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(54) **MULTI-LAYER POLYMER FOAM FILM FOR PACKAGING APPLICATIONS AND THE METHOD OF MAKING THE SAME**

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(57) **ABSTRACT**

A multilayer foam film suitable for direct and non-direct food contact and aseptic packaging application is disclosed.

23 Claims, No Drawings

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**MULTI-LAYER POLYMER FOAM FILM FOR
PACKAGING APPLICATIONS AND THE
METHOD OF MAKING THE SAME**

RELATED APPLICATION

This application is a continuation-in-part of the U.S. patent application Ser. No. 16/875,198 filed on May 15, 2020 and which claims priority to U.S. provisional patent application Ser. No. 62/849,329 filed on May 17, 2019, which are both incorporated herein by reference in their entireties.

FIELD

This invention relates to a multilayer polymer foam film (e.g., comprising high density polyethylene (HDPE)), which may be used for paper replacement applications in the aseptic packaging industry.

BACKGROUND

Paperboards consumption for packaging applications accounts for almost one-third of the total packaging market. For the direct food contact packaging, paper boards work safely with a barrier coating of some form. Conventionally, for the food packaging applications where the barrier properties are essential, the paper boards are paraffin wax coated or laminated with a polymer film, which is usually polyethylene. For the shelf-stable products that are stored at room temperature, and the packaging is done aseptically followed by hermetic sealing, oxygen barrier property is essential. The advent of paper-foil-plastic laminated containers, e.g., Tetrahedron in 1959, was an inflection point in packaging industries where it could be replaced with metal cans and glass containers. So, typically a layer of a metalized polymer film or aluminum film is incorporated in the structure of the paperboard. This can cause a significant recycling issue because the vast majority of the recycling sites are deficient in infrastructure that can provide a certain recycling technology. There has been cumulative popularity and interest for the sterilized and pasteurized products that are being packaged aseptically which eliminates refrigeration and prevents spoilage without using preservatives, for example, milk, baby foods, tomato products, broths, soups, vegetables, desserts, liquid egg, yogurt, dressings, etc. So, with the vast demand growth in food packaging in emerging markets, it would be desirable to produce in a lightweight recyclable polymeric film with improved oxygen and moisture barrier properties that possesses surface quality for printing and preprinting shelf life, bending stiffness values comparable to the paperboards used in packaging, and sufficient barrier properties, all of which may be essential attributes for a product to replace the kinds of paperboard currently being used in packaging industries. Moreover, the mentioned product can address the wicking issues of coated paperboards.

One of the foremost issues during the production of flexible aseptically packaged products, made of a multilayer sheet or film, is the defects in the packages due to the occurrence of physical damages of any form to the sheet and specifically the oxygen barrier layers, for example, in the form of micro-cracks that might be initiated and then propagate during the creasing, scoring, piercing, punching, or folding process. For instance, these cracks happen typically in the aluminum layer, metalized layer, or even Ethylene vinyl alcohol (EVOH) layers that are conventionally

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included in the structure of the multilayer sheet and film that are currently being used in the packaging industry. These defects can deteriorate the integrity of the oxygen barrier properties of the whole package resulting in the decline in the shelf life time of the product. So, it would be beneficial to innovate a method to protect the barrier layer in the multilayer sheet or film from getting physical damages when it undergoes the foresaid processes.

SUMMARY

A multilayer polymer foam film which, for example, may be used for aseptic packaging application is described herein.

As described further below, in some embodiments, the multilayer films retain their oxygen transmission rate (OTR) properties after a creasing, folding or scoring step. That is, the creased, folded or scored multilayer film has an OTR similar to that of an identical multilayer film prior creasing, folding or scoring. This can be an advantage over conventional multilayer films that may experience increases in OTR, for example, as a result of physical damage during creasing, folding or scoring.

In some embodiments, the film can have a very smooth surface resulting in superior printing quality and high enough bending stiffness to replace paper boards. The film may be recyclable and lightweight.

In one aspect, a creased, folded or scored multilayer foam film is provided. The film comprises a foam layer including a plurality of cells. At least 10% of the cells are closed cells. The film further comprises two solid skin layers comprising HDPE on each side of the foam layer. The film further comprises a solid layer comprising ethylene vinyl alcohol (EVOH). The foam layer is between one of the solid skin layers and the solid layer comprising EVOH. The film has an overall thickness equal to or greater than 8 mils. The ratio of the oxygen transmission rate of the creased, folded or scored film in $\text{cc}/\text{m}^2/24 \text{ hr}$, according to ASTM D3985, over that of an identical film prior to creasing, folding or scoring is less than 1.1.

In another aspect, a method of making a creased, folded or scored multilayer film is provided. The method comprises co-extruding a foam layer, two solid skin layers comprising HDPE and one solid layer comprising ethylene vinyl alcohol (EVOH) to form a multilayer film. The foam layer includes a plurality of cells, wherein at least 10% of the cells are closed cells. The foam layer is between one of the solid skin layers and the layer comprising EVOH. The film has an overall thickness equal to or greater than 8 mils. The method further comprises creasing, folding or scoring the multilayer film. The oxygen transmission rate value of the creased, folded or scored film in $\text{cc}/\text{m}^2/\text{day}$, according to ASTM D3985 does not increase more than 10% of the oxygen transmission rate value of the multi-layer film prior to creasing, folding or scoring in $\text{cc}/\text{m}^2/\text{day}$, according to ASTM D3985.

Other aspects, embodiments, advantages, and features will become apparent from the following detailed description.

DETAILED DESCRIPTION

The singular forms “a,” “an,” and “the” include plural referents unless the context clearly dictates otherwise.

All ranges disclosed herein are inclusive of the recited endpoint and independently combinable (for example, the range of the bending stiffness in Taber unit configuration

from 18 to 100” is inclusive of the endpoints, 18 and 100, and all the intermediate values. In the same context, for example, the overall thickness of greater than 8 mils is inclusive of the endpoint, 8 mils.)

As used herein, approximating language may be applied to modify any quantitative representation that may vary without resulting in a change in the basic function to which it is related. Accordingly, a value modified by a term or terms, such as “about” and “substantially,” may not be limited to the precise value specified. The modifier “about” should also be considered as disclosing the range defined by the absolute value of the two endpoints. For example, the expression “from about 0.05 to about 15” also discloses the range “from 0.05 to 15”.

As used herein, the term “lightweight” refers to the bulk density value of the products described herein being less than, or equal to, the density of their solid counterpart made from the associated base virgin resin, or the density of the associated base virgin resin. In a similar context, it refers to the bulk density value of the products described herein being less than, or at least equal to, the density of the paperboards with the same thickness or with the same weight values per unit area in gr/m^2 . For example, bulk density values of the products of this invention can be less than $0.962 \text{ gr}/\text{cm}^3$ which is less than the density value of the associated base virgin resin of $0.962 \text{ gr}/\text{cm}^3$, or less than the bulk density value of $0.962 \text{ gr}/\text{cm}^3$ of its solid counterpart made from the associated base virgin resin.

