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Shin et al.

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(54) **IMAGING LENS SYSTEM HAVING SEVEN LENSES OF +-+--+ OR +-+--+ REFRACTIVE POWERS**

(58) **Field of Classification Search**
CPC G02B 13/0045; G02B 9/64
See application file for complete search history.

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(56) **References Cited**

U.S. PATENT DOCUMENTS

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10,656,380 B2 5/2020 Chen
10,670,837 B2 6/2020 Kuo
10,690,886 B2 6/2020 Tang et al.
2014/0139719 A1 5/2014 Fukaya

(Continued)

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FOREIGN PATENT DOCUMENTS

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 8 days.

CN 204065539 U 12/2014
CN 105445907 A 3/2016

(Continued)

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OTHER PUBLICATIONS

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Related U.S. Application Data

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(30) **Foreign Application Priority Data**

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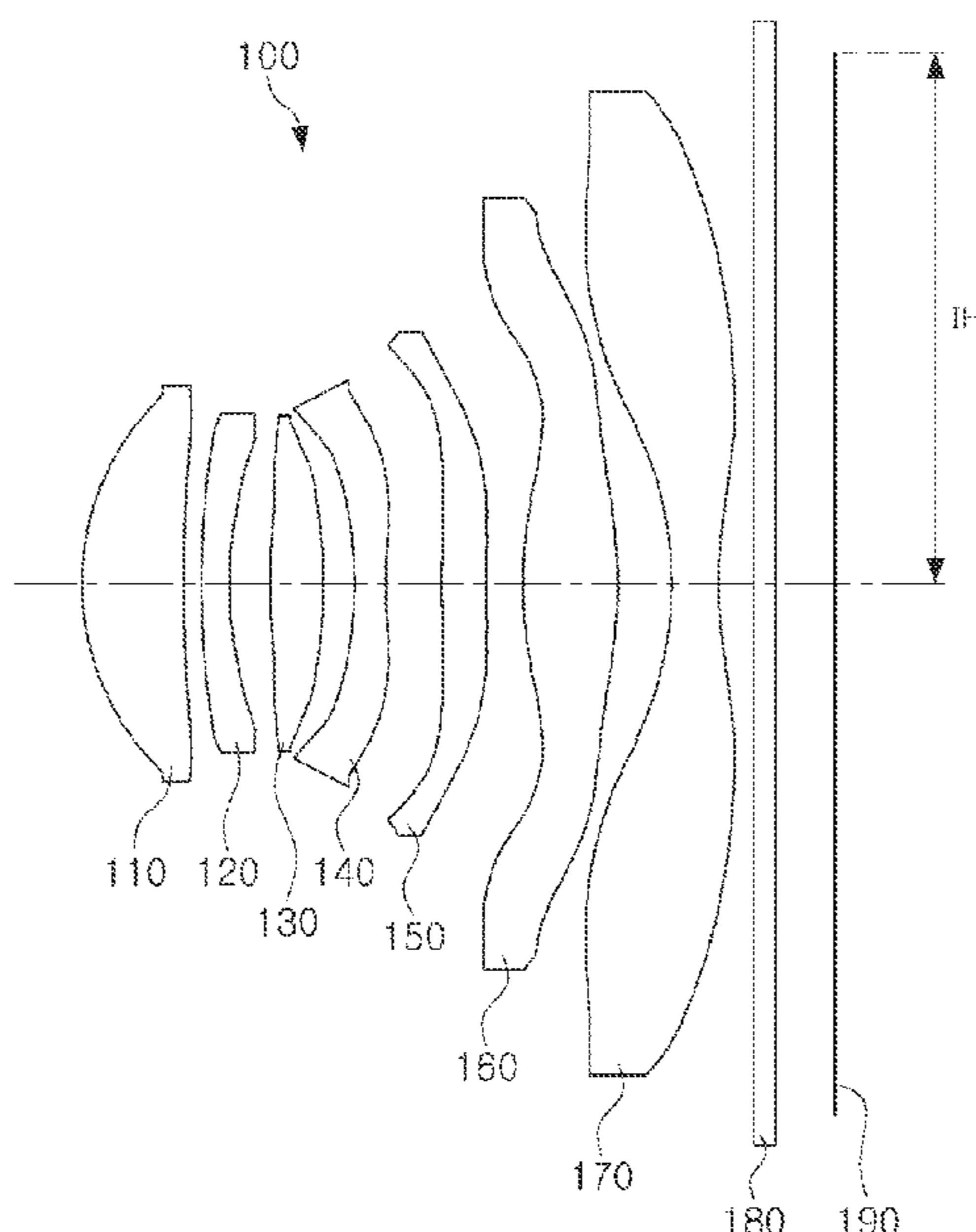
(57) **ABSTRACT**

(51) **Int. Cl.**
G02B 13/00 (2006.01)
G02B 9/64 (2006.01)

(52) **U.S. Cl.**
CPC **G02B 13/0045** (2013.01); **G02B 9/64** (2013.01)

An imaging lens system includes a first lens, a second lens, a third lens, a fourth lens, a fifth lens, a sixth lens, and a seventh lens, sequentially disposed at intervals from an object side of the imaging lens system. The imaging lens system satisfies $1.5 < Nd5 < 1.6$, $30 < V5 < 50$, and $TTL/2IH < 0.730$, where Nd5 is a refractive index of the fifth lens, V5 is an Abbe number of the fifth lens, TTL is a distance from an object side surface of the first lens to an imaging plane, and 2IH is a diagonal length of the imaging plane.

10 Claims, 12 Drawing Sheets



(56)

References Cited

U.S. PATENT DOCUMENTS

2015/0009578 A1 1/2015 Shinohara et al.
 2015/0198791 A1 7/2015 Kubota et al.
 2016/0062086 A1 3/2016 Tsai et al.
 2016/0241756 A1 8/2016 Chen
 2017/0184822 A1 6/2017 Shi
 2018/0188482 A1 7/2018 Jhang et al.
 2019/0004285 A1 1/2019 Tang et al.
 2019/0004288 A1 1/2019 Kubota et al.
 2019/0025549 A1 1/2019 Hsueh et al.
 2019/0025551 A1 1/2019 Kuo
 2019/0079273 A1 3/2019 Kubota et al.
 2019/0094494 A1* 3/2019 Hsu G02B 27/0025
 2019/0154974 A1 5/2019 Chen
 2019/0155000 A1 5/2019 Hashimoto
 2019/0170987 A1 6/2019 Gao et al.
 2019/0227277 A1 7/2019 Tang et al.
 2020/0209548 A1* 7/2020 Bian G02B 13/0045
 2020/0209562 A1* 7/2020 Zhao G02B 9/64
 2020/0363611 A1* 11/2020 Huang G02B 27/0025
 2021/0033821 A1* 2/2021 Fukaya G02B 13/0045

FOREIGN PATENT DOCUMENTS

CN 107621683 A 1/2018
 CN 109212717 A 1/2019

CN 109283657 A 1/2019
 CN 109828345 A 5/2019
 JP 2014-102408 A 6/2014
 TW 1644142 B 12/2018

OTHER PUBLICATIONS

Korean Office Action dated Jan. 27, 2023, in counterpart Korean Patent Application No. 10-2022-0042252 (7 pages in English, 5 pages in Korean).
 Korean Office Action dated Sep. 4, 2020 in the corresponding Korean Patent Application No. 10-2019-0071406 (12 pages in English, 8 pages in Korean).
 Korean Office Action dated Jul. 7, 2021 in counterpart Korean Patent Application No. 10-2021-0078506 (7 pages in English; 5 pages in Korean).
 Chinese Office Action dated Nov. 1, 2022, in counterpart Chinese Patent Application No. 201911407923.8 (8 Pages in Chinese, 8 Pages in English).
 Chinese Office Action dated Mar. 3, 2022, in counterpart Chinese Patent Application No. 201911407923.8 (6 pages in English and 9 pages in Chinese).
 Korean Office Action dated Jul. 27, 2023, in counterpart Korean Patent Application No. 10-2022-0042252 (6 pages in English, 5 pages in Korean).

