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**Kitamura**

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(54) **AIRFLOW VELOCITY MEASURING APPARATUS AND AIRFLOW RATE MEASURING APPARATUS**

(71) Applicant: **Murata Manufacturing Co., Ltd.**, Nagaokakyo (JP)

(72) Inventor: **Akihiro Kitamura**, Nagaokakyo (JP)

(73) Assignee: **MURATA MANUFACTURING CO., LTD.**, Nagaokakyo (JP)

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**G01F 1/69** (2006.01)  
(Continued)

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(58) **Field of Classification Search**  
CPC . G01P 5/12; G01F 1/69; G01F 15/043; G01K 7/22; G01K 7/16  
See application file for complete search history.

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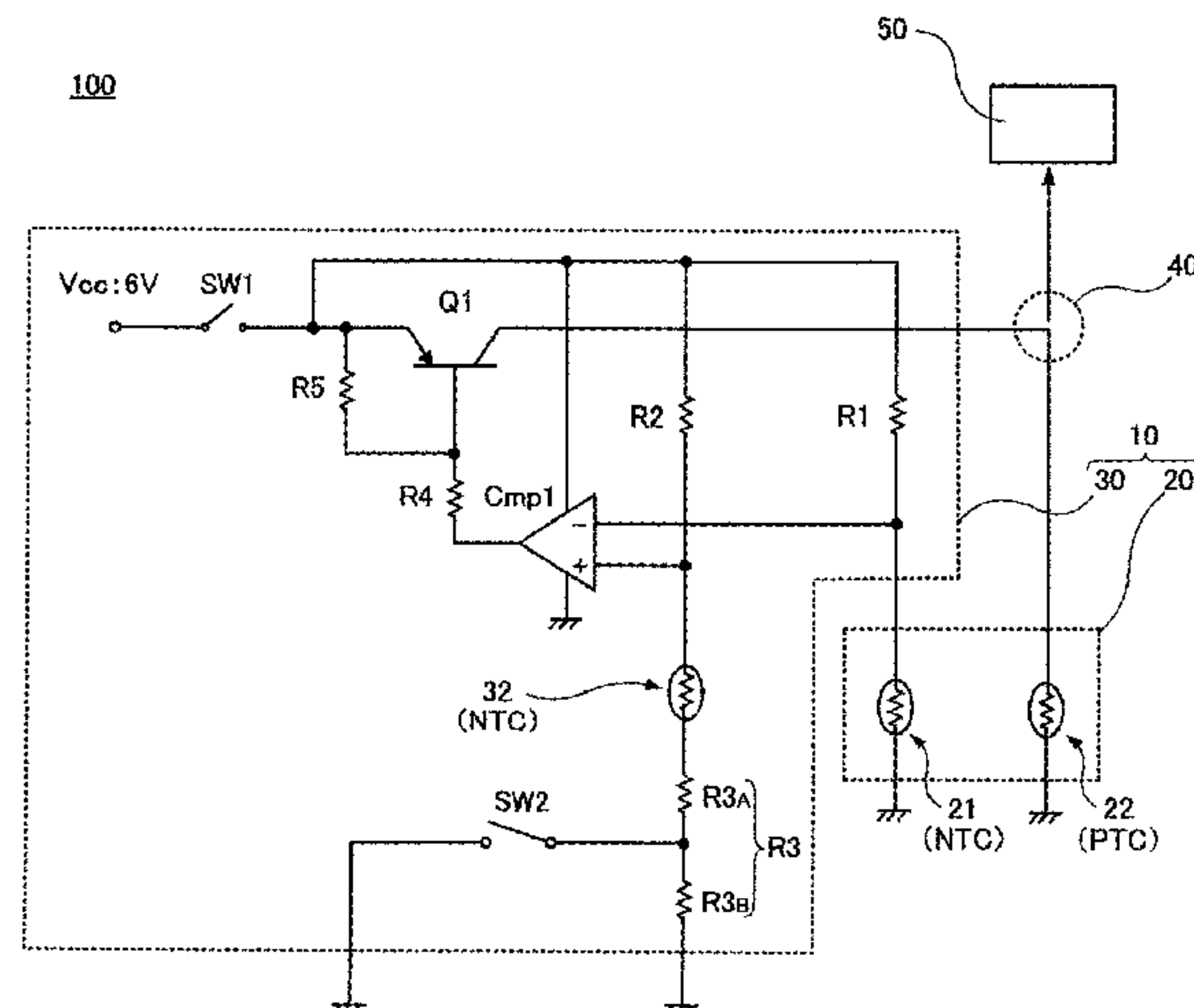
*Primary Examiner* — Ryan D Walsh

(74) *Attorney, Agent, or Firm* — Arent Fox LLP

(57) **ABSTRACT**

An airflow velocity measuring apparatus that includes a fixed-temperature heat generating device. The fixed-temperature heat generating device includes a power supply, a positive-temperature-coefficient thermistor element, a switching element, a comparator element, a first negative-temperature-coefficient thermistor element, a second negative-temperature-coefficient thermistor element, and plural resistor elements. The positive-temperature-coefficient thermistor element is disposed at a measuring point at which the velocity of airflow is measured. The switching element is repeatedly turned ON and OFF so as to cause the positive-temperature-coefficient thermistor element to generate heat at a preset temperature, thereby applying a pulse voltage from the power supply to the positive-temperature-coefficient thermistor element. The airflow velocity measuring apparatus measures the velocity of airflow at the measuring point based on the waveform of this pulse voltage. Adding of a second switch makes it possible to correct measurement errors caused by a rise or a fall in the temperature of subject airflow.

**13 Claims, 9 Drawing Sheets**



- (51) **Int. Cl.**  
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**G01K 7/22** (2006.01)  
**G01K 7/16** (2006.01)

