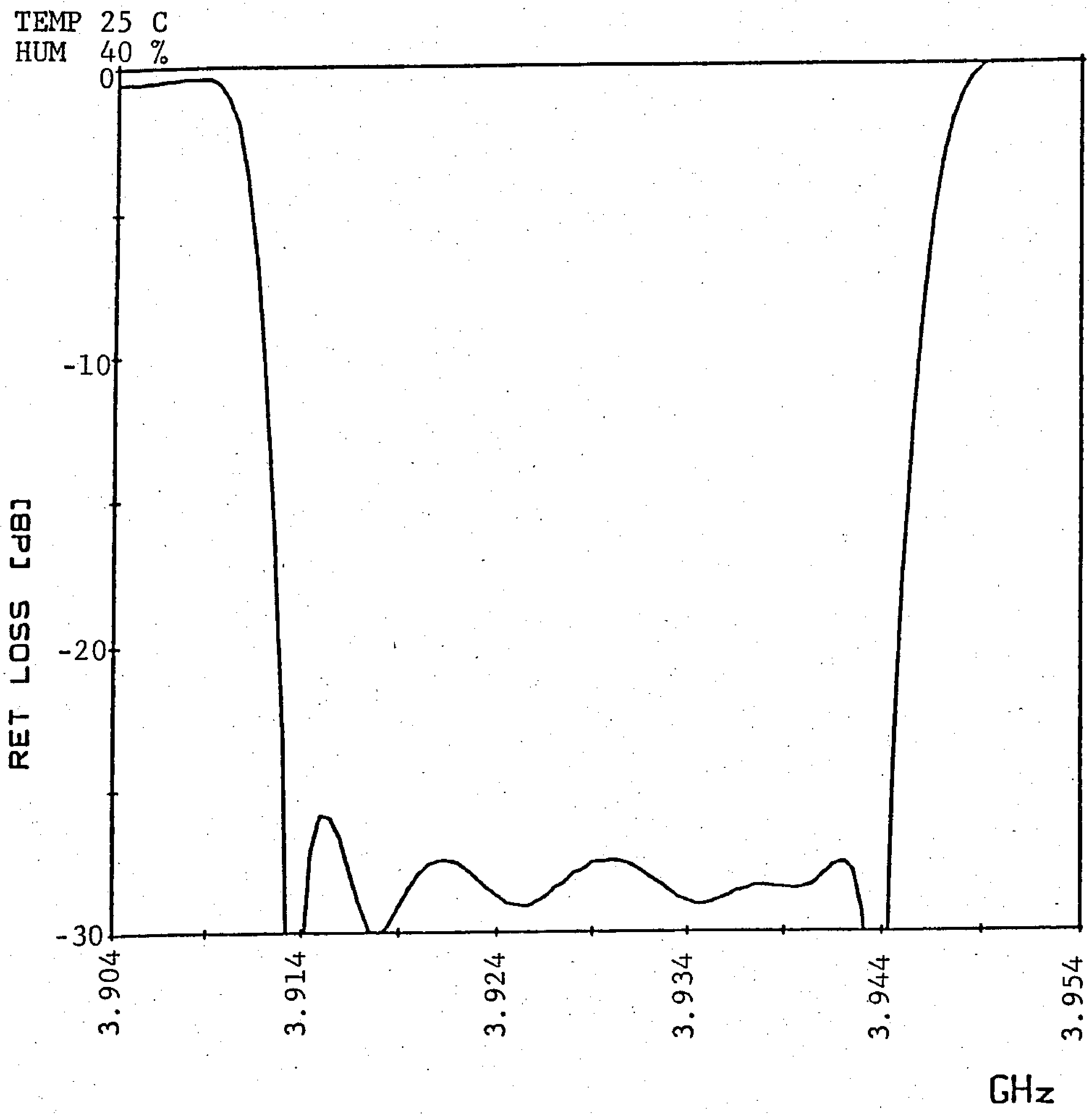

TEMP 25 C
HUM 40 %
0
-10
-20
-30
RET LOSS [dB]
3.904
3.914
3.924
3.934
3.944
3.954
GHz

FIGURE 4B

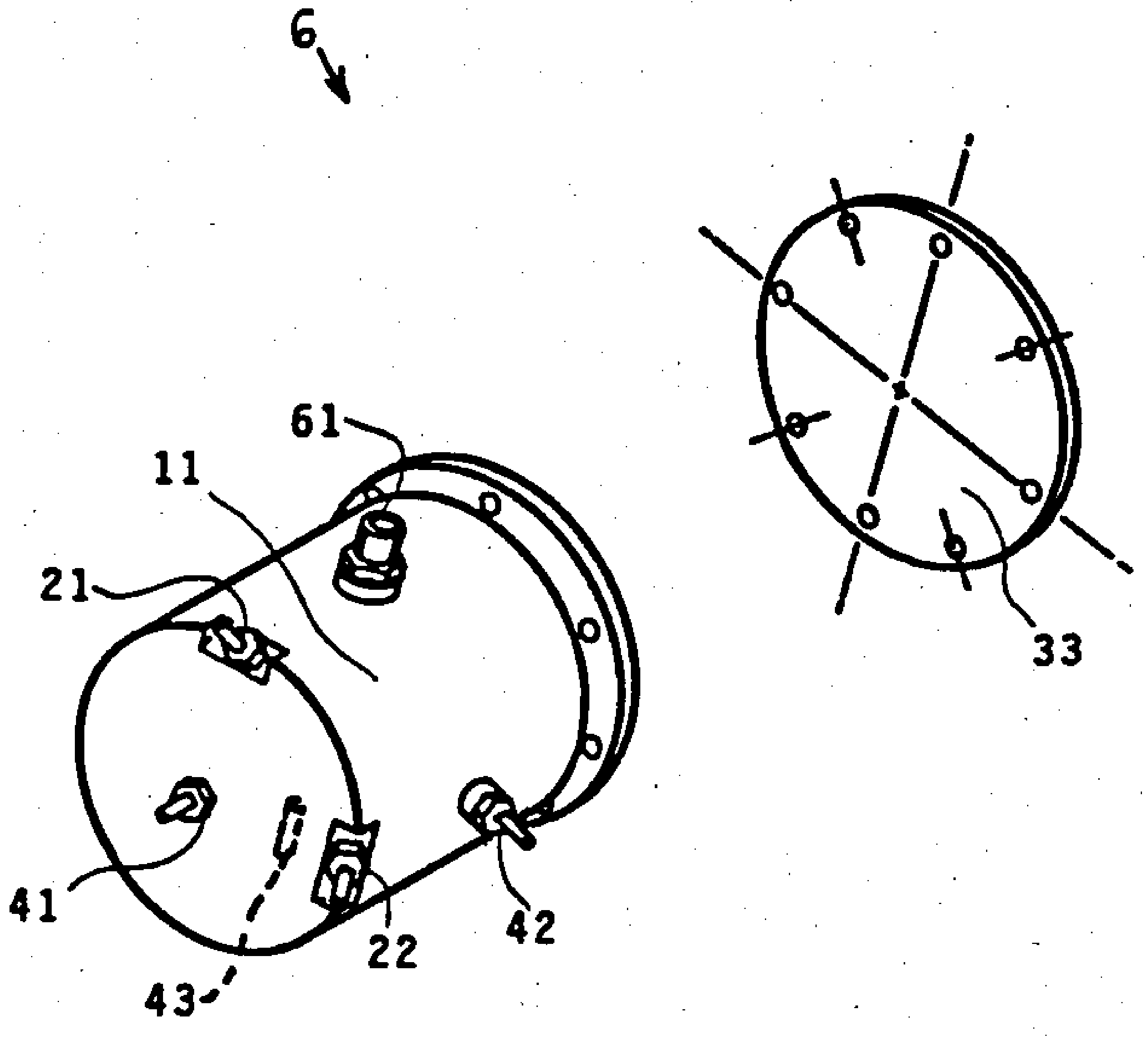


FIGURE 5A

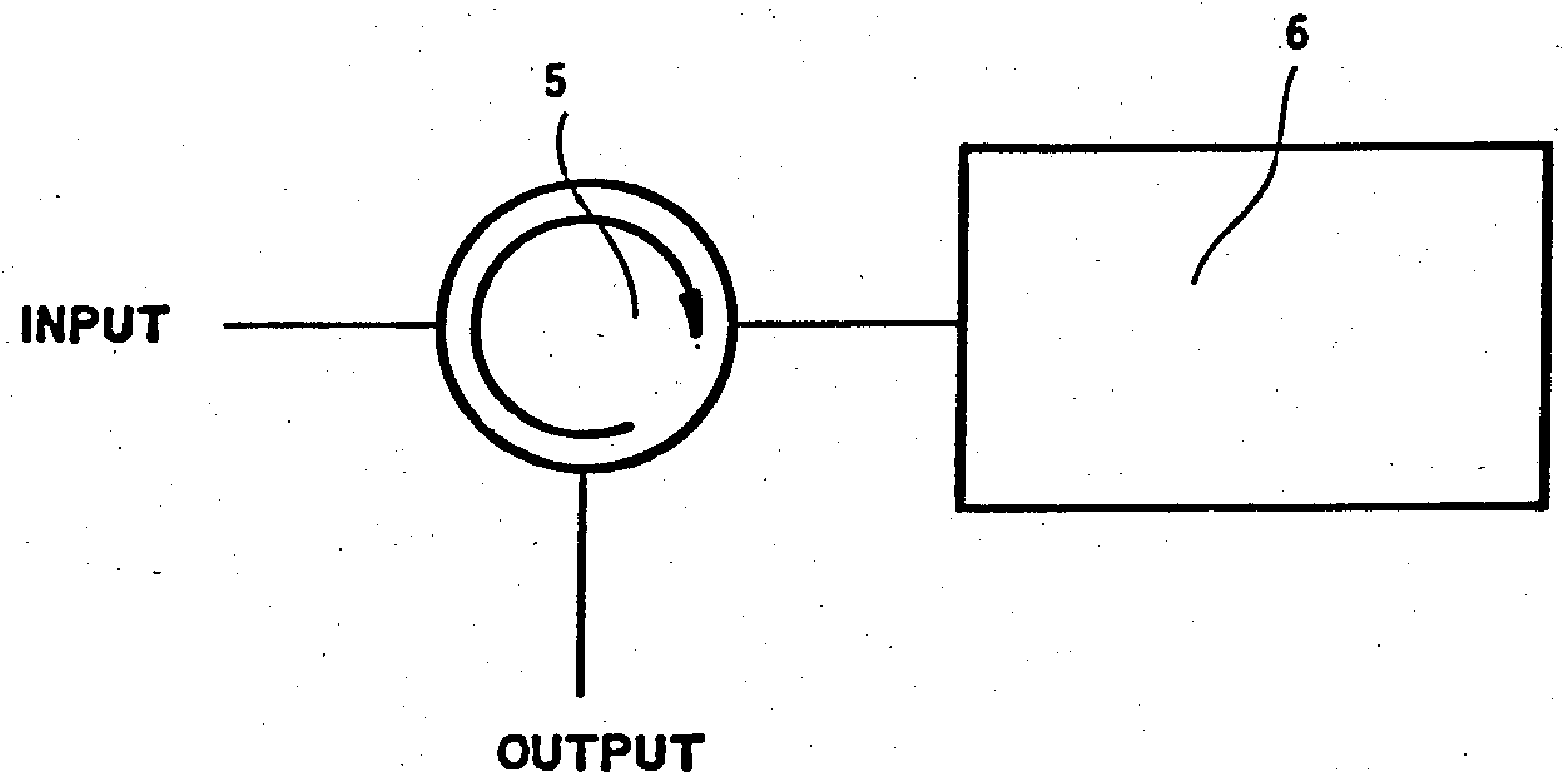


FIGURE 5B

