

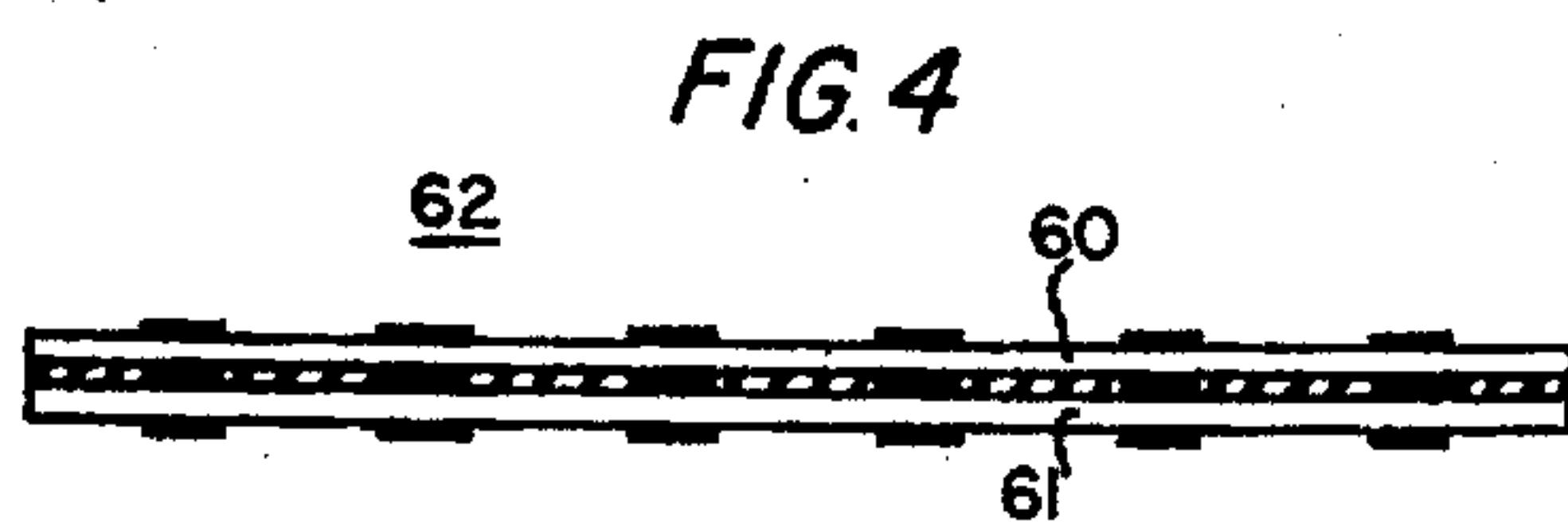
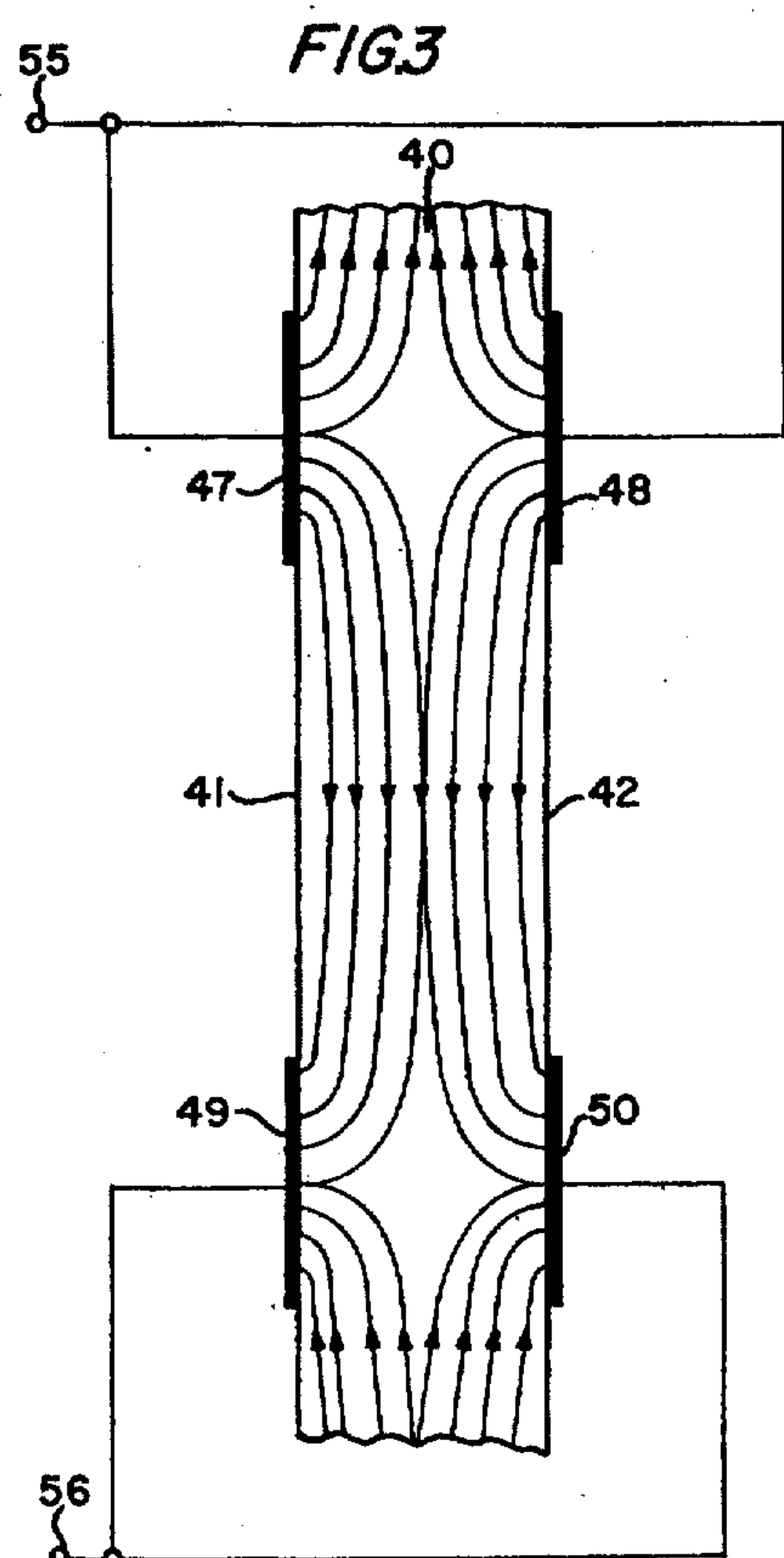
