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(54) AEROFOIL COOLING ARRANGEMENT

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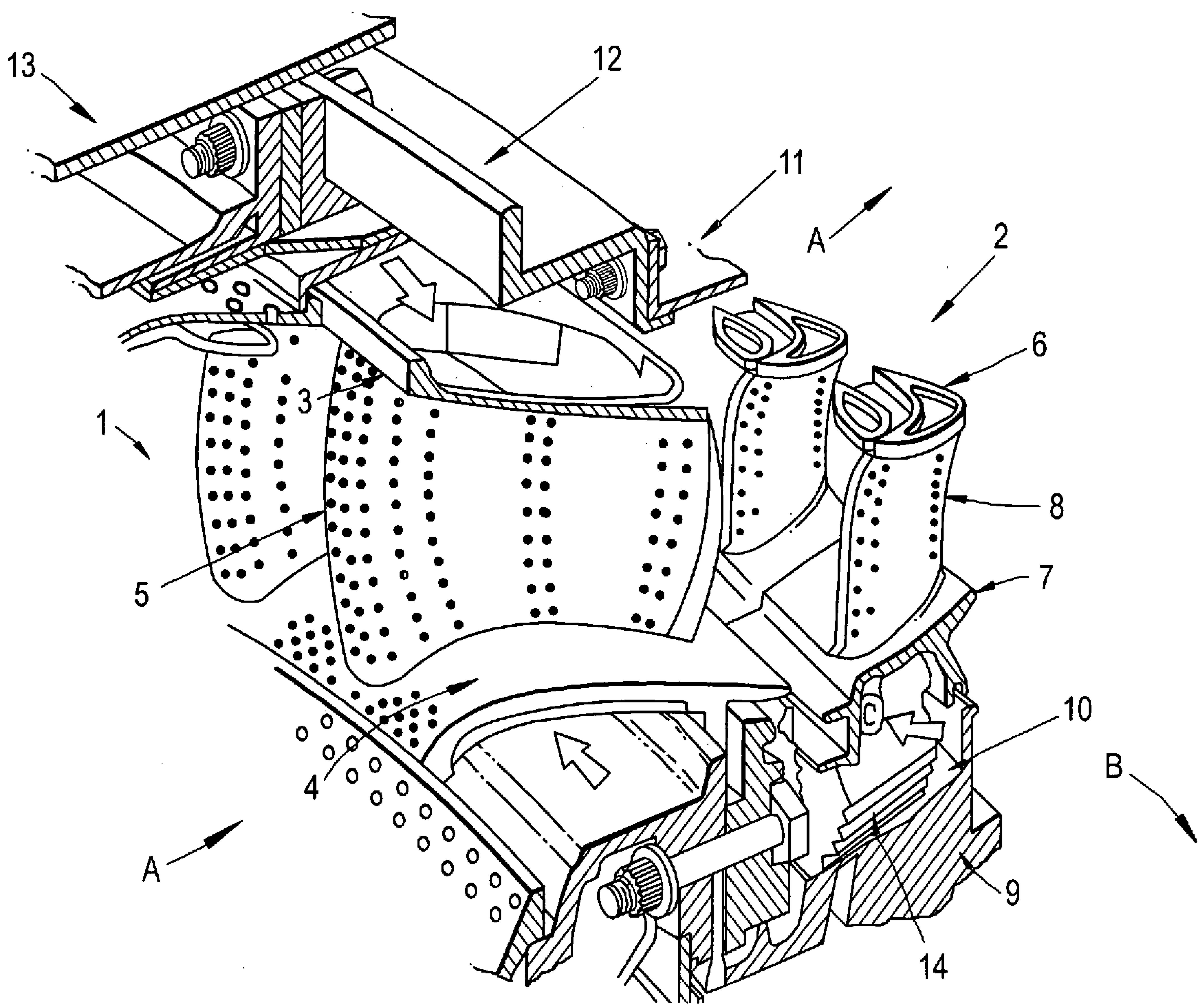
(57) ABSTRACT

Within aerofoils (**50**, **150**, **250**, **350**), and in particular nozzle guide vane aerofoils in gas turbine engines problems can occur with regard to coolant flows (**56**, **57**; **156**, **157**; **256**, **257**; **356**, **357**) from respective inlets at opposite ends of a cavity (**60**, **160**, **260**, **360**) within the aerofoil (**50**, **150**, **250**, **350**). The cavity (**60**, **160**, **260**, **360**) generally defines a hollow core and unless care is taken coolant flow can pass directly across the internal cavity. Previously baffle plates were inserted within the cavity to prevent such direct jetting across the cavity. Such baffle plates are subject to additional costs as well as potential unreliability problems. Baffles (**55**, **155**, **255**, **355**) formed integrally with a wall (**54**, **154**, **254**, **35**) within the aerofoil (**50**, **150**, **250**, **350**) allow more reliability with regard to positioning as well as consistency of performance. The baffles (**55**, **155**, **255**, **355**) can be perpendicular, upward or downwardly orientated or have a compound angle.



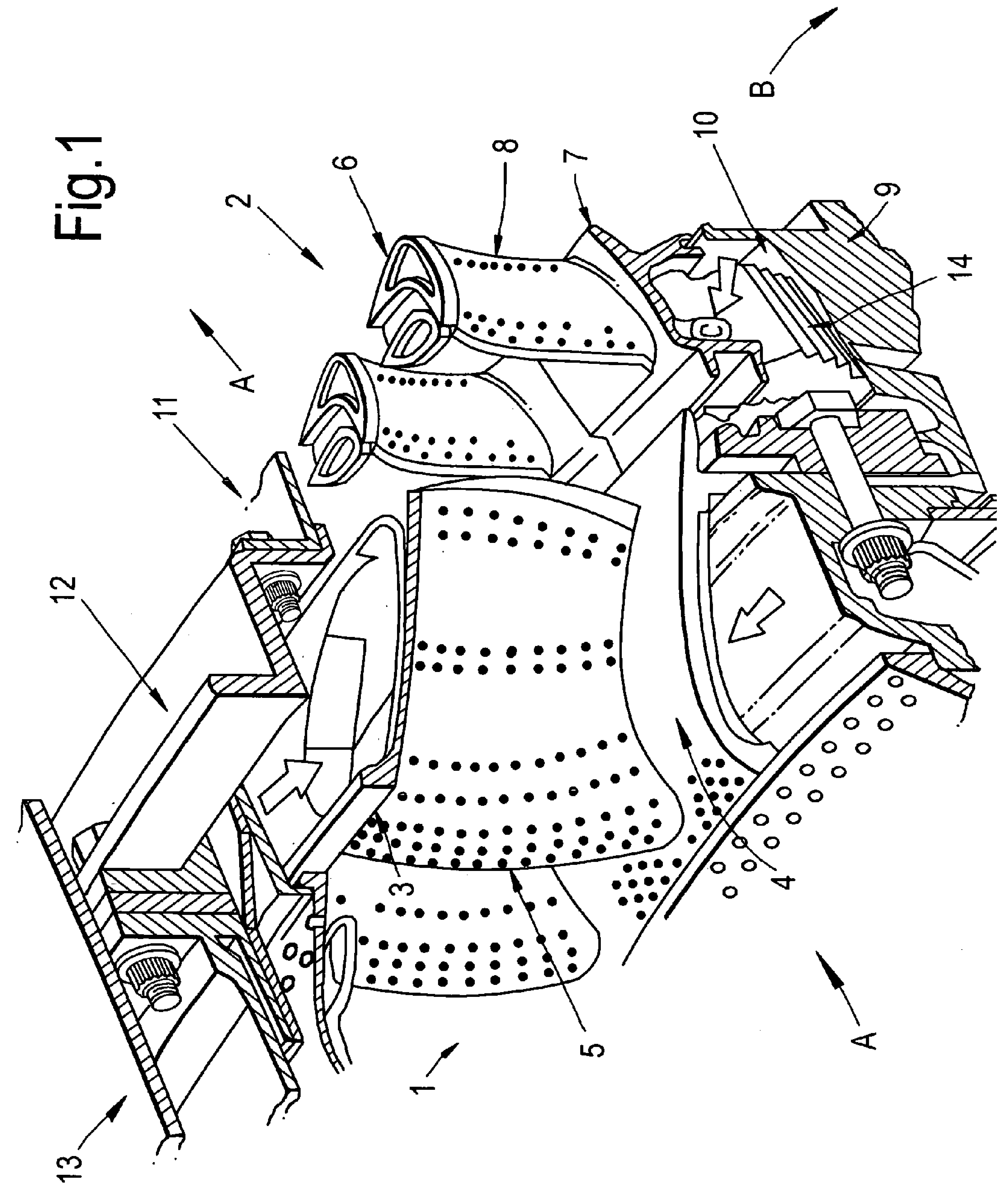
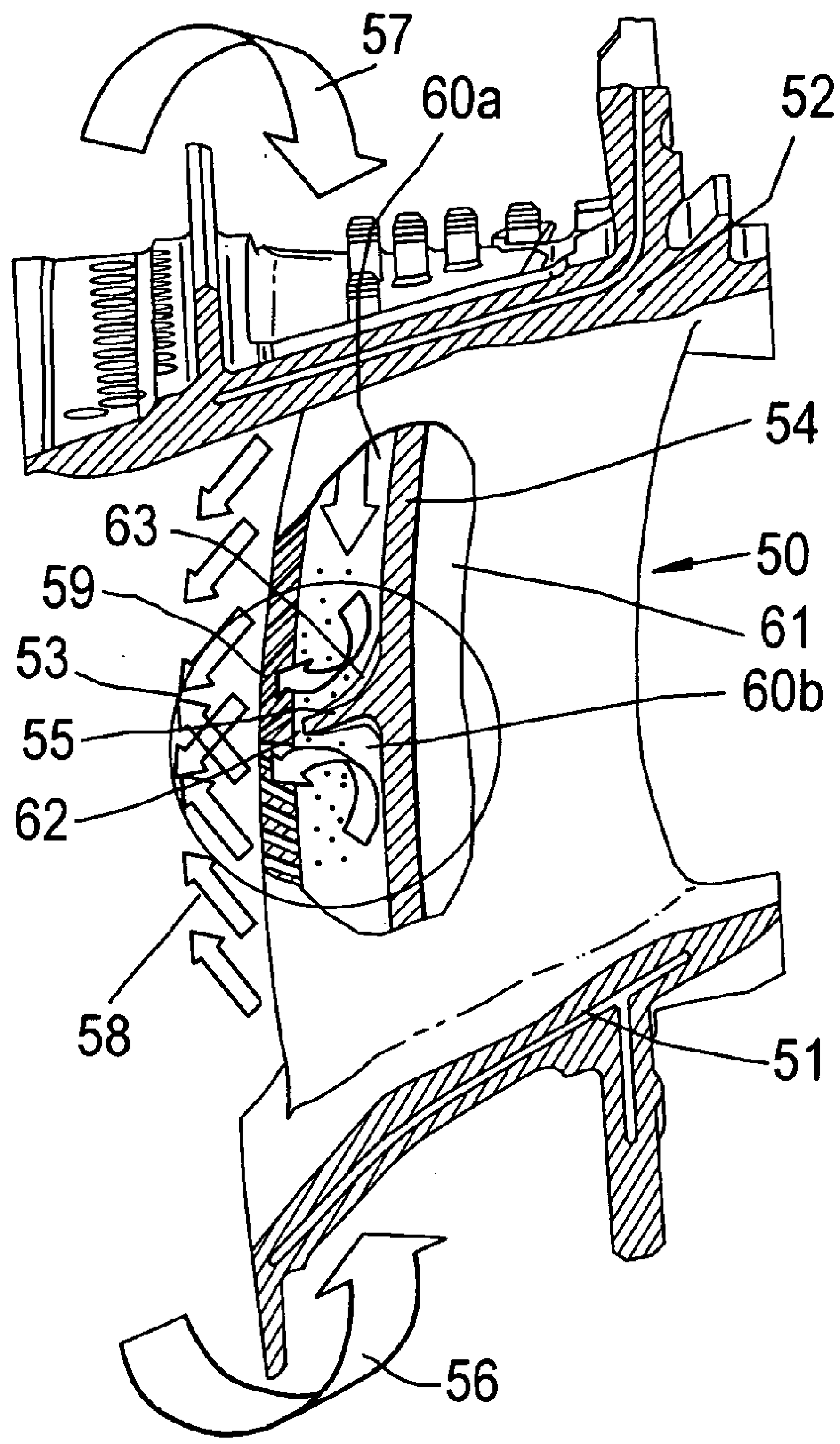


Fig.1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60a
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Fig.2

