

[54] **CONTROL SYSTEM AND METHOD FOR LIMITING POWER DEMAND OF AN INDUSTRIAL PLANT**

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[51] Int. Cl. .... **G06f 15/06, G05b 15/00**

[58] Field of Search .... **235/151.21; 324/103; 307/52; 444/1**

[56] **References Cited**

**UNITED STATES PATENTS**

3,296,452 1/1967 Williams ..... 235/151.21 X

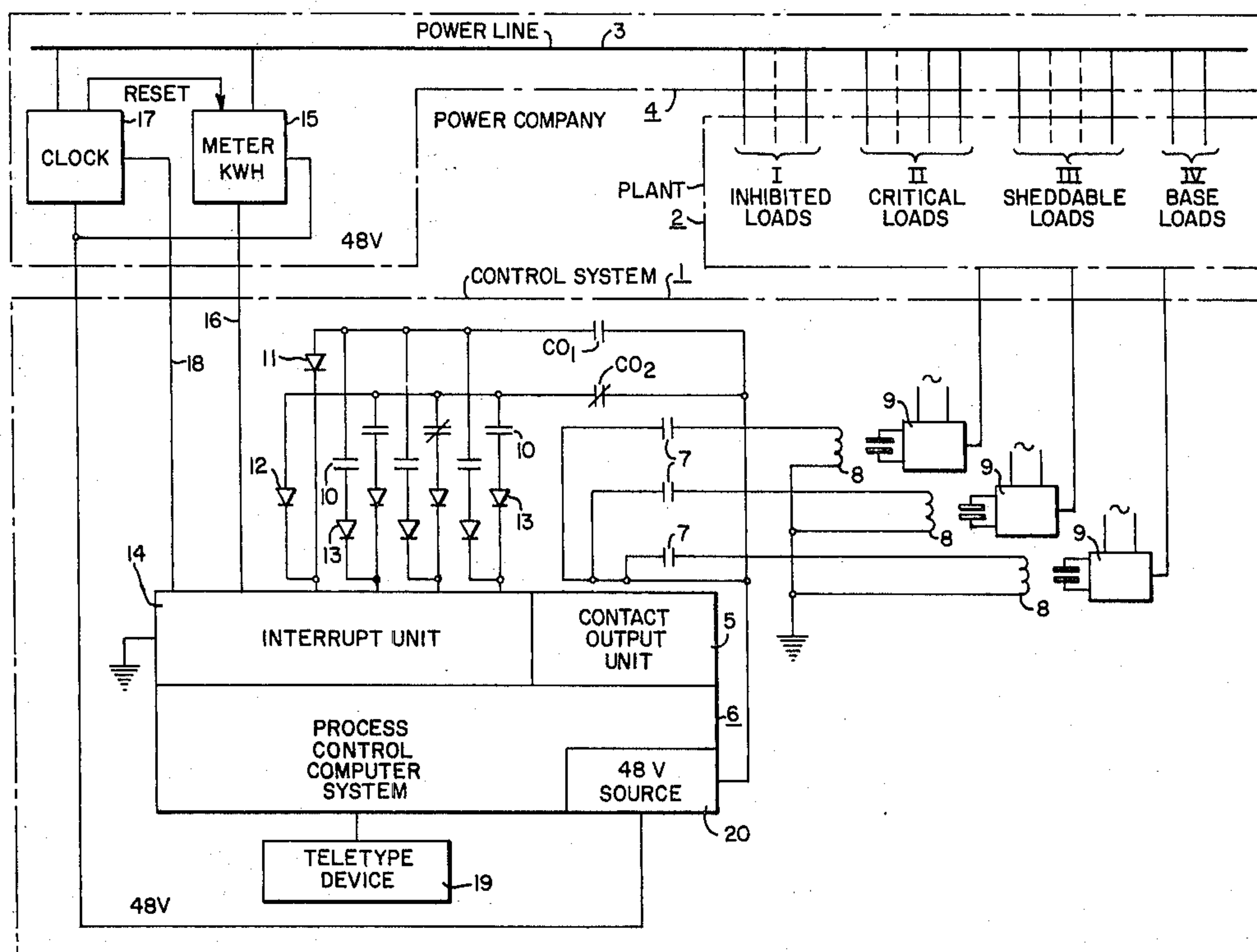
3,505,508	4/1970	Leyde .....	235/151.21 X
3,522,421	8/1970	Miller .....	235/151.21
3,602,703	8/1971	Polenz .....	235/151.21
3,659,114	4/1972	Polenz et al. ....	235/151.21 X
3,719,809	3/1973	Fink .....	235/151.21

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## [57] ABSTRACT

The invention relates in general to control of the consumption of energy derived by an industrial user from a power supply system (electrical, gas or like commodity), and more particularly to a control system for adjusting an industrial load system to limit the demand of power while respecting the constraints of the load system.