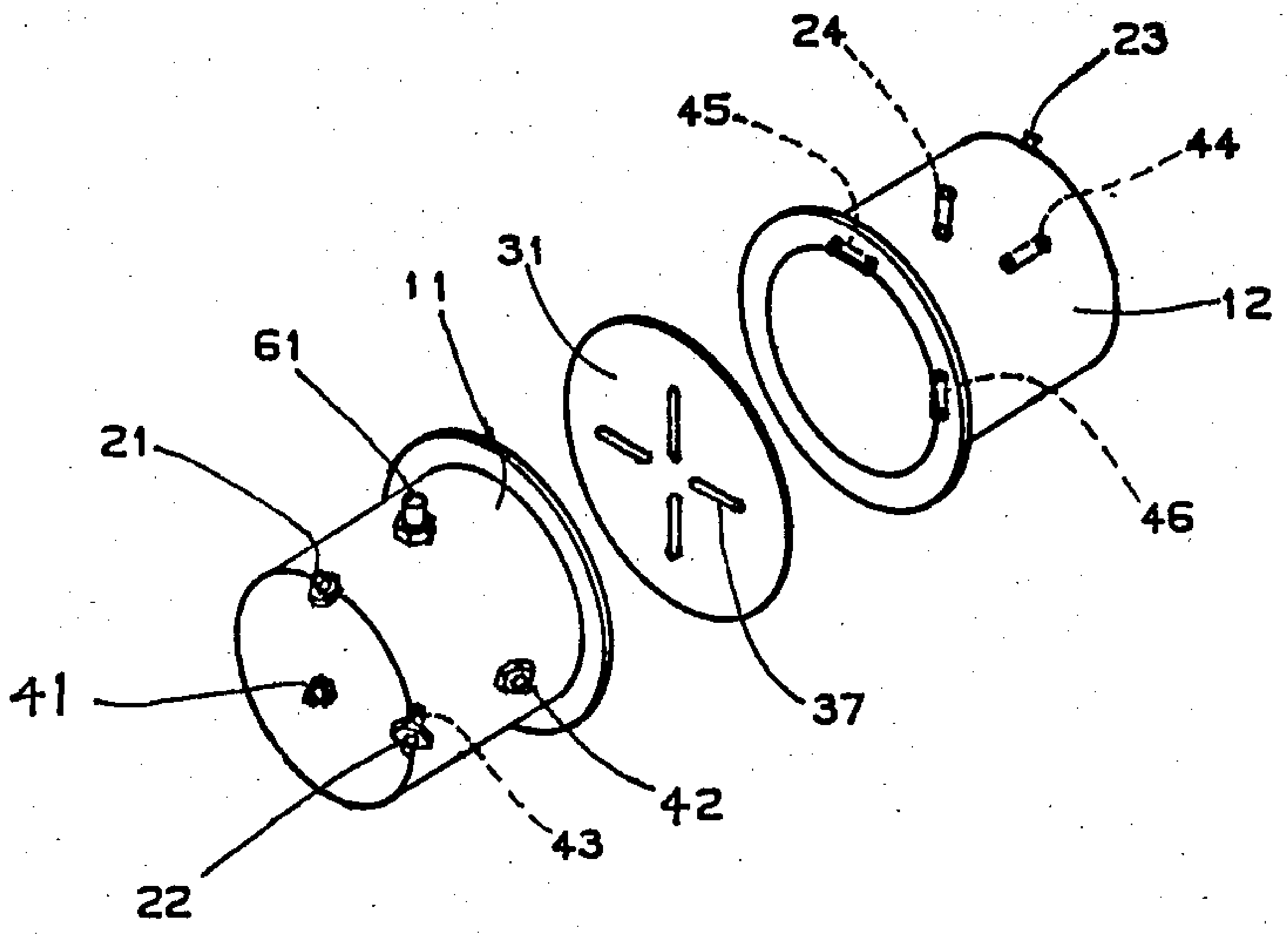


FIGURE 5C

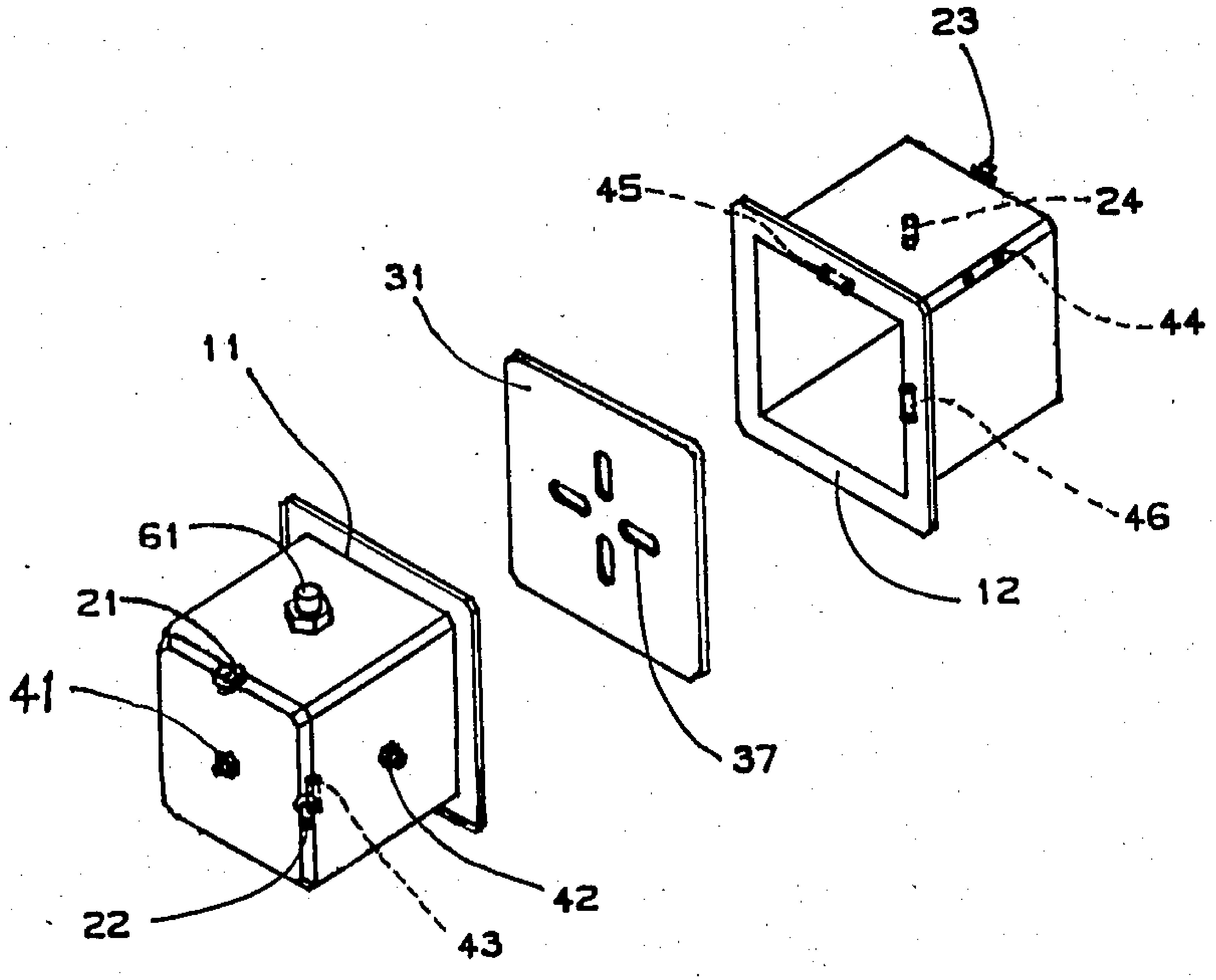


FIGURE 5D

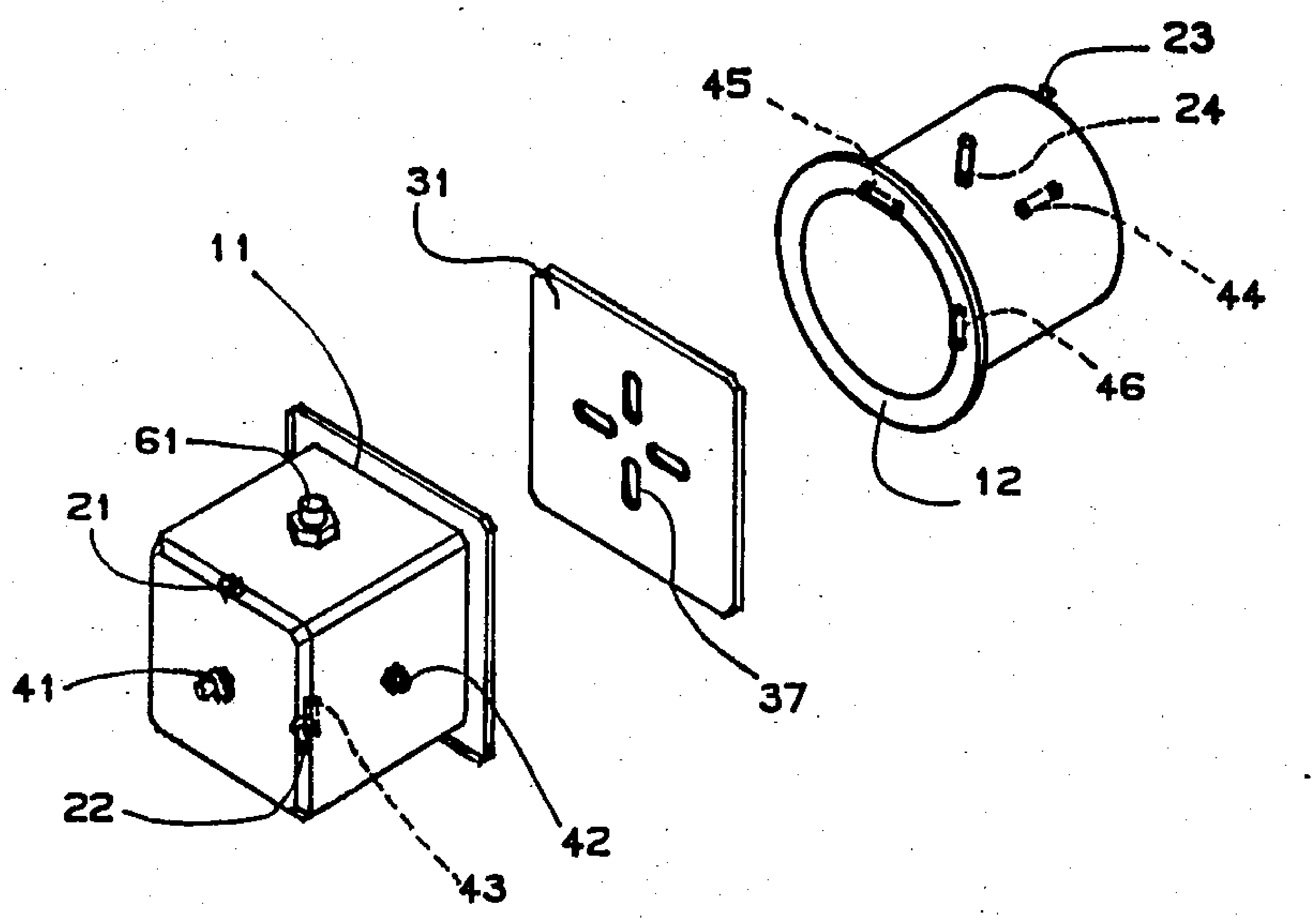


FIGURE 5E

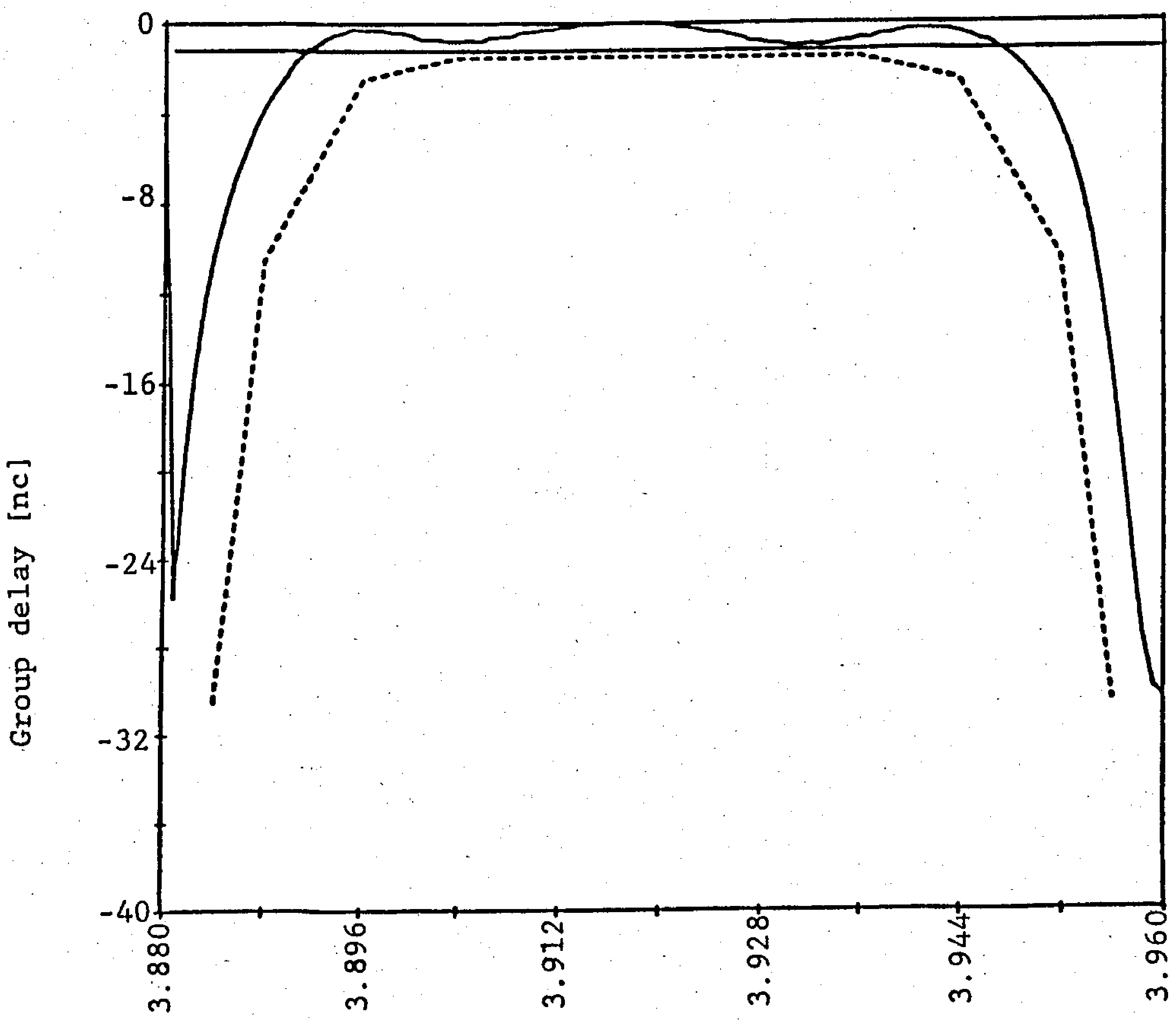


FIGURE 6A

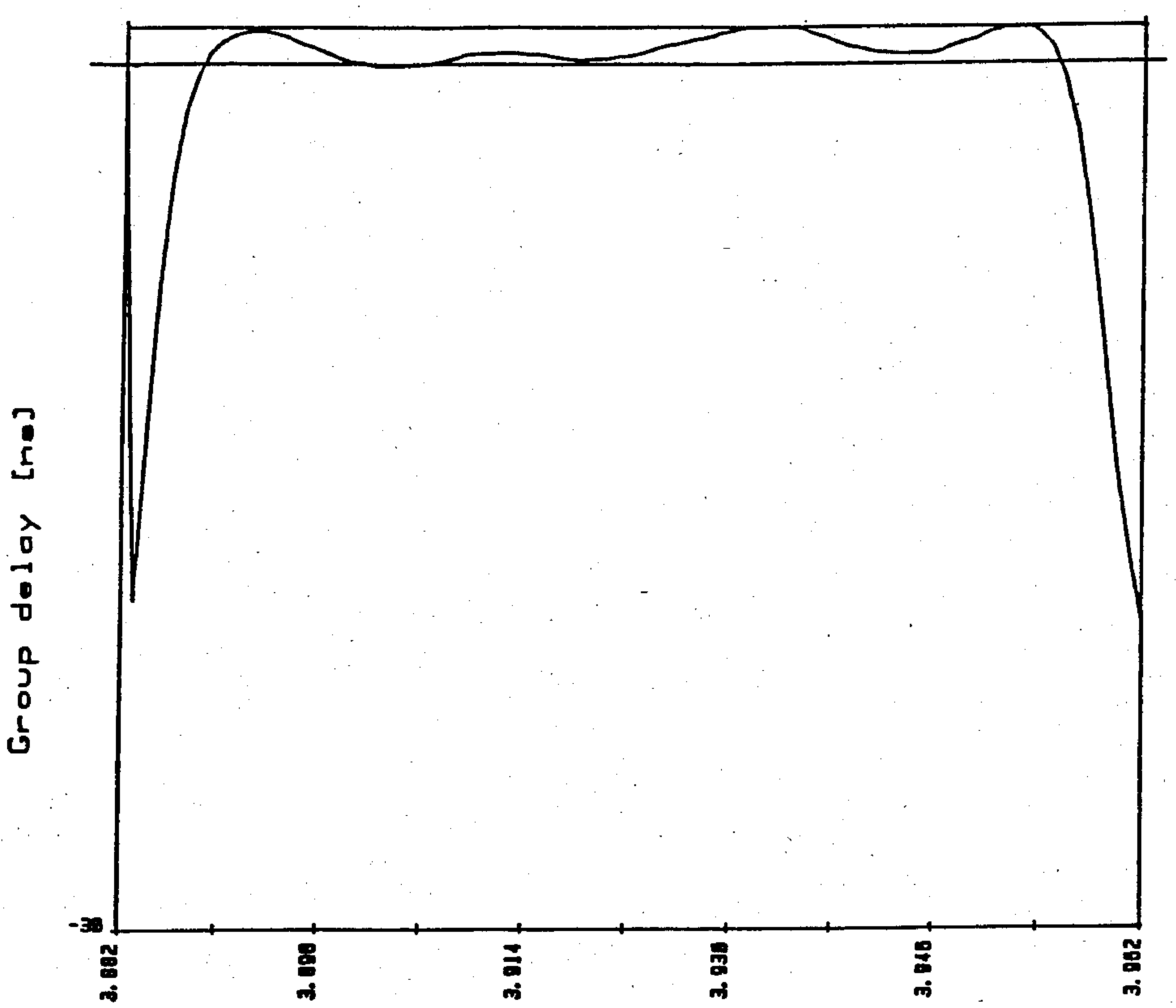