The present disclosure relates to multilayer lightweight polyethylene foam film suitable to be used in all sorts of aseptic packaging; packaging of all sorts of oxygen-sensitive products, packaging of pasteurized products; packaging of dry food products such as biscuits, cookies, cereals, tea, coffee, sugar, flour, dry food mixes, chocolates, sugar confectionaries, pet food; packaging of frozen foods such as chilled foods and ice creams; packaging of cooked and precooked products and foods; backing board for fresh products such as vegetables, fruits, meat and fishes; packaging of baby foods; packaging of all kinds of desserts; packaging of liquid food and beverages such as broths, soups, juice drinks, milk and all sorts of products derived from milk, concentrates, all kinds of dressing, liquid eggs, tomato products; and packaging of all kinds of laundry detergents, shampoos, and body washes; making all sorts of pouches to include SUP, sachets, and packaging of pet foods.

The abovementioned examples do not put any limitation on the application of the products of this disclosure, and other applications may be possible.

One of the rationales behind the production of the synthetic lightweight films described herein and material selection for paperboard replacement is to address the recyclability, and to avoid the drawbacks of using the wax-coated paper boards, metalized films, and the films and sheets with an aluminum layer all of which are either not recyclable or cannot be recycled easily; although in reality the vast majority of the consumers intuitively believe that the abovementioned products, such as aseptically-packaged milk boxes or long-shelf life beverage boxes, are recyclable.

Herein a recyclable lightweight multilayer film is disclosed which, in some embodiments, comprises no less than five layers, e.g., seven layers, to be a replacement for paper boards that are being used in packaging industries, e.g., for aseptic packaging applications, and for direct and non-direct food contact packaging application. The film comprises high-density polyethylene (HDPE) wherein at least one layer, excluding the solid skin layers, has a cellular structure. In some embodiments, at least 10% of the cells are closed-

cell; in some embodiments, more than 50% of the cells are closed cells; and, in some embodiments, more than 75% of the cells are closed cells. In some embodiments, 100% of the cells are closed cells. As used herein, a “closed cell” refers to a cell that has cell walls that completely surround the cell with no openings such that there is no interconnectivity to an adjacent cell. In some embodiments, the film comprises at least one solid layer containing EVOH, each of which located somewhere between the foam layer and solid layer, or between two of the solid layers. In some embodiments, the film comprises at least one foam layer and two solid skin layers, and one or more solid layers comprising EVOH, wherein the said foam layer is located between the skin layer and the layer comprising EVOH.

In some embodiments, the mass concentration of the EVOH in every unit area of the multilayer film is less than 5 percent of the mass of the unit area of the film. In some embodiments, the mass concentration of the EVOH in every unit area of the multilayer film is less than 10 percent of the mass of the unit area of the film. In some embodiments, the mass concentration of the EVOH in every unit area of the multilayer film is less than 5 percent of the mass of the unit area of the film. In some other embodiments, the mass concentration of the EVOH in every unit area of the multilayer film is less than 2 percent of the mass of the unit area of the film.

Furthermore, in some embodiments, the bending stiffness of the disclosed multilayer foamed film product could be improved over their solid counterparts to fulfill the property requirement in packaging industries. This could be done first and foremost by the inclusion of one or more cellular layer in the core of the multilayer film or between two solid skin layers, an accurate tune and alteration of the thickness of the cellular layer as well as fine-tuning the thickness of the solid skin layers. Generally, at the same thickness, a solid film of polyethylene can hardly possess bending stiffness values that paperboards can offer. This is due to the high degree of fiber alignment in paperboard which can significantly enhance the bending stiffness. In addition, it might be due to higher inherent stiffness of the individual fibers in the paperboard compared to the polymer chains in the polymeric film.

In general, HDPE owns a relatively low water vapor transmission rate of about $0.3\text{-}0.5 \text{ (g/100 in}^2\text{/24 hr)}$. Embodiments of the multilayer foamed film products described herein can exhibit significantly higher moisture barrier properties compared to its solid counterparts with the same value of mass per unit area (in gram per meter squared). Also, embodiments of the multilayer foamed film products described herein can exhibit an enhanced oxygen barrier property.

Also, one of the issues in industrial-scale use of the polymeric packages, which can be a crucial factor in the efficient and cost-effective packaging process, is the ability of them to be de-nested quickly and freely. De-nesting problems are typically due to the friction and static charge. Embodiments of the multilayer foam films described herein can exhibit an anti-static and low friction behavior by manipulating the skin layer’s structure and by the inclusion of appropriate amounts of slip agents, anti-block and anti-static agent into the solid skin layer.

In some embodiments, one of the steps for making the disclosed product is how the bending stiffness may be controlled and enhanced by the inclusion and controlling the thickness of the core cellular layer, or the cellular layers between the two skin layers, and fine-tuning the solid skins, as well as how the surface smoothness has been enhanced

significantly by adding a tiny amount of supercritical blowing agent. Moreover, how the unique structure and layer combination has resulted in a high barrier property without the inclusion of an aluminum or metalized barrier layer. That is, the film product may be free of any metal (e.g., aluminum) barrier layer.

In some embodiments, a blown film process may be used where the head pressure of the extruder can go high because of a very narrow gap that benefits the nucleation of cells in the foam layer. Using such a technique, the melt fracture should be avoided, and the resin should have excellent thermal stability and high enough melt strength. Typically, film manufacturers capitalize on a blend of a low-density polyethylene (LDPE) and a linear low-density polyethylene (LLDPE), while the blend is an immiscible blend in many cases, wherein LDPE can improve the processing ability and ductility while the LLDPE can enhance the modulus and strength. In some embodiments, all layers of the described multilayer film comprise HDPE and, in some cases, the polymeric material in one or more of these layers consists essentially of HDPE and, in some cases, the polymeric materials in at least one of the solid layers, excluding the solid skin layers, comprises EVOH. In one embodiment, at least one layer of the multilayer film can comprise LDPE.

In some embodiments, the multilayer film can be comprised of nine layers; in some embodiments, seven layers; and, in some embodiments, five layers.

For example, a five-layer film may comprise a foam core layer (e.g., comprising HDPE) and at least two solid layers (e.g., comprising HDPE), each one on respective opposite sides of the core layer, and at least one solid layer (e.g., comprising EVOH), each one between the foam layer and solid skin layer. In one embodiment, the five-layer film may comprise a solid core layer (e.g., comprising EVOH) and at least two solid layers (e.g., comprising HDPE), each one on respective opposite sides of the core layer, and at least two foam layers (e.g., comprising HDPE), each one between the foam layer and solid skin layer. In some embodiments, a five layer film may have a layer structure ABCBA (i.e., with layers A being the two outermost (skin) layers, layers B being in contact with respective A layers and layer C, and layer C being the middle layer). For example, layers A may be solid skin layers (e.g., comprising HDPE), layers B may be foam layers (e.g., comprising HDPE) and layer C may be an EVOH (e.g., solid) layer.