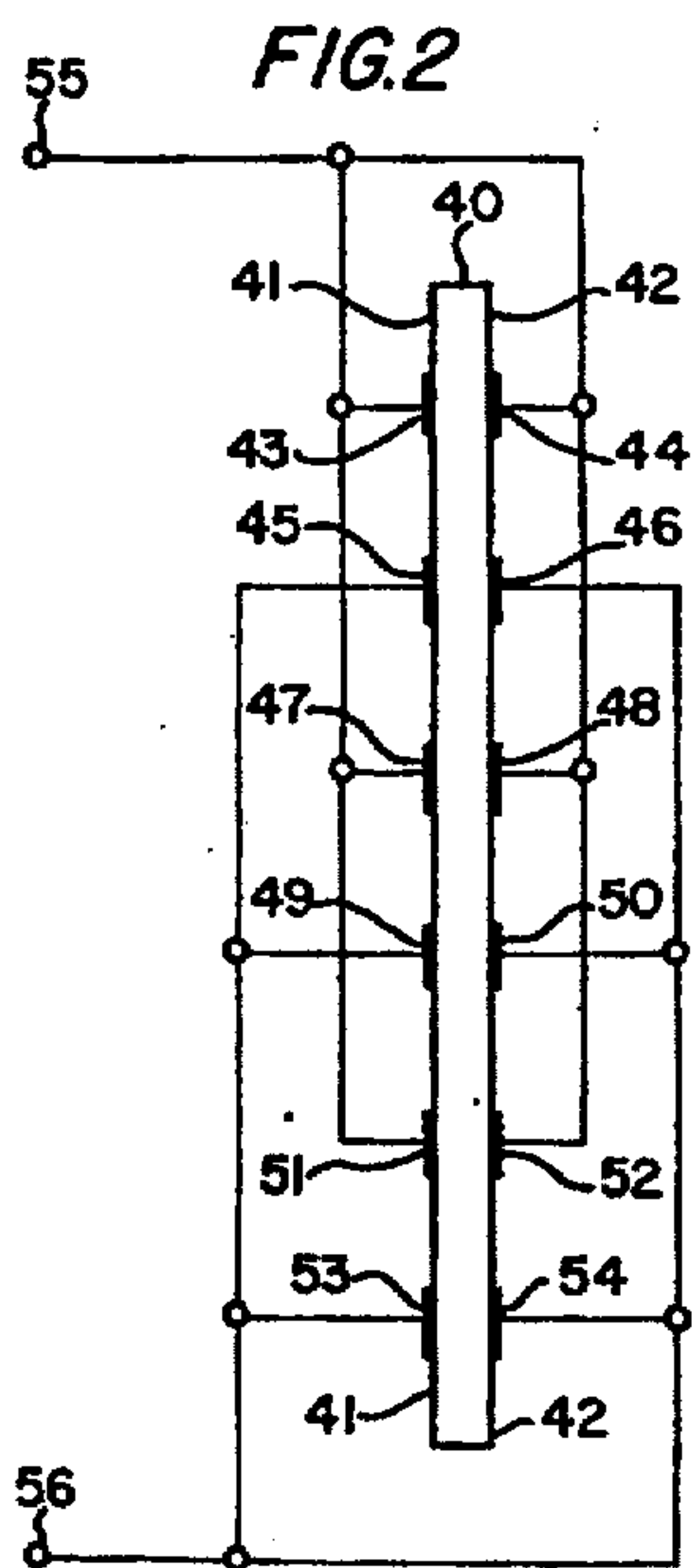
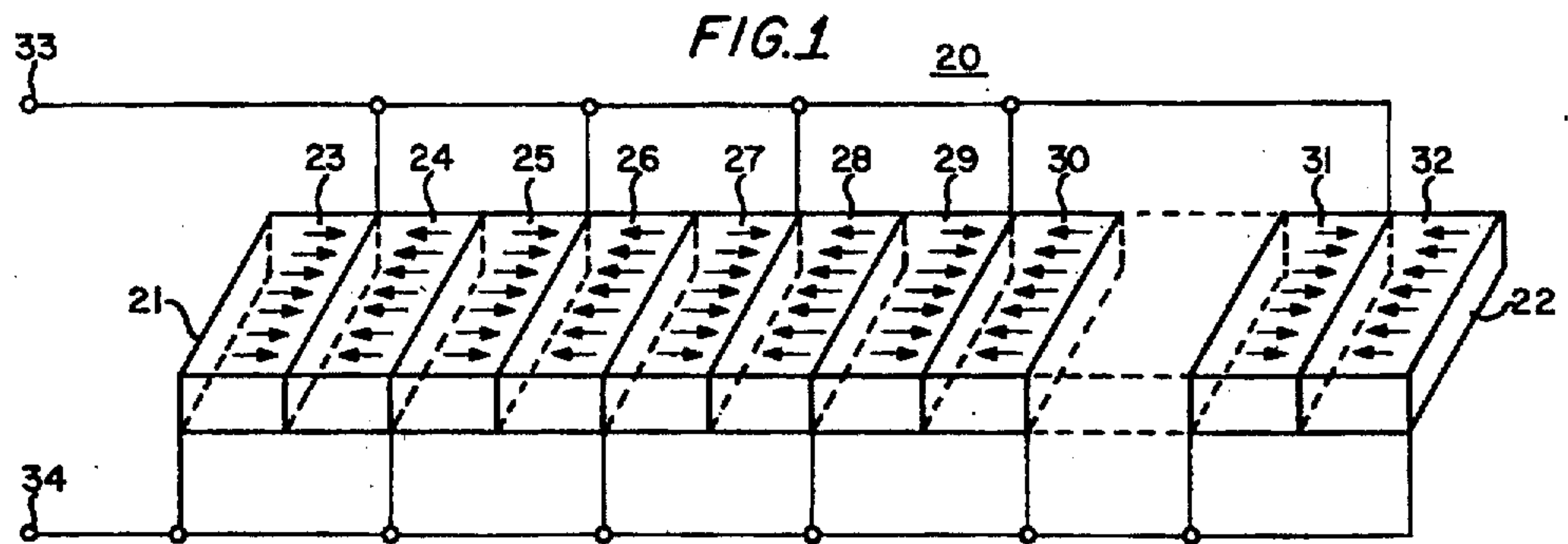
Feb. 6, 1951

