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(54) SURGICAL SYSTEM COUPLEABLE WITH STAPLE CARTRIDGE AND RADIO FREQUENCY CARTRIDGE, AND HAVING A PLURALITY OF RADIO-FREQUENCY ENERGY RETURN PATHS

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See application file for complete search history.

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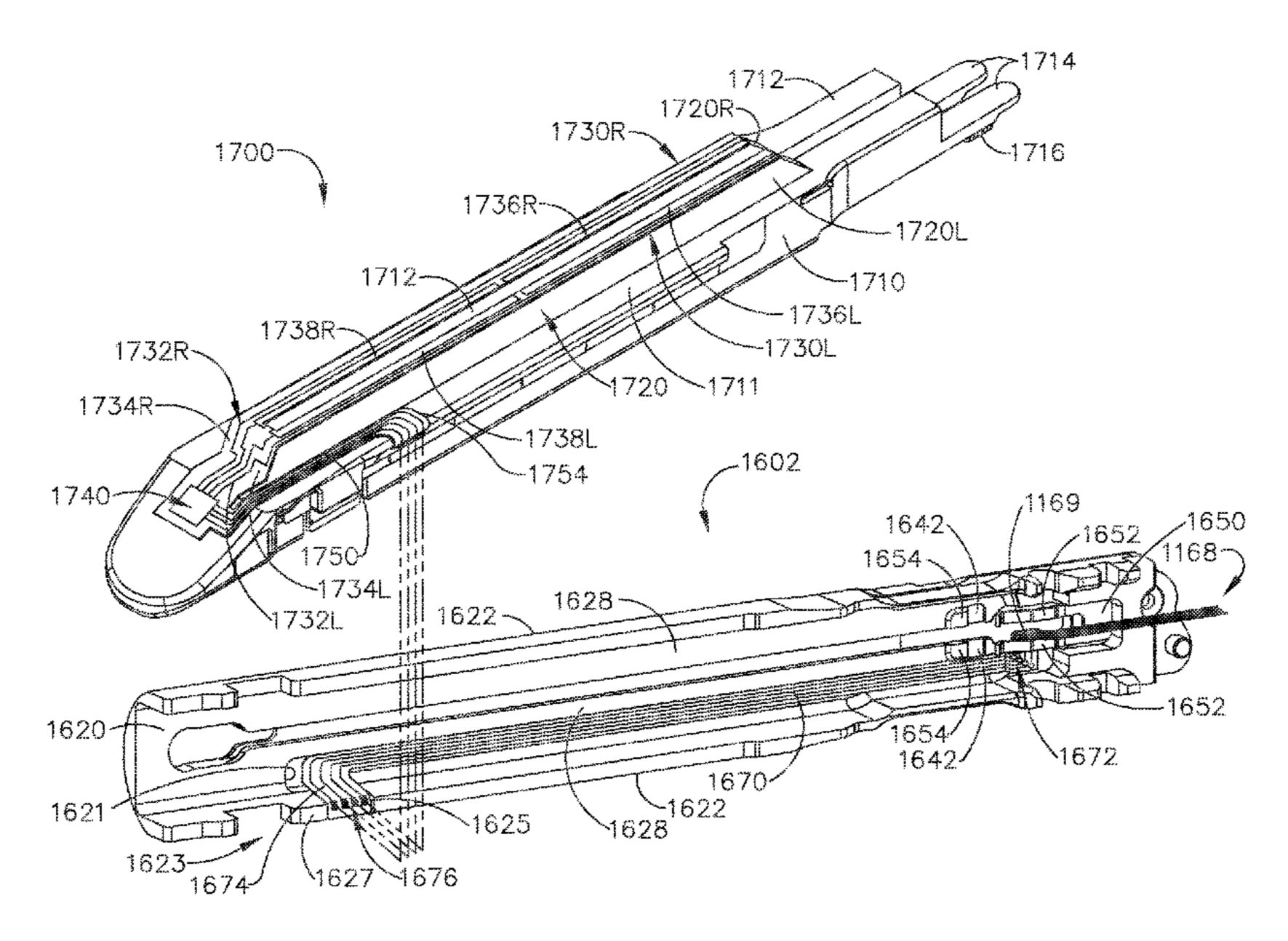
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(57) ABSTRACT

An interchangeable tool assembly is disclosed. The interchangeable tool assembly includes a first jaw configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period. A second jaw is coupled to the first jaw. A surface of the second jaw defines a plurality of staple forming pockets configured to form staples driven from the staple cartridge. An electrically insulative material covers segments of the surface of the second jaw other than the staple forming pockets. The staple forming pockets define at least one return path for radio-frequency energy delivered by the radio-frequency cartridge.

