

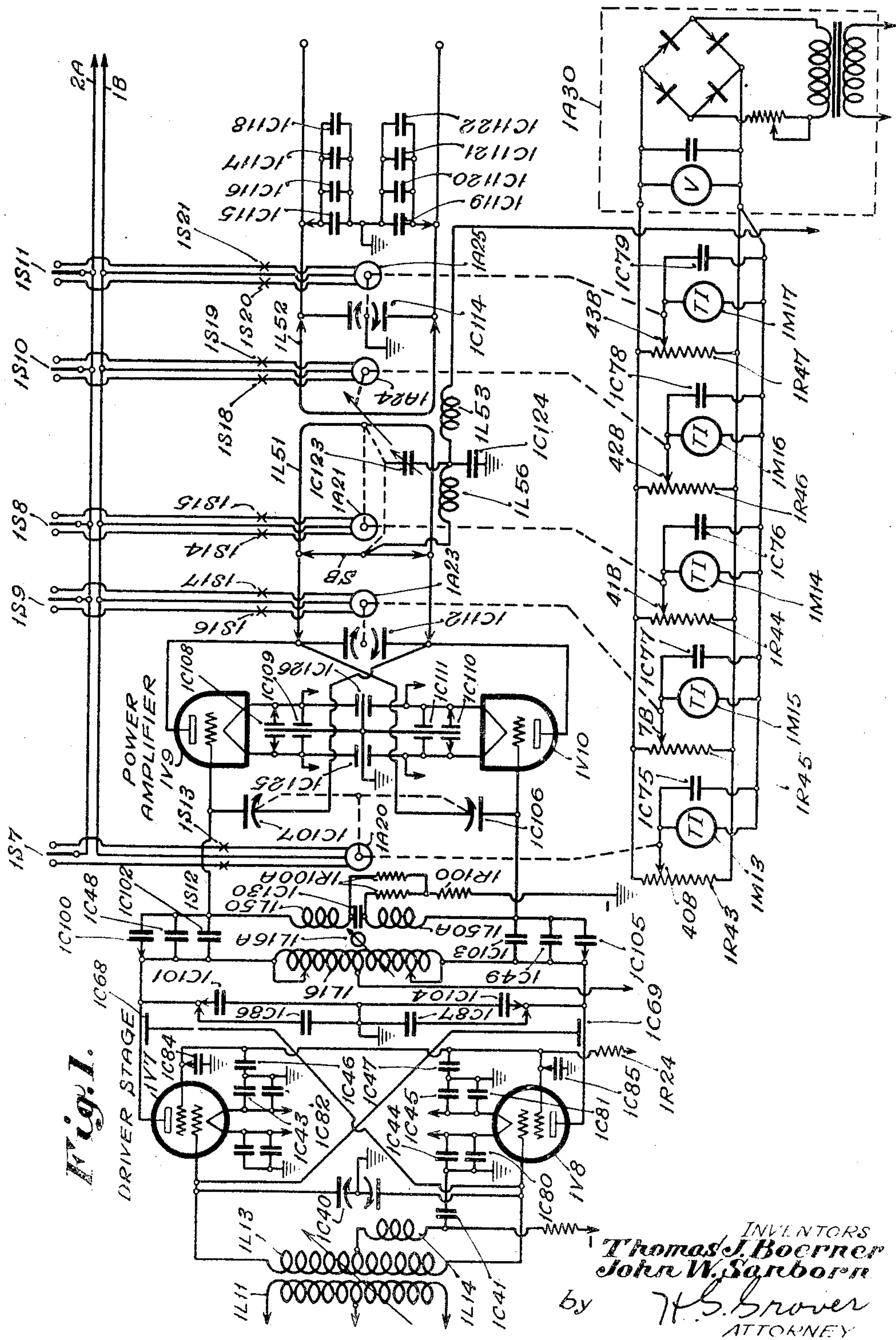
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T. J. BOERNER ET AL

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HIGH-FREQUENCY APPARATUS

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INVENTORS
Thomas J. Boerner
John W. Sarborn
by H. S. Brover
ATTORNEY

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HIGH-FREQUENCY APPARATUS

Thomas James Boerner, Collingswood, and John W. Sanborn, Merchantville, N. J., assignors to Radio Corporation of America, a corporation of Delaware

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1

This is a division of our copending application Serial No. 491,164, filed June 17, 1943, now Patent No. 2,412,314 issued December 10, 1946, and describes an invention which relates to high frequency apparatus and especially to the power amplifier stages of high frequency transmitters.