**3 Claims, 20 Drawing Figures**



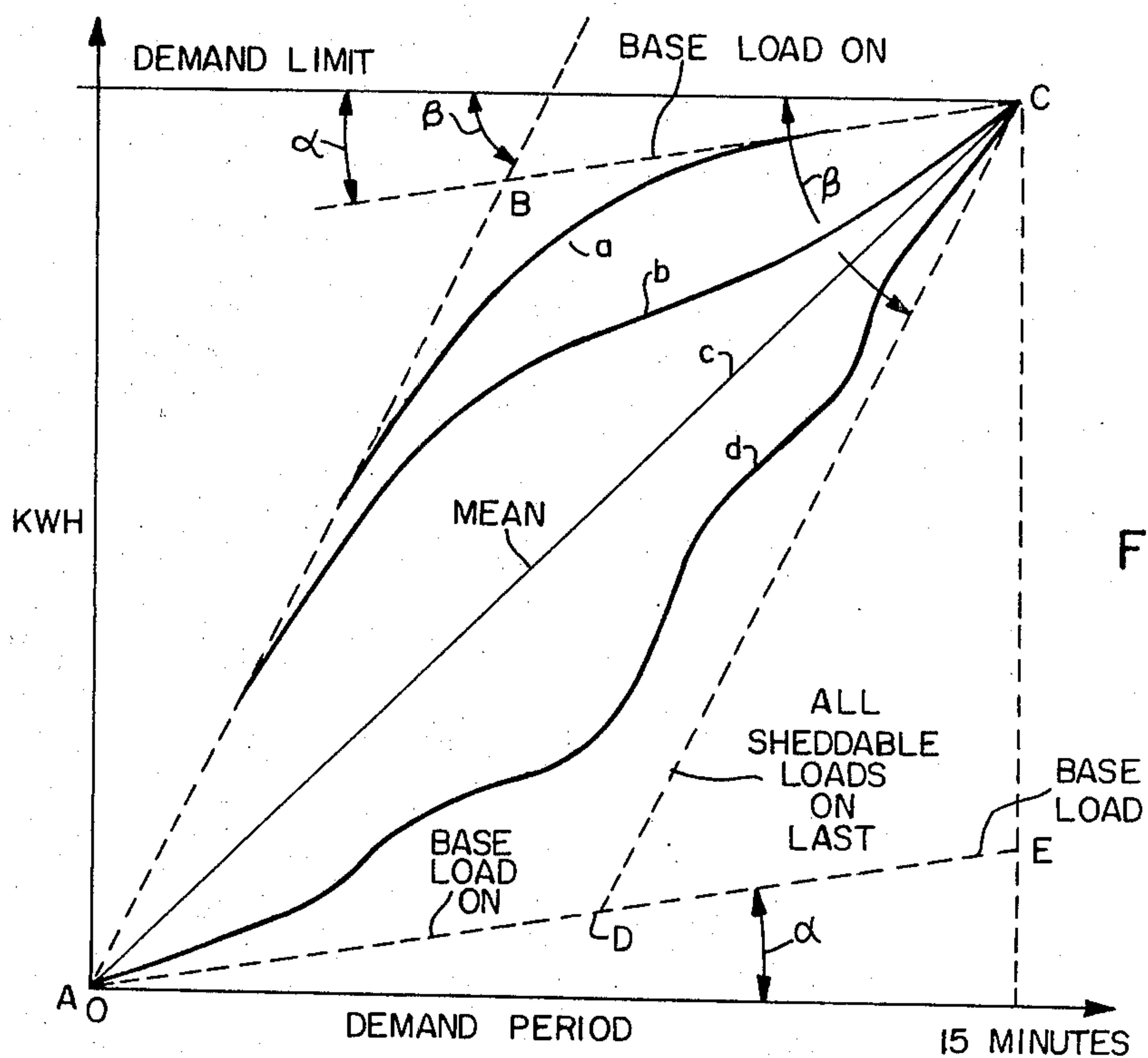


FIG. 1

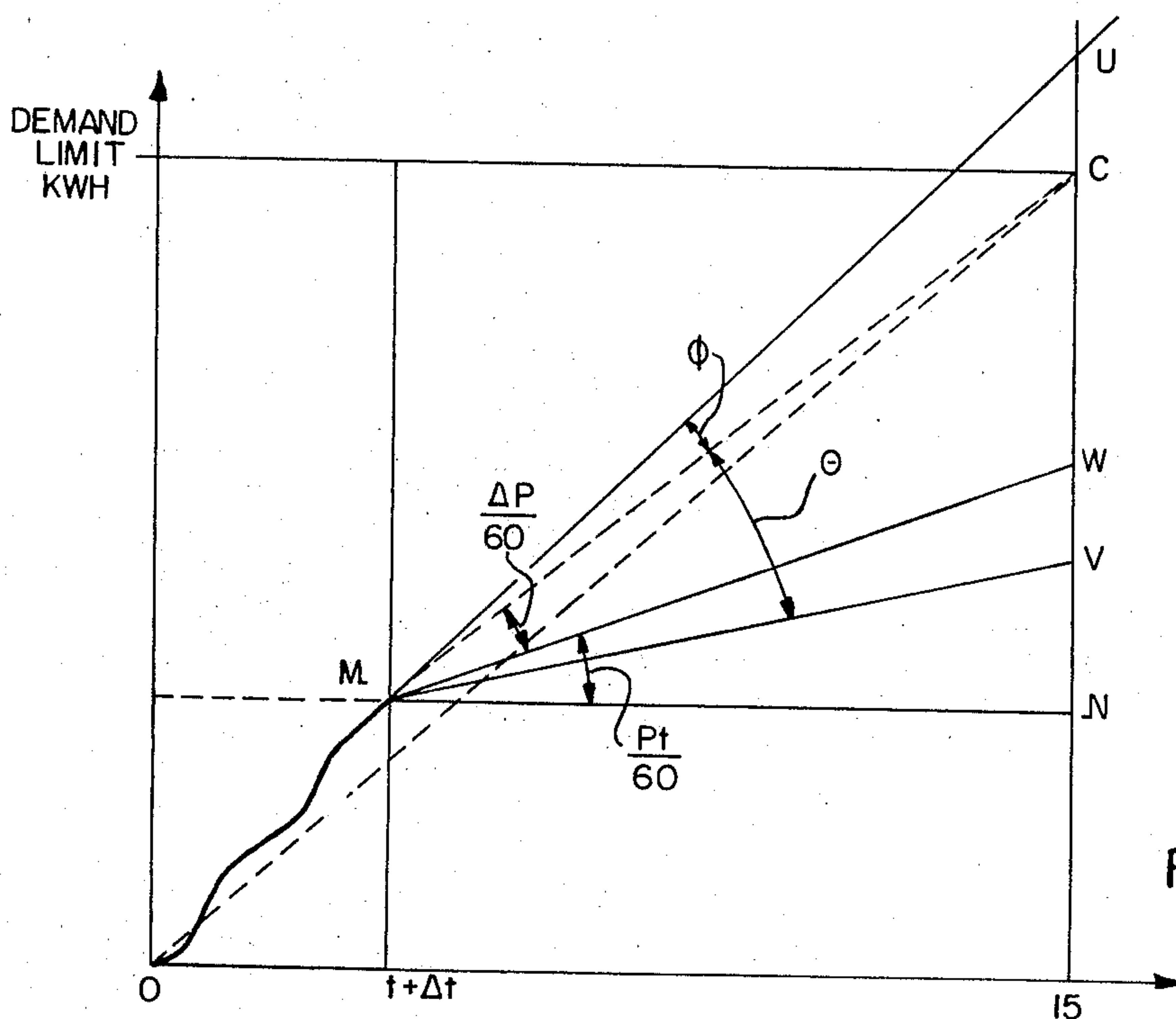
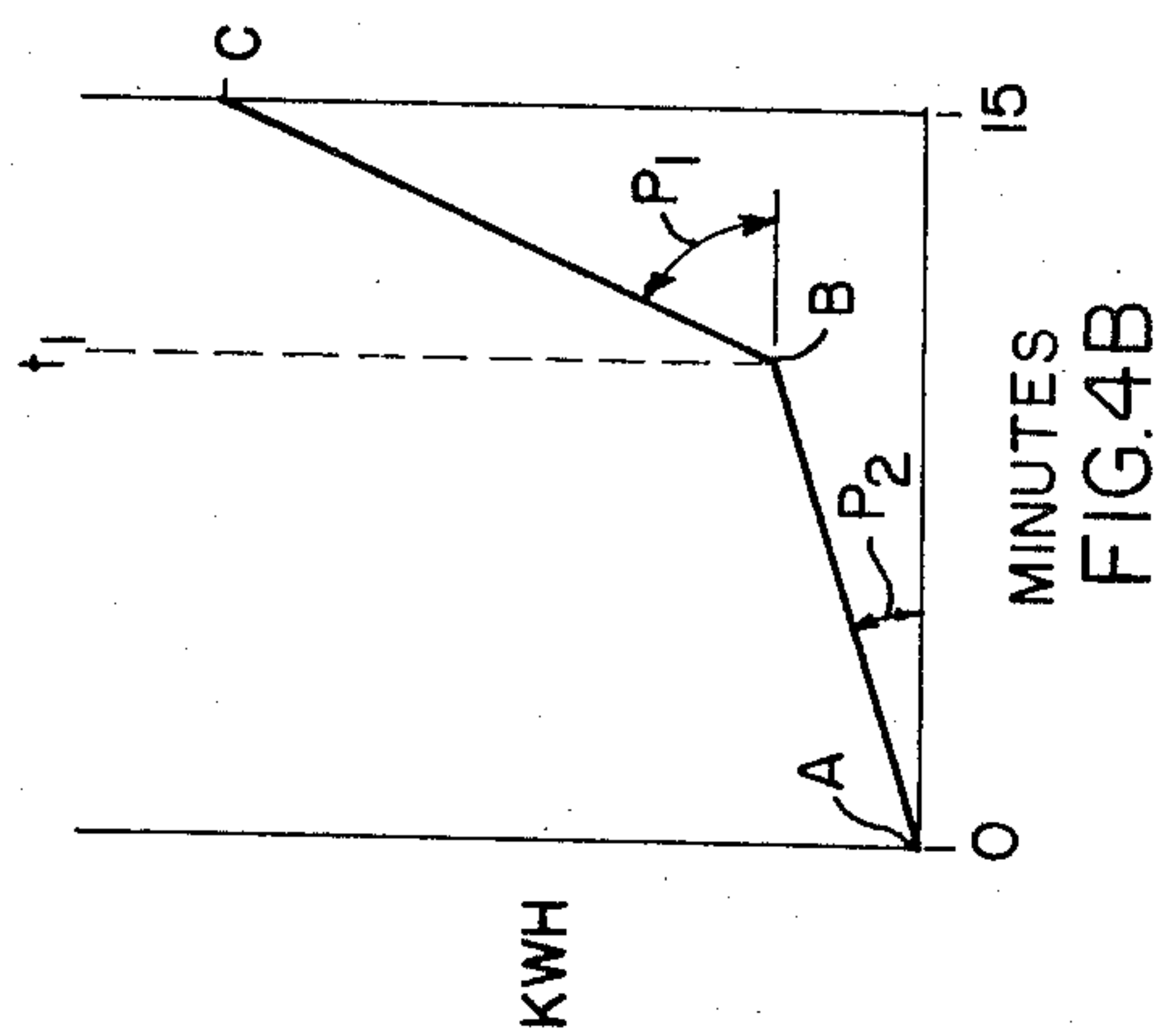
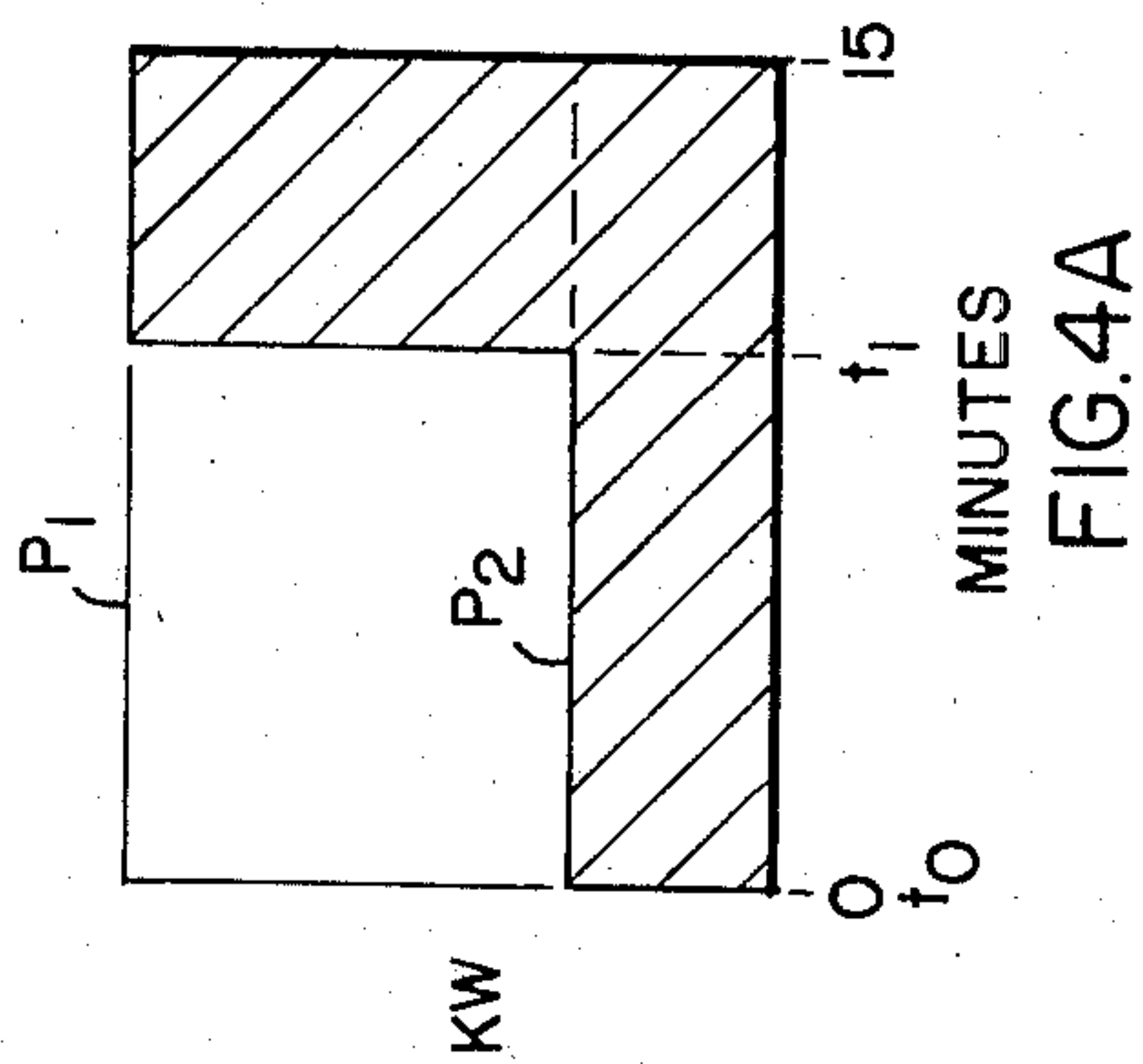
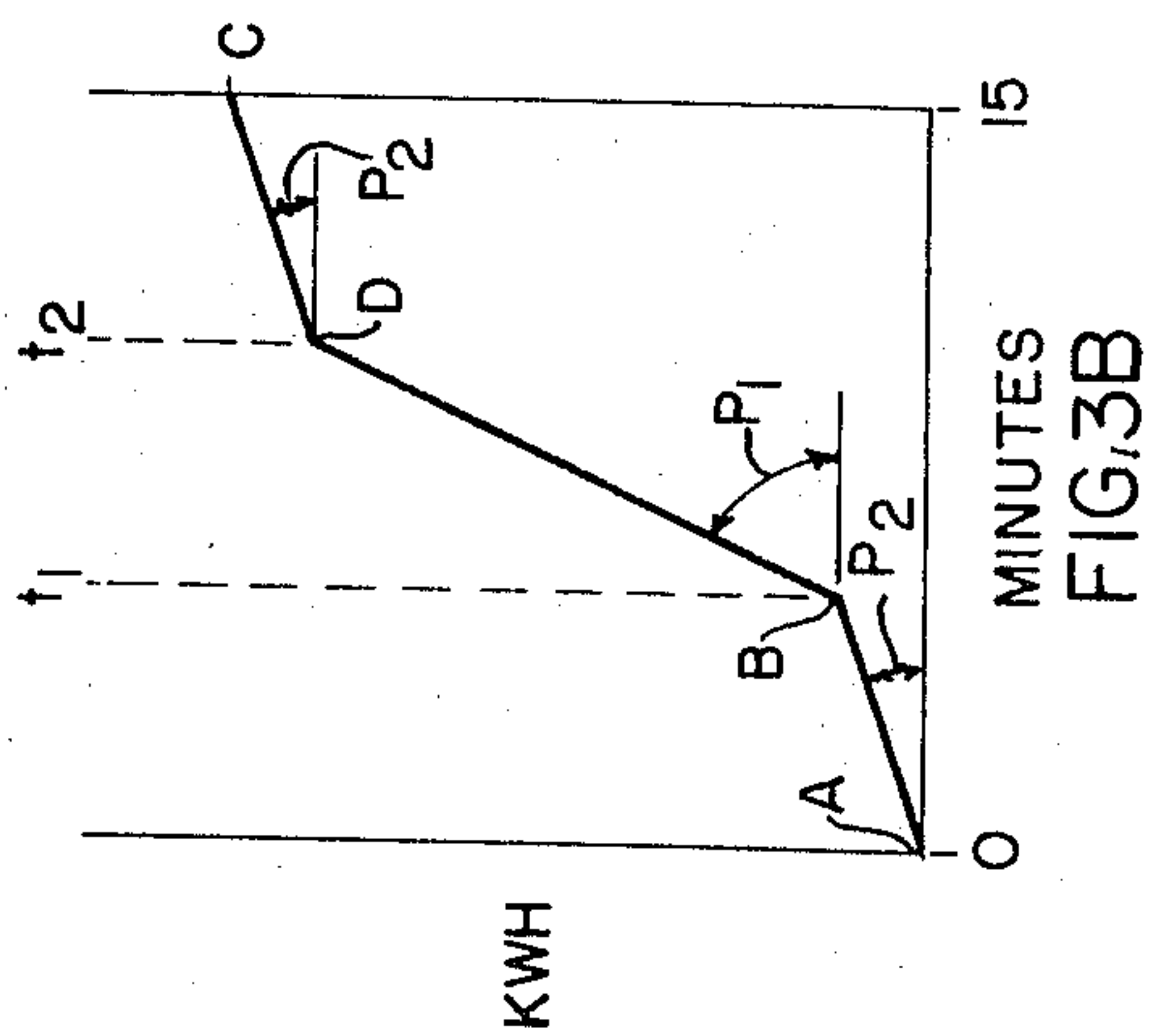
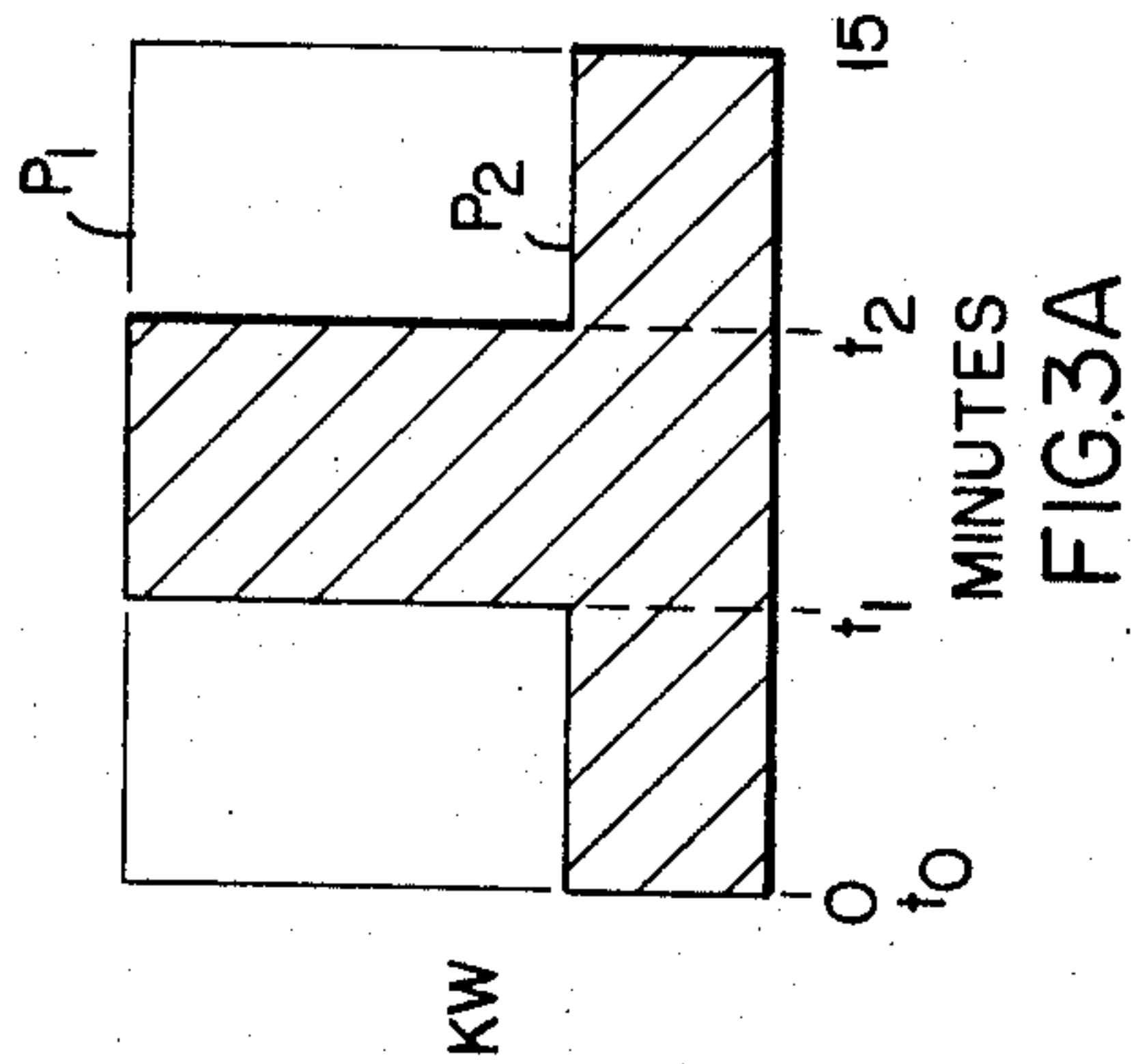
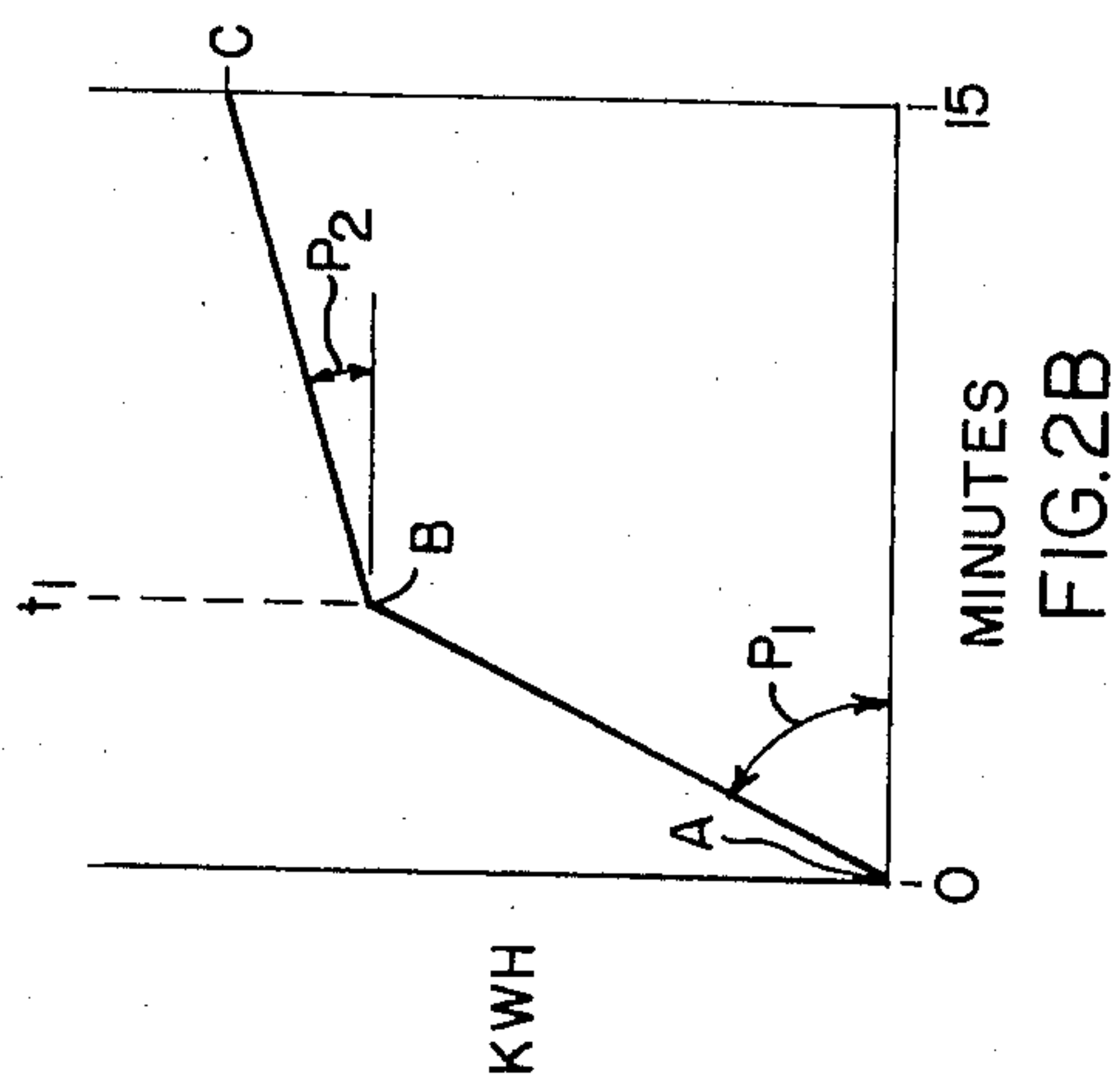
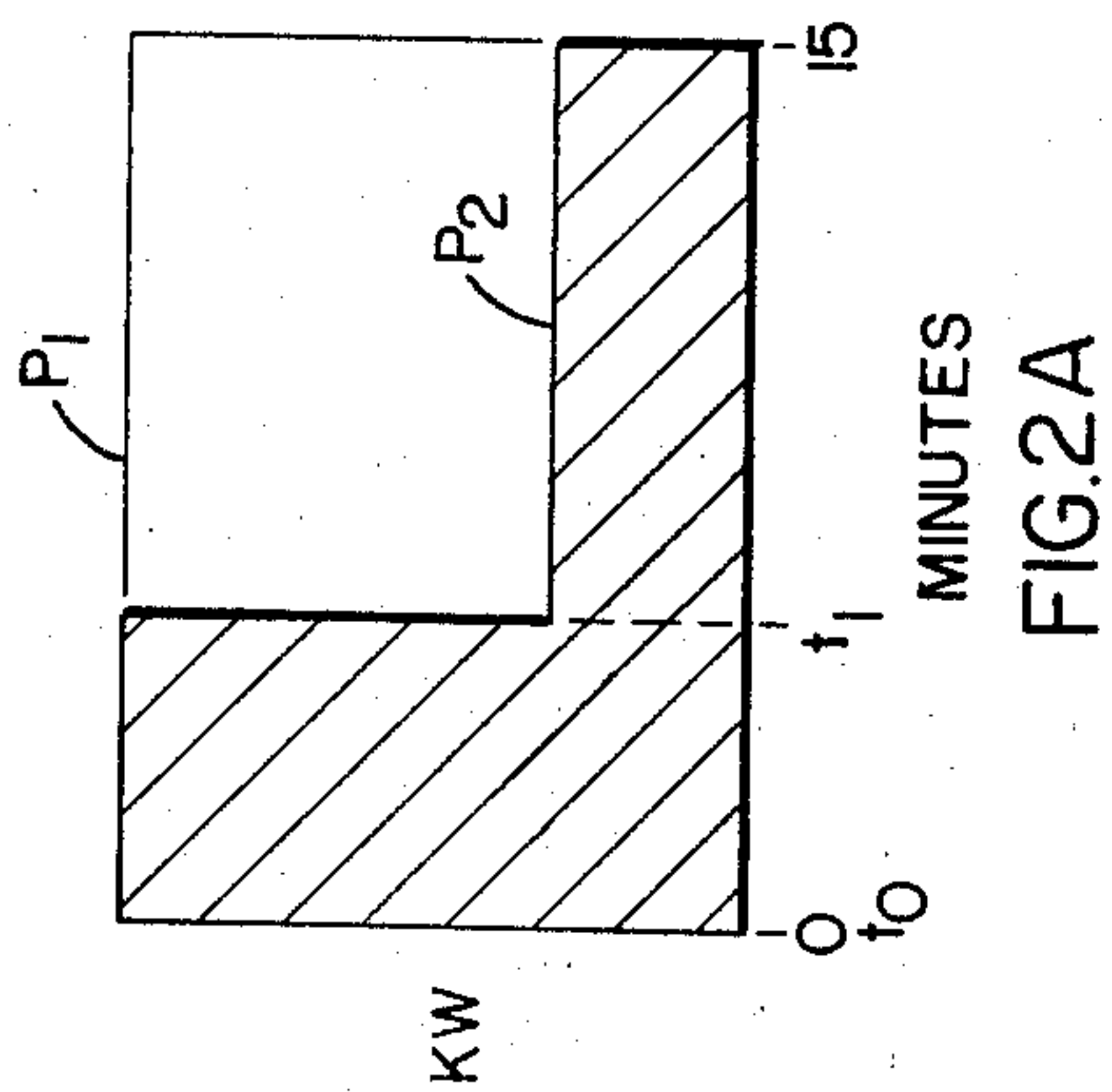
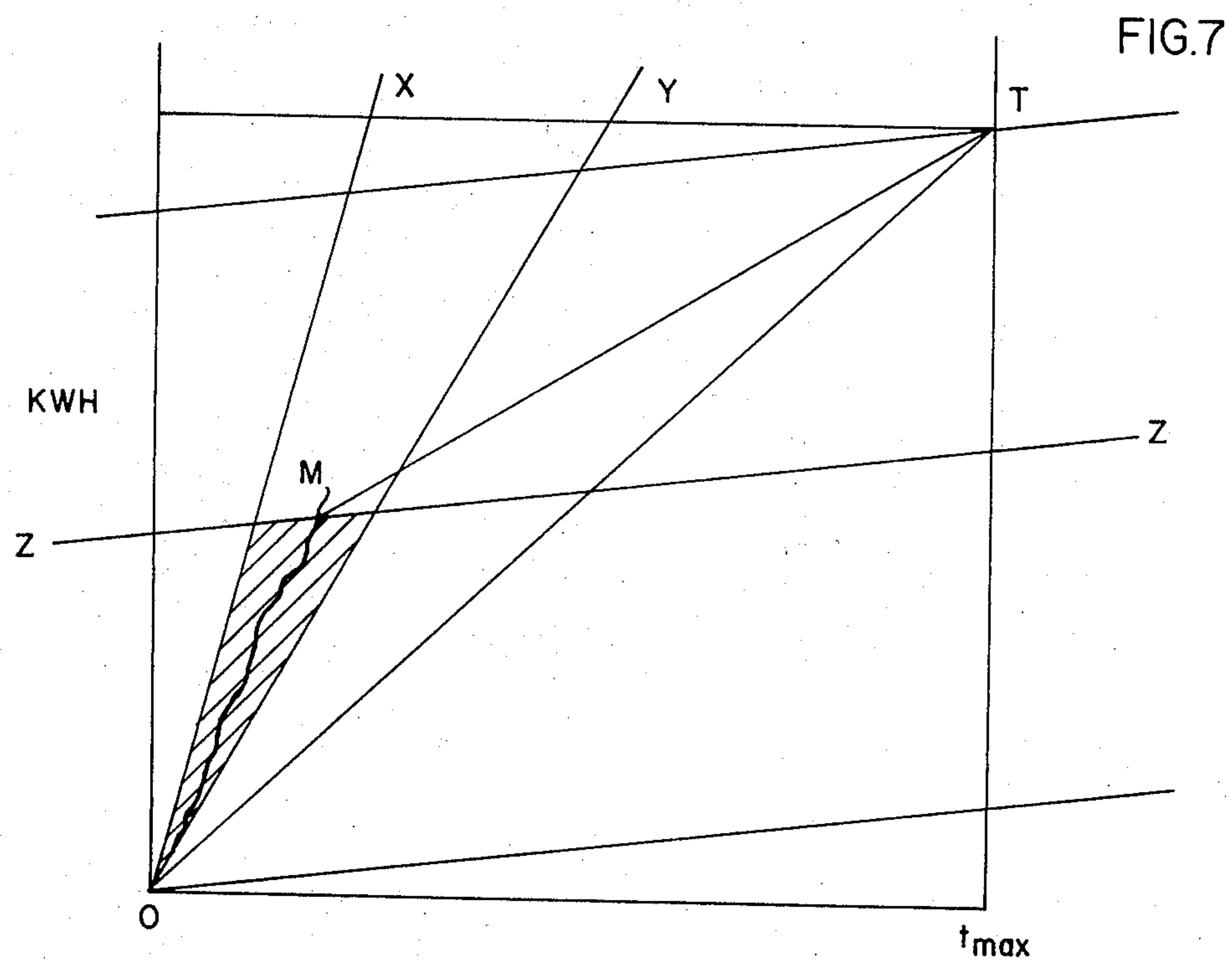
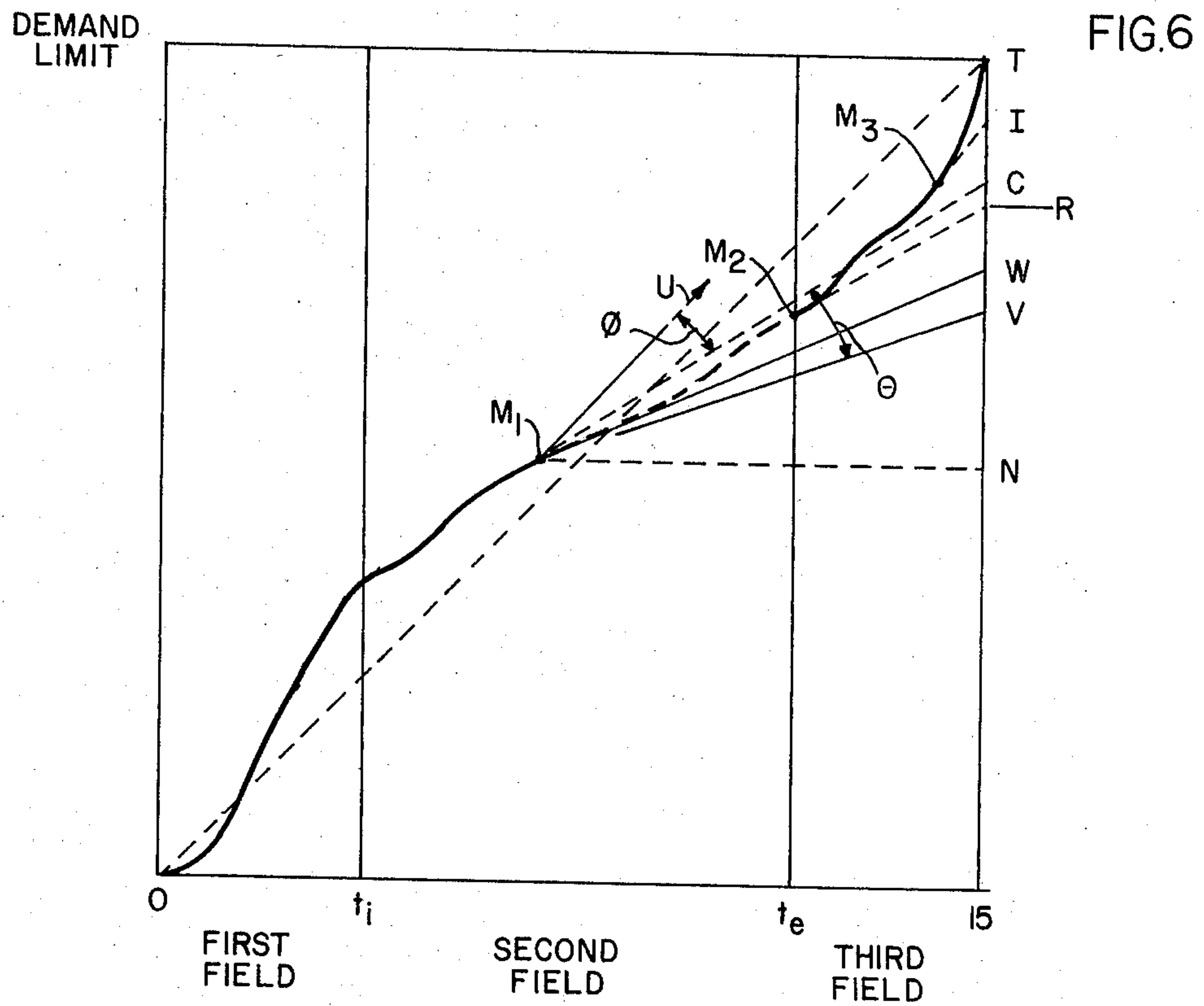
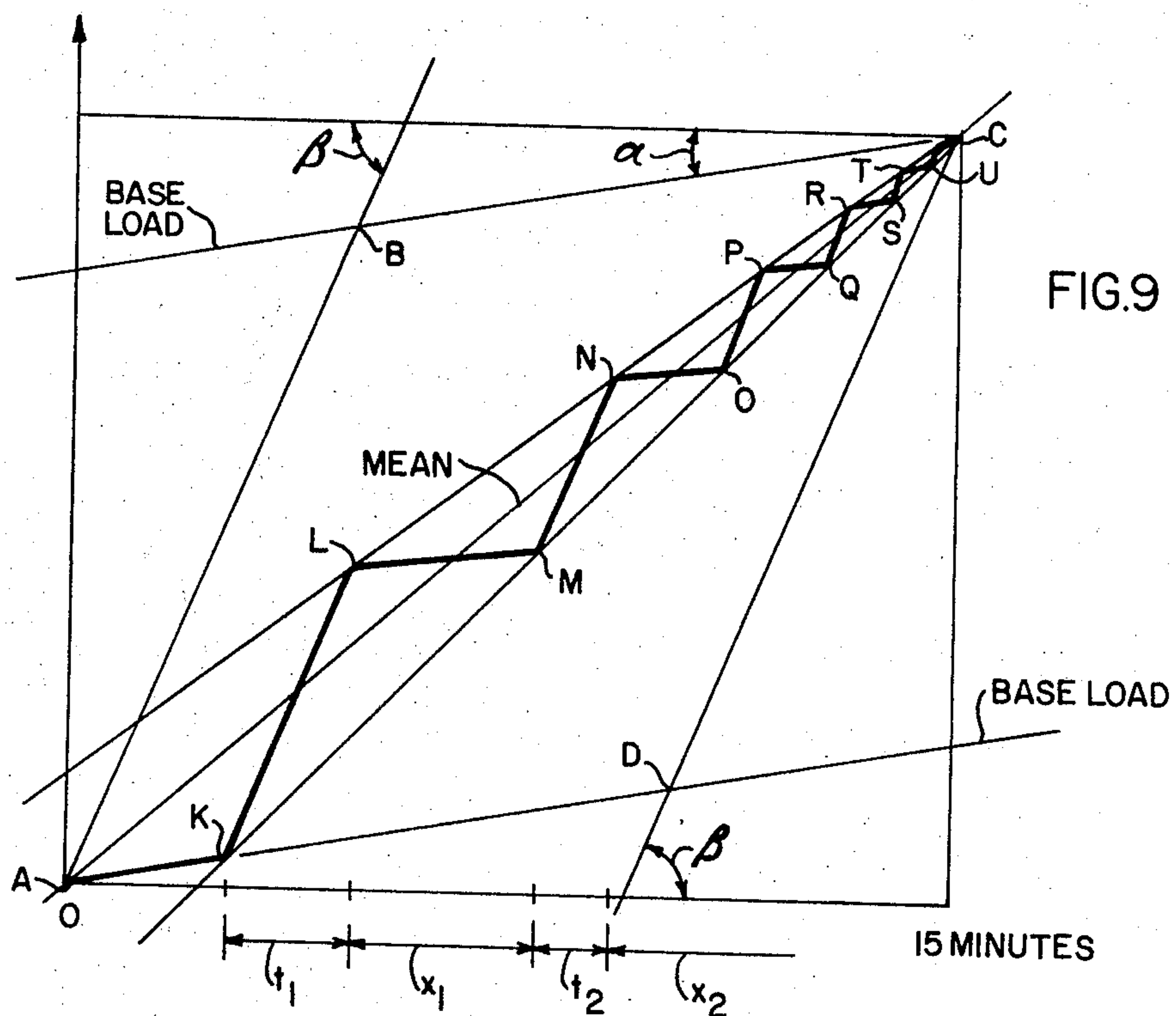
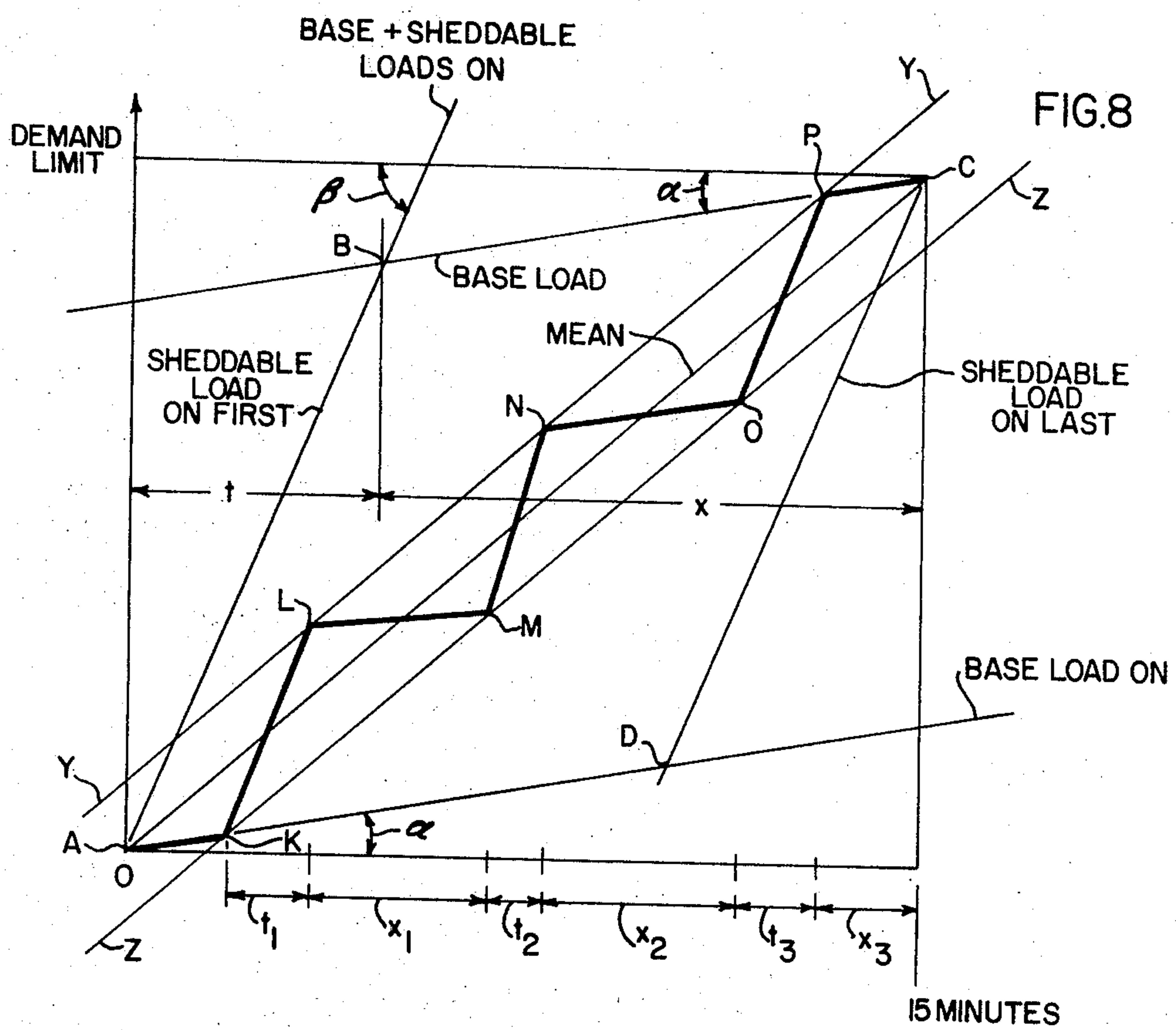