18 Claims, 21 Drawing Sheets

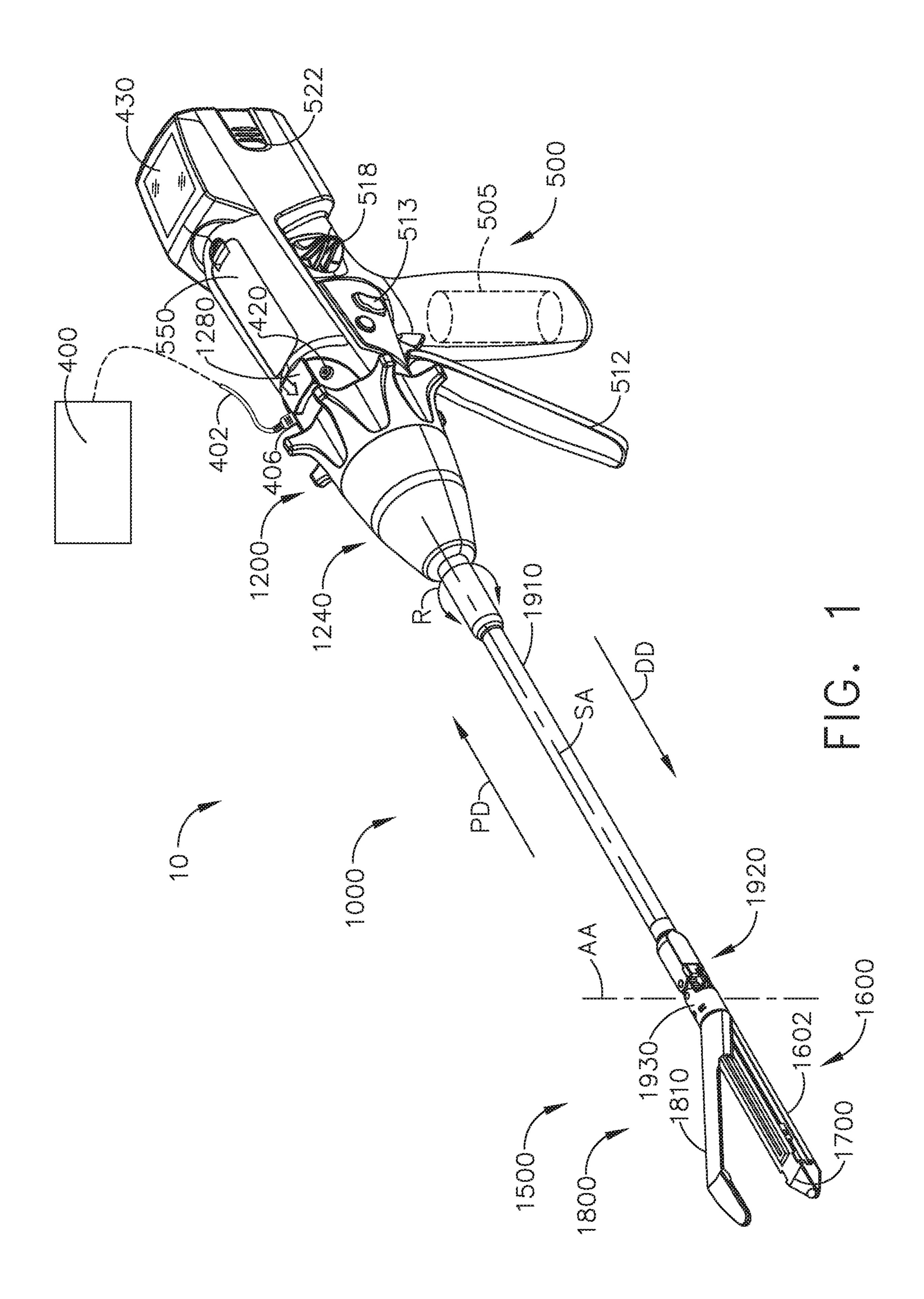


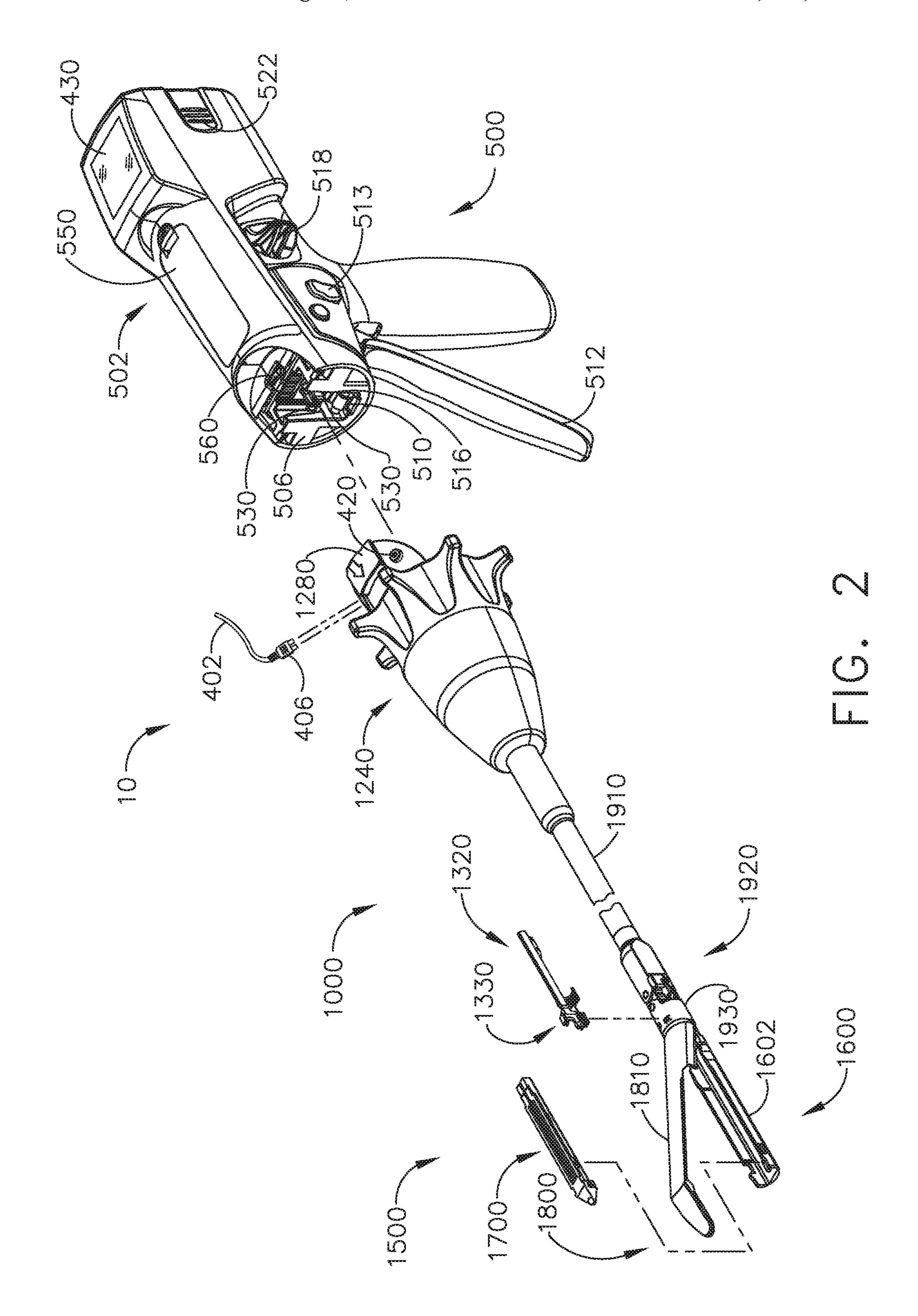
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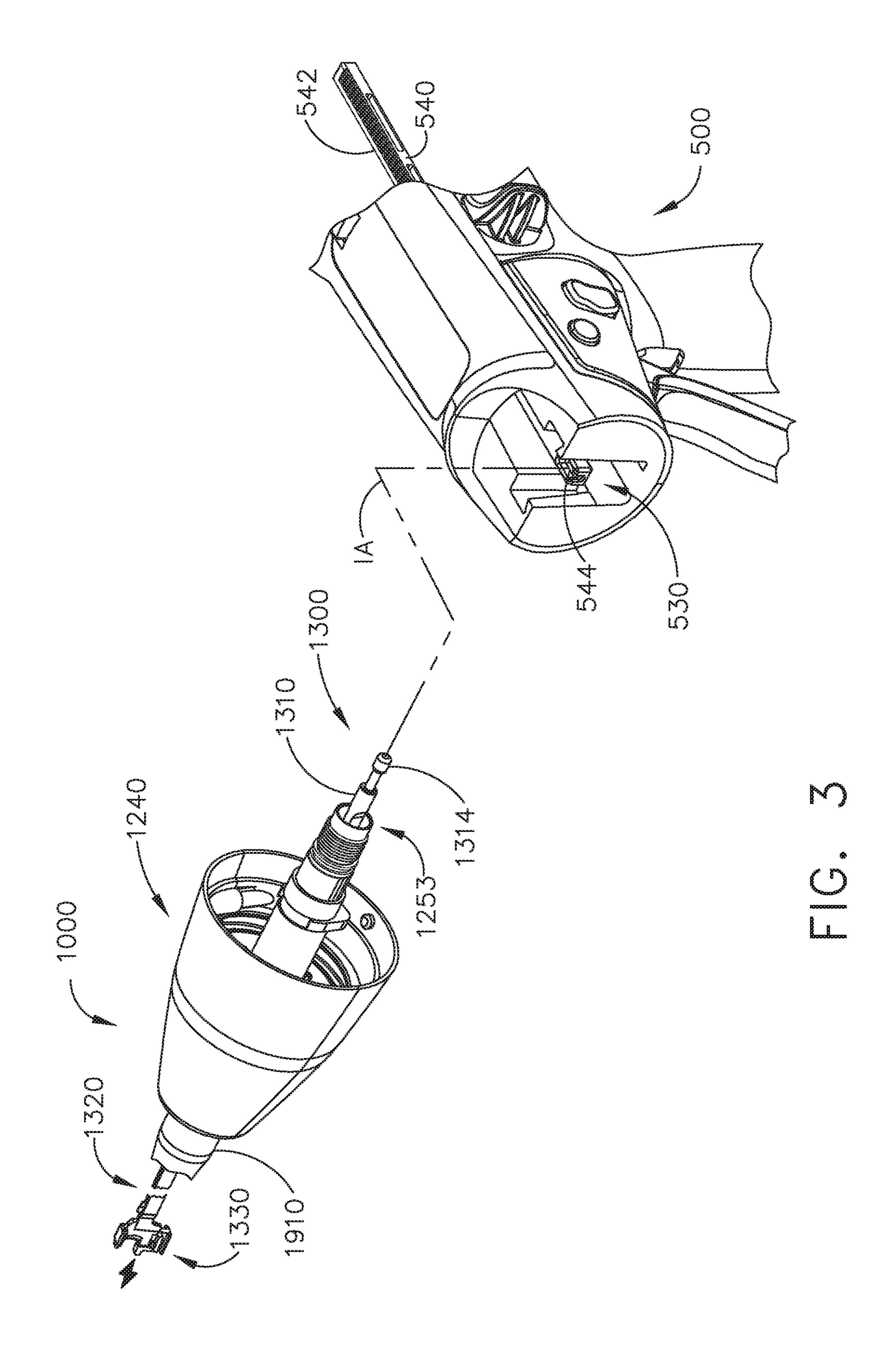
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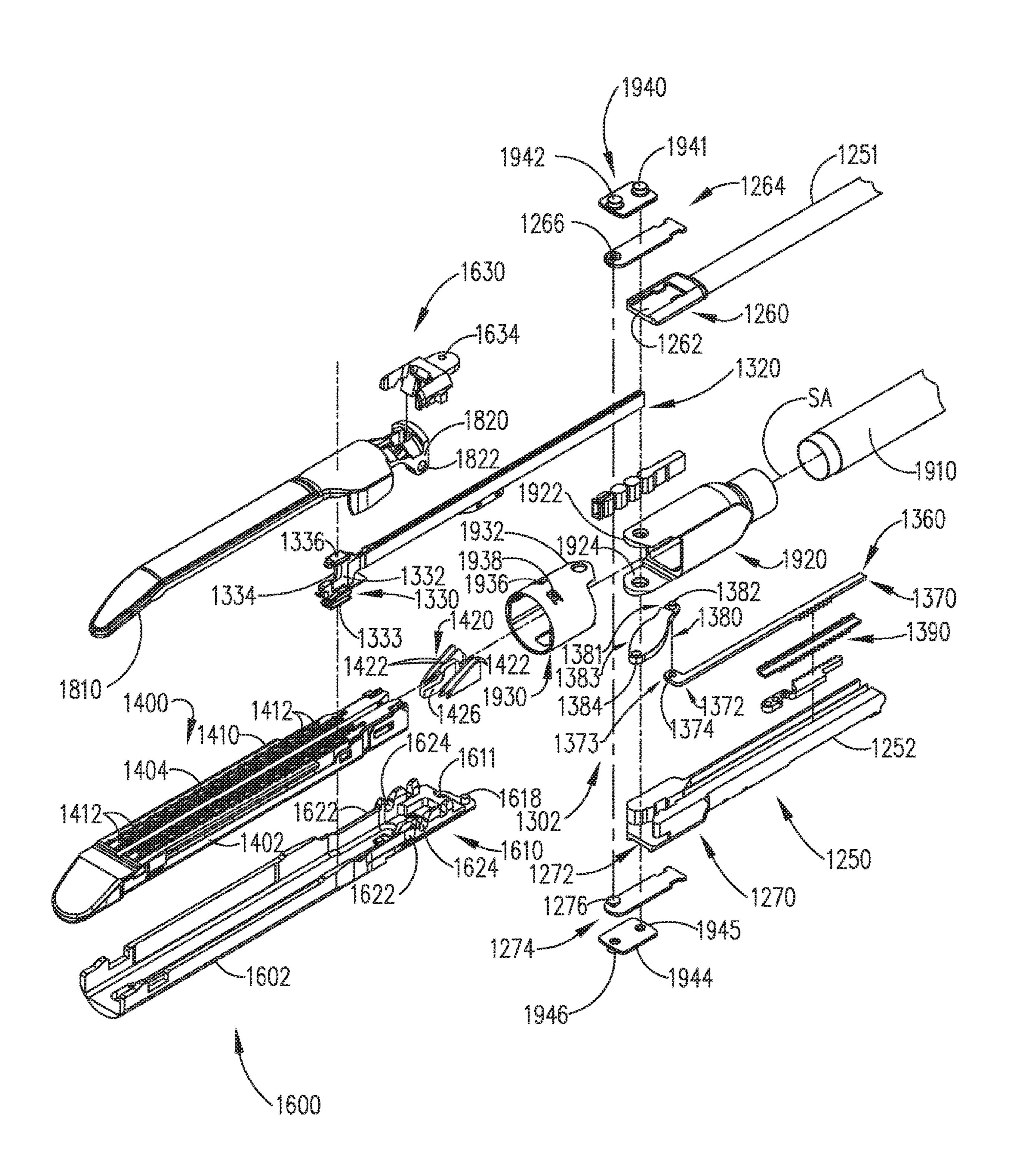