FIGURE 6B

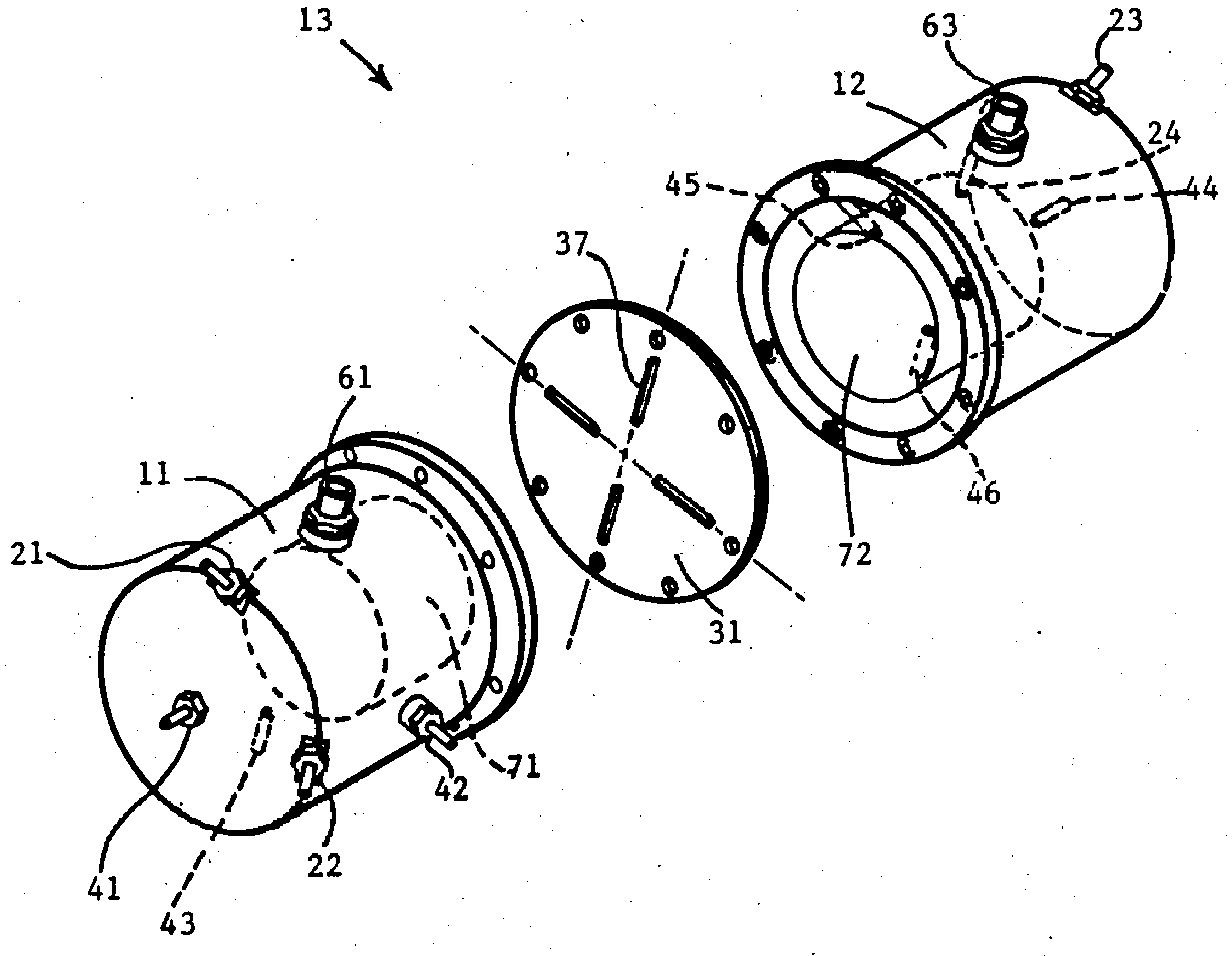


FIGURE 7

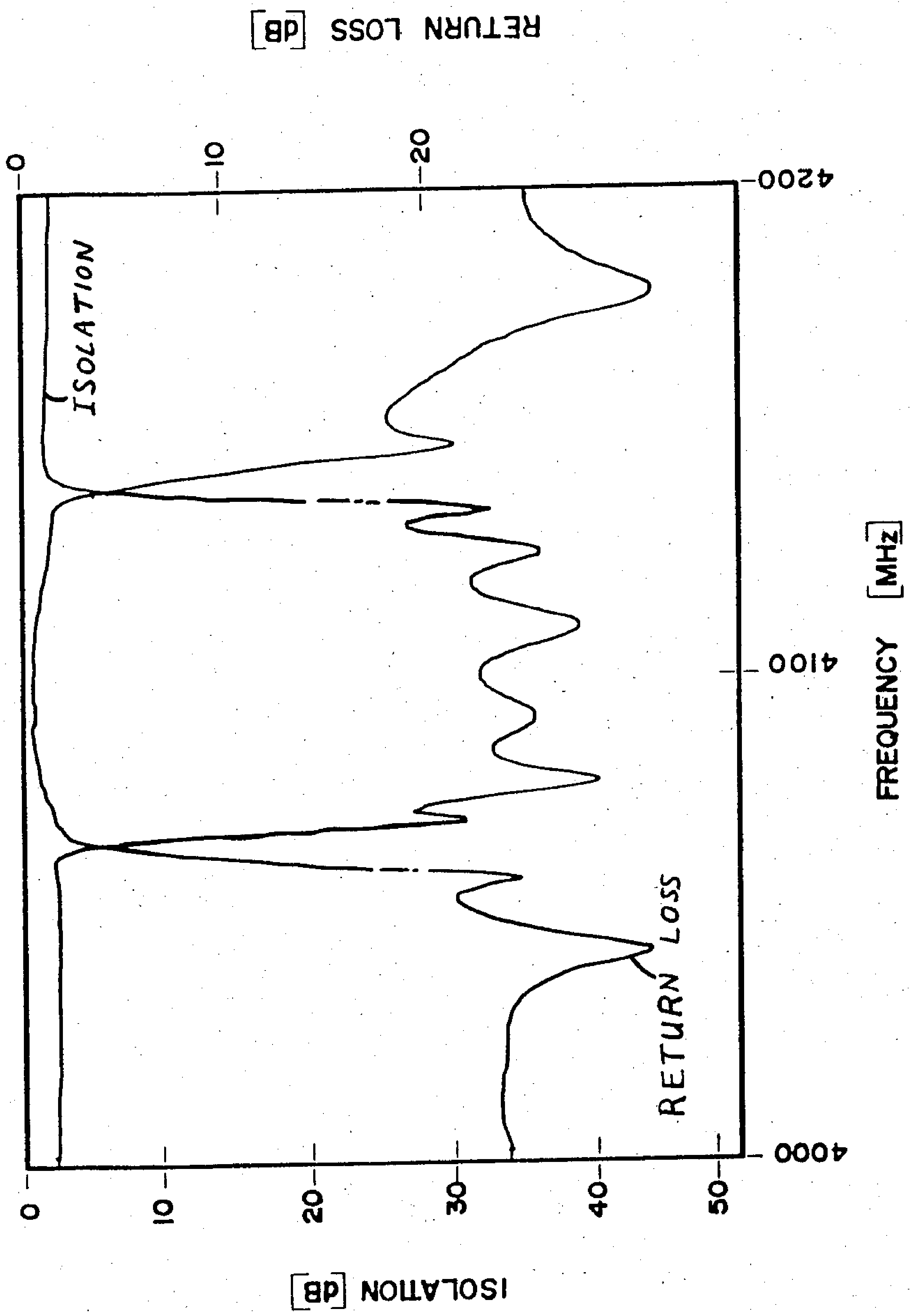

RETURN LOSS [dB]
0
10
20
ISOLATION
RETURN LOSS
ISOLATION [dB]
0
10
20
30
40
50
4000
4100
4200
FREQUENCY [MHz]

Figure 8

