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(54) **CARBON NANOTUBE PROBE TIP GROWN ON A SMALL PROBE**

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(57) **ABSTRACT**

A method of fabricating a carbon nanotube probe tip and the resultant probe tip, particularly for use in an atomic force microscope. A moderately sharply peaked support structure has its tip cut or flattened to have a substantially flat end of size of about 20 to 200 nm across. The support structure may be formed by etching a conical end into a silica optical fiber. Nickel or other catalyzing metal such as iron is directionally sputtered onto the flat end and the sloped sidewalls of the support structure. The nickel is anisotropically etched to remove all the nickel from the sidewalls but leaving at least 15 nm on the flat end to form a small nickel dot. A carbon nanotube is then grown with the nickel catalyzing its growth such that only a single nanotube forms on the nickel dot and its diameter conforms to the size of the nickel dot.

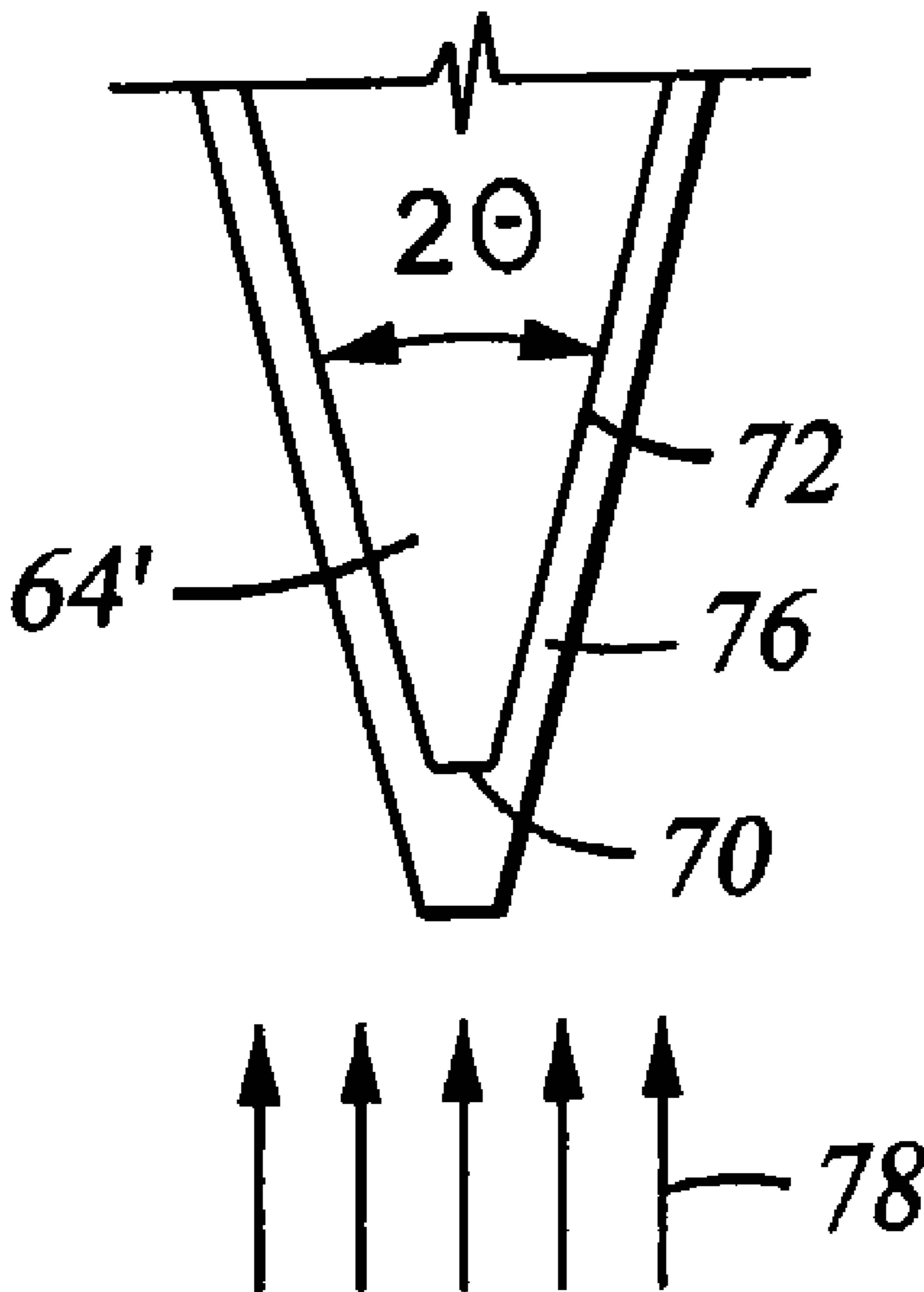
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Related U.S. Application Data

(63) **Continuation of application No. 09/657,428, filed on Sep. 8, 2000, now Pat. No. 6,457,350.**



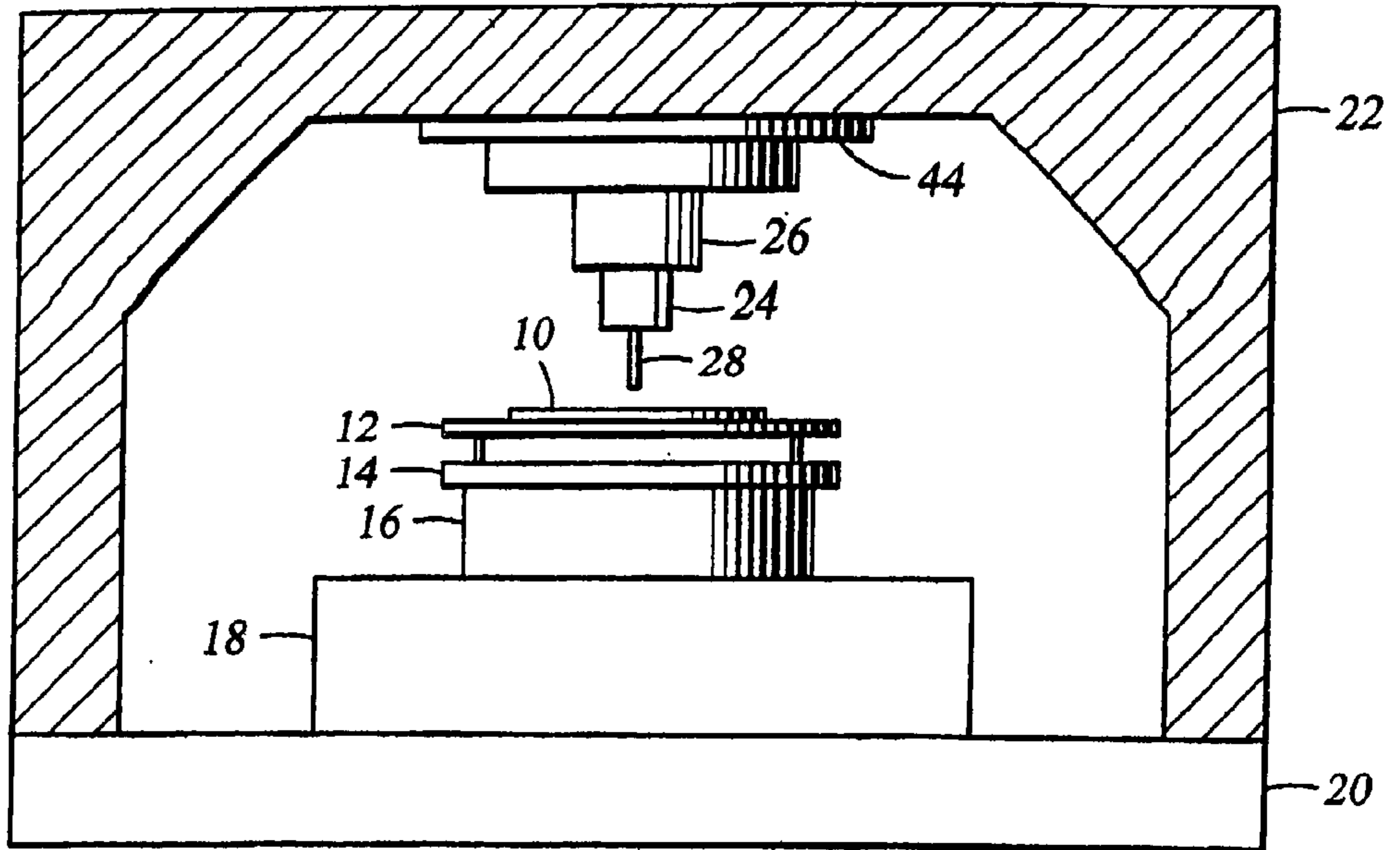


Fig. 1
(PRIOR ART)