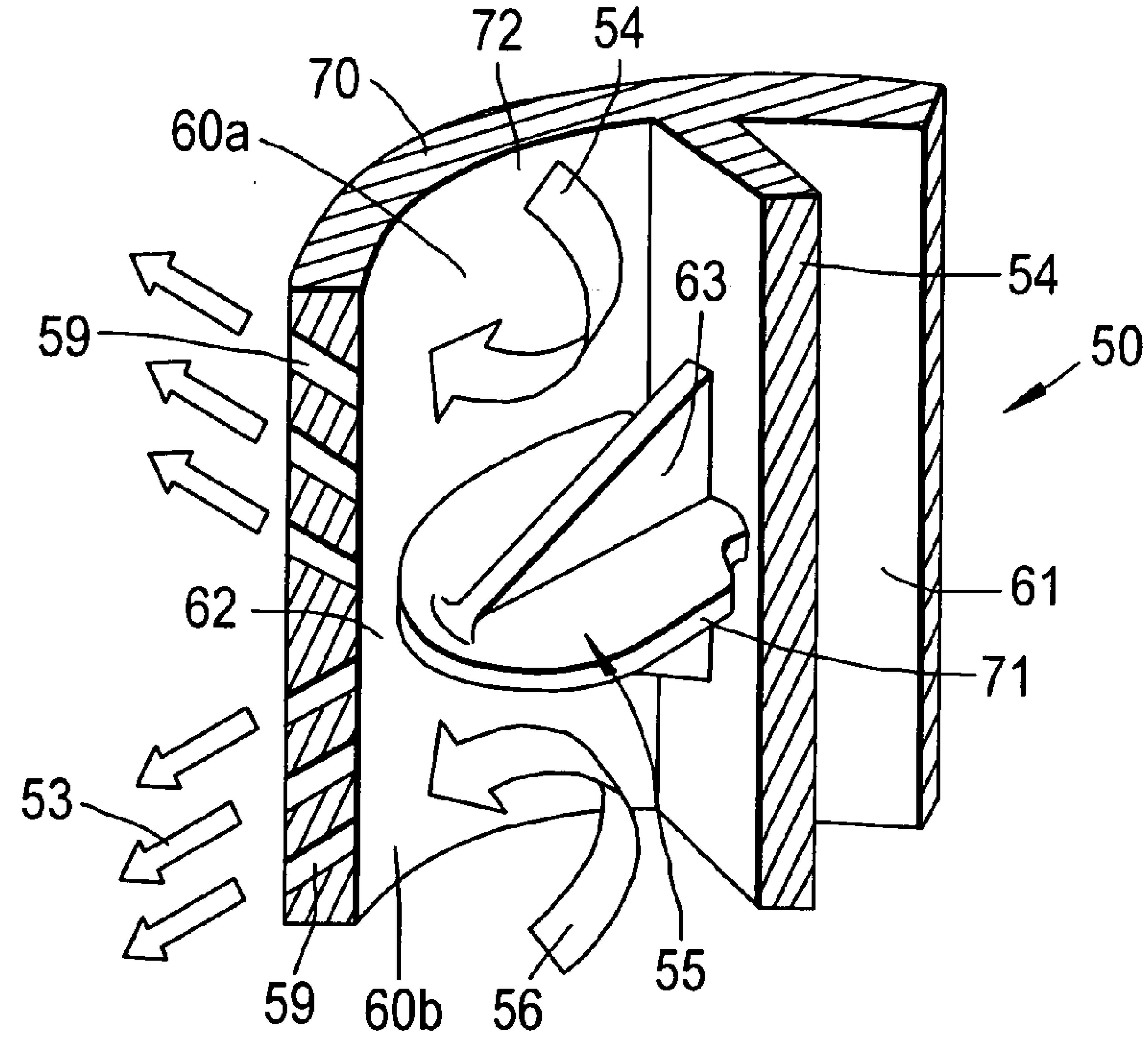
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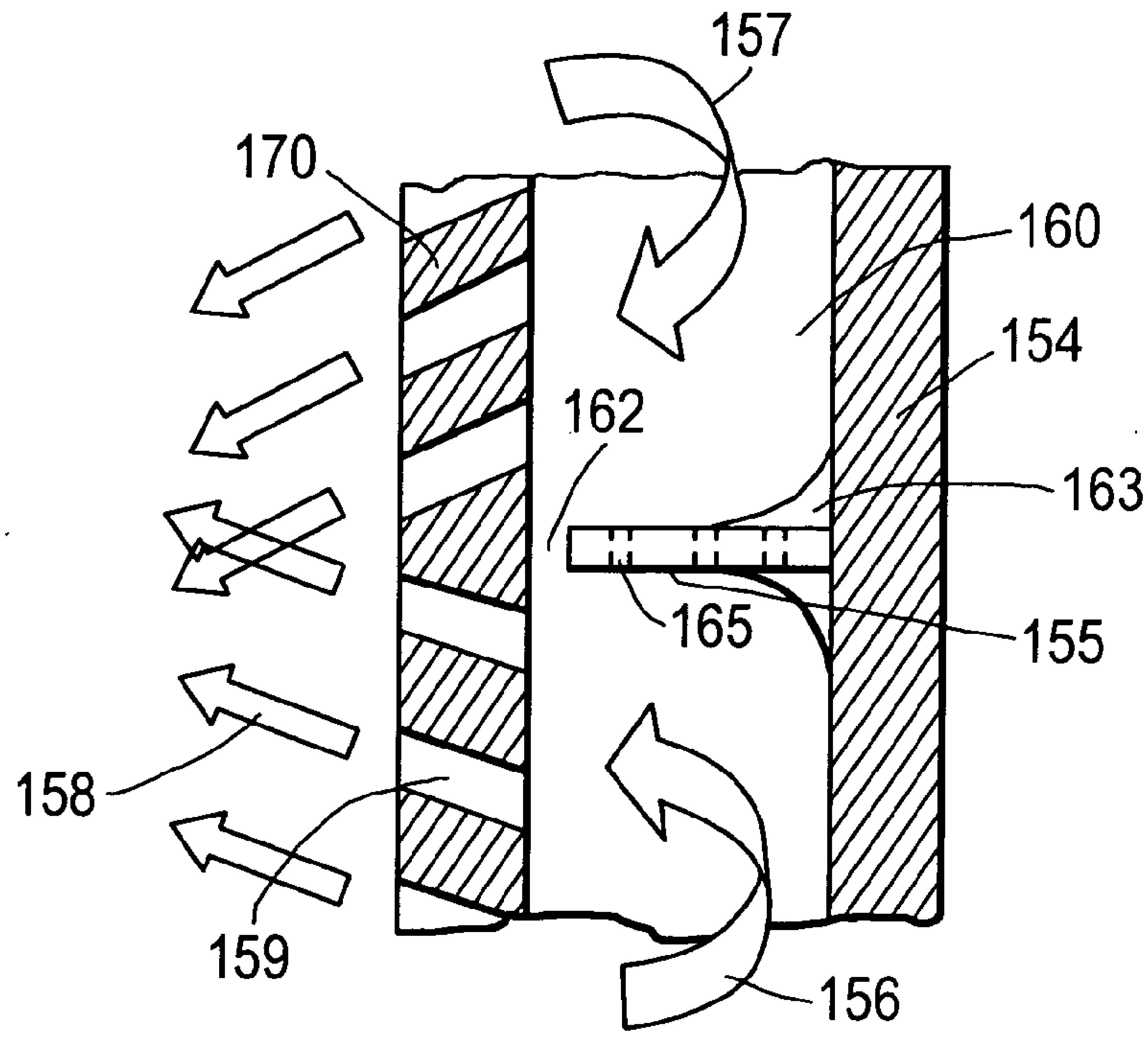
Fig.3

Fig.4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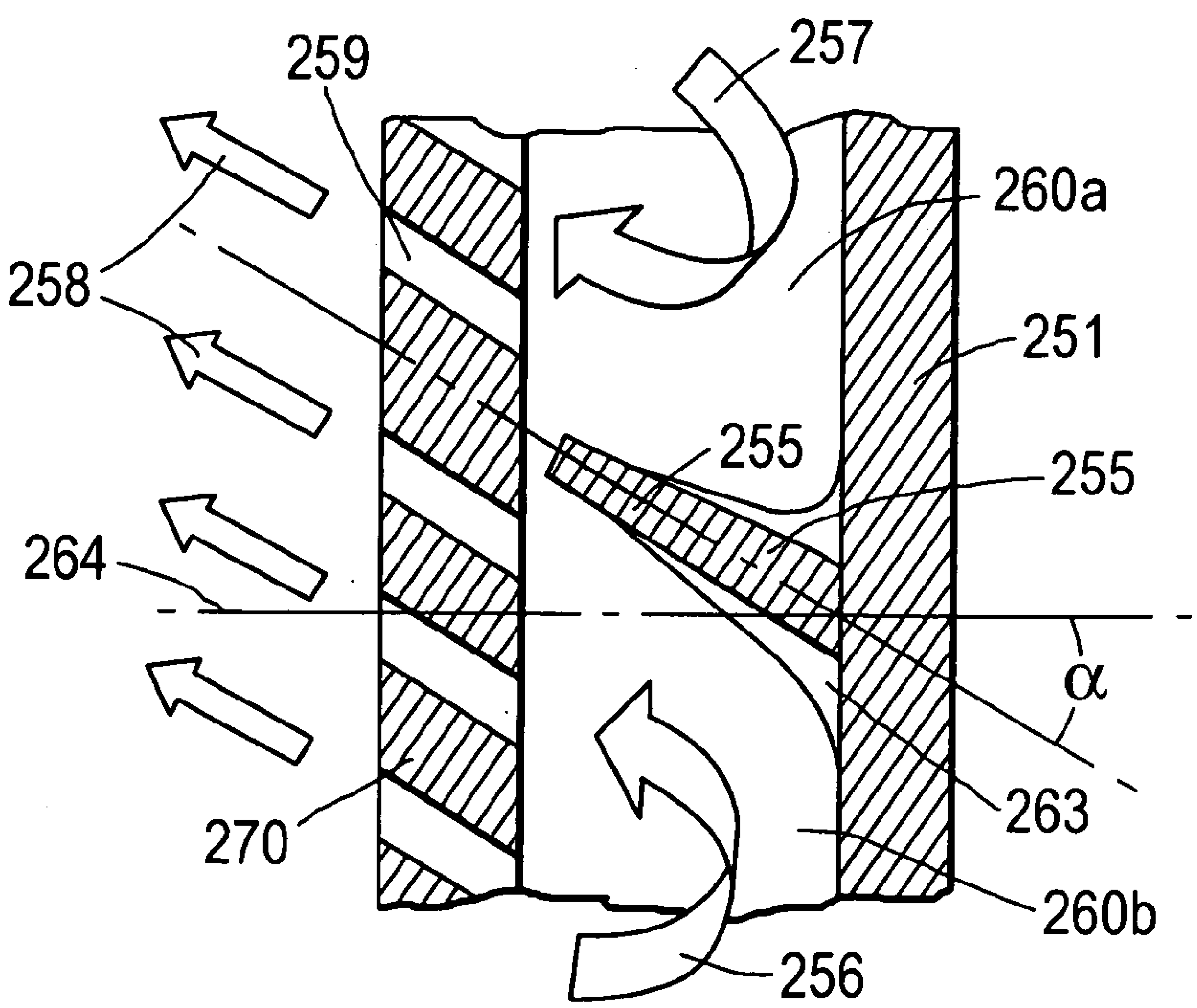
156

Fig.5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260a
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251
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255
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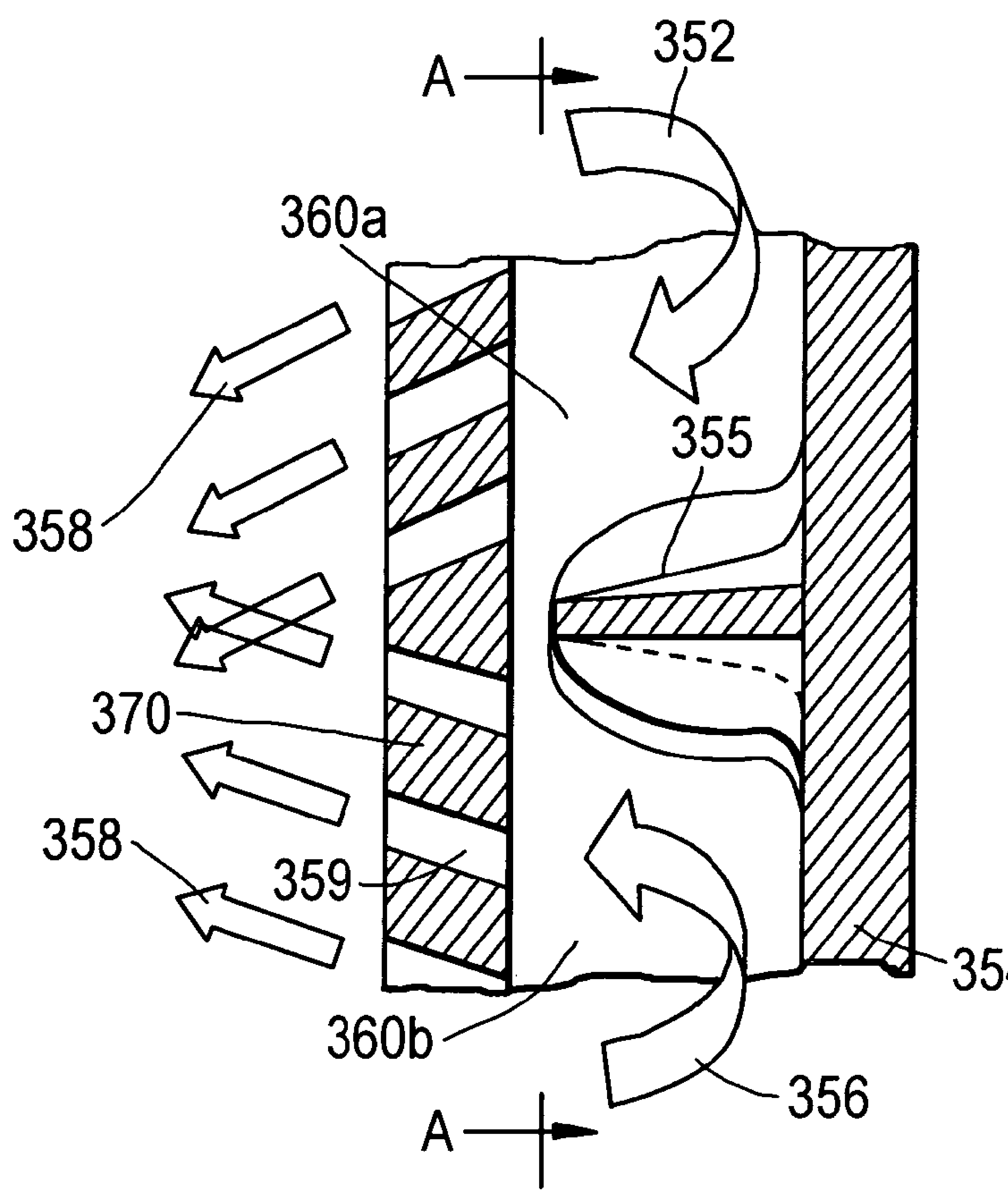
α
270
263
260b
256