In one case, a seven-layer foam film comprises a foam core layer (e.g., comprising HDPE) in the middle with two solid skin layers (e.g., comprising HDPE) on each opposite side of the core layer, and at least one solid layer (e.g., comprising EVOH), each one between the foam layer and solid skin layer. In another case, a seven-layer foam film comprises a solid core layer (e.g., comprising EVOH) in the middle with two solid skin layers (e.g., comprising HDPE) on each opposite side of the core layer, and at least one foam layer (e.g., comprising HDPE), each one between the solid core layer and the solid skin layer. In some embodiments, a seven layer film may have a layer structure ABCDCBA (i.e., with layers A being the two outermost (skin) layers, layers B being in contact with respective A layers and respective C layers, layers C being in contact with respective layers B and layer D and layer D being the middle layer). For example, layers A may be solid skin layers (e.g., comprising HDPE), layers B may be foam layers (e.g., comprising HDPE), layer C may be a solid tie layer (e.g., comprising HDPE) and layer D may be an EVOH (e.g., solid) layer.

In another embodiment, a nine-layer foam film comprises a foam core layer (e.g., comprising HDPE) in the middle

with two solid skin layers (e.g., comprising HDPE) on each opposite side of the core layer, and at least one solid layer (e.g., comprising EVOH), each one between the foam layer and solid skin layer. In another embodiment, a nine-layer foam film comprises a solid core layer (e.g., comprising EVOH) in the middle with two solid skin layers (e.g., comprising HDPE) on each opposite side of the core layer, and at least one foam layer (e.g., comprising HDPE), each one between the solid core layer and solid skin layer. In some embodiments, a nine layer film may have a layer structure ABCDEDCBA (i.e., with layers A being the two outermost (skin) layers, layers B being in contact with respective A layers and respective C layers, layers C being in contact with respective layers B and respective layers D, layers D being in contact with respective layers C and layer E, and layer E being the middle layer). For example, layers A may be solid skin layers (e.g., comprising HDPE), layers B may be solid tie layers (e.g., comprising HDPE), layers C may be (e.g., solid) EVOH layers, layers D may be solid tie layers (e.g., comprising HDPE) and layer E may be a foam layer (e.g., comprising HDPE).

In another embodiment, the multilayer film, which can be five, seven, or nine layers, comprises at least one foam layer and two solid skin layers, and at least one solid layer (e.g., comprising EVOH). In another embodiment, the multilayer film, which can be five, seven, or nine layers, comprises at least one solid layer, comprising EVOH, each of which located between the foam layer and solid layer, or between the two solid layers.

In some embodiments, the multilayer film described herein comprises multiple layers, e.g., from 3 layers to 19 layers, comprising at least one foam layer and one or more solid layers containing EVOH. In some other embodiments, the multilayer film described herein comprises multiple layers, e.g., from 3 layers to 19 layers, comprising at least one solid layer containing EVOH.

It should be understood that other layer configurations may be possible.

In one embodiment, the process to produce the described multilayer films may utilize a very small and precise amount of supercritical gas, for example, below 0.1 wt %, as a processing aid and blowing agent. In some embodiments, other gas concentrations, e.g., more than 0.1 percent by weight maybe possible. Such supercritical gas may be injected into the molten polymer at a high pressure, for example, greater than 34 bar, inside an efficient and effectual mixer, e.g., cavity transfer mixer, as an extension to the extruder's barrel. The supercritical blowing agent used in the process can be either nitrogen, carbon dioxide, or a mixture of nitrogen and carbon dioxide. In some embodiments, the supercritical blowing agent can be introduced inside the mixing section of the extruder at the injection pressure greater than or equal to 34 bar; in some cases, greater than or equal to 70 bar; in some cases, greater than or equal to 240 bar, and, in some cases, greater than or equal to 380 bar. The temperature of the mixer could be accurately controlled within $\pm 1^\circ$ C. The inclusion of a tiny amount of gas can offer a few important advantages in the process and, for example, blown film extrusion processes. For example, the gas can reduce the back pressure which allows processing at higher throughput and can delay any bubble instability. Therefore, melt fracture could be reduced significantly. Also, the gas can enhance the processing ability of the HDPE, and to serve as a physical blowing agent with the presence of a nucleating agent in the layer that has a cellular structure. The addition of the physical blowing agent can depress the development of melt fracture due to the viscosity manipulation of the melt

which may result in high surface smoothness. Hence the printing quality on the film can be improved significantly.

In general, conventional polymer processing equipment may be used to produce the films described herein. In some cases, for example, the film can be produced by the blown film process using an annular die with a die gap from 0.45 to 1.3 mm and a blow-up ratio ranging from 1.5:1 to 3.5:1. Higher blow-up ratios might result in a more balanced MD/TD (machine direction/transverse direction) orientation, which improves overall film toughness. The die geometry and specification may be manufactured according to, for example, the patent application US 2012/0228793 A1, which is incorporated by reference herein in its entirety.

The majority of the conventional PE blown films are processed using a PE blend comprising LDPE for enhancing bubble stability. Almost all the HDPE films are made in a high stock blown film process; otherwise, the tear strength of the HDPE film deteriorates significantly. As described above, in embodiments of the methods are used for producing the multi-layer films, a supercritical gas may be injected into the melt at a precisely controlled rate, inside a transfer mixer, before entering the annular die. This unit could be controlled as a separate temperature zone with an accuracy of $\pm 1^\circ$ C. and a gas injection pressure variation below 1%. The plasticization effect of the gas can result in a viscosity change of the molten resin which would enhance the processing ability of the resin inside the annular die at a lower temperature compared to the processing temperature which is being used conventionally. Hence, a relatively stable bubble can be made inside the pocket. Then, because of the overall high specific heat capacity of polyethylene, the transverse stretch of the bubble can be delayed until the film becomes cooler, which may further enhance the bubble stability and the frost line height. This also might be beneficial in manipulating the crystallization kinetics of the skin layers to improve a few other physiomechanical properties. The higher degree of crystallization in the skin might lower the coefficient of friction on the skin layers.

In some embodiments, the multilayer foam films described herein can be produced by the blown film process, cast film process, or other suitable methods.

In some embodiments, the polymer composition of each layer comprises some apt amounts of other additives, such as pigments, slip agents, antistatic agents, UV stabilizers, antioxidants, nucleating agents, clarifying agents, or maleic anhydride. The foam layer optionally may contain 0.05 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer optionally may contain 0.05 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer optionally may contain 1 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer optionally may contain 2.5 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer optionally may contain 5 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer optionally may contain 7.5 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer

optionally may contain 10 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. In some embodiments, the foam layer optionally may contain 12.5 to 15 percent by weight of an inorganic additive, an organic additive or a mixture of an inorganic and an organic additive as a nucleating agent. For example, the foam layer may contain up to about 15% by weight of talc as a nucleating agent. In some embodiments, at least one layer may include a clarifying agent at less than 1 percent by weight, such as less than 0.5 percent by weight, such as less than 0.1 percent by weight, such as less than 0.05 percent by weight. In some cases, at least one layer of the film may contain up to about 35 wt % of calcium carbonates. In some cases, at least one layer of the film may contain up to about 30 wt % of calcium carbonates. In some cases, at least one layer of the film may contain up to about 25 wt % of calcium carbonates. In some cases, at least one layer of the film may contain up to about 20 wt % of calcium carbonates. In some cases, at least one layer of the film may contain up to about 15 wt % of calcium carbonates.