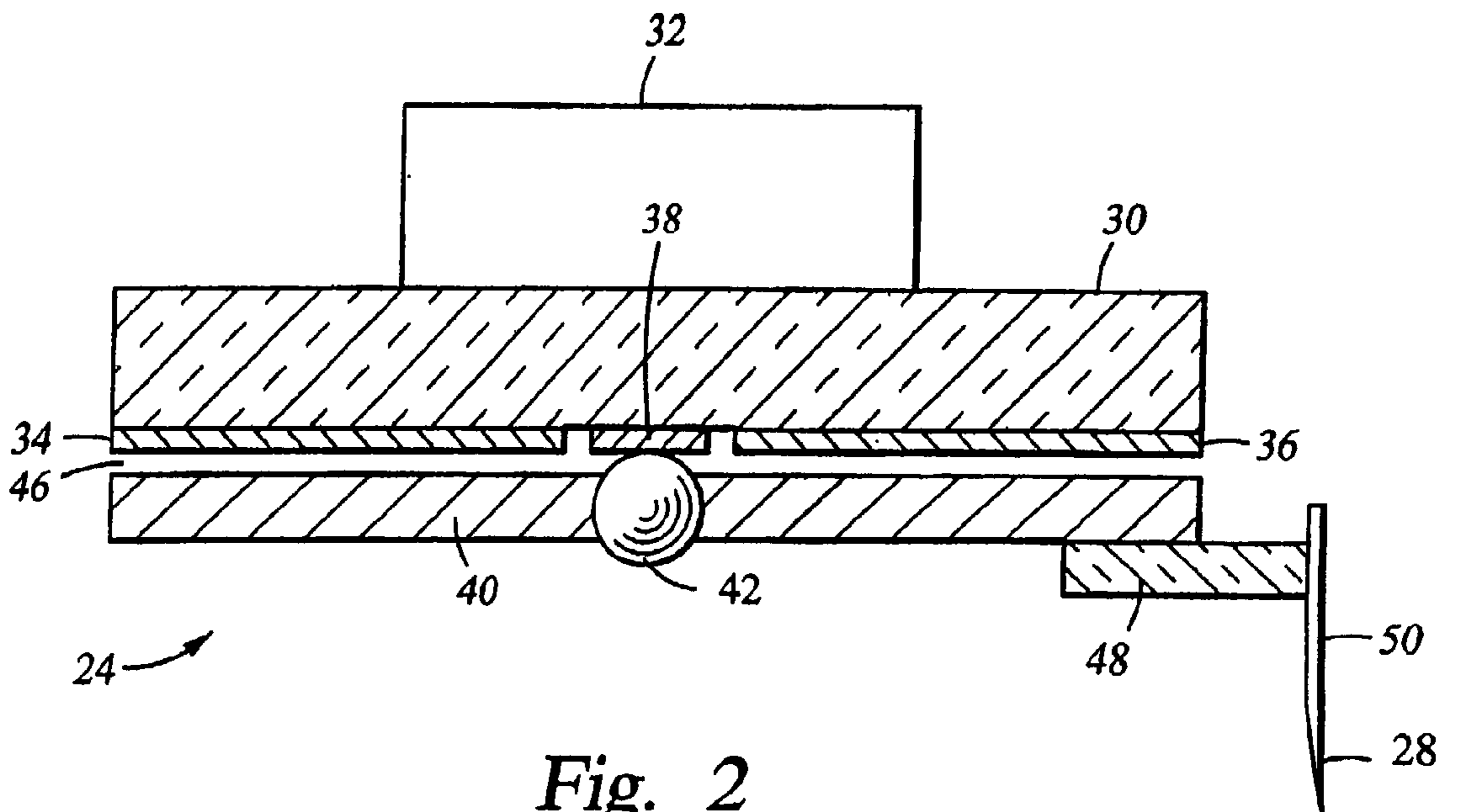


Fig. 2
(PRIOR ART)