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FIG. 1

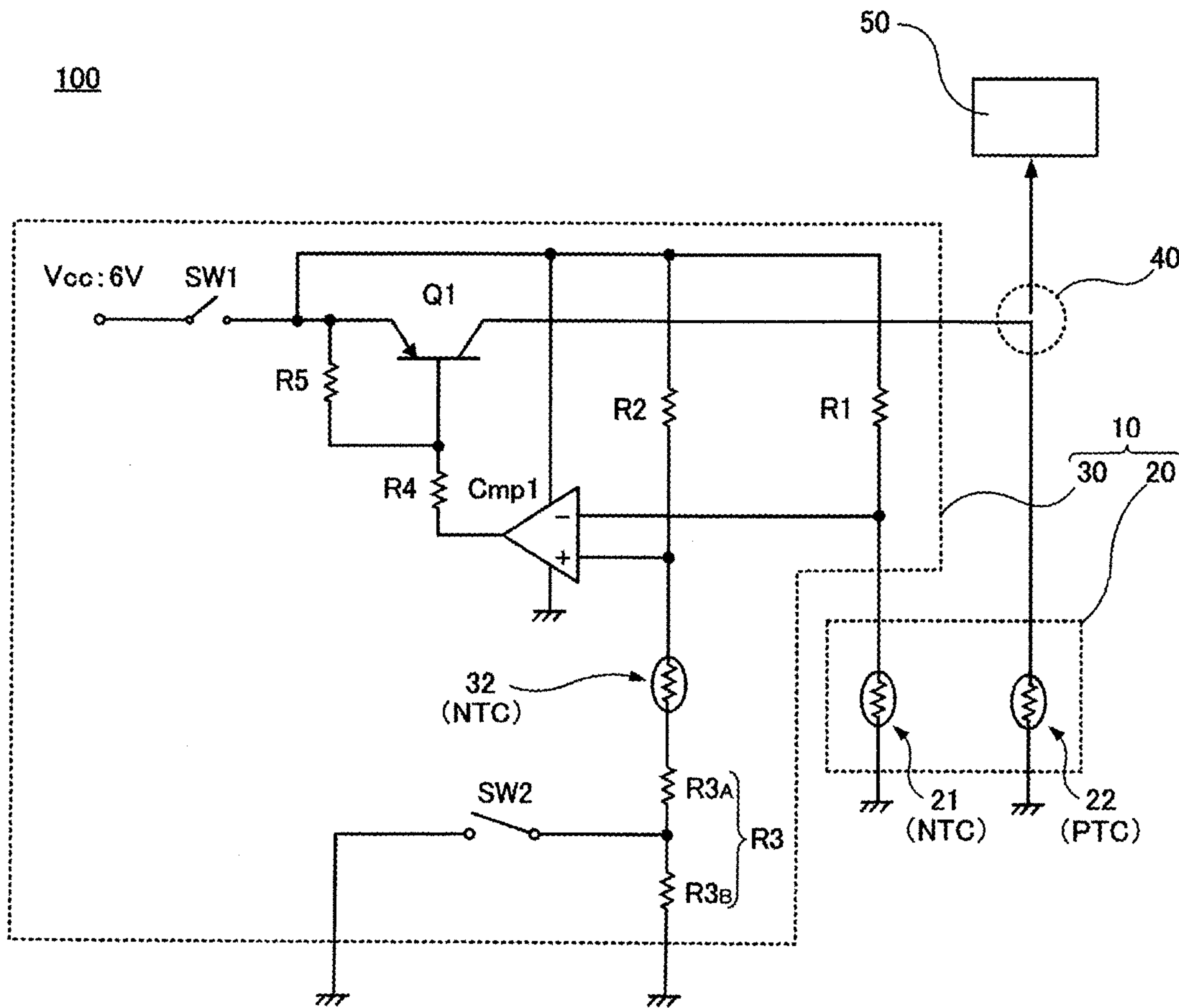


FIG. 2

AIRFLOW VELOCITY OF 5 m/SECOND

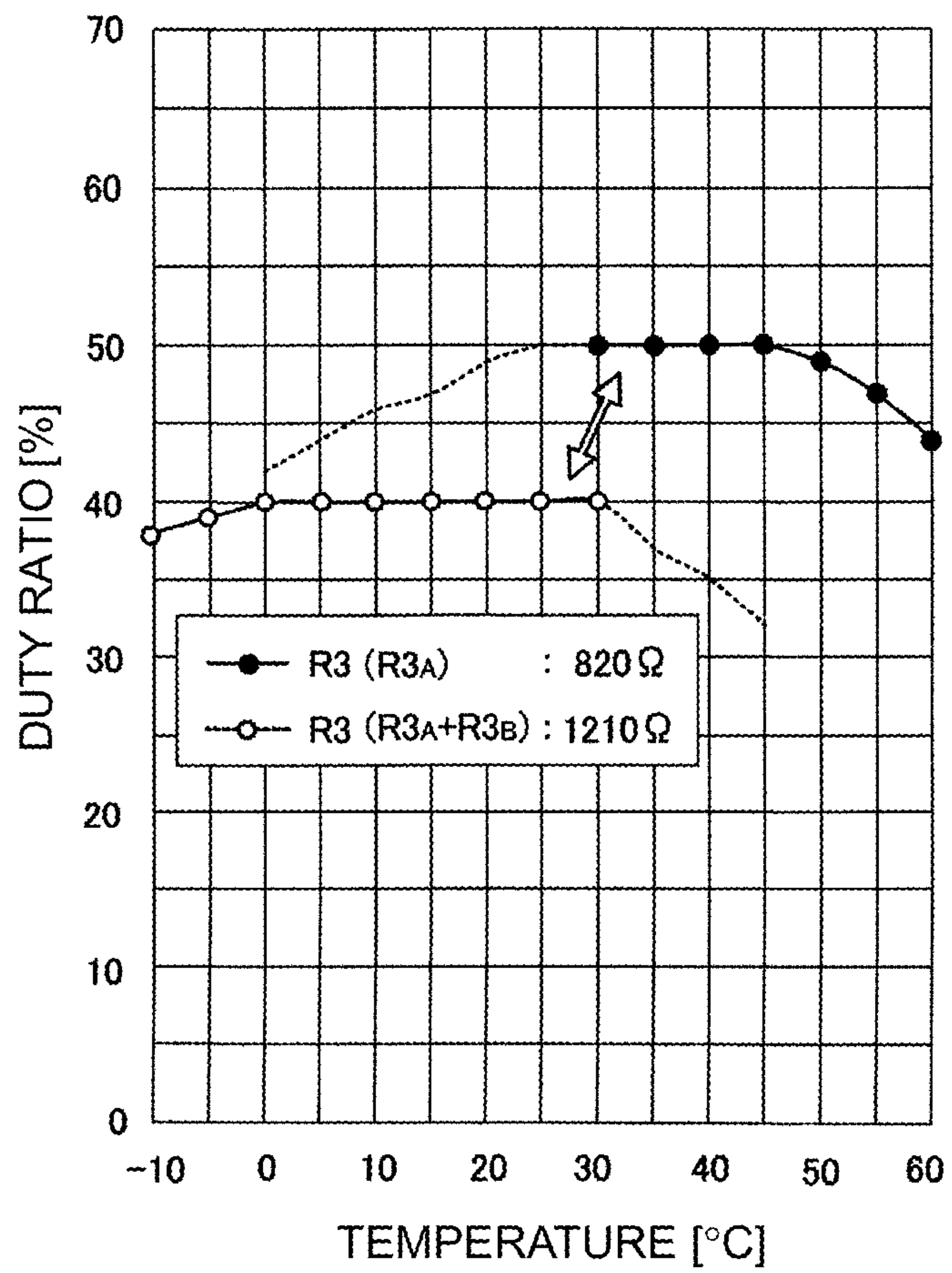


FIG. 3

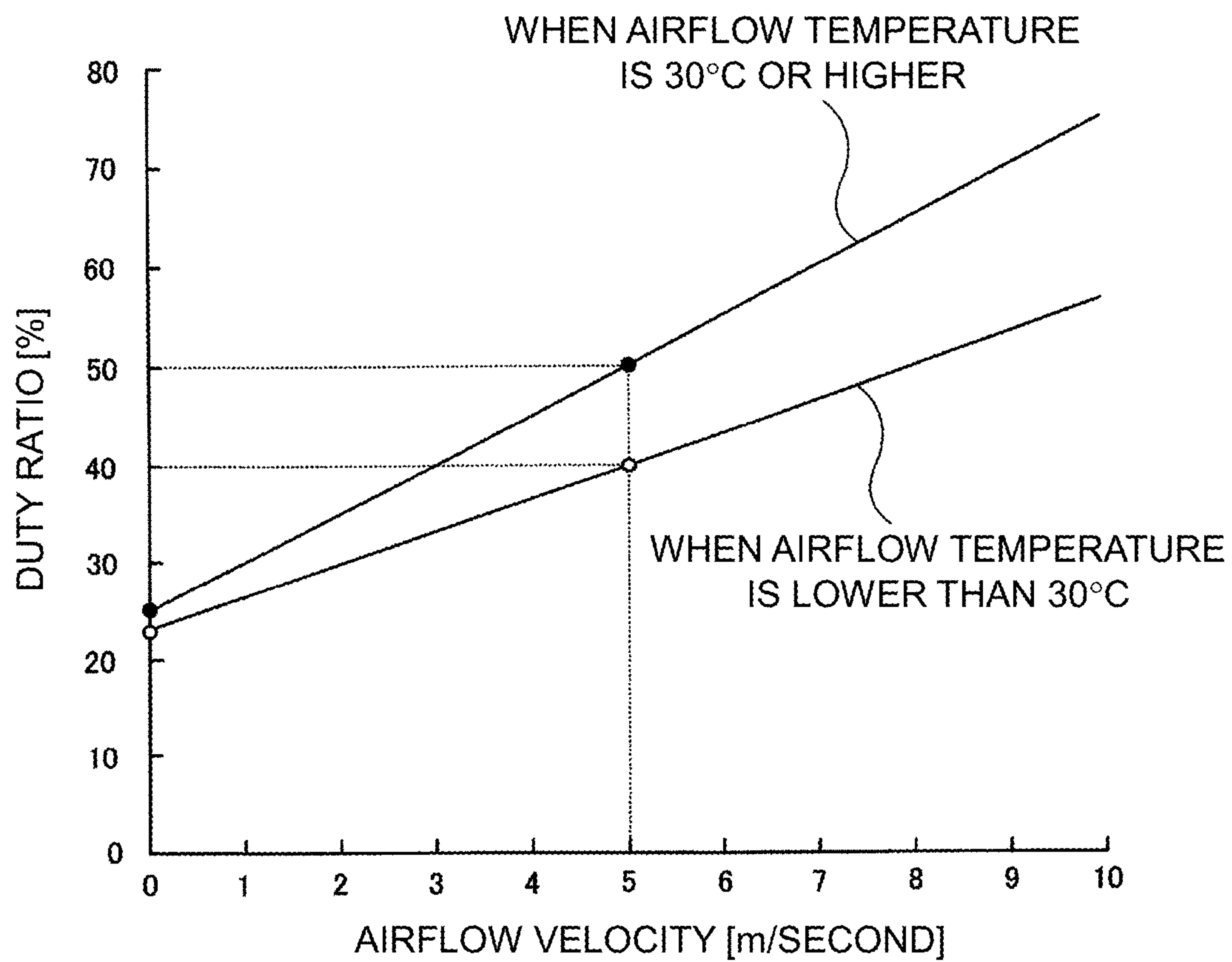




FIG. 4

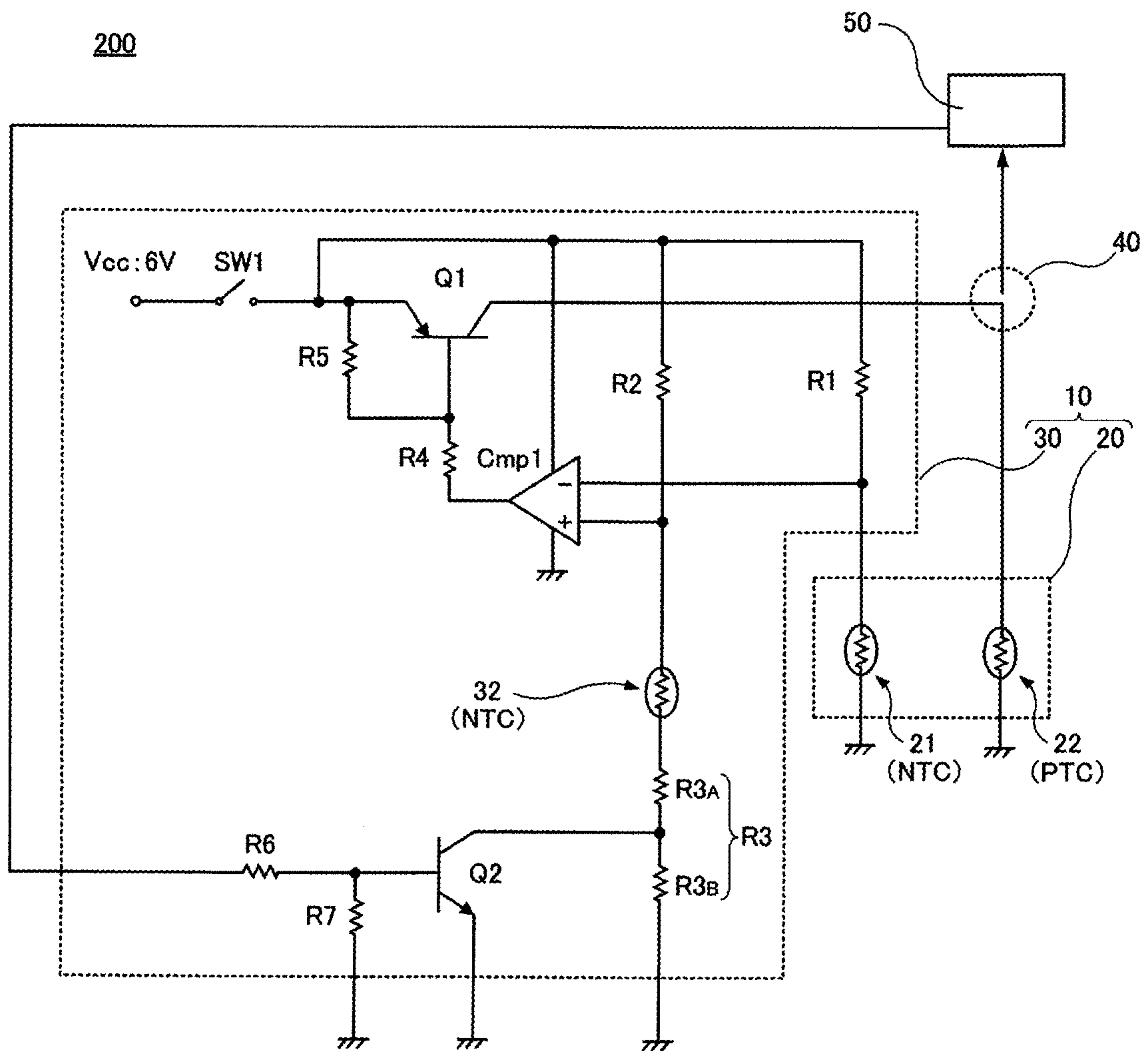