A. ELLETT
PIEZOELECTRIC TRANSDUCER AND
METHOD FOR PRODUCING SAME

2,540,194

Original Filed Dec. 26, 1947

2 Sheets-Sheet 1



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2 Sheets-Sheet 2

FIG. 5

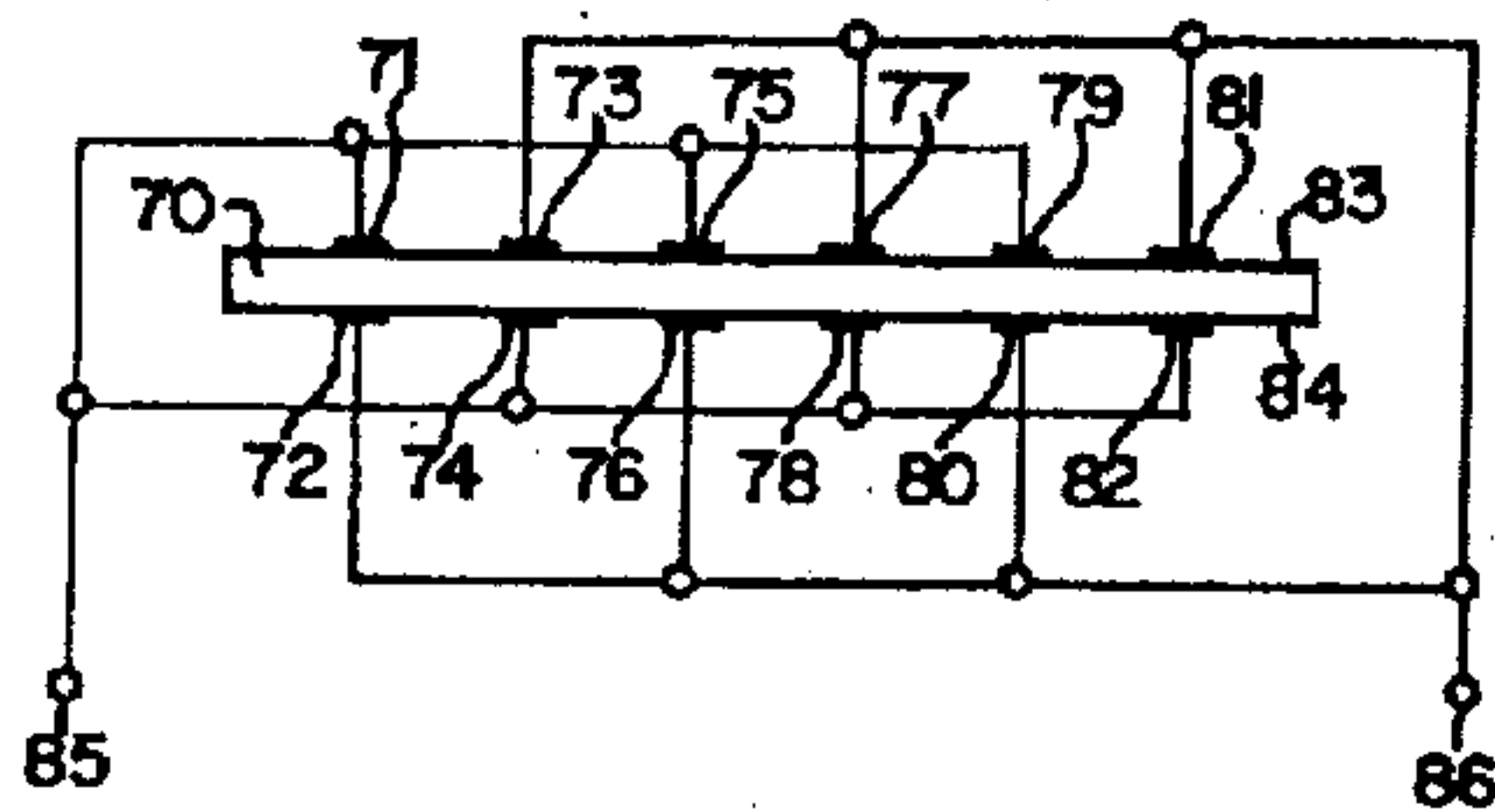


FIG. 6

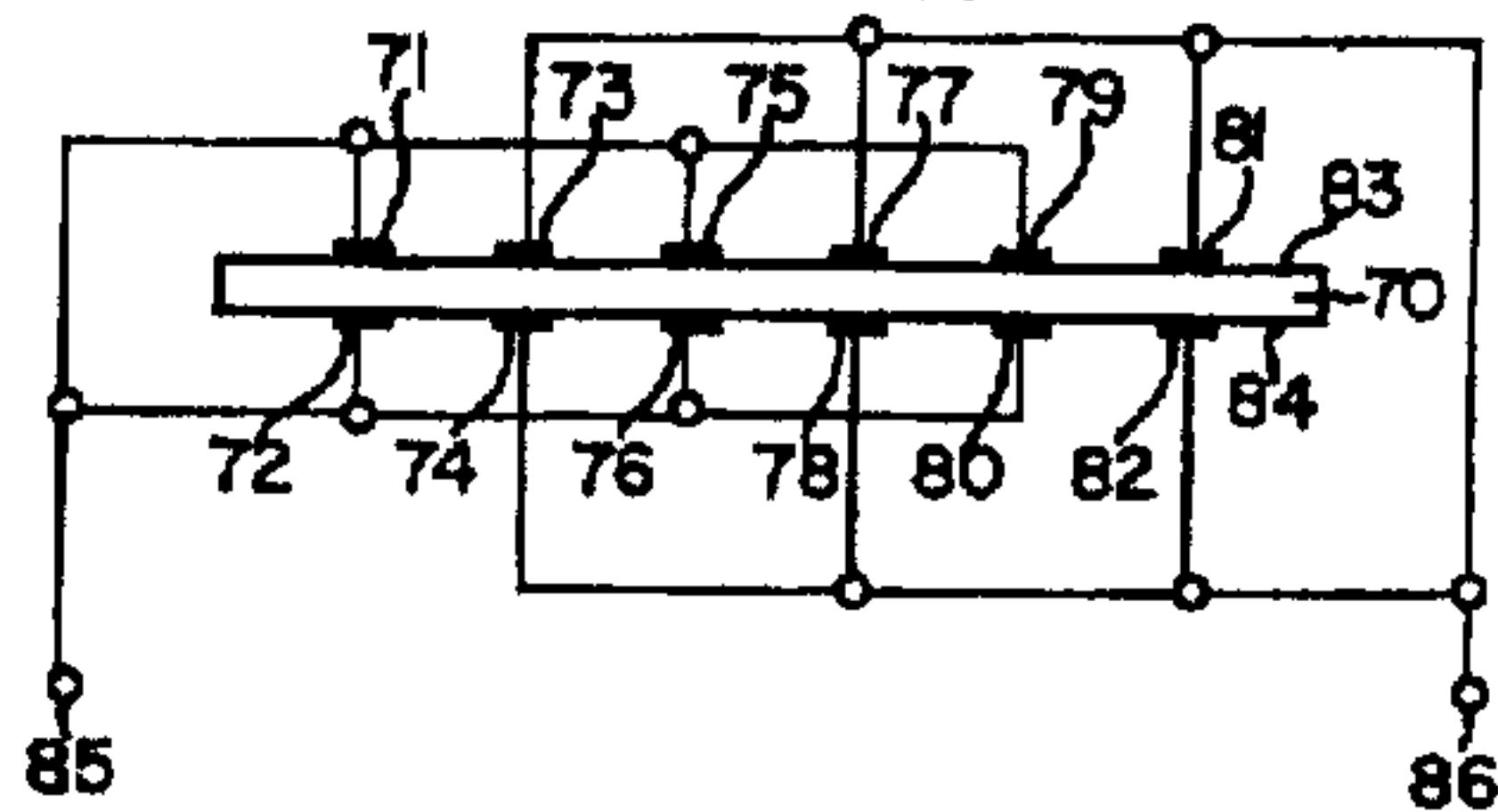


FIG. 7