Fig. 3

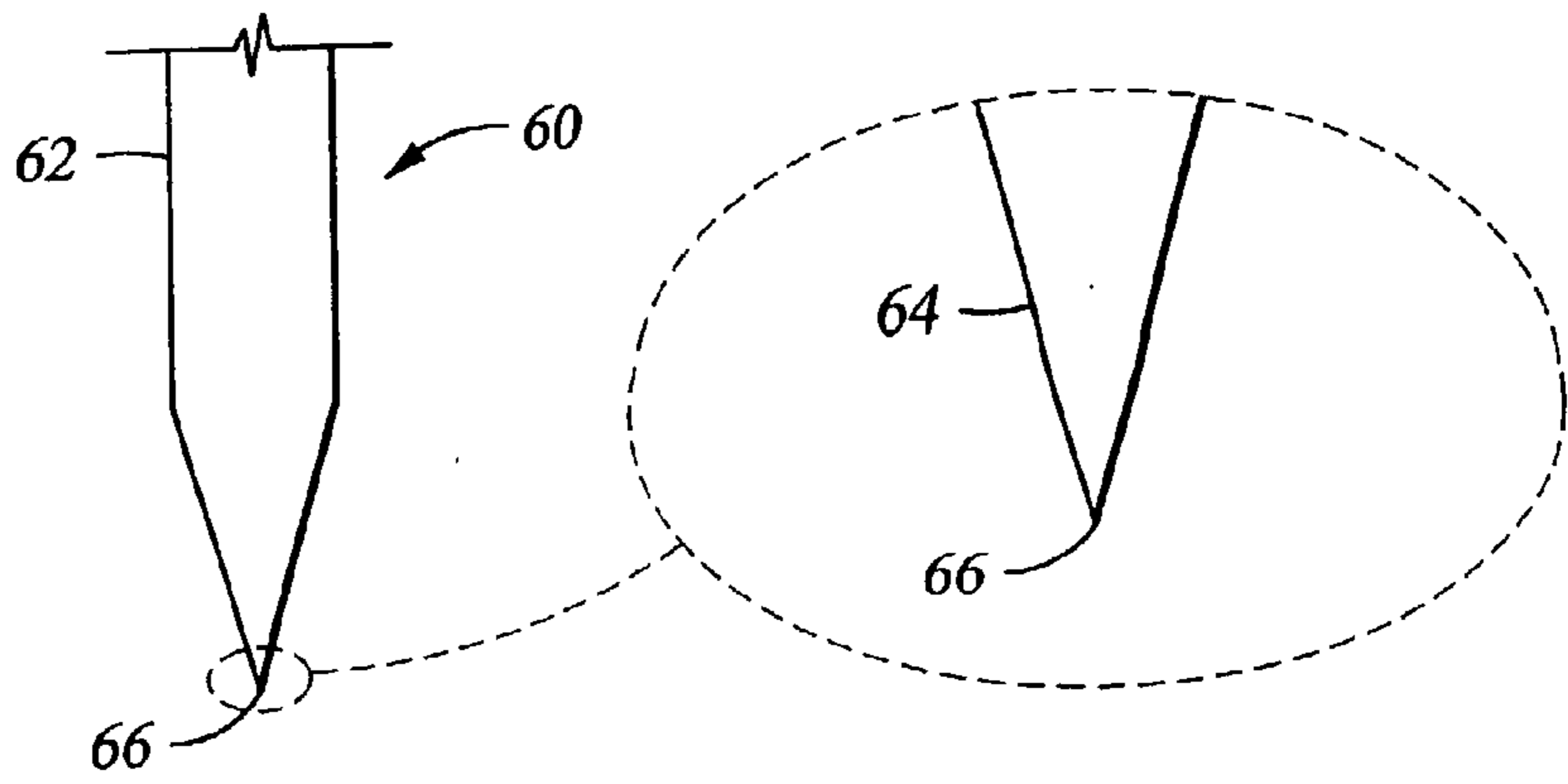


Fig. 4

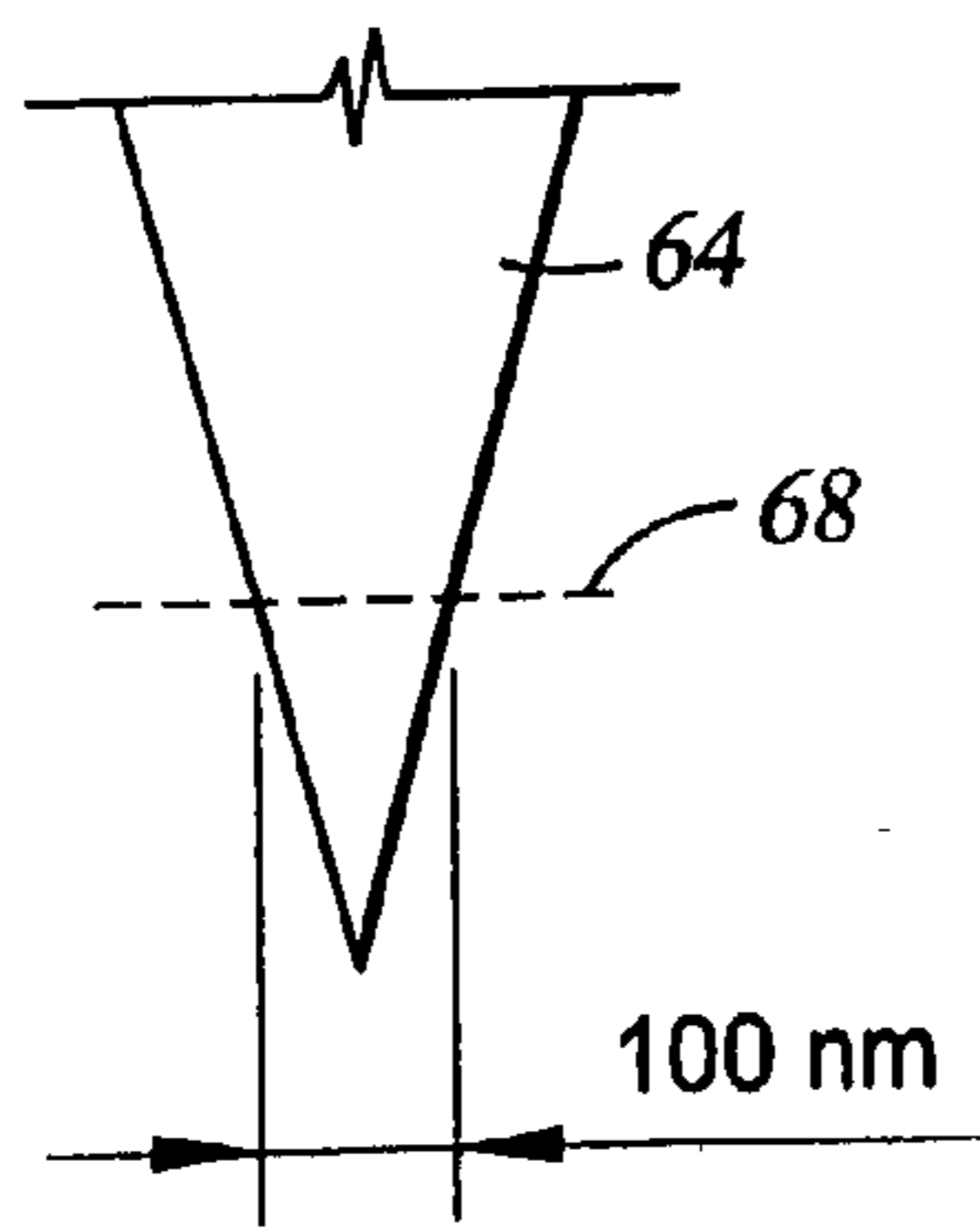


Fig. 5