FIG. 4

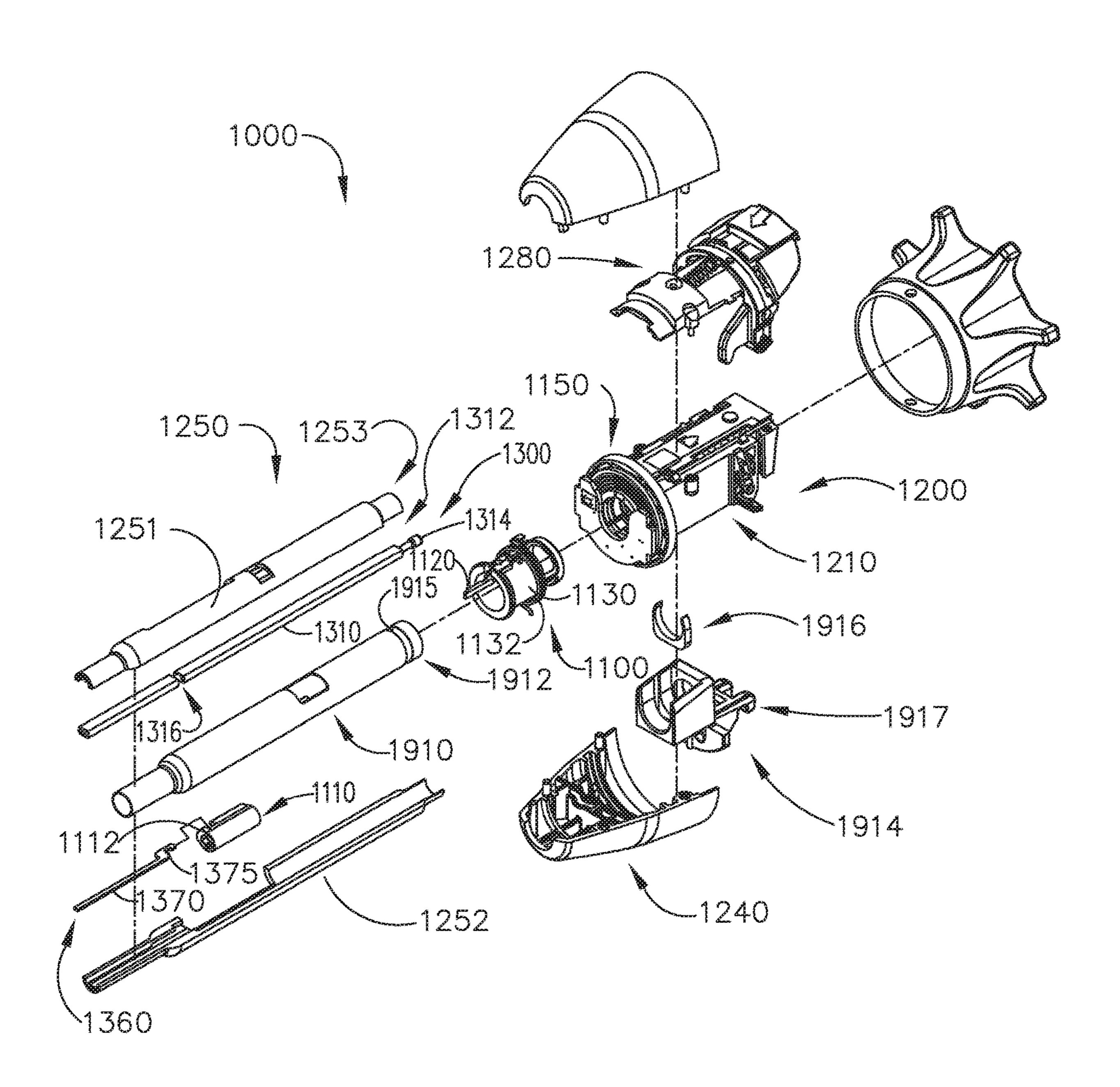
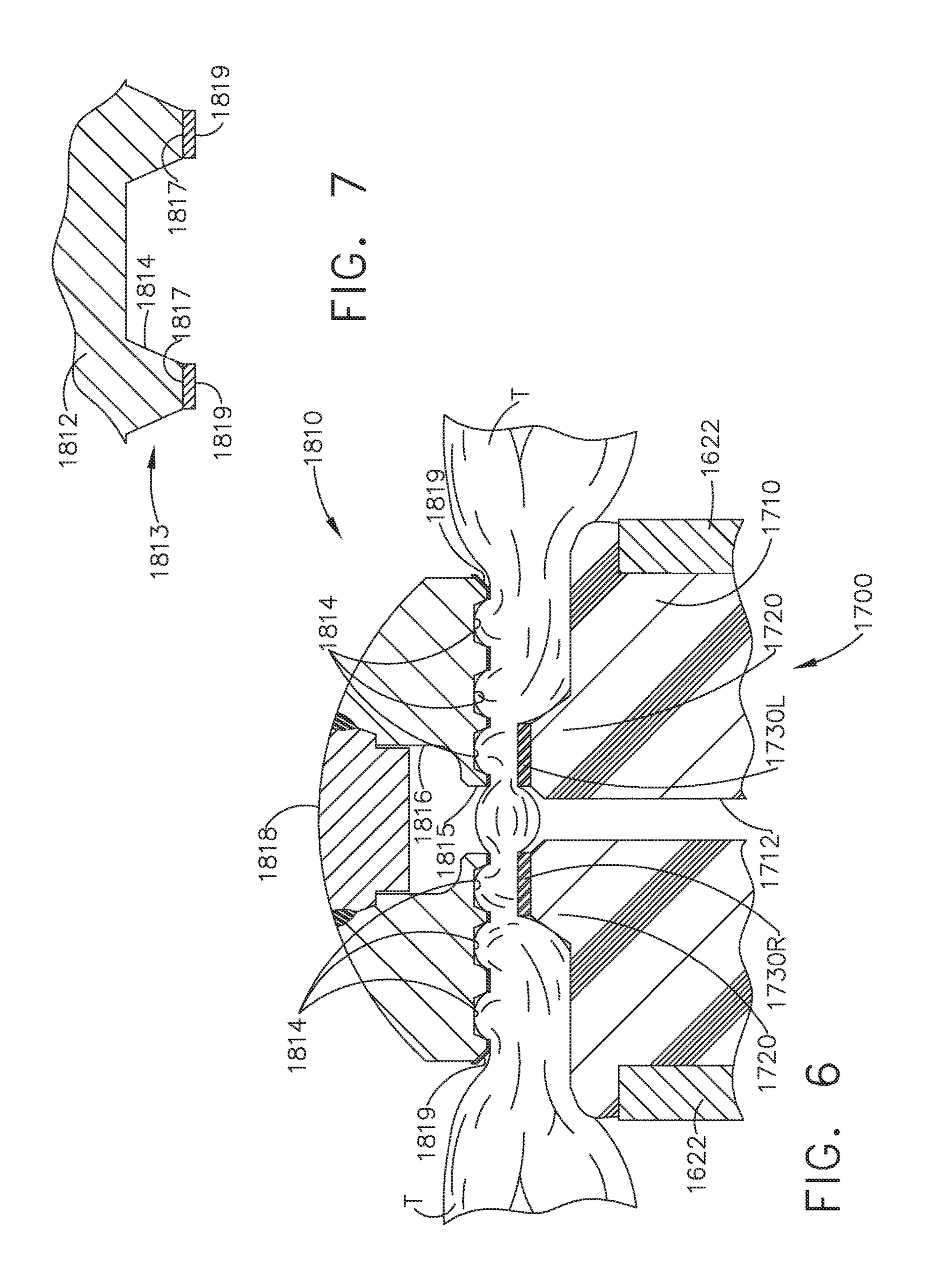
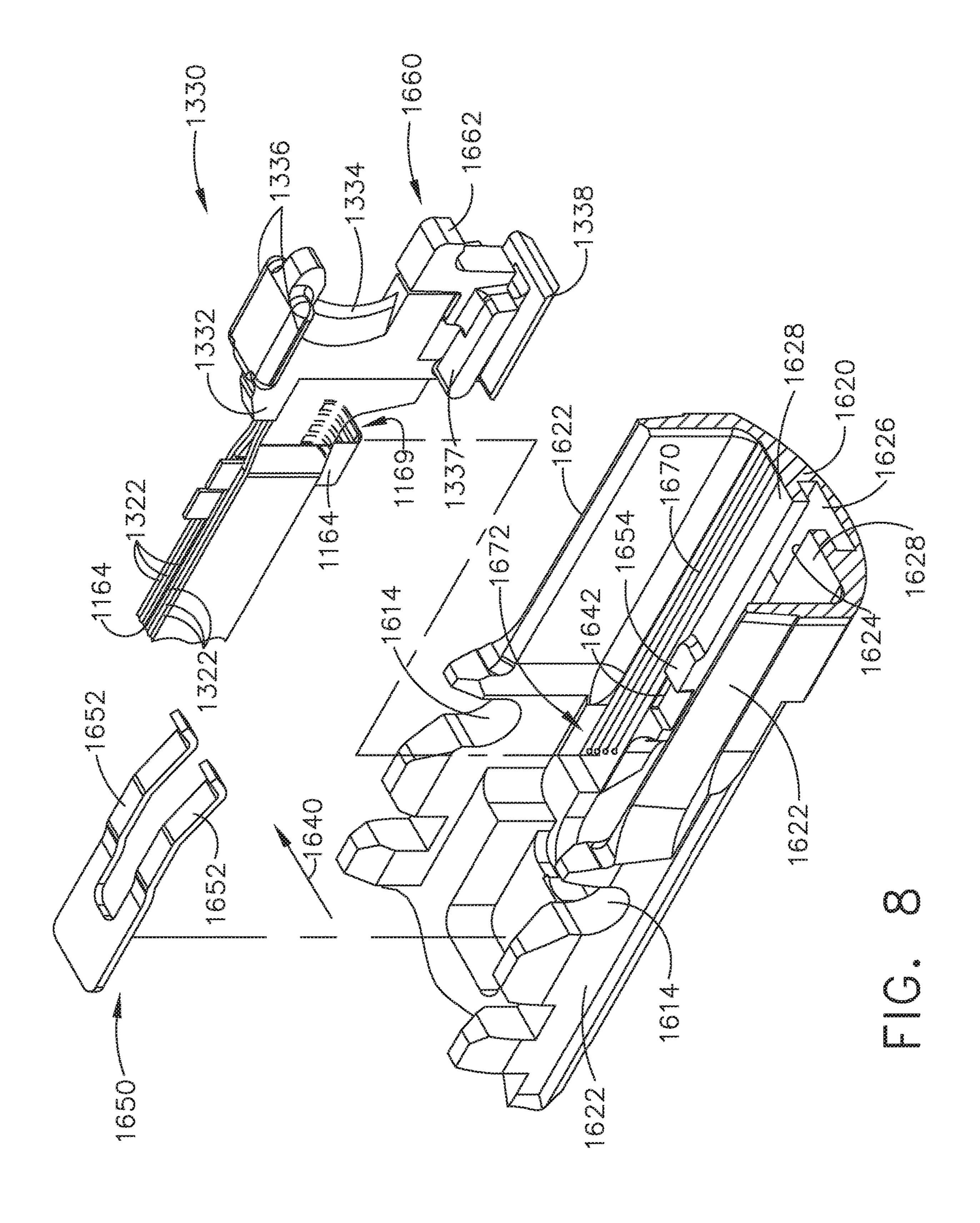
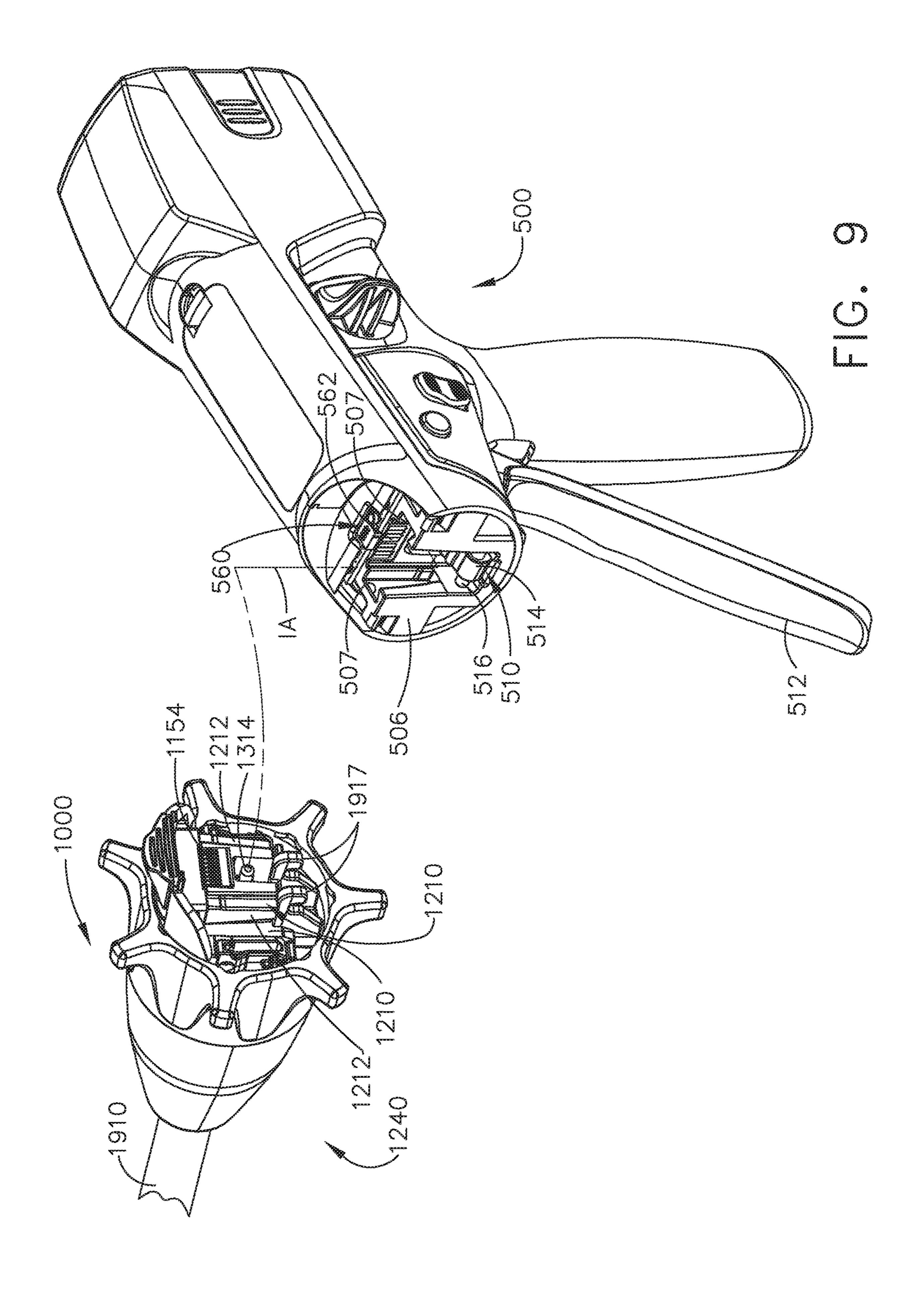
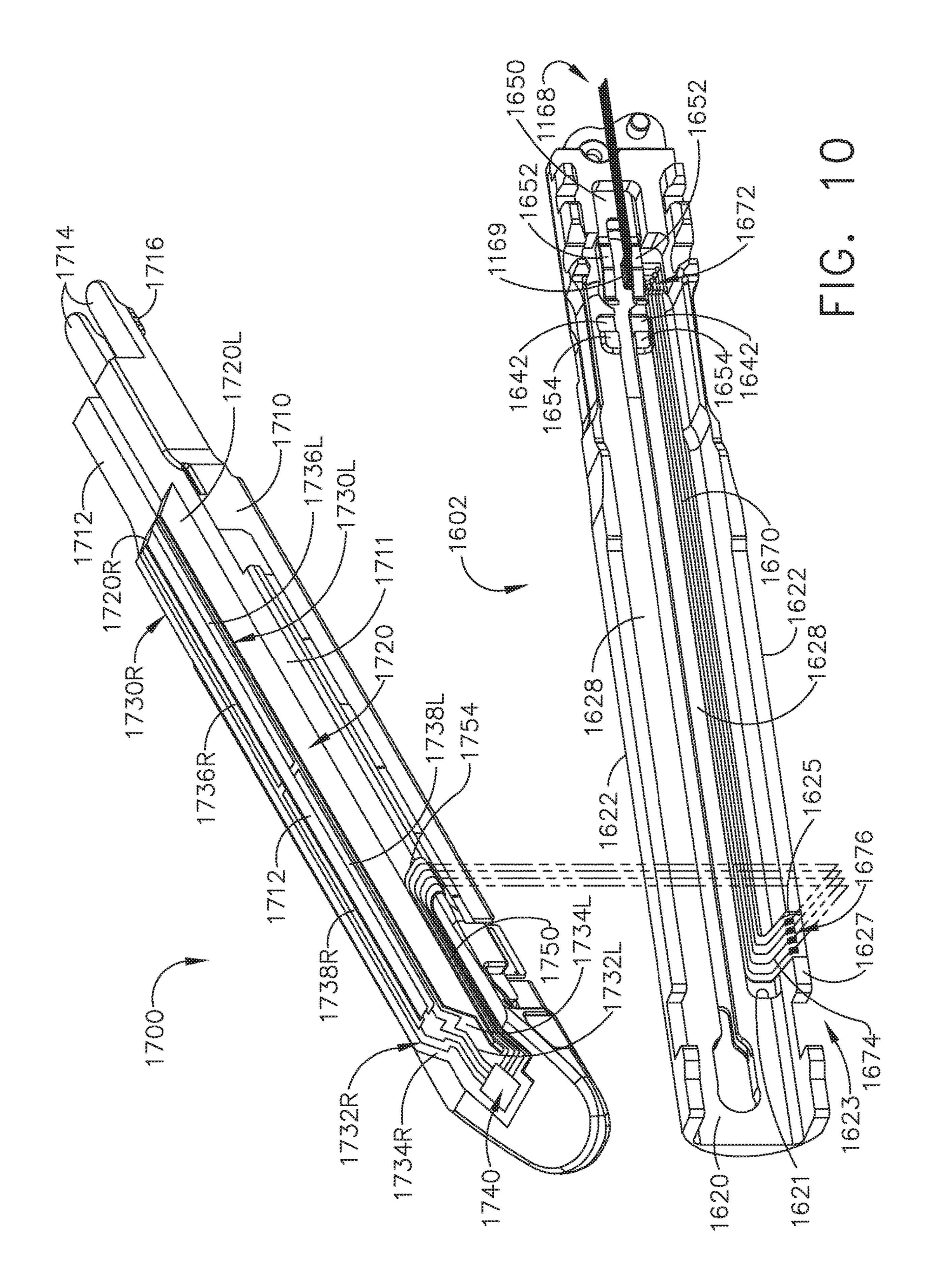