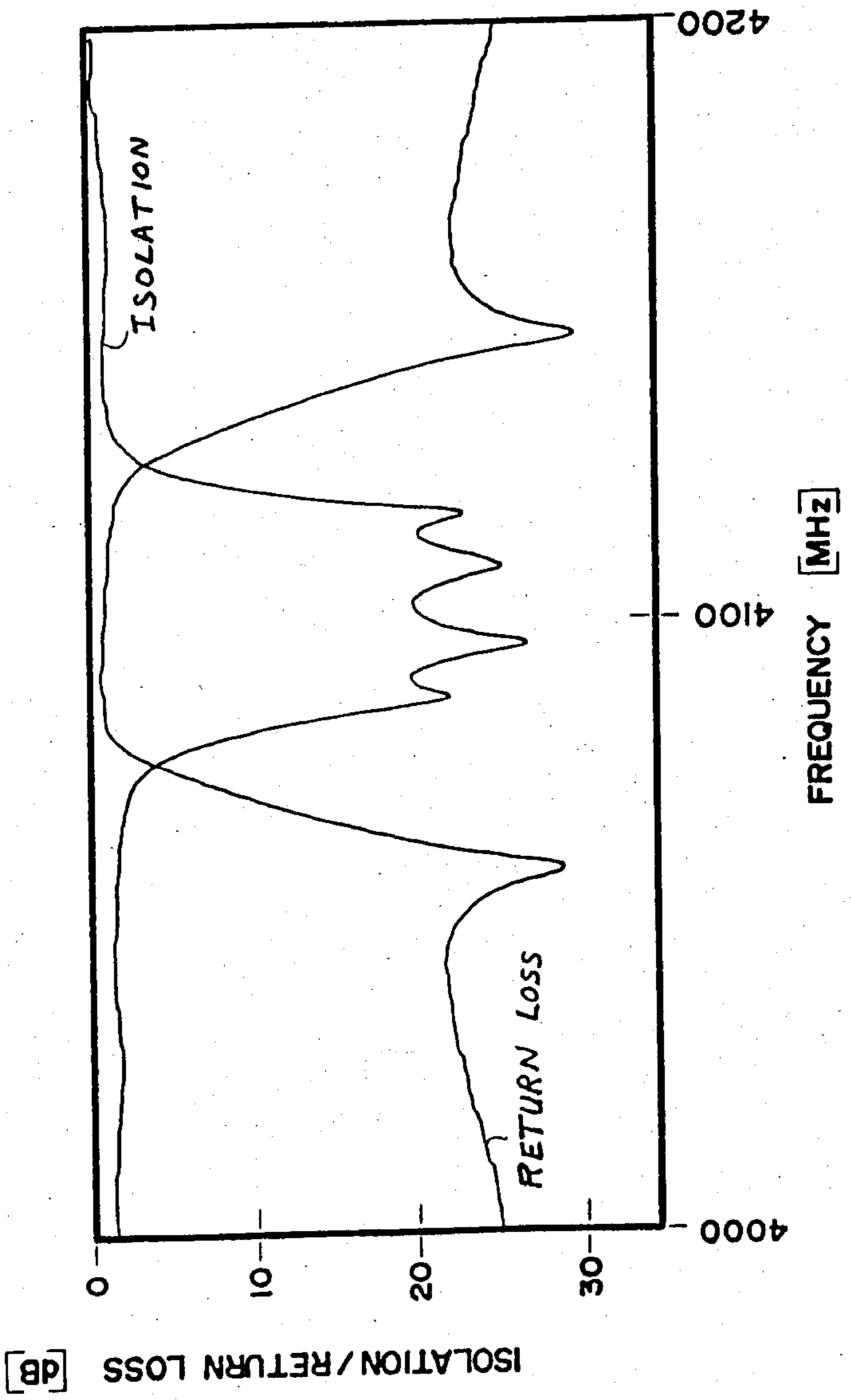

ISOLATION
RETURN LOSS
0
10
20
30
ISOLATION/RETURN LOSS [dB]
4000
4100
4200
FREQUENCY [MHz]

Figure 9

CASCADE WAVEGUIDE TRIPLE-MODE FILTERS USEABLE AS A GROUP DELAY EQUALIZER

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates to a triple mode filter and to a method of operating such a filter. In particular this invention relates to a filter having a cascade waveguide cavity resonating in first, second and third independent orthogonal modes simultaneously.