In some embodiments, at least one layer of the film described herein comprise less than 5 percent by weight maleic anhydride, for example, less than about 4 percent by weight, for example, less than about 3 percent by weight, for example, less than about 2.5 percent by weight, for example, less than about 2 percent by weight, for example, less than about 1 percent by weight.

In some cases, multilayer foam film can be comprised of two solid skin layers wherein one of the skin layers contains an apt amount of black pigments, for example, less than 1 percent by weight, for example, less than 0.75 percent by weight, for example, less than 0.5 percent by weight, and the other solid skin layer contains apt amounts of white pigments, for example, less than 1 percent by weight, for example, less than 0.75 percent by weight, for example, less than 0.5 percent by weight. In some other embodiments, both solid skin layers comprise an apt amount of white pigments.

In another case, the solid skin layers of the multilayer foam film comprise less than 0.5 percent by weight of an anti-blocking agent and/or less than 0.2 percent by weight of an anti-static agent.

In one embodiment, the multilayer foamed film has at least one solid skin layer with a static coefficient of friction value of less than 0.4, such as less than 0.38. In another embodiment, the film has at least one solid skin layer with a dynamic coefficient of friction value of less than 0.3.

The described multilayer film, comprising at least one foam layer, may have sets of significantly improved physiomechanical properties compared to known foamed film articles as in particular the bending stiffness value of greater than 18, in some cases greater than 20, and in some cases, greater than 25, all in Taber stiffness unit configuration, according to TAPPI/ANSI T 489 om-15, wherein the ratio of the mass per unit area (the mass of a unit area of the film in gram per meter-squared (gr/m^2)) over the stiffness value in Taber unit configuration is equal to or less than 13; in some cases, less than 11, and, in some cases, less than 10. In an embodiment, the film can have a Taber bending stiffness value of less than 280, according to TAPPI/ANSI T 489 om-15.

The described films can have a surface with an average Sheffield smoothness, according to TAPPI T 538, of less than 100. In some embodiments, the film may have an

average Sheffield smoothness of less than 50; in some cases, less than 40; in some cases, less than 30; and, in some cases, less than 15.

The multilayer foam film can have an overall thickness of greater than 8 mils, in some cases, greater than 10 mils, in some cases, greater than 13 mils, and in some cases greater than 15 mils.

In some embodiments, the lightweight film described herein has a bulk density less than 1 gr/cm³; in some cases, less than 0.962 gr/cm³; in some cases, less than 0.94 gr/cm³; in some cases, less than 0.9 gr/cm³; in some cases, less than 0.85 gr/cm³; and in some cases, less than 0.8 gr/cm³.

In some embodiments, the foam layer of the disclosed film has a far better cellular morphology compared to the known films. For example, the foam layers of the disclosed films can have uniformly distributed cells, for example with a closed-cell morphology, an average cell size of about 10-250 μm, for example, 50-250 μm, for example, 150-250 μm, for example, 200-250 μm; an average cell density with respect to the un-foamed polymer volume of about 10²-10⁹ cells/cm³, and an expansion ratio of the foamed layer from 1 to 9, for example an expansion ratio of the foamed layer from 1 to 8, for example an expansion ratio of the foamed layer from 1 to 7, for example an expansion ratio of the foamed layer from 1 to 6, for example an expansion ratio of the foamed layer from 1 to 5, for example an expansion ratio of the foamed layer from 1 to 4, for example an expansion ratio of the foamed layer from 1 to 3, for example an expansion ratio of the foamed layer from 1 to 2. In some cases, the foam layer comprises at least 10% closed cells and, in some cases, more than 50% closed cells. In one embodiment, the foam layer has a substantially entirely closed-cell morphology (e.g., greater than 95% closed cells).

In some embodiments, the multilayer foam film comprises at least one layer containing the PE/EVOH blend. In some embodiments, the multilayer foam film described herein comprises at least one layer, excluding the solid skin layers, containing from about 30 to 50 percent by weight of EVOH, for example, from about 35 to 49 percent by weight of EVOH, for example, from about 40 to 49 percent by weight of EVOH, for example, from about 45 to 49 percent by weight of EVOH, and less than 5 percent by weight maleic anhydride, e.g., 2 percent by weight. In some embodiments, the overall mass concentration of the EVOH in a unit area of the film does not exceed 10 percent of the mass of the unit area of the film. In some embodiments, the overall mass concentration of the EVOH in a unit area of the film does not exceed 7.5 percent of the mass of the unit area of the film. In some embodiments, the overall mass concentration of the EVOH in a unit area of the film does not exceed 5 percent of the mass of the unit area of the film. In some embodiments, the overall mass concentration of the EVOH in a unit area of the film does not exceed 4 percent of the mass of the unit area of the film. In some embodiments, the overall mass concentration of the EVOH in a unit area of the film does not exceed 3 percent of the mass of the unit area of the film. In some embodiments, the overall mass concentration of the EVOH in a unit area of the film does not exceed 2.5 percent of the mass of the unit area of the film.

The films described herein can have a water vapor transmission rate of less than 0.05 gr/100 in²/24 hr, according to ASTM E398-13. In one case, the water vapor transmission rate of the film is less than 0.1 gr/100 in²/24 hr. In some embodiments, the water vapor transmission rate of the film is less than 1 gr/m²/day.

In some embodiments, the described film can have an oxygen transmission rate of less than 0.65 cc/100 in²/24 hr,

or 10 cc/m²/24 hr, according to ASTM D3985. In some case, the described film can have an oxygen transmission rate of less than 0.32 cc/100 in²/24 hr, or 5 cc/m²/24 hr, according to ASTM D3985. In some embodiments, the described film can have an oxygen transmission rate of less than 0.13 cc/100 in²/24 hr, or 2 cc/m²/24 hr, according to ASTM D3985.

In some embodiments, the described film comprises at least one layer containing a resin with an oxygen transmission rate value of less than 0.65 cc/100 in²/24 hr, according to ASTM D3985. In another embodiment, the described film comprises at least one layer, excluding the solid skin layers, containing ethylene vinyl alcohol (EVOH).

In an exemplary embodiment, the multilayer foam film, e.g., five-layer foam film, has at least one solid skin layer with a static coefficient of friction value of less than 0.4, and/or less than 0.38. In another embodiment, the film, e.g., five-layer foam film, has at least one solid skin layer with a dynamic coefficient of friction value of less than 0.3.