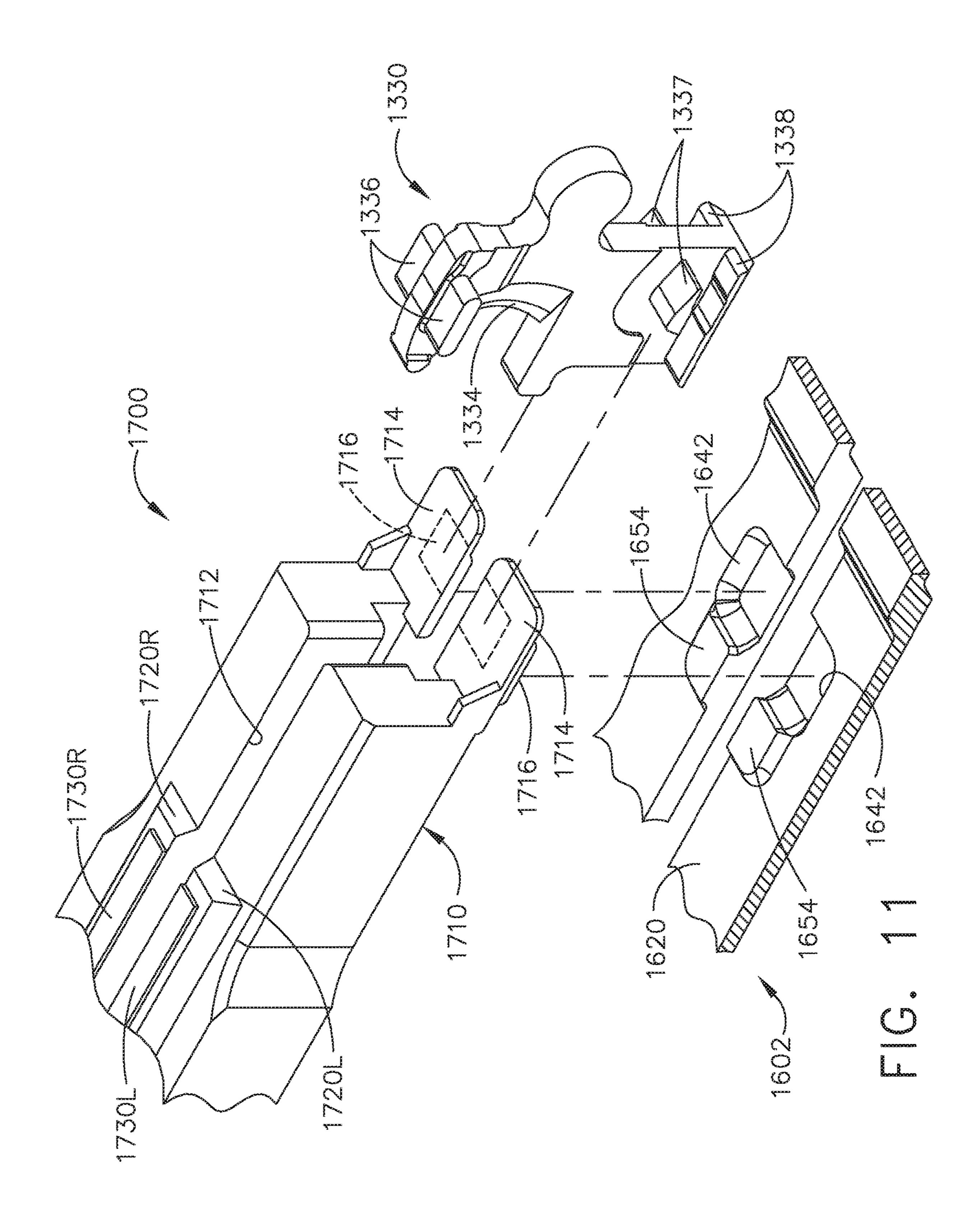
FIG. 5



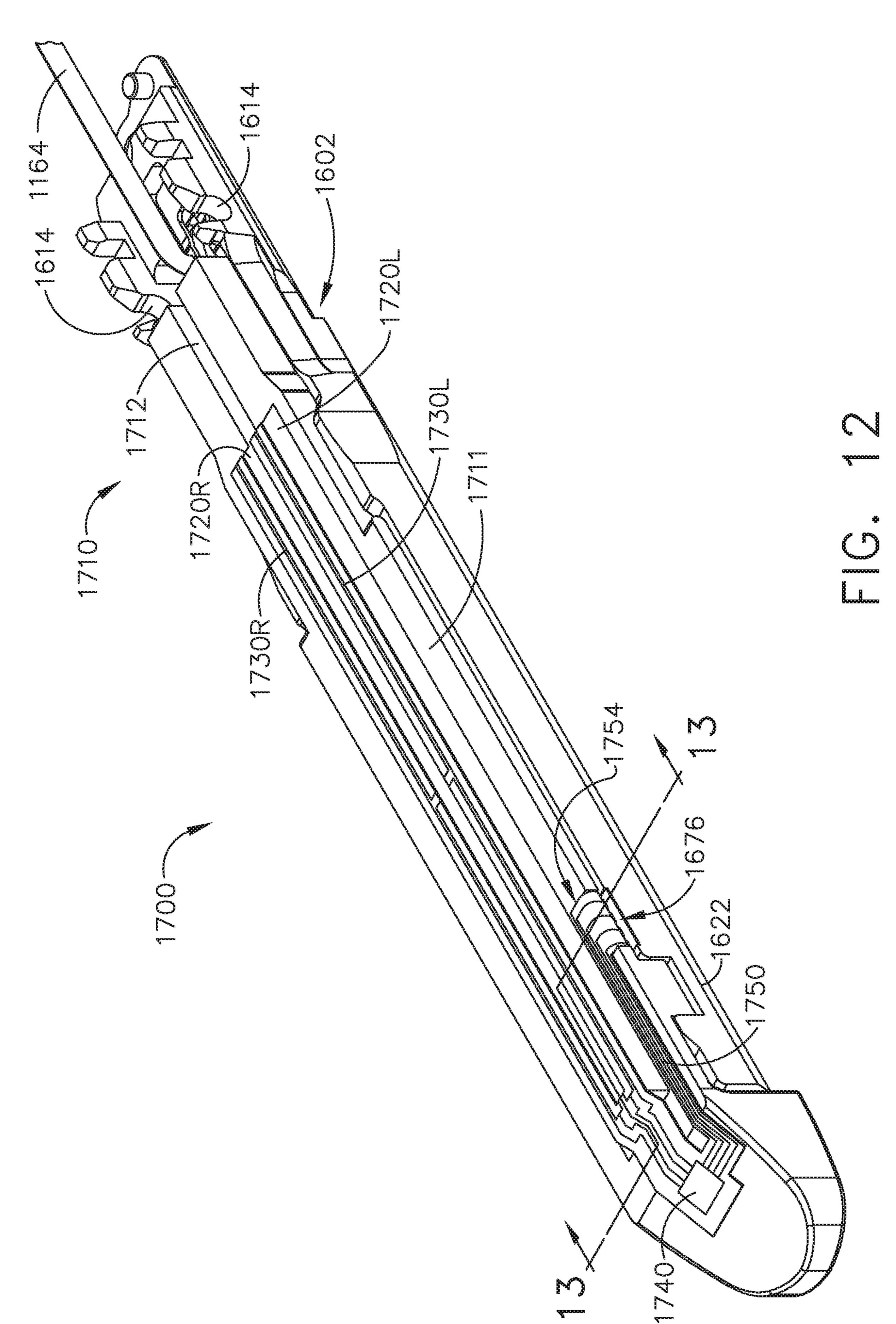


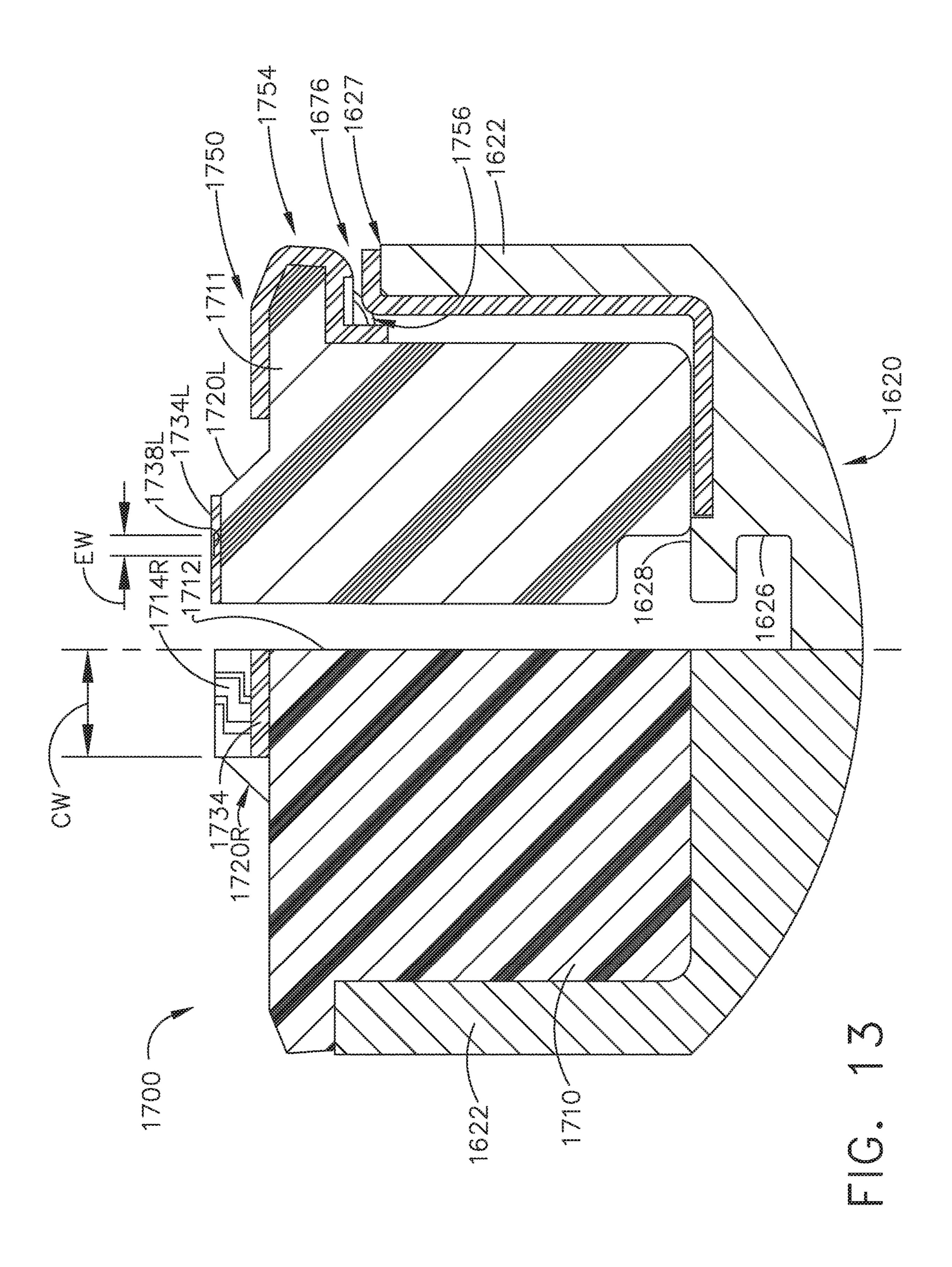


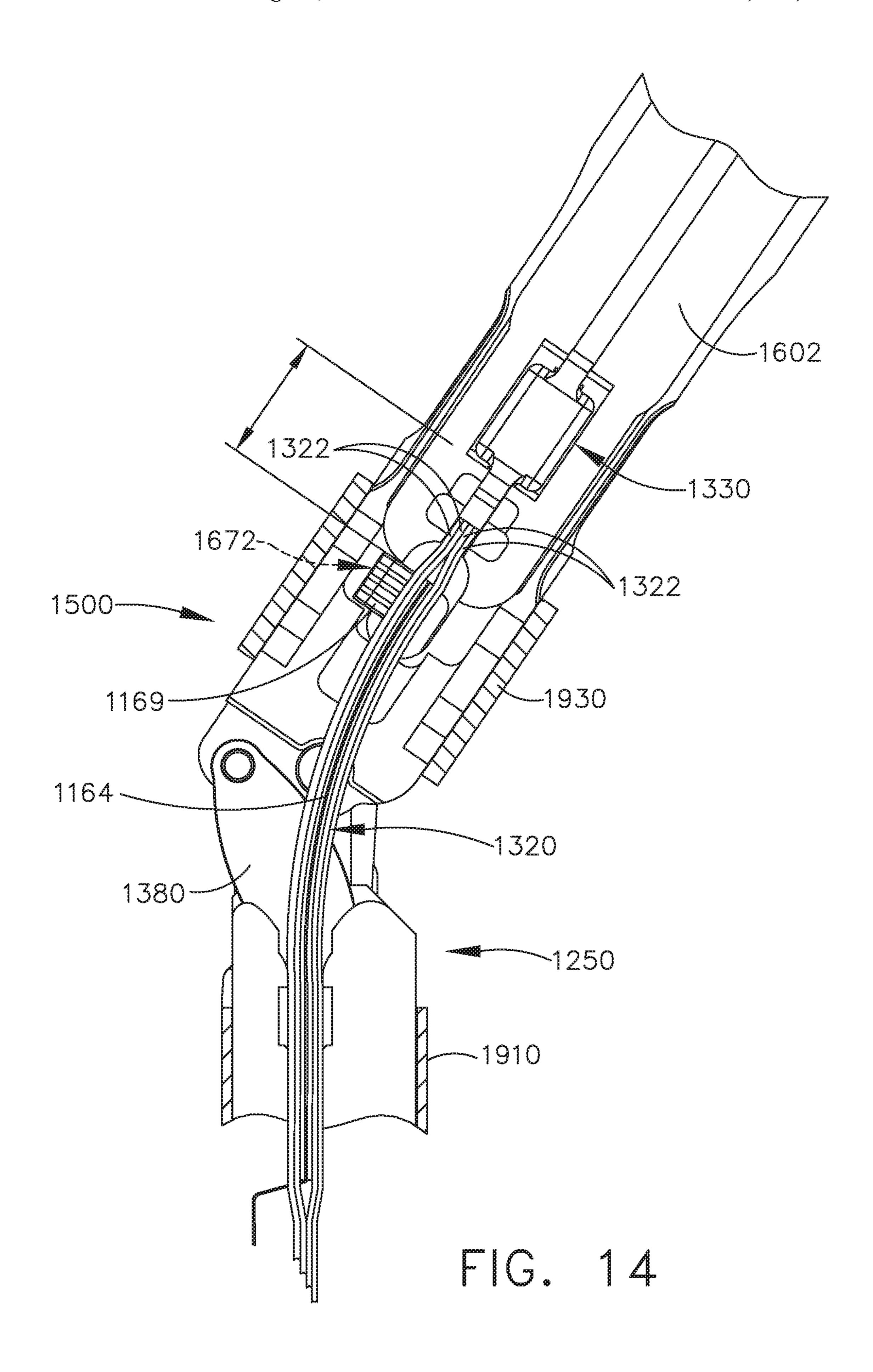


