

[54] **PULSED INDUCTION LOGGING FOR DETERMINING INVADED ZONE PROPERTIES**

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Related U.S. Application Data

[62] Division of Ser. No. 294,124, Aug. 19, 1981, Pat. No. 4,481,472.

[51] Int. Cl.⁴ **G01V 3/28**

[52] U.S. Cl. **324/339**

[58] Field of Search 324/337-341, 324/334, 343, 344-360

References Cited

U.S. PATENT DOCUMENTS

3,090,910	5/1963	Moran	324/339
3,391,334	7/1968	Ruehle	324/346 X
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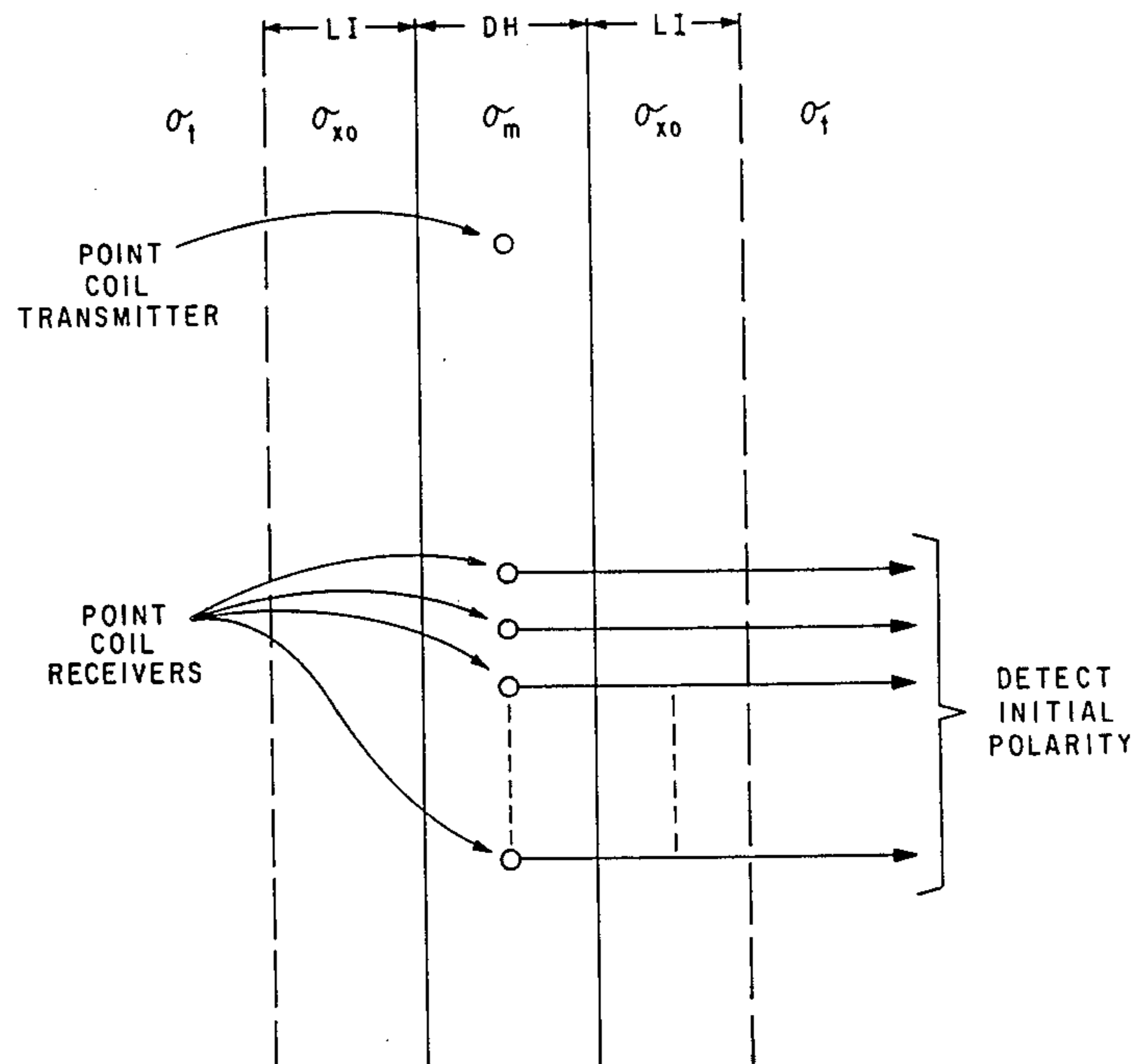
3,978,396	8/1976	Inouye et al.	324/337
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[57] **ABSTRACT**

A method for measuring properties of earth formations surrounding a borehole and, particularly, properties of the invaded zone of the formations. A short pulse of electrical energy is applied at a transmitter location, and signals are induced at a plurality of receiver locations. The polarities of the initial portions of the signals detected at the receiver locations are used in determining properties of the formation invaded zone, particularly its thickness and its conductivity as compared to the virgin formations.