In some embodiments, various thermoplastics can be used in at least one layer of the multilayer foam film and in the blown film process such as polyethylene (PE), polypropylene (PP), polyethylene terephthalate (PET), ethylene vinyl acetate (EVA), ethylene vinyl alcohol (EVOH), polyvinyl chloride (PVC), Polyvinylidene chloride (PVDC), polyamide (PA), LLDPE copolymer which include an α-olefin co-monomer such as butene, hexene, or octene; any of the resins known as TPE family such as, but not limited to, propylene-ethylene copolymer, thermoplastic olefin (TPO), and thermoplastic polyurethane (TPU). In some embodiments described herein which include HDPE layers, some or all of the HDPE layers are replaced by PP layers in the multilayer structure. In some embodiments described herein which include HDPE layers, some or all of the HDPE layers are replaced by PET layers in the multilayer structure.

In another embodiment, at least one layer, (e.g., excluding the outer skin layers), of the film may comprise LDPE, PP, PA, EVOH, EVA, or PVOH. The following examples demonstrate the process of the present disclosure. The examples are only demonstrative and are intended to put no limit on the disclosure with regards to the materials, conditions, or the processing parameters set forth herein.

Herein, a method of protecting the oxygen barrier layer (e.g., EVOH layer), in the described multilayer film, from getting any form of physical damages, e.g., micro-cracks, when the multilayer film undergoes a creasing, scoring, piercing, punching, or folding process is disclosed. In the said method, any oxygen barrier layer is supported by at least one foam layer adjacent to the oxygen barrier layer, on one side or both sides. In some embodiments, any oxygen barrier layer is supported by at least one foam layer close to the oxygen barrier layer. In some embodiments, any oxygen barrier layer is protected by the inclusion of one foam layer adjacent to any or both of the skin layers. In some embodiments, the oxygen barrier layer comprises EVOH.

Herein, a method of making a creased, folded or scored multilayer film (and related products) is disclosed, comprising co-extruding of at least one foam layer including a plurality of cells, wherein at least 10% of the cells are closed cells, and two solid skin layers comprising HDPE, and one or more solid layers, comprising ethylene vinyl alcohol (EVOH), wherein the said foam layer is being co-extruded between the skin layer and the layer comprising EVOH, and the film has an overall thickness equal to or greater than 8 mils; creasing, scoring or folding the said film, wherein the oxygen transmission rate value of the creased, scored or folded in cc/m²/day, according to ASTM D3985, does not

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increase more than 30% of the OTR value of an identical non-creased, non-scored or unfolded multi-layer film (i.e., before creasing, scoring or folding). In some embodiments, the oxygen transmission rate value of the creased, scored or folded film does not increase more than 20%, or more than 10%, or more than 5%, of the OTR value an identical non-creased, non-scored or unfolded multilayer film (i.e., before creasing scoring or folding). In some embodiments, the ratio of the OTR (in cc/m²/24 hr, according to ASTM D3985) over that of an identical film prior to creasing, folding or scoring is less than 1.1, in some cases, less than 1.075, in some cases, less than 1.05 and, in some cases less than 1.025.

EXAMPLES

All of the products resulting from the examples below were tested and characterized in terms of bending stiffness, surface smoothness, oxygen transmission rate, water vapor transmission rate, and density. To characterize the bending stiffness of the film, a TABER Stiffness Tester, Model 150-E from Taber Industries, was used. The smoothness of the products was evaluated using a Gurley™ 4340 Automatic Densometer & Smoothness Tester. The Oxygen Transmission Rate (OTR) of the products was measured using OX-TRAN 1/50 tester from AMETEK MOCON, according to ASTM D3985. The Water Vapor Transmission Rate (WVTR) of the samples was measured using a PERMATRAN-W Model 1/50 G+ tester from AMETEK MOCON, according to ASTM E398-13.

Example 1: Samples of multilayer HDPE film (seven layers) were produced using a 7 layer blown film line from Reifenhauer Extrusion System equipped with internal bubble cooling system, gauge control, mass throughput control, and layer thickness control, consisting seven extruders including two 55 mm Extruders denoted as "A" and "G", for the skins, two 65 mm Extruders denoted as "B" and "F", and three 35 mm extruders denoted as "C", "D", and "E. Both 65 mm extruders were equipped with supercritical gas injection unit, capable of injecting nitrogen, carbon dioxide, or a mixture of both, as well as two 65 mm MuCell Transfer Mixer (MTM), all from MuCell Extrusion LLC. All the films were produced by the blown film process using an annular die with a die gap ranging from 0.7 to 1.2 mm and a blow-up ratio ranging from 2.8:1 to 3.5:1. The lip of the annular die was boron nitride coated.

Table 1 contains the processing data, as well as the characterization results of the products, which were made, as non-limiting examples to elucidate this invention. The samples were produced with high-density polyethylene ELITE 5960 from Dow Chemical Company, having the melt

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index of 0.85 dg/min and the density of 0.962 gr/cm³. In all samples, where required, the additives, e.g., color pigments, were added in the form of a masterbatch with LDPE carrier. Obviously, the additives can be compounded in an HDPE carrier. In a few samples, a minor fraction of the LDPE 1321 from Dow Chemical Company with the melt index of 0.25 dg/min and the density of 0.921 gr/cm³ was used. The calcium carbonate and talc were prepared and introduced as a highly filled masterbatch of, respectively, 80 wt % filled calcium carbonate and 70 wt % filled talc within the HDPE as the base carrier resin. All of the tie layers comprise ADM ER adhesive resin, which is anhydride grafted polyolefin. In this example, the middle layer comprises Ethylene vinyl alcohol (EVOH) with an ethylene content of 32%.

All the samples were coextruded with a total throughput of 300 to 340 kg/hr, as it is listed in table 1. The temperature of the mixing section, wherein the supercritical gas was injected, was kept at 184° C. for all the samples. Supercritical nitrogen was used as a physical blowing agent and was injected into the MuCell Transfer Mixer (MTM) at the concentration from 0.01 wt % to 0.07 wt %, very accurately, into the molten polymer. The temperatures of the extruders' zones were set according to the conventional processing suggested in the datasheet of the materials.

Sample 2 and 3 are the foam versions of the solid sample 1 with the same basic weight of 342 gr/m², which have 40% and 45% less density compared to the solid sample 1, respectively.

As it is listed in table 1, sample 3 shows 190% higher bending stiffness value compared to its solid counterpart. Sample 5 and 6 are the foam versions of sample 4 with the same basic weight of about 390 gr/m², which have 37% and 39% less density compared to the solid sample 4. Samples 5 and 6 show 140% and 160% higher bending stiffness values compared to their solid counterpart, respectively. Sample 6 possesses the surface smoothness value of about 17.5, in Sheffield, which is comparable to sample 4. Both samples 5 and 6 show an oxygen transmission rate below 1.5 cc/m²/day.

Samples 8, 9, 10, and 11 are the foam version of sample 7 with a similar basic weight of about 240 g/m², which has about 20% to 30% less density. Samples 9 and 10 possess 140% and 190% higher bending stiffness compared to their solid counterpart. Although samples 8 and 9 have much thinner (almost half) middle layer compared to sample 10, they show an oxygen transmission rate in the same range all less than 3 cc/m²/day. Also, samples 8 and 9 have a surface smoothness value of below 10, in Sheffield, and comparable to their solid counterpart.