Fig.6


A
352
360a
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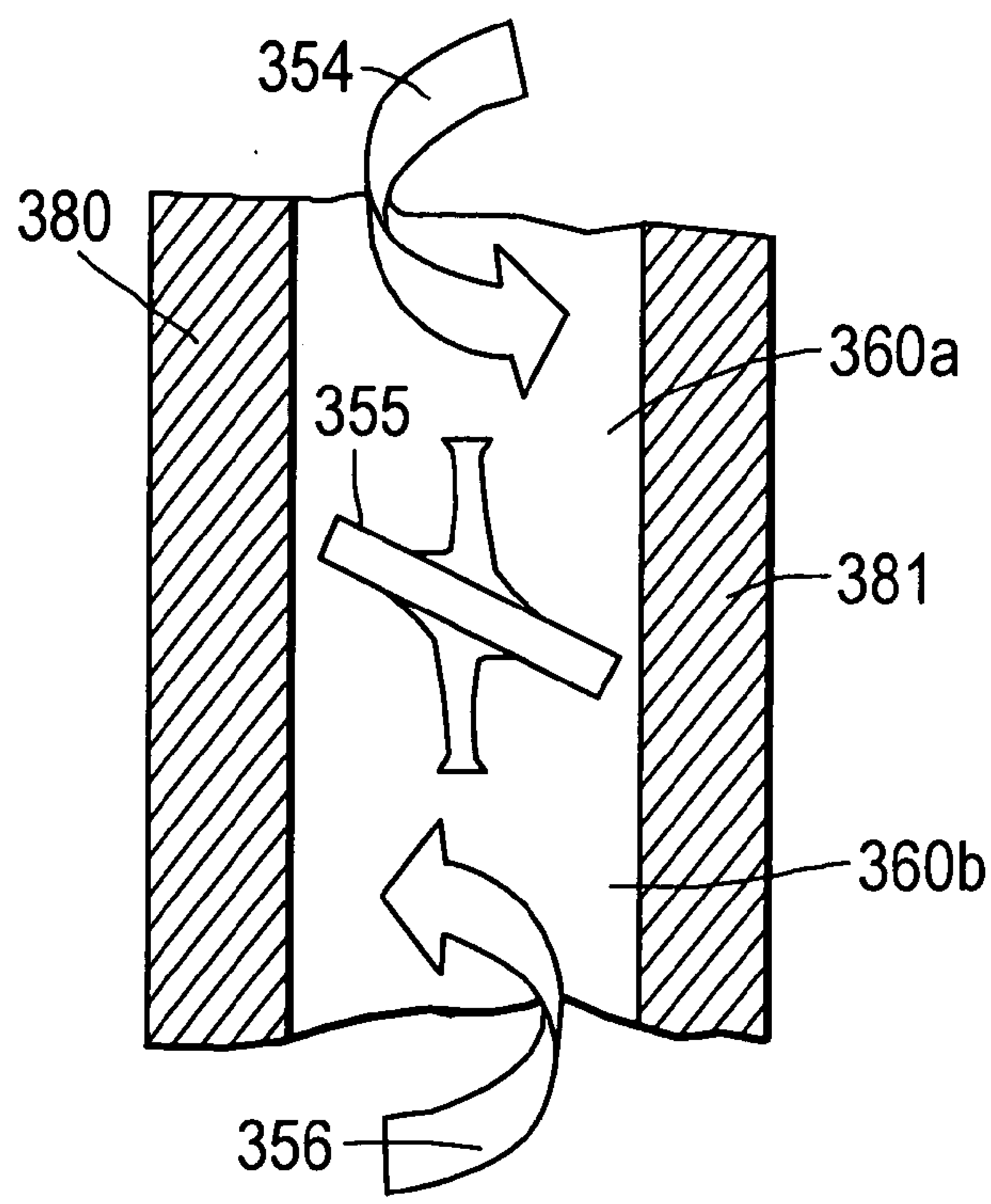
370
358
359
354
360b
356
A

Fig.7


354
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360a
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381
360b
356

Fig.8

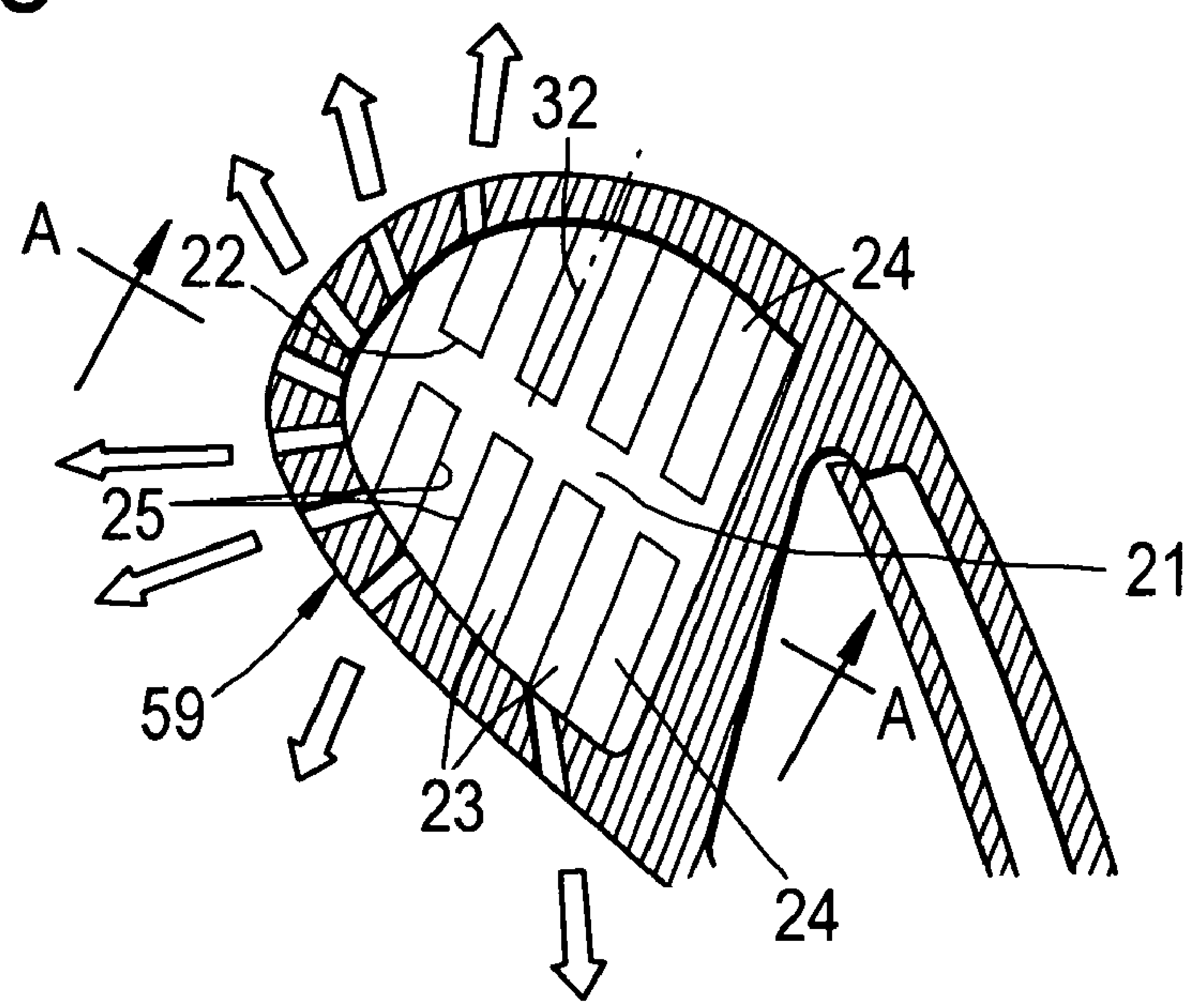


Fig.9

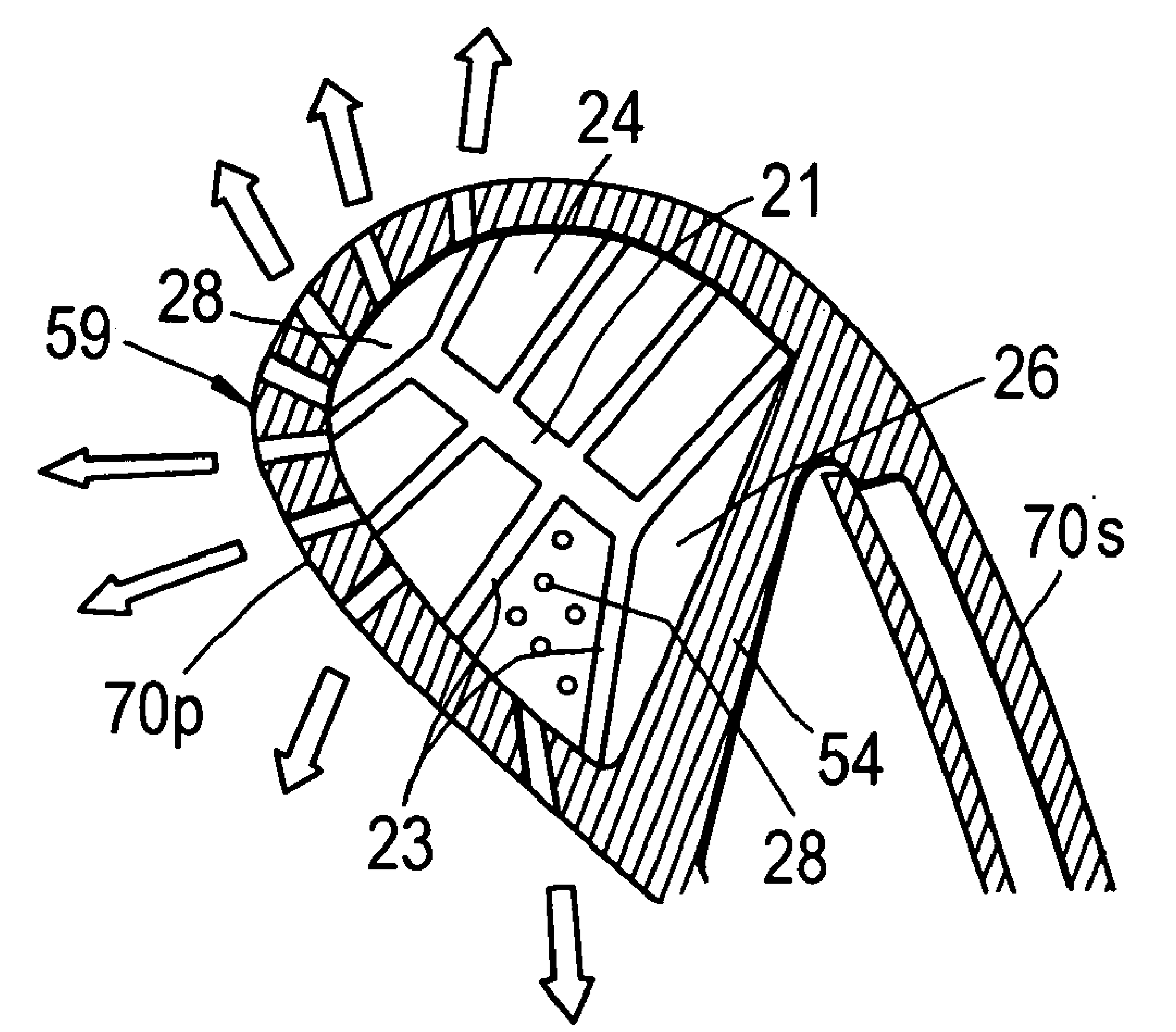
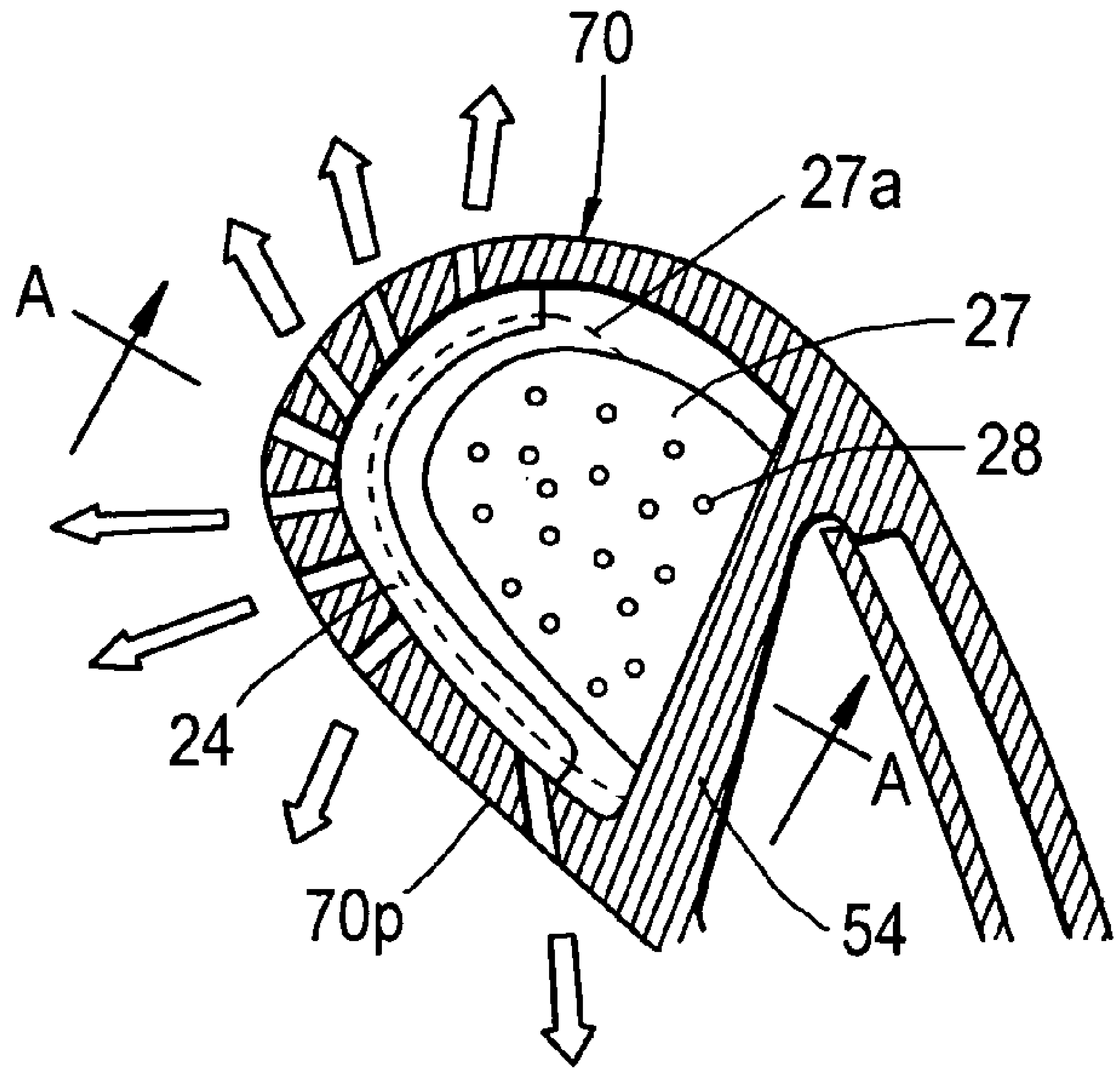