One object of the invention is to provide improved high frequency vacuum tube power amplifying apparatus and circuits which shall operate at high efficiency and in which spurious effects such as parasitic oscillations are minimized. A further object of our invention is to provide high frequency amplifying apparatus wherein the frequency of operation may readily and conveniently be changed.

In brief, certain features of the present invention may be outlined as follows:

A push-pull connected vacuum tube driver stage is coupled through a condenser-divider arrangement to a push-pull connected vacuum tube power amplifier. The condenser-divider operates in such a way that over a wide range of operating frequencies substantially constant radio frequency excitation is applied to the grids of the power amplifier with constant direct current voltage impressed upon the plates of the driver tubes. In this connection it may also be mentioned that biasing circuits are provided for the grids of the power amplifier tubes which operate so as to secure flow of equal grid currents over a wide operating range.

Reversible electric motors are provided for adjusting neutralizing and tuning condensers of the power amplifier stage and output circuit. Further instrumentalities under control of other reversible electric motors are provided for adjusting other circuits, etc., as will be explained more fully later. Limit switches are provided for the motors so as to prevent them from over-running in either direction. Instrumentalities are also provided whereby each reversible electric motor drives the variable arm of a potentiometer. Each potentiometer supplies voltage to a separate tuning indicator which may be in the form of a volt meter. In this way the tuning indicators give a measure, by the respective volt meter readings, of the capacity in circuit and in other cases the amount of coupling or the amount of inductance in the power amplifier tank circuit.

The drawing is a wiring diagram of a push-pull connected driver-amplifier stage feeding through a condenser-divider arrangement the grids of a pair of push-pull connected vacuum tube amplifiers of a high frequency power amplifier. As illustrated, reversible electric motors

2

are provided for varying neutralizing and tuning condensers, the inductance of the tank circuit, and the coupling between the tank circuit of the power amplifier and the final output circuit to which the tank circuit is coupled.

Referring to the drawing, any carrier frequency within a range of, say, for example, 6 to 22 megacycles is fed into the primary coil $1L1$ and thence into the secondary $1L3$, exciting the control grids of tubes $1V7$ and $1V8$ in phase opposition. The carrier may be generated by any suitable vacuum tube generator followed by amplifiers and frequency multipliers. The secondary $1L3$ is tuned by the split stator condenser $1C40$. The amplified output of the driver stage consisting of tubes $1V7$ and $1V8$ appears in the tuned output circuit comprising coil $1L16$ and condensers $1C101$, $1C86$, $1C87$ and $1C104$. The condensers are switched into the circuit as needed, depending upon the frequency employed.

In order to prevent spurious oscillations, the screen grids of the driver tubes $1V7$ and $1V8$ are by-passed to ground by condensers $1C46$ and $1C47$. For a range of lower frequencies, additional by-passing condensers $1C84$ and $1C85$ are also switched into the circuit, but are switched out of circuit in the range of higher frequencies. That is to say, condensers $1C47$ and $1C46$ will serve to give sufficient by-passing to ground at the higher frequencies since these condensers may be constructed integrally with the screen grid connections to the tubes.

Over the entire range of frequencies, however, neutralizing condensers $1C68$ and $1C69$, which may consist of sections of copper strap adjacent the anodes, are also employed. That is, these neutralizing condensers are employed in addition to the screen grids and their by-passing circuits to ground, over the entire operating range of frequencies. The use of such neutralizing circuits in addition to the screening circuits insures freedom from spurious oscillations and similar effects.