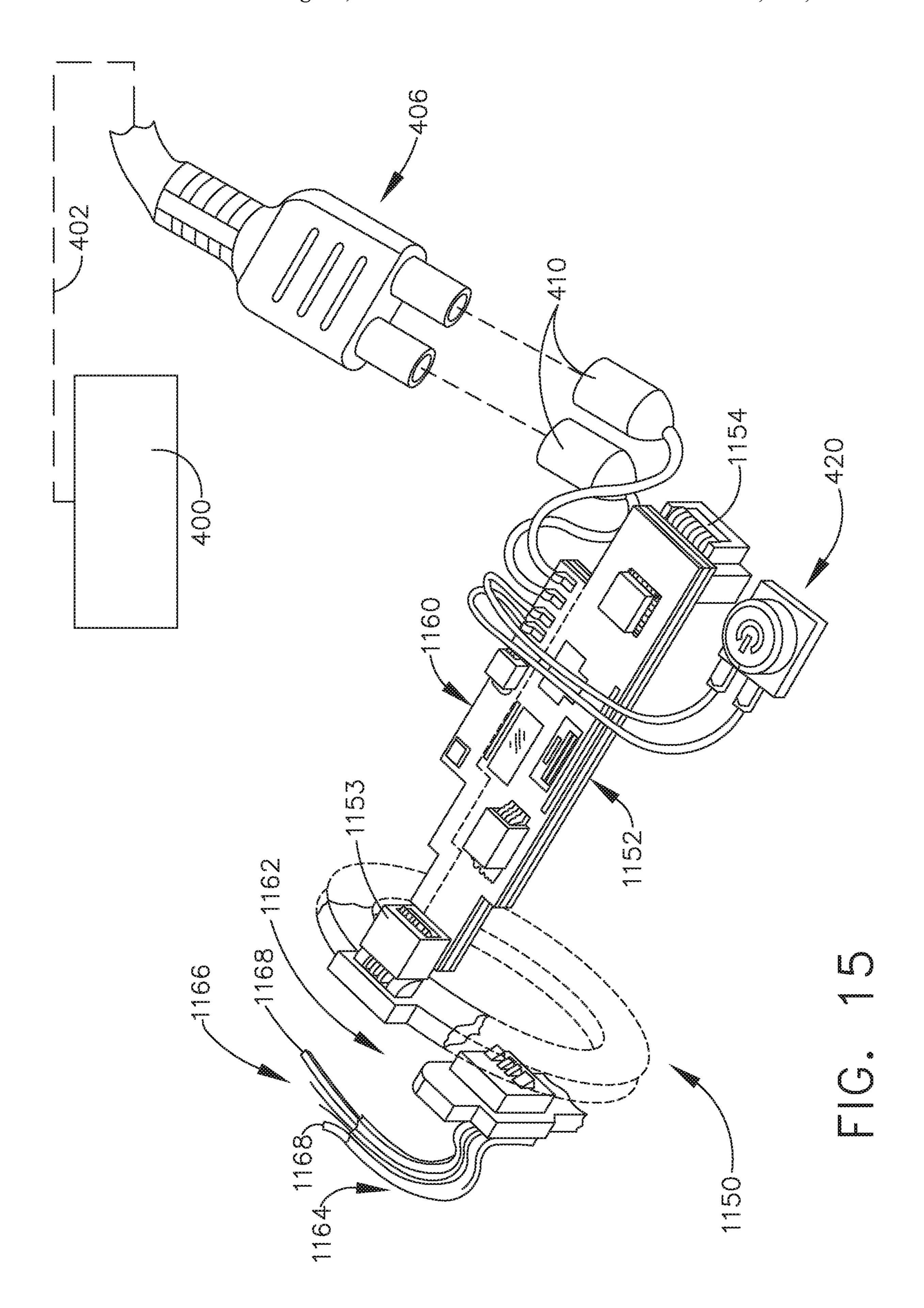


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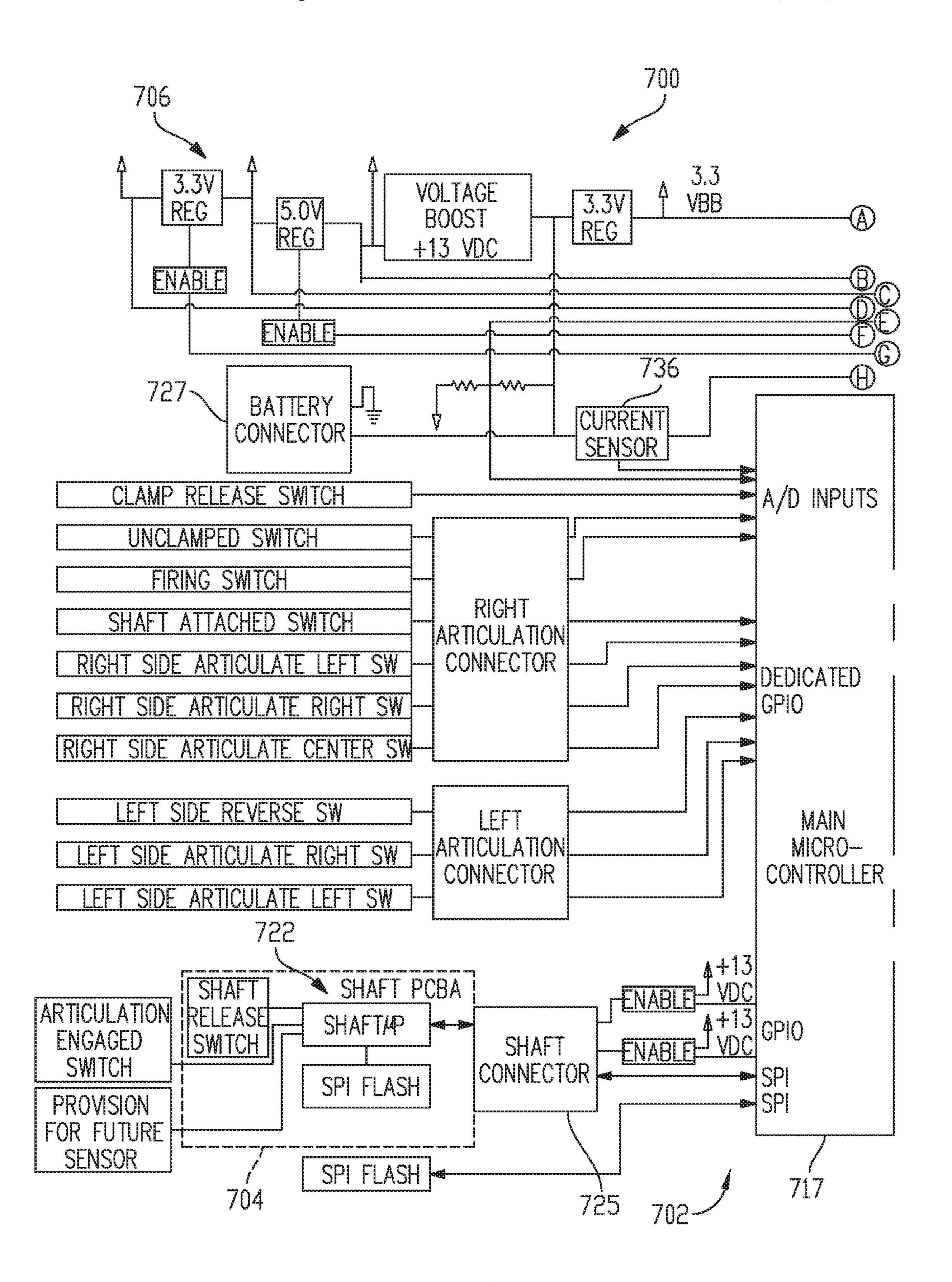