Fig.10



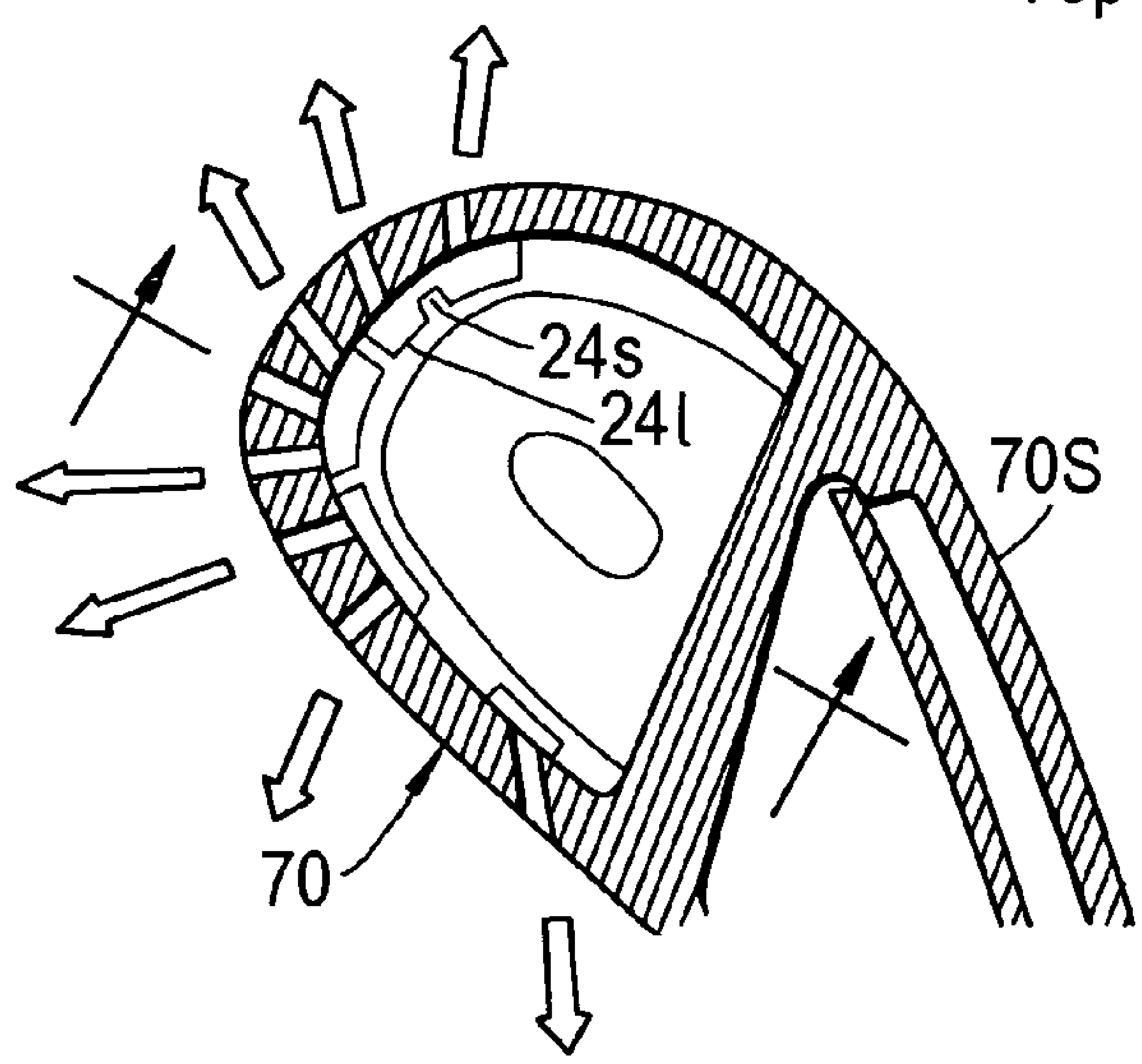


Fig.11

Fig.12

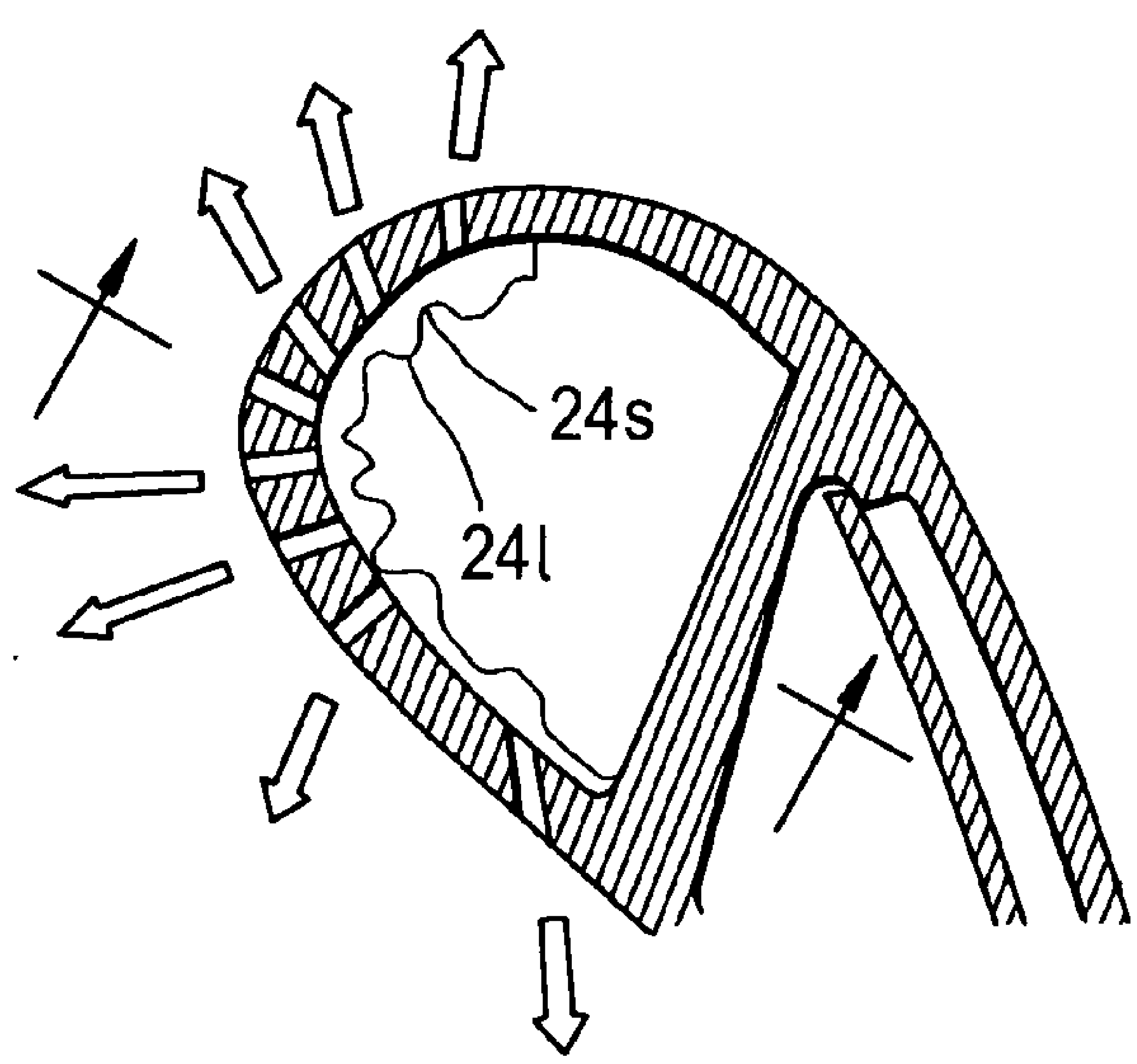


Fig.13

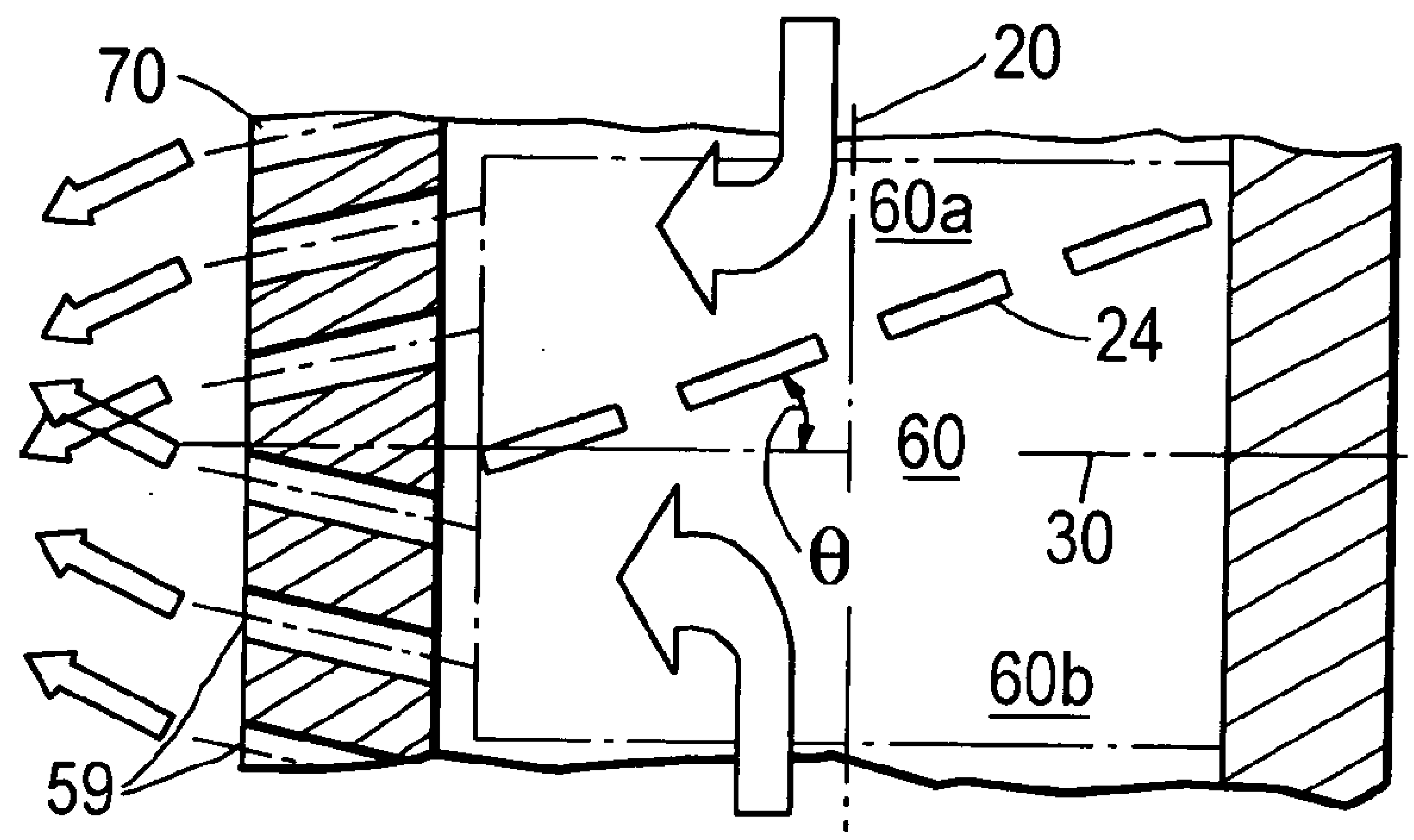


Fig.14

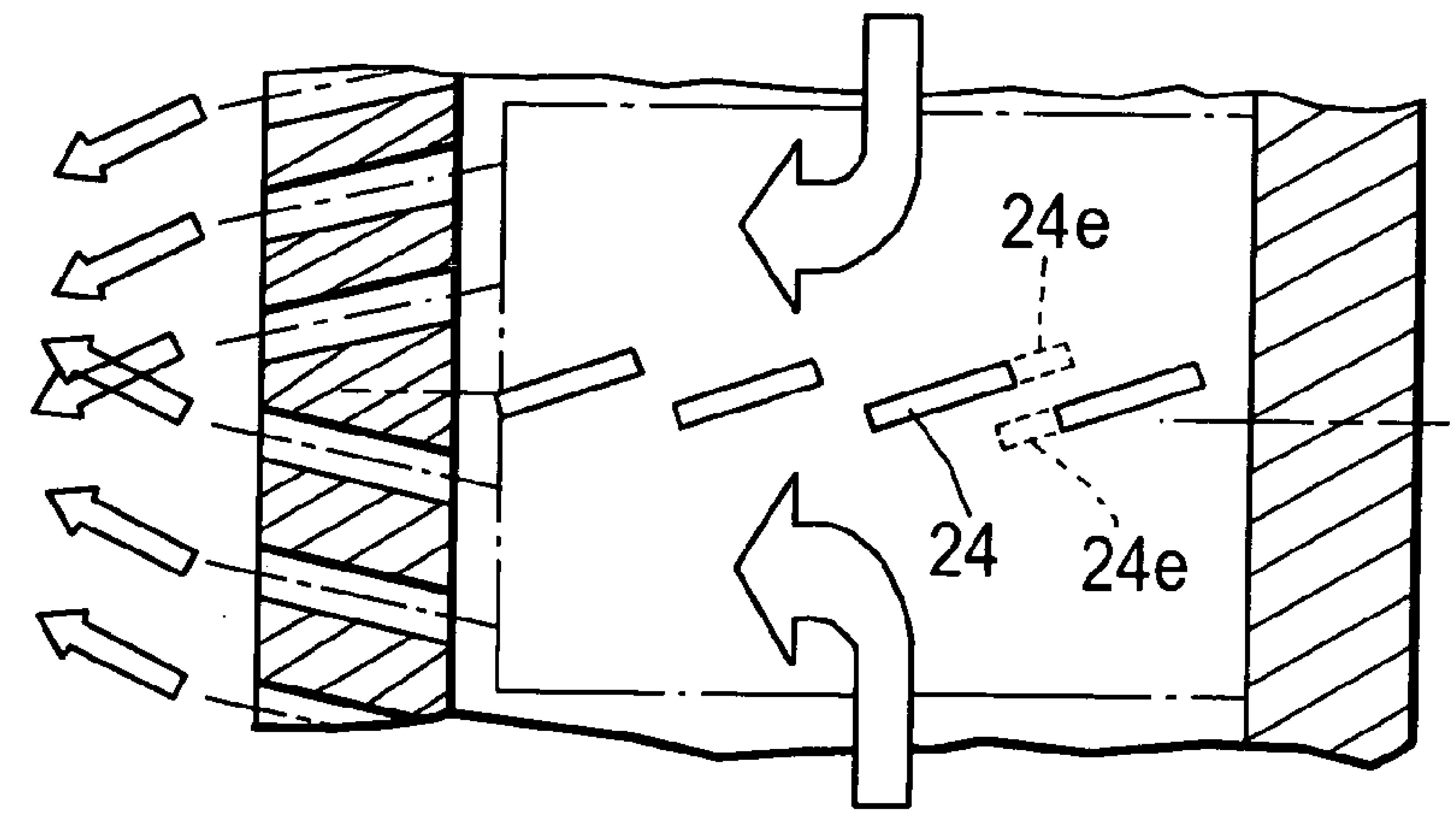
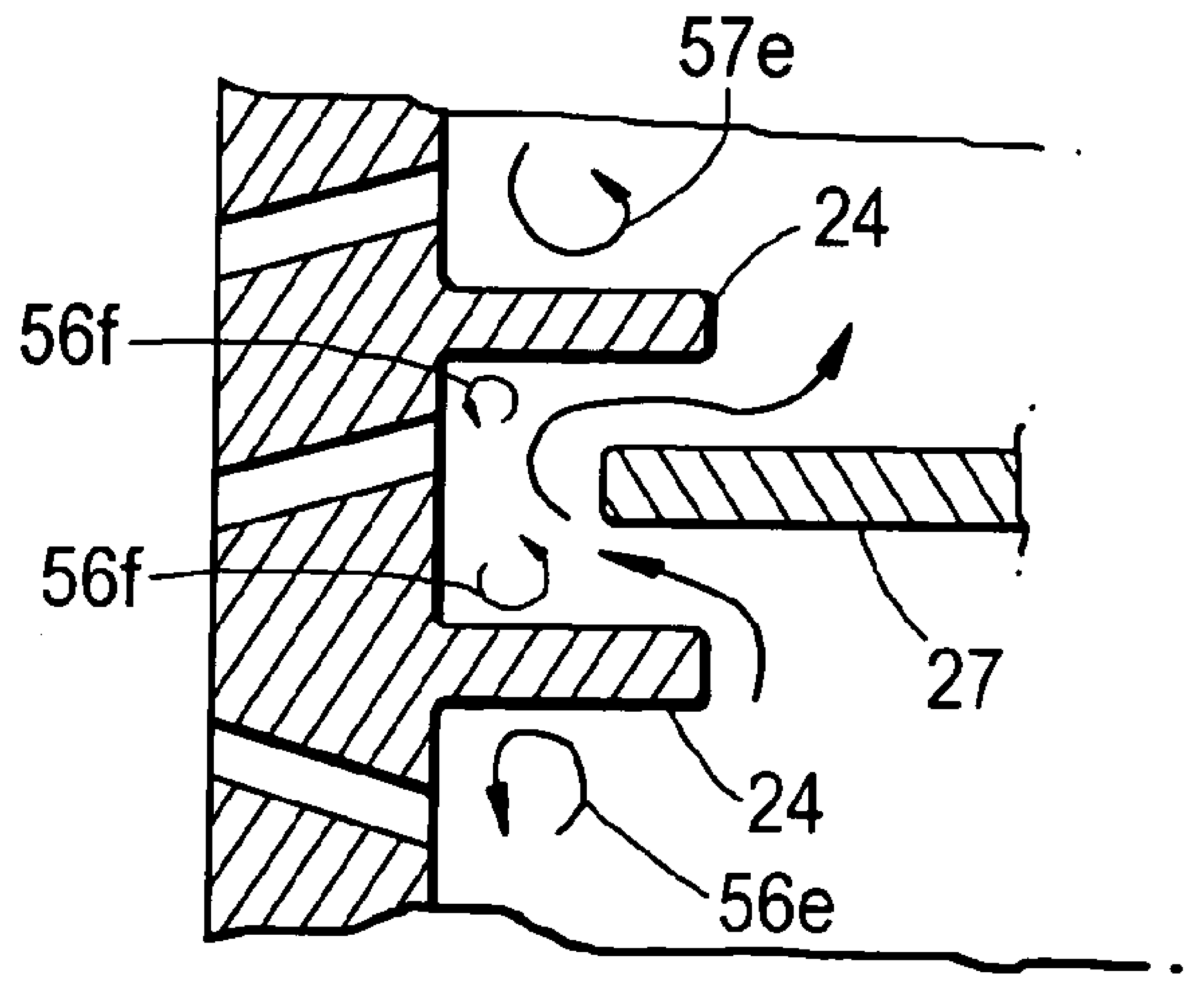