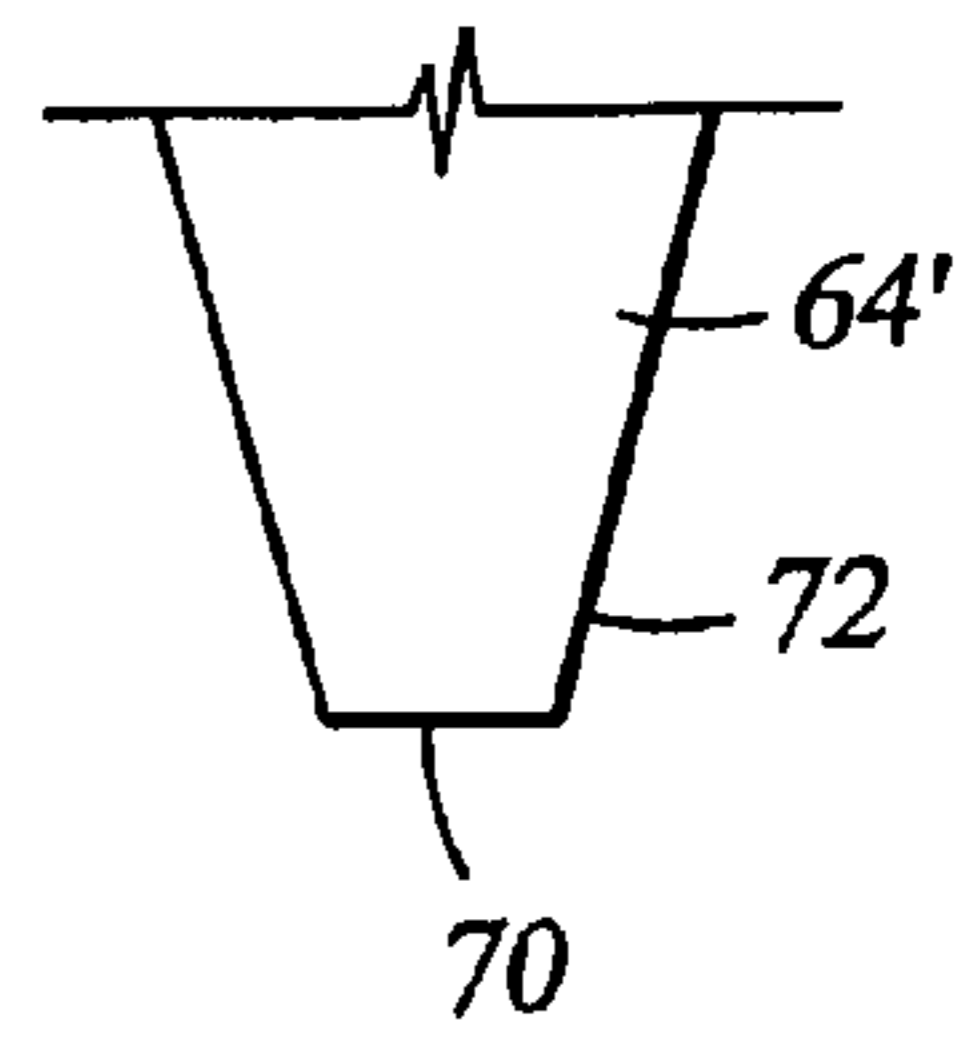


Fig. 6

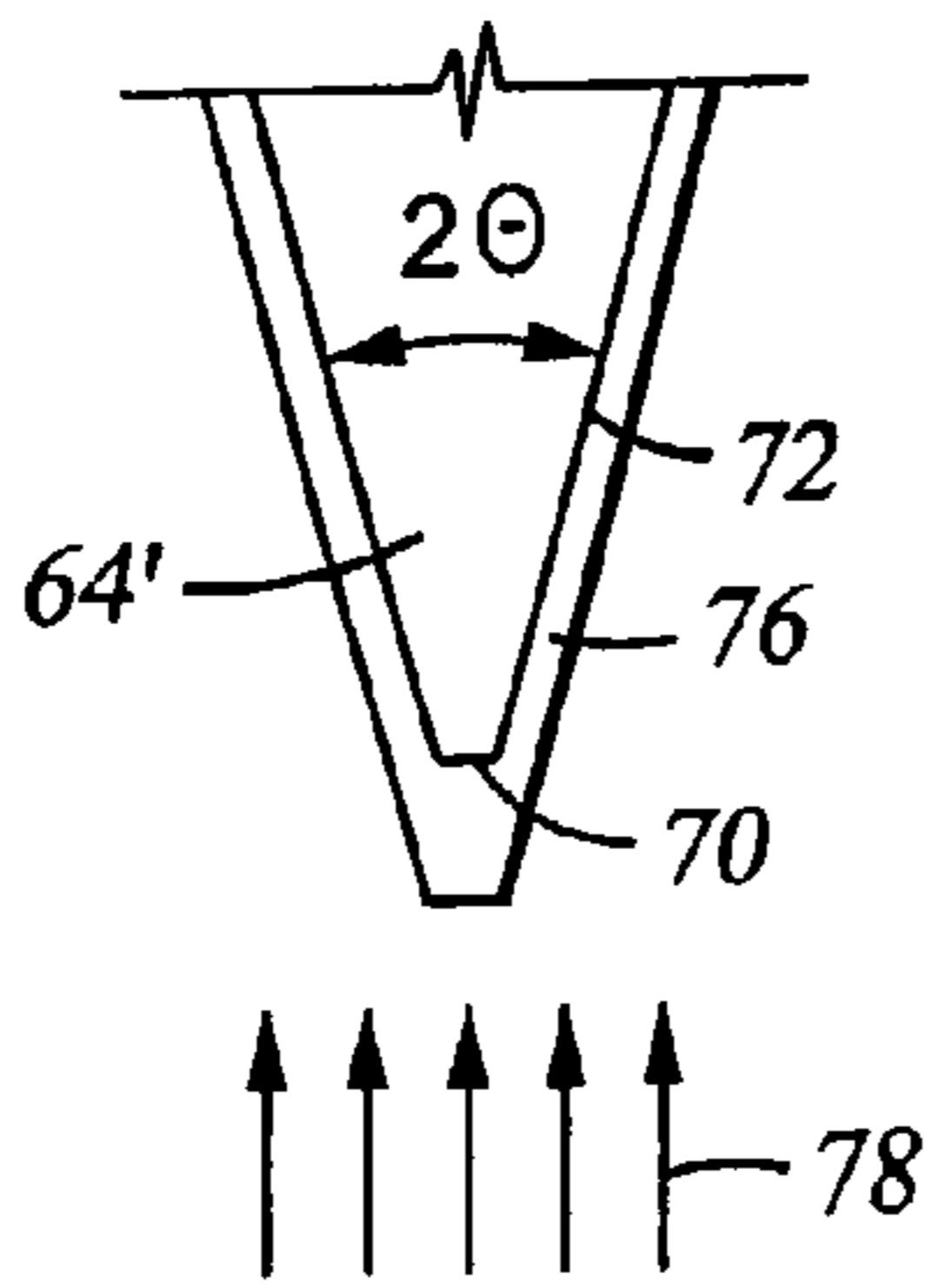


Fig. 7