2 Claims, 8 Drawing Figures



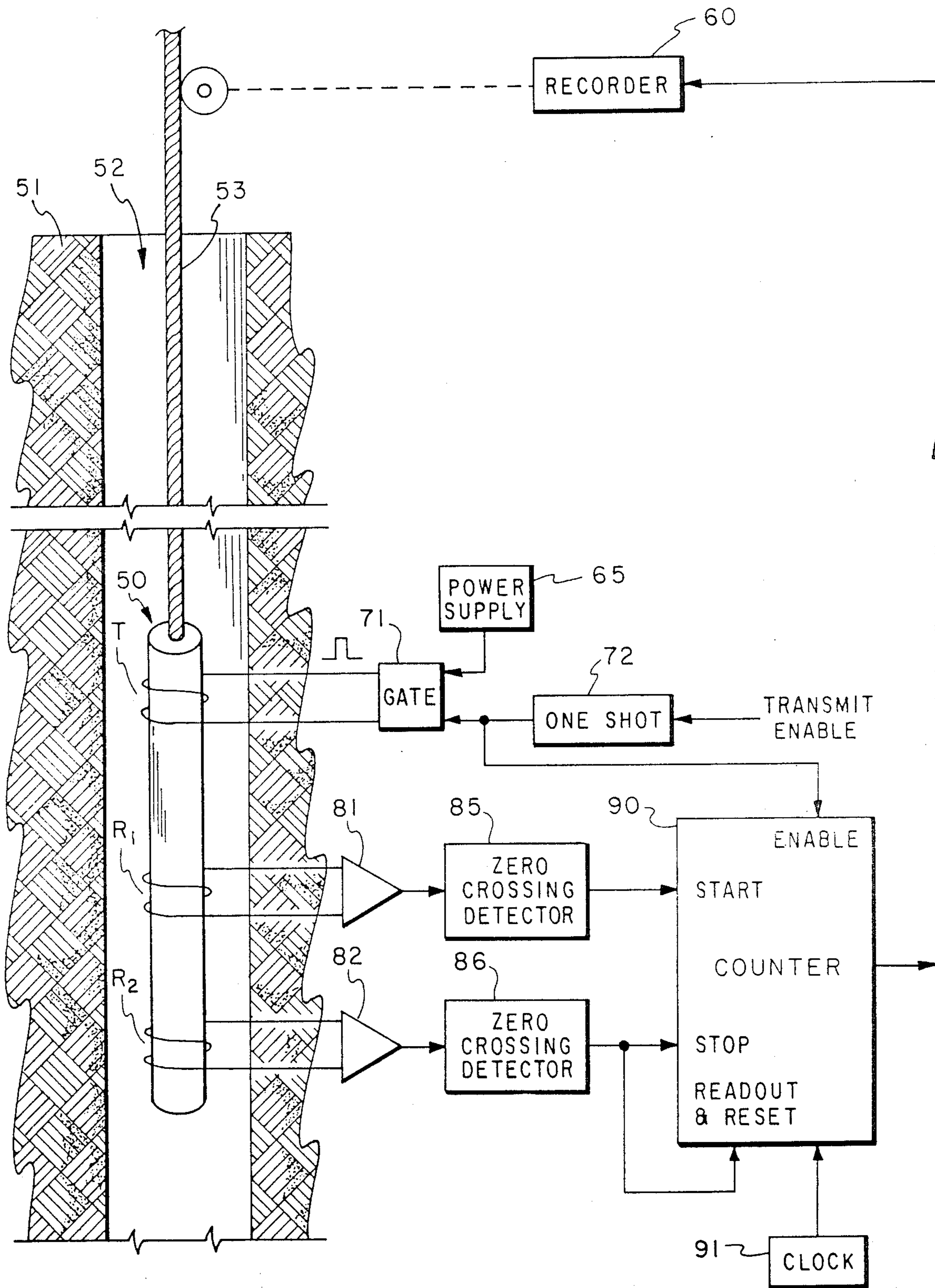


Fig. 1

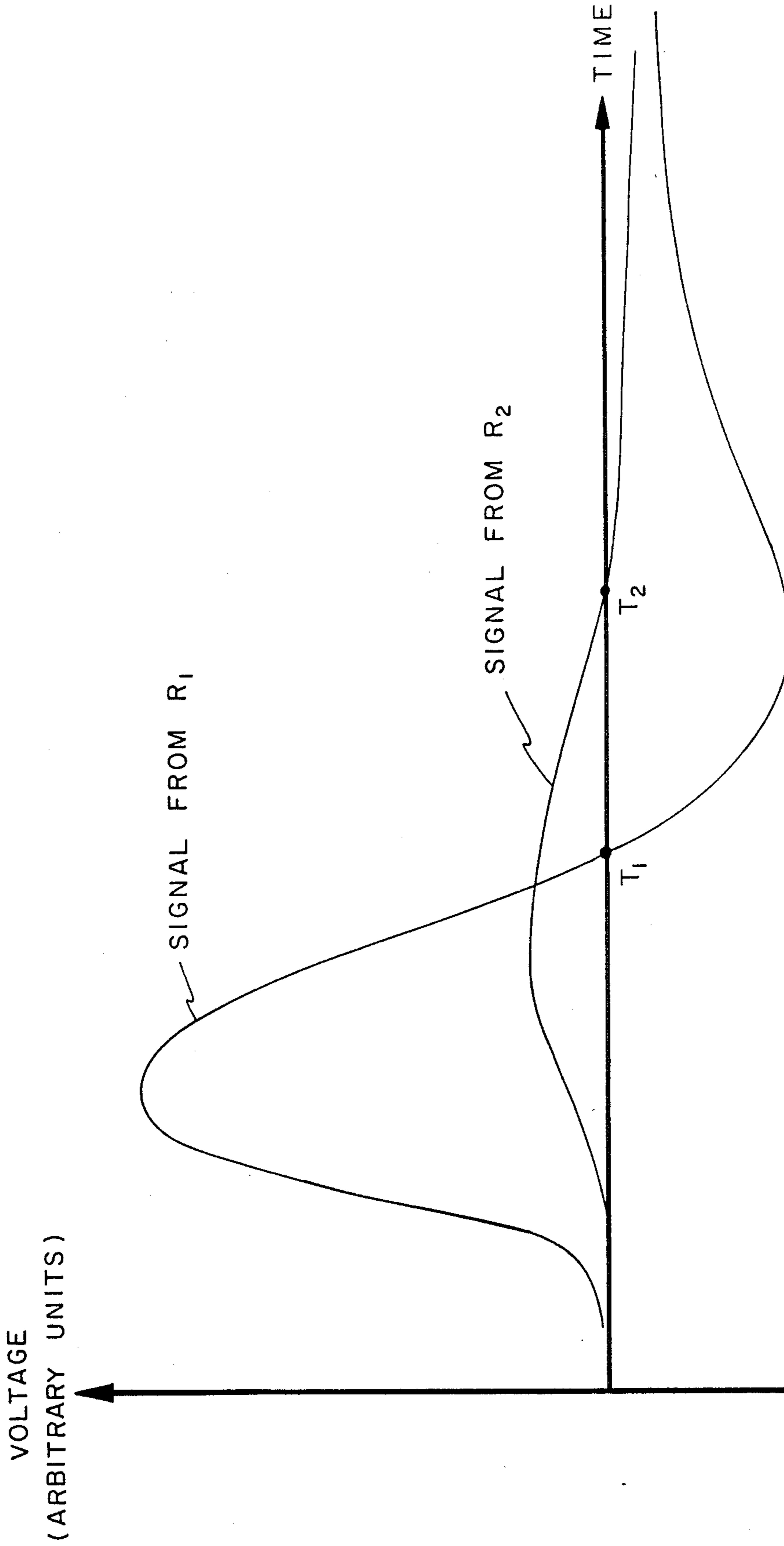


Fig. 2

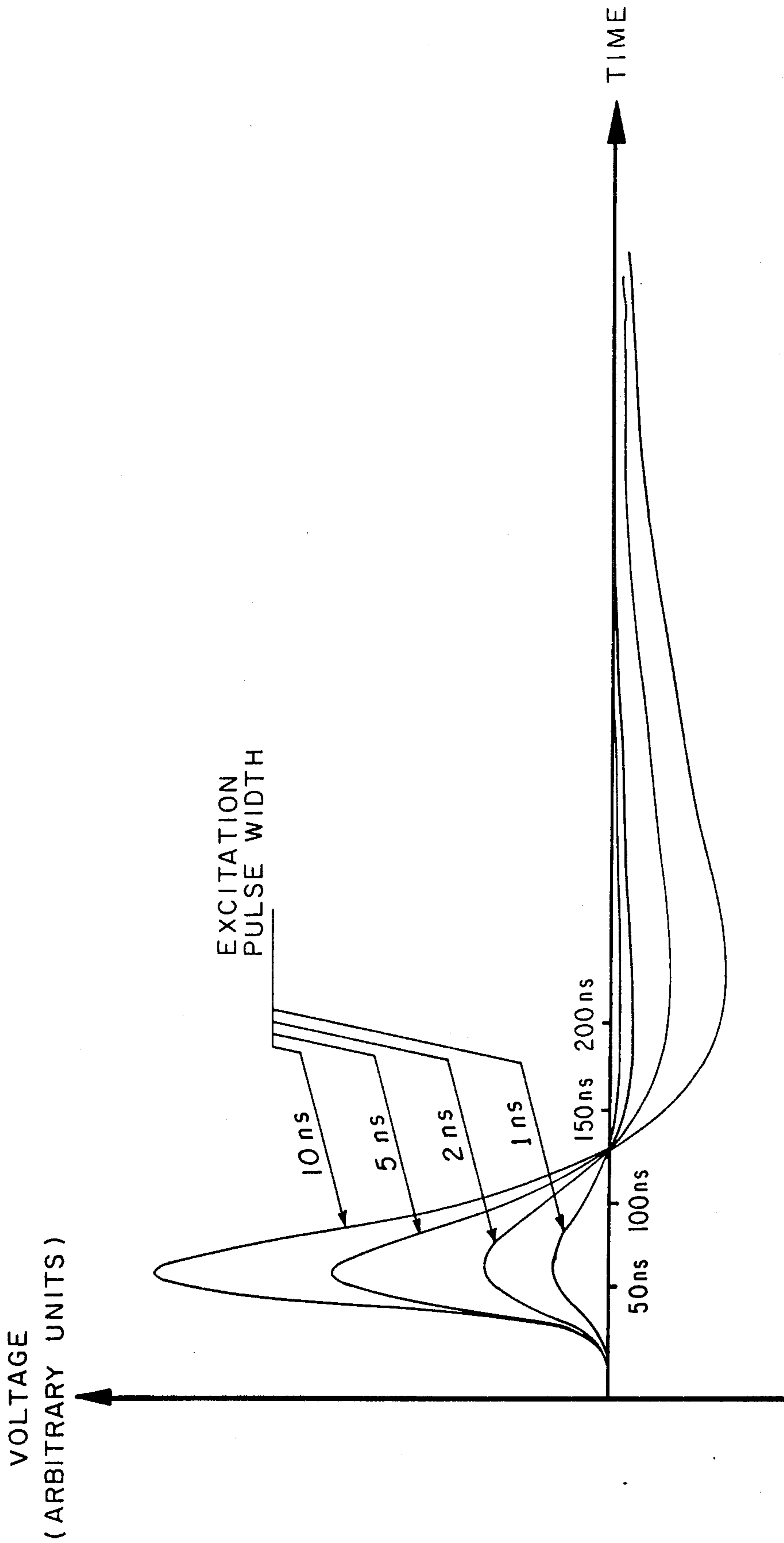


Fig. 3

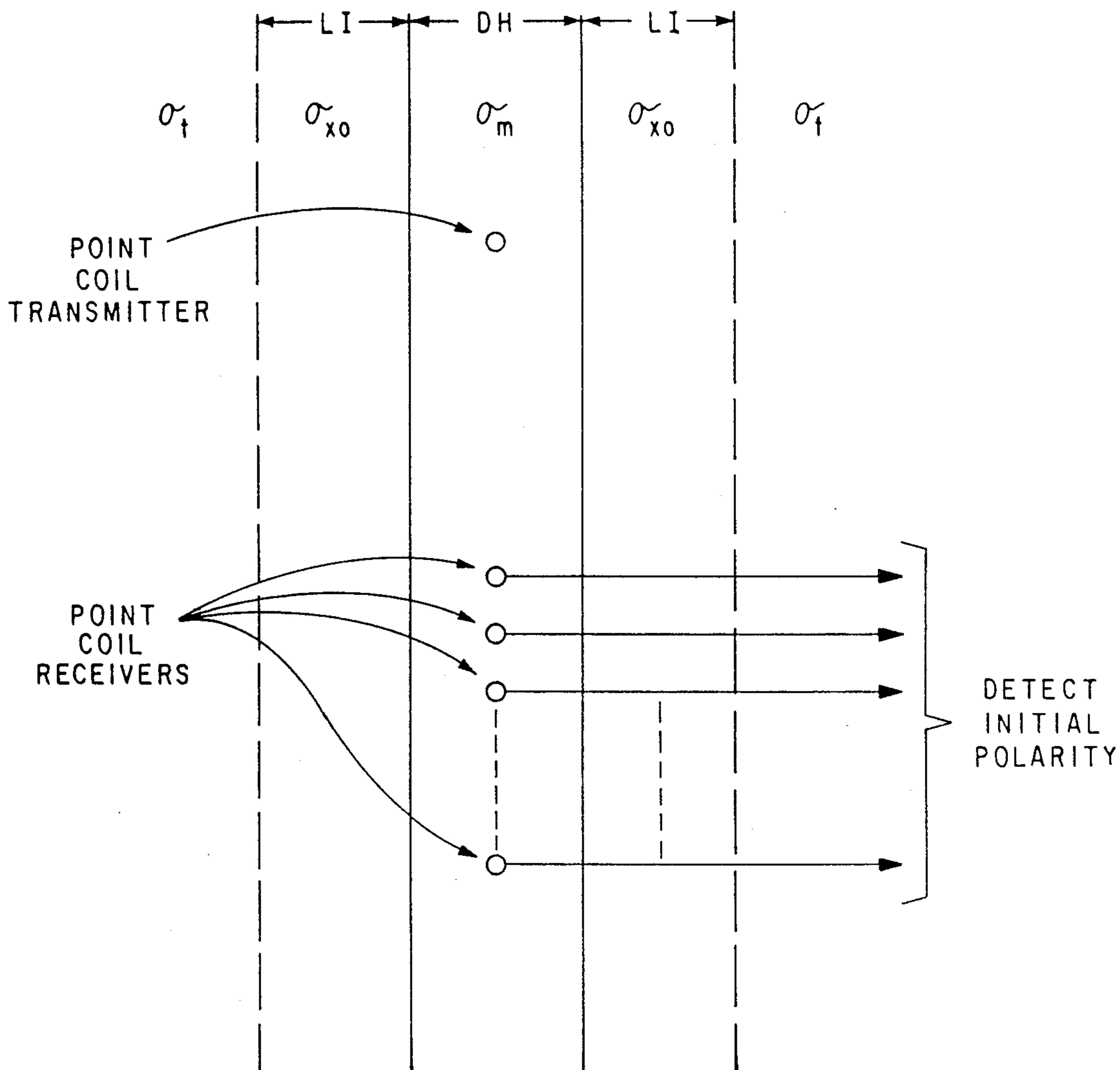


Fig. 4

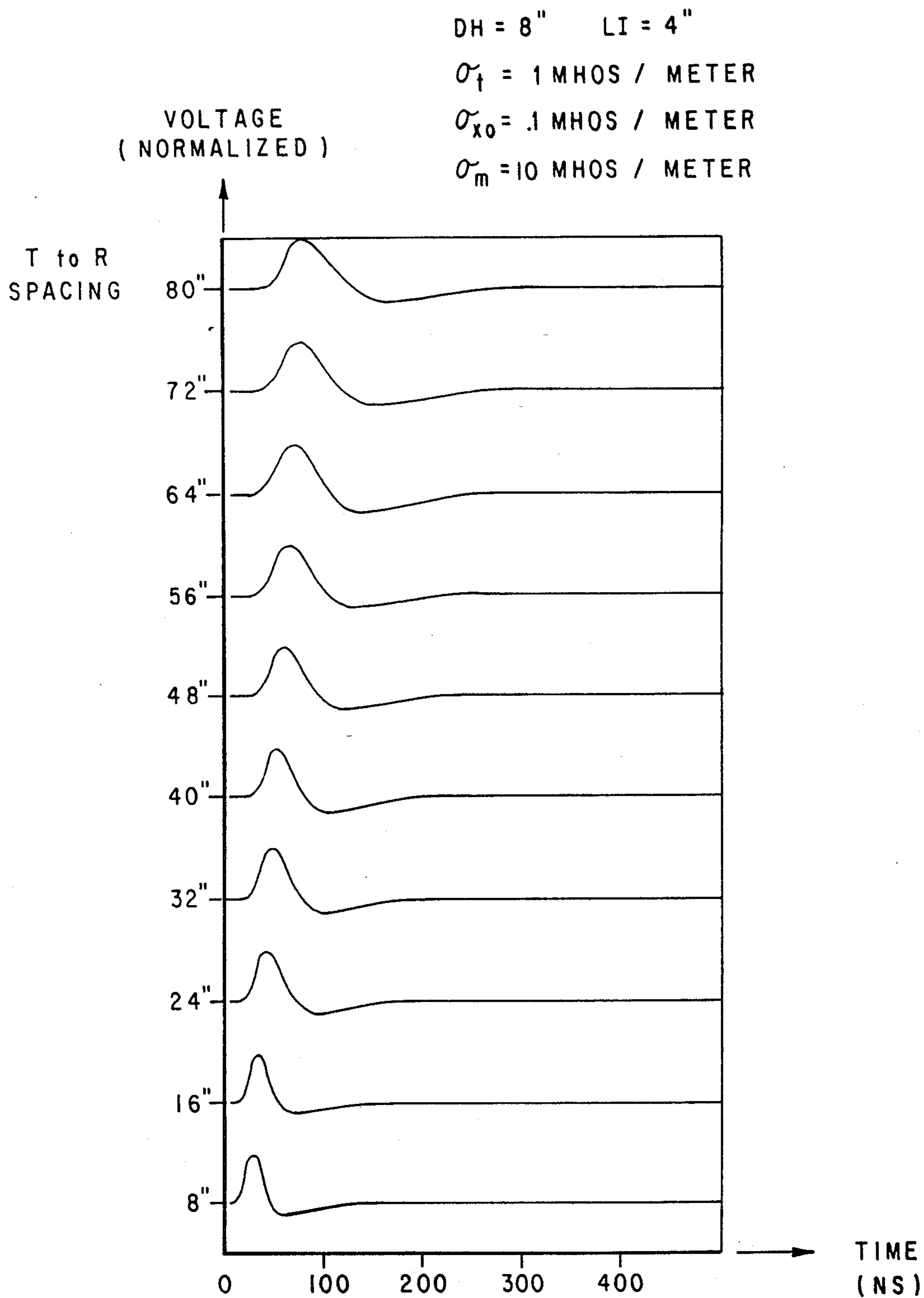


Fig. 5

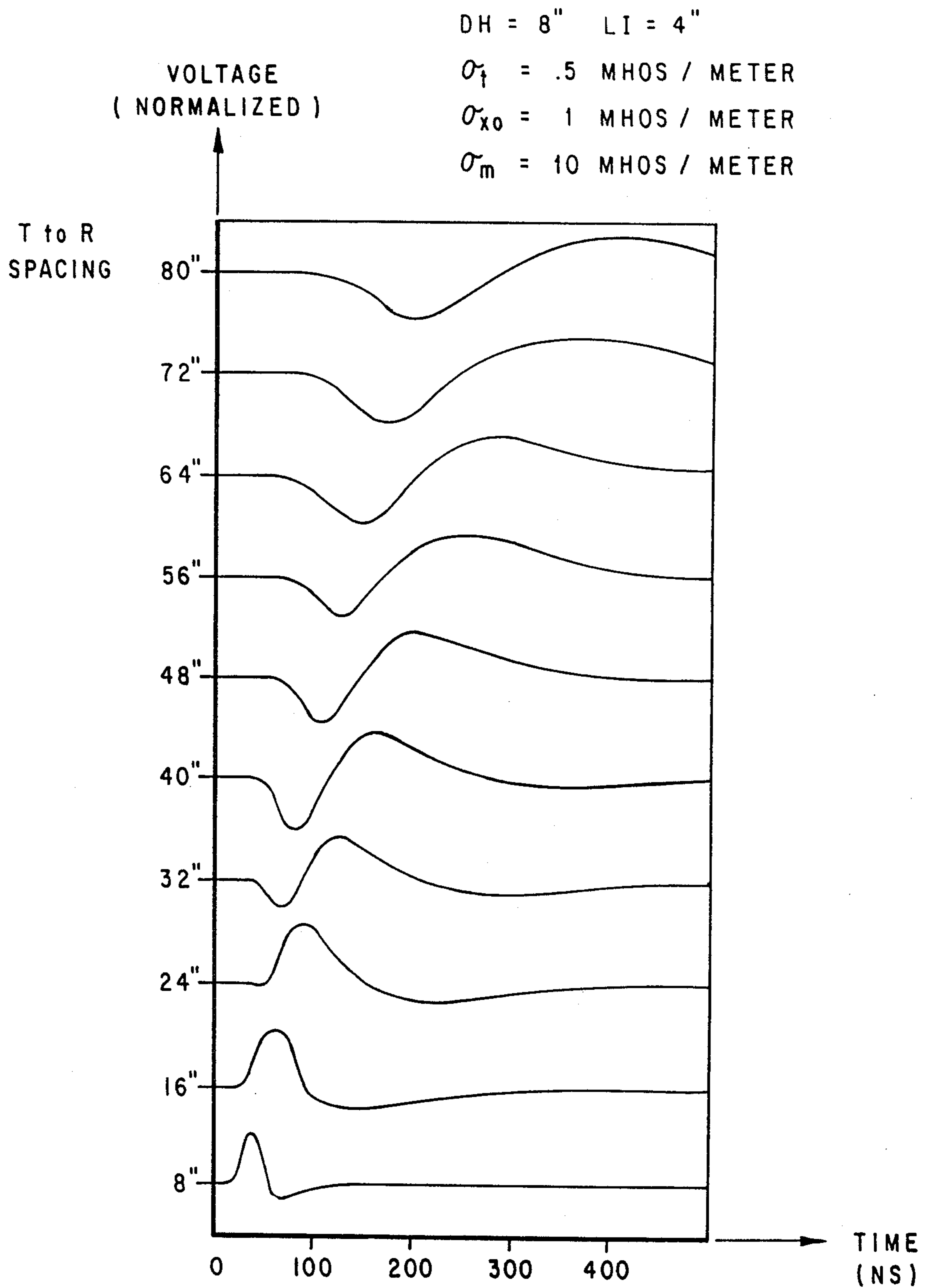


Fig. 6

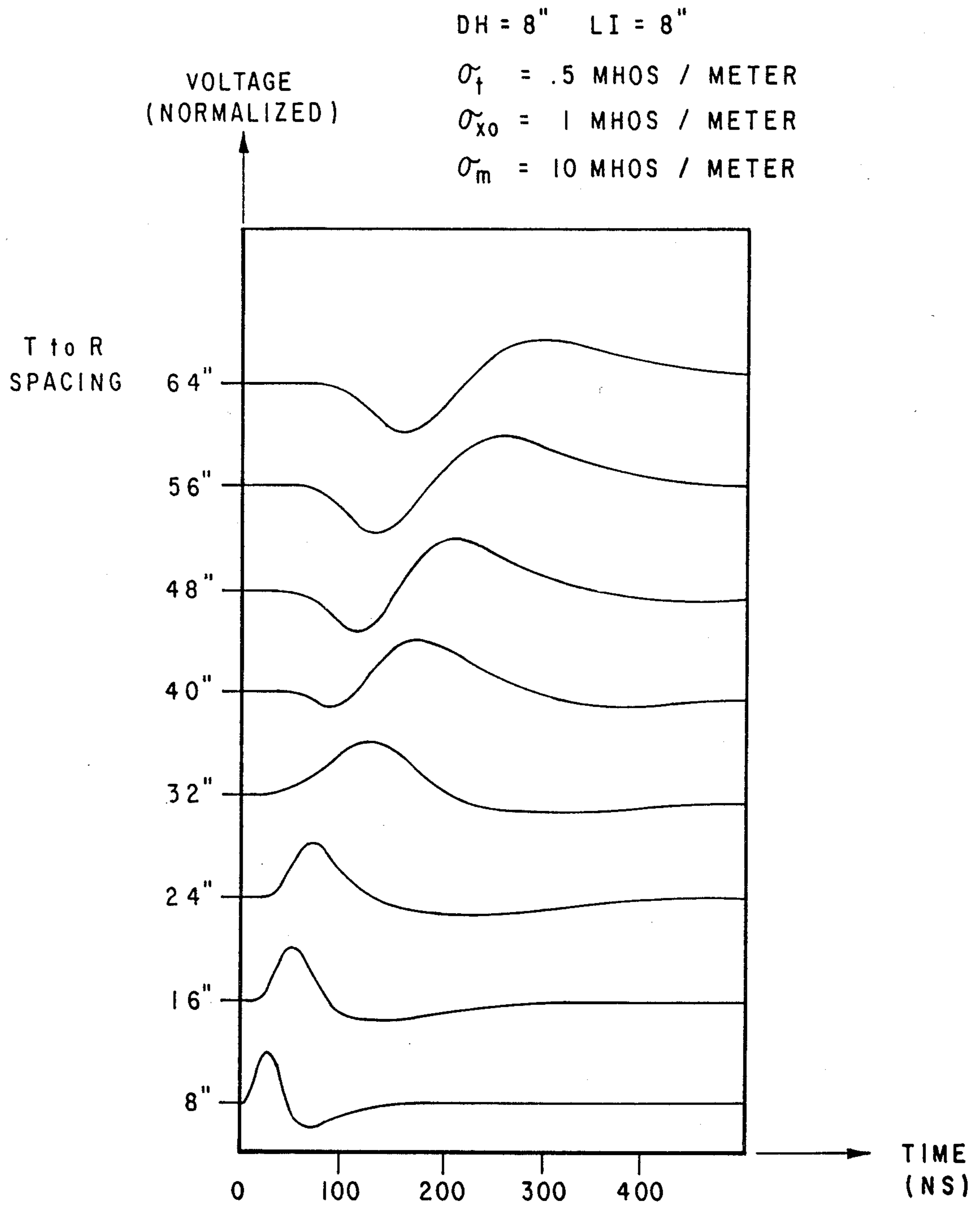


Fig. 7

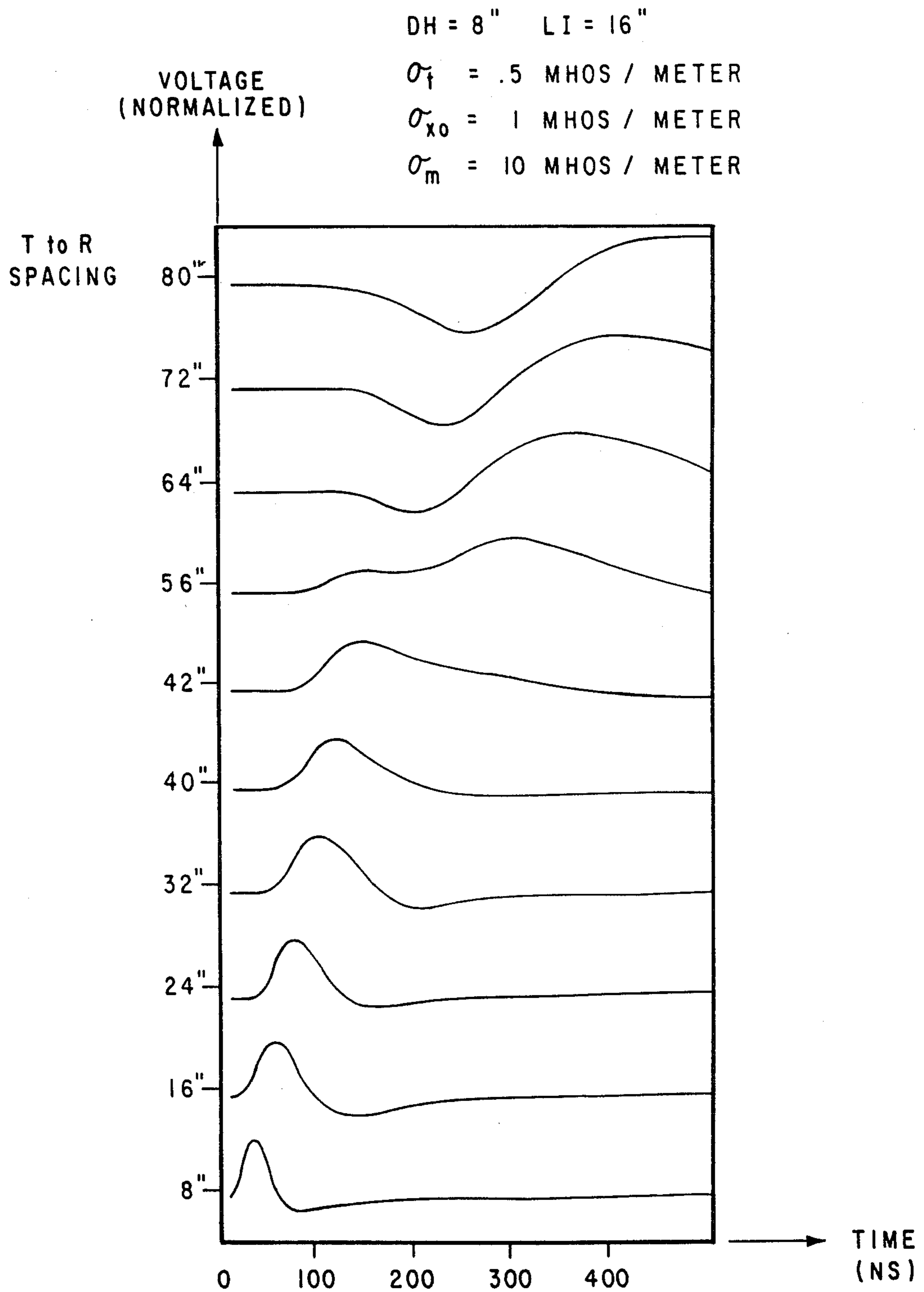


Fig. 8

PULSED INDUCTION LOGGING FOR DETERMINING INVADED ZONE PROPERTIES