2. Description of the Prior Art

It is known to have a triple mode waveguide cavity filters. In COMSAT Technical Review, Volume 1, pages 21 to 42, published in the Fall of 1971, Atia and Williams suggested the possibility of cascading two triple mode waveguide cavities to realize a six pole elliptic filter function response. In theory, triple mode filters have an advantage over dual mode filters in that they produce economies in weight, volume and cost because of the realization of three electrical cavities in one physical cavity. However, previous triple mode filters have been unable to achieve acceptable results and, in particular, have failed to realize an elliptic function response. Also, previous triple mode filters have had input or output coupling means that are too complex or too heavy; or the filters have been too inefficient to compete with dual mode filters; or the intercavity coupling could not be adequately controlled. As previous triple mode filters did not produce the expected results, they are not widely used and the dual mode filter is now the dominant filter for use in satellites and multi-plexers. The communications satellite industry has long sought a solution to the problems related to previous triple mode filters.

It is an object of the present invention to provide a triple-mode filter that produces acceptable results and is lighter in weight and smaller in volume than comparable dual-mode filters.

SUMMARY OF THE INVENTION

A bandpass filter in accordance with the present invention has a plurality of cascade waveguide cavities, each cavity having two ends that are parallel to one another, said filter having an input and an output, with at least two adjacent cavities mounted end to end relative to one another and resonating at their resonant frequency in three independent orthogonal modes. At least one of said modes is non-identical to the remaining two modes. An inter-cavity coupling iris is located between adjacent three mode cavities that are mounted end to end relative to one another. Each iris contains an aperture that is able to independently control three inter-cavity couplings simultaneously when said filter is operated in a suitable propagation mode for input and output coupling to produce an elliptic function response.

Preferably, each aperture has four separate radial slots located perpendicular to one another and offset from a centre of the iris.

Preferably, when the cavities are cylindrical, the filter is operated in a TE_{111} propagation mode for input and output coupling.

Preferably, when the cavities have a square cross-section, the filter is operated in a TE_{101} propagation mode for input and output coupling.

In a variation of the present invention, a filter has at least two adjacent cascade waveguide cavities, each cavity having two ends that are parallel to one another, said filter having an input and an output, two cavities being mounted end to end relative to one another resonating at their resonant frequency and three independent orthogonal modes. At least one of said modes being non-identical to the other two modes. An inter-cavity coupling iris is located between adjacent three mode cavities that are mounted end to end relative to one another. Each iris contains an aperture that is able to independently control three inter-cavity couplings simultaneously when said filter is operated in a suitable propagation mode for input and output coupling. An output cavity of said filter is short circuited so that the filter will function as a group delay equalizer.

BRIEF DESCRIPTION OF THE DRAWINGS

In the following drawings, there is shown a prior art filter as well as embodiments of the present invention:

FIG. 1 is an exploded perspective view of a prior art triple-mode filter having cylindrical waveguide cavities;

FIG. 1A is a front view of a prior art iris used in the filter of FIG. 1;

FIG. 2 is an exploded perspective view of a triple-mode filter in accordance with the present invention having cylindrical cavities and a coaxial interface;

FIG. 2A is a front view of an iris in accordance with the present invention;

FIG. 2B is an exploded perspective view of a triple-mode filter in accordance with the present invention, said filter having cavities with a square cross-section and a coaxial interface;

FIG. 2C is an exploded perspective view of a triple-mode filter in accordance with the present invention having a coaxial interface with one cavity having a circular cross-section and another cavity having a square cross-section;

FIG. 3 is an exploded perspective view of a filter in accordance with the present invention having cylindrical cavities and a waveguide interface;

FIGS. 4A and 4B are graphs showing experimental response characteristics of filters designed in accordance with the present invention;

FIG. 5A is an exploded perspective view of a one cavity triple-mode filter in accordance with the present invention where the output has been short circuited;

FIG. 5B is a schematic view of the use of a filter in accordance with the present invention as an allpass equalizer;

FIG. 5C is an exploded perspective view of a two cavity triple-mode filter, having two cylindrical cavities, where the output has been short circuited;

FIG. 5D is an exploded perspective view of a triple-mode filter in accordance with the present invention where the output has been short circuited, said filter having two cavities with a square cross-section;

FIG. 5E is an exploded perspective view of a triple-mode filter in accordance with the present invention where the output has been short circuited and the filter has one cavity with a circular cross-section and one cavity with a square cross-section;

FIG. 6A is a graph showing an experimental response of a conventional dual-mode allpass equalizer;

FIG. 6B is a graph showing an experimental response of a triple-mode allpass equalizer in accordance with the present invention; and,

FIG. 7 is an exploded perspective view of a triple-mode filter in accordance with the present invention containing dielectric resonators.

DESCRIPTION OF A PREFERRED EMBODIMENT

Referring to the drawings in greater detail, in FIG. **1**, there is shown a prior art triple-mode filter **8** in the form suggested by Atia and Williams. The filter **8** has a plurality of cascade waveguide cavities **11**, **12**, each of which resonates in a first TM_{010} mode, a second and third TE_{111} modes. The cavity **11** is an input cavity and the cavity **12** is an output cavity. Between the cavities **11**, **12**, there is located a coupling iris **31**, which provides inter-cavity coupling means through an aperture **36**. Since this is a triple-mode filter, each cavity is capable of supporting three independent modes. While there are two physical cavities **11**, **12**, there are six electrical cavities. Inter-cavity coupling between the three orthogonal modes within a given cavity is achieved by means of a physical discontinuity which perturbs the electrical field of one mode to couple energy into another mode. The physical discontinuity shown in FIG. **1** is represented by a series of coupling screws **21**, **22**, **23**, **24**. Said coupling screws are shown as being mounted at a 45 degree angle relative to tuning screws **41**, **42**, **43**, **44**, **45**, **46**. The tuning screws perturb the electrical field of each orthogonal mode independently and decrease the cut-off wavelength of the waveguide in the plane of each screw. Therefore, the cavity length for each mode appears electrically larger than its physical length.

Inter-cavity TE_{111} to TE_{111} coupling is influenced by a magnetic field energy transfer through the aperture **36** in the iris **31**. But, inter-cavity TM_{010} to TM_{010} coupling is influenced by both electric field and magnetic field energy transfer through the same aperture **36** in the iris **31**. The input and output coupling means **51**, **53** contains an aperture **52**, **54** respectively. The input/output coupling is influenced by magnetic field energy transfer through the aperture **52** in input coupling means **51** and through the aperture **54** in output coupling means **53**. These coupling means **51**, **53** will couple energy into and out of the TM_{010} mode. In other words, TM_{010} mode is the propagation mode for input and output coupling in the filter **8**. The aperture **36** of the iris **31** has a conventional cruciform shape. The shape of the aperture **36** controls only two independent inter-cavity couplings, namely L_1 and L_2 (see FIG. **1**A). In order to realize completely general transfer functions in a triple mode filter, it is necessary to control three inter-cavity couplings simultaneously. If three inter-cavity couplings cannot be independently controlled in the triple mode filter, the theoretical superiority of the triple mode design over dual mode filters is lost. In practical usage, the results achieved by the prior art triple mode filter **8** are unacceptable over the results achieved by conventional dual mode filters. In addition, the propagation mode TM_{010}, suggested by Atia and Williams cannot be controlled in the filter **8**. The physical slot dimension of the centrally located cruciform aperture **36** in the iris **31** is required to couple the remaining two TE_{111} orthogonal modes but also permits large amounts of inter-cavity coupling for the TM_{010} mode. Further, because of the use of the TM_{010} mode for input and output coupling, the physical structure of the coupling means **51**, **53** can be complex and sensitive, making the entire design impractical for use in a satellite transponder. This completes the discussion of the prior art triple mode filter **8**, as shown in FIGS. **1** and **1**A.