Fig.19



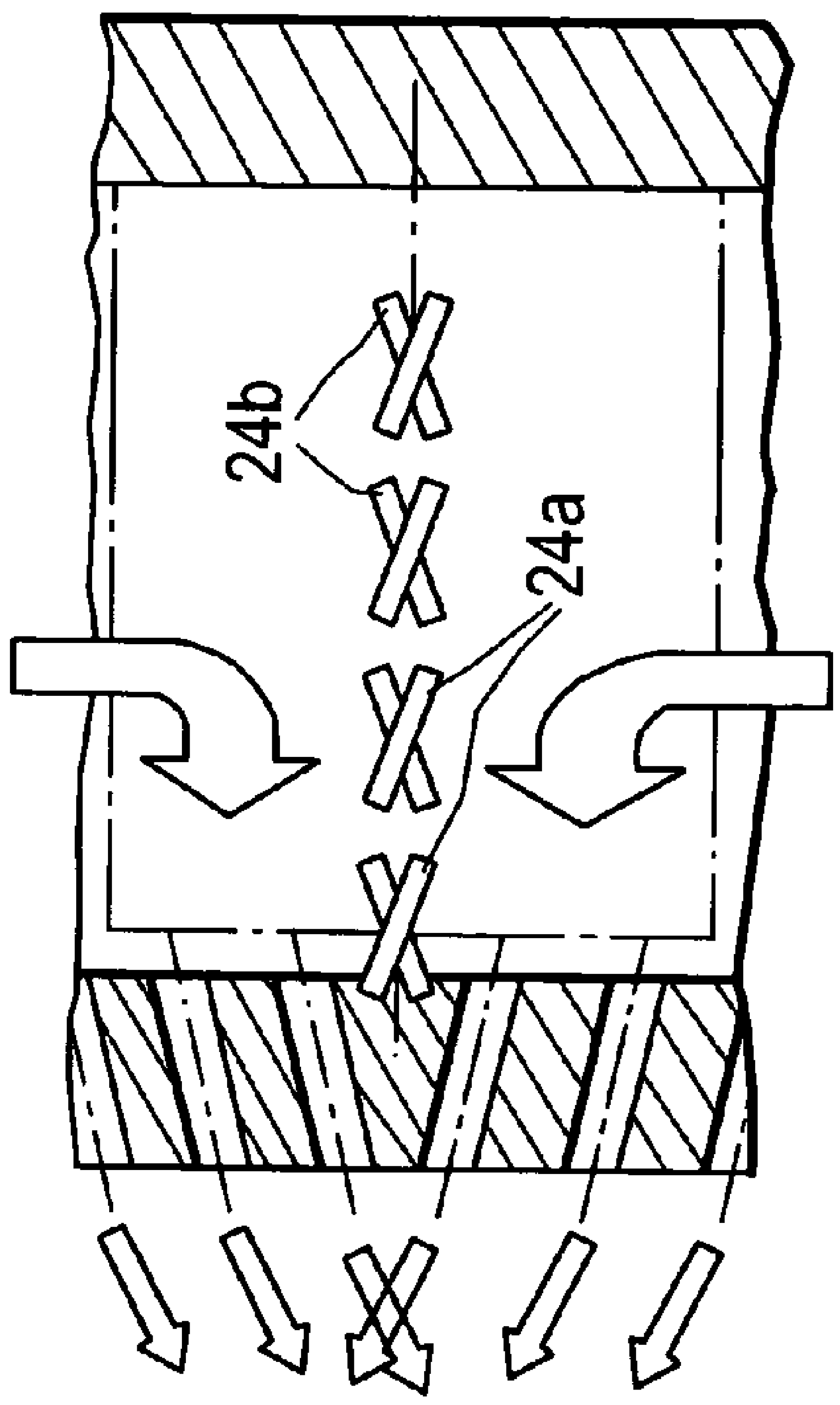


Fig.17

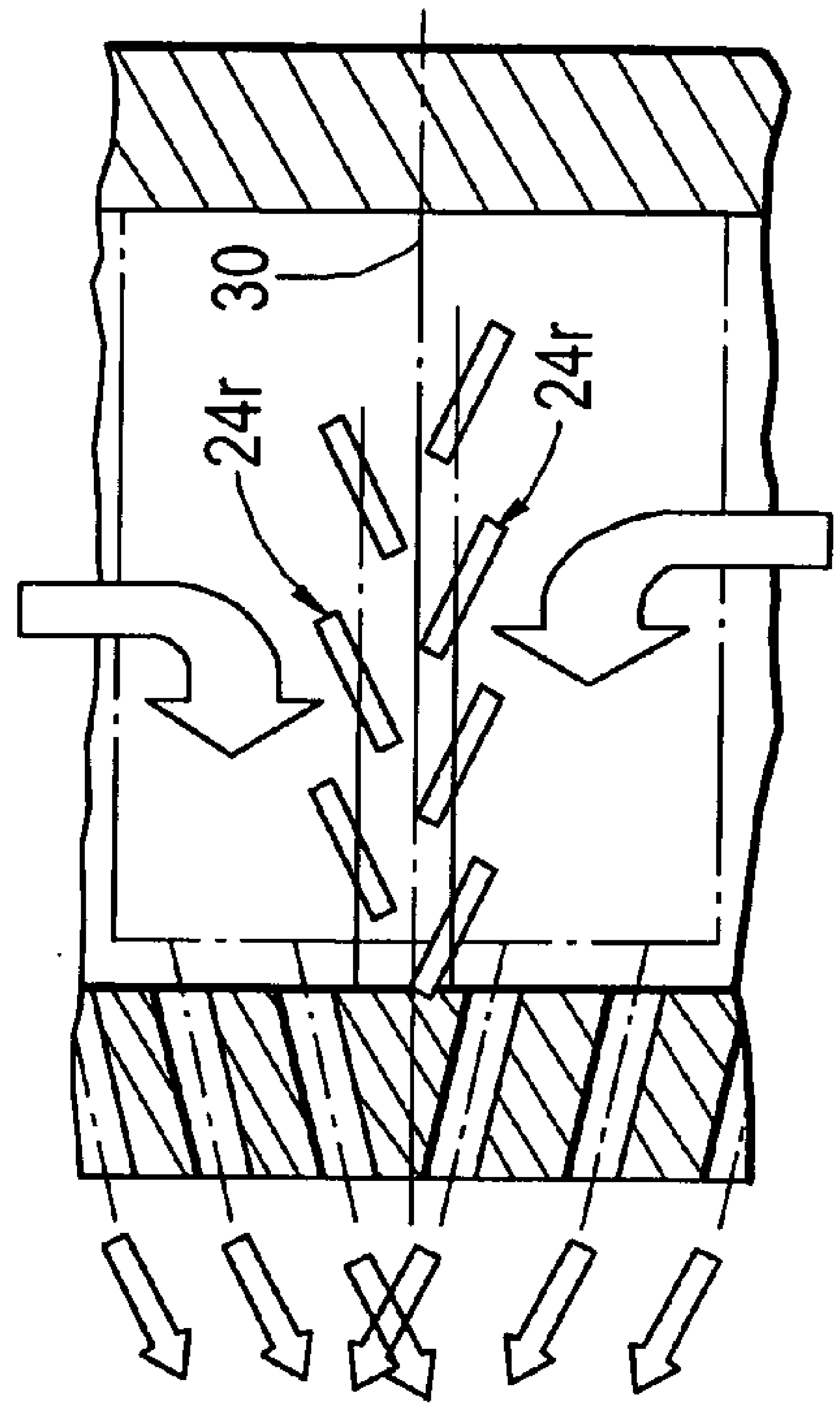


Fig.18

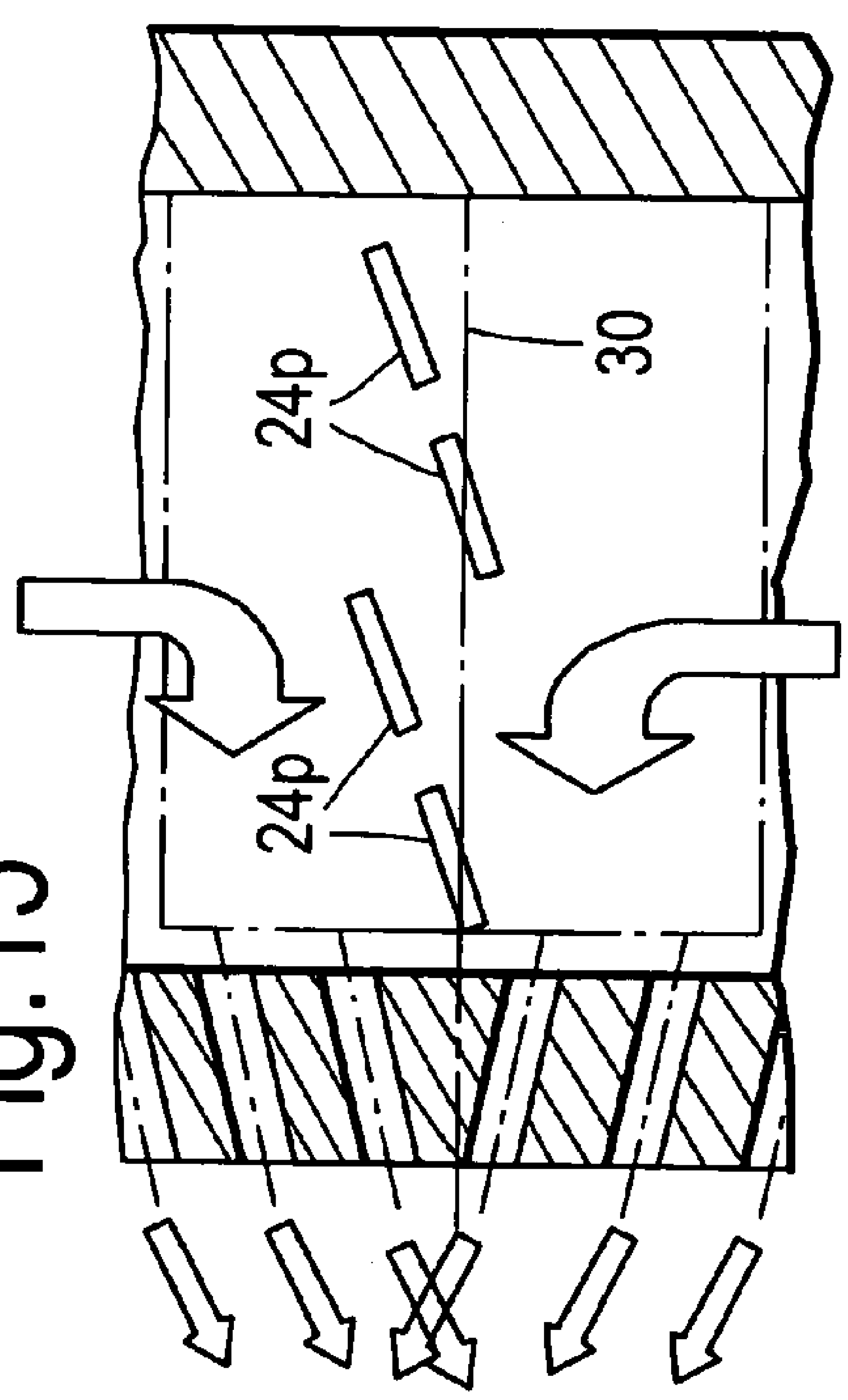


Fig.15

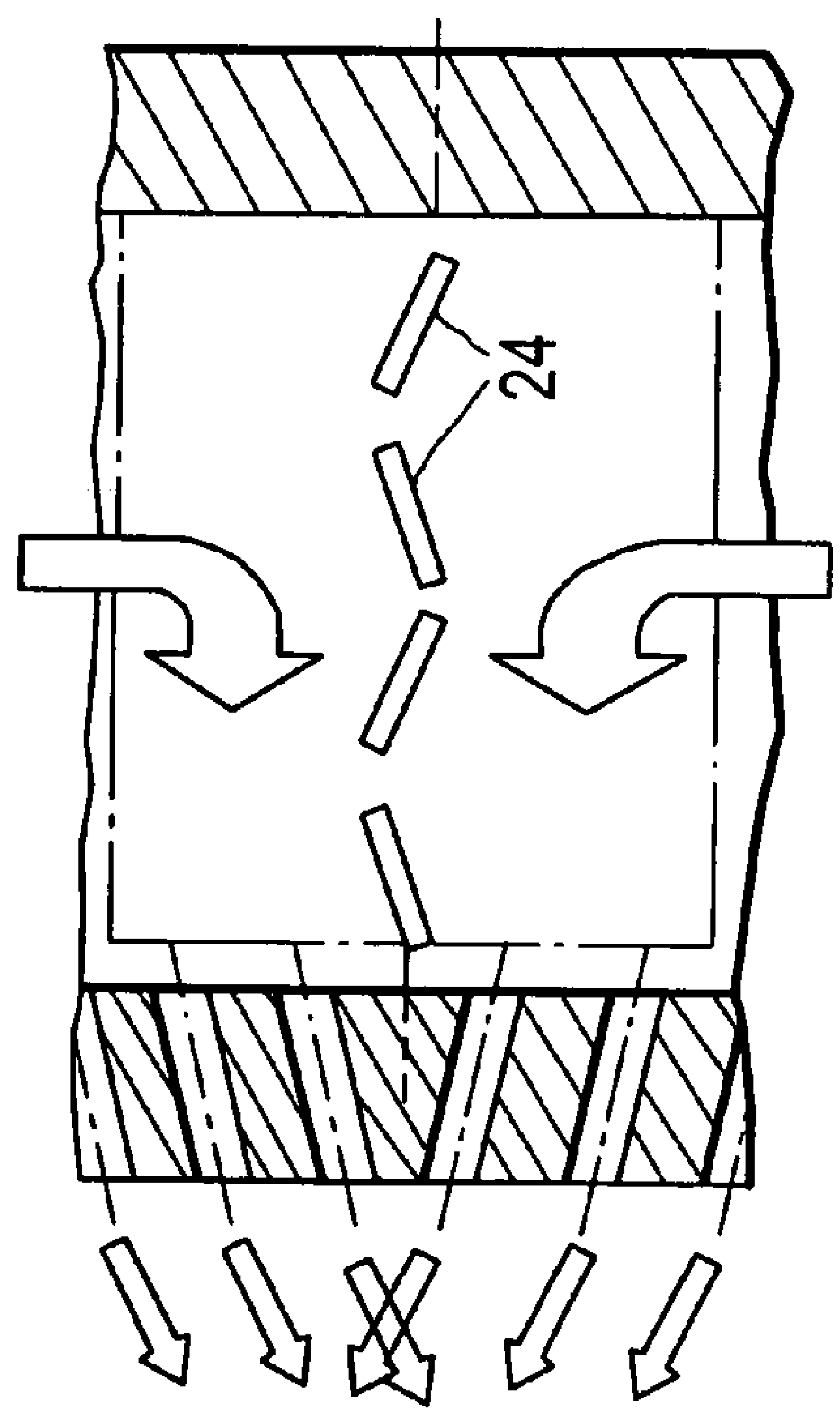


Fig.16

AEROFOIL COOLING ARRANGEMENT

[0001] The present invention relates to aerofoils and more particularly to nozzle guide vanes utilised in gas turbine engines.

[0002] Within a gas turbine engine it will be appreciated that the performance of the gas turbine engine cycle, whether made in terms of efficiency or specific output, is improved by increasing the turbine gas temperature. In such circumstances it is desirable to operate the turbine at as high a gas temperature as possible. For any engine cycle, in terms of compression ratio or bypass ratio, increasing the turbine entry gas temperature will always produce more specific thrust. Unfortunately, as turbine engine temperature increases it will be understood that the life of an uncooled turbine blade falls necessitating the development of better materials and/or internal cooling of the blades.

[0003] Modern gas turbine engines operate at turbine gas temperatures which are significantly hotter than the melting point of the blade material used. Thus, at least high pressure turbines as well as possibly intermediate pressure turbines and low pressure turbines are cooled. During passage through the turbine it will be understood that the temperature of the gas decreases as power is extracted. In such circumstances the need to cool static or rotating parts of the engine decreases as the gas moves from the high temperature stages to the low temperature stages through to the exit nozzle for the engine.

[0004] Typical forms of cooling include internal convection and external films. A high pressure turbine nozzle guide vane (NGV) consumes the greatest amount of cooling air. High pressure turbine blades typically use approximately half of the coolant that is required for nozzle guide vanes. Intermediate and low pressure stages down stream of the high pressure turbine progressively utilise and need less cooling air.

[0005] The coolant used is high pressure air taken from a compressor. The coolant bypasses the combustor and is therefore relatively cool compared to the gas temperature of the working fluid. The coolant temperature often will be 700 to 1000K whilst working gas temperatures will be in the excess of 2000K.

[0006] By taking cooling air from the compressor it will be understood that the extracted compressed air can not be utilised to produce work at the turbine. Extracting coolant flow from the compressor has an adverse effect upon engine overall operating efficiency. In such circumstances it is essential that coolant air is used most effectively.