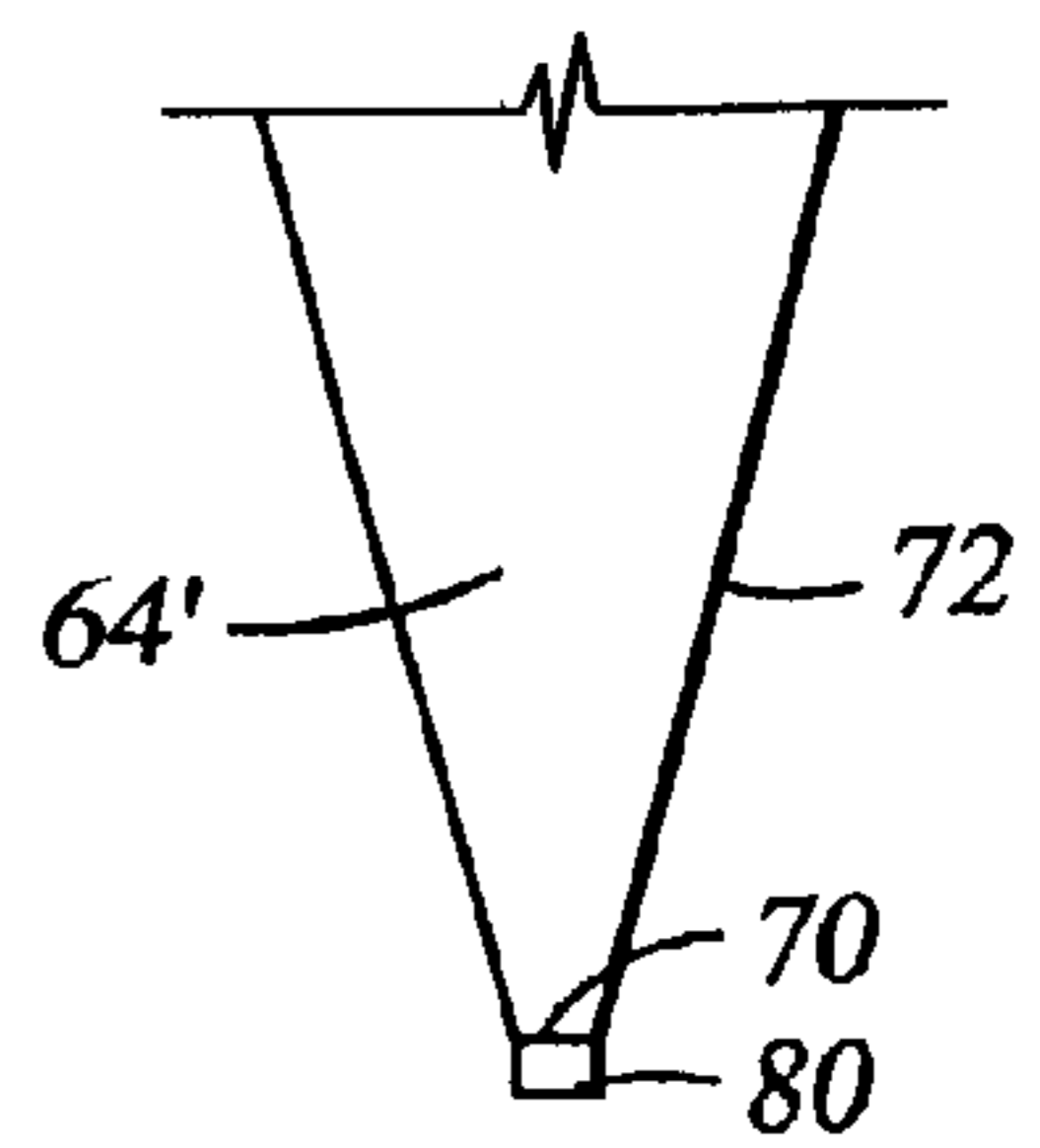


Fig. 8

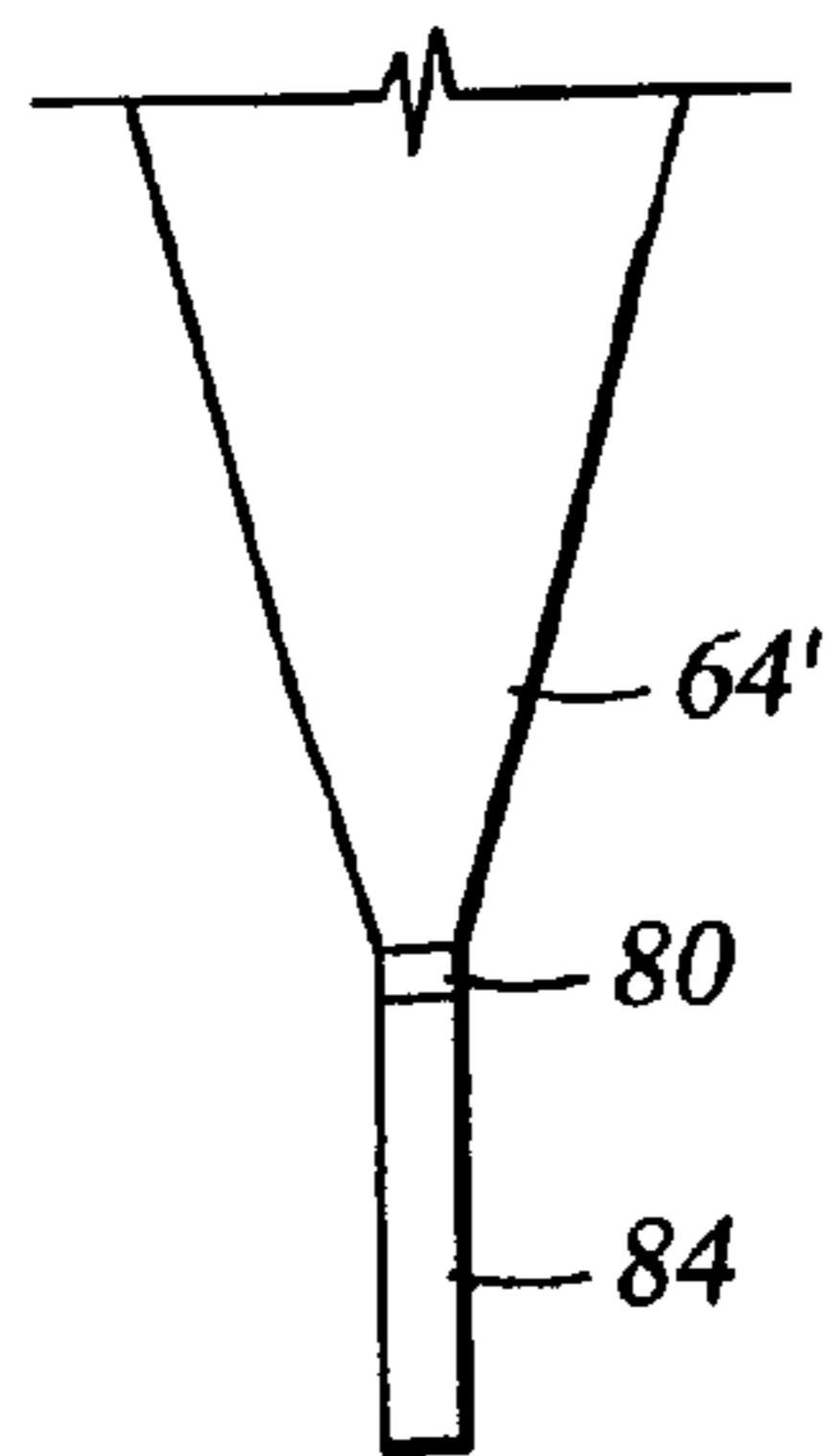
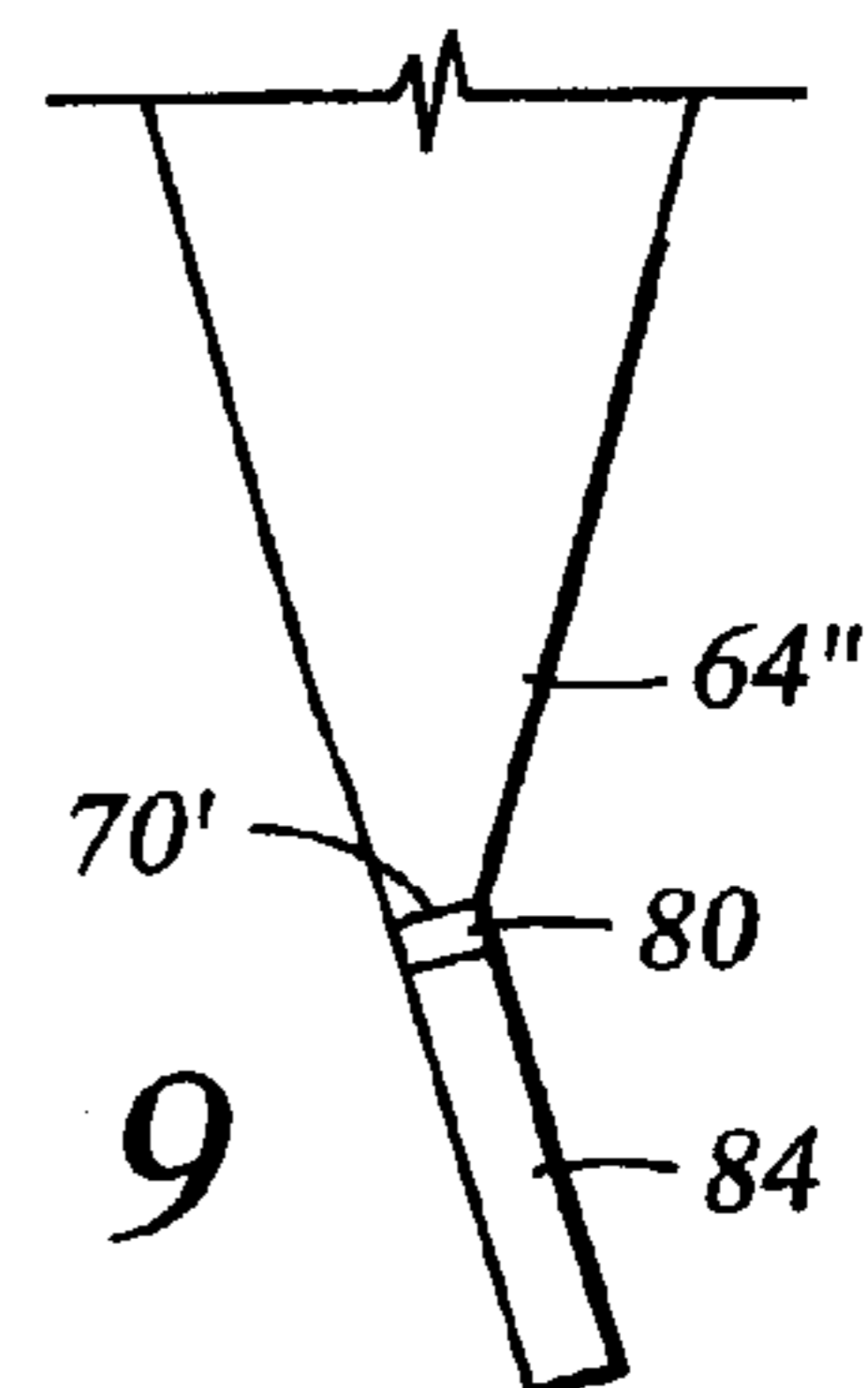