FIG. 5









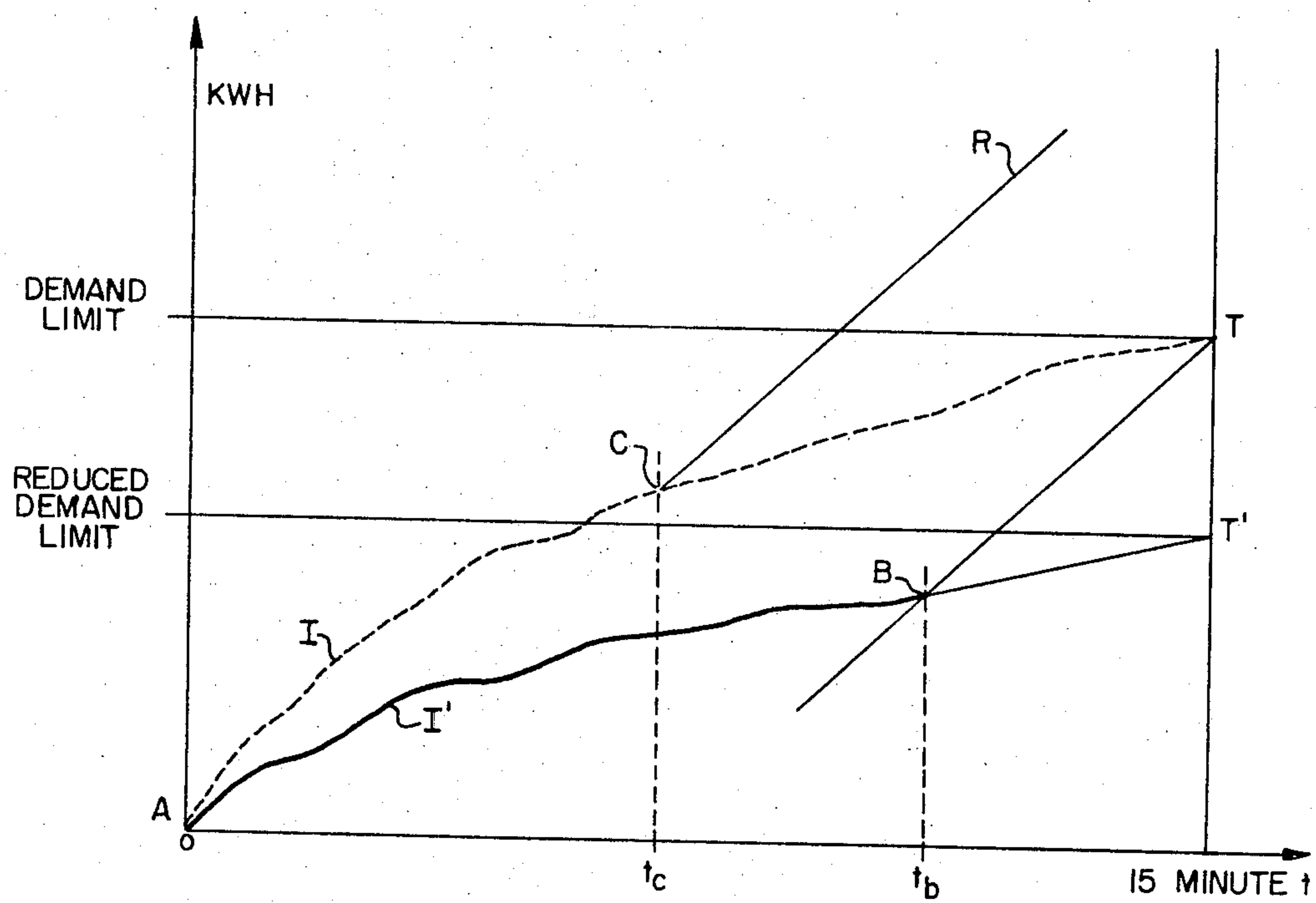


FIG. 10

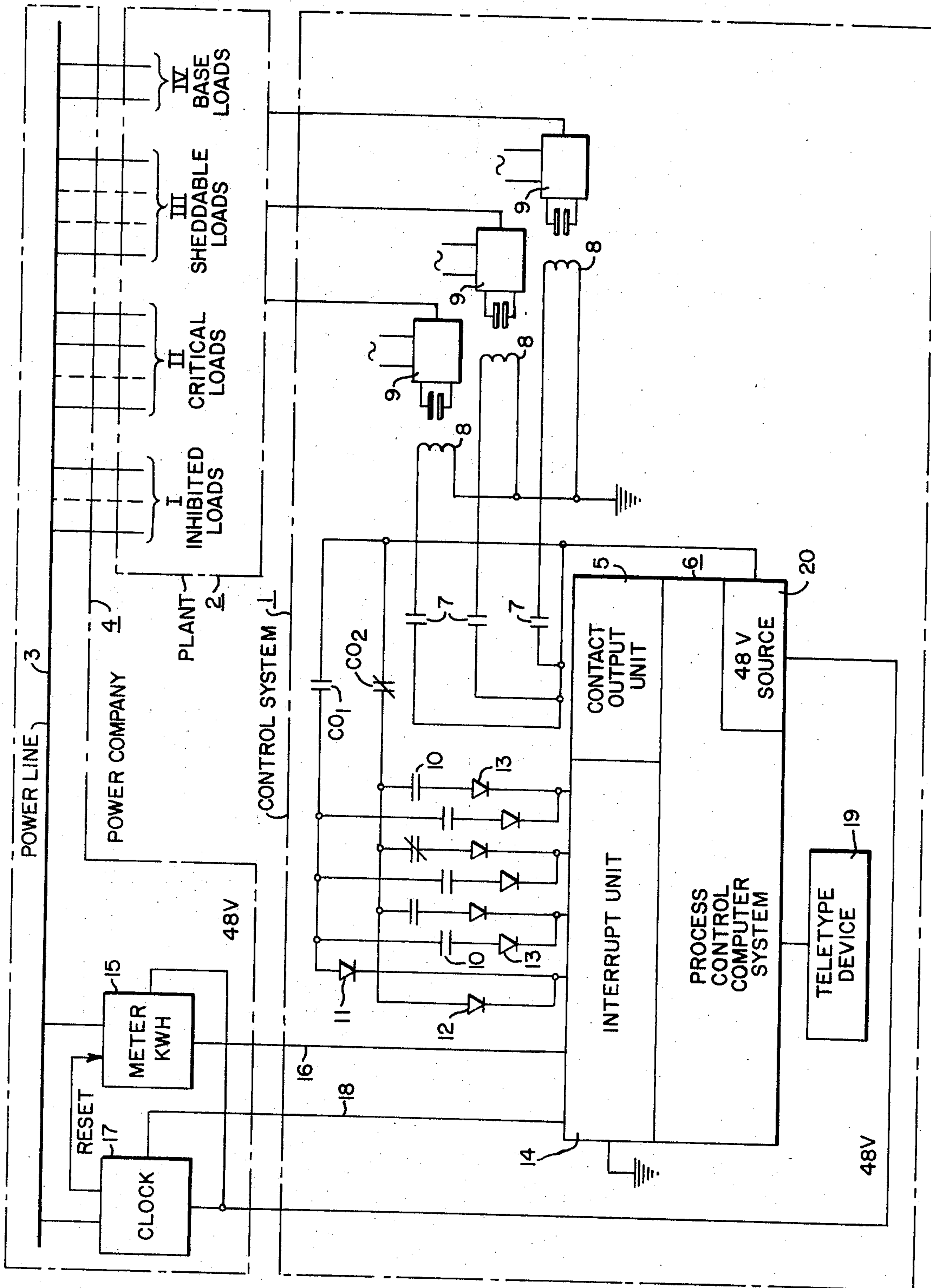
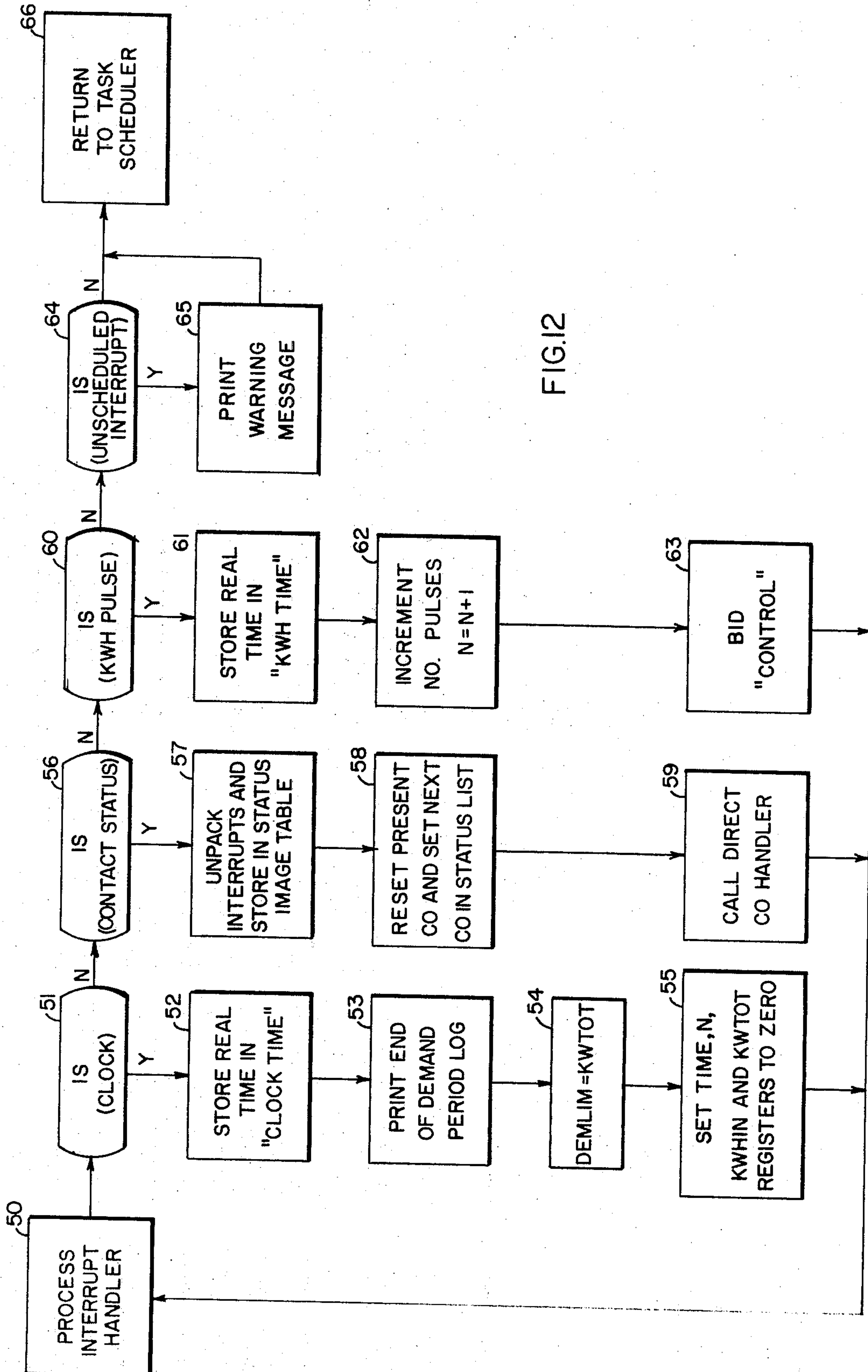
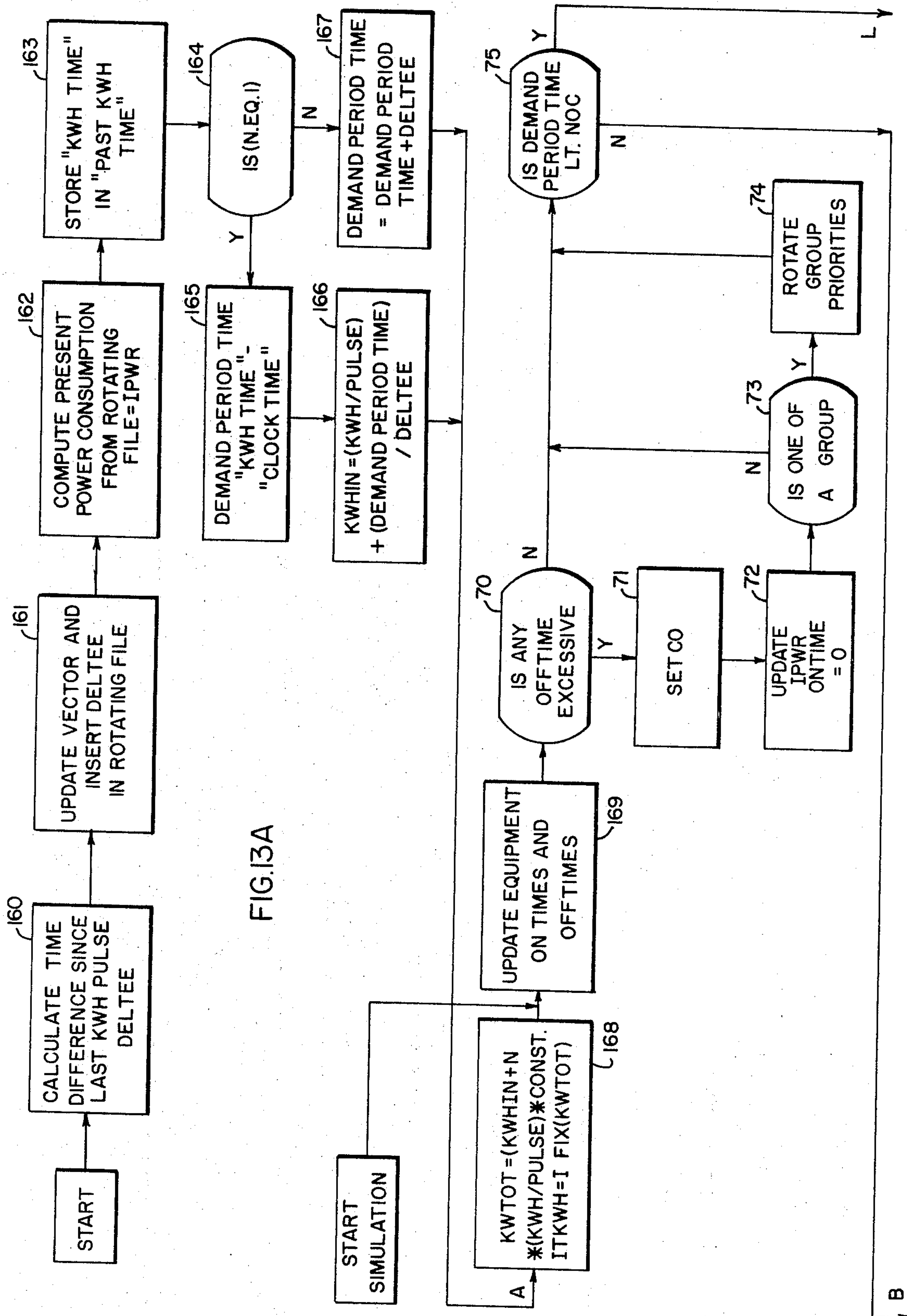