* cited by examiner

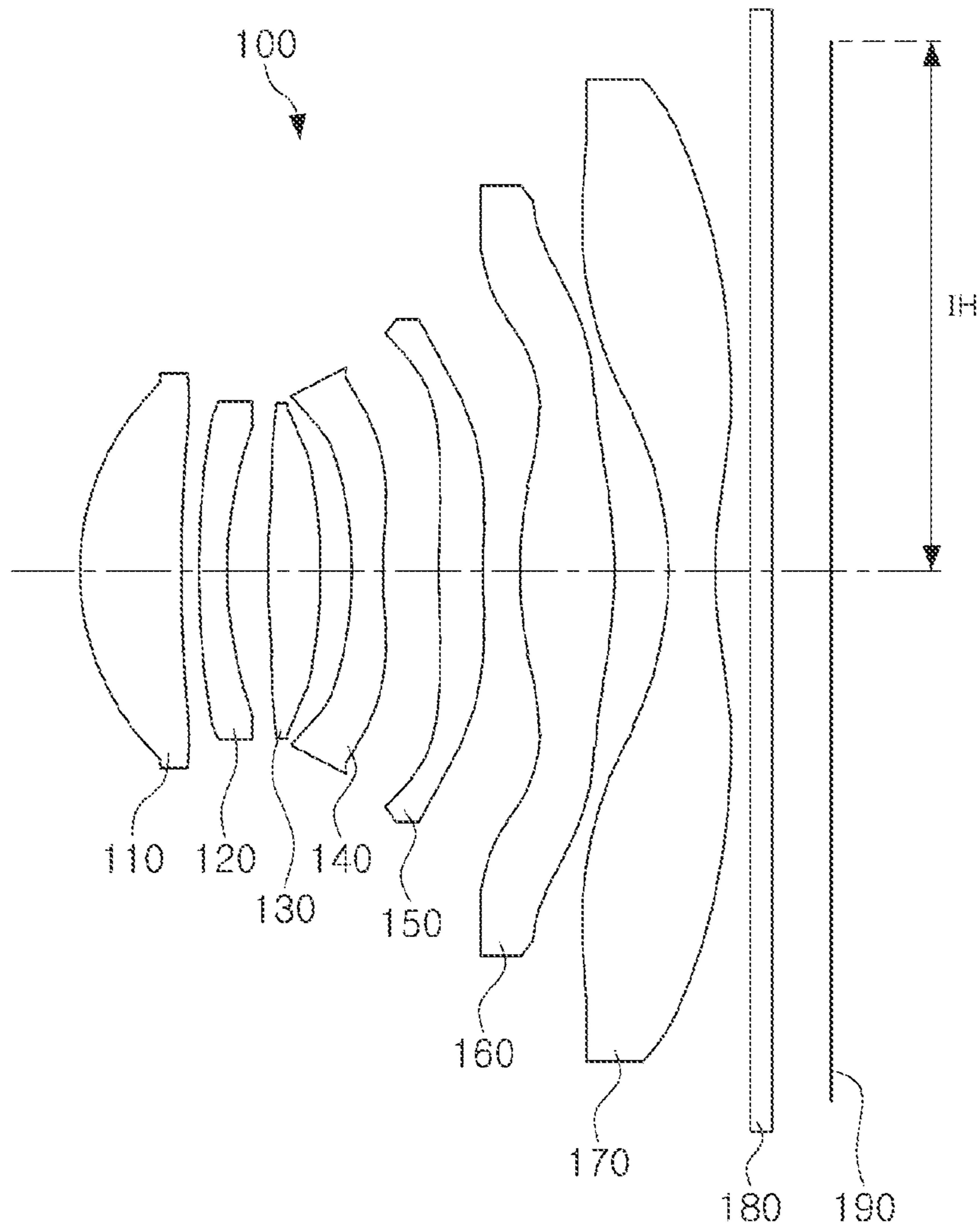


FIG. 1

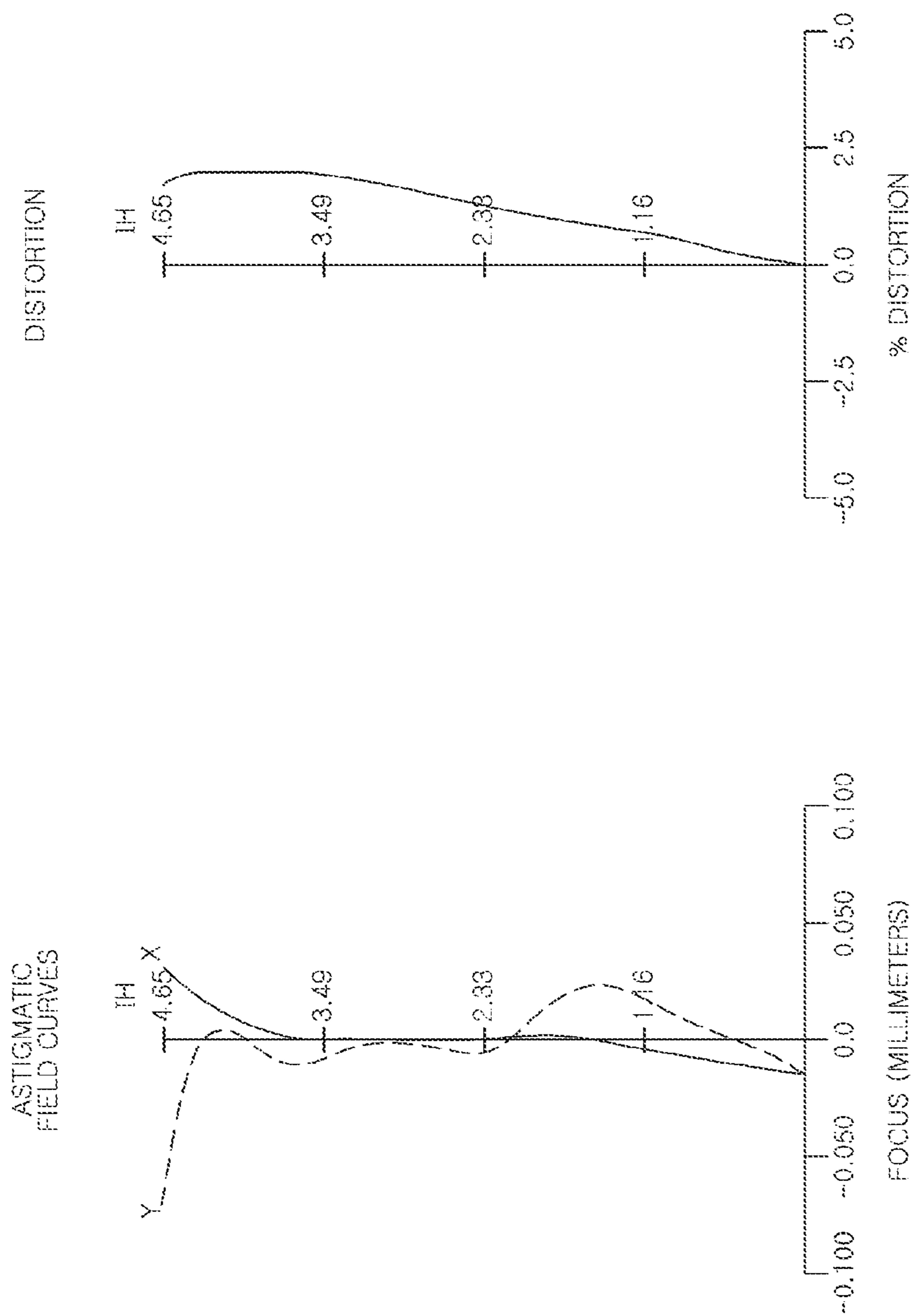


FIG. 2

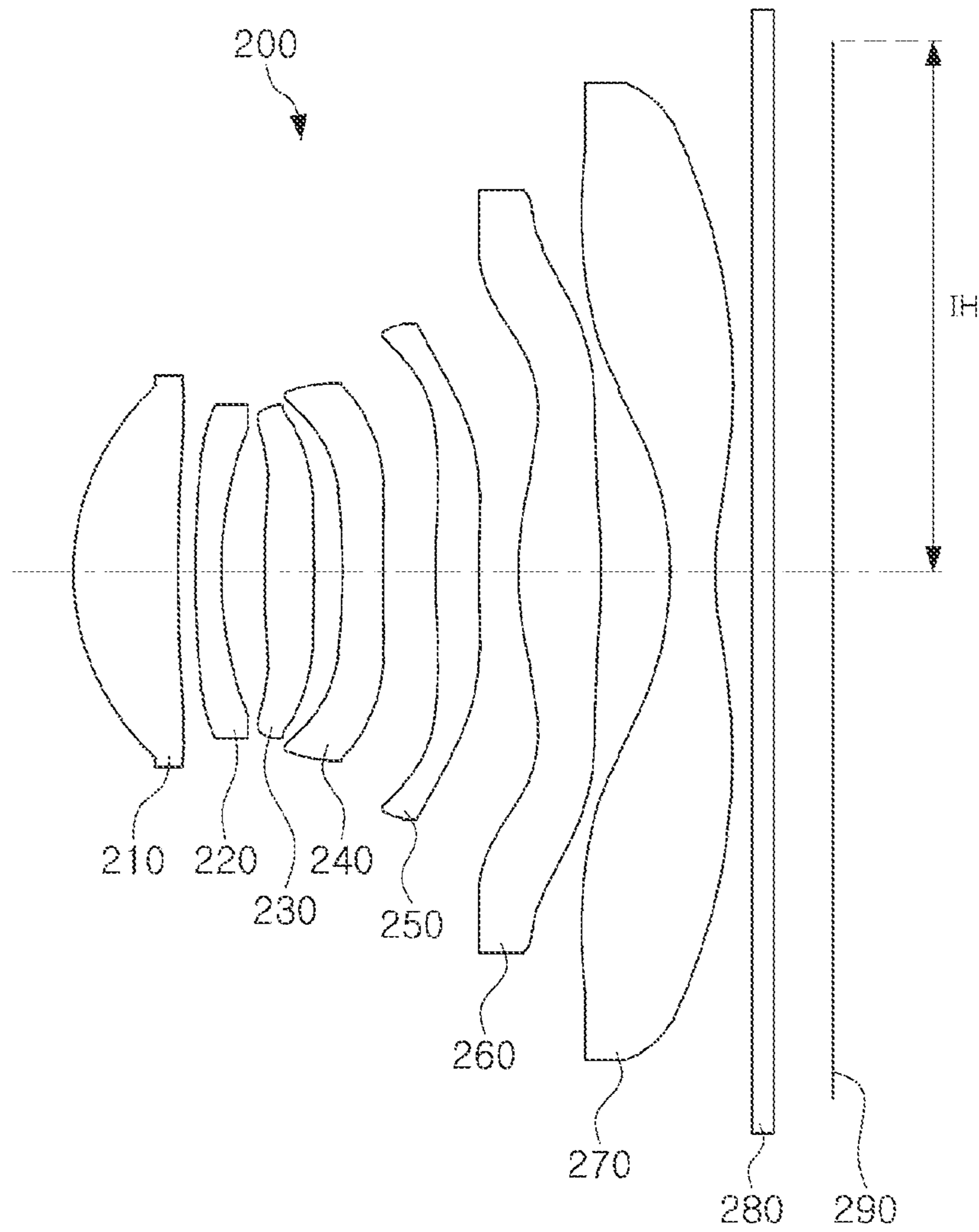


FIG. 3

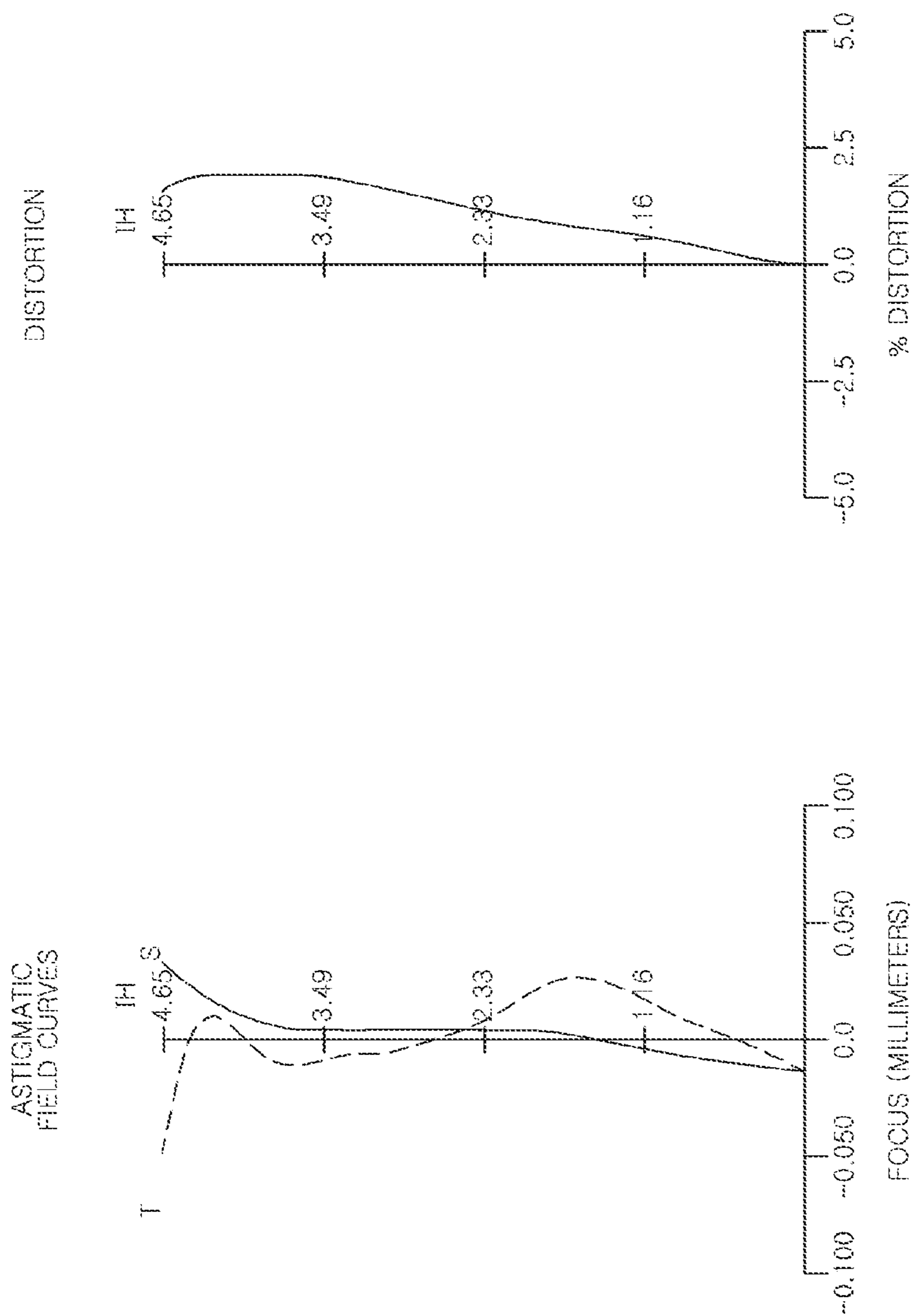


FIG. 4

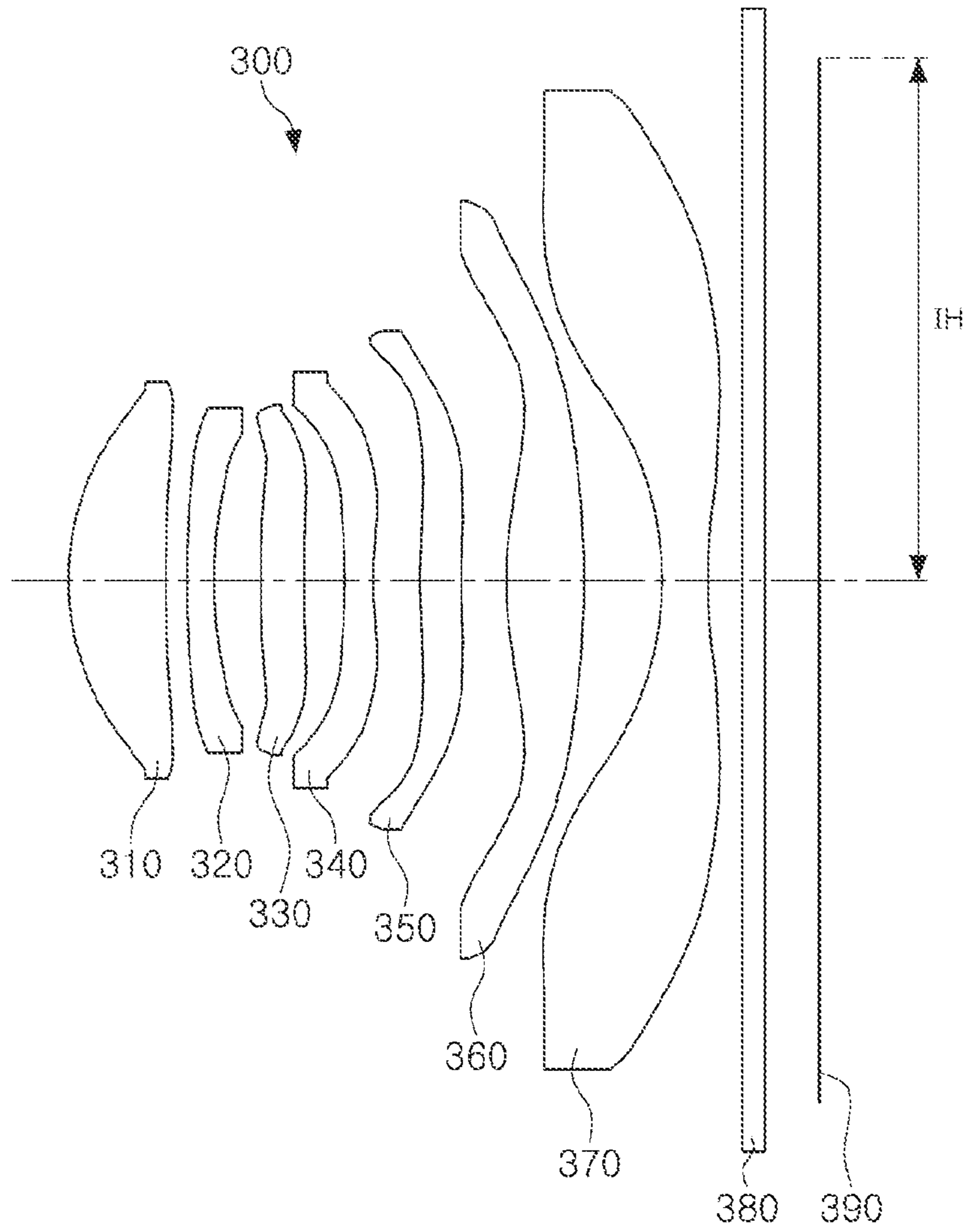


FIG. 5

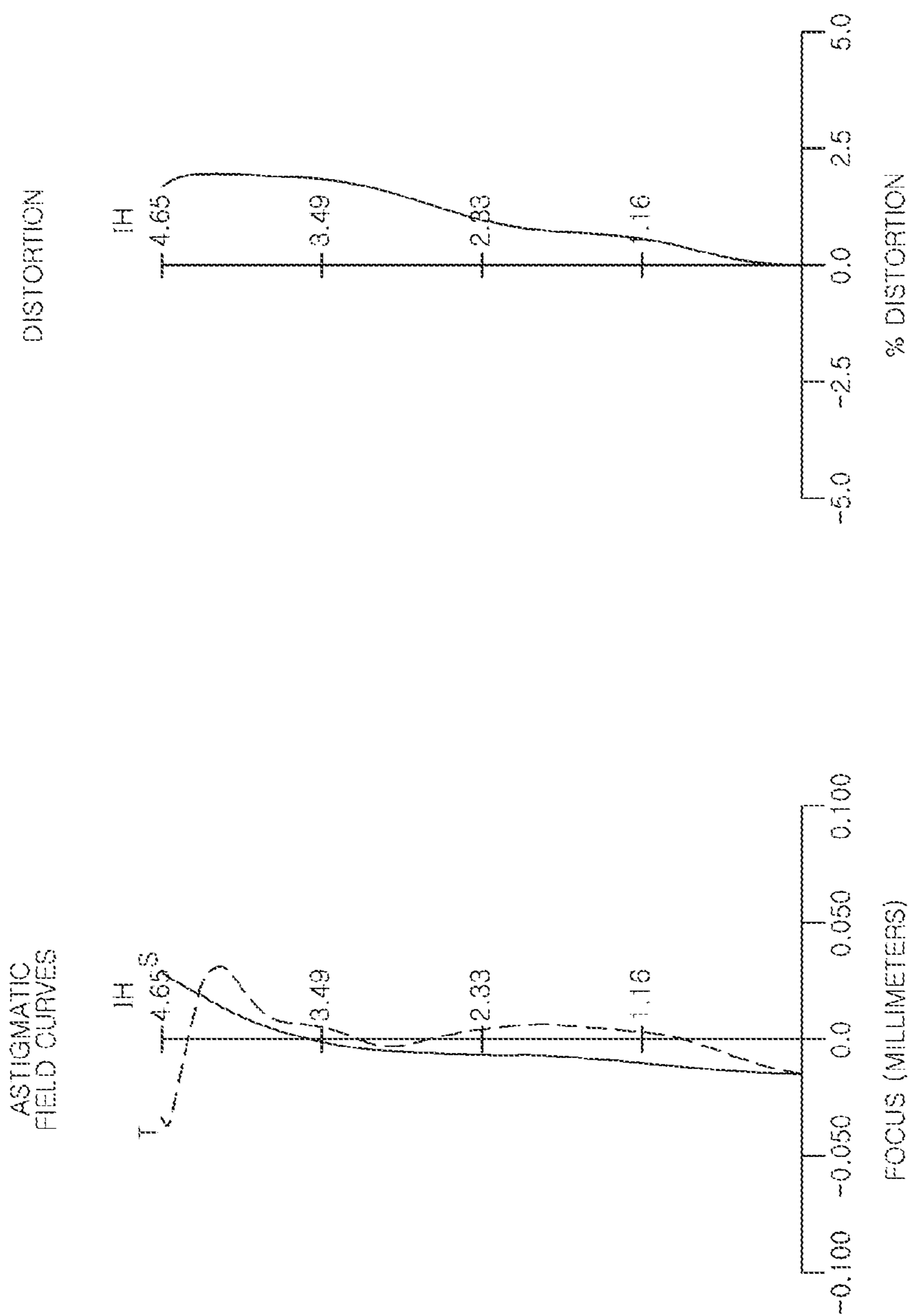


FIG. 6

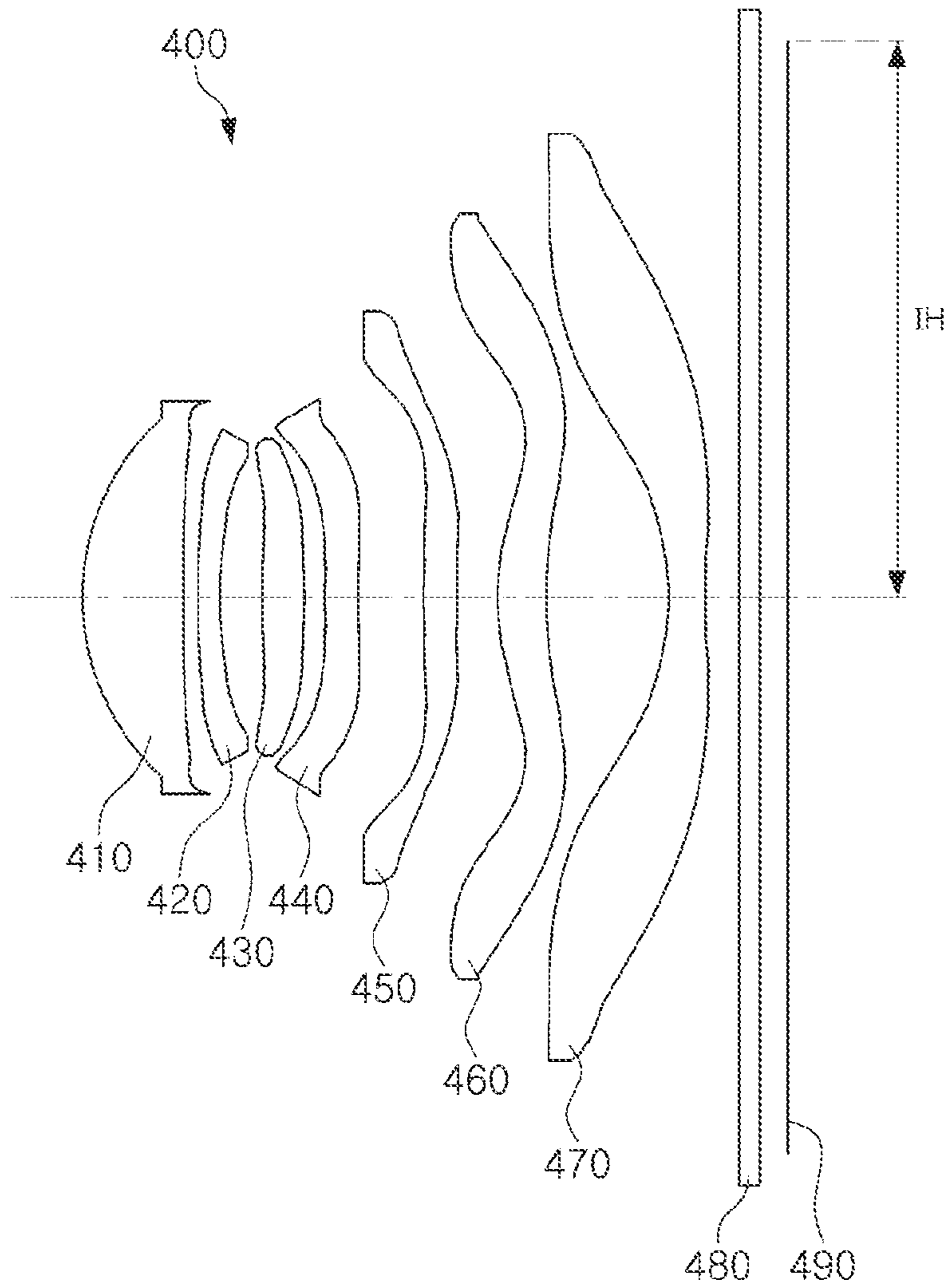


FIG. 7