Fig. 9



CARBON NANOTUBE PROBE TIP GROWN ON A SMALL PROBE

FIELD OF THE INVENTION

[0001] The invention relates generally to mechanical probe tips such as those used in atomic force microscopy. In particular, the invention relates to a carbon nanotube grown directly on a pointed end of a probe.

BACKGROUND ART

[0002] Atomic force microscopes (AFMs) have been recently developed for mechanically profiling small features, for example, determining critical dimensions (CDs) of via holes in semiconductor integrated circuits. Such holes have depths of about 1 μm and widths which are being pushed to 180 nm and below. For detailed measurement of the feature, an exceedingly fine probe tip is disposed on the end of a cantilever overlying the feature. In the pixel mode of operation, the probe tip is successively positioned at points on a line above and traversing the feature being probed. The cantilever lowers the probe tip until it encounters the surface, and both the horizontal position and the vertical position at which the probe meets the surface are recorded. A series of such measurements provide the desired microscopic profile. An example of such an atomic force microscope is the Stylus Nanoprobe SNP available from Surface/Interface, Inc. of Sunnyvale, Calif. It employs technology similar to the rocking balanced beam probe disclosed by Griffith et al. in U.S. Pat. No. 5,307,693 and by Bryson et al. in U.S. Pat. No. 5,756,887.

[0003] Such a tool is schematically illustrated in the side view of FIG. 1. A few more details are found in U.S. patent application Ser. No. 09/354,528, filed Jul. 15, 1999 and incorporated herein by reference in its entirety. A wafer 10 or other sample to be is supported on a support surface 12 supported successively on a tilt stage 14, an x-slide 16, and a y-slide 18, all of which are movable along their respective axes so as to provide horizontal two-dimensional and tilt control of the wafer 10. Although these mechanical stages provide a relatively great range of motion, their resolutions are relatively coarse compared to the resolution sought in the probing. The bottom y-slide 18 rests on a heavy granite slab 20 providing vibrational stability. A gantry 22 is supported on the granite slab 20. A probe head 24 hangs in the vertical z-direction from the gantry 22 through an intermediate piezoelectric actuator 26 providing about 10 μm of motion in (x, y, z) by voltages applied across electrodes attached to the walls of a piezoelectric tube. A probe assembly with a tiny attached probe tip 28 projects downwardly from the probe head 24 to selectively engage the probe tip 28 with the top surface of the wafer 10 and to thereby determine its vertical and horizontal dimensions.

[0004] Principal parts of the probe head 24 of FIG. 2 are illustrated in the side view of FIG. 2. A dielectric support 30 fixed to the bottom of the piezoelectric actuator 26 includes on its top side, with respect to the view of FIG. 1, a magnet 32. On the bottom of the dielectric support 30 are deposited two isolated capacitor plates 34, 36 and two interconnected contact pads 38.

[0005] A beam 40 is medially fixed on its two lateral sides and is also electrically connected to two metallic and ferromagnetic ball bearings 42. The beam 40 is preferably

composed of heavily doped silicon so as to be electrically conductive, and a thin silver layer is deposited on it to make good electrical contacts to the ball bearings. The two ball bearings 42 are placed on respective ones of the two contact pads 38 and generally between the capacitor plates 34, 36, and the magnet 32 holds the ferromagnetic bearings 42 and the attached beam 40 to the dielectric support 30. The attached beam 40 is held in a position generally parallel to the dielectric support 40 with a balanced vertical gap 46 of about 25 μm between the capacitor plates 34, 36 and the beam 40. Unbalancing of the vertical gap allows a rocking motion of about 25 μm . The beam 40 holds on its distal end a glass tab 48 to which is fixed a stylus 50 having the probe tip 52 projecting downwardly to selectively engage the top of the wafer 10 being probed.

[0006] Two capacitors are formed between the respective capacitor plates 34, 36 and the conductive beam 40. The capacitor plates 34, 36 and the two contact pads 38, commonly electrically connected to the conductive beam 40, are separately connected by three unillustrated electrical lines to three terminals of external measurement and control circuitry. This servo system both measures the two capacitances and applies differential voltage to the two capacitor plates 34, 36 to keep them in the balanced position. When the piezoelectric actuator 26 lowers the stylus 50 to the point that it encounters the feature being probed, the beam 40 rocks upon contact of the probe tip 52 with the wafer 10. The difference in capacitance between the plates 34, 36 is detected, and the servo circuit attempts to rebalance the beam 40 by applying different voltages across the two capacitors, which amounts to a net force that the stylus 50 is applying to the wafer 10. When the force exceeds a threshold, the vertical position of the piezoelectric actuator 26 is used as an indication of the depth or height of the feature.

[0007] This and other types of AFMs have control and sensing elements more than adequate for the degree of precision for profiling a 1180 nm \times 1 μm hole. However, the probe tip presents a challenge for profiling the highly anisotropic holes desired in semiconductor fabrication as well as for other uses such as measuring DNA strands and the like. The probe tip needs to be long, narrow, and stiff. Its length needs to at least equal the depth of the hole being probed, and its width throughout this length needs to be less than the width of the hole. A fairly stiff probe tip reduces the biasing introduced by probe tips being deflected by a sloping surface.

[0008] One popular type of probe tip is a shaped silica tip, such as disclosed by Marchman in U.S. Pat. Nos. 5,395,741 and 5,480,049 and by Filas and Marchman in U.S. Pat. No. 5,703,979. A thin silica fiber has its end projecting downwardly into an etching solution. The etching forms a tapered portion near the surface of the fiber, and, with careful timing, the deeper portion of the fiber is etched to a cylinder of a much smaller diameter. The tip manufacturing is relatively straightforward, and the larger fiber away from the tip provides good mechanical support for the small tip. However, it is difficult to obtain the more desirable cylindrical probe tip by the progressive etching method rather than the tapered portion alone. Furthermore, silica is relatively soft so that its lifetime is limited because it is continually being forced against a relatively hard substrate.

[0009] One promising technology for AFM probe tips involves carbon nanotubes which can be made to spontaneously grow normal to a surface of an insulator such as glass covered with a thin layer of a catalyzing metal such as nickel. Carbon nanotubes can be grown to diameters ranging down to 5 to 20 nm and with lengths of significantly more than 1 μm . Nanotubes can form as single-wall nanotubes or as multiple-wall nanotubes. A single wall is a cylindrically shaped atomically thin sheet of carbon atoms arranged in a hexagonal crystalline structure with a graphitic type of bonding. Multiple walls bond to each other with a tetrahedral bonding structure, which is exceedingly robust. The modulus of elasticity for carbon nanotubes is significantly greater than that for silica. Thus, nanotubes offer a very stiff and very narrow probe tip well suited for atomic force microscopy. Furthermore, carbon nanotubes are electrically conductive so that they are well suited for scanning tunneling microscopy and other forms of probing relying upon passing a current through the probe tip. Dai et al. describe the manual fabrication of a nanotube probe tip in "Nanotubes as nanoprobe tips in scanning probe microscopy," *Nature*, vol. 384, 14 November 1996, pp. 147-150.