FIG. 11







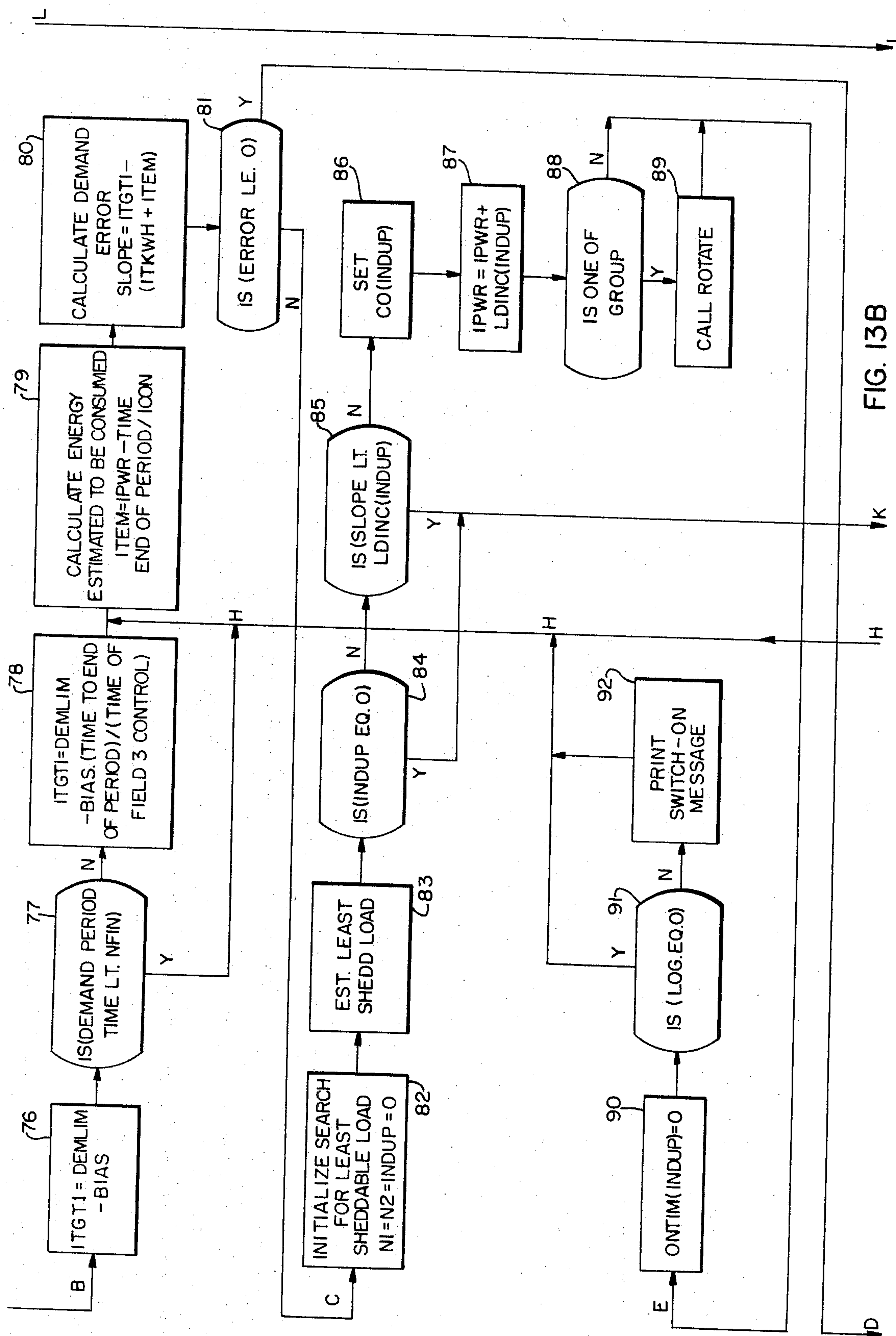
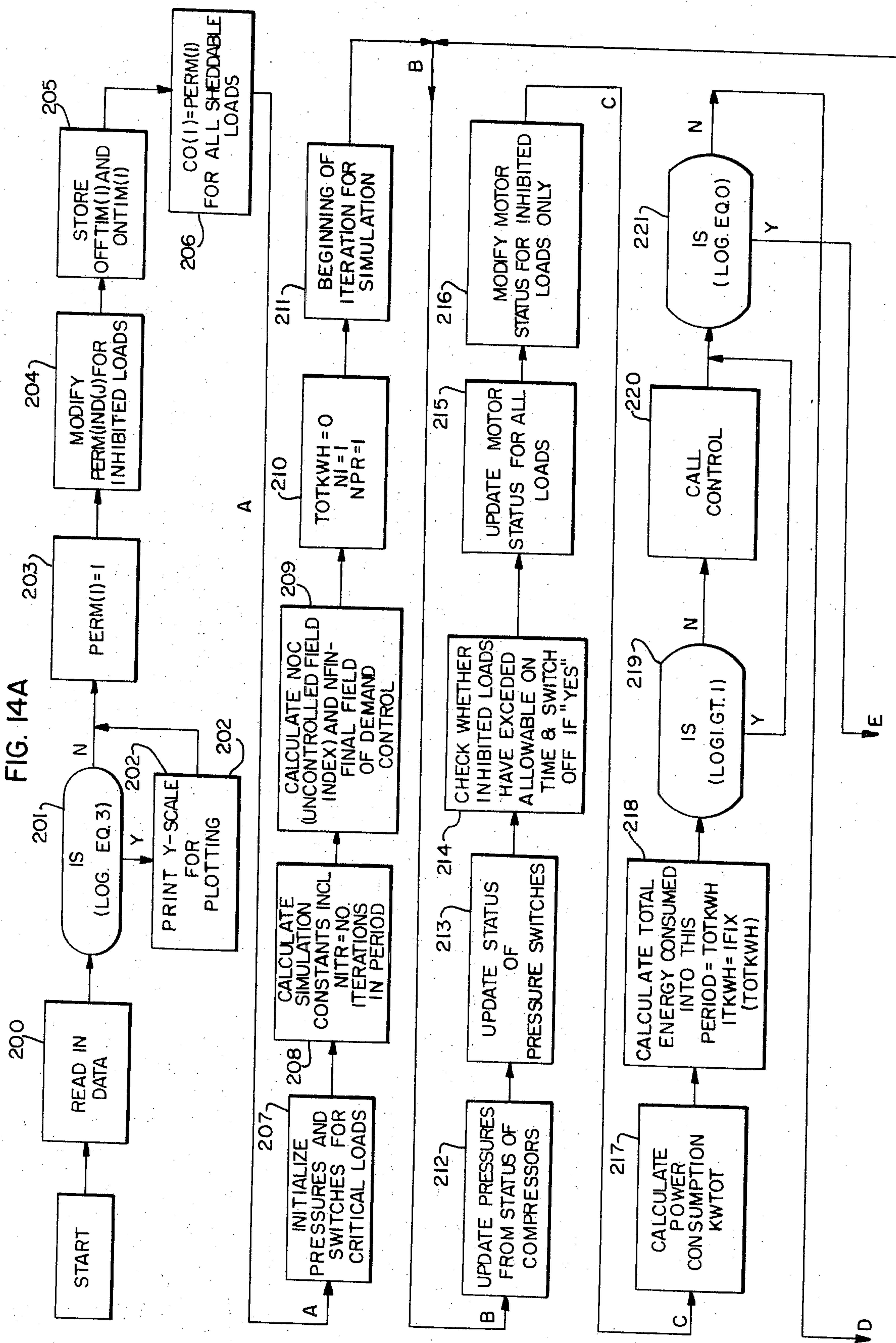
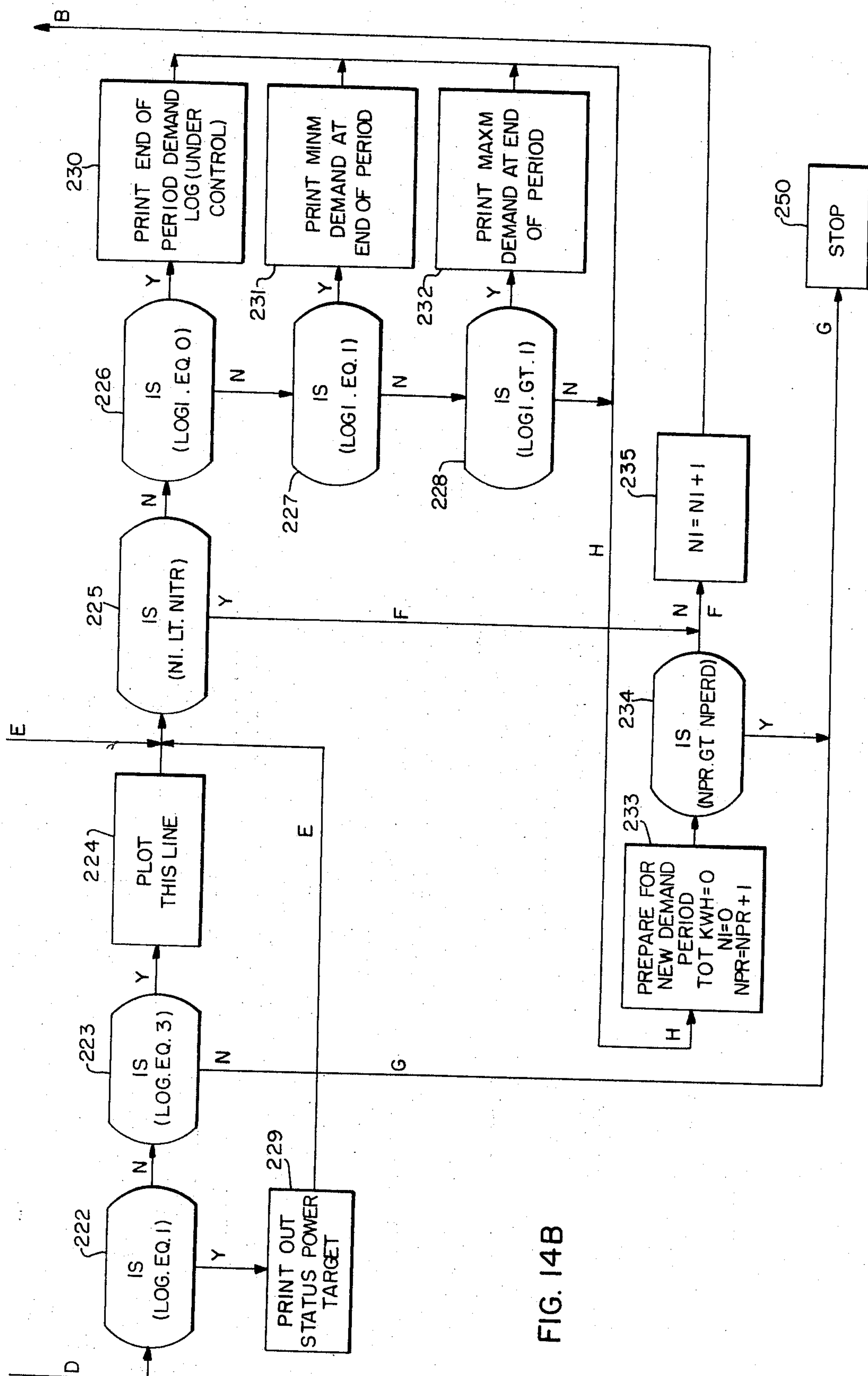




FIG. 14A









# CONTROL SYSTEM AND METHOD FOR LIMITING POWER DEMAND OF AN INDUSTRIAL PLANT

## BACKGROUND OF THE INVENTION

When a load is connected by an industrial customer on a power system the cost of the energy consumed is generally billed by the power supply company on the basis of the total amount of power having flow within a billing period. The more power that is used, the more is the cost to the customer, and a cost-conscious customer, provided he has the choice, will at times cut the total load or at least reduce it. When a plurality of interruptible loads are connected on the power system, the final cost will depend on the overall distribution of the active loads. It is important for the customer or user to decide what the distribution of the loads should be within a given demand period, as well as between respective demand periods, and for the purpose to selectively control the load distribution. Such decision making is particularly important with electrical loads in view of the practice by the power supply utility companies to charge the cost of supplied power with progressive rates in relation to the higher amounts of total power within a given demand period, and also in relation to the highest level of power reached within the demand period. The rate based on the amount of power is an incentive for the user to maximize the consumption during the period, thereby to help improve the utilization of the generating plants and the power transmission systems. The progressive rate on the total demand accounts for the increased facilities provided by the power company to meet the user's demand and for the capital costs involved.

It is known from an article entitled "Electric Demand Can Be Controlled" published in *Power*, November 1970, pages 58, 59 by Norman Peach, to use a digital computer control system in order to instantaneously determine within a demand period the trend of power consumption, to forecast the total amount of power at the end of the period and to either add or shed the loads of a plant so as to be able to keep the anticipated demand as close as possible to a predetermined demand limit. While such a control system, or method, provides for a more economical use of the power available from a power supply utility company without exceeding the total amount of KWH permissible at a given rate during the demand period, the prior art control system, and method, do not take into account the constraints imposed by the customer's industrial plant on the use of the loads.

It is an object of the present invention to effect demand control with increased accuracy, thereby to insure all the economic advantages which can be gained by running a load system with as high a load factor as reasonably practical.

It is another object of the present invention to make use of improved digital computer technology at a minimum cost within the economic gain attainable by control of a power demand.

It is a further object of the present invention to keep the anticipated power demand of a load system within limits while respecting the constraints imposed on the loads by the load system.

Still another object of the present invention is to achieve an improved control of a customer user's

power demand through anticipation of the power demand with a minimum of control operations.

It is still an object of the present invention to control a power demand in relation to anticipated demand and concurrently in relation to simulated load conditions.

## SUMMARY OF THE INVENTION

Briefly, the present invention provides for an improved power demand control system and method for maximizing a customer's power demand rate throughout a finite demand period without exceeding a predetermined demand limit of energy at the end of the period.

A control system is provided for regulating the consumption of power supplied by a power supply system to an industrial load system having a base load and a plurality of interruptible loads and including loads having controllable and non-controllable status. The control system is responsive to time pulses derived from the power supply company meter for equal increments of energy thereby to continuously sample the power consumption. On this basis, the control system computes the anticipated final energy demand which it compares with the desirable demand limit to derive a demand error. In response to the demand error the control system adds or sheds loads selected in accordance with a predetermined priority schedule. The selected loads are controlled to be shed or added against a background of non-controllable loads.

A deadband is introduced during at least a portion of the demand period, and such deadband is made variable under certain conditions, in particular to ease the switching of larger loads.

The control system is operated during a portion of the demand period with a bias relative to the demand limit, and such bias is progressively reduced to zero during another portion of the demand period ending therewith.

Simulation can be used in order to ascertain the effects of control under the established priority and constraints, and such simulation can be used concurrently with actual control to improve decision making and update the information used for decision making, to increase the margin of control or permit emergency measures to be taken under anticipated adverse conditions.

The present invention can be used for control of the consumption of the energy supplied by a power supply company, such as electricity, gas, or like energy. The control system will be described hereinafter in the context of the consumption of electricity from an electrical company.

The loads supplied with energy may be of several types:

- a. Lighting and space heating loads which are normally relatively constant and usually part of the base load.
- b. Loads which are either ON or OFF with short run up times and reasonable starting curves.
- c. Loads with their own ON/OFF controller. Examples of these are air or ammonia compressors, air conditioners, etc.
- d. Loads with extended run-up times and large starting currents.
- e. Large loads of short duration and relatively infrequent occurrence (e.g., test loads).



f. Arc furnaces and similar industrial process equipment where production penalties are paid for increased shut-down period. Safety requirements need also to be observed (e.g., toxicity of atmosphere).

Most of these loads have established constraints which must be respected when attempting to control separately or concurrently several kinds of loads to limit the power demand.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The invention will now be described in the context of the supply of electrical energy by a utility power supply company to an industrial plant, and reference shall be made to the accompanying drawings in which:

FIG. 1 represents the extreme and intermediary KWH/TIME trajectories toward a total value of the KWH established as a limit not to be exceeded when controlling the consumption by shedding or adding loads against a base of unsheddable loads.

FIGS. 2A, 2B, 3A, 3B, 4A, and 4B are curves representing the correlation between KW and KWH consumed during a demand period for three different time distributions of power consumption for the same total of KWH.