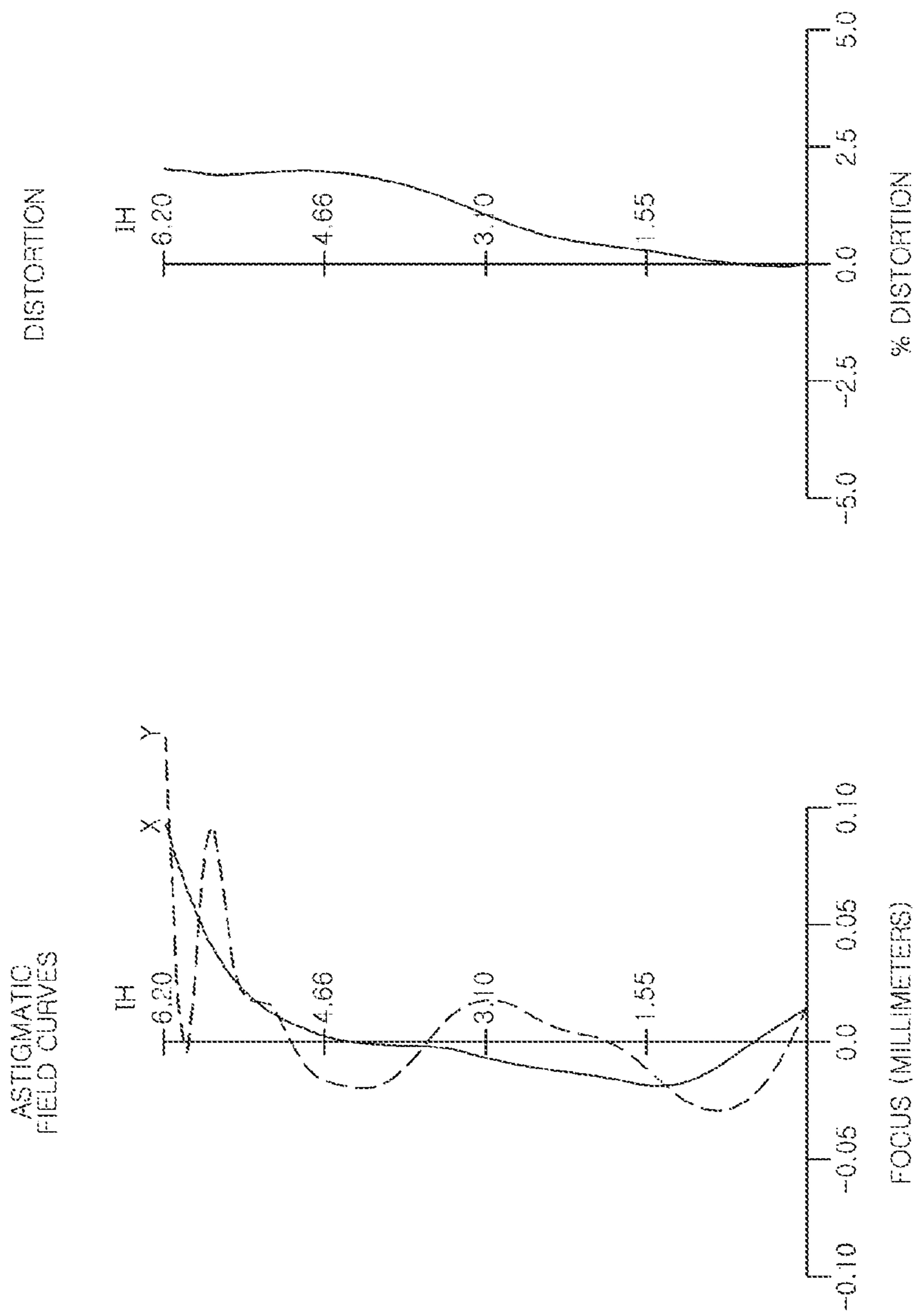


FIG. 8

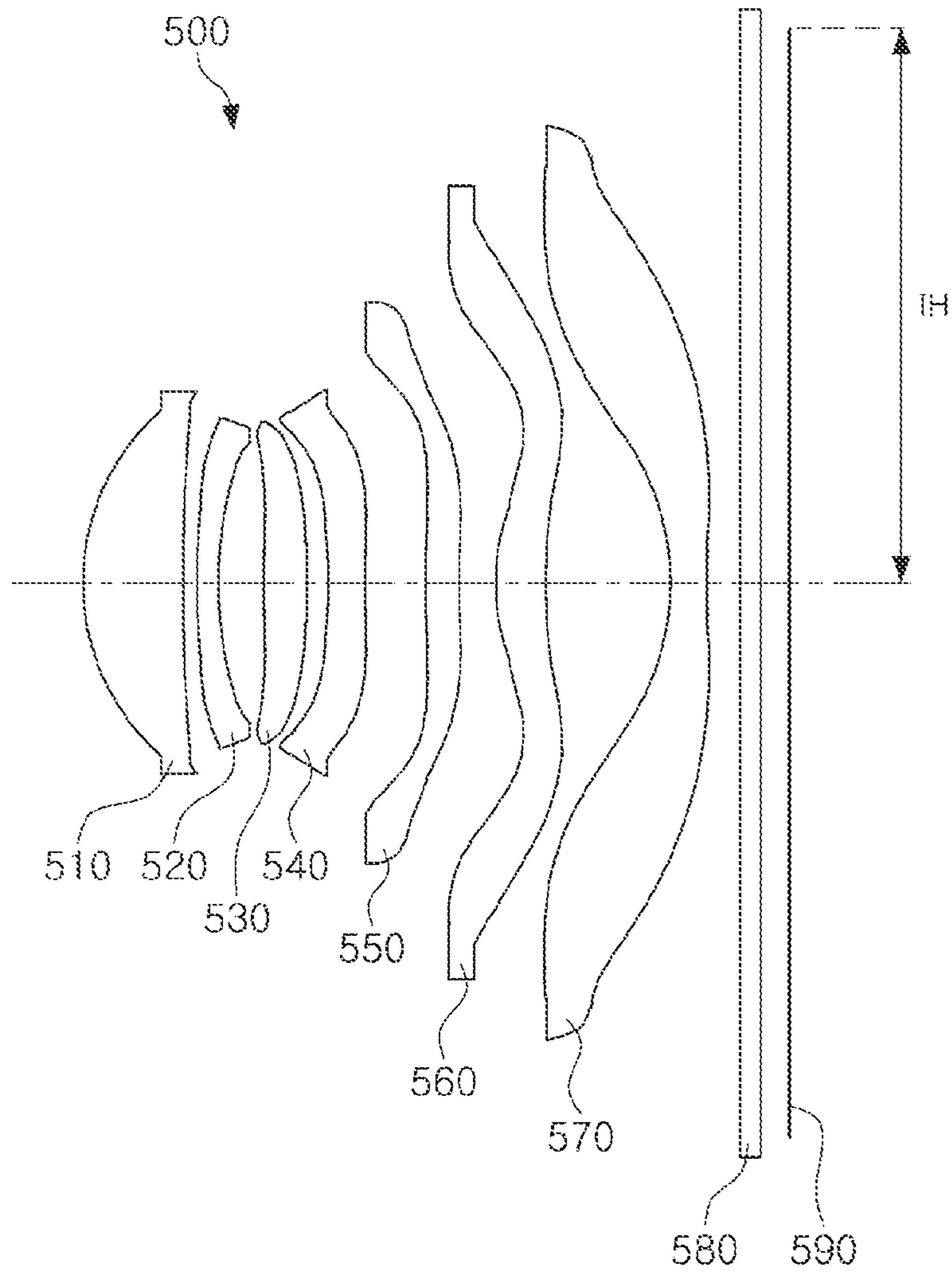


FIG. 9

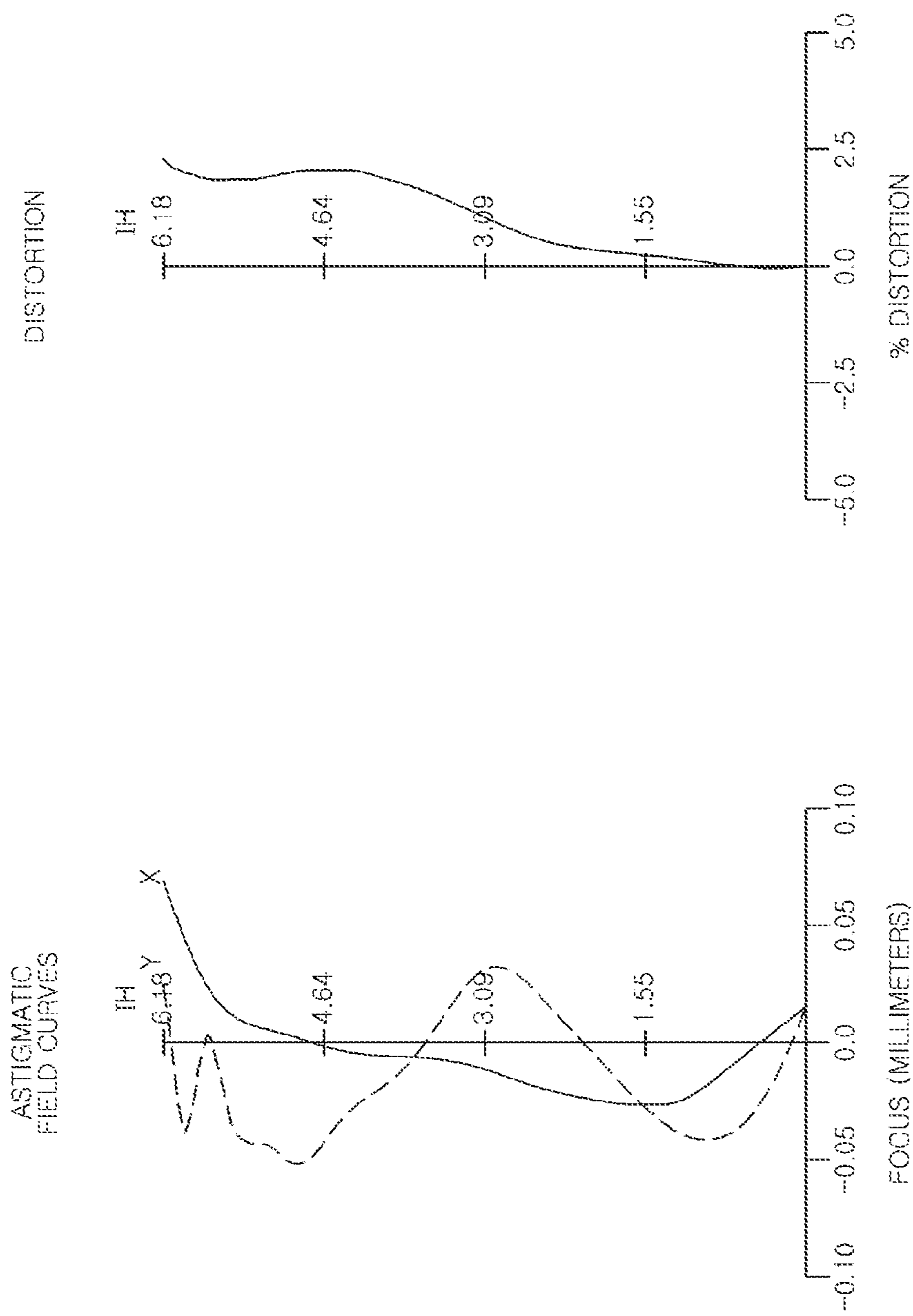


FIG. 10

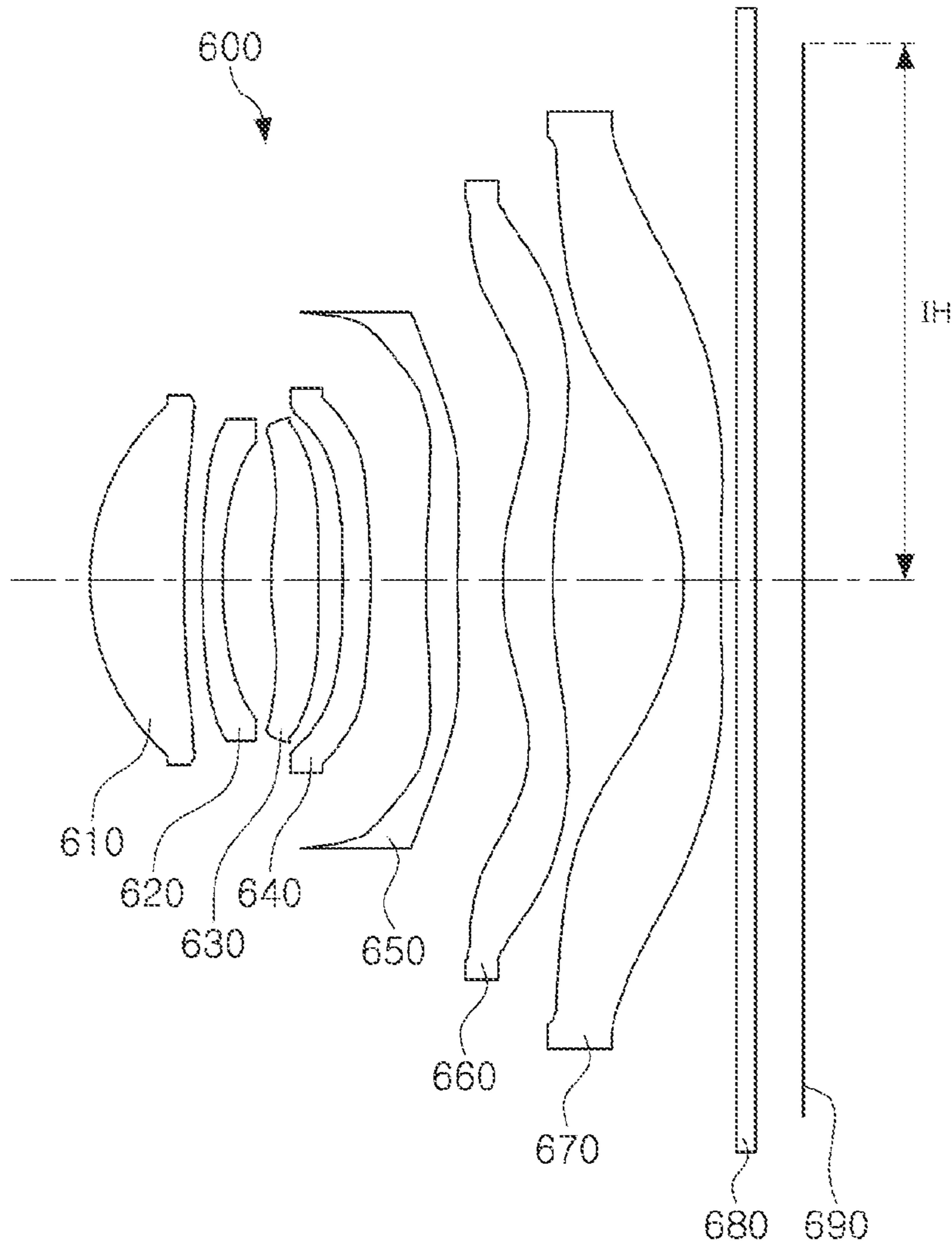


FIG. 11

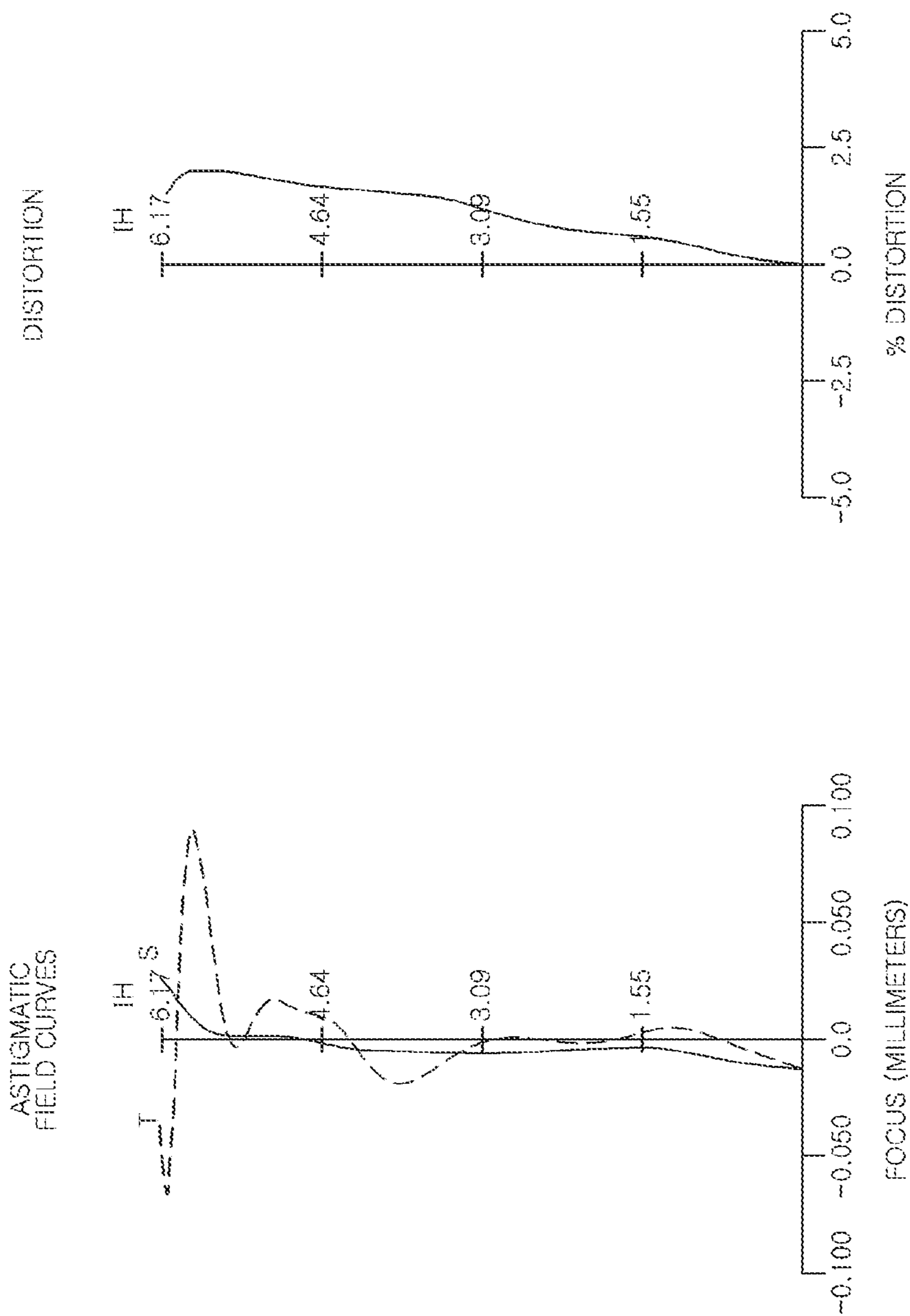


FIG. 12

**IMAGING LENS SYSTEM HAVING SEVEN
LENSES OF $+--++--$ OR $+--++--$
REFRACTIVE POWERS**

CROSS-REFERENCE TO RELATED
APPLICATIONS

This application is a continuation of U.S. Application Ser. No. 16/589,805 filed on Oct. 1, 2019, now U.S. Pat. No. 11,256,068 issued on Feb. 22, 2022, which claims the benefit under 35 USC 119(a) of Korean Patent Application No. 10-2019-0071406 filed on Jun. 17, 2019 in the Korean Intellectual Property Office, the entire disclosures of which are incorporated herein by reference for all purposes.