Coupling from the driver stage, including tubes $1V7$ and $1V8$, to the final power amplifier stage comprising water cooled tubes $1V9$ and $1V10$, is accomplished through capacitors $1C100$, $1C48$, $1C102$, $1C103$, $1C49$ and $1C105$.

The condensers $1C100$, $1C48$ and $1C102$ are equal in value, respectively, to condensers $1C103$, $1C49$ and $1C105$. The values of the upper three capacitors in parallel and the lower three are therefore equal; or, they may be used singly or in pairs so that the coupling capacities on both sides of the plate coil $1L16$ are equal. In this

way, proper voltage will be applied to the grids of the final power amplifier tubes for different operating conditions.

From the foregoing, it will be observed that the input capacity of the power amplifier tubes IV9 and IV10 form the low voltage legs of a condenser divider. Hence, as long as the radio frequency plate voltage of the driver stage is held constant, the condenser divider serves to maintain a correspondingly constant excitation voltage to the power amplifier across the power tubes of IV9 and IV10 over a very wide frequency range.

By virtue of the condenser divider tuning of the driver output stage can be adjusted over the entire frequency range without affecting the ratio of driver plate to power amplifier grid radio frequency voltage. Actually some fixed adjustment of the coupling capacitors of the voltage divider arrangement may be required. We have found that the entire range from six to twenty-two megacycles can be covered with three combinations of the condensers in the voltage divider with wide non-critical points of overlap. Further adjustment in the circuits may be made by means of the taps on coil IL16 and by changing the position and coupling of a short-circuited turn IL16A with respect to the turns of coil IL16.

The grids of the power amplifier tubes are subjected to biasing action through the action of a common resistor IR100 and the further resistors IR100A. As indicated, one of the latter is connected in series with the grid of tube IV9 and the other in series with the grid of the other tube IV10 of the power amplifier. Also, it will be noted that chokes IL50 and IL50A and radio frequency by-pass condenser IC130 have been provided in the grid circuit of the power amplifier stage. The grid circuit as described provides balanced grid currents over the entire range of frequencies employed.

Neutralizing condensers IC107 and IC106, which will be described in greater detail hereinafter, are provided for the power amplifier tubes IV9 and IV10. Also, as will be described more fully hereinafter, the tank circuit of the power amplifier comprises the inductance IL51, tuning condenser IC112, short-circuiting strap SB, condenser IC123, by-passing condenser IC124 and choke IL56.

The loading or output circuit, which also will be described more fully hereinafter, comprises the inductor IL52, tuning condenser IC114 and fixed condensers IC115 to IC1122 inclusive.

Motor-driven adjustment or tuning of various elements in the power amplifier stage and output circuit are provided. Thus, reversible electric motor IA20 drives neutralizing condensers IC106 and IC107. Direction of rotation is controlled by switch IS7. Limiting switches, diagrammatically indicated at IS12 and IS13, limit the amount of rotation of the motor in either direction. The angular position of motor IA20 is indicated on a tuning indicator IM13 which is in effect a voltmeter, the voltage of which depends upon the position of tap 40B upon potentiometer IR43. The tap 40B is moved along the potentiometer IR43 by the action of motor IA20. In other words, motor IA20 simultaneously varies condensers IC106 and IC107 and the position of tap 40B along potentiometer IR43.

Similarly, reversible driving motors IA23, IA21, IA24 and IA25, switches IS9, IS8, IS10, and IS11, limiting switches IS16, IS17, IS14, IS15, IS18, IS19, IS20 and IS21, and indicators IM15,

IM14, IM16 and IM17 are provided for adjusting and indicating the adjustment of condensers IC112, coupling between inductors IL51 and IL52 and condenser IC114. Supply voltage for the tuning indicating system is derived from the rectifier arrangement IA30. Motor driving power is furnished through leads IB and 2A. The power supply to these leads may be, for example, 220 volts 60 cycles A. C. current.