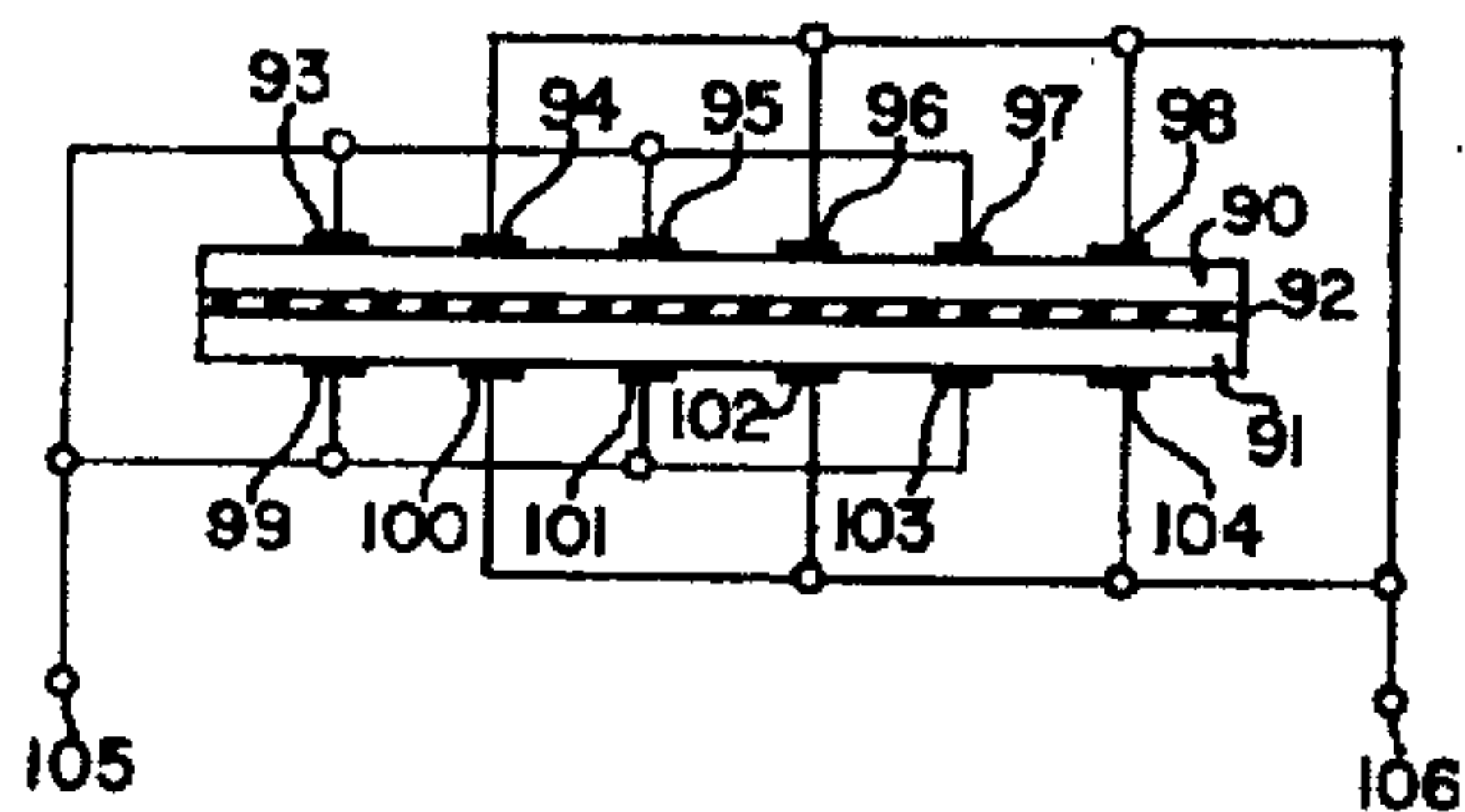


FIG. 8

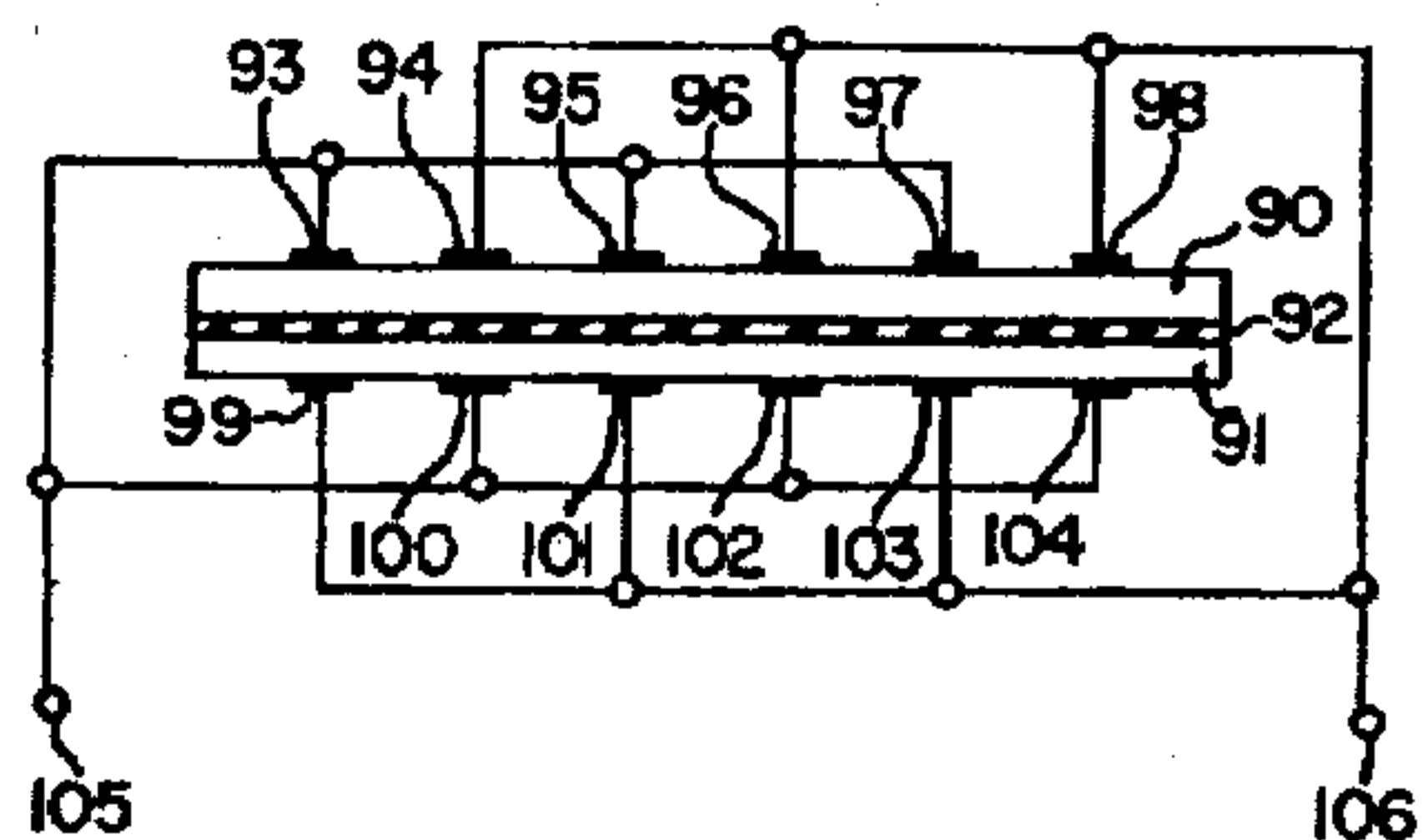


FIG. 9

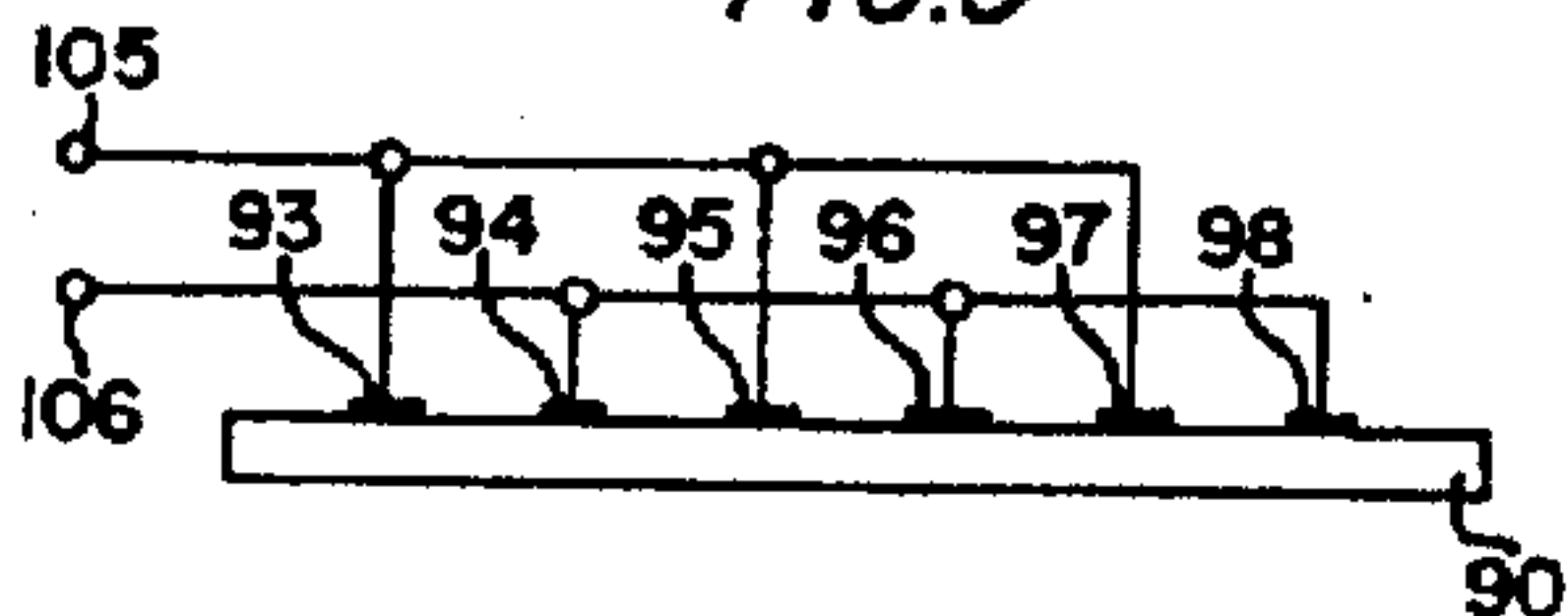
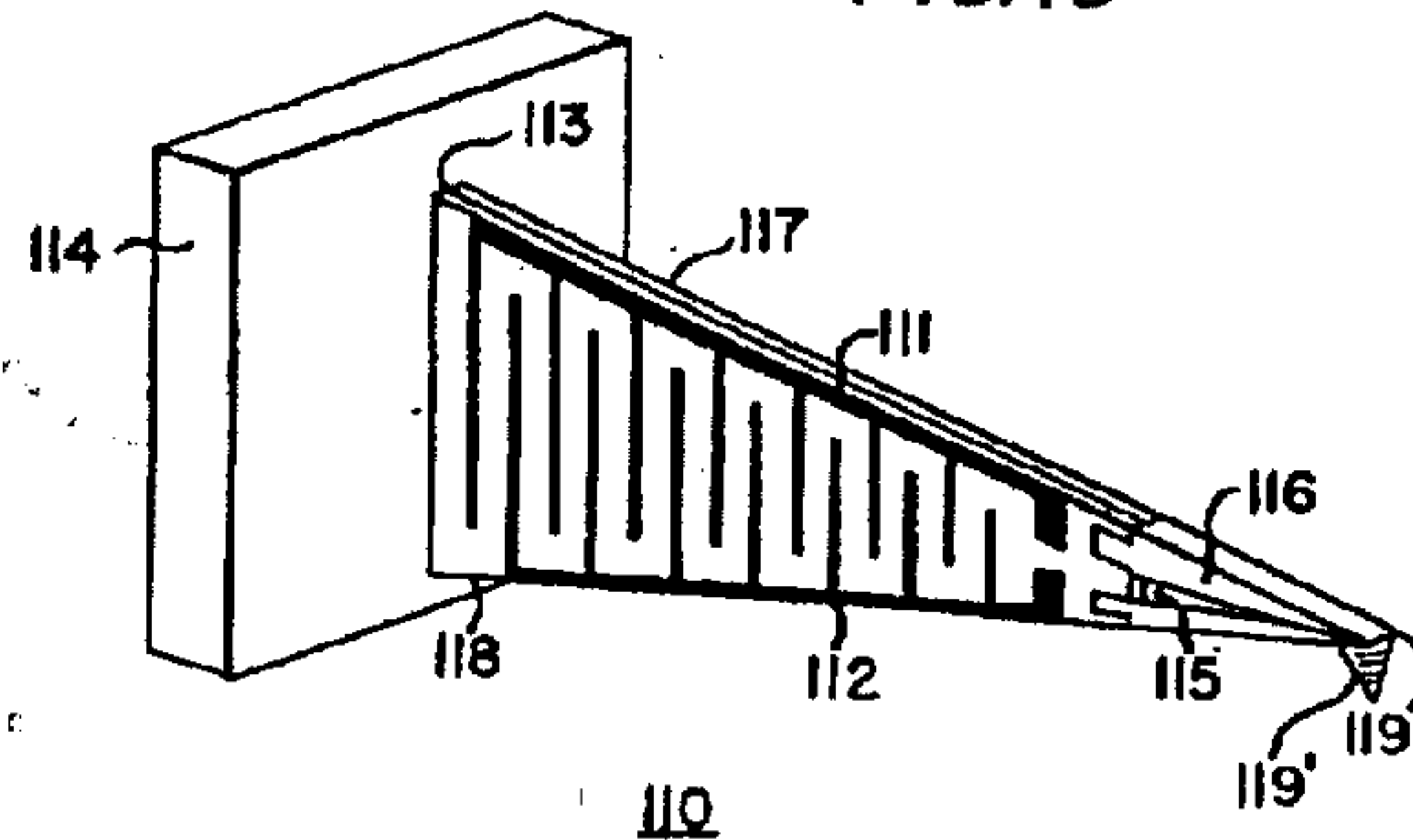