[0007] FIG. **1** provides a pictorial illustration of a typical prior blade arrangement including a nozzle guide vane (NGV) and a rotor blade **2**. A nozzle guide vane **1** comprises an outer platform **3**, an inner platform **4** and an aerofoil vane **5** between. A rotor blade **2** comprises a shroud **6**, a platform **7** with an aerofoil blade **8** between them. The guide vane **1** is substantially static and fixed whilst the rotor blade **2** rotates upon a rotor disc **9** secured through a blade root **10**. Generally, a seal shroud **11** is provided in association with a support casing **12** in order to define a path across the arrangement **13** in the direction of arrowheads A. The vanes **1** and rotor blades **2** will generally be in assembly as indicated with the vanes stable and static whilst the rotor blades **2** rotate in the direction of arrowheads B to generate flow.

[0008] In such circumstances generally coolant for respective vanes and blades **5**, **8** is through a combination of dedicated cooling air and secondary leakage flow especially from aerofoil components such as platforms and shrouds. Nozzle guide vane platforms **3**, **4** and blade platforms **7** generally use leakage flow to cool an upstream region. Dedicated coolant flow is used to cool down regions of the platforms **3**, **4**, **7**.

[0009] Generally, high pressure turbine nozzle guide vanes are formed as aerofoils with cooling air bled from cavities above an outer platform and from below an inner platform. The coolant flows to cool a leading edge of the aerofoils. As the feed pressure of the cooling air is available only marginally above the hot gas flow pressure at the stagnation point at the aerofoil leading edges, an inlet for coolant at both ends of the aerofoil is required. It will be understood that a single feed system will need an increase in the velocity of the coolant at entry to the aerofoil causing unacceptably high entry losses and associated pressure drop.

[0010] Unfortunately, feed pressures in the cavities formed within aerofoils to define nozzle guide vanes are not stable at the respective inlets at either end of the cavity. In such circumstances, it is necessary to partially block the coolant flow from passing directly through the aerofoil cavity from outboard to inboard or vice versa. It will be understood that if such direct flow were allowed to happen not only would entry losses become unacceptable but static pressure in the cavity itself, which drives film cooling would also fall below the required level to ensure hot gas ingestion does not occur.

[0011] One practical way of preventing cooling air jetting directly through the cavity in either direction is to introduce a sheet metal baffle or plate mounted on a backing plate which is secured to the inside of the cavity by a series of tangs. The position of the baffle plate within the cooling passage cavity can easily be controlled by changing the length of the backing plate. The ideal location of the baffle plate is where the feed pressure and losses are balanced to give the same minimum pressure margin between the internal coolant pressure and the hot gas flow at both aerofoil root and tip locations. Unfortunately it is also advisable to avoid peaks in hot gas profile if at all possible.