FIG. 5

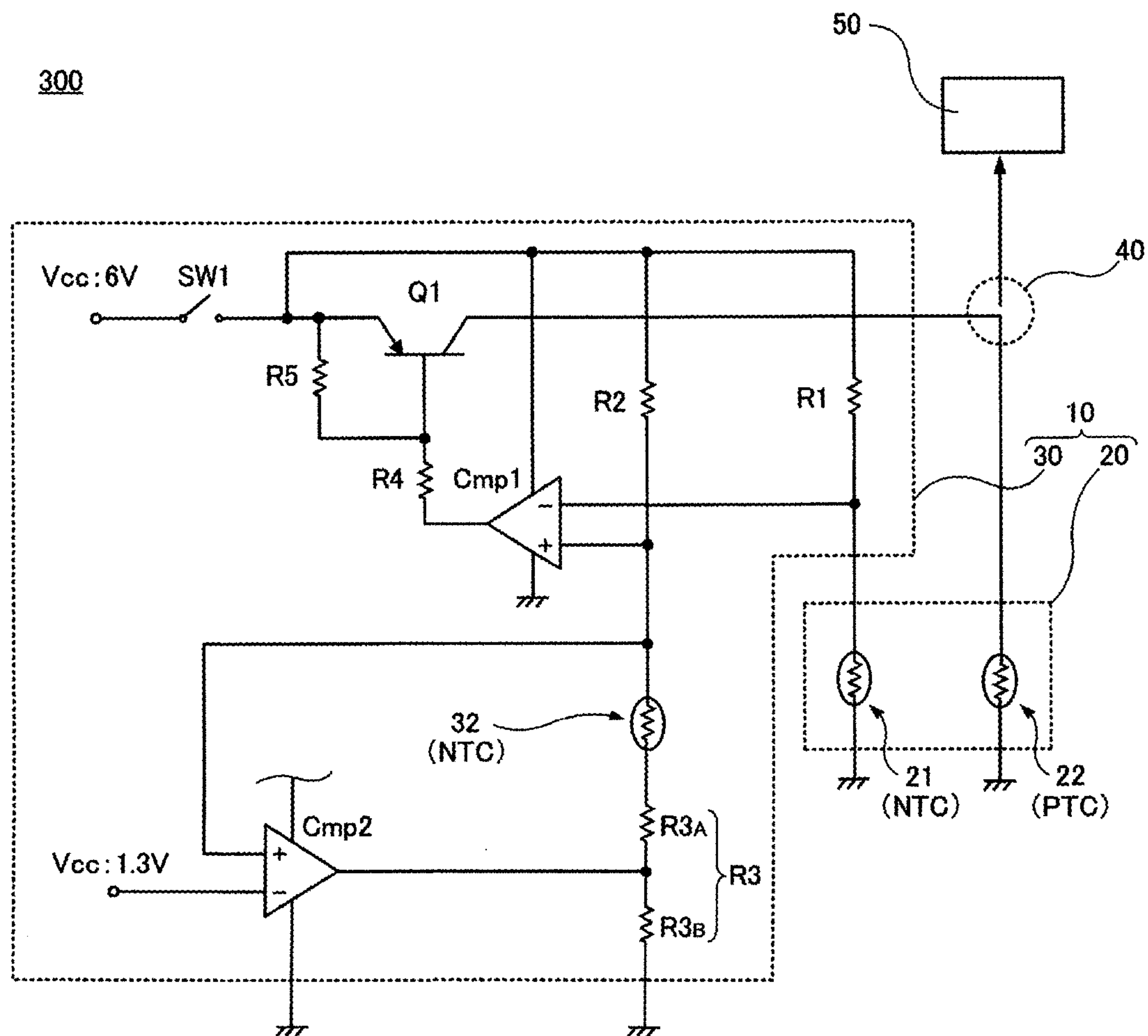


FIG. 6 – PRIOR ART

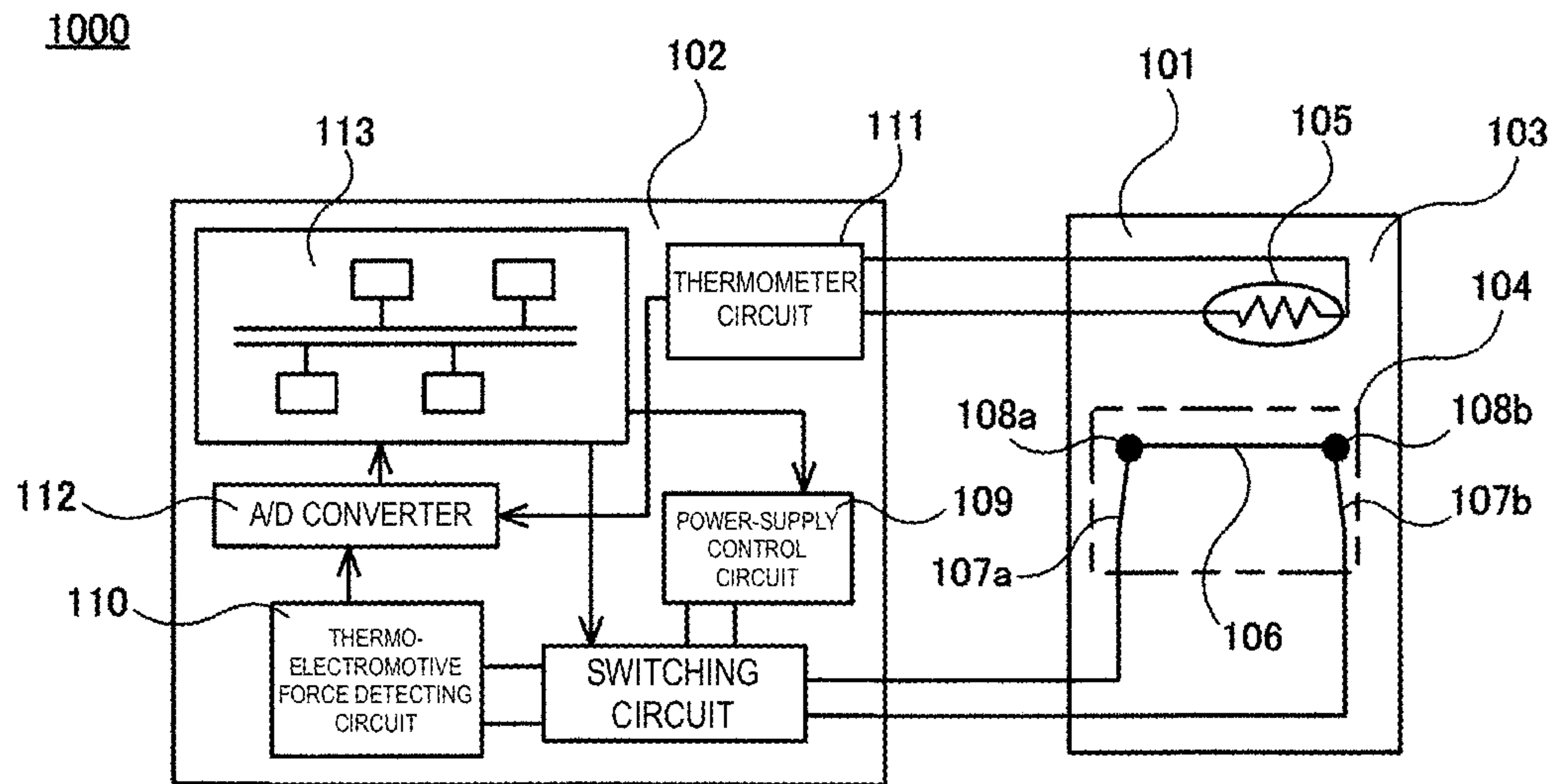


FIG. 7

AIRFLOW VELOCITY MEASURING APPARATUS  
USED AS REFERENCE: 1100A

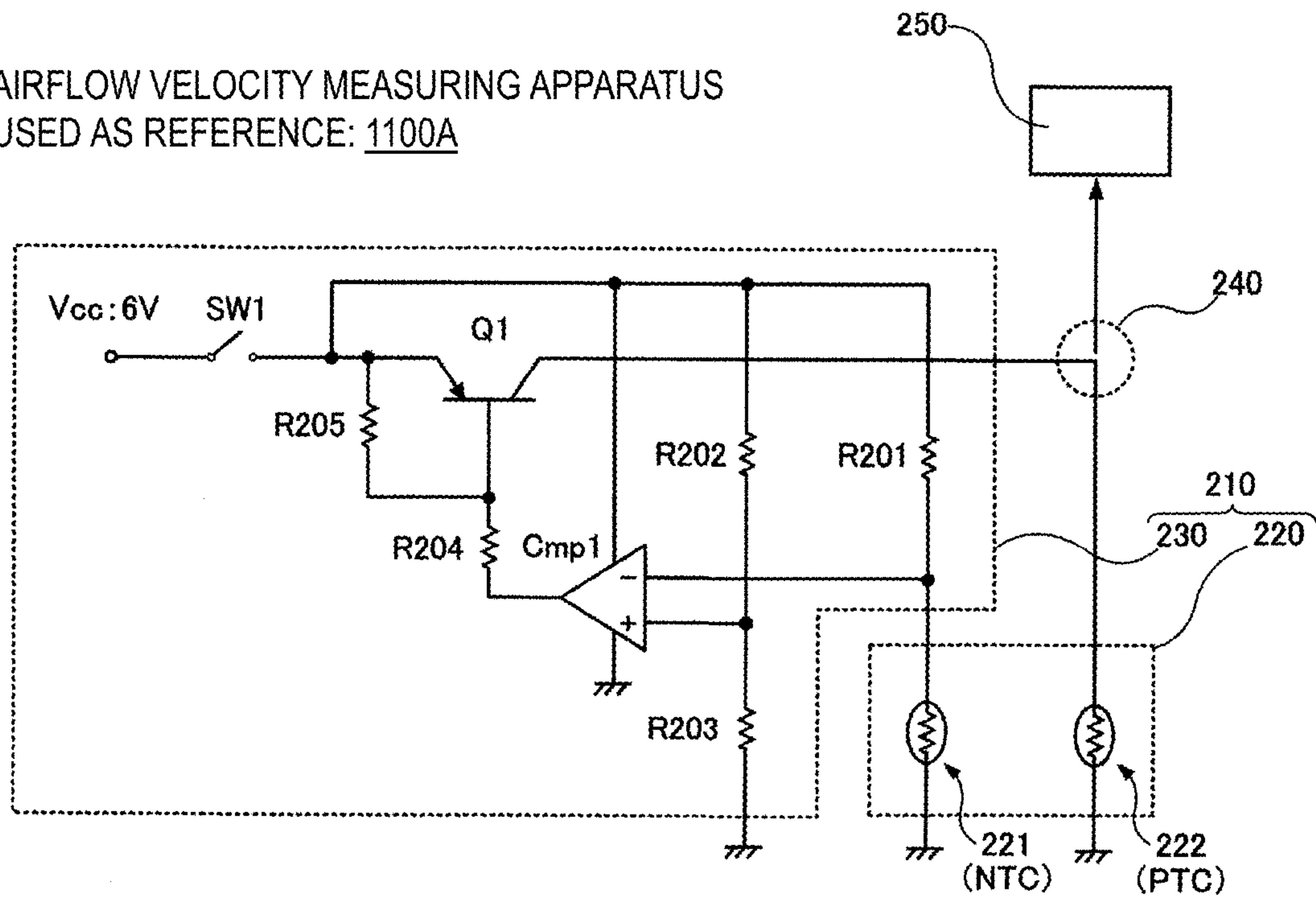




FIG. 8(A)

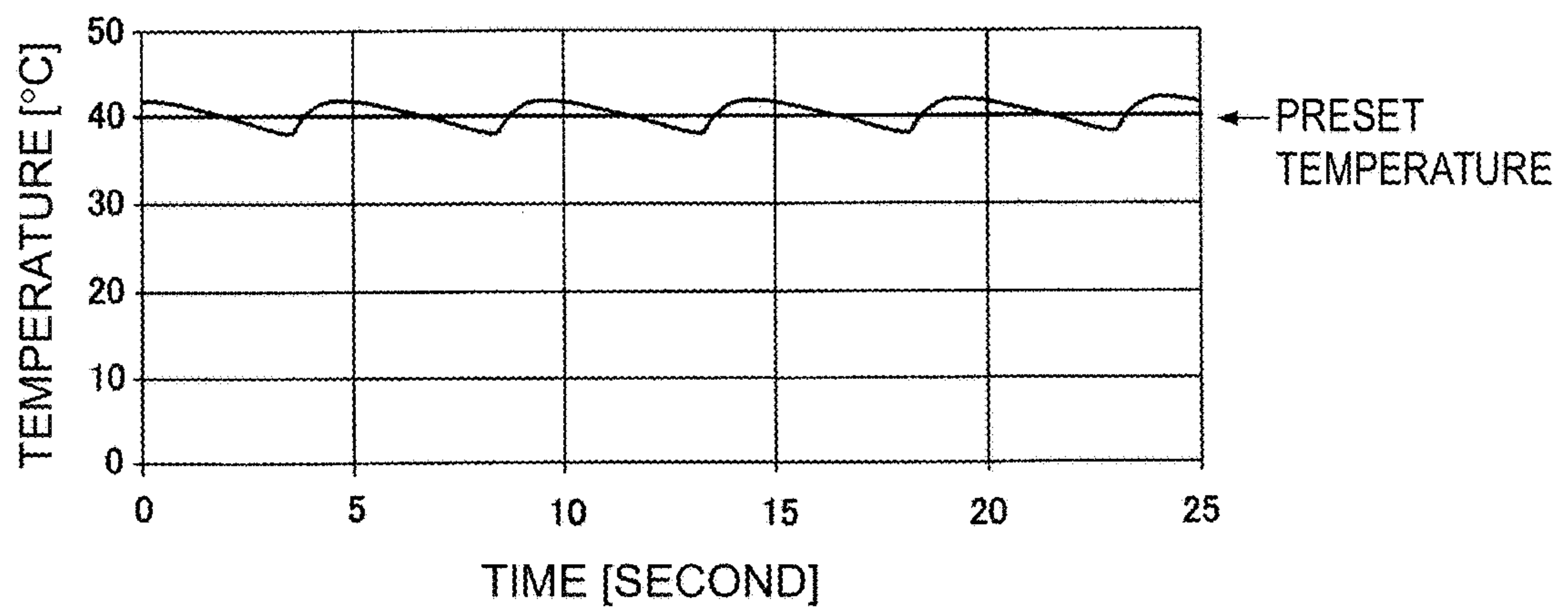


FIG. 8(B)