FIG. 10



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2,540,194

PIEZOELECTRIC TRANSDUCER AND
METHOD FOR PRODUCING SAMEAlexander Ellett, River Forest, Ill., assignor to
Zenith Radio Corporation, a corporation of
IllinoisOriginal application December 26, 1947, Serial No.
793,892. Divided and this application May 2,
1950, Serial No. 159,620

6 Claims. (Cl. 171—327)

1

This application is a division of the copending application of Robert Adler, Serial No. 793,892, filed December 26, 1947, assigned to the present assignee, and relates to piezo-electric transducers and to methods for producing such transducers. It is a primary object of the invention to provide an improved artificial transducer having permanent piezo-electric properties and to provide an improved method of producing such a transducer.

The use of polycrystalline aggregate such as barium titanate or barium strontium titanate, bonded with a ceramic binder, in the production of artificial piezo-electric transducers is specifically disclosed and claimed in the copending application of Walter L. Cherry, Jr., Serial No. 770,163, filed August 22, 1947, for Piezo-Electric Transducers, and which application is assigned to the same assignee as the present application.

Such artificial piezo-electric transducers as are specifically disclosed in the aforementioned copending Cherry application are particularly useful for high frequency applications. However, for optimum coupling, the direction of mechanical stress must be identical with that of the piezo-electric axis and that of the alternating field; consequently transducers of this type are not readily applicable to audio frequency devices. The minimum frequency at which such transducers may be operated is determined by the maximum capacitance, or electrical compliance, commensurate with practical values of mechanical compliance. If the mechanical compliance is made large enough to suit practical requirements by making the cross-sectional area small, the associated capacitance is too small for audio frequency applications. If, on the other hand, a practical value of capacitance is obtained by making the cross-sectional area large, the mechanical compliance becomes inconveniently small.

It is a particular object of this invention to provide an improved artificial piezo-electric transducer which is suitable for operation at audio frequencies.

In accordance with the above-identified Adler application, it has been found that the capacitance or electrical compliance of the artificial transducers may be increased while maintaining a practical value of mechanical compliance by varying the direction of the piezo-electric axis within a single-unit transducer. It is a further object of the invention to provide a novel ceramic transducer, sensitive to bending stress, which utilizes this principle.

Frequent applications of piezo-electric trans-

2

ducers in the audio frequency range are made in phonograph pickups, microphones, and the like. In such applications, it is necessary to provide a transducer which has permanent piezo-electric properties with respect to bending stress. It is an important object of the present invention to provide a novel piezo-electric polycrystalline aggregate transducer, sensitive to bending stress, which is suitable for use as a phonograph pickup or the like, and which is rugged, inexpensive, and durable.

In the specification and claims, the term "direction," as applied to the piezo-electric axis or to the polarizing field, includes the concept of sense, therefore the phrase "piezo-electric axes having different directions" includes piezo-electric axes of opposite sense.

The term "unidirectional," as applied to polarizing fields, is employed with reference to time, and not with reference to space. Hence a "unidirectional" polarizing field is one which is produced by a unidirectional potential difference.

The terminology "polycrystalline aggregate" is employed to connote a unitary structure comprising a large number of minute crystals. The term "ceramic" necessarily implies such a structure.

The features of the invention which are believed to be novel are set forth particularly in the appended claims. The invention may more readily be understood, however, by reference to the following description taken in connection with the accompanying drawings, in which like reference numerals indicate like elements, and in which:

Figure 1 is a schematic representation of a theoretical means for attaining the objects set forth above.

Figure 2 is a schematic representation of a practical method for approximating the theoretical optimum condition shown in Figure 1.

Figure 3 is an enlarged view of a section of Figure 2 showing the electrostatic flux distribution.

Figure 4 is a schematic representation, partly in section, of a ceramic element sensitive to bending stress.

Figures 5 and 6 are schematic representations of a ceramic transducer sensitive to bending stress.

Figures 7-9 are schematic representations of an embodiment constructed in accordance with the invention.

Figure 10 is a perspective view of a physical embodiment of the invention.