FIG. 16A

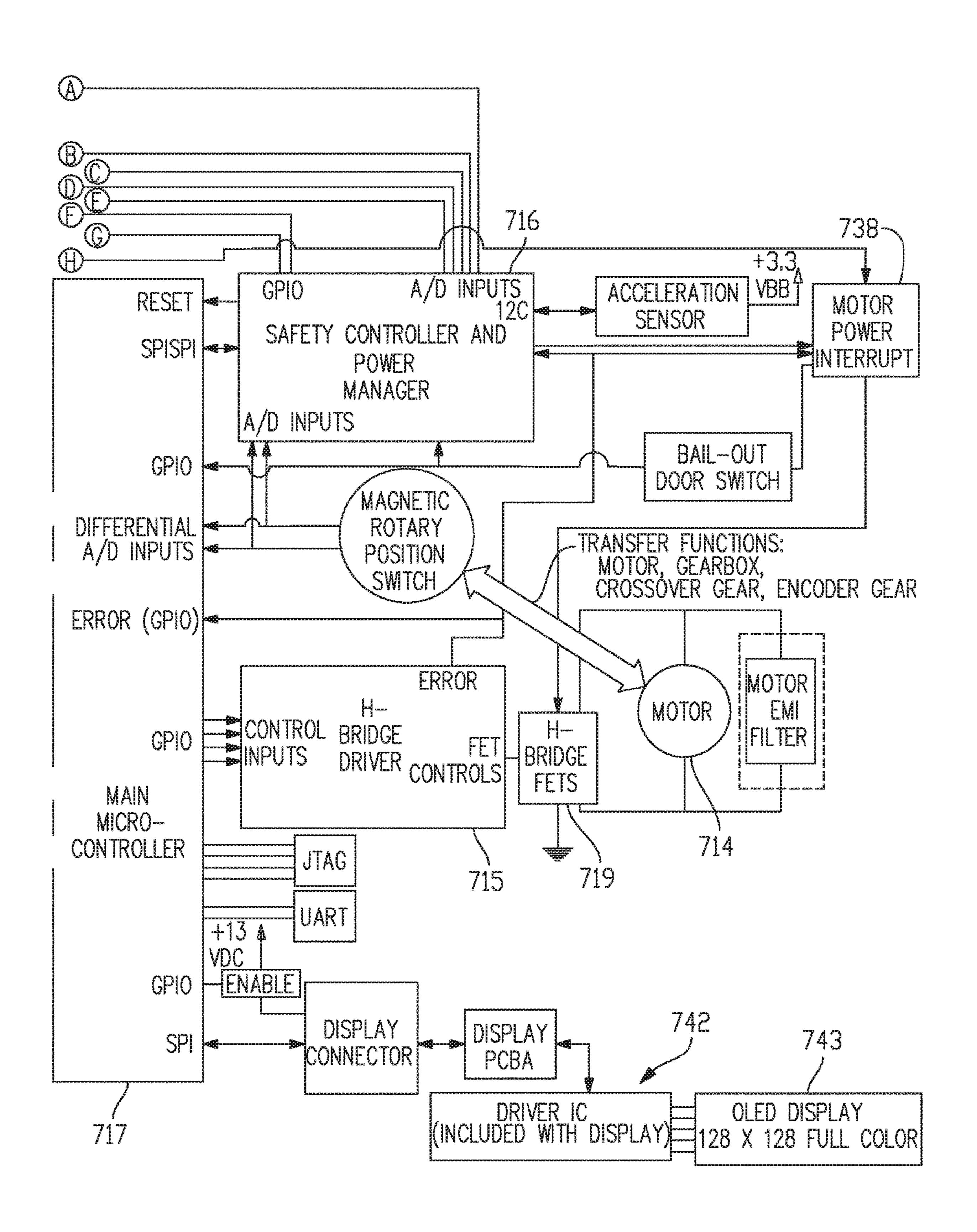
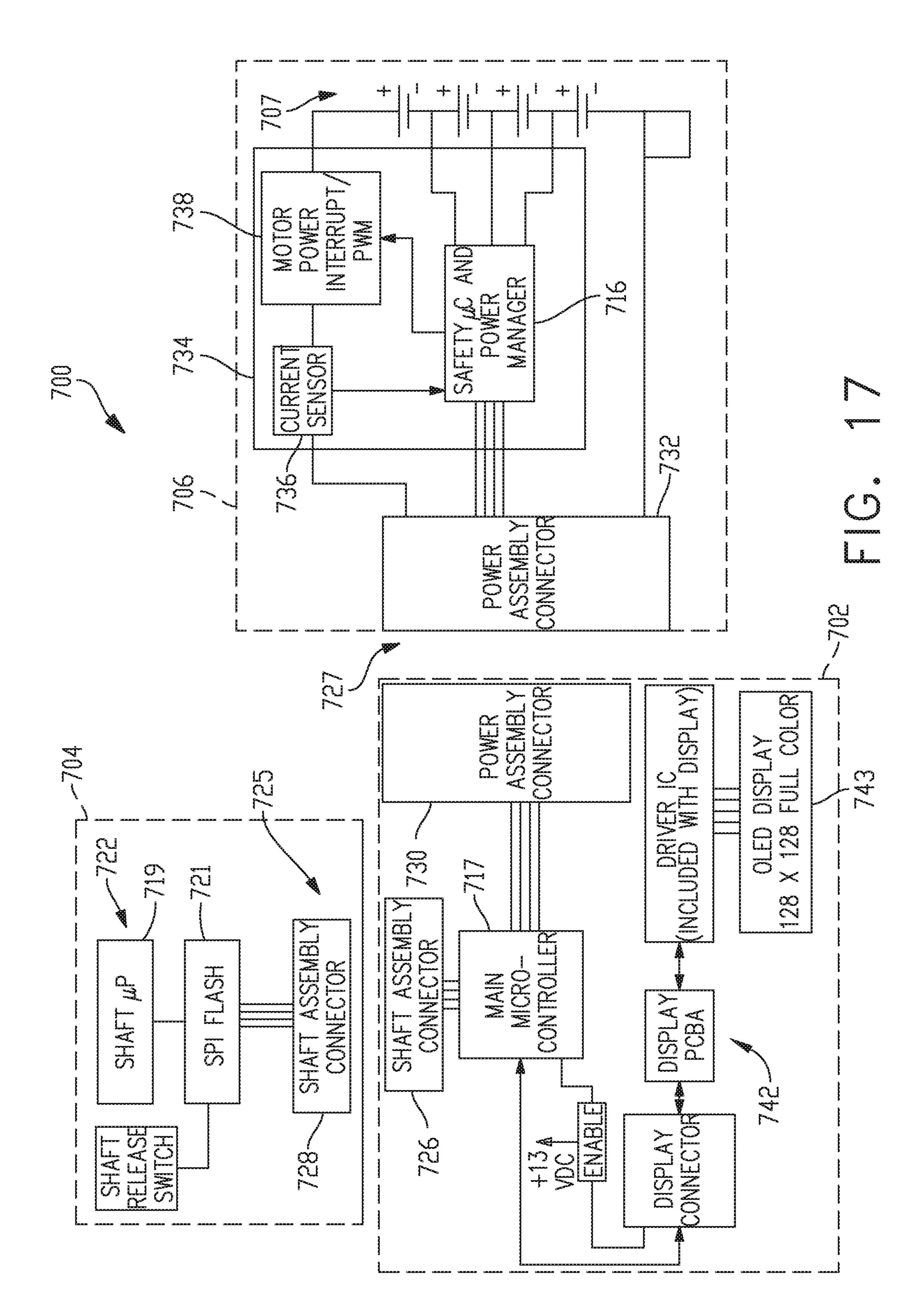
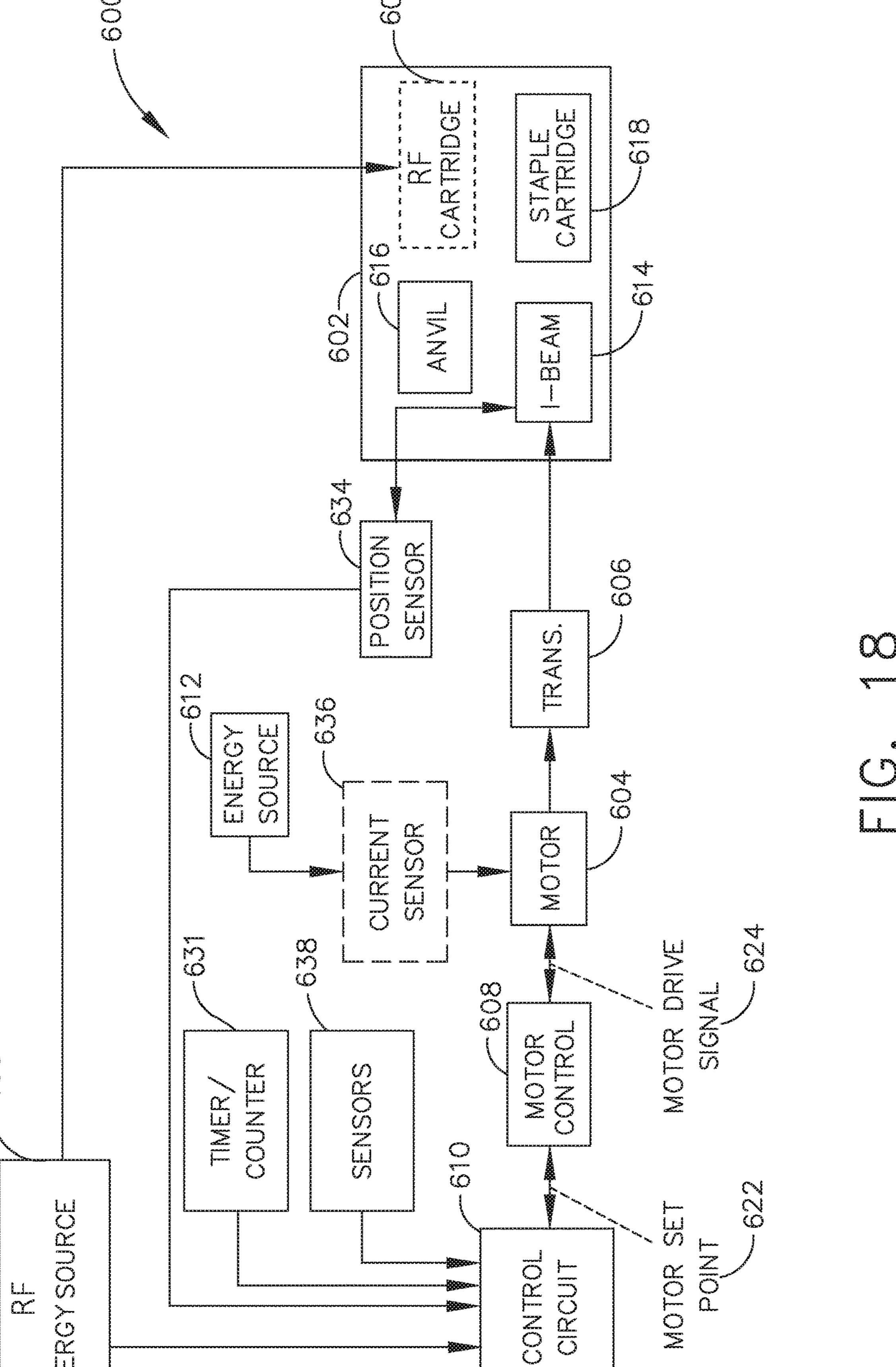
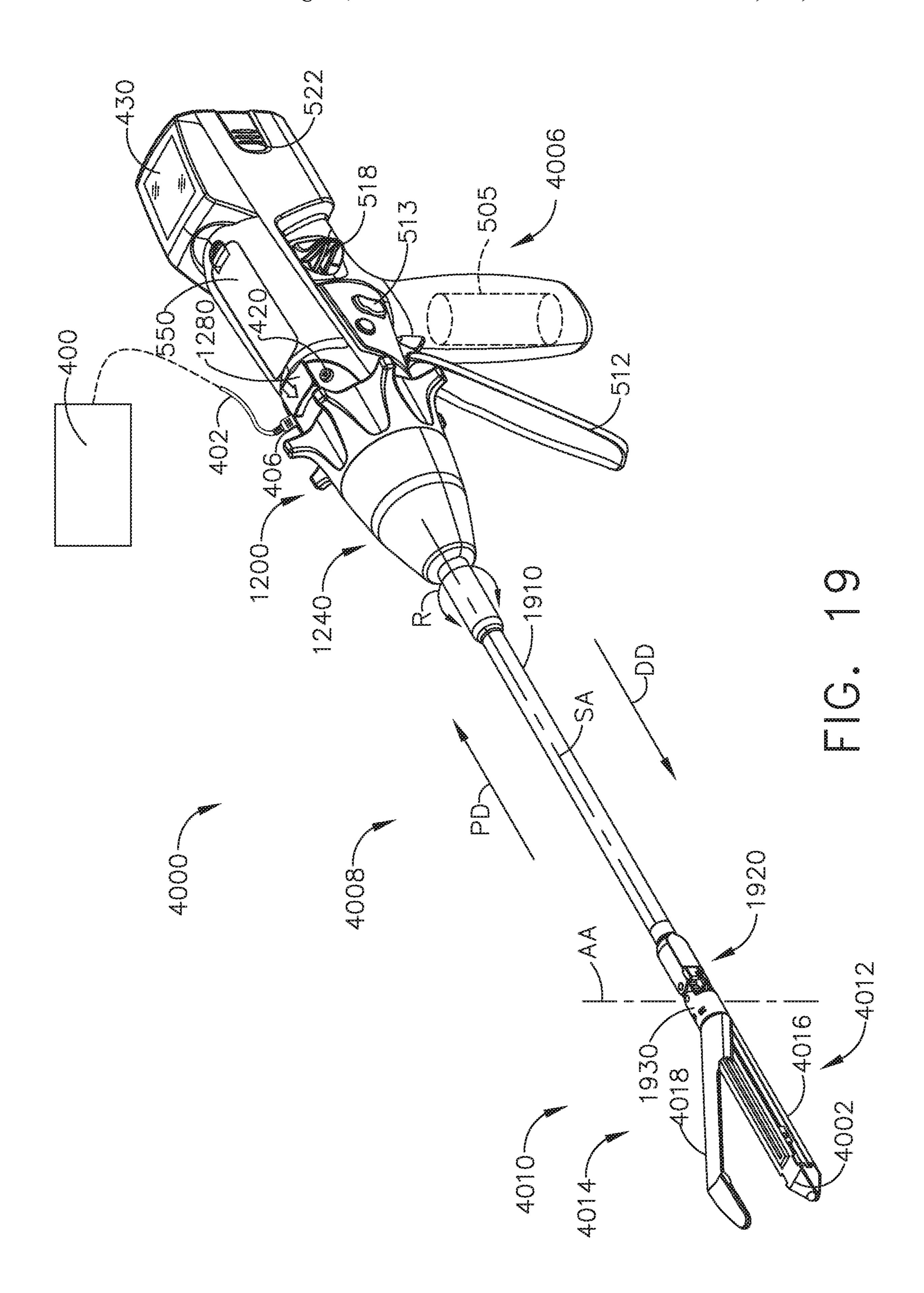
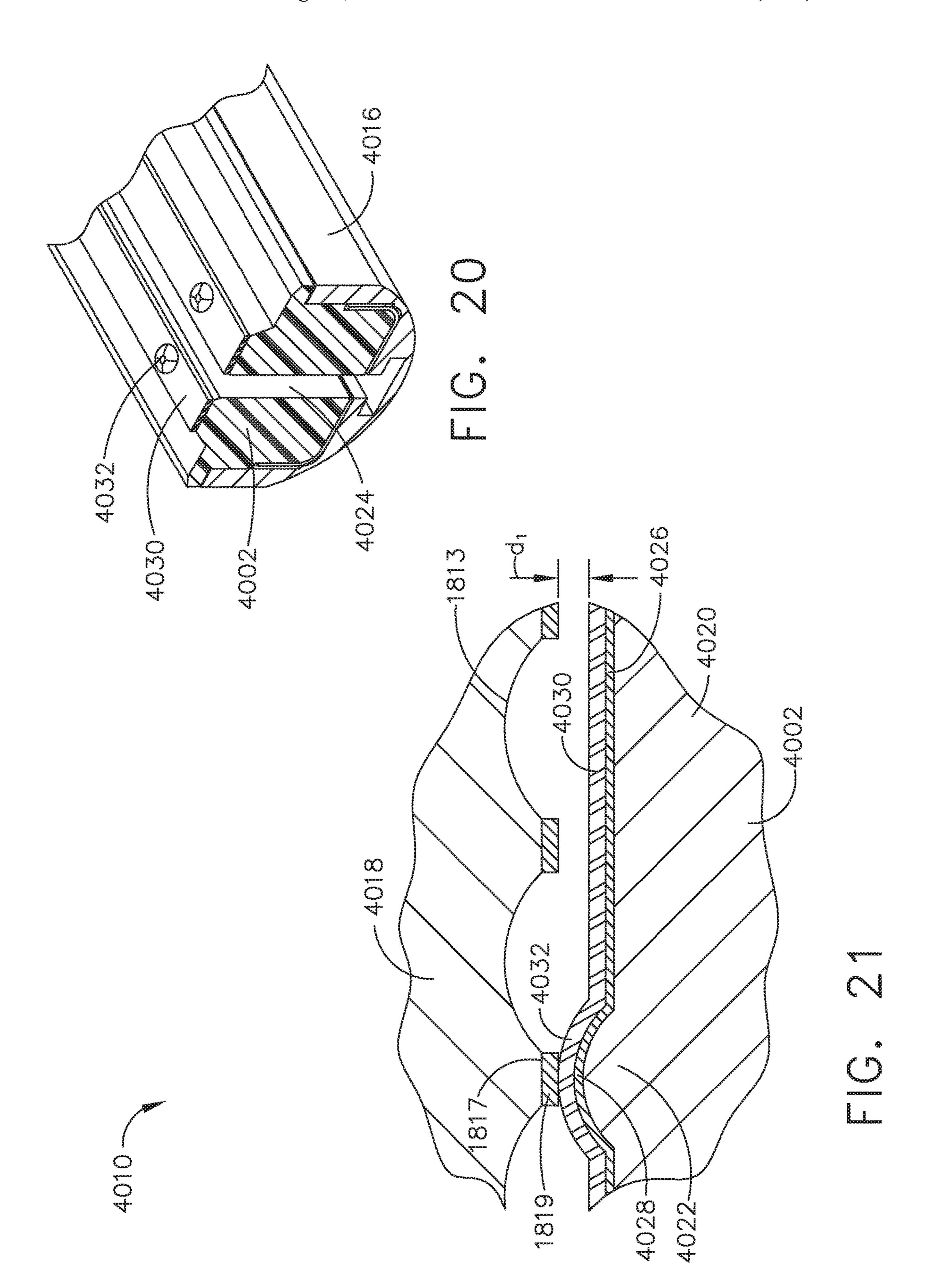


