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[54] PLL DETECTION CIRCUIT	[56] References Cited	
[75] Inventor: Hitoshi Hirata, Tokyo, Japan	U.S. PATENT DOCUMENTS 2,932,793 4/1960 Smith et al	
[73] Assignee: Pioneer Electronic Corporation, Tokyo, Japan	3,127,564 3/1964 Giger	
[21] Appl. No.: 326,994	3,903,473 9/1975 Foster	
[22] Filed: Dec. 3, 1981[30] Foreign Application Priority Data	Primary Examiner—John S. Heyman Attorney, Agent, or Firm—Sughrue, Mion, Zinn, Macpeak & Seas	
[30] Foreign Application Priority Data Dec. 8, 1980 [JP] Japan	[57] ABSTRACT	
[51] Int. Cl. ³	A time constant resistor in a phase lock loop filter is short-circuited by a plurality of diodes which are activated in response to a detection output indicating that the filter output is within a desired locking range. 4 Claims, 3 Drawing Figures	

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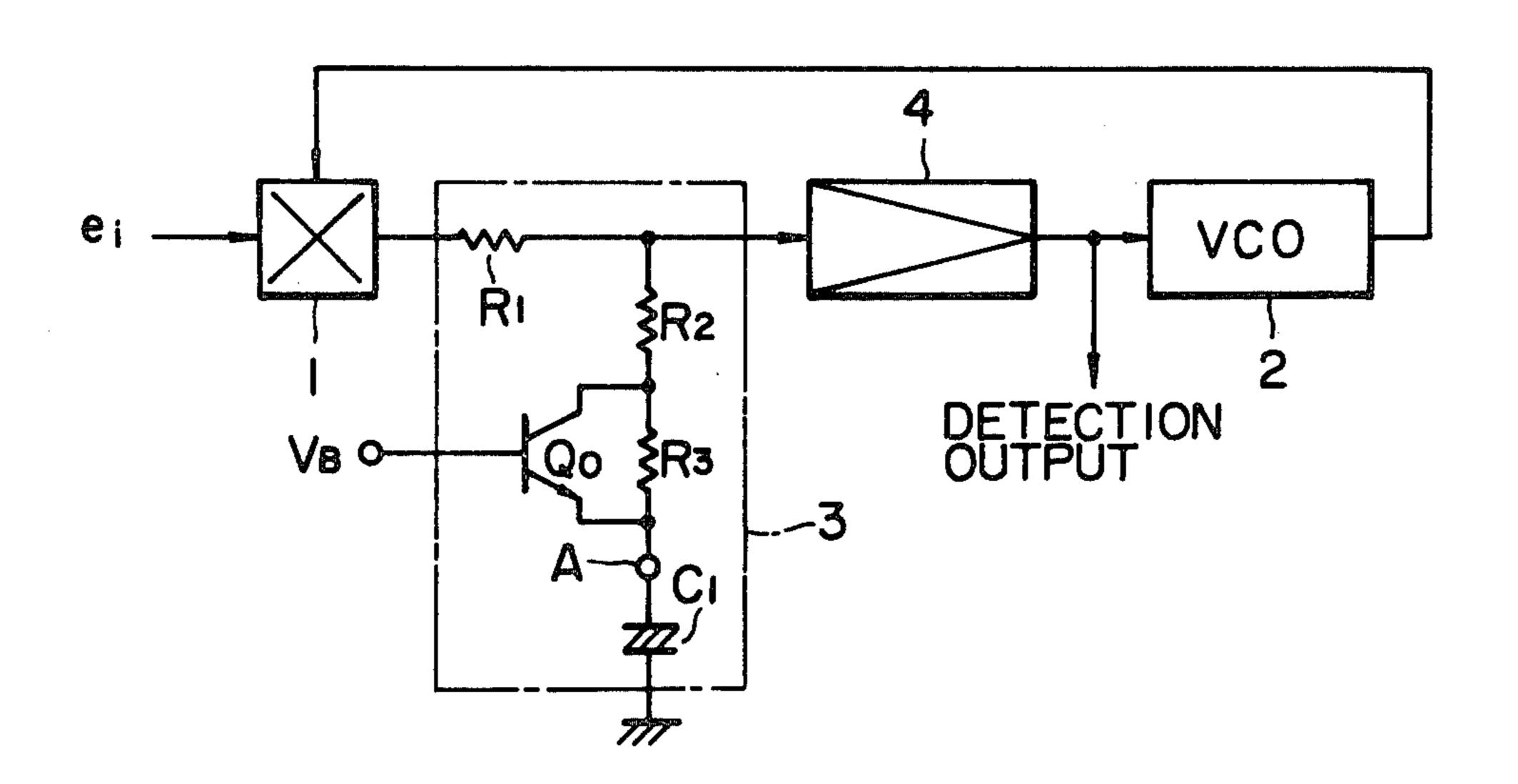