Referring now to Figure 1, there is shown sche-

3

matically a slab 20 of piezo-electric material, the direction of the piezo-electric axis being assumed to be longitudinal. It is seen that the mechanical compliance in the longitudinal direction may well be high enough to suit practical requirements, since the cross-sectional area is small relative to the length, but the capacitance between electrodes located on the small surfaces 21 and 22 separated by the full length of the piece 20 is inconveniently small. In order to increase the capacitance or electrical compliance, it is assumed that slab 20 is theoretically divided into n slices 23—32 of equal length; the dotted lines indicate any desired number of intermediate slices. The capacitance between the imaginary transverse surfaces of each slice is therefore n times that between the two end surfaces 21 and 22 of slab 20, while the mechanical compliance between surfaces 21 and 22 remains unchanged. Furthermore, by interconnecting alternate transverse faces of the imaginary slices 23—32, as shown, and by connecting each set of alternate transverse faces to one of a pair of terminals 33 and 34, the total capacitance between surfaces 21 and 22 is made equivalent to n times the capacitance between the end faces of an individual imaginary slice 23; consequently the effective capacitance between surfaces 21 and 22 is increased by a factor of n^2 .

Ideally such a condition may be accomplished by polarizing adjacent slices 23—32 along the same axis but in opposite directions. Such a condition is shown schematically by the arrows which indicate the direction of polarization, and hence the direction of the piezo-electric axis, in each of the imaginary slices.

It has been found that permanent piezo-electric properties may be induced in certain polycrystalline aggregates, and furthermore, that the direction of the piezo-electric axis induced in such aggregates is identical to that of the electrostatic flux set up by the polarizing fields. Consequently, such a condition as shown schematically in Figure 1 might be accomplished if suitable unidirectional polarizing fields could be set up between the transverse faces of each of the imaginary slices 23—32. Obviously, such a situation is impractical, since no electrodes exist on the imaginary transverse surfaces between the slices.

As a practical approach to the optimum condition shown in Figure 1, there is shown in Figure 2 a slab 40 of suitable polycrystalline aggregate, such as a ceramic comprising barium titanate or barium strontium titanate mixed with a small amount of a glass forming oxide and fired to vitrification in accordance with the aforementioned copending Cherry application, on opposite faces 41 and 42 of which have been disposed a plurality of electrical terminals or electrodes 43—54. For purpose of illustration, twelve terminals have been shown; however, other numbers of terminals may be employed. Alternate pairs of opposite terminals 43, 44, 47, 48, 51, 52 and 45, 46, 49, 50, 53, 54 are interconnected and brought out to a pair of input terminals 55 and 56 respectively. When a unidirectional potential difference is applied between input terminals 55 and 56, adjacent portions of slab 40 are polarized in substantially opposite directions.

In order more fully to show and explain such polarization, there is shown in Figure 3 a detail view of a portion of slab 40 of Figure 2. The electrostatic flux distribution, and hence the di-

4

rection of polarization, is assumed, for purposes of explanation, to have a sense from + to -. If then, it is assumed that input terminal 55 is the positive terminal and input terminal 56 is the negative terminal, the electrostatic field, and hence the direction of the piezo-electric axis differs abruptly from portion to portion as schematically shown in Figure 3.

It is seen that the embodiment shown and described in conjunction with Figures 2 and 3 is only an approximation of the ideal shown and described in conjunction with Figure 1. Since those portions of the slab 40 of ceramic material which lie between opposite pairs of terminals, 47 and 48, for example, carry little or no electrostatic flux, these portions may be regarded as being "waste portions." In order to effect a compromise between the desired effective increase in electrical compliance and a minimum of "waste material," it has been found that the width of the individual terminals 43—54 should be of the order of the thickness of the slab 40, and the distance between successive terminals, 47 and 48, for example, should be of the order of twice the thickness of the slab 40. These proportions are the result of practical experiment and are intended in no sense to be construed as limitations, as other proportions may be used with varying degrees of efficiency.

In certain audio frequency applications, it is desirable to employ a piezo-electric element which is sensitive to bending. Two elements, each formed in accordance with the method shown and described in connection with Figure 2, may be fastened together, by cement or in some other suitable manner, to provide such a dimorphic element. Such a configuration is shown in Figure 4, wherein a pair of elements 60 and 61 are fastened together to form a composite body 62. In operation one element 60 is instantaneously subjected to tensile stress while the other element 61 is instantaneously subjected to compressive stress, or vice versa. Therefore, care must be taken that elements 60 and 61 are assembled and electrically connected in such a manner that the useful outputs of the individual elements are additive in the composite transducer 62.

While a transducer having permanent piezo-electric properties with respect to bending stress may be produced in the manner shown and described in conjunction with Figure 4, a simplified transducer of this type may be provided. An element sensitive to bending stress may be provided by properly applying polarizing fields to a single unitary polycrystalline aggregate body. Such an element is shown in Figure 5, wherein a unitary slab 70 of barium titanate or other suitable aggregate is provided with a plurality of electrical terminals 71—82 similarly disposed along opposite faces 83 and 84. Alternate terminals 71, 75, and 79 on face 83 and alternate terminals 74, 78, and 82 on face 84 are interconnected and brought out to an input terminal 85, and the remainder of the terminals 72, 73, 76, 77, 80, and 81 are interconnected and brought out to a second input terminal 86.

By applying a unidirectional potential difference between input terminals 85 and 86, unidirectional polarizing fields are applied between successive terminals, 71 and 73, for example, on each face 83, 84 of slab 70. Furthermore, each terminal (71, for example) is oppositely polarized from the terminal (72, for example) which is directly opposite therefrom, and the polarizing

5

fields between opposite pairs of successive terminals (71, 73 and 72, 74 for example) are opposite in sense. By these means, the direction or sense of the piezo-electric axis is made to differ abruptly from portion to portion throughout the single piece 70 in a manner similar to the piezo-electric axis distribution in a composite dimorphic element such as that shown in Figure 4.

After maintaining the polarizing fields for a sufficient period of time at least to approach saturation of the piezo-electric effect, such fields are removed, and the connections of terminals 71—82 are changed to insure additive outputs in response to bending. Slab 70 with terminals 71—82 reconnected for proper output at terminals 85 and 86 is shown in Figure 6, in which alternate pairs of opposite terminals 71, 72, 75, 76, 79, and 80, and 73, 74, 77, 78, 81, and 82 are interconnected. Such an interconnection is desirable in order to minimize the shunt capacitance between output terminals 85 and 86 which effectively reduces the useful output of such a transducer. The embodiment of Figures 5 and 6 is specifically disclosed and claimed in the copending application of Walter L. Cherry, Jr., Serial No. 159,613, filed concurrently herewith, for Piezo-Electric Transducer and Method for Producing Same, and assigned to the present assignee.