This is a divisional of copending U.S. application Ser. No. 294,124, filed Aug. 19, 1981, now U.S. Pat. No. 4,481,472.

BACKGROUND OF THE INVENTION

This invention relates to the measurement of the properties of subsurface earth formations surrounding a borehole and, more particularly, to an apparatus and method for measuring conductivity and certain properties of the formation invaded zone.

Induction logging has been employed for many years for measuring the conductivity of subsurface earth formations surrounding an earth borehole. In conventional induction logging a number of coils are wound on a mandrel. One or more transmitter coils are energized by an alternating current. The resultant oscillating magnetic field causes induction of currents in the formations which are substantially proportional to its conductivity. These currents, in turn, cause a voltage to be induced in receiver coils.

In the U.S. Pat. No. 3,090,910, there is disclosed a system for measuring the conductivity of formations surrounding a borehole using an induction technique that is different from conventional induction logging. A transmitter coil is energized with a sawtooth current, and the response induced in a spaced receiver coil is detected. The patent teaches that the rapidity of rise of the voltage induced in the receiver coil will vary in value inversely as the conductivity of the medium in the region that is being investigated; i.e., a slow rise time will be indicative of a relatively high conductivity, and a fast rise time will be indicative of a relatively low conductivity. The technique disclosed in the patent, referred to as "inductive probing", is intended to overcome certain limitations of conventional induction logging, for example, problems encountered due to skin effect phenomena and problems caused by measurements being affected by changes in the magnetic permeability of the medium being investigated.