FIG. 5 illustrates diagrammatically the principle of calculation of the demand error used in the control system according to the present invention.

FIG. 6 is a diagram showing a strategy of control used in the control system according to the present invention.

FIG. 7 represents control between boundaries in the early part of the demand period irrespective of the demand limit.

FIG. 8 illustrates control on either side of the mean trajectory in relation to two parallel boundaries.

FIG. 9 differs from FIG. 8 in that the two boundaries are converging toward the demand limit at the end of the period.

FIG. 10 illustrates a particular strategy of control in accordance with the present invention.

FIG. 11 is an overview of the control system according to the present invention.

FIG. 12 is a flow chart explaining the operation of the Process Interrupt Handler which is part of the control system according to the present invention.

FIGS. 13A, 13B and 13C show an illustrative logic flow chart of a program according to the present invention.

FIGS. 14A and 14B show an illustrative logic flow chart of a simulation program that can be used with the control system according to the present invention.

To be in the context of the present invention it will be hereinafter assumed that the power demand results from a plurality of loads which at least in part can only be switched ON or OFF under constraints existing either at all times or occurring at least at the instant of control. However, by ON and OFF, it is understood that the loads, if electrical, need not be switched by electrical connecting or disconnecting. A power consumption can be increased or decreased by mechanical connection or disconnection of the load as well, such as by means of a clutch or valve actuation.

When several loads are available for being switched ON or OFF, to apply the strategies of the prior art just discussed, there is an ambiguity as to response that can be made for proper control, for example, at times a

load switched off by the demand controller may already be off. The particular load to be switched on by the demand controller might have been previously put out of service. It is also possible that control of the demand be prevented by an overriding and external control equipment associated with the load, as is usual with air conditioners, chillers, or air compressors, for instance. Other types of constraints can be found in the particular industrial plant of a customer to a power company, and are within the scope of application of the present invention.

The invention provides for a judicious selection of the loads in order to respect these constraints by eliminating the priorities set among the loads which are found to be in violation of the existing or anticipated constraints. Thus the priorities are not only determined by a predetermined classification of the loads, they are also changed in the course of the control process in order to take into account the history of the loads as it appears from a reappraisal of the availability to be switched ON, or OFF, during the demand limit control process.

The selection of a load not only depends upon the overall status of the different loads, but also upon the behavior of any particular load in the user's plant. The control system according to the present invention, therefore provides for a dynamic allocation of priorities for the selection of the loads to be controlled at any particular time.

The invention also provides for relative control, rather than an absolute control of the loads, any selected and controlled load change being effected independently from the base load and from non-controlled loads.

The control system also takes into account the established constraints. For instance, besides interruptible loads which can be selected to be shed or to be added, there may be in the plant loads having a non-controllable status, which otherwise could defeat the control system. However, the control system according to the present invention limits its own capability of switching loads in order to accept the non-controllable loads as a favorable factor of correction in the demand limit control process. In particular, the control system according to the invention makes use of a deadband to this effect.

The invention moreover calls for the determination of the constraints either off-line or on-line in order to be able to ascertain with improved accuracy the anticipated effect of control and prepare for the right decision in selecting the loads to be controlled at a given instant or for an emergency action by the present control operation. To this effect a special technique of simulation is provided on the basis of actual load behavior in the user's plant, and such technique of simulation is used either as an off-line information providing system to be used preparatory to running of the control system according to the invention, or as an on-line coordinated helper system for constantly revising predictions and updating data during control of the loads in real time.

Finally the invention provides for a control system in which the technique of shedding loads or adding loads to limit the total power demand as desired at the end of any given demand period is modified in order to maximize the needs for particular loads of the user by minimizing the effect of control of the plant's constraints. To this effect, control is not necessarily ex-



erted during a first portion of the demand period, on the assumption that sufficient possibilities of meeting the objectives are still left and are available, as a result of an improved control and improved selection, the the later part of the demand period. Moreover, when control is performed, during a second and major portion of the demand period, the technique involves the use of

a deadband, namely the use vector limits within which no switching (on or off) of load is effected. In order to allow switching of larger loads when they are selected under the assigned priorities, the control system pro-

$$\text{Target} = \frac{1}{60} \left[ \int_0^t P_t dt + P_t (t_{\max} - t) \right] \quad (3)$$

vides for a variable deadband. In addition, a temporary target below the objective is imposed for control until a certain time limit relatively close to the end of the demand period and when such limit has been reached the bias so established is progressively reduced to zero until the end of the demand period, at which time the demand limit is substantially achieved.

#### General Description Of The Limitation Of Power Demand By Control Of Interruptible Loads

Forecasting of the trend toward a total demand at the end of a given billing period is based on the following considerations:

A common form of presenting graphically the variations in power (KW) versus time is shown on FIG. 1 for a demand period of 15 minutes. This diagram is based upon pulses from the demand meter (which actually records KWH versus time), which represent time interval ( $\Delta t$ ) for equal increments of energy. FIG. 5 is a similar diagram showing the slope for one point M on the trajectory. The slope is derived from the following relation:

$$\text{Slope} = \text{power} = (\text{KWH})/60 \quad (1)$$

If nothing would change among the loads, the trajectory from point M would follow MW, until a point W where it intercepts the 15 minutes ordinate, thus below the demand limit C.

Referring again to FIG. 1, the energy curve is shown with the KWH plotted against time during a given demand period. The slope of the curves plotted on this diagram represent power in KW. In this case the base load (non-interruptible) has a slope  $\alpha$ . The sum of the base and the switchable loads has a slope  $\beta$ . In order that a control opportunity exist, the slope must at some time be greater than the slope of the mean AC. The possibility of control should first be examined under the assumption of a single load to be switched ON or OFF. The boundaries of acceptable trajectories to meet the requirements with a single load are given by lines ABC and ADC, and there is an infinite number of possible intermediary trajectories, such as *a, b, c, d*, within this envelope. Of course, interception of the 15 minute ordinate between C and E would respect the Demand Limit requirement but would provide a poor load factor. In the absence of any other consideration all of the trajectories have equal economic merit so far as the mere purchase of electrical energy is concerned. The

minimum requirement is that  $\alpha < \text{KW} < \beta$ , since the power in KW is for a given point M on the trajectory, the slope from that point.

A trajectory which would give a uniform reduction in power from the maximum ( $S+B$ ) to the minimum  $B$  would have a power  $P_t$  versus time relationship such that:

$$P_t = (S+B) - \frac{S}{t_{\max}} \cdot t \quad \text{with } B < P_t < (B+S) \quad (2)$$

wherein  $t_{\max}$  is 15 minutes,  $S$  the maximum power of all switchable loads ON and  $B$  the power of the base load. It can be shown that when a point M follows one of the trajectories of FIG. 1, in general:

Other continuous relationships between  $P_t$  and  $t$  are possible.

However, the power factor is a further requirement as can be seen from FIGS. 2A, 2B, 3A, 3B, 4A and 4B. For instance, an industrial load system may have a base load  $B$  comprised of a number of small loads such as lighting, small meters, etc., and a total switchable load  $S$  consisting of a number of smaller loads. FIGS. 2 to 4 represent three different load distributions which could be obtained under the same maximum demand but with three different load factors. Three different trajectories can be found on FIG. 1 which would correspond to these three different distributions of power. FIG. 2A shows a power  $P_1$  maintained up to time  $t_1$  and a lower power  $P_2$  maintained from time  $t_1$  to the end of the demand period. FIG. 3A shows a power  $P_2$  maintained from initial time 0 to an instant  $t_1$  and a higher power  $P_1$  consumed between time  $t_1$ , and a later time  $t_2$ , the power  $P_2$  being again supplied from time  $t_2$  during the remaining portion of the demand period. FIG. 4A is similar to FIG. 2A but with an inverse distribution of the powers  $P_1$  and  $P_2$  before and after time  $t_1$ . The trajectory to a common level of HWH at C is ABC for FIG. 2A, as shown by FIG. 2B, ABDC for FIG. 3A is shown in FIG. 3B and ABC for FIG. 4A as shown on FIG. 4B. Since the power consumed is constant during each of the time intervals, the integrated power follows a demand curve which is linear, the slope being  $P_1$ , or  $P_2$ , depending upon the level of power maintained during the particular time interval.

FIG. 5 illustrates the principle of calculation of the error for any point M along the trajectory during a demand period of 15 minutes. A clock installed by the power supply company determines the initial time of each demand period, or the final time of a preceding demand period). The watt-hour meter provides a "KWH pulse" which represent the magnitude of the power which has been consumed during a certain instant  $\Delta t$  corresponding to a full rotation of the disc of the meter, thus representing a constant increment or unit of energy (KWH). Thus, the  $\Delta t$  interval appearing along the time axis is essentially variable. This time interval is detected as a representation of the slope at point M and it represents the power  $P_t$  in KW hour/hour. If the load of the plant is maintained in the same condition until the end of the 15 minute period, the energy curve will follow the tangent MW. However, the Demand Limit should be at C therefore, there is an error CW by default. Which in terms of power is



$$\Delta P = [(60) \times CN / 15 - t] - P_i$$

as is evident from the geometry of triangles MNC and MWC. Having determined Slope =  $\Delta P / 60$  by triangulation, and the sign of the error, depending upon whether the intersection point *W* is above or below the target *C*, control is effected by selectively adding or shedding suitable loads in the plant. In order to more closely follow the target, a deadband is provided on either side of the trajectory by defining two angles  $\phi$  and  $\theta$  which should not be exceeded. The headband will contain excessive control but will leave free control of the loads as long as the projected tangent remains within two limits MU and MV (FIG. 5) so defined. In accordance with the present invention such deadband is made variable as will be explained later. The upper limit MU will represent the "decrease vector" and the lower limit MV of the deadband will represent the "increase vector" for control.

Since in the early part of the demand period the possibility of control is greater than in the later part, a differential treatment of the load control during the period is beneficial. Referring to FIG. 6 from time 0 to time *t<sub>i</sub>* no control is effected. This allows for a maximum utilization of the loads in the plant at an early time in the period when all possibilities of control to meet the target *T* are available. After this first field, the control system from time *t<sub>i</sub>* to time *t<sub>end</sub>* provides control in a second field in accordance with the general principles explained hereabove with reference to FIG. 5. Thus, at position *M* on the trajectory followed from time zero, the slope of the tangent indicates at *W* that the loads as they stand would bring total power consumption under the target *T* by as much as *TW*. Improved control is obtained when the distance from the point to the target has a reduced slope. It has been suggested therefore to create a bias relative to the target either by having an offset at the beginning of the trajectory, or by lowering the target such as at *C* on FIG. 6. This is the type of control achieved in the second field, e.g., between time *t<sub>i</sub>* and time *t<sub>end</sub>*. Therefore the control system is operative to calculate and correct an error from *W* to *C* rather than from *W* to *T*. When attempting to control the demand to correct the slope of *MW* by switching ON loads, there is a possibility that *MW* raises itself as far as to exceed the "increase load vector *MV*." The load will not be switched ON in such case. However, under the pressure imposed on the system by the non-controllable loads which may be switched ON nevertheless, it is possible that the vector *MW* still reaches a slope above the temporary target *C* or even the desired demand limit *T*. In such case the control system is operative to switch OFF loads against the "decrease load vector" MU.

Assuming that at time *t<sub>end</sub>* the trajectory reaches point *M<sub>2</sub>*, as shown on FIG. 6, there is still an error *RC*, although very small. At this instant the second field is terminated and a third field of control operation is established in the control system operation during which the bias *CT* is progressively reduced to zero at the end of the demand period of 15 minutes. Therefore, the trajectory will pass for instance by point *M<sub>3</sub>* as shown, heading toward the real target *T* at the end of the third period. This differential treatment of error anticipation and load control during the demand period affords a more judicial selection of the loads and a more effective control of the total demand.

Other strategies of control are possible. Instead of continuous control toward a target, a discontinuous strategy can be followed. For instance, as shown in FIG. 7 the trajectory is first only restricted to the area bounded by OX, OY and ZZ which have been selected irrespective of the demand limit *T*. *T* becomes a permanent target once one of the boundaries ZZ and YY, has been reached.

FIG. 8 illustrates another strategy for adding or shedding a load. It is seen here that control is effected so that the sum of the on-times is equal to the time necessary to reach *B* from *A*.

$$t \geq t_1 + t_2 + t_3 \quad (5)$$

$$X \leq X_1 + X_2 + X \quad (6)$$

Should the accumulated KWH intercept line BC, (as at *P*) only the base load must be left switched on if the limit *C* is not to be exceeded. In addition to satisfying relations (5) and (6), it may be stipulated at the plant that the minimum ON time should be more than "*t<sub>min</sub>*" and that the ON/OFF ratio for a given cycle should be less than "*t<sub>max</sub>*" before the load can be switched ON again. Thus, once the load has been switched ON, it will remain ON until

$$t_i > t_{min}$$

and once OFF, it will not be able to be switched OFF again unless

$$t_i / X_i < t_{max}$$

Such a strategy can be implemented by setting up constraints YY and ZZ on either side of the mean curve AC, the distance from the mean curve being chosen in order to make the ON times and OFF times, and ON/OFF ratios compatible with the slopes of the two load conditions. Particular care has to be exercised so that proper action is taken whenever the KWH curve intercepts BC. This is achieved by calculating the slope  $\lambda$  of MC the line joining the point *M* on the trajectory to *C*, and switching OFF a load other than base load once  $\alpha = \lambda$ .

FIG. 9 shows an alternate strategy with pivoted limits. This strategy is taught in the U.S. Pat. No. 3,621,271 issued on Nov. 16, 1971 to Carl J. Snyder. While  $t_i / X_i < t_{max}$  is being observed,  $t_i > t_{min}$  would not be, since the system would tend towards more frequent switching at the end of the demand period in the case of a single switched load.

#### THE DEMAND CONTROL SYSTEM OPERATION

Referring to FIG. 11 there is shown an overview of the control system 1 according to the present invention applied to the control of the loads of a plant 2 supplied with electrical power on the power supply lines 3 of a power supply company 4.

The loads are classified in the four categories of I base load, II inhibited loads, III sheddable loads, and IV critical loads.

The base load represents equipment which is constantly present or at least, if the equipment is switched on and off, such occurrence has in its narrowness a sufficient pattern to equate to a fairly steady load. Therefore, the base load is by definition a non-sheddable



load. If control of the base load is not possible, the base load affects by its presence the control of the sheddable loads, since it accounts for a portion of the KWH consumed at any given time. Typical of the base load are the lighting and heating loads, and also certain groups of motors and equipment.

An inhibited load is defined as a load which will be permitted to be switched ON during the first minute of any demand period but will be switched OFF after a certain duration has elapsed and will be inhibited from being switched on again until after the next demand period has begun. For these loads the control system needs to know the duration of ON time from the beginning of a given demand period, and at a given instant whether the load is available for use or not. If the load is available, it will be qualified as permissive.

The sheddable loads are by definition the loads which may become available on a priority basis to be switched ON, or OFF, by the control system. This is a general quality of the loads which are not a base load provided they have not a "non-controllable" status. Thus, the constraints of the present industrial plant may limit such "shedability."

The present invention provides for selection and control of the loads within such constraints in order to maximize the utilization of the power supplied and minimize the cost of the energy. Therefore, a sheddable load essentially is, within the concept of the invention, a load which can be switched ON or OFF during a certain demand period without affecting the operation of the plant.

An important limitation in the control of an interruptible load is the ON time and the OFF time. It is not advisable to start-up a load too often, for instance, for a motor this may have a damaging effect on the windings. Also electrical surges caused by starting, are costly. It might also be economically desirable not to leave an equipment off during an excessive time interval. When an excessive off time exists, such equipment must be switched on and another alternative has to be sought if the shedding of some load is the control action required at that time. The ratio between ON time and OFF time may also introduce a limitation, requiring to keep ON a load.

One important consideration in the control system operation according to the invention is that while sheddable loads may be available for switching, it is possible to spread the ON times and OFF times within a given demand period and between demand periods in order to spread wear.

The last category of load is the critical load. These are loads which are ON and OFF under external requirements at the plant. For instance the air conditioners and the compressors follow local conditions. Local control might override action by the control system. Switching ON or OFF of such loads although required by the demand control system, could be ineffective since the running time for such a load is not known in advance. For this type of load switching ON/OFF is constantly monitored.

Referring again to FIG. 11 the loads are controlled by a contact output unit 5, which is part of a process control computer system 6. The contact output unit 5 does operate a plurality of load contact outputs 7, each of which closes the energizing circuit of a corresponding relay 8 to actuate the switching element 9 of a load. Such switching element may be the starter of an electri-

cal motor, the plunger of the valve of a compressor, etc.

When a load is in the switched ON condition, a corresponding status contact interrupt 10 is closed as shown on FIG. 11, with the contacts being arranged so as to correspond to the loads. There is shown in FIG. 11 two such groups of contacts with one group being associated with a diode 11 and one scan contact output C01, and the other group being associated with a diode 12 and another scan contact output C02. Respective diodes 13 are connected in circuit with corresponding status contact interrupts 10 to establish a circuit from a 48V source 20 provided by the computer system, to ground with the associated diode, 11 or 12. As shown on FIG. 11, concurrent closing of one scan contact output such as C02 and one particular status contact interrupt 10, such as shown on the Figure, permits identification by the interrupt unit 14 of the status of the particular contact as being one of Group 2 (C02 on the Figure).

In order to control the power demand by shedding or adding loads, the control system 1 is responsive to the power consumption continuously recorded by the meter 15 of the power supply company. The process control computer receives over a line 16 the KWH pulse which as a  $\Delta t$  characterizes the consumption at any particular instant within the demand period. The power supply company also provides a clock 17 which determines the beginning and the end of each demand period. In the instant case it is assumed that each such demand period lasts 15 minutes. For each turn of the disc of the meter 15 there is a pulse generated which will be hereinafter called "KWH pulse." The succession of these pulses represent on a time scale the power consumed for one turn of the disc. The process control computer system 6 through the interrupt unit 14 assesses the status of the status contact interrupts 10, and more generally monitors all the input data fed into the computer system regarding the individual loads in the plant with their constraints, effectuates calculations, makes decisions, which are converted, after each of the above-mentioned KWH pulses, into whatever load control action is necessary through the controlled operated of the relays 8.

Included as part of the control system 1, is the process control computer system 6. This computer system can be a digital computer system, such as a Prodac 2000 (P2000) sold by Westinghouse Electric Corporation. A descriptive book entitled "Prodac 2000 Computers Systems Reference Manual" has been published in 1970 by Westinghouse Electric Corporation and made available for the purpose of describing in greater detail this computer system and its operation. The input systems, associated with the computer processor are well known and include a conventional contact closure input system to effectuate scanning of the contacts or other signals representing the status of the equipment. Also operator controlled and other information input devices and systems are provided such as the teletypewriter 19 shown in FIG. 11. The contact closure output system is also conventional and part of the Prodac 2000 general purpose digital computer system sold.

Although FIG. 11 shows electrical loads which are sheddable or which can be picked up by the demand control system, it should be understood that switching of an electrical load is not the only control action within the scope of the present invention. If it is found



not necessary or desirable to limit the demand by switch the actual electrical load on or off in every case, the same result can be obtained by other alternatives. For instance, fan loads can be reduced to some 20% of normal by closing the inlet vanes or damper by means of a servomotor, rather than switching off the motor. This operation could be performed relatively frequently and for short periods (for example towards the end of a demand period as a fine trim), whereas there is a limited number of starts per hour allowed for larger motors. When the load involves eddy current couplings or pneumatic clutches, the mechanical loads can be disconnected from their motors. With air compressors having inlet valves, these may be held open by the pressure control equipment when the pressure is high. The control of compressors to maintain demand below the desired level would operate in parallel with the pressure control system with the same goal. These alternatives avoid increasing the cost of maintenance of plant equipment.

The computer system used in the control system according to the invention includes both Hardware and Software. For instance the interrupt unit 14 is associated with an interrupt handler (50 in FIG. 12). Software is being used as a convenient means of quickly and efficiently performing operations as required in monitoring data, doing calculations, making decisions and translating treatment of information into control action within the short time intervals determined by the recurrent transmission of KWH pulses from the power supply company meter 15.