FIG. I PRIOR ART

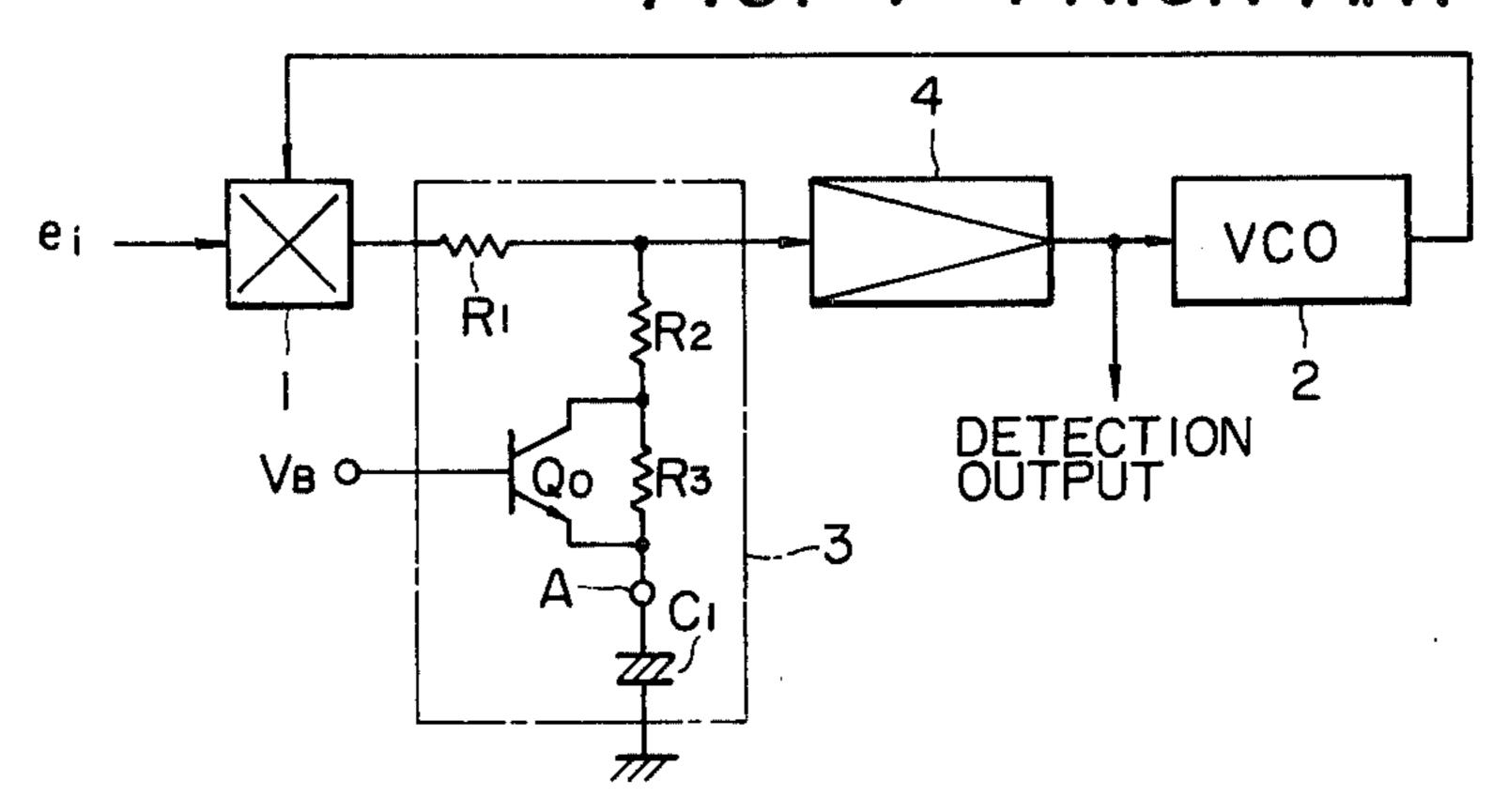