Moreover, almost all the samples 1 to 11 possess a water vapor transmission rate of less than 1 gr/m²/day.

TABLE 1

		Sample 1						
Code	Solid 330							
ID	C2-22-01							
Density (gr/cm ³)	1.284							
Thickness (um)	300							
Basic weight (gr/m ²)	342.3							
Total Throughput	300							
Layers	A	B	C	D	E	F	G	
HDPE (wt %)	70	50				50	70	
80% CaCO ₃ filled PE (wt %)		20				20		
mPE (wt %)			70		70			
Adhesive (wt %)			30		30			
EVOH (wt %)				100				

TABLE 1-continued

70% talc filled HDPE (wt %)	25						25
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5	10				10	5
SC-N2 (%)							
Layer Thickness (um)	55	82	8	10	8	82	55
Throughput (kg/hr)	53.2	85.2	6.4	10.4	6.4	85.2	53.2
Bending Stiffness (Taber)				38.4			
Smoothness (Sheffield)				14.2			
OTR (cc/m2/day)				1.33			
WVTR (gr/m2/day)				<1			
Sample 2							
Code	#1-0.055N2-330						
ID	C2-22-02						
Density (gr/cm ³)	0.796						
Thickness (um)	430						
Basic weight (gr/m ²)	342.3						
Total Throughput	300						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	70	50				50	70
80% CaCO ₃ filled PE (wt %)		20				20	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	25						25
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5	10				10	5
SC-N2 (%)		0.055				0.055	
Layer Thickness (um)	55	147	8	10	8	147	55
Throughput (kg/hr)	53.2	85.2	6.4	10.4	6.4	85.2	53.2
Bending Stiffness (Taber)							
Smoothness (Sheffield)							
OTR (cc/m2/day)							
WVTR (gr/m2/day)							
Sample 3							
Code	#2-0.065N2-330						
ID	C2-22-03						
Density (gr/cm ³)	0.712						
Thickness (um)	480						
Basic weight (gr/m ²)	342.3						
Total Throughput	300						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	70	50				50	70
80% CaCO ₃ filled PE (wt %)		20				20	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	25						25
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5	10				10	5
SC-N2 (%)		0.065				0.065	
Layer Thickness (um)	55	172	8	10	8	172	55
Throughput (kg/hr)	53.2	85.2	6.4	10.4	6.4	85.2	53.2
Bending Stiffness (Taber)				76.2			
Smoothness (Sheffield)				117.2			
OTR (cc/m2/day)				4.17 to 34.2			
WVTR (gr/m2/day)				0.93			
Sample 4							
Code	Solid 390						
ID	C2-22-04						
Density (gr/cm ³)	1.19						
Thickness (um)	330						
Basic weight (gr/m ²)	392.6						
Total Throughput	300						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	65	50				50	70
80% CaCO ₃ filled PE (wt %)		30				30	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	25						25
64% talc filled PE (wt %)		20				20	

TABLE 1-continued

LDPE (wt %)	10							5
SC-N2 (%)								
Layer Thickness (um)	55	90	15	10	15	90	55	
Throughput (kg/hr)	47.8	87.8	10.5	9.1	10.5	87.8	46.4	
Bending Stiffness (Taber)								50.5
Smoothness (Sheffield)								16.6
OTR (cc/m ² /day)								1.18
WVTR (gr/m ² /day)								<1
Sample 5								
Code								#4-0.065N@-390
ID								C2-22-05
Density (gr/cm ³)								0.742
Thickness (um)								535
Basic weight (gr/m ²)								396.7
Total Throughput								340
Layers	A	B	C	D	E	F	G	
HDPE (wt %)	65	50				50	70	
80% CaCO ₃ filled PE (wt %)		30				30		
mPE (wt %)			70		70			
Adhesive (wt %)			30		30			
EVOH (wt %)								100
70% talc filled HDPE (wt %)	25						25	
64% talc filled PE (wt %)		20				20		
LDPE (wt %)	10						5	
SC-N2 (%)		0.065				0.065		
Layer Thickness (um)	55	193	15	10	15	193	55	
Throughput (kg/hr)	53.6	100	11.8	10.2	11.8	100	52	
Bending Stiffness (Taber)								70.5
Smoothness (Sheffield)								26.7
OTR (cc/m ² /day)								1.45
WVTR (gr/m ² /day)								<1
Sample 6								
Code								#6
ID								C2-22-06
Density (gr/cm ³)								0.718
Thickness (um)								540
Basic weight (gr/m ²)								387.9
Total Throughput								340
Layers	A	B	C	D	E	F	G	
HDPE (wt %)	65						65	
80% CaCO ₃ filled PE (wt %)		20				20		
mPE (wt %)			70		70			
Adhesive (wt %)			30		30			
EVOH (wt %)								100
70% talc filled HDPE (wt %)	30						30	
64% talc filled PE (wt %)		20				20		
LDPE (wt %)	5	60				60	5	
SC-N2 (%)		0.065				0.065		
Layer Thickness (um)	55	97.5	15	10	15	97.5	55	
Throughput (kg/hr)	54.4	98.3	12.1	10.4	12.1	98.3	54.4	
Bending Stiffness (Taber)								80.5
Smoothness (Sheffield)								17.5
OTR (cc/m ² /day)								<1.5
WVTR (gr/m ² /day)								<1
Sample 7								
Code								Solid 243
ID								C2-18-01
Density (gr/cm ³)								1.174
Thickness (um)								207
Basic weight (gr/m ²)								243.1
Total Throughput								340
Layers	A	B	C	D	E	F	G	
HDPE (wt %)	65	30				30	65	
80% CaCO ₃ filled PE (wt %)		30				30		
mPE (wt %)			70		70			
Adhesive (wt %)			30		30			
EVOH (wt %)								100
70% talc filled HDPE (wt %)	30						30	
64% talc filled PE (wt %)		20				20		
LDPE (wt %)	5	20				20	5	
SC-N2 (%)								