[0012] Examples of typical prior approaches to providing sheet metal baffles relate to fitting the baffle plate within a forward cooling cavity of a nozzle guide vane. The baffle plate is inserted through an outer platform leading edge cavity and utilises locating lugs to position the baffle plate and lock the baffle plate in place by bending over tabs or tangs which extend through apertures in a wall located at the outer end of the backing plates. The baffle plates are attached to the backing plates by a weld joint. To prevent flapping in use the baffle plate is generally supported and presented upon a strengthening web. Coolant air is then allowed to enter the cavity from either end through appropriate inlets with the baffle plate then preventing direct jetting therethrough. A further alternative is to utilise a perforated metal tube again presented within the cavity formed within the aerofoil. A baffle plate is incorporated into the impingement tube to prevent cooling air from passing directly through the tube from inlets either side of the cavity.

[0013] In view of the above, prior arrangements are typically relatively fragile but also expensive to manufacture and fit. These baffle plates with backing plates are subject to vibration, fracture and the baffle itself may become detached from the backing plate resulting in aerofoils which do not operate correctly and therefore overheat and may oxidise prematurely.

[0014] Thus prior arrangements for providing baffles within aerofoils such as nozzle guide vanes have typically been expensive to manufacture and fit. Furthermore, by provision of separate baffle plates there is an increase in component count which can tend to provide unreliability in terms of remaining in place during the whole aerofoil's life with potential problems including vibration failure, relative movement between the mating parts due to wear. The arrangement is not failsafe in that it is possible there is incorrect location or failure to fit at all. Furthermore it will be appreciated that consistent positioning of the baffle is difficult in view of the potential for up-down slide movement of the baffle plate in use. It will also be understood that the baffle plate may be damaged or malformed during assembly procedures. Furthermore, where an aerofoil incorporates more than one cavity it is possible that incorrect baffle plates may be assembled in the wrong cavity resulting in inappropriate operation. Finally, as gas and coolant temperatures increase in an engine the sheet metal baffle plate material will become weaker and therefore less resistant to oxidation attack and degradation of the material from which the aerofoil is formed.

[0015] In accordance with aspects of the present invention there is provided an aerofoil having a radial axis, an external wall forming a pressure surface and a suction surface and an internal wall together defining a cavity that extends radially and comprises a radially inner inlet and a radially outer inlet for radial fluid flow in use, the external wall comprises an array of effusion cooling apertures, characterised in that the external wall comprises at least one first baffle extending across the cavity to restrict radial flow therethrough.

[0016] Preferably, a plurality of first baffles extend from the external wall and define an aperture between their free ends.

[0017] Normally, any gap between adjacent first baffles changes size dependent on temperature.

[0018] Alternatively, the aerofoil comprises an internal wall and together with the external wall defines the cavity, the internal wall comprises a second baffle extending across the cavity to restrict the radial flow.

[0019] Advantageously, the first baffle is position radially below and another first baffle is positioned radially above the second baffle.

[0020] Alternatively, the first and second baffles overlap one another.

[0021] Alternatively, the first baffle(s) is formed from any one of the group of shapes comprising castellated, sinusoidal and saw-toothed each having longer and short extending portions.

[0022] Preferably, the first baffle or the longer portion of the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

[0023] Preferably, the first baffle(s) is positioned radially adjacent and within 5× a diameter of the effusion cooling apertures.

[0024] Preferably, the first baffle(s) extends from the external wall at least 5× a diameter of the effusion cooling apertures.

[0025] Alternatively, the first and/or second baffle comprises an array of holes.

[0026] Alternatively, the first and/or second baffle is angled from the radial and/or a line perpendicular to the radial line.

[0027] Embodiments and aspects of the present invention will now be described by way of example and with reference to the accompanying drawings in which:

[0028] FIG. **1** provides a pictorial illustration of a typical prior blade arrangement including a nozzle guide vane (NGV) and a rotor blade **2**;

[0029] FIG. **2** is a schematic isometric view of a first embodiment of an aerofoil in accordance with aspects of the present invention;

[0030] FIG. **3** is a schematic illustration of a top perspective view of the aerofoil depicted in FIG. **2**;

[0031] FIG. **4** is a schematic cross section of a first baffle configuration in accordance with aspects of the present invention;

[0032] FIG. **5** is a schematic cross section of a second baffle configuration in accordance with aspects of the present invention;

[0033] FIG. **6** provides a side schematic view of a third configuration of a baffle in accordance with aspects of the present invention; and,

[0034] FIG. **7** is a side view in the direction of A-A of the baffle depicted in FIG. **6**.

[0035] FIGS. **8-11** are sections through a forward or leading edge portion of the aerofoil showing a number of embodiments of baffle arrangements in accordance with the present invention;

[0036] FIGS. **12-19** are a series of cross-sections, typically section A-A in FIG. **8**, of a number of embodiments of the baffle arrangements in accordance with the present invention.

[0037] Aspects of the present invention eliminate the need for a separate baffle plate. Such elimination is achieved through casting a baffle within a wall as part of the manufacturing process for the aerofoil. It will be appreciated that the aerofoil will incorporate apertures to allow development of a cooling film upon the aerofoil surfaces. These apertures may be cast into the aerofoil during a normal manufacturing process or formed by drilling post initial casting of the aerofoil. In any event aspects of the present invention ensure that the forming process for the apertures is arranged such that the baffle plate is not fouled or destroyed by this process.

[0038] FIG. **2** provides a cutaway side view of an aerofoil in accordance with aspects of the present invention. The aerofoil **50** at opposed ends defines an inner platform and an outer platform **52**. A cutaway portion **53** illustrates a wall **54** in which a baffle **55** is formed. This baffle **55** is cast, or potentially cut or otherwise formed, with the wall **54**. It will be appreciated that the opposed ends defined by the platforms **51**, **52** provide inlets for coolant flows **56**, **57**. The flows **56**, **57** are arranged to provide film cooling flows **58** through apertures **59** in a surface typically opposite the wall **54**. As described previously if the coolant flows **56**, **57** are not restrained by the baffle **55** there is a potential for direct cross jetting of the flows **56**, **57** from the respective opposed inlet ends defined by the platforms **51**, **52**. This will result in unacceptable entry losses for the flows **56**, **57** as well as a diminution in the coolant pressure particularly at intermediate portions of the aerofoil **50**. It will be understood that intermediate portions will also tend to be the hottest parts of the aerofoil **50** in use.

[0039] It will be noted that the baffle **55** extends nearly across a cavity **60** defined by the spacing between the wall and the generally opposed surface incorporating the apertures **59**. The apertures **59** are typically angled in order to create the film cooling effect. Furthermore, the baffle **55** is orientated and positioned such that forming the apertures **59** will not compromise the baffle **55** or creation of the apertures **59**.

[0040] As illustrated it will be noted that the wall **54** is generally a divider wall within the aerofoil **50**. Thus as illustrated there is normally a front cavity **60** and a rear cavity **61**. Baffles can be presented and projected across both cavities **60**, **61** but normally consideration is particularly important with regard to the leading edge or front cavity **60**. The cavities **60**, **61** act as feed passages for coolant flow.

[0041] The baffle **55** extends substantially across the cavity **60** but a small cross sectional area **62** is retained to allow some fluid flow across the respective ends **60***a*, **60***b* of the cavity **60** for pressure balance.

[0042] As illustrated the baffle **55** substantially extends laterally with webs or fillets **63** to provide strength as well as reduce the potential for vibration in the baffle **55**.

[0043] FIG. **3** provides a more schematic isometric view of the first embodiment as depicted in FIG. **2**. The baffle **55** is cast with a wall **54** which is typically a divider wall within an aerofoil **50**. The divider wall **54** separates a forward cooling cavity **60** from a rear cooling cavity **61**. These cavities **60**, **61** define passages along which as illustrated coolant flows **56**, **57** are presented from inlets (not shown). The baffle **55** is presented intermediate along the length of the cavity **60** and extends substantially across the cavity **60**. It will be appreciated that the wall **54** is relatively cool compared to the external side walls of the cavity **60** whether considered as pressure or suction side walls. The temperature of the baffle **55** will not be as elevated and furthermore it will be appreciated that the baffle **55** is cooled by the coolant flows **56**, **57** within the cavity **60**. The baffle **55** is relatively well matched to the divider wall **54** resulting in reduced local thermal gradients in the aerofoil **50**.

[0044] The baffle **55** is cast with the wall **54** and provides a necessary interruption and restriction to flows **56**, **57** along the aerofoil **50**. As the baffle **55** is formed integrally upon casting the aerofoil **50** it will be appreciated that there is a reduction in cost in comparison with forming a separate sheet metal baffle arrangement as well as assembly of that sheet metal baffle arrangement within the aerofoil. In terms of manufacture it will be appreciated that the creation of the baffle **55** is typically achieved through alteration to a ceramic core utilised for casting of the aerofoil **50** in use.

[0045] In order to appropriately present the baffle **55** generally webs **63** are provided either side of the baffle **55**. These webs **63** can comprise fillets extending laterally from the baffle **55** upon the wall **54**. The webs **63** prevent the baffle **55** vibrating due to unsteady buffeting from the air flows **56**, **57**.

[0046] As described previously the baffle **55** will extend substantially across a gap or spacing between the wall **54** and an opposed surface incorporating the apertures **59**. Generally, the gap extends about the periphery **71** with respect to a side of the opposed surface **70** incorporating the apertures **59**. The cross sectional area **62** as described previously is provided as a gap to allow pressure exchange between the cavity ends **60***a*, **60***b*. Small quantities of coolant can pass from the radially outer cavity **60***a* to the radially inner cavity **60***b* and vice versa. The terms radially inner and radially outer are with respect to a main rotational axis of a gas turbine engine and when the aerofoil is installed in the engine.

[0047] The baffle **55** in terms of shape and orientation can be varied to accommodate differing aperture **59** patterns. The apertures **59** are arranged in order to achieve the desired film cooling **58** and can be different dependent upon aerofoil **50** configuration. In accordance with aspects of the present invention the baffle **55** is arranged such that the process tool utilised to form or finish pre-cast apertures **59** will not damage or be influenced by the baffle integrally formed with the wall **54**. A further consideration is with regard to the natural vibration or frequency of the baffle **55**. In such circumstances the shape of the baffle **55** may also be determined and designed to avoid any possibility of high cycle fatigue failure due to air flows through the apertures **59** and across the gap defined by the area **62**.

[0048] FIGS. **4** to **7** illustrate three different embodiments of a baffle in accordance with aspects of the present invention. These embodiments are provided for illustration purposes and it will be appreciated that other shapes, orientations and configurations of baffle are possible in accordance with aspects of the present invention.

[0049] FIG. **4** illustrates a first embodiment of a baffle **155** that is presented perpendicularly from a wall **154** towards a surface which is typically an external wall **170** of an aerofoil. The surface **170** opposite the wall **154** incorporates apertures **159** to direct coolant flows **156**, **157** to generate film cooling **158**.

[0050] The baffle **155** is configured perpendicular to a general direction of the coolant flows **156**, **157**. Thus the baffle **155** is substantially perpendicular to a plane of the wall **154**. The apertures **155** are typically drilled at an angle to improve the film cooling effect. The angles for the apertures **159** are chosen to benefit from dynamic pressure in the passages defined by the cavities **160**. Thus, the apertures **159** are generally aligned or at least turned towards the direction of coolant flow **156**, **157** in the outer as well as inner cavity sections of the cavity **160**.

[0051] As previously, the baffle **155** extends substantially across the cavity **160** to only leave a relatively small gap to an inner side of the surface **170** comprising the apertures **159**. This gap allows a small available cross sectional area **162** for the coolant flows **156**, **157** to be exchanged within the cavity **160**.

[0052] A perpendicular presentation of the baffle **155** is potentially the simplest configuration for cast formation and integral association with the wall **154**. However, such perpendicular presentation may also be subject to the greatest potential problems vibration and therefore stressing in use. Hence webs **163** are provided to prevent vibration as well as ensure robustness in use.

[0053] FIG. **5** illustrates a second embodiment of a baffle **255** in accordance with aspects of the present invention. The baffle **255** again projects from a wall **254** towards an opposed surface **270** incorporating apertures **259**. As previously coolant flows **256**, **257** generally pass from inlets at opposed ends of an aerofoil. The coolant flows **256**, **257** are arranged to provide film cooling **258**. The baffle **255** as previously essentially divides a cavity **260** into an outer cavity section **260***a* and a inner cavity section **260***b*.

[0054] Generally the baffle **255** will be inclined at an angle between 30° and 60° to a perpendicular projection from a plane surface of the wall **254**. Furthermore, the baffle **255** will be typically aligned with the apertures **259**. Such alignment between the baffle **255** and the apertures **259** obviates or reduces the possibility of striking the baffle **255** when utilising a forming or process tool such as an electrode or laser beam to form the apertures **259**. Nevertheless it will be appreciated that only half of the apertures **259** can benefit from a dynamic pressure head created within the cavity **260**. It will be noted that the baffles **255** can be orientated upward or downward dependent upon requirements for an aerofoil. Similarly, the angle can be chosen dependent upon the angle of the apertures **259** or to achieve desired separation within the cavity **260**. Again it will be noted that the baffle **255** extends substantially fully across the cavity **260** with an open cross sectional area **252** remaining available to allow coolant flow **256**, **257** exchange across the respective cavity sections **260***a*, **260***b*.

[0055] Webs **263** or fillets are provided either side of the baffle **255** to provide support of and achieve greater strength in the baffle **255**.