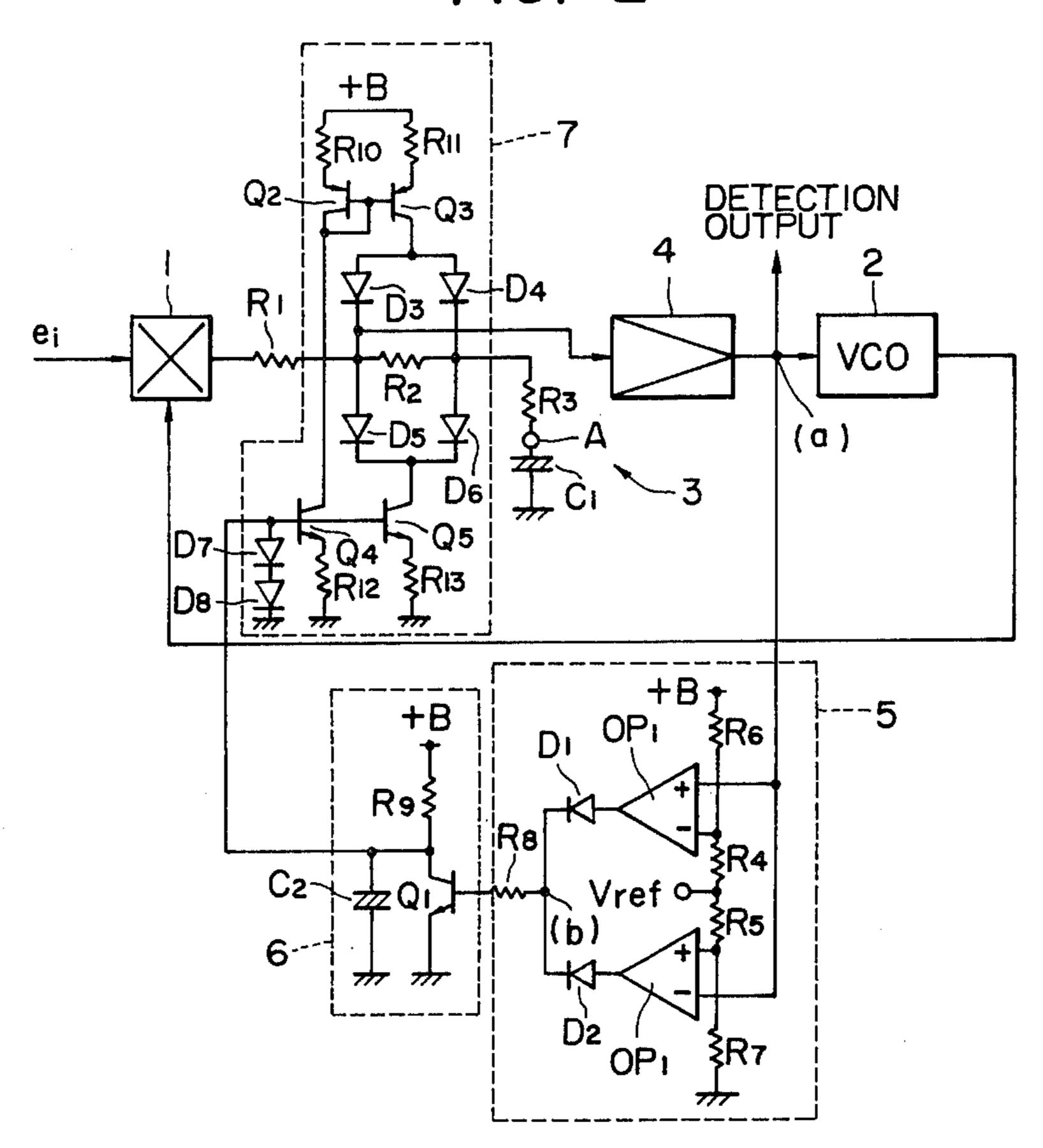