It is observed that the inputs consist of interrupts which are successively handled by the process interrupt handler (see FIG. 12). One interrupt will receive the 48V DC pulse generated by the external clock and is used to reset the demand meter owned by the power company. This same pulse will reset the associated registers in the computer when it is received. Another interrupt will receive a train of 48V DC pulses transmitted by the meter 15, each pulse representing KWH (or KVAH) consumed. Another interrupt could be reserved for a second KWH meter if needed. Three other interrupts (the scan contact interrupts 10 of FIG. 11) will receive a status which corresponds to the status of one load contact in the plant and belongs to one group of three associated with one scan contact output (C01, C02 on FIG. 11).

The normal operator interface with the system will be via a teletypewriter 19. This device will also provide a log of system performance together with any other messages that may be required. Via the typewriter keyboard the operator will also be able to change the values of various constants relating to the system as a whole or to individual items of equipment. The time and data and onpeak and off-peak demand levels can also be changed using the same keyboard.

Having considered the Hardware aspect of the control system according to the invention, consideration will now be given to the software components of the computer system referring in particular to the flowcharts of FIGS. 12, 13A, 13B, 13C, 14A and 14B. Referring to FIG. 12, the operation of the interrupt handler 50 of the computer system is described. This program will receive T (at step 51) an interrupt from the clock at the beginning of each demand period together with a KWH pulse (at step 60) from the KWH (or KVAH) meter 15 for each revolution of the disc.

In response to a clock pulse, the decision at step 51 is a yes, and the data are transferred to a buffer. These data include time (step 52) the demand limit desired at the end of the demand period (coded as DEMLIN) which is set in the total kilowatt register (KWTOT). At step 53, the program puts data to be printed out for the preceding demand period. The next step (55) is to clear all registers in which accumulated values are stored including time into period and KWH during the period (time, number of pulses N, KWHIN, and KWHTOT registers). Prorated values of time and KWH are stored in those registers when the KWH pulse does not coincide with the clock pulse. The chain returns to the process interrupt handler 50.

If the interrupt relates to a contact status, as seen at step 56, the interrupt is stored at step 51 at the proper location to provide a status image of the array of contact interrupts 10 (FIG. 11). The present contact output is reset and the next contact output is set in the status list (at step 58). At step 59 the contact output handler which corresponds to the contact output unit 5 (FIG. 11) is bid, and the chain returns to the process interrupt handler 50. If the interrupt is the KWH pulse from the meter, as seen at step 60, this data is stored as real time in a "KWH TIME" register. For each turn of the disc of the meter, e.g., for equal increments of energy, one KWH pulse is received. The count is effected at step 62 ( $N = N + 1$ ), and whenever required, there is a bid for control at step 63. This chain returns also to the process interrupt handler 50. Besides the preceding interrupts which directly determine operation of the control system, there may be other interrupts received, as seen at step 64. Such "unscheduled" interrupts cause at step 65 the printing of a warning message, and there is a return to the task scheduler of the computer system.

FIGS. 13A, 13B, 13C show a flowchart of the main control program, which is provided to explain the operation of the control system according to the present invention.

When control starts, "DELTEE," e.g., the  $\Delta t$  between two successive KWH pulses, is determined by difference. This is step 160. Then a rotating file is updated by adding the last of three successive vectors corresponding to three successive times  $t_1, t_2, t_3$  being for the latest  $\Delta t$  at step 161. At step 162, the present power consumption (IPWR) is computed from the rotating file, and from the present status IPWR is translated at step 163 into the "Past KWH TIME" register. At step 162 the present power consumed is calculated by averaging for three successive points on the trajectory corresponding to times  $t_1$ ,

$$P_t = [a(a/k/t_1) + (1-a)(k/t_2) + (1-a)(k/t_3)] \quad (7)$$

or

$$P_t = k [a/a/t_1 + 1 - a/t_2 + 1 - a/t_3] \quad (8)$$

where  $0.1 < a < 0.4$  and  $t_1$  is in hours and  $k$  — KWH/pulse.

It is recalled here that while each KWH pulse is received for the same increment of energy (one turn of the disc of the KWH meter), the "DELTEE" represents the power consumed since the time between each



pulse depends upon the speed of the disc rotation. It is necessary to compute the total time into the demand period and the total energy consumed within the period. The first is obtained by integrating the DELTEES corresponding to all KWH pulses received during the period. The energy consumed is equal to the number of pulses multiplied by the meter factor (KWH/pulse). The decision at step 164 (since  $N$  is normally greater than 1) is to go to step 167, where the demand period time is found to be the sum of the  $\Delta t$ 's in the period.

The DELTEE corresponding to the first pulse after the clock pulse ( $N=1$ ) belongs in part to the last demand period and only in part to the new demand period. In such case, the decision at 164 is to go through steps 165 and 166 which provide a prorated value of the KWHIN in proportion to the fraction of DELTEE pertaining to the new demand period. Accordingly, step 165 provides the time difference between KWH Time and clock time, and at step 166 the prorated value KWHIN is computed.

Looking to A on FIG. 13A, the next step is to compute KWTOT, e.g., the energy consumed during the present demand period until the particular iteration, converted to equivalent power at the end of the period. KWTOT is equal to  $N$  (number of pulses) \* KWH/pulse \* Constant plus the fraction prorated at step 66, if there is one, e.g., KWHIN. Since computation is done with a floating point for increased accuracy, conversion to integer is effected as indicated by  $ITKWH = IFIX(KWTOT)$  (168).

Then, at step 169 the system looks at the status of the ON times and OFF times of the loads, while adding the  $\Delta t$  (DELTEE) and it is determined at step 70 whether any load exceeds the OFF time assigned to it. In such case, a decision is made at 70 to set the contact output to switch the particular load ON (step 71) thereby not to violate the constraint. Since the load has been switched ON, the ON time of this particular load is set to zero (step 72). Also, the energy estimated to be consumed in the overall industrial load system (IPWR) must be updated in order to take into account the load so picked up. However, if the load exceeding its OFF time belongs to a class, or priority including several other loads in order to reduce wear, all the loads of the same class, or priority, are rotated. Rotation is effected at step 74.

The next decision is at 75 depending upon whether the system is under the first field previously mentioned, e.g., a first portion of the demand period for which no control is effected (NOC). When the first field terminates, the second field begins which is a field of control, namely at B after step 75. If in response to the decision 75 the control system operates in the no control condition (NOC), the system goes to 109. As a result, the contact output handler will ascertain the status of the contacts. Considering now the chain starting at B for control operation, the second and third fields of controls (from  $t_1$  to  $t_1$  and from  $t_1$  to 15 minutes) should be explained again by reference to FIG. 6. C represents the BIAS in the second field of control, T the original target corresponding to the desired Demand Limit (DEMLIN). The target (ITGTI) in the second field is represented by C, e.g., DEMLIN-BIAS. The control system (FIG. 13B) is set accordingly at step 76. A decision is made at step 77 to choose between the second and third field of control depending upon whether the time in demand period has reached  $t_e$  (NFIN) or not.

If we are still in the second field, the flowchart goes from 77 directly to step 79. If the third field is required, at step 78, the BIAS is reduced at each iteration until the end of the period. Accordingly, a fraction is used to reduce the BIAS by a ratio between the time left in the period and the duration of the third field. This amounts to a displacement of the target for each point on the trajectory. At steps 79 and 80 the demand error is calculated. ITGTI represents the ordinate of the target (C in the second field, I in the third field, T at the end of the demand period). The ordinate of N (see FIG. 6) is  $ITKWH$  obtained at step 168. The ordinate of W is  $ITKWH + ITEM$  (e.g., WN). Therefore, the error due to W being too low, or too high, relative to the target is  $Slope = IGTI - (ITKWH + ITEM)$ . First, at step 79 ITEM is calculated, using data obtained at step 162 (IPWR = present power consumption), and computing the second term in equation (3), e.g.,  $P_i(T_{max} - t)$ . Knowing  $ITKWH$  and ITEM, the demand error is calculated at step 80. Then the sign of the error Y or N at 81 will tell whether the projected point W lies above or below the target. If it is above, the error is negative and loads have to be switched OFF. The flow chart goes to D. If point W lies below the error is positive and loads must be switched ON. The flow chart goes to C.

First, the situation when the error is positive will be considered, by taking the flow chart from C on, in order to find (1) whether there is a load to be switched ON, (2) whether a selected load can be switched ON by step 86.

The computer system then first looks for a load. Step 82 initializes a search for the least sheddable load.

In the table of priorities, the loads are classified from the least sheddable to the most sheddable (which can be understood as from the first to be switched ON to the last to be switched ON). In other words, the search goes from one end of the table when the search is to switch ON a load, and from the opposite end if the search is to switch OFF a load. (The last situation would be at D on the flow chart).

As a general consideration at this point (valid also for OFF switching at D) in a table can be stored or reserved in memory the following characteristics associated with each item of equipment to be of the switchable load type:

- Equipment Identity No.
- Power Consumed When Starting
- Starting Period
- Power Consumed When Running
- Group Priority
- Subgroup Priority
- Maximum Allowable Off Time
- Minimum On/Off Time Ratio
- Minimum Time Between Starts
- Availability For Use By The Demand Control System
- Address of Associated Contact Output
- Amount of Time 'Off' since Being Switched Off - Updated Each sec., or after
- Amount of Time On Since Being Switched On each KWH Pulse.

The group priority is assigned by the user, the most sheddable loads being low numbers. Priority, or group, numbers increase with the importance of the load to the overall plant operation. The programs associated with this table will be called immediately after the switching decision subroutine, or once per second to



effect: a search through the table to determine the identity of the next load to be switched and the power difference this will make. In the case of large starting currents, a check can be made to see whether starting this motor will cause the maximum demand to be exceeded. If so, the next motor in the sequence will be selected. Similarly, it can be presumed that if the sum of OFF plus ON time is less than the minimum between starts, another unit will be selected for switching on. In the case of large loads not directly controlled by the computer but for which the computer provides a permissive contact, a check will be made to determine whether the maximum time into the period has not been exceeded and close or open this contact accordingly (see Step 70 on FIG. 13A). If loads have imposed a maximum off time and a minimum on/off time ratio, the computer system would include a program to (1) switch that load ON regardless, whenever the off time has exceeded the maximum allowable off time; (2) prevent the load from being switched OFF unless the ON/OFF time ratio is greater than the minimum allowed.

Returning to C on the flow chart (FIG. 13B), step 82 provides for indexation of the priority order ( $N_1$ ) and of the subpriority order ( $N_2$ ) for a load to be switched ON (INDUP). At step 83 the search is established accordingly. If the search has not provided at least sheddable load, the decision at step 84 is to go to K, e.g., a no control chain leading to a bid for the CO handler at 109. At step 108, the projection W on the final ordinate of the tangent from the point M on the trajectory (see FIG. 6) is determined as ITGT by the difference between the target and the error. Such information can be conveniently logged for the following reason. ITGT = Ordinate of target (C, if in the second field of control) - error (CW). This is the way ITGT is determined at step 108. But ITGT is also equal to:  $WN + \text{ordinate of } N$  (See FIG. 6). Since  $WN = \text{ITEM}$  and ordinate of  $N = \text{ITKWH}$ , both known by steps 168 and 79, then ITGT is known from previous computations. However, when late in the demand period ITEM becomes very small, therefore a log of ITGT provides a value which tends to be ITKWH equal to the final demand at the end of the demand period.

At step 109 the CO handler of the computer is called upon to check the contact outputs and there is a return to the task scheduler of the computer system.

If however, a load to be switched ON has been found (NO at 85) (INDUP), the deadband is put into effect at step 85. If the deadband (LDINC) includes vector MW, then no control is effected (YES at 85) and the flow chart goes again to K (again a log of ITGT and a bid for the CO handler). However, if there is a NO at 85 then MW is outside the deadband (LDINC), control is possible and action is bid at step 86. At step 87 the new present power consumed IPWR is calculated by including the added power LDINC and due rotation is effected within a group of loads at step 89 if the load is one of a group.

Having called for the load to be ON, the ON time (ONTIM) for the particular load (or for the rotated group of loads if steps 88, 89 are followed) is initialized at 90 (E), while at step 91 a decision is made to print the "Switch-On" message (92) if the control operation requires it.

Considering now the decision at 85 to switch a selected load ON (if N) or not to switch (if Y), the error CW (FIG. 6 for second field of control) is compared

with the increase of power LDINC expected. Control will occur only if LDINC is less than the error. If the selected load can be switched (85) the control action is determined at step 86 and the increased amount of power is accounted for in the new IPWR (step 87).

When the demand error (81) is negative a load must be switched OFF because ITGT is above the target. In such case the flow chart goes to D (FIG. 13C). Steps 93 and 94 correspond to the steps 82, 83 encountered at C for the positive demand error. The search here is for the most sheddable load, thus from the opposite end of the table of priorities and subpriorities ( $N_4, N_5$ ) as opposed to steps 82, 83 for ON switching. When no load to be switched OFF is found, the program indicates 100 as a flag. If this is the case, the flow chart goes to K, and no control is exercised as previously indicated with respect to steps 108, 109. If there is such a load (INDDN), the decision (95, N) is to test the relation of LDINC (the correlative decrease of power if the particular load were effectively switched OFF) to ITEMP which determines the deadband. Two situations happen at this stage depending upon whether the load exceeds 180 KW (Y) or not (N) and the decision is made at 97. If it is a Y, ITEMP is made half of what it is at step 96. In other words 96 can be read as making the deadband ITEMP = LDINC and 99 as making the deadband ITEMP =  $\frac{1}{2}$  LDINC. Assuming 97 leads to N, then ITEMP is made equal to LDINC. This means that at step 98 the slope (CW if in the second field) which is negative is in fact subtracted from LDINC. This difference is a residual error sign of which (in the second field 100 goes to 102) is checked for decision at 102 to control (103) or not (108) switching of the particular load. Again, if the vector or W is within the deadband (between MV and MC) there will be no control. If MW is outside the deadband, then the load will be switched OFF. If control is in the third field (101) then the system merely looks to the error (negative here) to switch (Y) or not the loads OFF.

Once a load is shed (at step 103) the present power IPWR is updated (104). At step 105, the OFFTIM (computed off-time of the load) is updated at each iteration. A decision is made thereafter to log the information (step 106) and to print a switch-OFF message (step 107). After each control operation (shedding or pick-up), the energy estimated to be consumed is estimated (at step 79) and the demand error is again calculated in order to establish whether a new load should be switched ON (at C) or OFF (at D).

Once counting of time and power consumption has started for a given demand period, a first field is established during which the load system is left to its own constraints without control (75, 108, NOC). Since there is no control, the slope varies only with the loads. There is no need for a calculation of the slope at any point of the trajectory. Although there is no control during the first field, the status of certain of the interruptible loads may have changed during that time. For instance, in the particular example of the embodiment described, the OFF time of certain loads may have become excessive, and according to step 70, the contact output of such load would have been set (71). Therefore, the control system calls for the CO handler which is the software counterpart of the contact unit 5 (FIG. 2). Thus a bid is made (109) for the CO handler in order to implement the status of the contact outputs established by the previous iteration. The system then returns to the



task handler. The first field ends at time  $t_i$  (FIG. 6) and a second field is established thereafter (N,75).

It should be observed here that there is a difference between (1) the switching ON of a load which has been OFF for an excessive OFF time, such as operated by the system at 70 and 71 (FIG. 13A) and (2) the switching ON of a selected load such as at 86 on FIG. 13B. When there has been an excessive OFF time, the system indeed provides for the switching ON of the load. However, such switching is not really a "controlled" switching in the sense that (a) there is no selection made of the load, no prediction made of the KWH and no decision is done to switch under predetermined conditions which suppose alternative situations; and (b) the additional load created at 70 and 71 might go against the overall objective to limit the demand. In contrast, when switching ON a load at 86, a selection (82,83) is made and the decision to switch is based on an anticipation (80) of an error. Therefore, when referring to switching such as at 70, e.g., under the constraints assigned to the load, the load should be considered as in a "non-controllable" status.

An important application of the control system according to the present invention can be found when the industrial plant includes among other interruptible and switchable loads, one load for instance, which could not be switched without causing overshooting of the target T, such as at CR at point C of the trajectory I on FIG. 10. By reducing the demand limit to T during a portion of the demand period, for instance from time 0 to time  $t_b$ , the control system will operate more rigidly against the constraints (DEMLIN at step 76 on FIG. 13B) and the trajectory followed will be I', as shown on FIG. 10. The demand control system described hereabove, is capable of determining at which time  $t_b$  the projected line representing the load which could not be switched will intersect the last ordinate at T, the desired demand limit. To do this it is sufficient for instance, that the computer system at 76 (FIG. 13B) identifies the target (T' first, then T) and determine an error on selection (82) which is zero.

A last remark can be made regarding the overall operations of the control system according to the inven-

tion. Since loads in a non-controllable status spontaneously are switched ON when their OFF time has been exceeded, when a flag 100 has appeared to indicate that no load is available to be shed, the system will by itself become effective for control, since more loads will become available at the next iterations.

Associated with the main control program just described, is a simulation program which can also be used separately as a source of information to study the condition of control according to the invention for a given set of loads and constraints in the particular plant. The simulation program runs on a P - 2000 computer. The simulation program is based upon equal time intervals. It simulates for instance the behavior of air compressors and similar controlled devices, and the instantaneous power consumption as a function not only of the switchable loads, but also with a base load having noise superimposed.

The following notations are used by the program:

RAND - random no. generator for base load noise

CONTROL - the principal demand control algorithm

ROTATE - designed to rotate group priorities every time any one unit in a multiple-unit group is started

PRINT - prints a message every time CONTROL switches a unit on or off in its effort to maintain the demand limit

SCALE - sets up Y-scale values when plotting is requested (KW)

LINYY - sets up Y-scale marks

PLOTT - plots up to nine selected loads (KW)

INDX - alpha form of time index (secs) to be printed on every tenth plotted line.

The main data base used with the control algorithm CONTROL is an integer matrix called DAT(N,11) where N is the total number of controlled loads in the system.

Loads are classified as inhibited. The number of inhibited loads being INHL; others are sheddable, the number of which is SHLD. Compressors and similar critical loads are a subset of SHLD, arranged as a continuous group starting from the first sheddable load. The number of critical loads is CRLD. The group of DAT (N,11) are therefore assigned as follows:

TABLE I

(limited to seven of the 11 columns provided on the card because several of the data are computed by/the program).

Title	1	2	3	4	5	6	7	8
110	20	50	4700					
120	1	3	0					
130(Base Load)	2000	2	17	2				
140	3	1	2	19				
150	0	1	0					
160	6	2	2	2	8	1	2	
Load Ref.								
170	932	149	450					
180	2238	0	450					
190	112	100	160	3	1			
200	112	100	160	3	2			
210	410	200	80	6	1			
220	410	200	80	6	2			
230	186	180	80	5	0			
240	75	180	100	4	1			
250	75	180	100	4	2			
260	75	180	100	4	3			
270	75	180	100	4	4			
280	75	180	1000	4	5			
290	75	180	100	4	6			
300	75	180	100	4	7			
310	75	180	100	4	8			
320	37	300	100	1	1			
330	37	300	100	1	2			
340	336	300	160	2	1			
350	105	300	160	2	2			

Inhibited Loads

Critical Loads

Sheddable Loads



### Inhibited Loads

An inhibited load is defined as one which will be permitted to be switched on during the first minutes of any demand period but will be switched off after the duration DURN has elapsed and will be inhibited from being switched on again until the next demand period has begun. With inhibited loads the columns are in principle assigned as follows:

1. LDON - power drawn when load is on (KW)
2. LDOFF - power drawn when load is off (KW)
3. DURN - Duration of on-time for this load from beginning of period (secs.)
- 4-5. Not used
6. PERM - Permissive flag indicating whether this load is available for use or not (1 or 0). (see steps 203 and 204 on FIG. 14). Therefore this column is in the present case not used in Table I.
- 7-8. Not Used
9. C $\phi$  - Status of contact output (1 or 0)
10. MOSTAT - The logical AND of CO and PERM (1 or 0)
11. CWRD - Reserved for the future CO control word assigned to this unit (Hexadecimal notation).

However, the program here also computes the data of column 9, 10 and 11, therefore these columns are not used in Table I.

There must be at least one inhibited load in the system even if this is a dummy with zero power on and off.

### Sheddable Loads

Sheddable loads are defined as loads which will be switched "on" if they have been off longer than an assigned off time (OFFTIM); but having been switched on, will remain on until a given ON/OFF ratio (ON-RATO) has been exceeded. If the off time is critical, off time will be computed, not inferentially from c $\phi$  status, but from the actual motor or equipment status (MOSTAT) as scanned directly by the computer.