TABLE 1-continued

Layer Thickness (um)	45	46.5	8	8	8	46.5	45
Throughput (kg/hr)	71.1	82	10.3	13.3	10.3	82	71.1
Bending Stiffness (Taber)				15.7			
Smoothness (Sheffield)				7			
OTR (cc/m ² /day)				1.63			
WVTR (gr/m ² /day)				<1			
Sample 8							
Code	#1A-F Foam						
ID	C2-18-02						
Density (gr/cm ³)	0.959						
Thickness (um)	250						
Basic weight (gr/m ²)	239.8						
Total Throughput	343.5						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	65	20				20	65
80% CaCO ₃ filled PE (wt %)		30				30	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	30						30
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5	30				30	5
SC-N2 (%)						0.065	
Layer Thickness (um)	44.7	46.2	9.9	4	9.8	90.6	44.8
Throughput (kg/hr)	72.3	82.9	13	6.8	12.9	83.1	72.4
Bending Stiffness (Taber)				15.8			
Smoothness (Sheffield)				7.3			
OTR (cc/m ² /day)				2.47			
WVTR (gr/m ² /day)				0.694			
Sample 9							
Code	#1B, F&B Foam						
ID	C2-18-03						
Density (gr/cm ³)	0.856						
Thickness (um)	280						
Basic weight (gr/m ²)	239.6						
Total Throughput	342.8						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	65	20				20	65
80% CaCO ₃ filled PE (wt %)		30				30	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	30						30
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5	30				30	5
SC-N2 (%)		0.065				0.065	
Layer Thickness (um)	44.4	83.5	9.9	4.1	9.8	83.5	44.8
Throughput (kg/hr)	71.7	82.8	13	7	12.9	83	72.4
Bending Stiffness (Taber)				21.8			
Smoothness (Sheffield)				5.6			
OTR (cc/m ² /day)				2.76			
WVTR (gr/m ² /day)				0.739			
Sample 10							
Code	#2						
ID	C2-18-04						
Density (gr/cm ³)	0.842						
Thickness (um)	300						
Basic weight (gr/m ²)	252.7						
Total Throughput	340						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	65	50				50	65
80% CaCO ₃ filled PE (wt %)		30				30	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	30						30
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5						5
SC-N2 (%)		0.065				0.065	
Layer Thickness (um)	45	89.7	10.5	10	10.2	89.7	45
Throughput (kg/hr)	68.4	80.8	13	16	12.6	80.8	68.4

TABLE 1-continued

Bending Stiffness (Taber)	30.1						
Smoothness (Sheffield)	31.7						
OTR (cc/m ² /day)	3.09						
WVTR (gr/m ² /day)	1.07						
	Sample 11						
Code	#3						
ID	C2-18-05						
Density (gr/cm ³)	0.81						
Thickness (um)	300						
Basic weight (gr/m ²)	243.1						
Total Throughput	340						
Layers	A	B	C	D	E	F	G
HDPE (wt %)	65	50				50	65
80% CaCO ₃ filled PE (wt %)		30				30	
mPE (wt %)			70		70		
Adhesive (wt %)			30		30		
EVOH (wt %)				100			
70% talc filled HDPE (wt %)	30						30
64% talc filled PE (wt %)		20				20	
LDPE (wt %)	5						5
SC-N ₂ (%)		0.065				0.065	
Layer Thickness (um)	45	93	8	8	8	93	45
Throughput (kg/hr)	71.1	82	10.3	13.3	10.3	82	71.1
Bending Stiffness (Taber)							
Smoothness (Sheffield)							
OTR (cc/m ² /day)							
WVTR (gr/m ² /day)							

Example 2: Samples of multilayer HDPE film (three layers) were produced using a blown film line from Windmoeller & Hoelscher Corporation comprising one 105 mm main extruder and two identical 75 mm co-extruders. The core extruder was equipped with a supercritical gas injection unit, capable of injecting nitrogen or carbon dioxide, and a 120 mm MuCell Transfer Mixer, both from MuCell Extrusion LLC. All the films were produced by the blown film process using an annular die with a die gap ranging from 0.45 to 1.3 mm and a blow-up ratio ranging from 2.8:1 to 3.5:1. The lip of the annular die was boron nitride coated.

Table 2 contains the characterization results of the products (samples 12 to 15) were made, as non-limiting examples to elucidate on some embodiments of this invention. The samples were produced with high-density polyethylene ELITE 5960 from Dow Chemical Company, having the melt index of 0.85 dg/min and the density of 0.962 gr/cm³. The calcium carbonate and talc were prepared and

introduced as a highly filled masterbatch of, respectively, 80 wt % filled calcium carbonate and 70 wt % filled talc within the HDPE as the base carrier resin. The foamed core layer of all samples contains talc as the cell nucleating agent.

All the samples were coextruded with the total throughput of about 260 to 290 kg/hr, as it is listed in table 2. The temperature of the mixing section, wherein the supercritical gas was injected, was kept at 190° C. for all the samples 12 to 15. Supercritical nitrogen was used as a physical blowing agent and was injected into the MuCell Transfer Mixer (MTM) at the concentration from 0.011 wt % to 0.02 wt %, very accurately, into the molten polymer.

Sample 15 is the solid counterpart of samples 12, 13, and 14 which have about 18% to 25% less density compared to sample 15. Sample 15 showed an oxygen transmission rate of less than 1.4 cc/m²/day. All the samples exhibit a water vapor transmission rate of less than 1, as well as a surface smoothness value of less than 10, in Sheffield.

TABLE 2

	Sample											
	12			13			14			15		
ID	C2-14-1			C2-14-2			C2-14-4			C2-14-5		
Density (gr/cm ³)	0.9			0.88			0.826			1.104		
Thickness (um)	121			125			155			104.5		
Basic weight (gr/m ²)	110			110			128			110		
Total Throughput	287.2			261			261			261		
Layers	A	B	C	A	B	C	A	B	C	A	B	C
HDPE (wt %)	68	80	98	68	80	98	68	35	98	68	35	98
64% talc filled PE (wt %)		18			18			18			18	
70% talc filled HDPE (wt %)	30			30			30			30		
Maleic anhydride (wt %)		2			2			2			2	
EVOH (wt %)								45			45	
LDPE (wt %)	2		2	2		2	2		2	2		2
SC-N ₂ (%)		0.01			0.01			0.01			<<0.011	
Layer Thickness (um)	31.5	49.1	40.4	24.7	37.2	44.5	29	73.7	52.3	24.9	34.7	44.9
Throughput (kg/hr)	91.5	92.2	104	65.3	92.2	104	65.3	92.2	104	65.3	92.2	104

TABLE 2-continued

	Sample			
	12	13	14	15
Smoothness (Sheffield)	<10	<10	<10	<10
OTR (cc/m ² /day)	239	276	6.64	1.38
WVTR (gr/m ² /day)	0.571	0.581	0.847	0.86

Example 3: Creased samples of the sample 11 in Table 1 were prepared, according to TAPPI/ANSI T512 sp-12, and the oxygen transmission rate (OTR) before and after creasing and folding was tested. As explained, the OTR values in cc/m²/24 hr were measured according to ASTM D3985 at a standard temperature of 73° F. (23° C.) and 0% relative humidity (RH). All of the tested samples were identical. The average measured OTR value of sample 11 before creasing and after creasing were 1.56 cc/m²/24 hr and 1.6 cc/m²/24 hr respectively.

The creased sample of the solid counterpart to the sample 11 in Table 1 were prepared and the OTR values were measured according to the aforementioned methods. The thickness of the samples was 260 μm. The average measured OTR values before creasing and after creasing were 0.95 cc/m²/24 hr and 1.17 cc/m²/24 hr respectively.