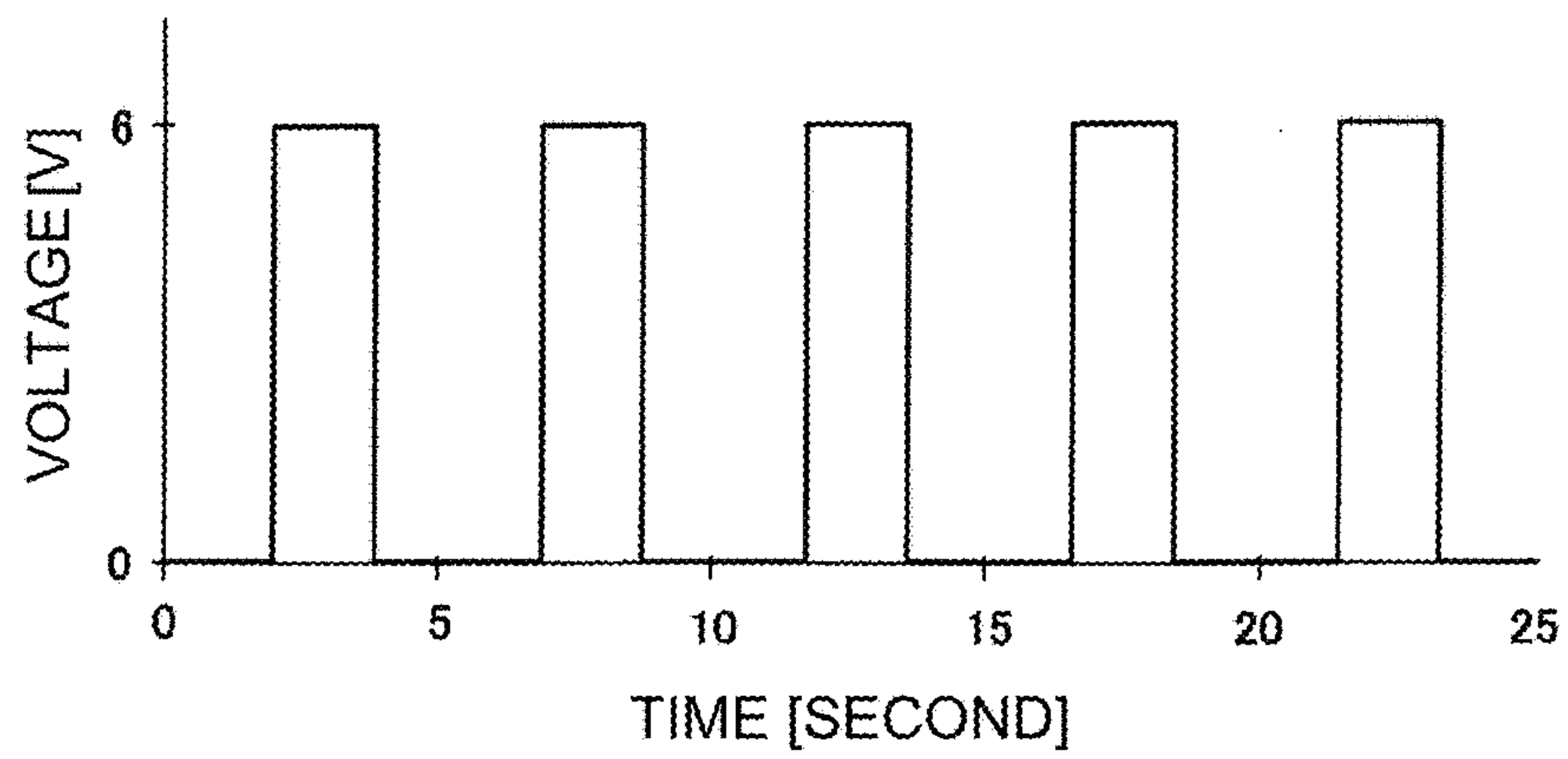


FIG. 9

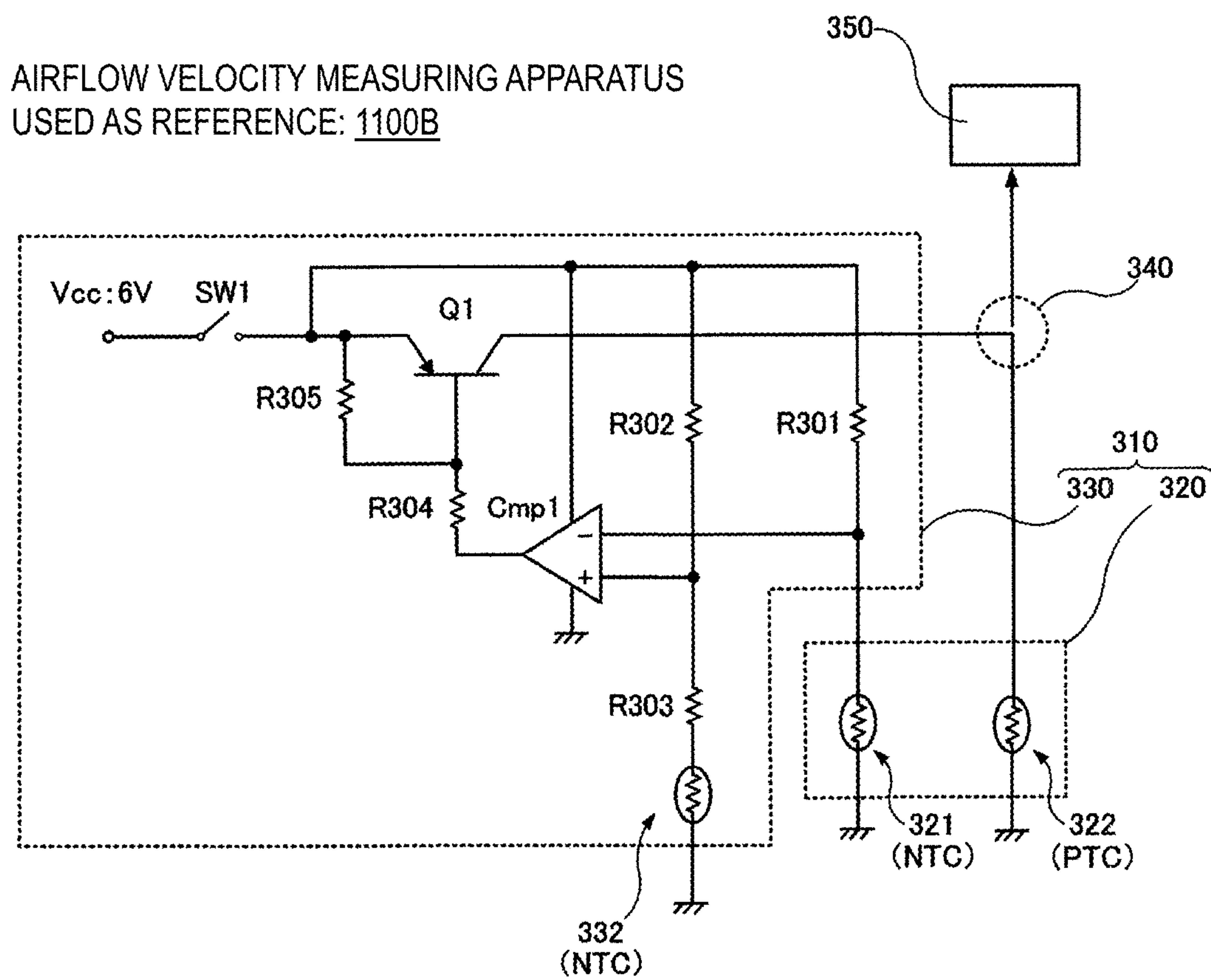
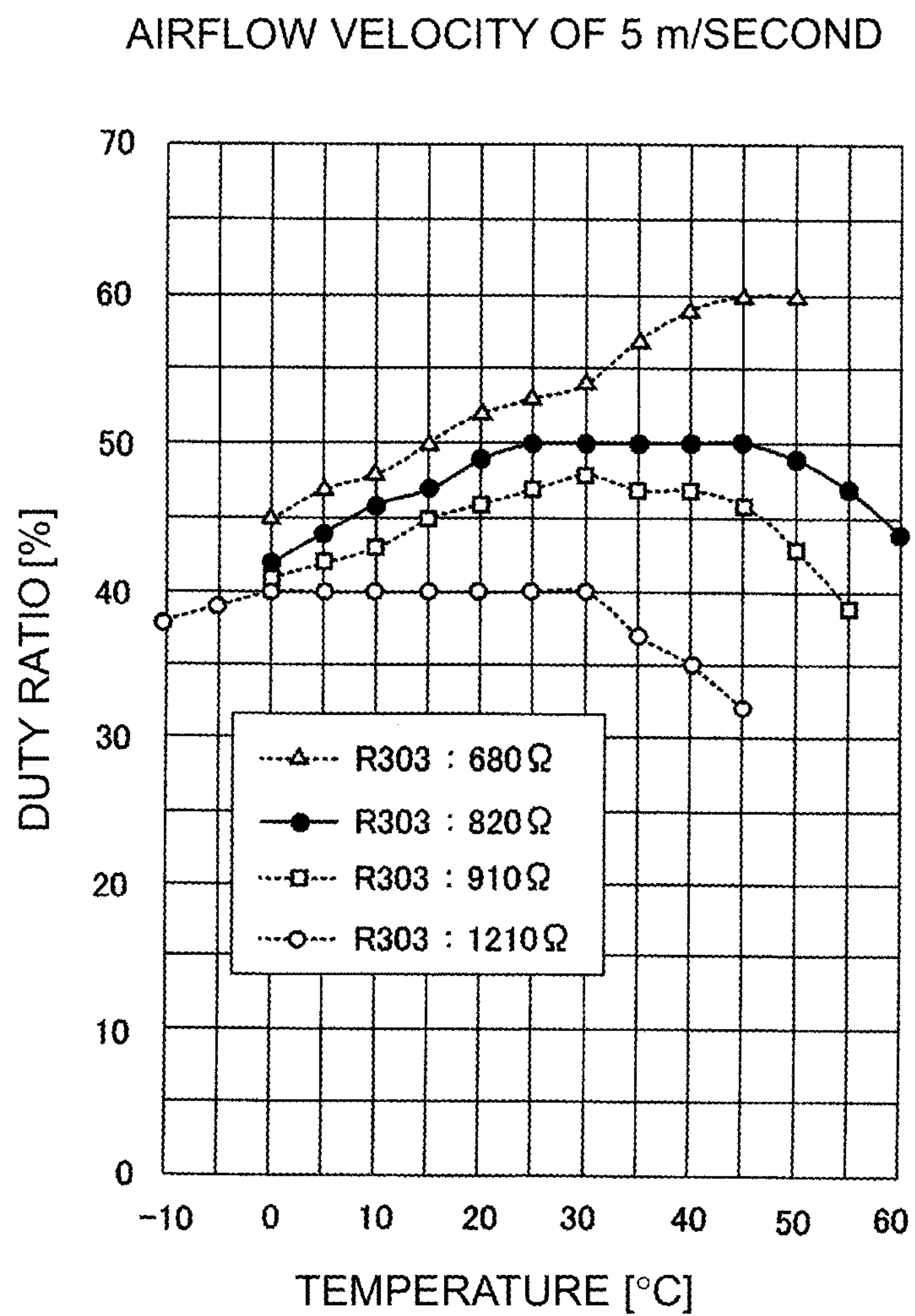


FIG. 10





**AIRFLOW VELOCITY MEASURING  
APPARATUS AND AIRFLOW RATE  
MEASURING APPARATUS**

CROSS REFERENCE TO RELATED  
APPLICATIONS

The present application is a continuation of International application No. PCT/JP2018/028802, filed Aug. 1, 2018, which claims priority to Japanese Patent Application No. 2017-152066, filed Aug. 5, 2017, the entire contents of each of which are incorporated herein by reference.

FIELD OF THE INVENTION

The present invention relates to an airflow velocity measuring apparatus, and more particularly, to an airflow velocity measuring apparatus that has a simple structure and is easy to manufacture at low cost and achieves high accuracy of measurement. The airflow velocity measuring apparatus of the present invention has a function of correcting measurement errors that occur in the airflow velocity caused by a rise or a fall in the temperature of subject airflow.

The present invention also relates to an airflow rate measuring apparatus that uses the above-described airflow velocity measuring apparatus.

BACKGROUND OF THE INVENTION

An airflow velocity measuring apparatus that is disposed within a duct, for example, to measure the velocity of a gas passing through the apparatus is disclosed in Patent Document 1 (Japanese Unexamined Patent Application Publication No. 2008-241318). A gas flowmeter **1000** disclosed in Patent Document 1 is shown in FIG. 6. The gas flowmeter **1000** is a device for measuring “airflow rate (gas flow rate)” instead of “airflow velocity.” As suggested in Patent Document 1, however, converting between “airflow rate” and “airflow velocity” is very easy.

The gas flowmeter **1000** includes a sensor body **101** and a controller **102**.

The sensor body **101** includes a thermocouple **104** and a thermistor element (thermistor) **105** formed on a printed substrate **103**.

The thermocouple **104** includes heating wire **106** and copper foils **107a** and **107b** bonded to the respective ends of the heating wire **106**. The heating wire **106** is formed of constantan, which is one type of Cu—Ni alloy, generating a thermo-electromotive force between the heating wire **106** and copper. In the thermocouple **104**, as a result of supplying power to the heating wire **106**, a thermo-electromotive force is generated between nodes **108a** and **108b**, which are disposed between the heating wire **106** and the respective copper foils **107a** and **107b**.

The controller **102** includes a power-supply control circuit **109**, a thermo-electromotive force detecting circuit **110**, a thermometer circuit **111**, an A/D converter **112**, and a control circuit **113**. The power-supply control circuit **109** controls power supply to the heating wire **106**. The thermo-electromotive force detecting circuit **110** detects a thermo-electromotive force generated between the nodes **108a** and **108b**. The thermometer circuit **111** receives output from the thermistor element **105**. The A/D converter **112** converts an analog signal supplied from the thermo-electromotive force detecting circuit **110** or the thermometer circuit **111** into a digital signal. The control circuit **113** controls the above-described elements.

In the case of a gentle gas flow, the gas flowmeter **1000** causes the thermo-electromotive force detecting circuit **110** to detect a thermo-electromotive force corresponding to a temperature difference  $\Delta T$  between the nodes **108a** and **108b**. The gas flowmeter **1000** then calculates a gas flow rate based on the magnitude of the thermo-electromotive force.