The limit switches, such as IS12 and IS13, may be operated by cams, in turn operated or driven by reduction gearing coupled to the motor IA20, so that after a given number of revolutions in one direction, limit switch IS12 will be opened and after a given number of revolutions in the other direction limit switch IS13 will be opened. Similarly, the potentiometer and tap arrangement IR43 and 40B may be controlled by reduction gearing also coupled to the motor IA20, the tap being in contact with and moved over a circularly shaped potentiometer winding. Similar comments are applicable to the other limit switches and potentiometers controlling the tuning indicators TI. The latter are provided with by-passing condensers IC75 to IC79 inclusive.

Having thus described our invention, what we claim is:

1. A control system for high frequency apparatus having a push-pull connected vacuum tube power amplifier, comprising a variable condenser arrangement including at least two variable condensers, each one of said condensers connected to the respective vacuum tubes of said amplifier, a reversible electric motor, switching apparatus for controlling the direction of rotation of said motor in either direction, and mechanical linkage between the armature of said motor to a variable element on each one of said variable condensers, whereby movement of said motor simultaneously varies each condenser capacity.

2. A control system for high frequency apparatus, comprising a plurality of variable condenser and inductor impedance elements connected to said high frequency apparatus, a plurality of reversible electric motors there being a motor individual to each condenser and inductor element, switching apparatus for controlling the direction and the amount of rotation of each one of said motors, and mechanical linkage between said motors and the respective condensers and inductors, whereby the movement of said motors varies the reactance of the impedance element linked thereto.

3. A motor control system including a push-pull connected vacuum tube amplifier, comprising a variable condenser arrangement including at least two variable condensers, each one of said condensers being connected to the respective vacuum tubes of said amplifier, a source of voltage, a reversible electric motor, a potentiometer, a meter, connections from said source of voltage to said potentiometer, a movable tap on said potentiometer, said meter being connected to one side of said potentiometer and its movable tap, switching apparatus for controlling the direction of rotation of said motor and mechanical linkage between the armature of said motor and each one of said variable condensers and also said movable tap, whereby the movement of said motor varies the values of said condensers and simultaneously the position of said tap, and the meter indicates the angular position of said motor.

4. A control system for high frequency appa-

5

ratus having a plurality of variable condensers and inductors connected to said high frequency apparatus, comprising a source of voltage, a plurality of electric motors, there being a motor controlling each condenser and a motor controlling each inductor, a plurality of meters, a plurality of potentiometers each having a movable tap, each one of said potentiometers being connected across said source of voltage, each one of said meters being connected to one side of each potentiometer and its movable tap, there being a potentiometer associated with each condenser and with each inductor, a link between the tap on each potentiometer and its associated motor, switching apparatus for controlling the direction and the amount of rotation of each one of said motors, whereby the movement of any motor varies the reactance of the condenser or inductor linked thereto and simultaneously causes the meter associated with its respective potentiometer to measure the change in said reactance.

5. A control system for high frequency apparatus having a plurality of variable condensers and an inductor connected to said high frequency apparatus comprising a source of voltage, a movable short-circuiting strap across a portion of said inductor, a plurality of electric motors, a plurality of meters, a potentiometer individual to each condenser and to said inductor, each potentiometer having a movable tap, said potentiometers being connected across said source of voltage, each one of said meters being connected to one side of each potentiometer and its movable tap, switching apparatus for controlling the direction of the amount of rotation of each one of said motors, and mechanical coupling apparatus coupling said motors respectively to different condensers and to said short-circuiting strap, and linkage between each motor and the movable tap

6

on its associated potentiometer, whereby the movement of one of said motors varies the capacity of a condenser and another motor moves said short-circuiting strap simultaneously, and the meters indicate the degree of movement of said motors.

6. A control system for high frequency apparatus including vacuum tube amplifiers connected in push-pull relationship comprising two vacuum tubes each having at least an anode, a grid and a cathode, two neutralizing condensers each in circuit connection between the anode of one tube and the grid of another tube, a source of voltage, a reversible electric motor linked to both neutralizing condensers for simultaneously varying the same, a potentiometer connected in shunt with said source of voltage, a variable tap for said potentiometer, said variable tap being linked to said motor, and a meter in shunt with said potentiometer.

THOMAS JAMES BOERNER.
JOHN W. SANBORN.

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