With sheddable loads of both types the columns are unprinciple assigned as follows:

1. LDINC - increase in power drawn when C $\phi$  is closed (KW).
2. OFFMAX - maximum off time (secs.)
3. ONRATO - minimum on/off ratio expressed as a percentage (e.g., 100 = 100%, 20 = 20%, etc.)
4. PRIOR - main group priority assigned to this unit  
1 = most sheddable - 99 = least sheddable
5. SUBPRI - subgroup priority

6. PERM - permissive indicating whether this load is available or not (0 or 1)
7. OFFTIM - Computed off time for this unit, updated at each iteration if the unit is off (secs)
8. ONTIM - computed on time to this unit, updated at each iteration if the unit is on (secs)
9. C $\phi$  - status of control algorithm output (1 or 0)
10. MOSTAT - status of equipment (if a critical load) or logical .AND. of C $\phi$  and PERM (1 or 0)
11. CWRD - reserved for the future control word for the C $\phi$  assigned to this unit.

Here too certain clauses of Table I are not used in the card because the program makes the computation. A typical set of input data is shown on Table I the data being read-in in 1016 format. The description of the card reference numbers on the attached coding sheet is as follows:

110 - ITIME - estimated between KWH meter pulses (secs)

BIAS - initial low bias to be applied to the desired limit (KW)

DEMLIN - demand limit desired at end of period (KW)

120 - LOG - type of output where:

0 = appropriate demand period summary only is desired

1 = print out of equipment status, power consumption and predicted target at such iteration in addition to summary

3 = plot of selected loads as well as summary

NPERD - no. of consecutive demand periods to be studied

LOGI = 0 = exercise demand control

1 = establish minimum demand which would be obtained if all constraints are rigidly exercised

2 = establish maximum demand if no constraints or controls are exercised.

The program is written so that if LOG = 3, the LOGI is forced to be zero regardless of what is on its data input card.

130 BASE - base load (KW)  
INHL - number of inhibited loads  
SHLD - number of critical loads  
CRLD - number of critical loads

140 NN - number of loads for which PERM(I) is to be controlled by data on card immediately following (otherwise PERM(I) = 1)

IND(I) - index of loads from 1 to NN

150 TEMP(I) - status of PERM(I) for loads with index IND(I) (1 or 0)

160 MGRP - number of priority groups in the total system

MAX(I) - maximum number of units in each group 1 through MGRP

170 LDON(I) - Power drawn when C $\phi$  closed (KW)

180 LDOFF(I) - power drawn when C $\phi$  opened (KW)

DRUN(I) - duration of on time in any period

190 LDINC(I)

through OFFMAX (I) data for each of the 17 sheddable loads

350 ONRATO(I)

PRIOR(I)

SUBPRI(I)

These two cards are for the two inhibited loads (secs.)

The simulation starts at step 200 by reading data from the data file. The data have been hereabove listed (see Table I). A logic table will be used hereinafter with the flow chart of FIG. 13 reading as follows:

TABLE II

Simulation Interval - ITIME secs.  
Demand Period = Demper mins.



No. of Periods = NPERD

Log = 0 = Summary of Period Only

Log = 1 = Print out of each iteration plus summary

Log = 3 = Plot of each iteration plus summary

Log = 0 = On control

Log = 1 = Compute demand limit with all constraints operating

Log = 1 = 2 = Not Under Control (NOC)

If, at step 201, Log. Eq. 3, (see Table II) the decision is to print the y-scale of a graph to be plot (step 202). The reset step, at 203 is to check  $PERM(I) = 1$ . Then at 204  $PERM(I)$  is modified according to data on the cards for the inhibited loads  $PERM(IND(I))$ . At step 205 the ON Time and OFF Time are stored and finally at 206 the contact outputs for all sheddable loads are set with the permissive flag for all permissive loads ( $CO(I) = PERM(I)$ ). The preceding steps are necessary in order to prepare for actual simulation. After this, for critical loads the conditions of operation are initialized. In the instant case, the load is a compressor and the pressure and pressure switches are initialized. For instance the margin of pressure for ON and OFF may be 90 psi to 100 psi. This step is seen at 207. The next step (208) is the calculation of the constants to be used in the simulation.

At step 209, the program determines the index after which Demand control should begin to be exercised. This is the end of the first field for which no control is effected (NOC) and the beginning of the second field. At step 209, the program also determines the index after which the third field of control should begin (NFIN). At step 210 is initialized the energy consumed during demand period converted to equivalent power at the end of the period. (TOTKWH), with the iteration index (NI) equal to one and the index of the present demand period (NPR) equal to one. Thereafter iteration for simulation begins (step 211).

At step 212 pressure from the status of Compressors are updated and at step 213 the same is done for the pressure switches. At step 214, a check is made whether the inhibited loads have exceeded the allowable ON Time in which case they are switched off. At step 215 the status of all the motors is updated, while for inhibited loads the motor status is modified (step 216).

On the preceding basis, the energy consumed during the present demand period up until the iteration, converted to equivalent power at the end of the period, (TOTKWH) is calculated (step 217) and the total energy consumed into the period is thereafter calculated at step 218.

If Log 1. GT1, (step 219) is a NO, then the system calls for control (220) which step appears on FIG. 13 between steps 168 and 169. If Log 1 equals 0 (step 221) which means that the system is on control, it is a YES, and the flow chart goes to the printing line

marked D, but after step 224, without plotting.

If the system is on control the flow chart goes to D which provides over steps 222 and 229 for a print out of the status, the power and the target for each iteration plus summary. At step 225 a determination is made whether the iteration index (NI) is equal to the total number of iterations at I Time (seconds) intervals for a demand period which is "DEMPER" minutes long. As a result, over steps 226, 230, or 227, 231, 232 either an order is given to print the end of period demand log under control (230), or to print the minimum demand at the end of the period (231), or to print the maximum demand at the end of the period (232). If we are during the demand period, the decision at step 225 is to print in accordance with step 229 already considered.

From the lines of steps 226 to 228, in the alternative, the flow chart goes to 233 to prepare for a new demand period (TOTKWH=0, NI=0 and NPR=NPR+1). Therefore, if the index of the present demand period (NPR) reaches the number of consecutive demand periods to be studied (NPERD) then the simulation goes to a stop (step 250). Otherwise there is another iteration (NI=NI+1) at step 235, which is also the step taken from the YES decision at 225.

#### GENERAL DESCRIPTION OF INSTRUCTION PROGRAM LISTING

In the Appendix there is included an instruction program listing that has been prepared to control the operation of an industrial load system in accordance with the here-disclosed control system and method. The instruction program listing is written in the machine language of the PRODAC P2000 digital computer system, which is sold by Westinghouse Electric Corporation for real time process control computer applications. Many of these digital computer systems have already been supplied to customers, including customer instruction books and descriptive documentation to explain to persons skilled in this art the operation of the hardware logic and the executive software of this digital computer system. This instruction program listing is included to provide an illustration of one suitable embodiment of the present control system and method that has actually been prepared. This instruction program listing at the present time has not been extensively debugged through the course of practical operation for the real time control of an industrial load system. It is well known by persons skilled in this art that most real time process control application programs contain some bugs or minor errors, and it is within the skill of such persons and takes varying periods of actual operation time to identify and correct the more critical of these bugs.

This instruction program listing included in the Appendix was prepared in relation to the flow-charts shown in FIGS. 12, 13A, 13B, 13C, 14A and 14B.

```

X E BINARY
U E
X D TEMP
U D
X D TEMP
U 4 D
• FTN4
LIST,S,B
C

```

```

      INTEGER SIMULATION PROGRAM FOR DEMAND CONTROL
      INTEGER DAT(30,11),BASE,INHL,SHLD,CRLD,IND(20),PS(20)

```



-Continued

```

INTEGER LDON(10),LDOFF(10),DURN(10),TEMP(10)
INTEGER LDINC(30),OFFMAX(30),ONRAT(30),PRIOR(30),SUBPRI(30)
INTEGER PERM(30),OFFTIM(30),ONTIM(30),CB(30),MSTAT(30),CWRD(30)
INTEGER BIAS,DEMLIM,KW(30),MAX(22)
INTEGER CR,LP
INTEGER LINB(71)
REAL PR(20)
COMMON /COMDAT/LDINC,OFFMAX,ONRAT,PRIOR,SUBPRI,PERM,OFFTIM,ONTIM,
1CB,MSTAT,CWRD
COMMON /CONINP/INHL,SHLD,CRLD,TIMEIT,BIAS,DEMLIM,LOG,NPERD,
1CONST,ICBN,NITR,ITIME,NOC,NFIN,NI,KWTOT,ITKWH,INDDN,INDUP,ITGT,
2LINE,LOG1
COMMON /DATBL/NN,IND,TEMP,BASE
COMMON /EQUIP/LP,CR
COMMON /ROTAT/IMIN,IMAX,MGRP,MAX
COMMON /PLBT/KW,KMIN,KMAX,IBASE,IDUFF,LINB
EQUIVALENCE (DAT(1,1),LDINC(1)),(DAT(1,1),LDON(1))
EQUIVALENCE (DAT(1,2),LDOFF(1)),(DAT(1,3),DURN(1))
LP=6
CR=1
LOG=1
YFL=0.
DEMPER=15.
IMIN=INHL+1
IMAX=INHL+SHLD
DO 3 I=IMIN,IMAX
3 PERM(I)=1
C PREPARE SIMULATION
C FIRST SET UP OVER-RIDE PERMISSIVES FOR 'NN' LOADS WITH INDEXES IND(I)
DO 4 I=1,NN
J=IND(I)
4 PERM(J)=TEMP(I)
C NOW MAKE CB'S FOR INHIBITED LOADS EQUAL TO PERMISSIVES
DO 6 I=1,INHL
6 CB(I)=PERM(I)
C INITIALIZE ON- AND OFF-TIMES AND CB'S FOR ALL SHEDDABLE LOADS
DO 5 I=IMIN,IMAX
OFFTIM(I)=80
ONTIM(I)=100
5 CB(I)=PERM(I)
C INITIALIZE AIR COMPRESSOR PRESSURES PR(I) AND STATUS OF
C PRESSURE SWITCHES PS(I)
PR(IMIN)=90.
I1=IMIN+1
PR(I1)=95.
PS(IMIN)=1
PS(I1)=1
TIMEIT=FLOAT(ITIME)
CONST=(60./DEMPER)*(TIMEIT/3600.)
ICBN=IFIX(1./CONST+.1)
NITR=IFIX(DEMPER*60./TIMEIT+.1)
C NOC AND NITR ARE CONSTANTS USED IN CONTROL ALGORITHM
C FOR SUSPENSION OF CONTROL AT BEGINNING AND CHANGE OF POLICY AT END
NOC=0
NFIN=NITR-(NITR*20)/90
TOTKWH=0.
NI=1
NPR=1
CALL DATIN
IF(LOG.GT.2) GO TO 41
GO TO 42
41 LOG1=C
CALL SCALE
CALL LINYY
WRITE(LP,300)LINB
300 FORMAT(1H,71A1)
42 CONTINUE
C BEGINNING OF SIMULATION LOOP
1000 CONTINUE

```

-Continued

```

C   CALCULATE PLANT CONDITIONS - PRESSURE
    DO 7 I=IMIN,I1
    IF(CB(I).EQ.0) GO TO 7
C   CALCULATE PRESSURES
    IF(MSTAT(I).EQ.1) PR(I)=PR(I)+2.*TIMEIT/10.
    IF(MSTAT(I).EQ.0) PR(I)=PR(I)+3.*TIMEIT/10.
C   CALCULATE STATUS OF PRESSURE SWITCHES
    IF(PR(I).LE.90.) PS(I)=1
    IF(PR(I).GE.100.) PS(I)=0
    7 CONTINUE
C   INHIBITING CONTROL
    DO 13 I=1,INHL
    IF(PERM(I).EQ.0) GO TO 13
    ITD=DURN(I)/ITIME
C   CHECK WHETHER THIS ITERATION WILL CAUSE MAXIMUM ON TIME RATIO
C   OF INHIBITED LOADS TO BE EXCEEDED
    IF(NI-ITD) 61,61,62
61  CB(I)=1
    GO TO 13
62  CB(I)=0
13  CONTINUE
C   CALCULATE CONTACTOR STATUS
    DO 8 I=1,IMAX
    8  MSTAT(I)=PERM(I)*CB(I)
    DO 9 I=IMIN,I1
    9  MSTAT(I)=MSTAT(I)*PS(I)
C   CALCULATE PLANT CONDITIONS - POWER
    CALL RAND(YFL)
C   'IBASE' REPRESENTS BASE LOAD PLUS NOISE
    IBASE=BASE+IFIX(600.*YFL)
    KWTOT=IBASE
C   COMPUTE POWER DRAWN BY INHIBITED LOADS
    DO 10 I=1,INHL
    IF(MSTAT(I).EQ.1) KW(I)=LDON(I)
    IF(MSTAT(I).EQ.0) KW(I)=LDOFF(I)
    IF(PERM(I).EQ.0) KW(I)=0
10  CONTINUE
C   COMPUTE POWER DRAWN BY SHEDDABLE LOADS
    DO 11 I=IMIN,IMAX
    KW(I)=0
    IF(MSTAT(I).EQ.1) KW(I)=LDINC(I)
11  CONTINUE
C   SUM TOTAL POWER CONSUMPTION OF THE PLANT
    DO 12 I=1,IMAX
12  KWTOT=KWTOT+KW(I)
C   CALCULATE PRESENT ENERGY CONSUMED, CONVERTED TO EQUIVALENT
C   DEMAND AT END OF THE PERIOD
    TOTKWH=TOTKWH+CONST*FLOAT(KWTOT)
    ITKWH=IFIX(TOTKWH)
    IF(LOG1.GT.1) GO TO 22
C   JUMP AROUND THE NEXT STATEMENT ONLY IF THE DEMAND LIMIT IS TO
C   BE ESTABLISHED ASSUMING NO CONTROL BEING EXERCISED
    CALL CONTRL
22  IF(LOG.EQ.0) GO TO 14
    IF(LOG.EQ.1) GO TO 18
    IF(LOG.EQ.3) GO TO 19
    GO TO 21
C   PLOTTING INSTRUCTIONS
19  CALL PLOTT
    WRITE(LP,300)LINB
    GO TO 14
C   PRINT OUT OF EQUIPMENT STATUS, POWER AND PREDICTED DEMAND LIMIT
18  WRITE(LP,15)NI,(MSTAT(J),J=1,IMAX),INDON,INDUP,KWTOT,ITGT
15  FORMAT(1H0,I4,1X,19I2,15,14,2I6)
14  IF(NI.LT.NITR) GO TO 1010
    IF(LOG1.EQ.0) GO TO 31
C   SUMMARY PRINT OUTS FOR MINIMUM AND MAXIMUM DEMAND LEVELS
    IF(LOG1.EQ.1) WRITE(LP,32) ITKWH
    IF(LOG1.GT.1) WRITE(LP,33) ITKWH
32  FORMAT(1H0,26HMIN DEMAND PERIOD POWER =,16,3H KW)

```

-Continued

```

33 FORMAT(1H0,26HMAXM DEMAND PERIOD POWER =,16,3H KW)
GO TO 34
31 II=ITKWH/4
C DEMAND PERIOD LOG AFTER BEING UNDER DEMAND CONTROL FOR THE PERIOD
WRITE(LP,16)DEMLIM,ITGT,II
16 FORMAT(1H0,34HEND OF DEMAND PERIOD LOG: TARGET ,16,2HKW,3X,
18HACTUAL ,16,2HKW,3X,7HENERGY ,16,3HKWH//)
34 CONTINUE
C PREPARE FOR A NEW DEMAND PERIOD
TOTKWH=0.
NI=0
NPR=NPR+1
CALL DATIN
IF(LOG.GT.2) GO TO 411
GO TO 421
411 LOG1=0
CALL SCALE
CALL LINYY
WRITE(LP,300)LINB
421 CONTINUE
IF(NPR.GT.NPERD) GO TO 21
1010 NI=NI+1
C RETURN TO THE BEGINNING OF THE ITERATION
GO TO 1000
C STOP WHEN 'NPERD' PERIODS HAVE BEEN RUN
21 CONTINUE
WRITE(LP,553)
553 FORMAT(1H ,18HTYPE IN LETTER 'S'//)
END

S
LIST,S,0
C RANDOM NUMBER GENERATOR SUBROUTINE
C
SUBROUTINE RAND(A)
DATA MP,MSK,M/3,*7FFF,4579/
DATA ACBN,BCBN/65536.,2147483647./
IF(A.NE.0.) GO TO 1
S LDA M
S STA IA
S1 LDA IA
S STZ 4
S MPY MP
S STA IB
S LDA IA
S ADD 4
S NJP 2
S JMP 3
S2 INC IB
S AND MSK
S3 STA IE
S LDA IB
S STA IA
YF1=FLBAT(IA)
IF(YF1.LT.0.) YF1=ACBN+YF1
YF2=FLBAT(IE)*ACBN
A=(YF1+YF2)/BCBN
RETURN
END

S
LIST,S,0
BLOCK DATA
INTEGER IND(20),TEMP(10),MAX(22)
INTEGER LDINC(30),OFFMAX(30),BNRAT0(30),PRI0R(30),SUBPRI(30)
INTEGER PERM(30),OFFTIM(30),ONTIM(30),C0(30),M0STAT(30),CWRD(30)
INTEGER SHLD,CRLD,BIAS,DEMLIM,BASE
COMMON /CONINP/INHL,SHLD,CRLD,TIMEIT,BIAS,DEMLIM,LOG,NPERD,
1CONST,ICBN,NITR,ITIME,N0C,NFIN,NI,KWT0T,ITKWH,INDDN,INDUP,ITGT,
2LINE,LOG1
COMMON /COMDAT/LDINC,OFFMAX,BNRAT0,PRI0R,SUBPRI,PERM,OFFTIM,ONTIM,
1C0,M0STAT,CWRD
COMMON /DATBL/NN,IND,TEMP,BASE
COMMON /R0TDAT/IMIN,IMAX,MGRP,MAX

```



-Continued

```

DATA BASE/2000/
DATA ITIME,BIAS,DEMLIM/20,50,4700/
DATA LOG,NPERD,LOG1/1,10000,0/
DATA INHL,SHLD,CRLD/2,17,2/
DATA NN,IND/3,1,2,19,17*0/
DATA TEMP/0,1,0,7*0/
DATA MGRP,MAX/6,2,2,2,8,1,2,16*0/
DATA LDINC/932,2238,112,112,410,410,186,75,75,75,75,75,75,
175,75,37,37,336,105,11*0/
DATA OFFMAX/149,0,100,100,200,200,180,180,180,180,180,180,
1180,180,180,300,300,300,300,11*0/
DATA BNRAT0/450,450,160,160,80,80,80,100,100,100,100,100,100,
1100,100,100,100,160,160,11*0/
DATA PRI0R/0,0,3,3,6,6,5,4,4,4,4,4,4,1,1,2,2,11*0/
DATA SUBPRI/0,0,1,2,1,2,0,1,2,3,4,5,6,7,8,1,2,1,2,11*0/
END

```

S  
LIST,S,0

C  
C MAIN DEMAND CONTROL ALGORITHM  
C

```

SUBROUTINE CONTROL
INTEGER INHL,SHLD,CRLD
INTEGER LDINC(30),OFFMAX(30),BNRAT0(30),PRI0R(30),SUBPRI(30)
INTEGER PERM(30),OFFTIM(30),BNTIM(30),CB(30),M0STAT(30),CWRD(30)
INTEGER BIAS,DEMLIM,SLOPE,MAX(22)
INTEGER CR,LP
LOGICAL IFL
COMMON /COMDAT/LDINC,OFFMAX,BNRAT0,PRI0R,SUBPRI,PERM,OFFTIM,BNTIM,
1CB,M0STAT,CWRD
COMMON /CONINP/INHL,SHLD,CRLD,TIMEIT,BIAS,DEMLIM,LOG,NPERD,
1CONST,IC0N,NITR,ITIME,N0C,NFIN,NI,KWT0T,ITKWH,INDDN,INDUP,ITGT,
2LINE,LOG1
COMMON /R0TDAT/IMIN,IMAX,MGRP,MAX
COMMON /EQUIP/LP,CR
DATA I100,I32TH/100,32000/
IPWR=KWT0T