[0010] Typically, nanotubes suffer from the disadvantage that a large number of them simultaneously form on a surface producing either a tangle or a forest of such tubes, as is clearly illustrated by Ren et al. in "Synthesis of large arrays of well-aligned carbon nanotubes on glass," *Science*, vol. 282, 6 November 1998, pp. 1105-1107. The task then remains to affix one nanotube to a somewhat small probe tip support. Dai et al. disclose an assembly method in which they coat the apex of a silicon pyramid at the probe end with adhesive. The coated silicon tip was then brushed against a bundle of nanotubes, and a single nanotube can be pulled from the bundle. This method is nonetheless considered expensive and tedious requiring both optical and electron microscopes. Additionally, there is little control over the final orientation of the nanotube, certainly not to the precision needed to analyze semiconductor features. Cheung et al. describe another method of growing and transferring nanotubes in "Growth and fabrication with single-walled carbon nanotube probe microscopy tips," *Applied Physics Letters*, vol. 76, no. 21, 22 May 2000, pp. 3136-3138. However, they either produce poor directional control with a very narrow, single nanotube or require a complex transfer mechanism with nanotube bundles.

[0011] Ren et al. describe a method of growing isolated nanotubes in "Growth of a single freestanding multiwall carbon nanotube on each nanonickel dot," *Applied Physics Letters*, vol. 75, no. 8, 23 August 1999, pp. 1086-1088. They deposit 15 nm of nickel on silicon and pattern it into a grid of nickel dots having sizes of somewhat more than 100 nm. Plasma-enhanced chemical vapor deposition using acetylene and ammonia produces a single nanotube on each dot having an obelisk shape with a base diameter of about 150 nm and a sharpened tip. However, Ren et al. do not address the difficult problem of transferring such a nanotube, which they describe as being tightly bonded to the nickel, from the nickel-plated substrate to a probe end.

[0012] Cheung et al. disclose another method of growing isolated nanotubes in "Carbon nanotube atomic force microscopy tips: Direct growth by chemical vapor deposition and application to high-resolution imaging," *Proceedings of the National Academy of Sciences*, vol. 97, no. 8, 11

April 2000, pp. 3809-3813. They etch anisotropic holes in a silicon tip and deposit the catalyzing iron or iron oxide in the bottom of the holes. The carbon nanotubes grow out of the holes. However, growth in such restricted geometries is considered to be disadvantageous and to favor single-wall rather than multiple-wall nanotubes. Further, this method provides only limited control over the number and size of the nanotubes being grown.

[0013] Accordingly, a more efficient method is desired for forming a probe tip having a single carbon nanotube. Furthermore, the structure of the probe end and probe tip should facilitate assembly of the probe and contribute to its robustness.

SUMMARY OF THE INVENTION

[0014] A probe end is shaped to have sloping sides and a generally flat end, that is, in the shape of sloping mesa. The diameter of the mesa top is preferably in the range of 20 to 300 nm. Nickel or other material that catalyzes the growth of carbon nanotubes is directionally deposited onto the probe end. Because of the geometry, the thickness of the deposited nickel, as measured from the underlying surface, is greater on the mesa top than on the mesa sides. The nickel is then isotropically etched for a time sufficient to remove the nickel from the mesa sides but to leave sufficient nickel on the mesa top to catalyze the growth of a single carbon nanotube. Typically, the nanotube grows with a bottom diameter approximately equal to that of the nickel dot on top of the mesa.

BRIEF DESCRIPTION OF THE DRAWINGS

[0015] FIG. 1 is a schematic elevational view of a rocking beam atomic force microscope.

[0016] FIG. 2 is a cross-sectional side view of a portion of the atomic force microscope of FIG. 1.

[0017] FIG. 3 is a cross-sectional side view of a probe end having a tapered tip and available in the prior art, the figure including an exploded view of the sharp probe end.

[0018] FIG. 4 is a cross-sectional view showing the position of a sectioning of the probe end of FIG. 2.

[0019] FIG. 5 is a cross-sectional view showing the sectioned probe end.

[0020] FIG. 6 is a cross-sectional view showing the directional deposition of nickel or other catalyzing material.

[0021] FIG. 7 is a cross-sectional view showing a nickel dot formed only on the sectioned end of the probe end.

[0022] FIG. 8 is a cross-sectional view showing a nanotube grown on the nickel dot.

[0023] FIG. 9 is a cross-sectional view showing a second embodiment of the invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0024] The invention allows the fabrication of a single carbon nanotube on a narrow support structure well suited for easy attachment to a probe of an atomic force microscope (AFM) or other type of microprobe.

[0025] A support structure **60**, illustrated in side view in **FIG. 3**, is formed having a relatively massive upper portion **62** and a shaped tip **64** with a sharp point **66** having a curvature of less than about 50 nm. On the scale of probe tips, the upper portion **62** and the shaped tip **64** have a common longitudinal axis. The support structure **60** is illustrated with the orientation of its intended final use in a microscope overlying a sample being probed. The support structure **60** may be the quartz (silica) fiber of Marchman in which the shaped tip **64** is formed by placing an end of a 125 μm fiber in a bath of hydrofluoric acid (HF) overlaid by a layer of oil and leaving it in that position for a sufficiently long period that the fiber end is etched to a point. That is, the etching continues to completely etch away the cylinder of the Marchman tip. The point at which the HF completely dissolves the fiber defines the sharp point **66**. Alternatively, the shaped tip can be defined by polishing and grinding, particularly for sapphire fiber. The shaped tip **64** need not have a strictly conical shape, but it is advantageous that there be an sloping portion between the sharp point **66** and the relatively massive fiber **62** to provide mechanical stability in the finally assembled probe.

[0026] The support structure **60** is then subjected to focused ion beam (FIB) milling along a line **68**, illustrated in the cross-sectional view of **FIG. 4**, that in this embodiment is transverse to the axis of the support structure and passes through a predetermined width of the shaped tip **64**. The predetermined width closely corresponds to the width of the final carbon nanotube and may be, for example, 100 nm. FIB milling is a well known technique for micromachining and relies upon a focused beam typically of gallium ions to mill structures with a resolution down to about 5 nm. Such a system is the FIB 200TEM available from FEI Company of Hillsboro, Oreg. Other milling techniques could be used, but FIB milling is effective and economical.

[0027] The milling produces a shaped tip **64'**, illustrated in the cross-sectional view of **FIG. 5**, having a flat end **70** and sloping sidewalls **72**. Then, as illustrated in the cross-sectional view of **FIG. 6**, a film **76** of nickel or other catalyzing metal is then directionally deposited onto the probe tip **64'**, preferably by sputtering metal atoms along the longitudinal axis of the shaped tip **64'**. The thickness of the deposition, as measured along the longitudinal axis, is substantially constant between the area of the flat end **70** and the sloping sidewalls **72** of the shaped tip **64'**. However, the thickness, as measured at a perpendicular to the underlying surface, is substantially thicker in the area overlying the flat **70** than in the areas overlying the sloping sidewalls **72**. The effect is primarily geometric. If the probe tip has a tip angle 2θ and the deposition is totally anisotropic, then the sidewall thickness is $\sin\theta$ times the end thickness. For example, if $2\theta=31.3^\circ$, then the sidewall thickness is 27% of the end thickness. The sputtering may be performed in an ion sputtering system using a nickel target. Such a system is the Model 681 High Resolution Ion Coater from Gatan of Pleasanton, Calif. Other types of deposition are possible, such as molecular beam techniques usually associated with molecular beam epitaxy.