BACKGROUND

The following description relates to an imaging lens system including seven lenses.

A compact camera may be mounted on a wireless terminal. For example, the compact camera may be mounted on a front surface and a rear surface thereof, respectively. Such a compact camera is used for a variety of purposes such as outdoor scenery photography, indoor portrait photography and the like, such that performance that is not inferior to a general camera is required. However, it is difficult to realize high performance because a small camera is limited by a mounting space due to a size of a wireless terminal. Therefore, it is necessary to develop an imaging lens system capable of improving the performance of a compact camera without increasing the size of the compact camera.

SUMMARY

This Summary is provided to introduce a selection of concepts in simplified form that are further described below in the Detailed Description. This Summary is not intended to identify key features or essential features of the claimed subject matter, nor is it intended to be used as an aid in determining the scope of the claimed subject matter.

In one general aspect, an imaging lens system includes a first lens, a second lens, a third lens, a fourth lens, a fifth lens, a sixth lens, and a seventh lens, sequentially disposed at intervals from an object side of the imaging lens system. The imaging lens system satisfies $1.5 < Nd_5 < 1.6$, $30 < V_5 < 50$, and $TTL/2IH < 0.730$, where Nd_5 is a refractive index of the fifth lens, V_5 is an Abbe number of the fifth lens, TTL is a distance from an object side surface of the first lens to an imaging plane, and $2IH$ is a diagonal length of the imaging plane.

The imaging lens system may satisfy $10 < V_1 - V_3 < 10$, where V_1 is an Abbe number of the first lens and V_3 is an Abbe number of the third lens.

The imaging lens system may satisfy $25 < V_1 - V_4 < 45$, where V_1 is an Abbe number of the first lens and V_4 is an Abbe number of the fourth lens.

The imaging lens system may satisfy $0 < V_1 - V_5 < 20$, where V_1 is an Abbe number of the first lens.

A refractive index of the fourth lens may be greater than 1.6.

The imaging lens system may satisfy $1.5 < f_3/f$, where f is a focal length of the imaging lens system and f_3 is a focal length of the third lens.

The fourth lens may have negative refractive power.

The fifth lens may have a convex shape on an object side surface.

The imaging lens system may have an F-number of 2.0 or less.

In another general aspect, an imaging lens system includes a first lens, a second lens, a third lens, a fourth lens, a fifth lens, a sixth lens, and a seventh lens, sequentially disposed at intervals from an object side of the imaging lens system. An object side surface of the fourth lens or an object side surface of the fifth lens is concave, and an F-number is 2.0 or less. The imaging lens system satisfies $TTL/2IH < 0.73$, where TTL is a distance from an object side surface of the first lens to an imaging plane and $2IH$ is a diagonal length of the imaging plane.

The third lens may have positive refractive power.

The fifth lens may have a concave shape on an image side surface.

The seventh lens may have a concave shape on an object side surface.

A refractive index of the fifth lens may be greater than 1.5 and less than 1.6.

The imaging lens system may satisfy $-10 < V_1 - V_3 < 10$, where V_1 is an Abbe number of the first lens and V_3 is an Abbe number of the third lens.

The imaging lens system may satisfy $0 < V_1 - V_5 < 20$, where V_5 is an Abbe number of the fifth lens.

A refractive power of the first lens may be greater than a refractive power of the third lens, and a refractive power of the sixth lens may be greater than the refractive power of the third lens.

The first lens may have positive refractive power, the second lens may have negative refractive power, the third lens may have positive refractive power, the fourth lens may have negative refractive power, the sixth lens may have positive refractive power, and the seventh lens may have negative refractive power.

Other features and aspects will be apparent from the following detailed description, the drawings, and the claims.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a configuration diagram of an imaging lens system according to a first example.

FIG. 2 illustrates aberration curves of the imaging lens system illustrated in FIG. 1.

FIG. 3 is a configuration diagram of an imaging lens system according to a second example.

FIG. 4 illustrates aberration curves of the imaging lens system illustrated in FIG. 3.

FIG. 5 is a configuration diagram of an imaging lens system according to a third example.

FIG. 6 illustrates aberration curves of the imaging lens system illustrated in FIG. 5.

FIG. 7 is a configuration diagram of an imaging lens system according to a fourth example.

FIG. 8 illustrates aberration curves of the imaging lens system illustrated in FIG. 7.

FIG. 9 is a configuration diagram of an imaging lens system according to a fifth example.

FIG. 10 illustrates aberration curves of the imaging lens system illustrated in FIG. 9.

FIG. 11 is a configuration diagram of an imaging lens system according to a sixth example.

FIG. 12 illustrates aberration curves of the imaging lens system illustrated in FIG. 11.

Throughout the drawings and the detailed description, the same reference numerals refer to the same elements. The drawings may not be to scale, and the relative size, propor-

tions, and depiction of elements in the drawings may be exaggerated for clarity, illustration, and convenience.

DETAILED DESCRIPTION

The following detailed description is provided to assist the reader in gaining a comprehensive understanding of the methods, apparatuses, and/or systems described herein. However, various changes, modifications, and equivalents of the methods, apparatuses, and/or systems described herein will be apparent to one of ordinary skill in the art. The sequences of operations described herein are merely examples, and are not limited to those set forth herein, but may be changed as will be apparent to one of ordinary skill in the art, with the exception of operations necessarily occurring in a certain order. Also, descriptions of functions and constructions that would be well known to one of ordinary skill in the art may be omitted for increased clarity and conciseness.

The features described herein may be embodied in different forms, and are not to be construed as being limited to the examples described herein. Rather, the examples described herein have been provided so that this disclosure will be thorough and complete, and will fully convey the scope of the disclosure to one of ordinary skill in the art.

Herein, it is noted that use of the term “may” with respect to an example or embodiment, e.g., as to what an example or embodiment may include or implement, means that at least one example or embodiment exists in which such a feature is included or implemented while all examples and embodiments are not limited thereto.

Throughout the specification, when an element, such as a layer, region, or substrate, is described as being “on,” “connected to,” or “coupled to” another element, it may be directly “on,” “connected to,” or “coupled to” the other element, or there may be one or more other elements intervening therebetween. In contrast, when an element is described as being “directly on,” “directly connected to,” or “directly coupled to” another element, there can be no other elements intervening therebetween.

As used herein, the term “and/or” includes any one and any combination of any two or more of the associated listed items.

Although terms such as “first,” “second,” and “third” may be used herein to describe various members, components, regions, layers, or sections, these members, components, regions, layers, or sections are not to be limited by these terms. Rather, these terms are only used to distinguish one member, component, region, layer, or section from another member, component, region, layer, or section. Thus, a first member, component, region, layer, or section referred to in examples described herein may also be referred to as a second member, component, region, layer, or section without departing from the teachings of the examples.

Spatially relative terms such as “above,” “upper,” “below,” and “lower” may be used herein for ease of description to describe one element’s relationship to another element as shown in the figures. Such spatially relative terms are intended to encompass different orientations of the device in use or operation in addition to the orientation depicted in the figures. For example, if the device in the figures is turned over, an element described as being “above” or “upper” relative to another element will then be “below” or “lower” relative to the other element. Thus, the term “above” encompasses both the above and below orientations depending on the spatial orientation of the device. The device may also be oriented in other ways (for example,

rotated 90 degrees or at other orientations), and the spatially relative terms used herein are to be interpreted accordingly.

The terminology used herein is for describing various examples only, and is not to be used to limit the disclosure.

The articles “a,” “an,” and “the” are intended to include the plural forms as well, unless the context clearly indicates otherwise. The terms “comprises,” “includes,” and “has” specify the presence of stated features, numbers, operations, members, elements, and/or combinations thereof, but do not preclude the presence or addition of one or more other features, numbers, operations, members, elements, and/or combinations thereof.

Due to manufacturing techniques and/or tolerances, variations of the shapes shown in the drawings may occur. Thus, the examples described herein are not limited to the specific shapes shown in the drawings, but include changes in shape that occur during manufacturing.

The features of the examples described herein may be combined in various ways as will be apparent after an understanding of the disclosure of this application. Further, although the examples described herein have a variety of configurations, other configurations are possible as will be apparent after an understanding of the disclosure of this application.

Herein, a first lens means a lens closest to an object (or a subject), and a seventh lens means a lens closest to an imaging surface (or an image sensor). Herein, a unit of a curvature of radius, a thickness, TTL (a distance from an object side surface of the first lens to an imaging surface), 2IH (a diagonal length of the imaging surface), IH ($\frac{1}{2}$ of 2IH), and a focal length of the lens may be in millimeters (mm).

The thickness of the lens, the distance between the lenses, and the TTL are a distance from an optical axis of the lens. In an explanation of a shape of each lens, a convex shape of one surface may mean that a paraxial region of the surface may be convex, and a concave shape of one surface may mean that a paraxial region of the surface may be concave. Therefore, even when one surface of the lens is described as having a convex shape, an edge portion of the lens may be concave. Similarly, even when one surface of the lens is described as having a concave shape, an edge portion of the lens may be convex.

The imaging lens system includes seven lenses. For example, the imaging lens system may include a first lens, a second lens, a third lens, a fourth lens, a fifth lens, a sixth lens, and a seventh lens, sequentially disposed from an object side. The first to the seventh lenses are disposed with a predetermined interval between successive/adjacent lenses. For example, each lens does not contact an image side surface and an object side surface of a neighboring lens in the paraxial region. An F-number of the imaging lens system may be 2.0 or less.

The first lens has refractive power. For example, the first lens has positive refractive power. The first lens has a convex shape on one surface. For example, the first lens has a convex shape on an object side surface.

The first lens includes an aspherical surface. For example, both surfaces of the first lens may be aspherical. The first lens may be made of a material having high light transmittance and excellent workability. For example, the first lens may be made of a plastic material. The first lens has a low refractive index. For example, the refractive index of the first lens may be less than 1.6.

The second lens has refractive power. For example, the second lens may have negative refractive power. The second

lens has a convex shape on one surface. For example, the second lens may have a convex shape on an object side surface.

The second lens includes an aspherical surface. For example, both surfaces of the second lens may be aspherical. The second lens may be made of a material having high light transmittance and excellent workability. For example, the second lens may be made of a plastic material. However, the material of the second lens is not limited to plastic. For example, the second lens may be made of a plastic material. The second lens has a refractive index greater than the refractive index of the first lens. For example, the refractive index of the second lens may be 1.6 or greater. In addition, a lower limit value of the refractive index of the second lens may be further increased. For example, the refractive index of the second lens may be 1.67 or greater.

The third lens has refractive power. For example, the third lens has positive refractive power. At least one surface of the third lens may have a convex shape. For example, the third lens may have a convex shape on an object side surface.

The third lens includes an aspherical surface. For example, both surfaces of the third lens may be aspherical. The third lens may be made of a material having high light transmittance and excellent workability. For example, the third lens may be made of a plastic material. The third lens has a refractive index substantially similar to the refractive index of the first lens. For example, the refractive index of the third lens may be less than 1.6.

The fourth lens has refractive power. For example, the fourth lens has negative refractive power. The fourth lens has a concave shape on one surface. For example, the fourth lens may have a concave shape on an object side surface.

The fourth lens includes an aspherical surface. For example, both surfaces of the fourth lens may be aspherical. The fourth lens may be made of a material having high light transmittance and excellent workability. For example, the fourth lens may be made of a plastic material. The fourth lens has a refractive index greater than the refractive index of the first lens. For example, the refractive index of the fourth lens may be 1.6 or greater.

The fifth lens has refractive power. For example, the fifth lens may have positive or negative refractive power. The fifth lens has a convex shape on one surface. For example, the fifth lens may have a convex shape on an object side surface. The fifth lens may have a shape having an inflection point. For example, an inflection point may be formed on at least one surface of the object side surface and an image side surface of the fifth lens.

The fifth lens includes an aspherical surface. For example, both surfaces of the fifth lens may be aspherical. The fifth lens may be made of a material having high light transmittance and excellent workability. For example, the fifth lens may be made of a plastic material. The fifth lens may have a refractive index substantially similar to the refractive index of the first lens. For example, the refractive index of the fifth lens may be less than 1.6. As another example, the refractive index of the fifth lens may be greater than 1.5 and smaller than 1.6. An Abbe number of the fifth lens may be greater than 30 and less than 50.

The sixth lens has refractive power. For example, the sixth lens has positive refractive power. The sixth lens has a convex shape on one surface. For example, the sixth lens may have a convex shape on an object side surface. The sixth lens may have a shape having an inflection point. For example, an inflection point may be formed on at least one surface of the object side surface and the image side surface of the sixth lens.

The sixth lens includes an aspherical surface. For example, both surfaces of the sixth lens may be aspherical. The sixth lens may be made of a material having high light transmittance and excellent workability. For example, the sixth lens may be made of a plastic material. The sixth lens has a refractive index substantially similar to the refractive index of the fifth lens. For example, the refractive index of the sixth lens may be less than 1.6.

The seventh lens has refractive power. For example, the seventh lens has negative refractive power. The seventh lens may have a concave shape on at least one surface. For example, the seventh lens may have a concave shape on an object side surface. The seventh lens may have a shape having an inflection point. For example, one or more inflection points may be formed on at least one surface of the object side surface and the image side surface of the seventh lens.

The seventh lens includes an aspherical surface. For example, both surfaces of the seventh lens may be aspherical. The seventh lens may be made of a material having high light transmittance and excellent workability. For example, the seventh lens may be made of a plastic material. The seventh lens may have a refractive index substantially similar to the refractive index of the sixth lens. For example, the refractive index of the seventh lens may be less than 0.6.