In the case of a strong gas flow, however, the heating wire **106** is exposed to the strong gas flow and is cooled, which makes it difficult for the thermocouple **104** to measure a gas flow rate. For a strong gas flow, the gas flowmeter **1000** detects the substrate temperature  $T$  of the printed substrate **103** by using the thermistor element **105**, and calculates a gas flow rate based on the detected substrate temperature  $T$ .

Patent Document 1: Japanese Unexamined Patent Application Publication No. 2008-241318

SUMMARY OF THE INVENTION

The above-described gas flowmeter **1000** measures a thermo-electromotive force generated between the nodes **108a** and **108b** or the substrate temperature  $T$  of the printed substrate **103** detected by the thermistor element **105**, based on the magnitude of the voltage. The measurements are thus vulnerable to noise, which decreases the measurement accuracy of a gas flow rate. Additionally, in the gas flowmeter **1000**, highly accurate, regular calibration is required for the thermo-electromotive force detecting circuit **110** and the thermometer circuit **111**, which increases the burden of maintenance. If regular calibration is not performed or calibration is not accurately performed for the thermo-electromotive force detecting circuit **110** and the thermometer circuit **111**, the gas flowmeter **1000** fails to measure a correct gas flow rate.

Additionally, the gas flowmeter **1000** has a complicated structure and is not easy to manufacture. The gas flowmeter **1000** also requires an expensive element, such as the A/D converter **112**, and is not possible to manufacture at low cost.

The present invention has been made to solve the above-described problems of the related art. As measures to solve the problems, an airflow velocity measuring apparatus of the present invention includes a fixed-temperature heat generating device that generates heat at or around a preset temperature. The fixed-temperature heat generating device includes a power supply, a heating element, a switching element, a comparator element, a first negative-temperature-coefficient thermistor element, and plural resistor elements. The heating element and the first negative-temperature-coefficient thermistor element are disposed at a measuring point at which a velocity of airflow is measured. The heating element is caused to generate heat by the power supply. The switching element is inserted between the power supply and the heating element. The comparator element controls ON and OFF of the switching element. The first negative-temperature-coefficient thermistor element is disposed near the heating element and is thermally coupled with the heating element so as to be able to accurately detect the temperature of the heating element. The resistance value of the first negative-temperature-coefficient thermistor element at the preset temperature is used as a threshold resistance value. The first negative-temperature-coefficient thermistor element and at least one of the plural resistor elements are connected in series with each other so as to form a temperature-detecting voltage divider circuit. A temperature-detecting voltage is output from a node between the first negative-temperature-coefficient thermistor element and the at least one of the plural resistor elements of the temperature-detecting voltage divider circuit. At least two of the



plural resistor elements are connected in series with each other so as to form a comparison voltage divider circuit. A comparison voltage is output from a node between one resistor element and another resistor element of the at least two of the plural resistor elements of the comparison voltage divider circuit. The comparator element compares the temperature-detecting voltage and the comparison voltage with each other and turns ON or OFF the switching element in accordance with a comparison result. As a result of the switching element being repeatedly turned ON and OFF, a pulse voltage is applied from the power supply to the heating element. The airflow velocity measuring apparatus measures the velocity of airflow at the measuring point based on a waveform of the applied pulse voltage. One of the at least two of the plural resistor elements forming the comparison voltage divider circuit includes at least a first divided resistor element, a second divided resistor element, and a second negative-temperature-coefficient thermistor element connected in series with each other. The airflow velocity measuring apparatus further includes a switch that switches between a first state in which both the first and second divided resistor elements are connected to the comparison voltage divider circuit and a second state in which only one of the first and second divided resistor elements is connected to the comparison voltage divider circuit.

In this airflow velocity measuring apparatus, a fixed voltage may be applied to the temperature-detecting voltage divider circuit, and a fixed voltage may be applied to the comparison voltage divider circuit. The resistance value of the at least one of the plural resistor elements of the temperature-detecting voltage divider circuit, the resistance values of the at least two of the plural resistor elements of the comparison voltage divider circuit, and the fixed voltage applied to each of the temperature-detecting voltage divider circuit and the comparison voltage divider circuit may be set so that the temperature-detecting voltage and the comparison voltage become equal to each other when the temperature of the first negative-temperature-coefficient thermistor element is the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is the threshold resistance value. When the temperature of the first negative-temperature-coefficient thermistor element is lower than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is greater than the threshold resistance value, the temperature-detecting voltage may be greater than the comparison voltage, and when the temperature of the first negative-temperature-coefficient thermistor element is higher than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is smaller than the threshold resistance value, the temperature-detecting voltage may be smaller than the comparison voltage. Alternatively, when the temperature of the first negative-temperature-coefficient thermistor element is lower than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is greater than the threshold resistance value, the temperature-detecting voltage may be smaller than the comparison voltage, and when the temperature of the first negative-temperature-coefficient thermistor element is higher than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is smaller than the threshold resistance value, the temperature-detecting voltage may be greater than the comparison voltage. The comparator element may compare the temperature-detecting voltage and the comparison voltage with each other. When the temperature of the first

negative-temperature-coefficient thermistor element is lower than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is greater than the threshold resistance value, the comparator element may turn ON the switching element. When the temperature of the first negative-temperature-coefficient thermistor element is higher than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is smaller than the threshold resistance value, the comparator element may turn OFF the switching element. The switch may switch between the first and second states in response to the temperature of airflow passing through the measuring point. With this configuration, the velocity of airflow can be measured without the occurrence of measurement errors caused by a change in the temperature of airflow.

For example, as a result of a microcomputer having detected the temperature of airflow passing through the measuring point, the switch may switch between the first and second states under control of the microcomputer. With this configuration, the switch can suitably switch between the first and second states in accordance with the temperature of airflow.

Alternatively, the switch may switch between the first and second states in response to the resistance value of the second negative-temperature-coefficient thermistor element. The resistance value is changed by the temperature of airflow passing through the measuring point. In this case, the switch can suitably switch between the first and second states in accordance with the temperature of airflow merely by using the airflow velocity measuring apparatus.

The airflow velocity measuring apparatus of the present invention may be used as an airflow rate measuring apparatus.

The airflow velocity measuring apparatus of the present invention is able to correct measurement errors caused by a change in the airflow temperature and thus achieves high accuracy of measurement. The airflow velocity measuring apparatus of the present invention is less vulnerable to noise and thus achieves high accuracy of measurement. The airflow velocity measuring apparatus of the present invention has a simple structure and is easy to manufacture. The airflow velocity measuring apparatus of the present invention does not require an expensive element, such as an A/D converter, and can be manufactured at low cost.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is an equivalent circuit diagram of an airflow velocity measuring apparatus 100 according to a first embodiment.

FIG. 2 is a graph illustrating the relationship between the airflow temperature and the duty ratio of a pulse voltage when the airflow velocity is 5 m/second in the airflow velocity measuring apparatus 100.

FIG. 3 is a graph illustrating the relationship between the airflow velocity and the duty ratio of a pulse voltage in the airflow velocity measuring apparatus 100.

FIG. 4 is an equivalent circuit diagram of an airflow velocity measuring apparatus 200 according to a second embodiment.

FIG. 5 is an equivalent circuit diagram of an airflow velocity measuring apparatus 300 according to a third embodiment.

FIG. 6 is an equivalent circuit diagram of a gas flowmeter 1000 disclosed in Patent Document 1.



FIG. 7 is an equivalent circuit diagram of an airflow velocity measuring apparatus **1100A** used as a reference.

FIG. 8(A) is a graph illustrating the temperature transition of a positive-temperature-coefficient thermistor element **222** and a first negative-temperature-coefficient thermistor element **221** at a certain airflow velocity in the airflow velocity measuring apparatus **1100A**; and FIG. 8(B) is a graph illustrating the pulse voltage supplied from a power supply  $V_{cc}$  to the positive-temperature-coefficient thermistor element **222** in accordance with a time change in FIG. 8(A).

FIG. 9 is an equivalent circuit diagram of an airflow velocity measuring apparatus **1100B** used as a reference.

FIG. 10 is a graph illustrating the relationship between the airflow temperature and the duty ratio of a pulse voltage when the airflow velocity is 5 m/second in the airflow velocity measuring apparatus **1100B**.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Hereinafter, embodiments of the present invention will be described below with reference to the drawings. The individual embodiments merely illustrate examples of embodiments of the invention, and the invention is not restricted thereto. Different embodiments may suitably be combined with each other and be carried out, and the content of such a combined embodiment is encompassed within the invention. The drawings are provided for the better understanding of the specification and some drawings are only schematically shown. The size ratio of each component or the size ratio of one component to that of another component shown in the drawings may not match that described in the specification. Some components described in the specification may not be shown in the drawings, or a component shown in a drawing may not be as many as that described in the specification.

#### First Embodiment; Airflow Velocity Measuring Apparatus **100**

An airflow velocity measuring apparatus **100** according to a first embodiment is shown in FIG. 1.

Before completing the invention of this application, the inventor of this application has developed an airflow velocity measuring apparatus **1100A** (see FIG. 7) as a reference outside the scope of the invention of this application. The airflow velocity measuring apparatus **1100A** achieves high accuracy of measurement and has a simple structure and is easy to manufacture at low cost without requiring an expensive element, such as an A/D converter. In the airflow velocity measuring apparatus **1100A**, however, measurement errors occur in the airflow velocity caused by a rise or a fall in the temperature of subject airflow.

To address this issue, the inventor of this application has made improvements in the airflow velocity measuring apparatus **1100A** and developed an airflow velocity measuring apparatus **1100B** (see FIG. 9) used as a reference outside the scope of the invention of this application. The airflow velocity measuring apparatus **1100B** has a function of suitably correcting measurement errors in the airflow velocity caused by a rise or a fall in the temperature of subject airflow. The airflow velocity measuring apparatus **1100B** is able to measure the airflow velocity with high accuracy without being influenced by a rise or a fall in the temperature of subject airflow. However, the airflow velocity measuring apparatus **1100B** can correct measurement errors in the airflow velocity only within a limited range of temperatures.

To address this issue, the inventor of this application has made improvements in the airflow velocity measuring apparatus **1100B** and completed the invention of this application. That is, the airflow velocity measuring apparatus of the invention of this application is free from the problem found in the airflow velocity measuring apparatus **1100B**, and can suitably correct measurement errors in the airflow velocity over a wide temperature range.

In view of the background and history that have led to the completion of the invention of this application, before the airflow velocity measuring apparatus **100** according to the first embodiment is explained, the airflow velocity measuring apparatuses **1100A** and **1100B** used as references outside the scope of the invention of this application will be discussed below.

(Airflow Velocity Measuring Apparatus **1100A** as Reference)

The airflow velocity measuring apparatus **1100A** used as a reference outside the scope of the invention of this application is shown in FIG. 7.

The airflow velocity measuring apparatus **1100A** includes a fixed-temperature heat generating device **210**. The preset temperature of the fixed-temperature heat generating device **210** is about 40° C. That is, the fixed-temperature heat generating device **210** is designed to generate heat at a fixed temperature of about 40° C.

The fixed-temperature heat generating device **210** includes a heating unit **220** and a temperature controller **230**.

The heating unit **220** includes a first negative-temperature-coefficient thermistor element **221** and a positive-temperature-coefficient thermistor element **222**, which is a heating element. The first negative-temperature-coefficient thermistor element **221** and the positive-temperature-coefficient thermistor element **222** are thermally coupled with each other. The first negative-temperature-coefficient thermistor element **221** is used for measuring the temperature of the positive-temperature-coefficient thermistor element **222**. As the positive-temperature-coefficient thermistor element **222**, a heating element having a resistance value of 68 kΩ at 25° C. is used. The type of heating element is not limited to the positive-temperature-coefficient thermistor element **222**, and a heater element may alternatively be used.

The temperature controller **230** includes a power supply  $V_{cc}$ . A direct current of 6 V, for example, is used as the power supply  $V_{cc}$ . A switch SW1 is connected to the power supply  $V_{cc}$  as a power supply switch.

The temperature controller **230** includes a switching element Q1. The switching element Q1 is connected at one end to the switch SW1 and at the other end to the positive-temperature-coefficient thermistor element **222**. The switching element Q1 switches ON and OFF of power supply from the power supply  $V_{cc}$  to the positive-temperature-coefficient thermistor element **222**. As the switching element Q1, a PNP transistor, for example, is used.