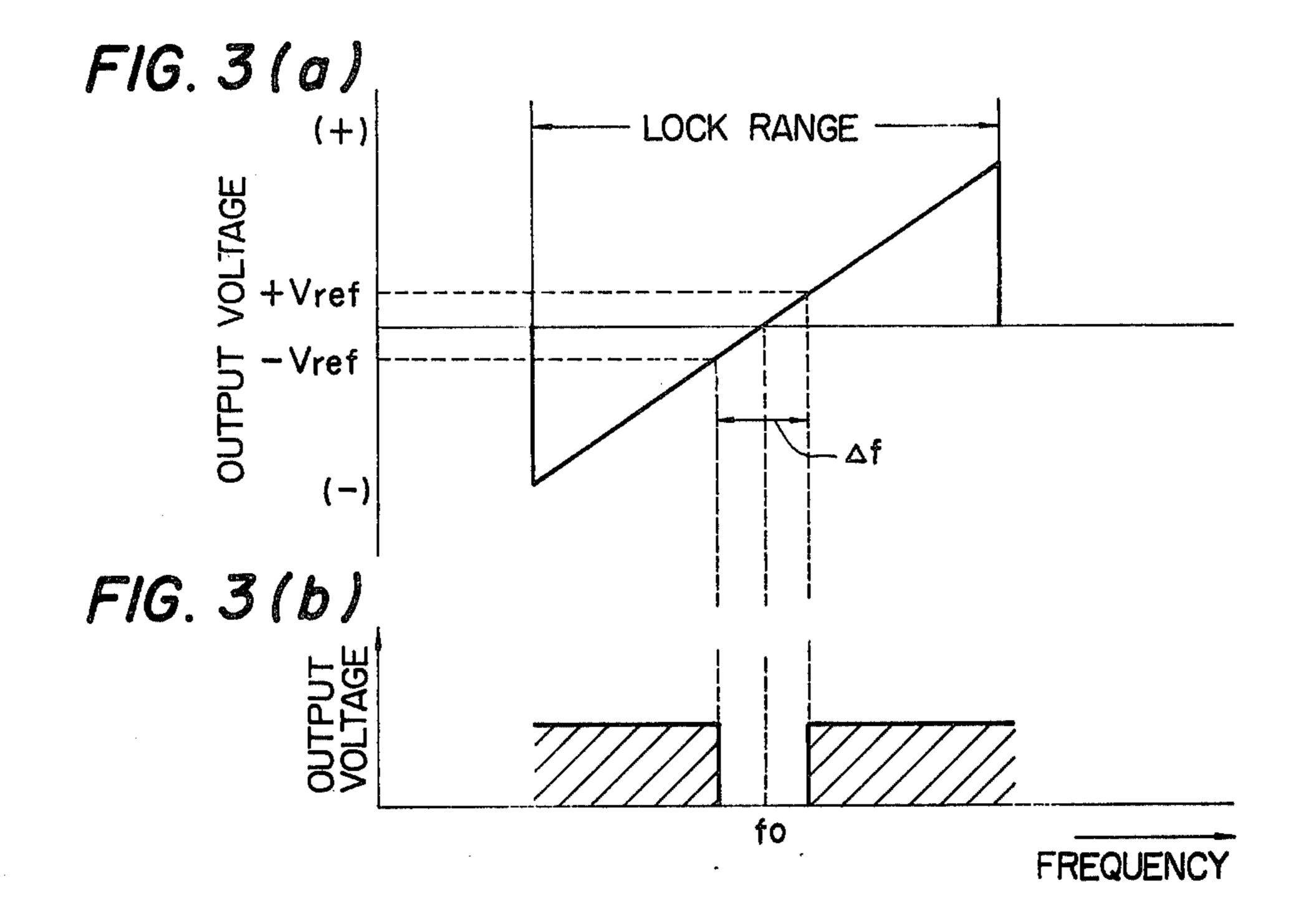