[0028] As illustrated in the cross-sectional view of **FIG. 7**, the nickel-plated shaped tip **64'** is subjected to isotropic etching of the nickel for a time just sufficient to remove the nickel from the tip sidewalls **72** but leaving a nickel dot **80** over the tip end **70**. A minimum thickness of approximately

15 to 20, preferably 30 to 40 nm, of nickel is desired in the area of the nickel dot **80** to catalyze the nanotube growth. Assuming the lower value of 15 nm and a tip angle 2θ of 31.3° , about 27 nm of nickel needs to be anisotropically deposited over the area of the tip end **70** to account for the end nickel being thinned during removal of the sidewall nickel, which has an initial thickness of 7 nm. The etching time obviously needs to be controlled so that it continues long enough to remove the sidewall nickel while leaving sufficient of the end nickel.

[0029] It may be advantageous to oxidize the nickel prior to etching, and in any case nickel will typically have an oxidized surface layer upon any exposure to air. Any number of isotropic wet etchants for nickel and nickel oxide are known, as tabulated in *CRC Handbook of Metal Etchants*, eds. Walker et al., CRC Press, 1991, pp. 857-875 and include dilute nitric and sulfuric acids for nickel and ammonium hydroxide for nickel oxide.

[0030] The nickel dot **80** provides a small catalyzing area for the growth of a single carbon nanotube **84** illustrated in cross-sectional view in **FIG. 8**. Ren et al. and Cheung et al. describe the process for selective growth of nanotubes in the above cited references. The diameter of the nanotube **84** corresponds generally to the diameter or average lateral extent of the flattened end **70** of the shaped tip **64'**. For a non-circular end **80**, the nanotube diameter is approximately equal to the minimum lateral extent of the end.

[0031] It has proven difficult to control the length to which nanotubes grow. Accordingly, it may be necessary to perform an additional step of cutting the carbon nanotube to a prescribed length, for example, by FIB milling.

[0032] The probe structure illustrated in **FIG. 8** includes a relatively rugged support structure **62**, illustrated in **FIG. 3**, which is ready to be mounted onto the probe of the AFM or other microscope using a stylus.

[0033] The method described above requires that the sidewalls of the shaped tip slope away from the tip end. To achieve the required differential but isotropic etching, the slope is preferably at least 60° from the plane. The differential coating works even with a slope of 90° , that is, vertical sidewalls. Such a shape may be produced by FIB milling, for example, a cylinder having a diameter of 100 nm or a similarly sized rectangular post into the tip **66** at the end of the conical tip **64** prior to nickel deposition.

[0034] The embodiment described above produces a carbon nanotube extending along the axis of the conical tip. However, in another embodiment illustrated in the cross-sectional view of **FIG. 9**, a shaped tip **64''** is formed by milling the conical tip **64** to have an inclined flat end **70'**. That is, the flat end **70'** is not perpendicular to the axis of the fiber or the shaped tip **64''**. The deposition of the nickel **80** and the growth of the carbon nanotube **84** are then performed as described above. This configuration is particularly useful for probing very narrow features at the bottom edges of somewhat wider holes, for example, punch through occurring at the corner of a narrow trench, which occurs in semiconductor processing.

[0035] Although the above description includes a support structure formed from a quartz fiber, it is known that the preferential etching of $\langle 111 \rangle$ planes of $\langle 001 \rangle$ -oriented silicon can form pyramids having an apex angle of

$2\theta=70.5^\circ$, which is equivalent to a slope of 54.74° from the plane. Often a thin layer of silicon nitride is coated on the silicon pyramid. After cutting, a square end surface is formed. The underlying silicon is very easily mounted to the AFM probe. Cheung et al. describe a method of cutting a flat surface at the pyramid apex by dragging the pyramid across a hard surface. Such a surface may not be completely flat but most probably deviates by less than 10° from a planar surface. The support structure may be composed of other materials.

[0036] Nickel is not the only possible material for catalyzing nanotube growth. Iron and iron oxide have been used. Cobalt has been suggested as a catalyst. All these catalyzing materials can be used with the process described above.

[0037] None of the steps described above are particularly difficult or problematic. FIB milling has been shown to be easily and reliably performed. Thereby, probe tips produced according to the invention are relatively economical. Further, the sputter coating and isotropic etching can be simultaneously performed upon a large number of probe tips mounted on a common tip holder, thereby further improving the efficiency of the fabrication method of the invention.

[0038] The carbon nanotubes produced according to the invention are grown on substantially planar and well defined areas of nickel or other catalyzing material. Thereby, the tip diameter and orientation are well controlled. Carbon nanotube tips have the well known characteristics of high stiffness and toughness to wear under continued use.

What is claimed is:

1. A method of forming a probe tip, comprising the steps of:

providing a member comprising a shaped tip having sidewalls and extending along an axis;

cutting a flat surface in said shaped tip;

anisotropically depositing a catalytic material onto said flat surface and onto said sloping sidewalls;

directionally etching said catalytic material to remove said catalytic material from said sidewalls while leaving a thickness of said catalytic material on said flat surface; and

growing a carbon nanotube on a portion of said catalytic material remaining on said flat surface in a process catalyzed by said catalytic material.

2. The method of claim 1, wherein said flat surface has a minimum lateral size of between 15 and 300 nm.

3. The method of claim 1, wherein said catalytic material comprises nickel.

4. The method of claim 1, wherein said catalytic material comprises iron.

5. The method of claim 1, wherein said member comprises silicon oxide.

6. The method of claim 1, wherein said member is formed from silica fiber.

7. The method of claim 6, wherein said member has said ends formed into said fiber and said sidewalls slope from an axis of said fiber.

8. The method of claim 6, wherein said planar end is cut to be non-perpendicular to an axis of said fiber.

9. The method of claim 1, wherein said cutting step cuts said sidewalls into said member to be parallel to each other.

10. The method of claim 1, wherein said member comprises silicon.

11. The method of claim 1, wherein said shaped tip has a pyramidal shape.

12. The method of claim 1, wherein said anisotropic coating step comprises sputtering.

13. The method of claim 1, wherein said cutting step comprises focused ion beam milling.

14. The method of claim 1, further comprising cutting said carbon nanotube to reduce its length.

15. The method of claim 14, wherein said cutting said carbon nanotube comprises focused ion beam milling.

16. A probe tip, comprising:

a support including a shaped tip having a planar end of minimum lateral extent of between 15 and 300 nm and sidewalls sloping from said planar end;

a catalyzing layer of material capable of catalyzing growth of carbon nanotubes formed on said planar end but not on said sidewalls; and

a single carbon nanotube formed on said catalyzing layer.

17. The probe tip of claim 16, wherein said nanotube is a multi-wall nanotube.

18. The probe tip of claim 16, wherein said material comprises metallic nickel.

19. The probe tip of claim 15, wherein said material comprises nickel oxide.

20. The probe tip of claim 15, wherein said material comprises metallic iron or iron oxide.

21. The probe tip of claim 15, wherein said sidewalls slope from said planar end by between 60° and 90° .

22. The probe tip of claim 15, wherein said catalyzing layer has a thickness of at least 15 nm.

23. An atomic force microscope including the probe tip of claim 15 and a vertical actuator, wherein said actuator causes said probe tip to encounter a surface being probed.

* * * * *