The temperature controller **230** includes a resistor element R201. The resistor element R201 is connected in series with the first negative-temperature-coefficient thermistor element **221** so as to form a temperature-detecting voltage divider circuit. The temperature-detecting voltage divider circuit outputs a temperature-detecting voltage from a node between the resistor element R201 and the first negative-temperature-coefficient thermistor element **221**.

The temperature controller **230** includes a comparison voltage divider circuit having resistor elements R202 and R203 connected in series with each other. The comparison voltage divider circuit outputs a comparison voltage from a node between the resistor elements R202 and R203.



The temperature controller **230** includes a comparator element **Cmp1**.

The node between the resistor element **R201** and the first negative-temperature-coefficient thermistor element **221** forming the temperature-detecting voltage divider circuit is connected to the inverting input terminal – of the comparator element **Cmp1**.

The node between the resistor elements **R202** and **R203** forming the comparison voltage divider circuit is connected to the non-inverting input terminal + of the comparator element **Cmp1**.

The positive power supply terminal of the comparator element **Cmp1** is connected to the load terminal of the switch **SW1**.

The negative power supply terminal of the comparator element **Cmp1** is connected to a ground.

The output terminal of the comparator element **Cmp1** is connected to the control terminal of the switching element **Q1** via a resistor element **R204**.

A node between the resistor element **R204** and the switching element **Q1** is connected to the load terminal of the switch **SW1** via a resistor element **R205**.

The resistance values of the resistor elements **R201**, **R202**, and **R203** are shown in Table 1. The resistance-temperature characteristics of the first negative-temperature-coefficient thermistor element **221** are shown in Table 2. Table 1 also shows the resistance value of the first negative-temperature-coefficient thermistor element **221** at 40° C. The resistance values of the resistor elements **R204** and **R205** are suitably set.

TABLE 1

	Resistance value	Voltage
R201	4.7 kΩ	<<Temperature-detecting voltage at 40° C.>>
221	5.6 kΩ	5.6
(NTC)	(Resistance value at 40° C.)	$\frac{5.6}{4.7 + 5.6} \times 6.0 \approx 3.26$ (V: 40° C.)
R202	4.7 kΩ	<<Comparison voltage>>
R203	5.6 kΩ	$\frac{5.6}{4.7 + 5.6} \times 6.0 \approx 3.26$ (V)

TABLE 2

Resistance-temperature characteristics of first negative-temperature-coefficient thermistor 221	
25° C.	10 kΩ
30° C.	8.3 kΩ
35° C.	6.9 kΩ
40° C.	5.6 kΩ
45° C.	4.9 kΩ
50° C.	4.2 kΩ

When using the airflow velocity measuring apparatus **1100A**, the heating unit **220** having the thermally coupled first negative-temperature-coefficient thermistor element **221** and positive-temperature-coefficient thermistor element **222** is placed in the flow channel of subject airflow.

For example, at an ambient temperature of 25° C., the switch **SW1** of the fixed-temperature heat generating device **210** is turned ON, and then, a voltage of 6 V is applied to the temperature-detecting voltage divider circuit having the series-connected resistor element **R201** and first negative-temperature-coefficient thermistor element **221** and to the comparison voltage divider circuit having the series-connected resistor elements **R202** and **R203**. At this time, the

resistance value of the resistor element **R201** of the temperature-detecting voltage divider circuit is 4.7 kΩ, and the resistance value of the first negative-temperature-coefficient thermistor element **221** is 10 kΩ (see Table 2). The resulting voltage output from the temperature-detecting voltage divider circuit to the inverting input terminal – of the comparator element **Cmp1** is about 4.08 V. The resistance value of the resistor element **R202** of the comparison voltage divider circuit is 4.7 kΩ, and that of the resistor element **R203** is 5.6 kΩ. The resulting voltage output from the comparison voltage divider circuit to the non-inverting input terminal + of the comparator element **Cmp1** is about 3.26 V.

If the resulting voltage output from the temperature-detecting voltage divider circuit to the inverting input terminal – is greater than that output from the comparison voltage divider circuit to the non-inverting input terminal +, the comparator element **Cmp1** turns ON the switching element **Q1**. Conversely, if the resulting voltage output from the temperature-detecting voltage divider circuit to the inverting input terminal – is smaller than that output from the comparison voltage divider circuit to the non-inverting input terminal +, the comparator element **Cmp1** turns OFF the switching element **Q1**.

When the switch **SW1** of the fixed-temperature heat generating device **210** is turned ON, the resulting voltage output from the temperature-detecting voltage divider circuit to the inverting input terminal – is greater than that output from the comparison voltage divider circuit to the non-inverting input terminal +. The comparator element **Cmp1** thus turns ON the switching element **Q1**. As a result of turning ON the switch **SW1** of the fixed-temperature heat generating device **210**, power is supplied from the power supply **Vcc** to the positive-temperature-coefficient thermistor element **222** via the switching element **Q1**, so that the positive-temperature-coefficient thermistor element **222** starts generating heat.

As the temperature of the positive-temperature-coefficient thermistor element **222** rises, the temperature of the thermally coupled first negative-temperature-coefficient thermistor element **221** also rises, and the resistance value of the first negative-temperature-coefficient thermistor element **221** drops. The resulting voltage output from the temperature-detecting voltage divider circuit to the inverting input terminal – starts to drop from about 4.08 V, which is the initial value.

The temperatures of the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221** rise to 40° C., which is the preset temperature, and the resistance value of the first negative-temperature-coefficient thermistor element **221** drops to 5.6 kΩ. The resulting voltage output from the temperature-detecting voltage divider circuit drops to about 3.26 V, which is the same voltage output from the comparison voltage divider circuit. At this time point, the comparator element **Cmp1** turns OFF the switching element **Q1** to stop supplying power from the power supply **Vcc** to the positive-temperature-coefficient thermistor element **222**.

As a result of stopping supplying power from the power supply **Vcc** to the positive-temperature-coefficient thermistor element **222**, the temperature of the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221** becomes lower than 40° C., which is the preset temperature. Then, the comparator element **Cmp1** turns ON the switching element **Q1** to restart supplying power from the power supply **Vcc** to the positive-temperature-coefficient thermistor element **222**.



In this manner, as a result of repeatedly supplying and stopping power to the positive-temperature-coefficient thermistor element **222**, the fixed-temperature heat generating device **210** maintains the temperature of the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221** at around 40° C., which is the preset temperature.

The temperature transition of the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221** at a certain airflow velocity is illustrated in FIG. **8(A)**. The voltage supplied from the power supply Vcc to the positive-temperature-coefficient thermistor element **222** in accordance with a time change in FIG. **8(A)** is illustrated in FIG. **8(B)**. FIG. **8(B)** shows that a regular, a pulsating voltage (hereinafter called a pulse voltage) is supplied from the power supply Vcc to the positive-temperature-coefficient thermistor element **222**.

As shown in FIG. **7**, in the airflow velocity measuring apparatus **1100A**, a pulse voltage monitor **240** is disposed between the switching element Q1 of the temperature controller **230** and the positive-temperature-coefficient thermistor element **222** of the heating unit **220**. In the pulse voltage monitor **240**, the waveform of a pulse voltage is monitored by a counter of a microcomputer **250**, for example. The counter of the microcomputer **250** includes a 1000-Hz oscillator, for example, and reads the value of the pulse voltage one thousand times per second to detect the waveform of the pulse voltage.

The airflow velocity measuring apparatus **1100A** measures (calculates) the airflow velocity based on the duration of one "ON" time period of the waveform of the pulse voltage read by the microcomputer **250** or the duty ratio of the waveform of the pulse voltage. More specifically, as the airflow velocity increases in order of zero, low, intermediate, and high, heat is more likely to be taken away from the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221**. The fixed-temperature heat generating device **210** thus increases the "ON" time period of the pulse voltage to be longer and the duty ratio to be higher in order to maintain the preset temperature. The airflow velocity measuring apparatus **1100A** measures (calculates) the airflow velocity based on the "ON" time period or the duty ratio of the pulse voltage.

The airflow velocity measuring apparatus **1100A** configured as described above achieves high accuracy of measurement and has a simple structure and is easy to manufacture at low cost without requiring an expensive element, such as an A/D converter.

In the airflow velocity measuring apparatus **1100A**, however, measurement errors occur in the airflow velocity caused by a rise or a fall in the temperature of subject airflow. More specifically, if the airflow velocity measuring apparatus **1100A** is designed with a preset (assumed) airflow temperature of an ambient temperature of 25° C., when the airflow temperature becomes higher than 25° C., the duty ratio of the waveform of a detected pulse voltage becomes lower than that corresponding to the actual airflow velocity under the influence of a rise in the airflow temperature. The reason for this is as follows. When the airflow temperature becomes higher than 25° C., the temperature of the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221** rises faster than that at a temperature of 25° C. because of a rise in the airflow temperature. Conversely, when the airflow temperature becomes lower than 25° C., the duty

ratio of the waveform of a detected pulse voltage becomes higher than that corresponding to the actual airflow velocity under the influence of a fall in the airflow temperature. The reason for this is as follows. When the airflow temperature becomes lower than 25° C., the temperature of the positive-temperature-coefficient thermistor element **222** and the first negative-temperature-coefficient thermistor element **221** rises more slowly than that at a temperature of 25° C. because of a fall in the airflow temperature.

In this manner, the following problem arises in the airflow velocity measuring apparatus **1100A**. When the airflow temperature becomes higher than 25° C., the duty ratio of the waveform of a detected pulse voltage becomes lower than that corresponding to the actual airflow velocity. Conversely, when the airflow temperature becomes lower than 25° C., the duty ratio of the waveform of a detected pulse voltage becomes higher than that corresponding to the actual airflow velocity.

To address this issue, the inventor of this application has made improvements in the airflow velocity measuring apparatus **1100A** and developed the airflow velocity measuring apparatus **1100B** having a function of suitably correcting measurement errors in the airflow velocity caused by a rise or a fall in the temperature of subject airflow.

(Airflow Velocity Measuring Apparatus **1100B** as Reference)

The airflow velocity measuring apparatus **1100B** used as a reference outside the scope of the invention of this application is shown in FIG. **9**.

The airflow velocity measuring apparatus **1100B** includes a fixed-temperature heat generating device **310**. The preset temperature of the fixed-temperature heat generating device **310** is about 35° C. The fixed-temperature heat generating device **310** includes a heating unit **320** and a temperature controller **330**.

The heating unit **320** includes a first negative-temperature-coefficient thermistor element **321**, which is a first temperature sensor element, and a positive-temperature-coefficient thermistor element **322**, which is a heating element. As the first negative-temperature-coefficient thermistor element **321**, the same thermistor element as the first negative-temperature-coefficient thermistor element **221** of the airflow velocity measuring apparatus **1100A** is used. As the positive-temperature-coefficient thermistor element **322**, the same thermistor element as the positive-temperature-coefficient thermistor element **222** of the airflow velocity measuring apparatus **1100A** is used.

As in the airflow velocity measuring apparatus **1100A**, the temperature controller **330** includes a power supply Vcc. A direct current of 6 V, for example, is used as the power supply Vcc. A switch SW1 is connected to the power supply Vcc as a power supply switch.

As in the airflow velocity measuring apparatus **1100A**, the temperature controller **330** includes a switching element Q1.

The temperature controller **330** includes a resistor element **R301**. The resistor element **R301** is connected in series with the first negative-temperature-coefficient thermistor element **321** so as to form a temperature-detecting voltage divider circuit. The temperature-detecting voltage divider circuit outputs a temperature-detecting voltage from a node between the resistor element **R301** and the first negative-temperature-coefficient thermistor element **321**.

The temperature controller **330** includes a comparison voltage divider circuit having resistor elements **R302** and **R303** and a second negative-temperature-coefficient thermistor **332** connected in series with each other. The second negative-temperature-coefficient thermistor **332** serves to



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correct measurement errors in the airflow velocity caused by a rise or a fall in the temperature of subject airflow. The comparison voltage divider circuit outputs a comparison voltage from a node between the resistor elements R302 and R303. As the second negative-temperature-coefficient thermistor 232, a thermistor element having the same resistance-temperature characteristics as the first negative-temperature-coefficient thermistor element 321 is used.

The second negative-temperature-coefficient thermistor 332 is disposed near the heating unit 320 such that it is thermally separated from the positive-temperature-coefficient thermistor element 322 and the first negative-temperature-coefficient thermistor element 321 of the heating unit 320. In accordance with the temperature of subject airflow, the second negative-temperature-coefficient thermistor 232 changes its temperature and changes its resistance.

As in the airflow velocity measuring apparatus 1100A, the temperature controller 330 includes a comparator element Cmp1.