```

```

C FORCE LOAD ON IF OFF EXCESSIVELY AND RESET TIME COUNTERS
DO 1 I=IMIN,IMAX
IF(PERM(I).EQ.0) OFFTIM(I)=0
IF(M0STAT(I).EQ.0) GO TO 3
BNTIM(I)=BNTIM(I)+ITIME
GO TO 1
3 OFFTIM(I)=OFFTIM(I)+ITIME
IF(OFFTIM(I).LE.OFFMAX(I)) GO TO 1
CB(I)=1
IPWR=IPWR+LDINC(I)
IF(SUBPRI(I).EQ.0) GO TO 6
CALL ROTATE(PRI0R,SUBPRI,I)
6 BNTIM(I)=0
1 CONTINUE
IF(LOG1.EQ.0) GO TO 91
C DO LOOP N0. 92 CAUSES UNITS TO BE SWITCHED ON IF THE 'BNRAT0' HAS
C BEEN EXCEEDED AND THE ASSOCIATED CONSTRAINT IS TO BE EXERCISED
C RIGIDLY (I.E. LOG1=1)
DO 92 J=IMIN,IMAX
ITEM=OFFTIM(J)
ITT=BNTIM(J)
S STZ 4
S MPY I100
S BJP 161
S JMP 162
S61 LDA I32TH
S62 DIV ITEM
S STA ITEM
IF(ITEM.LT.BNRAT0(J)) GO TO 92
CB(J)=0
OFFTIM(J)=0
BNTIM(J)=0
92 CONTINUE
RETURN

```



-Continued

```

91 CONTINUE
C   CALCULATE TARGET AND EXERCISE CONTRL
   IF(NI.LE.NOC) GO TO 1000
   ITGT1=DEMLIM+BIAS
   IF(NI.LE.NFIN) GO TO 13
   ITGT1=DEMLIM*(BIAS*(NITR-NI))/(NITR-NFIN)
13 CONTINUE
200 IFL=FALSE.
S   STZ    4
S   LDA    NITR
S   SUB    NI
S   MPY    IPWR
S   DIV    ICON
S   STA    ITEM
   SLOPE=ITGT1-(ITKWH+ITEM)
   IF(SLOPE.LE.0) GO TO 219
C   SEARCH FOR LEAST SHEDDABLE LOAD
   N1=0
   N2=0
   INDUP=0
   DO 11 I=IMIN,IMAX
   IF(PERM(I).EQ.0) GO TO 11
   IF(I.EQ.INDDN) GO TO 11
   IF(PRIOR(I).LT.N1) GO TO 11
   IF(CO(I).EQ.1) GO TO 11
   IF(PRIOR(I).NE.N1) GO TO 12
   IF(SUBPRI(I).LE.N2) GO TO 11
12 INDUP=I
   N1=PRIOR(I)
   N2=SUBPRI(I)
11 CONTINUE
   IF(INDUP.EQ.0) GO TO 1000
   IF(SLOPE.LT.LDINC(INDUP)) GO TO 1000
   CO(INDUP)=1
   IPWR=IPWR+LDINC(INDUP)
   IF(SUBPRI(INDUP).EQ.0) GO TO 14
   CALL ROTATE(PRIOR,SUBPRI,INDUP)
14 ENTIM(INDUP)=0
   IF(LOG.NE.1) GO TO 200
   INDPR=0
   CALL PRINT(INDPR,INDUP,IPWR)
   GO TO 200
219 CONTINUE
C   SEARCH FOR MOST SHEDDABLE LOAD
   N4=100
   N5=100
   INDDN=100
   DO 7 I=IMIN,IMAX
   IF(PRIOR(I).GT.N4) GO TO 8
   IF(CO(I).EQ.0) GO TO 8
   IF(PRIOR(I).NE.N4) GO TO 9
   IF(SUBPRI(I).GE.N5) GO TO 8
9   IF(IFL) GO TO 10
   IF(OFFTIM(I).LT.1) GO TO 10
   ITEM=OFFTIM(I)
   ITT=ENTIM(I)
S   STZ    4
S   MPY    1100
S   BJP    165
S   JMP    166
S65 LDA    132TH
S66 DIV    ITEM
S   STA    ITEM
   IF(ITEM.LT.ENTIM(I)) GO TO 8
10 INDDN=I
   N4=PRIOR(I)
   N5=SUBPRI(I)
8   CONTINUE
7   CONTINUE
900 IF(INDDN.EQ.100) GO TO 120
   ITEMP=LDINC(INDDN)
   IF(ITEM.GT.180) ITEMP=ITEM/2
   ITEMP=SLOPE+ITEM
   IF(NI.LT.NFIN) GO TO 121

```

- Continued

```

      IF(SLOPE.LT.0) GO TO 130
121 IF(ITEMP.GT.0) GO TO 1000
130 C0(INDDN)=0
      IPWR=IPWR+LDINC(INDDN)
      0FFTIM(INDDN)=0
      IF(L0G.NE.1) GO TO 200
      INDPR=1
      CALL PRINT(INDPR,INDDN,IPWR)
      GO TO 200
120 IF(NI.EQ.NFIN) WRITE(LP,111)
111 FORMAT(1H,30HCONSTRAINTS MAY BE OVER-RIDDEN//)
      IF(IFL) GO TO 1000
1000 CONTINUE
      ITGT=ITGT1-SLOPE
      RETURN
      END

```

S  
LIST,S,0

C  
C SUBROUTINE TO ROTATE PRIORITIES

```

C
      SUBROUTINE ROTATE(PRIOR,SUBPRI,IND)
      INTEGER PRIOR(30),SUBPRI(30),MAX(22)
      COMMON /ROTDAT/IMIN,IMAX,MGRP,MAX
      N1=PRIOR(IND)
      DO 1 I=1,IMAX
      IF(PRIOR(I).NE.N1) GO TO 1
      SUBPRI(I)=SUBPRI(I)+1
      IF(SUBPRI(I).EQ.0) SUBPRI(I)=MAX(N1)
1 CONTINUE
      RETURN
      END

```

S  
LIST,S,0

C  
C PRINT OUT OF MESSAGE AS CONTROLLER SWITCHES LOADS

```

C
      SUBROUTINE PRINT(IND,LD,IPWR)
      INTEGER LP,CR
      INTEGER A(4),B(4)
      COMMON /EQUIP/LP,CR
      DATA A/1HU,1HP,1H,1H/,B/1HD,1H0,1HW,1HN/
      IF(IND.EQ.0) WRITE(LP,1) A,LD,IPWR
      IF(IND.EQ.1) WRITE(LP,1) B,LD,IPWR
1 FORMAT(1H,4A1,2X,6HUNIT#,13,2X,6HP0WER,15,3H KW)
      RETURN
      END

```

S  
LIST,S,0

C  
C SET UP OF SCALE VALUES FOR PLOT OF LOADS

```

C
      SUBROUTINE SCALE
      INTEGER KW(30),IBASE
      INTEGER CR,LP
      INTEGER LINB(71)
      REAL A(5)
      COMMON /PLOT/KW,KMIN,KMAX,IBASE,IDUFF,LINB
      COMMON /EQUIP/LP,CR
      A(5)=6500.
      A(1)=0.
      DIFF=(A(5)+A(1))/4.
      DO 1 I=2,4
1 A(I)=A(1)+DIFF*FLOAT(I-1)
      KMIN=IFIX(A(1))
      KMAX=IFIX(A(5))
      IDUFF=KMAX-KMIN
      WRITE(LP,2)A
2 FORMAT(1H0,G9.3,6X,G9.3,7X,G9.3,8X,G9.3,5X,G9.3)
      RETURN
      END

```

S  
LIST,S,0  
C

-Continued

C SET UP OF Y ORDINATE SCALE MARKS

C

```

SUBROUTINE LINYY
  INTEGER KW(30), IND(5), IBASE
  INTEGER LINB(71), Y, H0R
  DATA Y, H0R/1H Y, 1H= /, IND/1, 18, 36, 54, 71/
  DO 1 I=1, 71
1  LINB(I)=H0R
  DO 2 I=1, 5
    J=IND(I)
2  LINB(J)=Y
  RETURN
END

```

S

LIST, S, 0

C

C CHARACTER SET UP IN LINE BUFFER AS FUNCTION OF 9 INPUTS  
C AND PERFORMS PLOTTING FUNCTION

C

```

SUBROUTINE PLOTT
  INTEGER SHLD, CRLD, BIAS, IBASE, DEMLIM, KW(30), IB(9), IND(9)
  INTEGER LINB(71), CHAR(9), BLANK, EYE
  COMMON /CONINP/INHL, SHLD, CRLD, TIMEIT, BIAS, DEMLIM, LOG, NPERD,
1  CONST, IC0N, NITR, ITIME, N0C, NFIN, NI, KWT0T, ITKWH, INDDN, INDUP, ITGT,
2  LINE
  COMMON /PLOT/KW, KMIN, KMAX, IBASE, IDUFF, LINB
  DATA BLANK, EYE/1H , 1H I /, IND/2, 3, 4, 7, 8, 18, 1, 1, 1/
  DATA CHAR/1H), 1H(, 1H*, 1H+, 1H0, 1H#, 1H%, 1H&, 1H*/
  DATA I72/72/
  ITEM=NI/50
  ITEM=ITEM*50
  IF(ITEM.EQ.NI) GO TO 1
  IF(NITR.EQ.NI) GO TO 1
  DO 2 I=1, 71
2  LINB(I)=BLANK
  LINB(1)=EYE
  GO TO 3
1  CALL LINYY
  MULT=ITIME*NI
  CALL INDX(MULT)
3  DO 44 J=1, 6
    IND1=IND(J)
44  IB(J)=KW(IND1)
    IB(3)=IB(3)*9+100
    IB(4)=IBASE
    IB(5)=IB(5)*10+100
    IB(6)=IB(6)*10+250
    IB(7)=KWT0T
    IB(8)=ITKWH
    IB(9)=DEMLIM
  DO 4 I=1, 9
    ITEM=IB(I)
S  STZ 4
S  SUB KMIN
S  MPY I72
S  DIV IDUFF
S  STA IN
    IF(IN.GT.71) IN=71
    IF(IN.LT.1) IN=1
4  LINB(IN)=CHAR(I)
    ITEM=NI/10
    ITEM=ITEM*10
    IF(ITEM.NE.NI) GO TO 150
    MULT=ITIME*NI
    CALL INDX(MULT)
150 CONTINUE
  RETURN
END

```

S

LIST, S, 0

C

C SET UP OF NO. OF SECONDS TO THIS ITERATION

C

SUBROUTINE INDX(MULT)



- Continued

```

INTEGER KW(30),IBASE
INTEGER LINB(71),NUMB(10)
COMMON /PLBT/KW,KMIN,KMAX,IBASE,IDUFF,LINB
DATA NUMB/1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1H0/
ITEM=MULT
K=1
IF(ITEM.GE.10) K=2
IF(ITEM.GE.100) K=3
DO 2 J=1,K
K1=10**(K-J)
DO 1 I=1,10
ITEM=ITEM+K1
IF(ITEM.GE.0) GO TO 1
ITEM=ITEM+K1
I1=I-1
IF(I1.EQ.0) I1=10
LINB(J)=NUMB(I1)
GO TO 2
1 CONTINUE
WRITE(LP,4) MULT
4 FORMAT(1H,12HFAULT: SECS=,I6)
GO TO 20
2 CONTINUE
RETURN
20 CONTINUE
END

```

S

LIST,S,0

```

SUBROUTINE DATIN
INTEGER SHLD,CRLD
INTEGER LP,CR
INTEGER J1(3),PERM(30),BASE,BIAS,DEMLIM,D(30,11)
INTEGER A(8),M(3,5)
INTEGER BLANK,B(10)
COMMON /EQUIP/LP,CR
COMMON /COMDAT/D
COMMON /CONINP/INHL,SHLD,CRLD,TIMEIT,BIAS,DEMLIM,LBG,NPERD,
1CONST,ICON,NITR,ITIME,NOC,NFIN,NI,KWTOT,ITKWH,INDDN,INDUP,ITGT,
2LINE,LBG1
EQUIVALENCE (D(1,6),PERM(1))
DATA A/1HB,1HU,1HT,1HD,1HA,1HP,1HL,1HE/
DATA B/1H1,1H2,1H3,1H4,1H5,1H6,1H7,1H8,1H9,1H0/
DATA BLANK/1H /
100 WRITE(LP,28)
WRITE(LP,1)
CALL ENPACK(M,N,A,B)
IF(N.NE.1) GO TO 100
28 FORMAT(1H )
1 FORMAT(1H,14HENTER MNEMONIC)
J=0
DO 2 I=1,8
IF(M(1,5).NE.A(I)) GO TO 2
J=I
2 CONTINUE
IF(J.EQ.0) GO TO 100
IF(J.EQ.8) GO TO 1000
GO TO(101,102,103,104,105,106,107),J
101 WRITE(LP,201)
GO TO 150
102 WRITE(LP,202)
GO TO 150
103 WRITE(LP,203)
GO TO 150
104 WRITE(LP,204)
GO TO 150
105 WRITE(LP,205)
GO TO 150
106 WRITE(LP,206)
GO TO 150
107 WRITE(LP,207)
150 CONTINUE
201 FORMAT(1H,18HENTER BASE LOAD KW)
202 FORMAT(1H,21HENTER UNDER-TARGET KW)
203 FORMAT(1H,39HENTER TIME INTERVAL BETWEEN PULSES SECS)

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-Continued

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204 F0RMAT(1H ,21HENTER DEMAND LIMIT KW)
205 F0RMAT(1H ,44HENTER UNIT# AND AVAILABILITY (STATUS 1 OR 0))
206 F0RMAT(1H ,48HENTER UNIT CHARACTERISTICS, UNIT#, COLUMN#,VALUE)
207 F0RMAT(1H ,34HENTER LOG TP.,# PERIODS, SUMM. TP.)
    IF(J.LE.4) K=1
    IF(J.EQ.5) K=2
    IF(J.GT.5) K=3
    WRITE(LP,5) K
    5 F0RMAT(1H ,3X,6HENTER ,I1,22H INTEGER DATA ELEMENTS)
260 CALL ENPACK(M,N,A,B)
    IF(N.EQ.K) GO TO 230
200 WRITE(LP,28)
    WRITE(LP,60)K
    GO TO 260
    60 F0RMAT(1H0,17HWRONG| RE=ENTER ,I1,22H INTEGER DATA ELEMENTS)
230 DO 111 I=1,K
    I1=6
    ITOT=C
    DO 11 M1=1,5
    I2=I1-M1
    IF(M(I,I2).EQ.BLANK) GO TO 11
    DO 12 M2=1,10
    IF(B(M2).EQ.M(I,I2)) GO TO 13
    12 CONTINUE
    GO TO 200
    13 IF(M2.EQ.10) M2=0
    ITOT=ITOT+M2*(10**(M1-1))
    11 CONTINUE
    J1(I)=ITOT
111 CONTINUE
    GO TO(301,302,303,304,305,306,307),J
301 BASE=J1(1)
    WRITE(LP,401)BASE
    GO TO 100
302 BIAS=J1(1)
    WRITE(LP,402)BIAS
    GO TO 100
303 ITIME=J1(1)
    WRITE(LP,403)ITIME
    GO TO 100
304 DEMLIM=J1(1)
    WRITE(LP,404)DEMLIM
    GO TO 100
305 IF(J1(2).GT.30) GO TO 200
    IF(J1(1).GT.1) GO TO 200
    II=J1(2)
    PERM(II)=J1(1)
    WRITE(LP,405) J1(2),PERM(II)
    GO TO 100
306 IF(J1(1).GT.10000) GO TO 200
    IF(J1(2).GT.11) GO TO 200
    IF(J1(3).GT.30) GO TO 200
    II=J1(2)
    IJ=J1(3)
    D(IJ,II)=J1(1)
    WRITE(LP,406) J1(3),J1(2),D(IJ,II)
    GO TO 100
307 LOG=J1(3)
    NPERD=J1(2)
    LOG1=J1(1)
    WRITE(LP,407)LOG,NPERD,LOG1
    GO TO 100
401 F0RMAT(1H ,13HBASE LOAD IS ,I6,3H KW)
402 F0RMAT(1H ,8HBIAS IS ,I4,3H KW)
403 F0RMAT(1H ,18HPULSE INTERVAL IS ,I4,5H SECS)
404 F0RMAT(1H ,16HDEMAND LIMIT IS ,I6,3H KW)
405 F0RMAT(1H ,7HUNIT # ,I2,9H STATUS ,I1)
406 F0RMAT(1H ,7HUNIT # ,I2,10H COLUMN # ,I2,8H VALUE ,I6)
407 F0RMAT(1H ,9HLOG TYPE ,I1,13H NO. PERIODS ,I3,10H SUMMARY ,I1)
1000 CONTINUE
    RETURN
    END

```



```

SUBROUTINE ENPACK(M,M1,A,B)
INTEGER LIN(50),M(3,5),BLANK,COMMA,A(8),B(10)
INTEGER LP,CR
DATA LP,CR/6,1/
DATA BLANK,COMMA/1H ,1H,/
DO 50 I=1,50
LIN(I)=BLANK
DO 51 I=1,3
DO 51 J=1,5
M(I,J)=BLANK
READ(CR,1) LIN
FORMAT(50A1)
N1=51
M1=0
M3=0
IFL=0
N1=N1+1
IF(N1.EQ.0) RETURN
IF(LIN(N1).EQ.BLANK) GO TO 22
IF(LIN(N1).EQ.COMMA) GO TO 22
GO TO 2
M3=M1+1
IF(M3.GT.3) RETURN
GO TO 100
DO 10 J=1,8
IF(LIN(N1).EQ.A(J)) GO TO 11
CONTINUE
GO TO 12
IFL=1
GO TO 4
DO 3 J=1,10
IF(LIN(N1).EQ.B(J)) GO TO 4
CONTINUE
M1=0
RETURN
IF(M3.EQ.M1) GO TO 5
M1=M3
M2=6
M2=M2+1
IF(M2.GT.0) GO TO 6
M1=0
RETURN
M(M1,M2)=LIN(N1)
IF(IFL.EQ.0) GO TO 100
RETURN
END

```

```

X A LIB5
U 8 A
X D TEMP
U 5 D
X E BINARY
U 4 E
  LDR5
    0G,1600,HD,,,0,3,LD
    LD,LD,LD,LD,LD,LD,LD
    LD,LD,LD,LD
    LB,MP,UN,PP,XT
X E BINARY
U 5 E
Z
L
U D
U 4
U 5
U 8
U 6 6
U 5 5
U 4 4
U 3 3
U 2 2
U 1 1

```

I claim:

1. In a control system for holding to a demand limit at the end of a billing period the power demand of an industrial plant having a plurality of interruptible loads, including means for providing an indication of power consumption of said loads during a billing period; means responsive to said means for providing an indication of power consumption for predicting a demand at the end of said billing period; means responsive to said demand predicting means for providing a demand error relative to said demand limit; means for selecting a suitable amount of power; comparator means responsive to said demand error providing means and to said power selecting means for establishing a residual error relative to said demand limit; and means responsive to the output of said comparator means for load control; the combination of:

means for setting switching constraints to at least part of said loads thereby to define among said interruptible loads and at times during said billing period, loads of controllable status and loads of non-controllable status;

said load control means including means for switching a load of a switchable amount of power in response to the sign of the output of said comparator means;

means for indicating the switching status of said loads at anytime during said billing period;

said power selecting means including priority means operative with a priority list of loads of controllable status and in accordance with the output of said switching status indicating means;

said power selecting means being operative in response to said residual error during successive decision periods within said billing period to provide

a switchable amount of power from said priority list;

said switching means being operative in response to said power selecting means during such said decision period and operative in response to said constraint setting means before such said decision period; and,

wherein said demand predicting means is responsive to operation of said constraint setting means before any such said decision period.

2. The control system of claim 1 with means for establishing said residual error relative to a biased said demand limit,

said comparator means being selectively operable relative to said demand limit and to said biased demand limit;

wherein said comparator means and said switching means are operated relative to said biased demand limit during a first period within said billing period and wherein a predetermined priority load is selected by said priority means during a second period following said first period;

with said comparator means and said switching means being operated relative to the unbiased said demand limit during said second period.

3. The control system of claim 1 with means for preventing operation of said switching means during an initial period of said billing period;

with means for establishing a bias to said demand limit during an intermediary period following said initial period; and

with means for reducing said bias progressively to zero during a final period following said intermediary period and ending with said billing period.

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