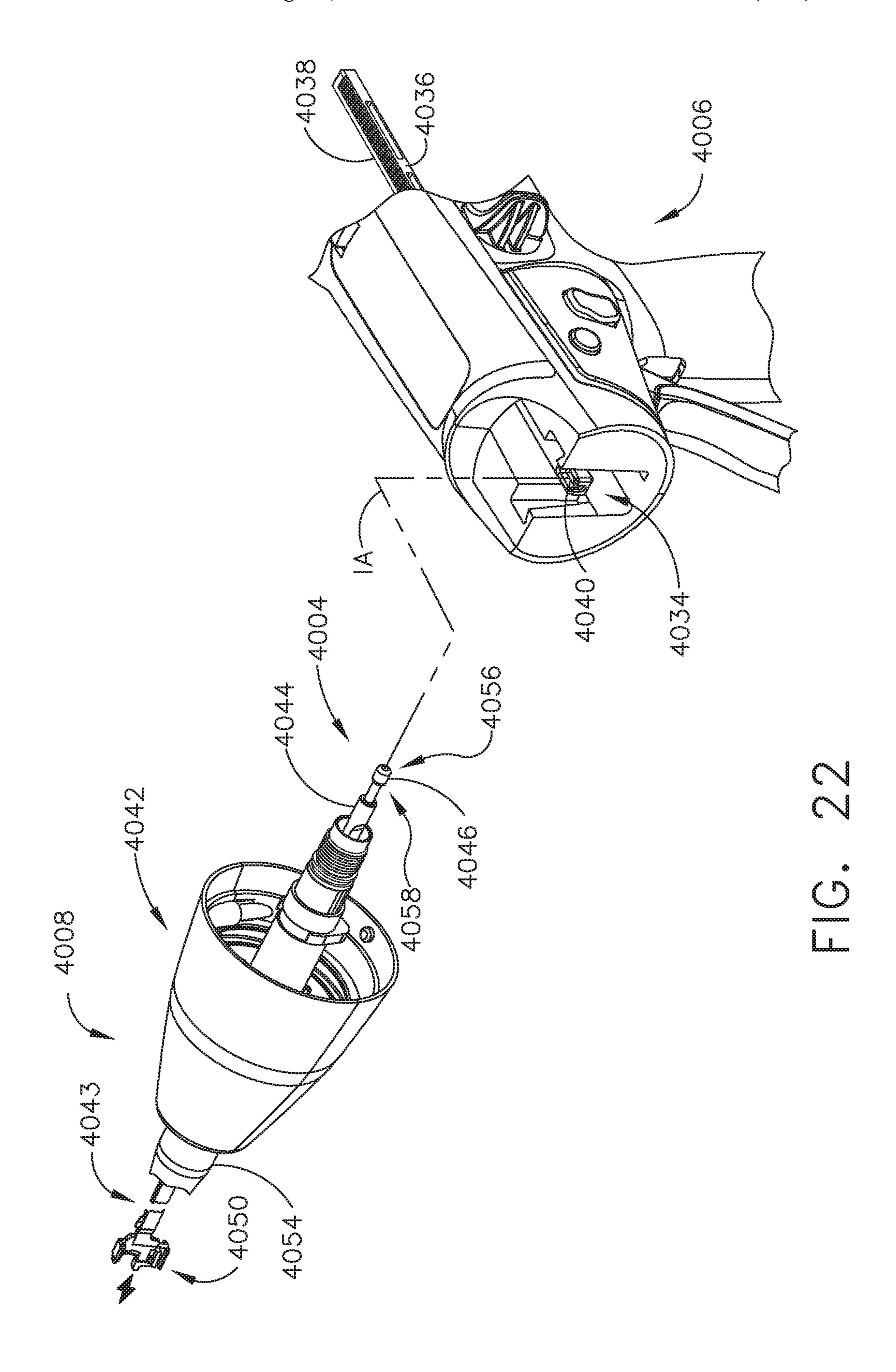
FIG. 16B











SURGICAL SYSTEM COUPLEABLE WITH STAPLE CARTRIDGE AND RADIO FREQUENCY CARTRIDGE, AND HAVING A PLURALITY OF RADIO-FREQUENCY ENERGY RETURN PATHS

TECHNICAL FIELD

The present disclosure relates to electrosurgical devices and, in various aspects, to compressive jaw components that ¹⁰ are designed to conduct electrical energy into a tissue compressed therewith.