Embodiments of the present invention will now be discussed using the same numerals, as used in FIGS. **1** and **1**A, for those parts that are the same or similar. In accordance with the present invention, as shown in FIG. **2**, a bandpass filter **9** has a plurality of cascade waveguide cavities **11**, **12**. The cavities **11**, **12** are adjacent to one another and resonate at their resonant frequency in three independent orthogonal modes. The cavities **11**, **12** have generally the same arrangement of coupling screws **21**, **22**, **23**, **24** and tuning screws **41**, **42**, **43**, **44**, **45**, **46** as previously described for the prior art filter **8**. An inter-cavity coupling iris **31** is located between the adjacent three mode cavities **11**, **12**. Each iris **31** contains an aperture **37** that is able to control three inter-cavity couplings simultaneously, when said filter **9** is operated in a suitable propagation mode for input and output coupling, to produce an elliptic function response. The aperture **37** has four separate radial slots located perpendicular to one another, with all the slots being offset from a centre of the iris.

As shown in FIG. 2A, two of the slots that are aligned with one another are the same length L_2 and are offset from said centre by an equal distance r_2. The remaining two slots are also aligned with one another but have a different length L_1 and are offset by an equal distance r_1 that is different from the distance r_2. The radial slot arrangement of the aperture **37** provides three independent and controllable variables, firstly, the slot length L_1, secondly, the slot length L_2 and thirdly, the radial distance r_1 and r_2 of the slots from the centre. In addition, the pattern of the slots takes advantage of known electrical and magnetic field patterns to provide the necessary control for the TM_{010} mode so that the filter **9** will function in an acceptable manner relative to dual-mode filters.

The coupling due to the TM_{010} mode is minimal near the circumference of the iris or inter-cavity coupling means **31**. By locating the slots of the aperture **37** a distance r_1 and r_2 from the centre of the iris **37**, the coupling of the TM_{010} mode can be properly controlled. The lengths L_1 and L_2 of the slots of the aperture **37** provide the necessary control for the TE_{111} propagation modes.

In the filter **9** of the present invention, the cavities **11**, **12** are cylindrical in shape. When the cavities are cylindrical, the filter **9** is operated in a TE_{11n} propagation mode for input and output coupling, n being a positive integer. Preferably, the filter **9** is operated in a TE_{111} propagation mode for input and output coupling. The use of the TE_{11n} propagation mode permits input and output couplings via coaxial probes **61**, **63**, as shown in FIG. **2**, thus accomplishing a saving in weight and volume. In addition, the use of the TE_{11n} mode also permits maximum permissible control of inter-cavity couplings to enable the filter to realize general transfer functions required for satellite filters and multiplexers. By way of example, when a TE_{111} propagation mode is used for input and output coupling in the filter **9**, each cavity **11**, **12** can be made to resonate in a first TM_{010} mode and second and third orthogonal TE_{111} modes.

While the cavities **11**, **12** of the filter **9** are cylindrical, the cavities could be designed with a square cross-section as shown in FIG. 2B. When the cavities have a square cross-section, the filter is operated in a TE_{10n} propagation mode for input and output coupling, n being a positive integer. Preferably, when the cavities have a square cross-section, the filter is operated in a TE_{101} propagation mode for input and output coupling. By way of example, when a TE_{101} propagation mode is used for input and output coupling, each cavity can be made to resonate in a first TM_{110} mode and second and third orthogonal TE_{101} modes. Of course, it would also be possible to have a filter made up of one or more cylindrical cavities and one or more cavities having a square cross-section as shown in FIG. 2C. Also, it would be possible to have a bandpass filter with one or more triple-mode cavities and one or more single or dual-mode cavities. The same reference numerals are used on FIGS. 2B and 2C as those used in FIG. 2 as the components of the filters are identical except for the cross-sectional shape of the cavities and iris. All three filters **9** operate in the same manner.

In FIG. 3, a filter **10** is nearly identical to filter **9**. The only difference is that waveguide input and output coupling means **71, 73** are used via radial slots **72, 74** respectively for input and output coupling. The same modes would be used with the filter **10** as described for the filter **9**.

In FIGS. 4A and 4B, there are shown measured amplitude response and return loss response respectively for a prototypesix pole elliptic filter constructed in accordance with the filter **9** shown in FIG. 2. It can readily be seen that the response shown in FIG. 4A represents a true elliptic function and FIG. 4B shows that the filter achieves a better than 25 dB return loss. In achieving the results shown with the filter **9**, each cavity was caused to resonate at its resonant frequency in a first and second TE_{111} mode and a third TM_{010} mode. A TE_{111} mode was used for input and output coupling.

In FIG. 5A, in a further embodiment of the present invention, there is shown a reactant cavity **6**. The reactant cavity **6** has a cavity **11** and a similar arrangement of coupling screws **21, 22** and tuning screws **41, 42, 43** as cavity **11** of the filter **9** shown in FIG. 2. In addition, the input coupling means **61** is the same as that shown in FIG. 2. However, an output from the cavity **11** has been short circuited using a shorting plate **33** making the reactant cavity **6** a one-port network. When the reactant cavity **6** is used in conjunction with a non-reciprocal structure or circulator **5**, as shown schematically in FIG. 5B, it performs the function of an allpass filter (commonly referred to as an allpass equalizer or a group delay equalizer). It will be readily apparent to those skilled in the art that other non-reciprocal structures can be used in substitution for the circulator **5** for example, a hybrid-coupled allpass network could be used as a non-reciprocal structure. The phase of the allpass filter and, hence, the group delay is controlled by the resonance frequencies and the couplings of three independent modes excited in the physical cavity. Preferably, these modes are the same as those previously described for the filter **9** of FIG. 2. Compared to the conventional dual-mode allpass network, the allpass filter shown in FIG. 5B yields significantly superior phase and group delay characteristics. FIG. 6A describes the group delay of a conventional dual-mode allpass equalizer. In FIG. 6B, there is shown the group delay over the same frequency band using the triple-mode allpass filter of FIG. 5B. The equalized band width shows an improvement of nearly twenty percent, thereby enhancing the channel capacity and hence the revenue earning potential of a satellite in which such an allpass filter would be used.

As will be readily apparent to those skilled in the art, the allpass filter described in FIGS. 5A and 5B could be designed to use any reasonable number of cavities. However, it is not possible to have more than two adjacent cavities arranged end to end relative to one another and resonating in three independent orthogonal modes. While it is possible to have an allpass filter with more than three cavities functioning in a triple mode, the three cavities cannot be located end to end and adjacent to one another. When two adjacent cascade waveguide cavities are resonating at their resonant frequency and three independent orthogonal modes, there will be located between them an inter-cavity coupling iris as shown in FIGS. 5C, 5D and 5E. The same reference numerals are used in FIGS. 5C, 5D and 5E as those used in FIG. 2 as the cavities **11, 12** of FIGS. 5C, 5D and 5E have the same components except that the output **63** of the filter **9** has been short circuited so that the filter will function as a group delay equalizer when used with a circulator in the same manner as described in FIG. 5B for the reactant cavity **6**. Each iris **31** will contain an aperture **37** that is able to control three inter-cavity couplings simultaneously when said filter is operated in a suitable propagation mode for input and output coupling. An output of said filter is short circuited so that the filter will function as a group delay equalizer when used with a circulator. Preferably, the aperture has four radial slots located perpendicular to one another and offset from a centre of the iris. Preferably, two of the slots are aligned with one another and are the same length and offset from said centre by an equal distance. The remaining two slots are also aligned with one another but have a different length and are offset from said centre by a different but equal distance. Preferably, the filter is operated in a TE_{11n} propagation mode for input and output coupling, n being a positive integer, where the cavities are cylindrical and in a TE_{10n} propagation mode for input and output coupling, n being a positive integer, where the cavities have a square cross-section. Still more preferably, n is equal to 1.