FIG. 2





PLL DETECTION CIRCUIT

BACKGROUND OF THE INVENTION

This invention relates to a PLL (phase locked loop) detection circuit.

FIG. 1 is a circuit diagram showing a conventional PLL detection circuit. In FIG. 1, a predetermined signal ei is applied to one input terminal of a phase comparator 1, to the other input terminal of which the oscillation output of a VCO (voltage-controlled oscillator) 2 is applied. Thus, the phase comparator provides an output according to the difference in frequency and phase between the oscillation output and the FM input signal ei. The output of the phase comparator 1 is converted into a DC voltage by a loop filter 3. The DC voltage, after being amplified by a DC amplifier 4, becomes a detection output, and is applied, as a control voltage, to the VCO 2.

The loop filter 3, for instance, comprises: a resistor R_1 is connected between the output terminal of the phase comparator 1 and the input terminal of the DC amplifier 4; and a series circuit of resistors R_2 and R_3 and a capacitor, which is connected between the output terminal of the resistor R_1 and ground. A transistor Q_0 is connected in parallel with the resistor R_3 . In response to a control signal V_B which is produced when a turning point is substantially detected, the transistor Q_0 short-circuits the resistor R_3 , to change the time constant of the loop filter 3, to thereby make the filter characteristic narrow and to reduce the lock-in time. In providing the PLL detection circuit in the form of an integrated circuit, the capacitor C_1 is externally connected to a terminal (or a pin) A.

In the PLL detection circuit thus organized, the time constant of the loop filter 3 is changed by the switching operation of the transistor Q₀. However, this method is disadvantageous in that, when the transistor Q₀ is employed as the switching element, a DC offset voltage 40 occurs which produces spike noise and makes the PLL loop unstable.

SUMMARY OF THE INVENTION

Accordingly, an object of this invention is to provide 45 a PLL detection circuit in which the above-described difficulties have been eliminated by suppressing the occurrence of the offset voltage in switching the time constant of the loop filter.

A specific feature of the PLL detection circuit according to this invention resides in that the time constant of the loop filter is changed by a diode switch circuit which comprises: first and second diodes the cathodes of which are connected respectively to both ends of at least one of the elements which defines a time 55 constant for the loop filter, with the anodes thereof connected to each other; third and fourth diodes the anodes of which are connected respectively to the two ends of the element, with the cathode thereof connected to each other; and means for activating the first through 60 fourth diodes in response to a predetermined signal.

BRIEF DESCRIPTION OF THE DRAWINGS

One embodiment of this invention will be described with reference to the accompanying drawings, in 65 which:

FIG. 1 is a circuit diagram showing a conventional PLL detection circuit;

FIG. 2 is a circuit diagram showing one example of a PLL detection circuit according to this invention;

FIG. 3(a) is a waveform diagram showing a detection output; and

FIG. 3(b) is a waveform diagram showing the output of a zero volt switch circuit in FIG. 2.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 2 is a circuit diagram showing an embodiment of this invention. In FIG. 2, those elements which have been described with reference to FIG. 1 are therefore designated by the same reference numerals or characters. In FIG. 2, reference numeral 5 designates a zero volt switch circuit which detects when the output of the switch filter 3 amplified by the DC amplifier 4, i.e., when the detection output is in a predetermined level range, at which time it provides a detection signal. Thus, the zero volt switch circuit is a type of window comparator. The circuit 5 comprises an operational amplifier OP₁ which receives the detection output through its non-inversion input terminal; and an operational amplifier OP₂ which receives the detection output through its inversion input terminal. A reference voltage V_{ref} is applied to the inversion input terminal of the operational amplifier OP₁ and the non-inversion input terminal of the operational amplifier OP2, respectively, through resistors R4 and R5. The inversion input terminal of the amplifier OP1 is connected through a resistor R₆ to a power source +B, and the non-inversion input terminal of the amplifier OP2 is grounded through a resistor R₇. The outputs of the operational amplifiers OP₁ and OP₂ are applied through diodes D₁ and D₂ and a resistor to a delay circuit 6. The delay 35 circuit 6 comprises a transistor Q₁, a resistor R₁ and a capacitor C₂. The output of the delay circuit 6 is applied to a diode switch circuit 7 adapted to change the time constant of the loop filter 3.