Figure 7 shows an alternative method of producing essentially the same result while greatly reducing any shunt capacitance across the output terminals. In this embodiment, in accordance with the present invention, a pair of polycrystalline aggregate bodies 90 and 91 are fastened together by cementing means 92 of low dielectric constant thereby to form a composite body. Cementing means 92 may comprise a layer of cementing material of low dielectric constant, although the desired results may be achieved by glazing slabs 90 and 91 and firing with the glazed sides in contact, by firing a "sandwich" of three ceramic slabs, or by other suitable means. Opposite faces of the composite body are provided with a plurality of similarly disposed electrical terminals or electrodes 93—98 and 99—104, alternate pairs of opposite terminals 93, 99, 95, 101, 97, 103, and 94, 100, 96, 102, 98, 104 being interconnected and brought out to a pair of input terminals 105, and 106, respectively. After polarizing in the usual manner, the terminal connections on one face of the composite body are reversed to insure additive outputs in response to bending, as shown in Figure 8, and terminals 105 and 106 become output terminals. Although opposite terminals (93 and 99, for example) have opposite polarities associated therewith, the thin layer of cementing material 92 so reduces the effective capacitance shunting the output that satisfactory operation is insured.

While the embodiment shown in Figures 7 and 8 is formed by cementing bodies 90 and 91 together before polarization, it is to be understood that the individual bodies 90 and 91 may be polarized separately and then firmly united in such manner as to insure additive outputs in response to bending. Such a method is shown schematically in Figure 9, in which body 90 is separately polarized. Alternate terminals 93, 95, 97 and 94, 96, 98 are connected to respective input terminals 105 and 106. After polarization, two such bodies are cemented or otherwise fastened together to produce a composite body such as that shown in Figure 8.

It is also to be understood that, although pairs of terminals 93—104 have been shown connected

6

in parallel, pairs of terminals may be connected in series in certain applications in which such connection is desirable.

As a variant of this embodiment, two slabs of polycrystalline aggregate such as slab 90 in Figure 9 may be provided each with electrical terminals differently disposed in such a way that, after polarization, such slabs may be fastened together in a manner similar to that shown and described in conjunction with Figure 4. In this way, objectionable shunt capacitance between the output terminals may be avoided without the use of low dielectric constant cementing means.

As a further variant, the composite body shown in Figures 7 and 8 may be polarized with the terminals 93—104 connected as in Figure 8, in which case the terminals 93—104 are reconnected as shown in Figure 7 to insure additive outputs. In this manner, the shunt capacitance across the output is minimized by interconnecting opposite terminals.

There is shown in Figure 10 a phonograph pickup 110 constructed in accordance with the invention. The terminals 111 and 112 are shown in the form of a pair of intermeshing combs for efficient polarization, and may be of silver paint or other suitable material applied by silk screen, vacuum evaporation, or other suitable process. In a practical application, the terminals applied on the back side (not shown) of element 110 may be made in the form of a mirror image of those applied to the front side in order to minimize the undesired capacitance shunting the output. One end 113 of transducer 110 is firmly clamped in a bracket 114, and the other end 115 is provided with a rigid extension 116 so constructed and arranged that the edges 117 and 118 of transducer 110 and extension 116 all converge to a point 119. Lateral motion at point 119, which may be translated from the undulations of a record disk by means of a stylus 119' secured to extension 116 at point 119, then results in corresponding electrical output between terminals 111 and 112; by making transducer 110 trapezoidal in shape, the conditions of a uniform-stress beam are approached.

While there has been shown and described a certain preferred embodiment of the invention, it will be understood that numerous variations and modifications may be made, and it is contemplated, in the appended claims, to cover all such variations and modifications as fall within the true spirit and scope of the invention.

I claim:

1. The process of producing a permanently piezo-electric ceramic body sensitive to bending stress, said process comprising fastening together corresponding faces of a pair of polycrystalline aggregate bodies thereby to produce a composite body, similarly disposing along each of two opposite faces of said composite body a plurality of parallel electrodes, applying unidirectional polarizing fields having substantially opposite directions between successive pairs of electrodes on each of said opposite faces, and maintaining said fields for a period of time sufficient at least to approach saturation of the piezo-electric effect in said composite body.

2. The process of producing a permanently piezo-electric ceramic body sensitive to bending stress, said process comprising fastening together corresponding faces of a pair of polycrystalline aggregate bodies by cementing means having a dielectric constant which is low relative to that of said aggregate thereby to produce a composite

7

body, similarly disposing along each of two opposite faces of said composite body a plurality of parallel electrodes, applying polarizing fields having substantially opposite directions between successive pairs of electrodes on each of said opposite faces, and maintaining said fields for a period of time sufficient at least to approach saturation of the piezo-electric effect in said composite body.

3. The process of producing a permanently piezo-electric ceramic body sensitive to bending stress, said process comprising disposing along a single face of each of a pair of similar polycrystalline aggregate bodies a plurality of parallel electrodes, applying unidirectional polarizing fields having substantially opposite directions between successive pairs of electrodes disposed along each of said faces, maintaining said fields for a period of time sufficient at least to approach saturation of the piezo-electric effect in said bodies, and firmly uniting the faces of said bodies which are opposite to the electrode-bearing faces.

4. The process of producing a permanently piezo-electric ceramic body sensitive to bending stress, said process comprising disposing along a single face of each of a pair of similar polycrystalline aggregate bodies a plurality of parallel electrodes, the disposition of electrodes on the second of said bodies being substantially a mirror image of that on the first of said bodies, applying unidirectional polarizing fields having substantially opposite directions between successive pairs of electrodes disposed along each of said faces, maintaining said fields for a period of time sufficient at least to approach saturation of the piezo-electric effect in said bodies, and firmly uniting the faces of said bodies which are opposite to the electrode-bearing faces.

8

5. A ceramic element having permanent piezo-electric properties, said element including a pair of solid polycrystalline aggregate bodies fastened together by cementing means having a dielectric constant which is low relative to that of said aggregate thereby to form a composite body, and a plurality of electrodes similarly disposed along each of two opposite faces of said composite body, the direction of the piezo-electric axis being substantially opposite between successive pairs of electrodes on each of said faces.

6. A ceramic element having permanent piezo-electric properties, said element including a pair of solid polycrystalline aggregate bodies fastened together by cementing means having a dielectric constant which is low relative to that of said aggregate thereby to form a composite body, said aggregate including individual crystals of barium titanate bonded together with a ceramic binder, and a plurality of electrodes similarly disposed along each of two opposite faces of said composite body, the direction of the piezo-electric axis being substantially opposite between successive pairs of electrodes on each of said faces.

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