As will be readily understood by those skilled in the art, the coupling that occurs in the cavities **11, 12** of FIGS. 5C, 5D and 5E is the same as that described for the filter **9** of FIG. 2 except that the fact that the output **63** has been short circuited causes the cavities **11, 12** to function as an allpass filter when used in conjunction with a non-reciprocal structure or circular as shown schematically in FIG. 5B. When the output of the reactant cavity **6** of FIG. 5A or of the cavities **11, 12** of FIGS. 5C, 5D and 5E is short circuited, the input **61** also becomes the output. As shown in FIG. 5B, the circulator **5** is connected to the input/output **61** so that the filter will function as a group delay equalizer.

It is believed that by using a triple-mode structure in accordance with the present invention, a weight and volume saving of approximately one-third can be achieved relative to dual-mode filters. The present generation of communication satellites carry twenty-four channels, each channel comprising an input filter and an output filter having a typical weight and volume of approximately 360 grams and 600 cubic centimeters per channel respectively. A typical prior art channel has three dual-mode cavities. With the present invention, each channel would have two triple-mode cavities. Therefore, the use of triple-mode filters should represent a weight and volume saving of approximately 2.9 kilograms and 4,800 cubic centimeters respectively for a twenty-four channel satellite.

Use of a triple-mode structure as an allpass filter or network represents a significant performance improvement relative to a dual-mode allpass network or filter. This improved performance should be achievable with no penalty in weight or volume relative to known dual-mode allpass equalizer networks.

The filters **9** and **10** shown in FIGS. **2** and **3** respectively, have two cavities **11**, **12**. As will be readily apparent to those skilled in the art, within the scope of the attached claims, it will be possible to design a filter having any reasonable number of cavities. Where a filter is of the order N, N being an integral multiple of 3, the number of cavities is equal to N/3. However, it is presently not possible to have more than two adjacent cavities resonating in a triple mode when the cavities are arranged end to end relative to one another. When this occurs, the centre cavity or cavities cannot be made to resonate in a triple-mode. However, as long as the cavities are arranged so that each cavity that resonates in a triple-mode has one end that is exposed, any reasonable number of cavities can be used. For example, one could design an eight cavity triple mode filter where there are four sets of two cavities each. Each set of two cavities has the cavities arranged end to end but the sets themselves are adjacent to one another. In this way, each cavity of the eight cavity filter will have one end exposed so that each cavity can be made to function in a triple mode. Alternatively, it would be possible, though impractical, to have a three cavity filter with each cavity resonating in a triple mode where the centre cavity is turned sideways relative to the two end cavities so that both ends of the centre cavity would be exposed.

In a further embodiment of the invention as shown in FIG. 7, a filter **13** has a plurality of cascade waveguide cavities **11**, **12**. The cavities **11**, **12** are adjacent to one another and resonate at their resonant frequency in three independent orthogonal modes. The coupling screws **21**, **22**, **23**, **24** and tuning screws **41**, **42**, **43**, **44**, **45**, **46**, as well as the coaxial probes **61**, **63** are identical to those shown in FIG. **2**. The iris **31** and the apertures **37** are also identical to that shown in FIG. **2**. As with the filter of FIG. **2**, the physical characteristics of the aperture **37** and iris **31** could be varied so long as the aperture **37** is able to control three inter-cavity couplings simultaneously, when said filter **13** is operated in a suitable propagation mode for input and output coupling, to produce an elliptic function response. Within the cavities **11**, **12** there are located dielectric resonators **71**, **72** respectively. The purpose of the resonators **71**, **72** is to further reduce the overall weight and volume requirement of the triple-mode filters **9** and **10**. The use of dielectric loaded resonators with dual-mode filter is described by Fiedziuszko in the IEEE-MTT-S International Microwave Symposium Digest published in June, 1982, pp 386 to 388.

What I claim as my invention is:

1. A bandpass filter comprising a plurality of cascade waveguide cavities, each cavity having two ends that are parallel to one another, said filter having an input and an output, with at least two adjacent cavities mounted end to end relative to one another and resonating at their resonant frequency in three independent orthogonal modes, at least one of said modes being non-identical to the other two modes, with an inter-cavity coupling iris located between adjacent three mode cavities that are mounted end to end relative to one another, each iris containing an aperture that is able to independently control three inter-cavity couplings simultaneously, when said filter is operated in a suitable propagation mode for input and output coupling, to produce an elliptic function response.

2. A bandpass filter as claimed in claim **1** wherein each aperture is comprised of four non-contacting radial slots, said slots being 90° apart from one another so that there are two sets of two slots each, the slots of each set being aligned with one another.

3. A bandpass filter as claimed in claim **2** wherein all of the radial slots are offset from a centre of the iris.

4. A bandpass filter as claimed in claim **3** wherein the slots of each set are the same length and offset from said centre by an equal distance, the slots of one set having a different length and being offset from the centre by a different distance than the length and distance of the slots of the other set.

5. A bandpass filter as claimed in claim **3** wherein the filter has two cavities only, both resonating at their resonant frequency in said three independent orthogonal modes.

6. A bandpass filter as claimed in any one of claims **1**, **4** or **5** wherein the cavities are cylindrical and the filter is operated in a TE_{11n} propagation mode for input and output coupling, n being a positive integer.

7. A bandpass filter as claimed in any one of claims **1**, **4** or **5** wherein the cavities are cylindrical and the filter is operated in a TE_{111} propagation mode for input and output coupling.

8. A bandpass filter as claimed in any one of claims **1**, **4** or **5** wherein the cavities have a square cross-section and the filter is operated in a TE_{10n} propagation mode for input and output coupling, n being a positive integer.

9. A bandpass filter as claimed in any one of claims **1**, **4** or **5** wherein the cavities have a square cross-section and the filter is operated in a TE_{101} propagation mode for input and output coupling.

10. A bandpass filter as claimed in any one of claims **1**, **4** or **5** wherein at least one cavity is cylindrical and at least one cavity has a square cross-section.

11. A bandpass filter as claimed in any one of claims **1**, **4** or **5** when the filter is of the order N, N being an integer multiple of three and the number of cavities is equal to N divided by three.

12. A bandpass filter as claimed in any one of claims **1**, **2** or **5** wherein there is at least one cavity that does not resonate in three independent orthogonal modes.

13. An allpass filter comprising at least two adjacent cascade waveguide cavities, each cavity having two ends that are parallel to one another, said filter having an input and an output, two cavities being mounted end to end relative to one another and resonating at their resonant frequency in three independent orthogonal modes, at least one of said modes being non-identical to the other two modes with an inter-cavity coupling iris located between adjacent three mode cavities that are mounted end to end relative to one another, each iris containing an aperture that is able to independently control three inter-cavity couplings simultaneously, when said filter is operated in a suitable propagation mode for input and output coupling, an output of said filter being short circuited so that the filter will function as a group delay equalizer, when used with a non-reciprocal structure.

14. A filter as claimed in claim **13** wherein each aperture has four radial slots located 90° apart from one another, so that there are two sets of two slots each, the slots of each set being aligned with one another.

15. A filter as claimed in claim **14** wherein all of the radial slots are offset from a centre of the iris and the non-reciprocal structure is a circulator.

16. A filter as claimed in claim **15** wherein the filter has two cavities.

17. A filter as claimed in claim **16** wherein the slots of each set are the same length and offset from said centre by an equal distance, the slots of one set having a different length and being offset from the centre by a different distance than the length and distance of the slots of the other set.

18. A bandpass filter as claimed in any one of claims **13**, **15** or **17** wherein the cavities are cylindrical and the filter is operated in a TE_{11n} propagation mode for input and output coupling, n being a positive integer.

19. A filter as claimed in any one of claims **13**, **15** or **17** wherein the cavities are cylindrical and the filter is operated in a TE_{111} propagation mode for input and output coupling.

20. A filter as claimed in any one of claims **13**, **15** or **17** wherein the cavities have a square cross-section and the filter is operated in a TE_{10n} propagation mode for input and output coupling, n being a positive integer.

21. A filter as claimed in any one of claims **13**, **15** or **17** wherein the cavities have a square cross-section and the filter is operated in a TE_{101} propagation mode for input and output coupling.

22. A filter as claimed in any one of claims **13**, **15** or **17** wherein at least one cavity is cylindrical and at least one cavity has a square cross-section.

23. A bandpass filter as claimed in any one of claims **1**, **4** or **5** wherein there is a dielectric resonator in each cavity.

24. A filter as claimed in any one of claims **13**, **15** or **16** wherein there is a dielectric resonator in each cavity.

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