The diode switch circuit 7 comprises first and second diodes D₃ and D₄ the cathodes of which are connected to both ends of at least one of the elements defining the time constant of the loop filter 3 (which is for instance the resistor R₂), with the anodes being connected together; third and fourth diodes D₅ and D₆ the anodes of which are connected to both ends of the resistor R₂, with the cathodes being connected together; and a current mirror circuit for activating these diodes D₃ through D₆ in response to the output of the delay circuit 6. The current mirror circuit comprises a diode-connected transistor Q2; a transistor Q3 having its base connected to the base of the transistor Q2 and having its collector connected to the connecting point of the anodes of the diodes D₃ and D₄; a transistor Q₄ having its collector connected to the collector of the transistor Q2 and receiving the ouptut of the delay circuit 6 through its base; and a transistor Q5 having its base connected to the base of the transistor Q4 and having its collector connected to the connecting point of the cathodes of the diodes D_5 and D_6 . The emitters of the transistors Q_2 and Q₃ are connected respectively through resistors R₁₀ and R₁₁ to the power source +B, and the emitters of the transistors Q4 and Q5 are grounded respectively through resistors R₁₂ and R₁₃. The base of the transistor Q₄ is grounded through diodes D₇ and D₈.

When, in the circuit thus organized, the frequency of the input signal ei is gradually swept and the input signal ei comes within the locking range of the PLL detection circuit, the PLL detection circuit is readily locked since the filtering characteristic of the PLL detection circuit is of a wide band. FIGS. 3(a) and 3(b) show the waveform of the detection output and the waveform of the output of the zero volt switch circuit 5, respectively. If the frequency of the input signal ei is out of the band 5 Δf , then the detection output level is out of the range of from $-V_{ref}$ to $+V_{ref}$, and therefore the zero volt switch circuit 5 produces a high level output. Since this output is applied through the delay circuit to the diode switch circuit 7, the current mirror circuit is placed in an "off" 10 state, and accordingly the diodes D₃ through D₆ are placed in "non-active" states. Accordingly, the resistor R₂ is not short-circuited, and therefore the time constant of the loop filter 3 is defined by the resistors R₁ through R₃ and the capacitor C₁ and the wide band filtering 15 characteristic of the PLL is maintained unchanged.

When the input signal ei comes within the band Δf , the detection output level is in the range of from $+V_{ref}$ to $-V_{ref}$, and therefore the zero volt switch circuit 5 provides a low level output. In response to the low level 20 output, the current mirror circuit in the diode switch circuit 7 is placed in an "on" state, and therefore the diodes D_3 through D_6 are activated. As a result, the resistor R_2 is short-circuited, and therefore the time constant of the loop filter 3 is defined now by the resistors R_1 and R_3 and the capacitor C_1 . In this case, the PLL filter characteristic is of a narrow band. By further sweeping the input signal ei, the aforementioned wide band state is again obtained.

Since the time constant of the loop filter is changed 30 by the operation of the diodes (D₃ through D₆), the PLL filter characteristic can be changed without generating an offset voltage.

The time constant of the loop filter may be changed by switching a plurality of capacitors. However, if this 35 method is employed, and the PLL detection circuit is manufactured in the form of an integrated circuit, the number of terminals (or pins) of the integrated circuit must be increased because the number of capacitors which are externally connected thereto is increased. 40

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However, if the circuit according to this invention is employed, the number of such terminals is only one in correspondance to the capacitor C₁. The PLL detection circuit according to this invention can be suitably applied to an AM-FM stereo system AM receiver.

What is claimed is:

1. A phase lock loop detection circuit of the type comprising a loop filter having a time constant determined by a plurality of elements, means for detecting when an output of said loop filter is in a predetermined level range and providing a detection signal, and a switch circuit for changing a time constant of said loop filter in response to said detection signal, the improvement characterized in that said switch circuit comprises:

first and second diodes having cathodes which are connected respectively to both ends of at least one of said elements and anodes which are connected together;

third and fourth diodes having anodes which are connected respectively to said both ends of said one element, and cathodes connected together; and activating means for activating said first, second, third and fourth diodes in response to said detection signal.

2. A phase lock loop detection circuit as claimed in claim 1; wherein said activating means comprises a current mirror circuit having first and second current paths, said first current path conducting in response to said detection signal and said second current path being connected in series with said diodes.

3. A phase lock loop detection circuit as claimed in claim 1, further comprising delay means between said means for detecting and said activating means for delaying the operation of said activating means in response to said detection signal.

4. A phase lock loop detection circuit as claimed in claim 1, wherein said output of said loop filter is taken from the cathode of one of said first and second diodes.

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