It is an object of the present invention to provide another improved apparatus and method for measuring by induction the conductivity of earth formations surrounding a borehole, and also to provide a technique which is useful in determining properties of the invaded zone of said formations.

SUMMARY OF THE INVENTION

The present invention is directed to an apparatus and method for measuring properties of earth formations surrounding a borehole and, particularly, conductivity properties of the formations and certain properties of the invaded zone of the formations. In accordance with one embodiment of the invention, a logging device, movable through the borehole, has a transmitter coil and first and second spaced receiver coils mounted thereon. Means are provided for applying a pulse of electrical energy to the transmitter coil. The pulse is preferably a unipolar broadband pulse having a duration of less than about 1 microsecond. Means are provided for detecting signals induced in the first and second receiver coils. Finally, means are provided for determining a conductivity property of the surrounding formations as a function of the times of occurrence of predetermined characteristics of the signals detected in

the first and second receiver coils. In the preferred embodiment of this form of the invention, the means for determining a conductivity property of the formations includes for means for detecting a zero crossing of the signal induced in the first receiver coil, means for detecting a zero crossing of the signal induced in the second receiver coil, and means for determining the elapsed time between the respective zero crossings. The conductivity of the surrounding formations is determined from the elapsed time, it being substantially proportional to said elapsed time.

In accordance with a further form of the invention, there is disclosed a method for determining a property of the invaded zone of the formations surrounding a borehole. Again, a pulse of electromagnetic energy is generated at a transmitter location in the borehole. Induced electromagnetic energy is detected at a plurality of locations, preferably at least three locations, in the borehole, successively spaced from the transmitter location. The polarity of the initial portion of the energy received at the spaced receiver locations is then detected. Finally, a property of the invaded zone of the formations is determined from the detected polarities. In accordance with the feature of this form of the invention, the step of determining a property of the invaded zone comprises determining the presence or absence of a difference, as between different receiver locations, in the polarity of the initial portion of the energy detected at the spaced receiver locations. The difference is indicative that the invaded zone is more conductive than the non-invaded zone (or virgin formations). Also, by determining the particular receiver location at which the polarity of the initial portion of the energy detected is different than the polarity of the initial portion of the energy detected at the receiver location which is next closest to the transmitter location, one can determine the thickness of the invaded zone as being directly related to the spacing between the transmitter location and said particular receiver location.

Further features and advantages of the invention will become more readily apparent from the following detailed description when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic representation, partially in block diagram form, of an embodiment of one form of the invention.

FIG. 2 is a graph of two receiver response waveforms.

FIG. 3 is a graph of receiver response waveforms for a number of different pulse widths.

FIG. 4 is a simplified model of a section of earth formation traversed by a borehole, showing a point coil transmitter and a number of point coil receivers, which can be used in practicing the method of another form of the invention.

FIGS. 5-8 illustrate the receiver response waveforms at various receiver locations for different versions of the model of FIG. 4.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring to FIG. 1, there is shown a logging apparatus 50 in accordance with an embodiment of the present invention for investigating subsurface formations 51 traversed by a borehole 52. The investigating apparatus or logging device 50 is suspended in the borehole 52 on

an armored cable 53, the length of which substantially determines the relative depth of the device 50. The borehole 52 is typically filled with a drilling fluid or mud which contains finely divided solids in suspension. Generally, the fluid pressure in formations traversed by the borehole is less than the hydrostatic pressure of the column of mud in the borehole, so that the mud and mud filtrate flow somewhat into the formations. The volume of the formations that is "invaded" by the mud and mud filtrate is referred to as the "invaded zone". Also, the formations tend to screen some of the small particles suspended in the mud so that a mudcake is formed on the walls of the borehole.

The device 50 comprises a sonde which includes a cartridge that typically contains most of the electronics, and a mandrel around which is wound a transmitter coil, designated T, and, spaced therefrom, a pair of spaced receiver coils designated R₁ and R₂ which are, respectively, close and far receivers of a differential receiver arrangement. Disposed within the cable 53 are electrical conductors which may provide a supply of power from the surface (if desired, although the power supply 65 is shown as being contained within the logging device in the present embodiment), and which also carry electrical signals from the sonde to a recorder 60 at the surface of the earth.

The downhole electronics contained within the device 50 are shown, for convenience of illustration, at the side of the borehole in FIG. 1. Power supply 65 generates a DC level of electrical energy through a high impedance source, the electrical energy being coupled to one input of the gate 71. The gate 71 may be, for example, a silicon-controlled rectifier that is capable of handling a relatively high power signal. The control terminal of the gate 71 receives the output of monostable or one-shot multivibrator 72 which is, in turn, triggered by a transmit enable pulse that is periodically generated by a source not shown. In the present embodiment the one-shot multivibrator 72 has a characteristic "on" time preferably less than about 1 microsecond. During the output pulse of monostable multivibrator 72, the gate 71 is enabled to pass the energy generated by power supply 65, thereby coupling a generally rectangular impulse of electrical energy having a duration of less than about 1 microsecond to the transmitter coil T. The output of monostable multivibrator is also coupled to the enable terminal of a counter 90.

The receiver coils R₁ and R₂ are respectively coupled to amplifiers 81 and 82 whose outputs are, in turn, respectively coupled to zero-crossing detectors 85 and 86. In the present embodiment, the zero-crossing detectors are of the type that produce an output upon occurrence of a negative-going zero-crossing. The outputs of zero-crossing detectors 85 and 86 are respectively coupled to the "start" and "stop" terminals of counter 90 which receives clock pulses from a clock 91. The signal coupled to the "stop" terminal of counter 90 is also coupled to the readout and reset terminals of counter 90. The count read out of counter 90 is coupled to the surface of the earth and is recorded by recorder 60 as a function of borehole depth.

Before describing operation of the embodiment of FIG. 1, reference can be made to FIG. 2 which illustrates the type of signals, as a function of time, that are induced in the receiver coils R₁ and R₂. In the present example, each of the induced voltages is initially positive-going and then has a negative-going zero-crossing which occurs at times designated t₁ and t₂, respectively,

for the signals from R₁ and R₂. Applicant has determined that the apparent conductivity of the surrounding formations, designated σ_a , is substantially proportional to (t₂-t₁), and can be expressed as:

$$\sigma_a \sim \frac{t_2 - t_1}{\mu_o(L_2^2 - L_1^2)} \quad (1)$$

where μ_o is the magnetic permeability of free space (a constant) and L₂ and L₁ are respectively the distances between transmitter T and receiver R₁ (also constants). The relationship set forth can be determined from a model employing point coil transmitter and spaced receivers in a wellbore medium surrounded by a homogeneous formation, and by solving for the response at the receivers when the transmitter is excited with a broadband pulse.