The first to seventh lenses include aspherical surfaces as described above. The aspherical surfaces of the first to seventh lenses may be represented by the following Equation

$$z = \frac{cr^2}{1 + \sqrt{1 - (1+k)c^2r^2}} + Ar^4 + Br^6 + Cr^8 + Dr^{10} + Er^{12} + Fr^{14} + Gr^{16} + Hr^{18} + Jr^{20} \quad \text{Equation 1}$$

In Equation 1, c is a reciprocal of a radius of curvature of the lens, k is a conic constant, r is a distance from any point on an aspherical surface to an optical axis, A through J are aspherical surface constants, and Z (or SAG) is a height in an optical axis direction from any point on an aspheric surface to an apex of the aspheric surface.

The imaging lens system further includes a filter, an image sensor, and a stop.

The filter is disposed between the seventh lens and the image sensor. The filter may block some wavelengths of light. For example, the filter may block infrared light wavelengths. The image sensor forms an imaging plane on which light refracted through the first lens to the seventh lens may be formed. The image sensor converts an optical signal into an electrical signal. For example, the image sensor may convert an optical signal incident on the imaging plane into an electrical signal. The stop is disposed to adjust an amount of light incident on the lens. For example, the stop may be disposed between the first lens and the second lens or disposed between the second lens and the third lens.

The imaging lens system may satisfy at least one of the following conditional expressions.

$$\text{Conditional Expression 1: } 0 < f1/f < 2.0$$

$$\text{Conditional Expression 2: } 25 < V1 - V2 < 45$$

$$\text{Conditional Expression 3: } -10 < V1 - V3 < 10$$

-continued

Conditional Expression 4: $25 < V1 - V4 < 45$ Conditional Expression 5: $0 < V1 - V5 < 20$ Conditional Expression 6: $-3.5 < f2/f < 0$ Conditional Expression 7: $1.5 < f3/f$ Conditional Expression 8: $f4/f < 0$ Conditional Expression 9: $f5/f < 0$ Conditional Expression 10: $0 < f6/f$ Conditional Expression 11: $f7/f < 0$ Conditional Expression 12: $TTL/f < 1.4$ Conditional Expression 13: $-1.0 < f1/f2 < 0$ Conditional Expression 14: $-2.0 < f2/f3 < 0$ Conditional Expression 15: $BFL/f < 0.4$ Conditional Expression 16: $D12/f < 0.1$ Conditional Expression 17: $SD5/IH < 0.6$ Conditional Expression 18: $0.7 < SD6/IH$ Conditional Expression 19: $0.8 < SD7/IH$ Conditional Expression 20: $TTL/2IH < 0.730$ Conditional Expression 21: $30 < V5 < 50$

In the imaging lens system, the refractive power of the first lens is greater than the refractive power of the third lens, and the refractive power of the sixth lens is greater than the refractive power of the third lens. For example, the first lens, the third lens, and the sixth lens may satisfy all of the following conditional expressions.

Conditional Expression 22: $1/f3 < 1/f1$ Conditional Expression 23: $1/f3 < 1/f6$

In the conditional expressions, f is a focal length of the imaging lens system, $f1$ is a focal length of the first lens, $f2$ is a focal length of the second lens, $f3$ is a focal length of the third lens, $f4$ is a focal length of the fourth lens, $f5$ is a focal length of the fifth lens, $f6$ is a focal length of the sixth lens, and $f7$ is a focal length of the seventh lens, $V1$ is an Abbe number of the first lens, $V2$ is an Abbe number of the second lens, $V3$ is an Abbe number of the third lens, $V4$ is an Abbe number of the fourth lens, and $V5$ is an Abbe number of the fifth lens, TTL is a distance from an object side surface of the first lens to an imaging plane, BFL is a distance from an image side surface of the seventh lens to an imaging plane, $D12$ is a distance from the image side surface of the first lens to an object side surface of the second lens, $SD5$ is an effective radius of the fifth lens, $SD6$ is an effective radius of the sixth lens, and $2IH$ is a diagonal length of the imaging plane.

Conditional expression 1 is a condition for limiting appropriate refractive power of the first lens. The first lens that is outside of a numerical range of the conditional expression increases a focal length of the imaging lens system, making miniaturization of the imaging lens system difficult. Conditional expressions 2 to 5 are conditions for reducing chromatic aberrations of the imaging lens system. Conditional expressions 6 to 11 are conditions for limiting appropriate

refractive power of the second lens to the seventh lens, respectively. A lens that is outside of the numerical range of the conditional expressions is too high or too low to correct aberrations through each lens. Conditional expressions 12 and 15 are conditions for miniaturization of the imaging lens system. The imaging lens system that is outside of the upper limit value of the conditional expression is not suitable for a portable terminal because the distance from the object side surface of the first lens to the imaging plane is outside of the range that can be mounted on the portable terminal or the focal length of the imaging lens system is too short. Conditional expressions 13 and 14 are conditions for limiting an appropriate focal length of the first lens to the third lens. A lens that is outside of the numerical value of the conditional expression may cause aberration characteristics to deteriorate because the refractive power thereof may be too high. Conditional expression 16 is a condition for reducing chromatic aberrations through the first lens and the second lens. For example, if a distance between the first lens and the second lens is outside of the upper limit value of the conditional expression, it is difficult to improve the chromatic aberrations according to Abbe number deviation of the first lens and the second lens. Conditional expressions 17 to 19 are conditions for reducing a flare phenomenon. If effective radii of the fifth lens to the seventh lens are outside of the upper limit value or the lower limit value of the conditional expression, a sweep angle of each lens becomes wider, such that flare characteristics may be deteriorated.

An imaging lens system according to a first example will be described with reference to FIG. 1.

An imaging lens system **100** includes a first lens **110**, a second lens **120**, a third lens **130**, a fourth lens **140**, a fifth lens **150**, a sixth lens **160**, and a seventh lens **170**.

The first lens **110** has positive refractive power, and the first lens **110** has a convex shape on an object side surface and a concave shape on an image side surface. The second lens **120** has negative refractive power, and the second lens **120** has a convex shape on an object side surface and a concave shape on an image side surface. The third lens **130** has positive refractive power, and the third lens **130** has a convex shape on an object side surface and a convex shape on an image side surface. The fourth lens **140** has negative refractive power, and the fourth lens **140** has a concave shape on an object side surface and a concave shape on an image side surface. The fifth lens **150** has negative refractive power, and the fifth lens **150** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the fifth lens **150** has a shape in which an inflection point is formed on the object side surface and the image side surface. The sixth lens **160** has positive refractive power, and the sixth lens **160** has a convex shape on an object side surface and a convex shape on an image side surface. Further, the sixth lens **160** has a shape in which an inflection point is formed on the object side surface and the image side surface. The seventh lens **170** has negative refractive power, and the seventh lens **170** has a concave shape on an object side surface and a concave shape on an image side surface. Further, the seventh lens **170** has a shape in which an inflection point is formed on the object side surface and the image side surface.

The imaging lens system **100** further includes a filter **180** and an image sensor **190**. The filter **180** is disposed between the seventh lens **170** and the image sensor **190**. For reference, although not shown in the drawings, a stop may be disposed between the second lens **120** and the third lens **130**.

The imaging lens system **100**, configured as described above, illustrates aberration characteristics as shown in FIG.

2. Tables 1 and 2 illustrate lens characteristics and aspherical surface values of the imaging lens system **100**.

TABLE 1

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number
S1	First lens	2.31	0.912	1.544	56.1
S2		10.53	0.164		
S3		6.94	0.234		
S4	Third lens	3.85	0.422	1.544	56.1
S5		29.14	0.398		
S6		-24.16	0.264		
S7	Fourth lens	-15.48	0.384	1.661	20.4
S8		60.01	0.421		
S9	Fifth lens	6.03	0.391	1.568	37.4
S10		5.66	0.341		
S11	Sixth lens	3.16	0.721	1.544	56.1
S12		-6.06	0.608		
S13		-4.75	0.400		
S14	Seventh lens	2.67	0.305	1.514	64.1
S15		Infinity	0.210		
S16		Infinity	0.505		
Imaging Plane	Imaging Plane	Infinity	0.015		

TABLE 2

Ex. 1	K	A	B	C	D	E	F	G	H	J
S1	-1.0366	0.0116	-0.0008	0.0048	-0.0062	0.0047	-0.0020	0.0005	-4.53E-05	0
S2	23.6958	-0.0234	0.0212	-0.0193	0.0153	-0.0096	0.0038	-0.0008	0.0001	0
S3	14.9297	-0.0630	0.0570	-0.0346	0.0148	-0.0034	-0.0002	0.0004	-0.0001	0
S4	0.1548	-0.0490	0.0678	-0.0816	0.1019	-0.0934	0.0551	-0.0183	0.0027	0
S5	0	-0.0423	0.0589	-0.1884	0.3228	-0.3302	0.1974	-0.0637	0.0086	0
S6	1.2398	-0.0405	0.0131	-0.0336	0.0382	-0.0292	0.0134	-0.0031	0.0003	0
S7	0.00E+00	-0.0791	0.0820	-0.1699	0.2105	-0.1653	0.0785	-0.0206	0.0023	0
S8	0.00E+00	-0.0733	0.0632	-0.0860	0.0773	-0.0452	0.0163	-0.0033	0.0003	0
S9	0.00E+00	-0.1024	0.0794	-0.0551	0.0259	-0.0082	0.0017	-0.0002	1.10E-05	0
S10	-64.3279	-0.1135	0.0639	-0.0370	0.0160	-0.0045	0.0008	-0.0001	3.26E-06	0
S11	-6.4594	-0.0209	0.0062	-0.0036	0.0001	0.0002	-4.09E-05	3.12E-06	-8.70E-08	0
S12	-96.2611	0.0152	0.0068	-0.0073	0.0021	-0.0003	2.36E-05	-9.62E-07	1.55E-08	0
S13	-8.2127	-0.0827	0.0327	-0.0059	0.0006	-3.90E-05	1.43E-06	-2.71E-08	1.86E-10	0
S14	-13.2198	-0.0455	0.0159	-0.0036	0.0005	-4.84E-05	2.91E-06	-1.07E-07	2.19E-09	0

An imaging lens system according to a second example will be described with reference to FIG. 3.

An imaging lens system **200** includes a first lens **210**, a second lens **220**, a third lens **230**, a fourth lens **240**, a fifth lens **250**, a sixth lens **260**, and a seventh lens **270**.

The first lens **210** has positive refractive power, and the first lens **210** has a convex shape on an object side surface and a concave shape on an image side surface. The second lens **220** has negative refractive power, and the second lens **220** has a convex shape on an object side surface and a concave shape on an image side surface. The third lens **230** has positive refractive power, and the third lens **230** has a convex shape on an object side surface and a convex shape on an image side surface. The fourth lens **240** has negative refractive power, and the fourth lens **240** has a concave shape on an object side surface and a concave shape on an image side surface. The fifth lens **250** has negative refractive power, and the fifth lens **250** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the fifth lens **250** has a shape in which an inflection point is formed on the object side surface and the image side surface. The sixth lens **260** has positive refractive power, and the sixth lens **260** has a convex shape on an object side

surface and a convex shape on an image side surface. Further, the sixth lens **260** has a shape in which an inflection point is formed on the object side surface and the image side surface. The seventh lens **270** has negative refractive power, and the seventh lens **270** has a concave shape on an object side surface and a concave shape on an image side surface. Further, the seventh lens **270** has a shape in which an inflection point is formed on the object side surface and the image side surface.

The imaging lens system **200** further includes a filter **280** and an image sensor **290**. The filter **280** is disposed between the seventh lens **270** and the image sensor **290**. For reference, although not shown in the drawings, a stop may be disposed between the second lens **220** and the third lens **230**.

The imaging lens system **200** illustrates aberration characteristics as shown in FIG. 4. Tables 3 and 4 illustrate lens characteristics and aspherical surface values of the imaging lens system **200**.

TABLE 3

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number
S1	First lens	2.31	0.902	1.544	56.1
S2		10.41	0.165		

TABLE 3-continued

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number
S3	Second lens	6.90	0.230	1.671	19.3
S4		3.85	0.425		
S5	Third lens	29.98	0.400	1.544	56.1
S6		-22.77	0.254		
S7	Fourth lens	-14.79	0.381	1.661	20.4
S8		76.35	0.433		
S9	Fifth lens	5.97	0.385	1.568	37.4
S10		5.62	0.350		
S11	Sixth lens	3.16	0.724	1.544	56.1
S12		-6.24	0.611		
S13	Seventh lens	-4.77	0.404	1.544	56.1
S14		2.67	0.305		
S15	Filter	Infinity	0.210	1.514	64.1
S16		Infinity	0.506		
Imaging plane	Imaging plane	Infinity	0.015		

TABLE 4

Ex. 2	K	A	B	C	D	E	F	G	H	J
S1	-1.0458	0.0110	0.0016	0.0001	-0.0010	0.0013	-0.0008	0.0002	-2.34E-05	-1.89E-11
S2	23.3325	-0.0237	0.0220	-0.0210	0.0169	-0.0102	0.0039	-0.0008	0.0001	-1.89E-11
S3	14.9068	-0.0626	0.0550	-0.0321	0.0139	-0.0039	0.0005	0.0001	-4.75E-05	-1.89E-11
S4	0.1571	-0.0490	0.0681	-0.0849	0.1100	-0.1027	0.0608	-0.0201	0.0029	-1.89E-11
S5	0	-0.0435	0.0688	-0.2161	0.3638	-0.3653	0.2149	-0.0683	0.0091	-1.89E-11
S6	13.4162	-0.0370	0.0024	-0.0147	0.0143	-0.0093	0.0034	-0.0004	-4.30E-05	-1.89E-11
S7	0	-0.0731	0.0587	-0.1264	0.1595	-0.1292	0.0637	-0.0174	0.0020	-1.89E-11
S8	0	-0.0725	0.0621	-0.0871	0.0798	-0.0473	0.0173	-0.0035	0.0003	-1.89E-11
S9	0	-0.1048	0.0841	-0.0600	0.0290	-0.0096	0.0021	-0.0003	1.49E-05	-1.89E-11
S10	-63.2478	-0.1133	0.0633	-0.0349	0.0141	-0.0038	0.0006	-0.0001	2.56E-06	-1.89E-11
S11	-6.5212	-0.0205	0.0060	-0.0035	0.0001	0.0002	-3.94E-05	2.98E-06	-8.24E-08	-1.89E-11
S12	-98.4791	0.0159	0.0055	-0.0065	0.0019	-0.0003	2.00E-05	-7.81E-07	1.18E-08	-1.89E-11
S13	-7.8013	-0.0814	0.0318	-0.0057	0.0006	-3.69E-05	1.34E-06	-2.46E-08	1.48E-10	-1.89E-11
S14	-13.1752	-0.0450	0.0157	-0.0036	0.0005	-0.0001	3.37E-06	-1.37E-07	3.16E-09	-3.20E-11

An imaging lens system according to a third example will be described with reference to FIG. 5.