Example 4. The creased samples of the packaging tube of AVENO daily moisturizing lotion was prepared, according to TAPPI/ANSI T512 sp-12, and the oxygen transmission rate (OTR) before and after creasing and folding was tested. The total thickness of the sample was 480 μm comprising one EVOH layer with the thickness of 60 μm. As explained, the OTR values in cc/m²/24 hr were measured according to ASTM D3985 at a standard temperature of 73° F. (23° C.) and 0% relative humidity (RH). The average measured OTR before creasing and after creasing were 0.29 cc/m²/24 hr and 0.41 cc/m²/24 hr respectively.

The invention claimed is:

1. A creased, folded or scored multilayer foam film comprising:

a first foam layer including a plurality of cells, wherein at least 10% of the cells are closed cells,

a second foam layer including a plurality of cells, wherein at least 10% of the cells are closed cells,

two solid skin layers comprising HDPE such that the first and second foam layers are disposed between the two solid skin layers, and

a solid layer comprising ethylene vinyl alcohol (EVOH) between the first foam layer and the second foam layer, wherein the said first foam layer is between one of the solid skin layers and the solid layer comprising EVOH, and the said second foam layer is between one of the solid skin layers and the solid layer comprising EVOH, and the film has an overall thickness equal to or greater than 8 mils, and the ratio of the oxygen transmission rate of the creased, folded or scored film in cc/m²/24hr, according to ASTM D3985, over that of an identical film prior to creasing, folding or scoring is less than 1.1.

2. The film of claim 1, wherein the film has an average Sheffield smoothness of less than 40, according to TAPPI T 538.

3. The film of claim 1, wherein the film is pieced or punched.

4. The film of claim 1, wherein the film has a bulk density value of less than 0.962 gr/cm³.

5. The film of claim 1, wherein the film has an average Sheffield smoothness, according to TAPPI T 538, of less than 25.

6. The film of claim 1, wherein the film has a Taber bending stiffness value of greater than 18 according to TAPPI/ANSI T 489 om-15, and the ratio of the mass per unit area (the mass of a unit area of the film in gram per meter-squared (gr/m²)) over the Taber stiffness value is equal to or less than 13.

7. The film of claim 1, wherein the film has a water vapor transmission rate of less than 1 gr/m²/24hr, according to ASTM E398-13.

8. The film of claim 1, wherein the film has an oxygen transmission rate of less than 10 cc/m²/24hr, according to ASTM D3985.

9. The film of claim 1, wherein the first foam layer comprises an HDPE with a density of 0.94 to 0.962 gr/cm³.

10. The film of claim 1, wherein the film layer has a Taber bending stiffness value of less than 280, according to TAPPI/ANSI T 498 om-15.

11. The film of claim 1, wherein the film comprises one or more additives selected from the group consisting of pigments, slip agents, antistatic agents, UV stabilizers, maleic anhydride, and antioxidant.

12. The film of claim 1, wherein at least one of the solid skin layers has a static coefficient of friction value according to ASTM D1894 of less than 0.4.

13. The film of claim 1, wherein at least one of the solid skin layers has a dynamic coefficient of friction value according to ASTM D1894 of less than 0.3.

14. The film of claim 1, wherein the film comprises five, or seven layers.

15. The film of claim 1, wherein the first foam layer includes a nucleating agent and has an average cell size of 10 to 100 μm.

16. The film of claim 1, wherein the first foam layer has a cell density of 10² to 10⁹ cells/cm³, and the film density is 0.1 to 0.9 g/cm³.

17. The film of claim 1, wherein, in the first foam layer, at least 50% of the cells are closed cells.

18. The film of claim 1, wherein the first foam layer comprises a nucleating agent with a content of 0.05 to 15 percent by weight.

19. The film of claim 1, further comprising a solid layer, comprising HDPE with a melt index of 0.02 to 20 dg/min.

20. The film of claim 1, further comprising a layer that comprises LDPE.

21. A method of making a creased, folded or scored multilayer film, comprising:

co-extruding a first foam layer, a second foam layer, two solid skin layers comprising HDPE and one solid layer comprising ethylene vinyl alcohol (EVOH) to form a multilayer film,

wherein the first foam layer includes a plurality of cells, wherein at least 10% of the cells are closed cells, the second foam layer includes a plurality of cells, wherein at least 10% of the cells are closed cells,

the first and second foam layers are disposed between the two solid skin layers comprising HDPE, the solid layer comprising ethylene vinyl alcohol (EVOH) is between the first foam layer and the second foam layer, the first foam layer is between one of the solid skin layers and the solid layer comprising EVOH, and the second foam layer is between one of the solid skin layers and the solid layer comprising EVOH, and the multi-layer film has an overall thickness equal to or greater than 8 mils; and
creasing, folding or scoring the multi-layer film, wherein the ratio of the oxygen transmission rate of the creased, folded or scored film in cc/m²/24hr, according to ASTM D3985, over that of an identical film prior to creasing, folding or scoring is less than 1.1.

22. The method of claim **21**, wherein any the first foam layer is co-extruded directly adjacent to the solid layer comprising EVOH.

23. The method of claim **21**, further comprising piercing or punching the multi-layer film.

* * * * *

UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

PATENT NO. : 11,926,123 B2
APPLICATION NO. : 17/530407
DATED : March 12, 2024
INVENTOR(S) : Mehdi Saniei et al.

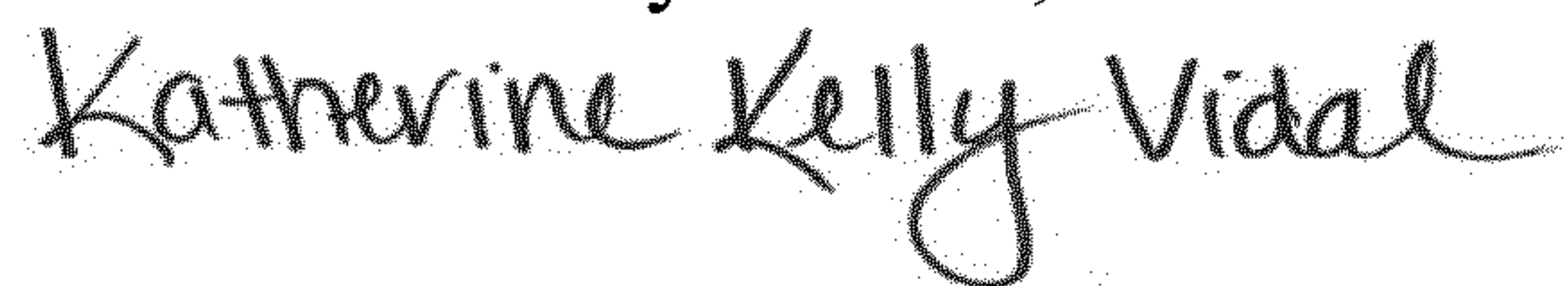
Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

In the Claims

Column 23, Claim 22, Line 16, "wherein any the" should read --wherein the--

Signed and Sealed this
Fourth Day of June, 2024



Katherine Kelly Vidal
Director of the United States Patent and Trademark Office