The output terminal of the comparator element Cmp1 is connected to the control terminal of the switching element Q1 via a resistor element R304. A node between the resistor element R304 and the switching element Q1 is connected to the load terminal of the switch SW1 via a resistor element R305.

The resistance values of the resistor elements R301, R302, and R303 are shown in Table 3. The resistance-temperature characteristics of the first negative-temperature-coefficient thermistor element 321 and the second negative-temperature-coefficient thermistor 332 are shown in Table 4. The resistance values of the resistor elements R304 and R305 are suitably set.

TABLE 3

	Resistance value
R301	22 k $\Omega$
R302	33 k $\Omega$
R303	820 $\Omega$

TABLE 4

Resistance-temperature characteristics of first and second negative-temperature-coefficient thermistors 321 and 332	
25° C.	10 k $\Omega$
30° C.	8.3 k $\Omega$
35° C.	6.9 k $\Omega$
40° C.	5.6 k $\Omega$
45° C.	4.9 k $\Omega$
50° C.	4.2 k $\Omega$

As in the airflow velocity measuring apparatus 1100A, the airflow velocity measuring apparatus 1100B includes a pulse voltage monitor 340. In the pulse voltage monitor 340, the waveform of a pulse voltage is monitored by a counter of a microcomputer 350, for example.

As a result of selecting the resistance values of the resistor elements R301, R302, and R303 and the resistance-temperature characteristics of the first negative-temperature-coefficient thermistor element 321 and the second negative-temperature-coefficient thermistor 332, as indicated in Table 3 and Table 4, the airflow velocity measuring apparatus 1100B can correct measurement errors in the airflow velocity caused by a rise or a fall in the temperature of subject airflow.

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More specifically, when the temperature of airflow measured at the second negative-temperature-coefficient thermistor 332 becomes higher than 25° C., the airflow velocity measuring apparatus 1100B adjusts the preset temperature of the fixed-temperature heat generating device 310 to be higher than 35° C., which is the initial preset temperature. When the temperature of the airflow becomes lower than 25° C., the airflow velocity measuring apparatus 1100B adjusts the preset temperature of the fixed-temperature heat generating device 310 to be lower than 35° C., which is the initial preset temperature. As a result, the duty ratio of a pulse voltage supplied from the power supply Vcc to the positive-temperature-coefficient thermistor element 322 changes solely by the velocity of subject airflow regardless of whether the airflow temperature rises or falls. That is, the airflow velocity measuring apparatus 1100B is able to detect a highly accurate airflow velocity without the occurrence of measurement errors caused by a rise or a fall in the airflow temperature.

However, the airflow velocity measuring apparatus 1100B can correct such measurement errors in the airflow velocity only within a limited range of temperatures. The range of temperatures within which measurement errors in the airflow velocity can be corrected is changed in accordance with the resistance value of the resistor element R303 forming the comparison voltage divider circuit.

As discussed above, in the airflow velocity measuring apparatus 1100B, the resistance value of the resistor element R303 is set to be 820 $\Omega$ . FIG. 10 is a graph illustrating the relationship between the airflow temperature and the duty ratio of a pulse voltage when the airflow velocity is 5 m/second in the airflow velocity measuring apparatus 1100B including the resistor element R303 of 820 $\Omega$  (solid line in the graph).

As is seen from FIG. 10, in the airflow velocity measuring apparatus 1100B including the resistor element R303 of 820 $\Omega$ , when the airflow temperature is about 25 to 50° C., the duty ratio of the pulse voltage is flat without being influenced by a change in the airflow temperature. That is, when the airflow temperature is about 25 to 50° C., the airflow velocity measuring apparatus 1100B including the resistor element R303 of 820 $\Omega$  is able to suitably correct measurement errors in the airflow velocity caused by a rise or a fall in the airflow temperature. In other words, when the airflow temperature is lower than 25° C. or exceeds 50° C., the airflow velocity measuring apparatus 1100B is unable to correct such measurement errors.

As described above, the range of temperatures within which measurement errors in the airflow velocity can be corrected is changed in accordance with the resistance value of the resistor element R303 forming the comparison voltage divider circuit. FIG. 10 also illustrates the relationship between the airflow temperature and the duty ratio of the pulse voltage at an airflow velocity of 5 m/second when the resistance value of the resistor element R303 is varied to 680  $\Omega$ , 910 $\Omega$ , and 1210 $\Omega$  (broken lines in the graph).

As is seen from FIG. 10, when the resistance value of the resistor element R303 is changed to 1210 $\Omega$ , the duty ratio of the pulse voltage becomes flat without being influenced by a change in the airflow temperature in a range of about 0 to 30° C. In other words, when the resistance value of the resistor element R303 is changed to 1210 $\Omega$ , measurement errors in the airflow velocity caused by a rise or a fall in the airflow temperature can be corrected in a range of the airflow temperature of about 0 to 30° C.

The inventor of this application has thus made improvements in the airflow velocity measuring apparatus 1100B



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and completed the invention of this application. That is, in the airflow velocity measuring apparatus of the invention of this application, the resistance value of the resistor element R303 is changed in accordance with whether the temperature of subject airflow is lower than a predetermined temperature (30° C., for example) or higher than the predetermined temperature. Then, measurement errors in the airflow velocity caused by a rise or a fall in the airflow temperature can suitably be corrected over a wide temperature range.

(Airflow Velocity Measuring Apparatus 100)

As described above, the airflow velocity measuring apparatus 100 according to the first embodiment is shown in FIG. 1. FIG. 1 is an equivalent circuit diagram of the airflow velocity measuring apparatus 100.

The airflow velocity measuring apparatus 100 includes a fixed-temperature heat generating device 10. The preset temperature of the fixed-temperature heat generating device 10 is about 35° C. That is, the fixed-temperature heat generating device 10 is designed to generate heat at a fixed temperature of about 35° C.

The fixed-temperature heat generating device 10 includes a heating unit 20 and a temperature controller 30.

The heating unit 20 includes a first negative-temperature-coefficient thermistor element 21 and a positive-temperature-coefficient thermistor element 22, which is a heating element. The first negative-temperature-coefficient thermistor element 21 and the positive-temperature-coefficient thermistor element 22 are thermally coupled with each other. The first negative-temperature-coefficient thermistor element 21 is used for measuring the temperature of the positive-temperature-coefficient thermistor element 22. As the positive-temperature-coefficient thermistor element 22, a thermistor element having a resistance value of 68 kΩ at 25° C. is used. The type of heating element is not limited to the positive-temperature-coefficient thermistor element 22, and a heater element may alternatively be used.

The temperature controller 30 includes a power supply Vcc. A direct current of 6 V, for example, is used as the power supply Vcc. A first switch SW1 is connected to the power supply Vcc as a power supply switch.

The temperature controller 30 includes a switching element Q1. The switching element Q1 is connected at one end to the first switch SW1 and at the other end to the positive-temperature-coefficient thermistor element 22. The switching element Q1 switches ON and OFF of power supply from the power supply Vcc to the positive-temperature-coefficient thermistor element 22. As the switching element Q1, a PNP transistor is used. However, the type of switching element Q1 is not limited to a PNP transistor, and another type of switching element may be used.

The temperature controller 30 includes a resistor element R1. The resistor element R1 is connected in series with the first negative-temperature-coefficient thermistor element 21 so as to form a temperature-detecting voltage divider circuit. The temperature-detecting voltage divider circuit outputs a temperature-detecting voltage from a node between the resistor element R1 and the first negative-temperature-coefficient thermistor element 21.

The temperature controller 30 includes a comparison voltage divider circuit having a resistor element R2, a second negative-temperature-coefficient thermistor element 32, and a resistor element R3 connected in series with each other. In practice, the resistor element R3 is divided into two resistor elements, that is, first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub>. The comparison voltage divider circuit outputs a comparison voltage from a node between

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the resistor element R2 and the second negative-temperature-coefficient thermistor element 32.

The temperature controller 30 includes a comparator element Cmp1.

The node between the resistor element R1 and the first negative-temperature-coefficient thermistor element 21 forming the temperature-detecting voltage divider circuit is connected to the inverting input terminal – of the comparator element Cmp1.

The node between the resistor element R2 and the second negative-temperature-coefficient thermistor element 32 forming the comparison voltage divider circuit is connected to the non-inverting input terminal + of the comparator element Cmp1.

The positive power supply terminal of the comparator element Cmp1 is connected to the load terminal of the first switch SW1.

The negative power supply terminal of the comparator element Cmp1 is connected to a ground.

The output terminal of the comparator element Cmp1 is connected to the control terminal of the switching element Q1 via a resistor element R4.

A node between the resistor element R4 and the switching element Q1 is connected to the load terminal of the switch SW1 via a resistor element R5.

The temperature controller 30 includes a second switch SW2 between a ground and a node between the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub>. The second switch SW2 is turned OFF when the temperature of subject airflow is lower than 30° C. and is turned ON when the temperature of subject airflow is 30° C. or higher.

As a result, when the temperature of subject airflow is lower than 30° C., the resistance value of the resistor element R3 forming the comparison voltage divider circuit becomes equal to the added value of the resistance values of the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub>. When the temperature of subject airflow is 30° C. or higher, the resistance value of the resistor element R3 becomes equal to that of only the first divided resistor element R3<sub>A</sub>.

The resistance values of the resistor elements R1, R2, and R3 and the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub> are shown in Table 5. The resistance-temperature characteristics of the first and second negative-temperature-coefficient thermistor elements 21 and 32 are shown in Table 6. The resistance values of the resistor elements R4 and R5 are suitably set.

TABLE 5

Resistance value		
R1		22 kΩ
R2		33 kΩ
R3	R3 <sub>A</sub> + R3 <sub>B</sub> (lower than 30° C.)	1210 Ω
	R3 <sub>A</sub> (30° C. or higher)	820 Ω
R3 <sub>A</sub>		820 Ω
R3 <sub>B</sub>		390 Ω

TABLE 6

Resistance-temperature characteristics of first and second negative-temperature-coefficient thermistors 21 and 32	
25° C.	10 kΩ
30° C.	8.3 kΩ
35° C.	6.9 kΩ
40° C.	5.6 kΩ
45° C.	4.9 kΩ
50° C.	4.2 kΩ



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According to the same principle of the airflow velocity measuring apparatuses **1100A** and **1100B**, as a result of turning ON the first switch **SW1**, the airflow velocity measuring apparatus **100** repeatedly supplies and stops power from the power supply to the positive-temperature-coefficient thermistor element **22**. This maintains the temperature of the positive-temperature-coefficient thermistor element **22** and the first negative-temperature-coefficient thermistor element **21** at around 35° C., which is the preset temperature.

According to the same principle of the airflow velocity measuring apparatuses **1100A** and **1100B**, the airflow velocity measuring apparatus **100** measures (calculates) the velocity of subject airflow based on the duty ratio of a pulse voltage (or the duration of one "ON" time period).

According to the same principle of the airflow velocity measuring apparatus **1100B**, the airflow velocity measuring apparatus **100** corrects measurement errors in the airflow velocity caused by a rise or a fall in the temperature of subject airflow. The airflow velocity measuring apparatus **100** corrects measurement errors after switching the resistance value of the resistor element **R3** (first and second divided resistor elements **R3<sub>A</sub>** and **R3<sub>B</sub>**) in accordance with whether the temperature of subject airflow is lower than 30° C. or higher than or equal to 30° C. That is, the airflow velocity measuring apparatus **100** corrects measurement errors by using two modes, that is, a low temperature mode to be used when the temperature of subject airflow is lower than 30° C. and a high temperature mode to be used when the temperature of subject airflow is 30° C. or higher.

The relationship between the airflow temperature and the duty ratio of a pulse voltage when the airflow velocity is 5 m/second is shown in FIG. 2. The relationship between the airflow temperature and the duty ratio of a pulse voltage when the airflow velocity is 0 m/second (velocity is 0) is shown in FIG. 2.

As is seen from FIG. 2, in the airflow velocity measuring apparatus **100**, as a result of switching between the low temperature mode and the high temperature mode in accordance with whether the temperature of subject airflow is lower than 30° C. or higher than or equal to 30° C., the duty ratio of the pulse voltage becomes constant (flat) without being influenced by a change in the airflow temperature. That is, regardless of when the airflow temperature is lower than 30° C. or 30° C. or higher, the airflow velocity measuring apparatus **100** is able to suitably correct measurement errors in the airflow velocity caused by a change in the airflow temperature.

Information concerning whether the airflow velocity measuring apparatus **100** is correcting measurement errors in the low temperature mode or the high temperature mode is transmitted from the airflow velocity measuring apparatus **100** to a microcomputer **50**. By taking this information into consideration, the microcomputer **50** calculates the airflow velocity based on the waveform of a pulse voltage obtained by a pulse voltage monitor **40**.