An imaging lens system 300 includes a first lens 310, a second lens 320, a third lens 330, a fourth lens 340, a fifth lens 350, a sixth lens 360, and a seventh lens 370.

The first lens 310 has positive refractive power, and the first lens 310 has a convex shape on an object side surface and a concave shape on an image side surface. The second lens 320 has negative refractive power, and the second lens 320 has a convex shape on an object side surface and a concave shape on an image side surface. The third lens 330 has positive refractive power, and the third lens 330 has a convex shape on an object side surface and a concave shape on an image side surface. The fourth lens 340 has negative refractive power, and the fourth lens 340 has a concave shape on an object side surface and a concave shape on an image side surface. The fifth lens 350 has positive refractive power, and the fifth lens 350 has a convex shape on an object side surface and a concave shape on an image side surface. Further, the fifth lens 350 has a shape in which an inflection point is formed on the object side surface and the image side surface. The sixth lens 360 has positive refractive power, and the sixth lens 360 has a convex shape on an object side surface and a convex shape on an image side surface. Further, the sixth lens 360 has a shape in which an inflection point is formed on the object side surface and the image side surface. The seventh lens 370 has negative refractive power, and the seventh lens 370 has a concave shape on an object side surface and a concave shape on an image side surface. Further, the seventh lens 370 has a shape in which an inflection point is formed on the object side surface and the image side surface.

The imaging lens system 300 further includes a filter 380 and an image sensor 390. The filter 380 is disposed between the seventh lens 370 and the image sensor 390. For refer-

ence, although not shown in the drawings, a stop may be disposed between the second lens 320 and the third lens 330.

The imaging lens system 300 illustrates aberration characteristics as shown in FIG. 6. Tables 5 and 6 illustrate lens characteristics and aspherical surface values of the imaging lens system 300.

TABLE 5

Surface number	Reference	Radius of curvature	Thickness/ distance	Refractive index	Abbe number
S1	First lens	2.31	0.872	1.544	56.1
S2		9.70	0.188		
S3	Second lens	6.75	0.230	1.671	19.3
S4		3.80	0.489		
S5	Third lens	16.19	0.385	1.544	56.1
S6		167.06	0.300		
S7	Fourth lens	-23.80	0.305	1.661	20.4
S8		40.38	0.366		
S9	Fifth lens	5.35	0.370	1.568	37.4
S10		5.32	0.395		
S11	Sixth lens	3.24	0.686	1.544	56.1
S12		-6.56	0.717		
S13	Seventh lens	-3.58	0.400	1.544	56.1
S14		3.42	0.305		
S15	Filter	Infinity	0.210	1.514	64.1
S16		Infinity	0.467		
Imaging plane	Imaging plane	Infinity	0.015		

TABLE 6

Ex. 3	K	A	B	C	D	E	F	G	H	J
S1	-1.1399	0.0126	-0.0026	0.0080	-0.0100	0.0073	-0.0031	0.0007	-0.0001	0
S2	17.5707	-0.0266	0.0136	-0.0013	-0.0051	0.0039	-0.0014	0.0002	-1.65E-05	0
S3	13.9756	-0.0693	0.0468	0.0053	-0.0362	0.0329	-0.0152	0.0037	-0.0004	0
S4	0.8385	-0.0479	0.0299	0.0494	-0.1079	0.1034	-0.0542	0.0149	-0.0016	0
S5	0	-0.0461	0.0540	-0.1587	0.2603	-0.2573	0.1493	-0.0469	0.0062	0
S6	-7.5340	-0.0448	0.0274	-0.0781	0.1061	-0.0865	0.0412	-0.0104	0.0011	0
S7	0	-0.0764	0.0778	-0.1673	0.1988	-0.1446	0.0632	-0.0151	0.0015	0
S8	0	-0.0847	0.0920	-0.1359	0.1217	-0.0680	0.0232	-0.0044	0.0004	0
S9	0	-0.1262	0.1233	-0.0966	0.0501	-0.0176	0.0040	-0.0005	3.07E-05	0
S10	-54.7889	-0.1208	0.0816	-0.0462	0.0181	-0.0049	0.0009	-0.0001	4.45E-06	0
S11	-8.7794	-0.0128	-0.0022	0.0010	-0.0010	0.0004	-0.0001	4.45E-06	-1.33E-07	0
S12	-40.2521	0.0295	-0.0189	0.0049	-0.0009	0.0002	-1.76E-05	1.16E-06	-3.12E-08	0

TABLE 6-continued

Ex. 3	K	A	B	C	D	E	F	G	H	J
S13	-3.6141	-0.0550	0.0087	0.0019	-0.0007	0.0001	-6.62E-06	2.36E-07	-3.47E-09	0
S14	-15.7838	-0.0378	0.0096	-0.0013	0.0001	-1.72E-06	-1.76E-07	1.40E-08	-4.05E-10	4.26E-12

An imaging lens system according to a fourth example will be described with reference to FIG. 7.

An imaging lens system **400** includes a first lens **410**, a second lens **420**, a third lens **430**, a fourth lens **440**, a fifth lens **450**, a sixth lens **460**, and a seventh lens **470**.

The first lens **410** has positive refractive power, and the first lens **410** has a convex shape on an object side surface and a concave shape on an image side surface. The second lens **420** has negative refractive power, and the second lens **420** has a convex shape on an object side surface and a concave shape on an image side surface. The third lens **430** has positive refractive power, and the third lens **430** has a convex shape on an object side surface and a concave shape on an image side surface. The fourth lens **440** has negative refractive power, and the fourth lens **440** has a concave shape on an object side surface and a concave shape on an image side surface. The fifth lens **450** has negative refractive power, and the fifth lens **450** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the fifth lens **450** has a shape in which an inflection point is formed on the object side surface and the image side surface. The sixth lens **460** has positive refractive power, and the sixth lens **460** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the sixth lens **460** has a shape in which an inflection point is formed on the object side surface and the image side surface. The seventh lens **470** has negative refractive power, and the seventh lens **470** has a concave shape on an object side surface and a concave shape on an image side surface. Further, the seventh lens **470** has a shape in which an inflection point is formed on the object side surface and the image side surface.

The imaging lens system **400** further includes a filter **480** and an image sensor **490**. The filter **480** is disposed between the seventh lens **470** and the image sensor **490**. For refer-

ence, although not shown in the drawings, a stop may be disposed between the second lens **420** and the third lens **430**.

The imaging lens system **400** illustrates aberration characteristics as shown in FIG. 8. Tables 7 and 8 illustrate lens characteristics and aspherical surface values of the imaging lens system **400**.

TABLE 7

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number
S1	First lens	2.723	1.100	1.544	56.1
S2		12.203	0.181		
S3		8.384	0.230		
S4	Third lens	4.498	0.529	1.544	56.1
S5		83.525	0.424		
S6		-31.911	0.232		
S7	Fourth lens	-40.873	0.408	1.661	20.4
S8		497.247	0.678		
S9		6.912	0.373		
S10	Fifth lens	5.807	0.443	1.568	37.4
S11		2.544	0.541		
S12		6.584	1.354		
S13	Seventh lens	-4.071	0.420	1.544	56.1
S14		7.701	0.377		
S15		Infinity	0.210		
S16	Filter	Infinity	0.345	1.514	64.2
Imaging plane		Imaging plane	Infinity		

TABLE 8

Ex. 4	K	A	B	C	D	E	F	G	H	J
S1	-1.0394	0.0040	0.0069	-0.0084	0.0069	-0.0036	0.0012	-0.0003	3.23E-05	-1.74E-06
S2	21.6009	-0.0171	0.0046	0.0082	-0.0127	0.0089	-0.0037	0.0009	-0.0001	7.09E-06
S3	15.9987	-0.0525	0.0325	0.0037	-0.0232	0.0211	-0.0103	0.0030	-0.0005	3.06E-05
S4	1.0581	-0.0412	0.0340	-0.0111	0.0039	-0.0057	0.0059	-0.0029	0.0007	-0.0001
S5	0	-0.0210	-0.0180	0.0475	-0.0705	0.0651	-0.0374	0.0129	-0.0025	0.0002
S6	-76.4723	-0.0373	0.0235	-0.0503	0.0666	-0.0527	0.0260	-0.0079	0.0013	-0.0001
S7	0	-0.0410	0.0064	-0.0081	0.0068	-0.0022	-0.0003	0.0004	-0.0001	1.26E-05
S8	0	-0.0354	0.0130	-0.0145	0.0106	-0.0045	0.0011	-0.0001	-7.15E-06	1.59E-06
S9	0	-0.0625	0.0399	-0.0218	0.0081	-0.0022	0.0004	-0.0001	0.0000	-1.37E-07
S10	-99.0000	-0.0603	0.0241	-0.0076	0.0016	-0.0002	2.98E-05	-3.23E-06	2.10E-07	-5.68E-09
S11	-7.2394	0.0102	-0.0102	0.0021	-0.0004	0.0001	-5.72E-06	3.13E-07	-9.05E-09	1.08E-10
S12	-27.2182	0.0362	-0.0182	0.0039	-0.0006	0.0001	-4.38E-06	2.05E-07	-5.44E-09	6.16E-11
S13	-4.2405	-0.0338	0.0065	-0.0004	1.56E-06	1.38E-06	-8.01E-08	1.82E-09	-1.07E-11	-1.27E-13
S14	-54.8281	-0.0218	0.0032	-0.0003	1.25E-05	-3.05E-07	1.15E-08	-8.25E-10	2.96E-11	-3.74E-13

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An imaging lens system according to a fifth example will be described with reference to FIG. 9.

An imaging lens system **500** includes a first lens **510**, a second lens **520**, a third lens **530**, a fourth lens **540**, a fifth lens **550**, a sixth lens **560**, and a seventh lens **570**.

The first lens **510** has positive refractive power, and the first lens **510** has a convex shape on an object side surface and a concave shape on an image side surface. The second lens **520** has negative refractive power, and the second lens **520** has a convex shape on an object side surface and a concave shape on an image side surface. The third lens **530** has positive refractive power, and the third lens **530** has a convex shape on an object side surface and a convex shape on an image side surface. The fourth lens **540** has negative refractive power, and the fourth lens **540** has a concave shape on an object side surface and a concave shape on an image side surface. The fifth lens **550** has negative refractive power, and the fifth lens **550** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the fifth lens **550** has a shape in which an inflection

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TABLE 9

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number	
5	S1	First lens	2.7185076	1.092	1.544	56.1
	S2		12.76	0.175		
	S3	Second lens	8.66	0.230	1.671	19.3
10	S4		4.58	0.542		
	S5	Third lens	58.30	0.437	1.544	56.1
	S6		-37.343513	0.233		
15	S7	Fourth lens	-39.38	0.455	1.639	23.5
	S8		197.62	0.629		
	S9	Fifth lens	6.51	0.370	1.568	37.4
20	S10		4.86	0.417		
	S11	Sixth lens	2.50	0.544	1.544	56.1
	S12		7.54	1.368		
20	S13	Seventh lens	-4.08	0.420	1.544	56.1
	S14		7.41	0.377		
	S15	Filter	Infinity	0.210	1.514	64.2
	S16		Infinity	0.347		
	Imaging plane	Imaging plane	Infinity	-0.015		

TABLE 10

Ex. 5	K	A	B	C	D	E	F	G	H	J
S1	-1.0355	0.0008	0.0147	-0.0193	0.0161	-0.0085	0.0029	-0.0006	0.0001	-3.66E-06
S2	23.2430	-0.0191	0.0100	0.0009	-0.0062	0.0051	-0.0023	0.0006	-0.0001	4.77E-06
S3	16.0208	-0.0571	0.0446	-0.0141	-0.0065	0.0106	-0.0060	0.0018	-0.0003	2.02E-05
S4	0.9155	-0.0438	0.0385	-0.0132	-0.0020	0.0049	-0.0023	0.0005	-1.72E-05	-4.19E-06
S5	0	-0.0212	-0.0159	0.0393	-0.0520	0.0426	-0.0217	0.0067	-0.0011	0.0001
S6	-43.9004	-0.0442	0.0384	-0.0699	0.0811	-0.0581	0.0263	-0.0074	0.0012	-0.0001
S7	0	-0.0412	0.0034	0.0035	-0.0134	0.0170	-0.0110	0.0039	-0.0007	0.0001
S8	0	-0.0371	0.0171	-0.0170	0.0098	-0.0028	0.0001	0.0002	-4.53E-05	3.78E-06
S9	0	-0.0761	0.0558	-0.0344	0.0147	-0.0045	0.0009	-0.0001	9.80E-06	-3.30E-07
S10	-75.9915	-0.0668	0.0292	-0.0101	0.0023	-0.0004	0.0001	-4.85E-06	2.85E-07	-7.22E-09
S11	-8.2269	0.0131	-0.0136	0.0036	-0.0008	0.0001	-1.04E-05	5.57E-07	-1.59E-08	1.90E-10
S12	-38.3867	0.0373	-0.0206	0.0051	-0.0008	0.0001	-7.88E-06	3.83E-07	-1.03E-08	1.18E-10
S13	-3.1329	-0.0341	0.0063	-0.0004	-7.92E-07	1.14E-06	-4.71E-08	1.78E-10	2.87E-11	-5.13E-13
S14	-42.1372	-0.0248	0.0041	-0.0004	2.77E-05	-1.22E-06	3.46E-08	-6.33E-10	9.25E-12	-1.06E-13

point is formed on the object side surface and the image side surface. The sixth lens **560** has positive refractive power, and the sixth lens **560** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the sixth lens **560** has a shape in which an inflection point is formed on the object side surface and the image side surface. The seventh lens **570** has negative refractive power, and the seventh lens **570** has a concave shape on an object side surface and a concave shape on an image side surface. Further, the seventh lens **570** has a shape in which an inflection point is formed on the object side surface and the image side surface.