In operation, it is seen that the recorder signal of FIG. 1 is substantially proportional to the apparent conductivity of the formations in accordance with relationship (1). The times of the negative-going zero-crossings which result in outputs from detectors 85 and 86 of FIG. 1 are respectively representative of the times such as t₁ and t₂ in FIG. 2. By starting the counter with the output of the zero-crossing detector 85 (at a time t₁) and then stopping the counter at the time of occurrence of an output from the zero-crossing detector 86 (at a time t₂), it is seen that the counter 90 will contain a final count representative of the time t₂-t₁. This digital count is recorded by recorder 60.

The technique of the present invention is relatively independent of the pulse width of the transmitted pulse, for short pulse widths of duration preferably less than about 1 microsecond. FIG. 3 illustrates the response that can be expected at a receiver an arbitrary distance of one meter from the transmitter, as computed for a model comprising a homogeneous medium of conductivity 1 mho/meter for different pulse durations τ . It is readily seen that the zero-crossing time τ is substantially independent of the transmitter pulse width for pulse widths between 1 and 10 nanoseconds.

In accordance with a further feature of the invention, applicant has discovered that the initial polarity of the received signal, and the receiver distance at which the initial polarity changes, can be utilized in determining characteristics of the invaded zone of the formations surrounding the borehole. In particular, the technique to be set forth can be used to determine the relative conductivity of the invaded zone as compared to the conductivity of the uninvaded zone and, in some cases, to determine the approximate thickness of the invaded zone. Consider the simplified model of FIG. 4 of a section of formation of conductivity σ_f with a borehole of diameter DH filled with mud of conductivity σ_m and having an invaded zone of conductivity σ_{xo} and thickness LI. If a point coil transmitter is positioned in the borehole, one can compute the response that would be expected at a series of receiver positions successively spaced from the transmitter position. FIG. 5 illustrates the response at receiver locations (at the various spacings from the transmitter location indicated in the FIGURE) for the type of pulse excitation described in conjunction with the FIG. 1 embodiment and with DH=8', LI=4', $\sigma_f=1$ mhos/meter, $\sigma_{xo}=0.1$ mhos/meter and $\sigma_m=10$ mhos/meter. In this example, where the invaded zone has a lower conductivity than the uninvaded zone (or virgin formation), the initial portion of

each waveform has the same polarity, that is, a positive polarity.

Consider next the FIGS. 6, 7 and 8 waveforms which each represent the receiver signals for a FIG. 4 receiver model wherein the invaded zone has a higher conductivity than the uninvaded zone (in particular, DH=8", LI=4", $\sigma_i=0.5$ mhos/meter, $\sigma_{xo}=1$ mhos/meter, and $\sigma_m=10$ mhos/meter for FIG. 6; DH=8", LI=8", $\sigma_i=0.5$ mhos/meter, $\sigma_{xo}=1$ mhos/meter and $\sigma_m=10$ mhos/meter for FIG. 7; and DH=8", LI=16", $\sigma_i=0.5$ mhos/meter, $\sigma_{xo}=1$ mhos/meter and $\sigma_m=10$ mhos/meter for FIG. 8). In these cases it is seen that at a certain distance from the transmitter the induced receiver voltage changes its nature; i.e., the initial portion of the waveform is negative, rather than positive (as it was for closer receiver locations). Also, applicant has determined that the receiver distance at which the initial waveform polarity first reverses is related to the thickness of the invaded zone, with the receiver distance at which such reversal occurs varying directly with the invaded zone thickness. Accordingly, the polarity information from the multiple receivers of FIG. 4 can be used to determine whether the invaded zone has greater or lesser conductivity than the virgin formation (by determining if an initial waveform polarity change takes place), and can also be used to approximate the thickness of the invaded zone (by determining the receiver spacing at which such polarity reversal occurs).

It will be understood that there are various ways that the methods described in conjunction with FIGS. 4-8 can be practiced, including providing multiple receiver elements whose responses are measured either from a single transmitter pulse or multiple transmitter pulses or by moving one or more receivers to different spacings from a transmitter location in the borehole. Detection of initial polarity can be performed by detecting the polarity of the initial zero crossing or by other known means of polarity detection. It will be understood that the embodiment illustrated in FIG. 1 is intended for operation preferably where either the invaded zone is less conductive than the virgin formation or, if not, where the receivers are close enough to the transmitter that polarity reversal will not occur.

The invention has been described with reference to particular embodiments, but variations within the spirit

and scope of the invention will occur to those skilled in the art. For example, in the embodiment of FIG. 1, there are various ways in which the energizing pulse can be generated and in which the relative timing of the receiver signals can be measured.

I claim:

1. A method for determining the relative conductivity of the invaded zone of formations surrounding a borehole, comprising the steps of:

generating a unipolar broadband pulse of electromagnetic energy at a transmitter location in said borehole;

detecting induced electromagnetic energy at at least three receiver locations in said borehole successively spaced from said transmitter location;

detecting the polarity of the initial portion of the energy detected at each of said spaced receiver locations; and

determining the presence or absence of a difference in the polarity of the initial portion of the energy detected between successive receiver locations, the presence of said difference being indicative of the invaded zone being more conductive than the non-invaded zone of said formations.

2. A method for determining the thickness of the invaded zone of formations surrounding a borehole, comprising the steps of: generating a unipolar broadband pulse of electromagnetic energy at a transmitter location in said borehole;

detecting induced electromagnetic energy at at least three receiver locations in said borehole successively spaced from said transmitter location;

detecting the polarity of the initial portion of the energy detected at each of said spaced receiver locations; and

determining the particular receiver location at which the polarity of the initial portion of the energy detected is different than the polarity of the initial portion of the energy detected at the receiver location which is next closest to said transmitter location, the thickness of the invaded zone of said formations being related to the spacing between said transmitter location and said particular receiver location.

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