The relationship between the velocity of subject airflow and the duty ratio of a pulse voltage is shown in FIG. 3. The airflow velocity measuring apparatus **100** selectively uses one of the two different relational expressions concerning the airflow velocity and the duty ratio of a pulse voltage in accordance with whether the airflow temperature is lower than 30° C. or higher than or equal to 30° C.

In the airflow velocity measuring apparatus **100**, measurement errors in the airflow velocity caused by a change in the airflow temperature can suitably be corrected over a wide temperature range.

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Second Embodiment; Airflow Velocity Measuring Apparatus **200**

An airflow velocity measuring apparatus **200** according to a second embodiment is shown in FIG. 4. FIG. 4 is an equivalent circuit diagram of the airflow velocity measuring apparatus **200**.

The airflow velocity measuring apparatus **200** is an apparatus in which part of the configuration of the airflow velocity measuring apparatus **100** of the above-described first embodiment is changed. In the airflow velocity measuring apparatus **100**, the second switch **SW2** is provided between a ground and a node between the first and second divided resistor elements **R3<sub>A</sub>** and **R3<sub>B</sub>**. In the airflow velocity measuring apparatus **200**, instead of the second switch **SW2**, a second switching element **Q2** is disposed between a ground and a node between the first and second divided resistor elements **R3<sub>A</sub>** and **R3<sub>B</sub>**. In this embodiment, an NPN transistor is used as the second switching element **Q2**. However, the type of second switching element **Q2** is not limited to an NPN transistor, and another type of switching element may be used.

The control terminal of the second switching element **Q2** is connected to the microcomputer **50**, so that the second switching element **Q2** can be controlled by the microcomputer **50**. The microcomputer **50** and the second switching element **Q2** are connected with each other such that a resistor element **R6** is inserted therebetween and a resistor element **R7** is inserted between a ground and a node between the resistor element **R6** and the second switching element **Q2**. The resistance values of the resistor elements **R6** and **R7** are suitably selected.

The microcomputer **50** obtains information concerning the temperature of subject airflow in advance. When the airflow temperature indicated by this information is found to be lower than 30° C., the microcomputer **50** turns OFF the second switching element **Q2**. When the airflow temperature indicated by this information is found to be 30° C. or higher, the microcomputer **50** turns ON the second switching element **Q2** so as to short-circuit the node between the first and second divided resistor elements **R3<sub>A</sub>** and **R3<sub>B</sub>** and connect the node to a ground.

In the airflow velocity measuring apparatus **200**, as well as in the airflow velocity measuring apparatus **100**, measurement errors in the airflow velocity caused by a change in the airflow temperature can suitably be corrected over a wide temperature range.

Third Embodiment; Airflow Velocity Measuring Apparatus **300**

An airflow velocity measuring apparatus **300** according to a third embodiment is shown in FIG. 5. FIG. 5 is an equivalent circuit diagram of the airflow velocity measuring apparatus **300**.

The airflow velocity measuring apparatus **300** is also an apparatus in which part of the configuration of the airflow velocity measuring apparatus **100** of the above-described first embodiment is changed. In the airflow velocity measuring apparatus **100**, the second switch **SW2** is provided between a ground and a node between the first and second divided resistor elements **R3<sub>A</sub>** and **R3<sub>B</sub>**. In the airflow velocity measuring apparatus **300**, instead of the second switch **SW2**, a second comparator element **Cmp2** is disposed.

A direct current of about 1.3 V is applied to the inverting input terminal - of the second comparator element **Cmp2**.



A node between the resistor elements R2 and R3 (first divided resistor element R3<sub>A</sub>) of the comparison voltage divider circuit is connected to the non-inverting input terminal + of the second comparator element Cmp2. The output terminal of the second comparator element Cmp2 is connected to a node between the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub>.

The second comparator element Cmp2 constantly monitors the voltage at the node between the resistor elements R2 and R3 (first divided resistor element R3<sub>A</sub>) of the comparison voltage divider circuit. When the temperature of subject airflow is lower than 30° C. and the resistance value of the second negative-temperature-coefficient thermistor element 32 is 8.3 kΩ or higher and when the voltage at the above-described node is about 1.3 V or higher, the second comparator element Cmp2 is turned OFF. Conversely, when the temperature of subject airflow is 30° C. or higher and the resistance value of the second negative-temperature-coefficient thermistor element 32 is lower than 8.3 kΩ and when the voltage at the above-described node is lower than about 1.3 V, the second comparator element Cmp2 is turned ON so as to short-circuit the node between the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub> and connect the node to a ground.

Strictly speaking, the voltage at the node between the resistor elements R2 and R3 (first divided resistor element R3<sub>A</sub>) of the comparison voltage divider circuit varies between when the second comparator element Cmp2 is ON and the second divided resistor element R3<sub>B</sub> is inserted in the comparison voltage divider circuit and when the second comparator element Cmp2 is OFF and the second divided resistor element R3<sub>B</sub> is not inserted in the comparison voltage divider circuit. However, the resistance value of the second divided resistor element R3<sub>B</sub> is as small as 390Ω, and the above-described variation can safely be ignored as the allowance.

In the airflow velocity measuring apparatus 300, as well as in the airflow velocity measuring apparatuses 100 and 200, measurement errors in the airflow velocity caused by a change in the airflow temperature can suitably be corrected over a wide temperature range.

The airflow velocity measuring apparatuses 100, 200, and 300 of the first through third embodiments have been discussed above. However, the present invention is not restricted to the above-described content, and various modifications may be made without departing from the scope and spirit of the invention.

For example, in the airflow velocity measuring apparatuses 100, 200, and 300, the resistor element R3 is divided into two resistor elements, that is, the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub>. However, the resistor element R3 may be divided into three or more elements, and the divided resistor elements may selectively be used by using a switch.

In the airflow velocity measuring apparatuses 100, 200, and 300, the preset temperature of the fixed-temperature heat generating device 10 is about 35° C. However, as the preset temperature of the fixed-temperature heat generating device 10, any desirable temperature may be set and be changed.

In the airflow velocity measuring apparatuses 100, 200, and 300, to correct measurement errors in the airflow velocity caused by a change in the airflow temperature, the low temperature mode and the high temperature mode are selectively used in accordance with whether the airflow temperature is lower than 30° C. or higher than or equal to

30° C. However, any desirable temperature may be set for switching between the low temperature mode and the high temperature mode.

The resistance values of the resistor elements R1, R2, and R3 and the first and second divided resistor elements R3<sub>A</sub> and R3<sub>B</sub> and the resistance-temperature characteristics of the first and second negative-temperature-coefficient thermistor elements 21 and 32 may also be desirably set.

An airflow rate measuring apparatus may be formed by using any of the airflow velocity measuring apparatuses 100, 200, and 300.

#### REFERENCE SIGNS LIST

- 10 fixed-temperature heat generating device
- 20 heating unit
- 30 temperature controller
- 21 first negative-temperature-coefficient thermistor element
- 22 positive-temperature-coefficient thermistor element (heating element)
- 32 second negative-temperature-coefficient thermistor element
- SW1 (first) switch
- SW2 second switch
- Q1 (first) switching element
- Q2 second switching element
- Cmp1 (first) comparator element
- Cmp2 second comparator element
- 40 pulse voltage monitor
- 50 microcomputer
- 100, 200, 300 airflow velocity measuring apparatus

The invention claimed is:

1. An airflow velocity measuring apparatus comprising:
  - a fixed-temperature heat generating device that generates heat at a preset temperature, the fixed-temperature heat generating device including:
    - a power supply;
    - a heating element that generates heat when receiving power from the power supply, the heating element disposed at a measuring point at which a velocity of airflow is to be measured;
    - a switching element between the power supply and the heating element;
    - a first negative-temperature-coefficient thermistor element thermally coupled with the heating element, wherein a resistance value of the first negative-temperature-coefficient thermistor element at the preset temperature is a threshold resistance value;
    - a first resistor element connected in series with the first negative-temperature-coefficient thermistor element so as to form a temperature-detecting voltage divider circuit, wherein a temperature-detecting voltage is output from a node between the first negative-temperature-coefficient thermistor element and the first resistor element of the temperature-detecting voltage divider circuit;
    - a second resistor element, a first divided resistor element, a second divided resistor element, and a second negative-temperature-coefficient thermistor element connected in series with each other so as to form a comparison voltage divider circuit, wherein a comparison voltage is output from a node between the second resistor element and the first divided resistor element of the comparison voltage divider circuit;
    - a comparator element that compares the temperature-detecting voltage and the comparison voltage with each



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other and turns ON or OFF the switching element in accordance with a comparison result, wherein, as a result of the switching element being repeatedly turned ON and OFF, a pulse voltage is applied from the power supply to the heating element; and

a switch that switches between a first state in which both the first and second divided resistor elements are connected to the comparison voltage divider circuit and a second state in which only one of the first and second divided resistor elements is connected to the comparison voltage divider circuit in accordance with the velocity of airflow at the measuring point based on a waveform of the applied pulse voltage.

2. The airflow velocity measuring apparatus according to claim 1, wherein:

a resistance value of the first resistor element of the temperature-detecting voltage divider circuit, resistance values of at least two of the second resistor element, the first divided resistor element, the second divided resistor element of the comparison voltage divider circuit, and a fixed voltage applied to each of the temperature-detecting voltage divider circuit and the comparison voltage divider circuit are set so that a temperature-detecting voltage and a comparison voltage become equal to each other when the temperature of the first negative-temperature-coefficient thermistor element is the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is the threshold resistance value,

when the temperature of the first negative-temperature-coefficient thermistor element is lower than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is greater than the threshold resistance value, the temperature-detecting voltage is greater than the comparison voltage, and when the temperature of the first negative-temperature-coefficient thermistor element is higher than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is smaller than the threshold resistance value, the temperature-detecting voltage is smaller than the comparison voltage, or when the temperature of the first negative-temperature-coefficient thermistor element is lower than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is greater than the threshold resistance value, the temperature-detecting voltage is smaller than the comparison voltage, and when the temperature of the first negative-temperature-coefficient thermistor element is higher than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is smaller than the threshold resistance value, the temperature-detecting voltage is greater than the comparison voltage,

the comparator element compares the temperature-detecting voltage and the comparison voltage with each other, and when the temperature of the first negative-temperature-coefficient thermistor element is lower than the preset temperature and when the resistance value of the

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first negative-temperature-coefficient thermistor element is greater than the threshold resistance value, the comparator element turns ON the switching element, and when the temperature of the first negative-temperature-coefficient thermistor element is higher than the preset temperature and when the resistance value of the first negative-temperature-coefficient thermistor element is smaller than the threshold resistance value, the comparator element turns OFF the switching element, and

the switch switches between the first and second states in response to the temperature of airflow passing through the measuring point.

3. The airflow velocity measuring apparatus according to claim 2, further comprising a microcomputer configured to receive an indication of the temperature of the airflow passing through the measuring point, and control the switch to switch between the first and second states.

4. The airflow velocity measuring apparatus according to claim 2, wherein the switch is configured so as to switch between the first and second states in response to a resistance value of the second negative-temperature-coefficient thermistor element, the resistance value being changed by the temperature of the airflow passing through the measuring point.

5. The airflow velocity measuring apparatus according to claim 1, further comprising a microcomputer configured to receive an indication of the temperature of the airflow passing through the measuring point, and control the switch to switch between the first and second states.

6. The airflow velocity measuring apparatus according to claim 1, wherein the switch is configured so as to switch between the first and second states in response to a resistance value of the second negative-temperature-coefficient thermistor element, the resistance value being changed by the temperature of the airflow passing through the measuring point.

7. The airflow velocity measuring apparatus according to claim 1, wherein the switch is connected between a ground and a node between the first and second divided resistor elements.

8. The airflow velocity measuring apparatus according to claim 1, wherein the switch is a second switching element.

9. The airflow velocity measuring apparatus according to claim 8, wherein the second switching element is disposed between a ground and a node between the first and second divided resistor elements.

10. The airflow velocity measuring apparatus according to claim 8, wherein the second switching element is an NPN transistor.

11. The airflow velocity measuring apparatus according to claim 1, wherein the comparator element is a first comparator element, and the switch is a second comparator element.

12. The airflow velocity measuring apparatus according to claim 11, wherein the second comparator element is disposed between a ground and a node between the first and second divided resistor elements.

13. An airflow rate measuring apparatus comprising the airflow velocity measuring apparatus according to claim 1.

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