The imaging lens system **500** further includes a filter **580** and an image sensor **590**. The filter **580** is disposed between the seventh lens **570** and the image sensor **590**. For reference, although not shown in the drawings, a stop may be disposed between the second lens **520** and the third lens **530**.

The imaging lens system **500** illustrates an aberration characteristic as shown in FIG. 10. Tables 9 and 10 illustrate lens characteristics and aspherical surface values of the imaging lens system **500**.

An imaging lens system according to a sixth example will be described with reference to FIG. 11.

An imaging lens system **600** includes a first lens **610**, a second lens **620**, a third lens **630**, a fourth lens **640**, a fifth lens **650**, a sixth lens **660**, and a seventh lens **670**.

The first lens **610** has positive refractive power, and the first lens **610** has a convex shape on an object side surface and a concave shape on an image side surface. The second lens **620** has negative refractive power, and the second lens **620** has a convex shape on an object side surface and a concave shape on an image side surface. The third lens **630** has positive refractive power, and the third lens **630** has a convex shape on an object side surface and a convex shape on an image side surface. The fourth lens **640** has negative refractive power, and the fourth lens **640** has a concave shape on an object side surface and a convex shape on an image side surface. The fifth lens **650** has positive refractive power, and the fifth lens **650** has a convex shape on an object side surface and a concave shape on an image side surface. Further, the fifth lens **650** has a shape in which an inflection point is formed on the object side surface and the image side surface. The sixth lens **660** has positive refractive power, and the sixth lens **660** has a convex shape on an object side

surface and a concave shape on an image side surface. Further, the sixth lens **660** has a shape in which an inflection point is formed on the object side surface and the image side surface. The seventh lens **670** has negative refractive power, and the seventh lens **670** has a concave shape on an object side surface and a concave shape on an image side surface. Further, the seventh lens **670** has a shape in which an inflection point is formed on the object side surface and the image side surface.

The imaging lens system **600** further includes a filter **680** and an image sensor **690**. The filter **680** is disposed between the seventh lens **670** and the image sensor **690**. For reference, although not shown in the drawings, a stop may be disposed between the second lens **620** and the third lens **630**.

The imaging lens system **600** illustrates aberration characteristics as shown in FIG. **12**. Tables 11 and 12 illustrate lens characteristics and aspherical surface values of the imaging lens system **600**.

TABLE 11

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number
S1	First lens	2.67	1.031	1.544	56.1
S2		9.43	0.200		

TABLE 11-continued

Surface number	Reference	Radius of curvature	Thickness/distance	Refractive index	Abbe number
5 S3	Second lens	6.95	0.230	1.680	18.4
S4		4.29	0.622		
S5	Third lens	59.38986	0.437	1.544	56.1
10 S6		-50.84	0.264		
S7	Fourth lens	-23.50	0.326	1.680	18.4
S8		-61.66	0.571		
S9	Fifth lens	6.42	0.359	1.568	37.4
15 S10		6.69	0.493		
S11	Sixth lens	3.06	0.552	1.544	56.1
S12		9.80	1.430		
S13	Seventh lens	-3.48	0.403	1.544	56.1
20 S14		10.26	0.181		
S15	Filter	Infinity	0.210	1.514	64.2
S16		Infinity	0.509		
Imaging plane	Imaging plane	Infinity	0.012		

TABLE 12

Ex. 6	K	A	B	C	D	E	F	G	H	J
S1	-1.0111	0.0031	0.0115	-0.0176	0.0170	-0.0102	0.0038	-0.0009	0.0001	-6.32E-06
S2	14.6338	-0.0181	0.0087	-0.0053	0.0039	-0.0024	0.0010	-0.0002	3.43E-05	-2.02E-06
S3	13.0489	-0.0453	0.0301	-0.0165	0.0139	-0.0111	0.0059	-0.0019	0.0003	-2.53E-05
S4	2.0700	-0.0302	0.0190	0.0095	-0.0239	0.0234	-0.0137	0.0048	-0.0010	0.0001
S5	0	-0.0158	-0.0302	0.0716	-0.1026	0.0914	-0.0512	0.0176	-0.0034	0.0003
S6	94.2471	-0.0214	-0.0101	0.0093	-0.0072	0.0054	-0.0031	0.0011	-0.0002	1.63E-05
S7	0	-0.0167	-0.0437	0.0720	-0.0791	0.0568	-0.0259	0.0072	-0.0011	0.0001
S8	0	-0.0186	-0.0236	0.0334	-0.0305	0.0182	-0.0069	0.0016	-0.0002	1.17E-05
S9	0	-0.0396	0.0203	-0.0108	0.0041	-0.0011	0.0002	-2.52E-05	1.79E-06	-5.46E-08
S10	-55.6301	-0.0479	0.0210	-0.0082	0.0024	-0.0005	0.0001	-7.14E-06	3.78E-07	-8.43E-09
S11	-7.3401	0.0023	-0.0046	0.0004	1.39E-06	-2.88E-06	3.40E-07	-2.51E-08	1.01E-09	-1.63E-11
S12	-70.2827	0.0258	-0.0110	0.0019	-0.0002	1.02E-05	-2.06E-07	-1.08E-08	7.73E-10	-1.41E-11
S13	-5.4006	-0.0324	0.0065	-0.0006	0.0001	-6.11E-06	4.47E-07	-1.95E-08	4.53E-10	-4.35E-12
S14	-81.9062	-0.0174	0.0025	-0.0002	1.41E-05	-1.05E-06	7.83E-08	-3.60E-09	8.34E-11	-7.60E-13

Table 13 illustrates characteristic values of the imaging lens system according to the first example to the sixth example.

TABLE 13

Reference	First Example	Second Example	Third Example	Fourth Example	Fifth Example	Sixth Example
f	5.4400	5.4400	5.5000	6.7900	6.7900	6.7700
f1	5.2118	5.2360	5.3400	6.1671	6.0930	6.4870
f2	-13.136	-13.269	-13.240	-14.973	-14.655	-16.875
f3	24.259	23.771	32.805	42.349	41.763	50.247
f4	-18.415	-18.540	-22.408	-56.614	-50.900	-55.460
f5	-264.430	-276.040	469.354	-72.648	-36.671	189.158
f6	3.9103	3.9450	4.0730	7.2520	6.5810	7.9250
f7	-3.0703	-3.0755	-3.1397	-4.8170	-4.7618	-4.7070
f12	7.4920	7.5199	7.7610	9.1670	4.8690	9.2468
TTL	6.6945	6.7000	6.7000	7.8300	7.8300	7.8298
BFL	1.0349	1.0360	0.9966	0.9175	0.9188	0.9120
FOV	80.0	80.0	80.0	82.0	82.0	82.0
IH	4.6500	4.6500	4.6500	6.0070	6.0070	6.0070
SD5	2.2950	2.2961	2.2430	3.0737	3.0639	2.9890
SD6	3.3180	3.3176	3.1810	4.2745	4.1594	4.2990
SD7	4.1960	4.2461	4.1426	5.0657	4.9940	5.1200

The imaging lens system according to the examples may generally have optical characteristics as follows. For example, a total length TTL of the imaging lens system is in a range of 5.7 to 8.8 mm, a total focal length is in a range of 4.8 to 7.4 mm, a focal length of the first lens is in a range of 5.0 to 6.7 mm, a focal length of the second length is in a range of -20 to -10 mm, a focal length of the third lens is in a range of 20 to 60 mm, a focal length of the fourth lens is in a range less than -15 mm, a focal length of the fifth lens is in a range of greater than 100 mm or less than -30 mm, a focal length of the sixth lens is in a range of 3.0 to 9.0 mm, and a focal length of the seventh lens is in a range of -5.6 to -2.2 mm. Further, an angle of view FOV of the imaging lens system is in a range of 78 to 88 degrees.

Table 14 illustrates conditional expression values of the imaging lens system according to the first example to the sixth example.

TABLE 14

Conditional expression	First Example	Second Example	Third Example	Fourth Example	Fifth Example	Sixth Example
f1/f	0.9581	0.9625	0.9709	0.9083	0.8973	0.9582
V1-V2	36.85	36.85	36.85	36.84	36.84	37.67
V1-V3	0	0	0	-0.01	-0.01	-0.01
V1-V4	35.75	35.75	35.75	35.74	32.57	37.67
V1-V5	18.74	18.74	18.74	18.73	18.73	18.73
f2/f	-2.4147	-2.4392	-2.4073	-2.2051	-2.1583	-2.4926
f3/f	4.4594	4.3697	5.9645	6.2369	6.1507	7.4219
f4/f	-3.3851	-3.4081	-4.0742	-8.3378	-7.4963	-8.1920
f5/f	-48.608	-50.743	85.337	-10.699	-5.401	27.941
f6/f	0.7188	0.7252	0.7405	1.0680	0.9692	1.1706
f7/f	-0.5644	-0.5653	-0.5709	-0.7094	-0.7013	-0.6953
TTL/f	1.2306	1.2316	1.2182	1.1532	1.1532	1.1565
f1/f2	-0.3968	-0.3946	-0.4033	-0.4119	-0.4158	-0.3844
f2/f3	-0.5415	-0.5582	-0.4036	-0.3536	-0.3509	-0.3358
BFL/f	0.1902	0.1904	0.1812	0.1351	0.1353	0.1347
D12/f	0.0302	0.0304	0.0341	0.0267	0.0257	0.0296
SD5/IH	0.4935	0.4938	0.4824	0.5117	0.5101	0.4976
SD6/IH	0.7135	0.7135	0.6841	0.7116	0.6924	0.7157
SD7/IH	0.9024	0.9131	0.8909	0.8433	0.8314	0.8523

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As set forth above, according to the examples, performance of a compact camera may be improved.

While this disclosure includes specific examples, it will be apparent to one of ordinary skill in the art that various changes in form and details may be made in these examples without departing from the spirit and scope of the claims and their equivalents. The examples described herein are to be considered in a descriptive sense only, and not for purposes of limitation. Descriptions of features or aspects in each example are to be considered as being applicable to similar features or aspects in other examples. Suitable results may be achieved if the described techniques are performed to have a different order, and/or if components in a described system, architecture, device, or circuit are combined in a different manner, and/or replaced or supplemented by other components or their equivalents. Therefore, the scope of the disclosure is defined not by the detailed description, but by the claims and their equivalents, and all variations within the scope of the claims and their equivalents are to be construed as being included in the disclosure.

What is claimed is:

1. An imaging lens system comprising:
 - a first lens comprising a convex object-side surface;
 - a second lens comprising a convex object-side surface;
 - a third lens comprising positive refractive power and a convex image-side surface in a paraxial region;
 - the third lens has a convex object-side surface;
 - a fourth lens comprising a concave image-side surface;
 - a fifth lens comprising negative refractive power and a convex object-side surface;
 - a sixth lens comprising a convex object-side surface and a concave image-side surface in a paraxial region; and
 - a seventh lens comprising a concave object-side surface, wherein the first to seventh lenses are sequentially disposed from an object side of the imaging lens system, and wherein an absolute value of a radius of curvature of an image-side surface of the first lens is greater than an

absolute value of a radius of curvature of the object-side surface of the fifth lens.

2. The imaging lens system of claim 1, wherein the first lens has a concave image-side surface.
3. The imaging lens system of claim 1, wherein the second lens has a concave image-side surface.
4. The imaging lens system of claim 1, wherein the fifth lens has a concave image-side surface.
5. The imaging lens system of claim 1, wherein the seventh lens has a concave image-side surface.
6. The imaging lens system of claim 1, wherein $TTL/f < 1.4$, where TTL is a distance from the object-side surface of the first lens to an imaging plane.
7. The imaging lens system of claim 1, wherein $1.5 < f3/f$, where f is a focal length of the imaging lens system and f3 is a focal length of the third lens.
8. The imaging lens system of claim 1, wherein $1.5 < Nd5 < 1.6$, where Nd5 is a refractive index of the fifth lens.
9. The imaging lens system of claim 1, wherein an F-number is 2.0 or less.

10. The imaging lens system of claim 1, wherein $25 < V1 - V4 < 45$, where $V4$ is an Abbe number of the fourth lens.

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