[0056] FIGS. **6**, and **7** provide illustrations respectively of a side and front schematic view of a third embodiment of a baffle **355** in accordance with the present invention. The baffle **355** extends within a cavity **360** to define an outer cavity section **360***a* and an inner cavity section **360***b*. The baffle **355** extends towards a surface **370** which is typically an external wall surface of an aerofoil. The surface **370** incorporates apertures **359** which receive coolant flows **356**, **357** in order to define film cooling **358**. As previously the baffle **355** divides the cavity **360** in order to prevent direct jetting of the coolant flows **356**, **357** across the passage defined by the cavity **360**. Generally a gap is provided around the baffle **355** to allow coolant flow exchange between the cavity section **360***a*, **360***b*.

[0057] The baffle **355** in accordance with the third embodiment is generally angled to be inclined from a first side **380** to a second side **381**. Such a configuration allows further coolant flow control to the apertures **359** for coolant film **358** creation. The baffle **355** is orientated at an angle when viewed in the direction of a wall **354** that is to say as viewed in the direction A-A. Such a configuration provides benefits including enabling construction of an aerofoil configuration with cooling film apertures in rows where the gap between apertures in the same row, to accommodate the baffle **355**, are not in alignment with a hot gas flow over the surface **370**.

[0058] Typically, the baffle **355** will be configured to have an orientation at a compound angle which is a combination of the upward or downward orientation as depicted in FIG. **5** together with an inclined angle or presentation as depicted in FIG. **7** from the first side **380** to the second side **381** of the cavity **360**.

[0059] Reference is now made to FIGS. **8-18** and here the present invention is directed to a turbine aerofoil comprising a baffle arrangement or array of baffles extending from the external or hot wall. The aerofoil has a radial axis **20** when in a gas turbine engine and an external wall **70** forming a pressure surface **70***p* and a suction surface **70***s* and an internal wall **54**. The external and internal walls together define the cavity **60** that extends radially. The cavity comprises a radially inner inlet **56***i* and a radially outer inlet **57***i* for radial fluid flows **56** and **57**. During normal operation the fluid flows **56** and **57** each enter their inlet in varying quantities as described earlier. The external wall comprises an array of effusion cooling apertures **59**.

[0060] The present invention is characterised by the external wall comprising at least one (first) baffle extending across the cavity to restrict radial flow(s) **56**, **57** therethrough. Conventional turbine aerofoils are subject to such hot environments that the sheet metal inserts forming a baffle are always located towards the internal and therefore cooler wall **54**. These conventional baffle arrangements are then disadvantaged because the baffle creates a sudden narrowing around its free edge and the external wall. Here, and particularly where there is a significant difference in coolant flow pressures between flows **56** and **57**, the coolant airflow is accelerated with an associated decrease in pressure. This is problematic because less and possibly no effusion cooling air flows through some of all the effusion cooling holes **59**. In turn this creates hot streaks on the outer surface of the external wall. Hot streaks cause accelerated oxidation and thermal fatigue to the aerofoil. The baffle arrangements, of the present invention, extending from the external wall obviate this problem as the baffle causing the fluid flow to slow locally to the effusion cooling apertures thereby increasing the coolant's static pressure and increasing the cooling flow through the apertures. This is shown on FIG. **19**, where, in this example, flow **56** is dominant and flows through the gap between the two first baffles **24** and the second baffle **27**. An eddy **56***e* is created in the lee of the radially lower first baffle **24** and another eddy **57***e* similarly radially above of the radially outer first baffle **24**. Other eddies **56***f* are created in the bluff and lee of the two first baffles as shown.

[0061] In FIGS. **8** and **9** the aerofoil, here shown in during use and therefore very hot, comprises a plurality of first baffles **24** extend from the external wall **70** to define a flow aperture **21** between their free ends **22**. When cold the aerofoil contracts and the gaps **23** between lateral edges **25** of the fingers or baffles **24** close up. Although some coolant may pass through these gaps **23**, they are sufficiently small in comparison to the flow aperture **21** not to increase the flow velocity therethrough. In these embodiments, the gaps are necessary to allow thermal expansions and contractions without over-stressing the baffles. In FIG. **9** an additional or second baffle **26** extends from the internal wall **54** to fill the flow aperture. The flow aperture **21** is shown generally central to the cavity so that the accelerated coolant flow is kept as far away from the effusion cooling holes as possible. However, depending on the flow regimes and pressure distributions both internally and externally the flow aperture **21** may be offset from the centre of the cavity.

[0062] In FIG. **9** most of the baffles or fingers **24** are trapezoidal, with its fee end being the smaller side length. The additional or second baffle **26** is generally triangular as is an opposing first baffle **28** extending from the external wall near to the leading edge of the aerofoil. These two baffles are shaped to fill the gaps left by the arrangement of trapezoidal baffles **24**.

[0063] Referring to FIGS. **10**, **11** and **12** there are three embodiments where, along with the first baffles extending from the external wall, a second baffle extends from the internal wall to restrict the radial flow. These configurations allow the first baffle on the external wall to extend a minimum amount into the cavity thereby reducing thermal strains in the baffle.

[0064] Importantly, although not essential for every effusion cooling hole, in each embodiment the first baffle is position radially below and another first baffle is positioned radially above the second baffle.

[0065] As shown in FIG. **19** and in a dashed line of figure the first and second baffles overlap one another, creating a more tortuous route and therefore more energy is lost and a slower flow regime which increases static pressure arises.

[0066] FIG. **10** shows a generally uniformly extending first baffle **24**, which is shown either overlapping or with a radial gap between it and the second baffle **27**. Where there is a radial gap the first and second baffles may be conveniently arranged at the same radial location, whereas the overlapping baffles will be radially spaced from one another. The first baffle(s) may be formed from any one of the group of shapes comprising castellated (FIG. **11**), sinusoidal (FIG. **12**) and saw-toothed (pointed instead of truncated as in FIG. **11**). Each baffle or finger has longer and short extending portions indicated **24*l*** and **24*s***. As shown and as far as practicable, the longer portion of the first baffle is positioned radially above or below at least one of the effusion cooling apertures to cause the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough. To be most effective the first baffle(s) is positioned within 5× a diameter of the effusion cooling apertures. Again for maximum effectiveness, the first baffle(s), or the longest part, extends from the external wall at least 5× a diameter of the effusion cooling apertures.

[0067] Further energy from the flows **56**, **57** may be lost where the first and/or second baffle comprises an array of holes **28**.

[0068] In FIGS. **13** to **18**, the baffles or fingers **24** of the first and/or second baffle are angled from a line **30** perpendicular to the radial line **20**. This line **30** is the tangential line when the aerofoil is sited in the engine. Effectively the baffles may be rotated or angled about their longitudinal axis **32** (see FIG. **8**). An angle θ of about 30 degrees is believes to be advantageous and can create additional flow disturbance to increase the static pressure and improve coolant flow through the effusion cooling holes. Angles θ can be anywhere between 0 and 90 degrees although the intention is to create the greatest pressure loss.

[0069] In FIG. **13** the baffles **24** are all aligned on the same line, itself angled at θ, with each baffle also angled at θ. In FIG. **14** the baffles lie on the line **30** and are each angled about their longitudinal axes at θ. In figure adjacent baffles may also be overlapping when viewed radially and as shown by extensions **24*e***. Again a more tortuous and loss inducing route is created for the flows **56**, **57**.

[0070] In FIG. **15**, the baffles may be arranged in a compound form combining FIGS. **13** and **14** embodiments with pairs of baffles **24*p*** arranged on an angled line, but each pair is then aligned along the line **30** with the other pair.

[0071] In FIG. **16** alternate baffles are angled + and −θ from the line **30**. In FIG. **17** the baffles from one side of the cavity **24*a*** are angled oppositely to those extending from the other side of the cavity **24*b***. In FIG. **18**, two rows of baffles **24*r*** are arranged generally parallel and are oppositely angled about their own axis.

[0072] It will be appreciated that integral formation of a baffle reduces costs and therefore expense of manufacture and part count which will aid logistically as well as administratively simpler provision of spare parts in use. Furthermore as the cast and integrally formed baffle cannot shake loose in operation there is greater reliability of operation. Furthermore the position of the baffle can be reliably and repeatedly achieved ensuring that where machine tools are utilised to define the film cooling apertures these machining tools, such as lasers or drills, will not strike of the baffle causing damage, deflection or loss.

[0073] As there is integral construction, a rigid structure can be provided which has less vibration problems and furthermore as there are no separate parts with respect to the baffle problems such as fretting and wear can be avoided. By integral forming within the aerofoil the potential for mistaken build without incorporation of the baffle plate is avoided. Additionally, problems with regard to incorrect fitting can be avoided by integral casting of the baffle within the cavity. By eliminating the necessity for locating lugs within a cavity the core tools utilised for forming the cavity in accordance with aspects of the present invention may be simplified.

[0074] By creating the baffle integrally within the cavity the potential for damage is avoided. It will be appreciated that plate baffles extending outwardly are generally relatively fragile and subject to damage.

[0075] The baffles in accordance with aspects of the present invention are designed and configured to accommodate differing leading and trailing edge cooling regimes in the respective cavities. As the baffle is formed from the same material as the aerofoil and as the baffle is bathed in coolant air problems of oxidation are avoided. The baffle and other internal surfaces of the cavity may be protected by an appropriate coating from sulphidation.

[0076] Alternative is to provide specific shaping of the baffle, for example a curved baffle, may be provided. This may take the form of a half cylindrical cross section angled upwards or downwards as described with regard to FIG. **5**. A further alternative is to provide a curved baffle in a scoop shape extending from the surface in order to create desired separation of a cavity within which coolant flows are presented. It will be appreciated that curved baffles will still typically incorporate webs to provide reinforcement and avoid vibration.

[0077] Internal walls within an aerofoil and in particular divider walls between a front and rear cavity are particularly advantageous for presenting baffles. However alternatively other internal walls of a cavity may be utilised to present the baffle plates as required.

[0078] An alternative to the small gap between the baffle and the opposed surface is to provide the baffle plate with perforations. These perforations will take the place of one or more holes which again will allow a small proportion of coolant flow exchange across the baffle but still substantially prevent direct jetting from inlets at opposite ends of the cavity.

[0079] Embodiments of the present invention described above illustrate a single substantial baffle extending across the cavity. However, in some situations a plurality of baffles may be provided. A principal baffle may be utilised along with a series of partial baffles which extend from the wall. These baffles may alter the gap and therefore the available cross sectional area in the spacing between the baffle **255** and the opposed surface incorporating the apertures **259**. Such variations in the available cross sectional area allows control of coolant flow and potentially accelerates the coolant flow in the passage progressively as flow is bled off through the apertures from the cavity. Such acceleration in flow increases the Reynolds number of the flow and therefore the heat transfer rate within the cavity.

[0080] A baffle might be considered as any cast feature that effectively blocks or partially blocks the passage of coolant flow within the cavity and prevents that coolant flow from passing from the inlet at one end of the cavity directly to the inlet at the other end of the cavity.

[0081] Modifications and alterations to aspects of the present invention will be appreciated by those skilled in the art. Thus sides of the baffle may be dished dependent upon requirements. An edge of the baffle may be fluted or castellated such that effectively segments are provided with gaps between rather than a continuous gap about the edge of the baffle towards an opposed surface incorporating the apertures to define film cooling.

[0082] Partial baffles may be provided extending proportionately from a wall or walls such that the combination of baffles within the cavity prevents a direct flow path and therefore direct jetting across the cavity in use. Such an approach may allow easier cast formation in creating integral baffles.

1. An aerofoil having a radial axis, an external wall forming a pressure surface and a suction surface and an internal wall together defining a cavity that extends radially and comprises a radially inner inlet and a radially outer inlet for radial fluid flow in use, the external wall comprises an array of effusion cooling apertures, wherein the external wall comprises at least one first baffle extending across the cavity to restrict radial flow therethrough.

2. The aerofoil as claimed in claim **1** wherein a plurality of first baffles extend from the external wall and define an aperture between their free ends.

3. The aerofoil as claimed in claim **2** wherein any gap between adjacent first baffles changes size dependent on temperature.

4. The aerofoil as claimed in claim **1** wherein the aerofoil comprises an internal wall and together with the external wall defines the cavity, the internal wall comprises a second baffle extending across the cavity to restrict the radial flow.

5. The aerofoil as claimed in claim **4** wherein the first baffle is positioned radially below and another first baffle is positioned radially above the second baffle.

6. The aerofoil as claimed in claim **4** wherein the first and second baffles overlap one another.

7. The aerofoil as claimed in claim **1** wherein at least one first baffle is formed from any one of the group of shapes comprising castellated, sinusoidal and saw-toothed each having longer and short extending portions.

8. The aerofoil as claimed in claim **1** wherein the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

9. The aerofoil as claimed in claim **1** wherein at least one first baffle is positioned radially adjacent and within 5× a diameter of the effusion cooling apertures.

10. The aerofoil as claimed in claim **1** wherein at least one first baffle extends from the external wall at least 5× a diameter of the effusion cooling apertures.

11. The aerofoil as claimed in claim **1** wherein the first and/or second baffle comprises an array of holes.

12. The aerofoil as claimed in claim **1** wherein the first and/or second baffle is angled from the radial and/or a line perpendicular to the radial line.

13. The aerofoil as claimed in claim **2** wherein the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

14. The aerofoil as claimed in claim **3** wherein the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

15. The aerofoil as claimed in claim **4** wherein the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

16. The aerofoil as claimed in claim **5** wherein the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

17. The aerofoil as claimed in claim **6** wherein the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

18. The aerofoil as claimed in claim **7** wherein the larger portion of the first baffle is positioned radially above or below at least one of the effusion cooling apertures causing the fluid flow to slow locally to the effusion cooling aperture and increase its static pressure to increase a cooling flow therethrough.

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