BACKGROUND

In some aspects, an electrosurgical device may be configured to induce a hemostatic seal in a tissue and/or between tissues. The hemostatic seal may be created by a combination of an applied compressive force to the tissue and an application of electrical energy to the tissue. In some aspects of an electrosurgical device, the compressive force may be supplied by a compression of the tissue between jaw assemblies. Additionally, the electrical energy may be supplied by one or more electrodes disposed within or on some components of the jaw assemblies. The amount of electrical energy sufficient to effect the hemostatic seal may depend, in part, on the thickness, density, and/or quality of tissue to be sealed.

It may be understood that an application of excessive electrical energy to a tissue may result in burning or scaring 30 of the tissue. However, the application of insufficient electrical energy to a tissue may result in an ineffective hemostatic seal. Thus, a user of the electrosurgical device may be required to adjust the amount of electrical energy delivered to the tissue compressed between the jaw assemblies of the device based on the tissue thickness, density, and quality. If a tissue compressed between the jaw assemblies is essentially homogeneous, the user of the electrosurgical device may use simple controls to adjust the amount of electrical energy delivered to the tissue. However, it may be recog-40 nized that some tissues for hemostatic sealing are inhomogeneous in any one or more of their thickness, density, and/or quality. As a result, a single control for the amount of electrical energy delivered to the tissue compressed between the jaw assemblies may result in burned portions as well as 45 insufficiently sealed portions of the tissue. It is therefore desirable to have an electrosurgical device that may be configured to deliver a variety of electrical energies to a piece of tissue compressed between the jaw assemblies.

SUMMARY

In one aspect, an interchangeable tool assembly is provided. The interchangeable tool assembly comprises a first jaw configured to support a staple cartridge during a first 55 time period and a radio-frequency cartridge during a second time period; a second jaw coupled to the first jaw, wherein a surface of the second jaw defines a plurality of staple forming pockets configured to form staples driven from the staple cartridge; and an electrically insulative material covering segments of the surface of the second jaw other than the staple forming pockets, wherein the staple forming pockets define at least one return path for radio-frequency energy delivered by the radio-frequency cartridge.

In another aspect, a surgical tool assembly is provided. 65 The surgical tool assembly, comprises an elongate channel configured to support a staple cartridge during a first time 2

period and a radio-frequency cartridge during a second time period; and an anvil coupled to the elongate channel, wherein the anvil comprises: a surface which faces the elongate channel and defines a plurality of staple forming pockets configured to form staples driven from the staple cartridge; and an electrically insulative material which covers segments of the surface of the second jaw, wherein the plurality of staple forming pockets provide for a plurality of different return paths for radio-frequency energy delivered by the radio-frequency cartridge.

In another aspect, an interchangeable tool assembly is provided. The interchangeable tool assembly comprises an end effector configured to releasably couple to a shaft assembly, wherein the end effector comprises: an elongate channel configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period; and an anvil coupled to the elongate channel, wherein the anvil comprises an electrically insulative material and defines a plurality of different return paths for radio-frequency energy delivered by the radio-frequency cartridge.

FIGURES

The novel features of the aspects described herein are set forth with particularity in the appended claims. These aspects, however, both as to organization and methods of operation may be better understood by reference to the following description, taken in conjunction with the accompanying drawings.

FIG. 1 is a perspective view of a surgical system including a handle assembly coupled to an interchangeable surgical tool assembly that is configured to be used in connection with conventional surgical staple/fastener cartridges and radio frequency (RF) cartridges according to one aspect of this disclosure.

FIG. 2 is an exploded perspective assembly view of the surgical system of FIG. 1 according to one aspect of this disclosure.

FIG. 3 is another exploded perspective assembly view of portions of the handle assembly and interchangeable surgical tool assembly of FIGS. 1 and 2 according to one aspect of this disclosure.

FIG. 4 is an exploded assembly view of a proximal portion of the interchangeable surgical tool assembly of FIGS. 1-3 according to one aspect of this disclosure.

FIG. 5 is another exploded assembly view of a distal portion of the interchangeable surgical tool assembly of FIGS. 1-5 according to one aspect of this disclosure.

FIG. 6 is a partial cross-sectional view of the end effector depicted in FIGS. 1-5 supporting an RF cartridge therein and with tissue clamped between the cartridge and the anvil according to one aspect of this disclosure.

FIG. 7 is a partial cross-sectional view of the anvil of FIG. 6 according to one aspect of this disclosure.

FIG. 8 is another exploded assembly view of a portion of the interchangeable surgical tool assembly of FIGS. 1-5 according to one aspect of this disclosure.

FIG. 9 is another exploded assembly view of the interchangeable surgical tool assembly and handle assembly of FIGS. 1 and 2 according to one aspect of this disclosure.

FIG. 10 is a perspective view of an RF cartridge and an elongate channel of the interchangeable surgical tool assembly of FIGS. 1-5 according to one aspect of this disclosure.

FIG. 11 is a partial perspective view of portions of the RF cartridge and elongate channel of FIG. 10 with a knife member according to one aspect of this disclosure.

FIG. 12 is another perspective view of the RF cartridge installed in the elongate channel of FIG. 10 and illustrating a portion of a flexible shaft circuit arrangement according to one aspect of this disclosure.

FIG. 13 is a cross-sectional end view of the RF cartridge 5 and elongate channel of FIG. 12 taken along lines 13-13 in FIG. 12 according to one aspect of this disclosure.

FIG. 14 is a top cross-sectional view of a portion of the interchangeable surgical tool assembly of FIGS. 1 and 5 with the end effector thereof in an articulated position 10 according to one aspect of this disclosure.

FIG. 15 is a perspective view of an onboard circuit board arrangement and RF generator plus configuration according to one aspect of this disclosure.

FIGS. 16A-16B is a block diagram of a control circuit of 15 the surgical instrument of FIG. 1 spanning two drawing sheets according to one aspect of this disclosure.

FIG. 17 is a block diagram of the control circuit of the surgical instrument of FIG. 1 illustrating interfaces between the handle assembly, the power assembly, and the handle 20 assembly and the interchangeable shaft assembly according to one aspect of this disclosure.

FIG. 18 is a schematic diagram of a surgical instrument configured to control various functions according to one aspect of this disclosure.

FIG. 19 is a perspective view of various aspects of a surgical system according to one aspect of this disclosure.

FIG. 20 is a partial cross-section of an end effector of the surgical system of FIG. 19 according to one aspect of this disclosure.

FIG. 21 is a partial perspective view of a radio-frequency cartridge supported by an elongate channel of the end effector of FIG. 20 according to one aspect of this disclosure.

FIG. 22 is an exploded perspective assembly view of portions of a handle assembly and an interchangeable tool ³⁵ assembly of the surgical system of FIG. 19 according to one aspect of this disclosure.

DESCRIPTION

Applicant of the present application owns the following patent applications filed Jun. 28, 2017, and which are each herein incorporated by reference in their respective entireties:

U.S. patent application Ser. No. 15/636,096, titled SUR-45 GICAL SYSTEM COUPLABLE WITH STAPLE CARTRIDGE AND RADIO FREQUENCY CARTRIDGE, AND METHOD OF USING SAME, by inventors Jeffrey D. Messerly et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000478.

U.S. patent application Ser. No. 15/636,103, titled SYSTEMS AND METHODS OF DISPLAYING SURGICAL INSTRUMENT STATUS, by inventors Jeffrey D. Messerly et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000533.

U.S. patent application Ser. No. 15/636,110, titled SHAFT MODULE CIRCUITRY ARRANGEMENTS, by inventors Jeffrey D. Messerly et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000525.

U.S. patent application Ser. No. 15/636,116, titled SYS-60 TEMS AND METHODS FOR CONTROLLING CONTROL CIRCUITS FOR INDEPENDENT ENERGY DELIVERY OVER SEGMENTED SECTIONS, by inventors Jeffrey D. Messerly et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000534.

U.S. patent application Ser. No. 15/636,123, titled FLEX-IBLE CIRCUIT ARRANGEMENT FOR SURGICAL FAS-

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TENING INSTRUMENTS, by inventors Jeffrey D. Messerly et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000531.

U.S. patent application Ser. No. 15/636,144, titled SYSTEMS AND METHODS FOR CONTROLLING CONTROL CIRCUITS FOR AN INDEPENDENT ENERGY DELIVERY OVER SEGMENTED SECTIONS, by inventors David C. Yates et al., filed Jun. 28, 2017, now U.S. Pat. No. 10,265,120.

U.S. patent application Ser. No. 15/636,150, titled SUR-GICAL END EFFECTOR FOR APPLYING ELECTRO-SURGICAL ENERGY TO DIFFERENT ELECTRODES ON DIFFERENT TIME PERIODS, by inventors Tamara Widenhouse et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000537.

U.S. patent application Ser. No. 15/636,162, titled ELECTROSURGICAL CARTRIDGE FOR USE IN THIN PROFILE SURGICAL CUTTING AND STAPLING INSTRUMENT, by inventors Tamara Wdenhouse et al., now U.S. Patent Application Publication No. 2019-0000538.

U.S. patent application Ser. No. 15/636,169, titled SUR-GICAL END EFFECTOR TO ADJUST JAW COMPRESSION, by inventors Frederick E. Shelton, I V et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 25 2019/0000532.

U.S. patent application Ser. No. 15/636,177, titled CARTRIDGE ARRANGEMENTS FOR SURGICAL CUTTING AND FASTENING INSTRUMENTS WITH LOCKOUT DISABLEMENT FEATURES, by inventors Jason L. Harris et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000479.

U.S. patent application Ser. No. 15/636,180, titled SUR-GICAL CUTTING AND FASTENING INSTRUMENTS WITH DUAL POWER SOURCES, by inventors Jeffrey D. Messerly et al., filed Jun. 28, 2017, now U.S. Patent Application Publication No. 2019/0000539.

Electrosurgical devices may be used in many surgical operations. Electrosurgical devices may apply electrical energy to tissue in order to treat tissue. An electrosurgical 40 device may comprise an instrument having a distally mounted end effector comprising one or more electrodes. The end effector can be positioned against tissue such that electrical current may be introduced into the tissue. Electrosurgical devices can be configured for monopolar or bipolar operation. During monopolar operation, current may be introduced into the tissue by an active (or source) electrode on the end effector and returned through a return electrode. The return electrode may be a grounding pad and separately located on a patient's body. During bipolar opera-50 tion, current may be introduced into and returned from the tissue by the active and return electrodes, respectively, of the end effector.

The end effector may include two or more jaw members. At least one of the jaw members may have at least one electrode. At least one jaw may be movable from a position spaced apart from the opposing jaw for receiving tissues to a position in which the space between the jaw members is less than that of the first position. This movement of the movable jaw may compress the tissue held between. Heat generated by the current flow through the tissue in combination with the compression achieved by the jaw's movement may form hemostatic seals within the tissue and/or between tissues and, thus, may be particularly useful for sealing blood vessels, for example. The end effector may comprise a cutting member. The cutting member may be movable relative to the tissue and the electrodes to transect the tissue.

Electrosurgical devices also may include mechanisms to clamp tissue together, such as a stapling device, and/or mechanisms to sever tissue, such as a tissue knife. An electrosurgical device may include a shaft for placing the end effector proximate to tissue undergoing treatment. The 5 shaft may be straight or curved, bendable or non-bendable. In an electrosurgical device including a straight and bendable shaft, the shaft may have one or more articulation joints to permit controlled bending of the shaft. Such joints may permit a user of the electrosurgical device to place the end 10 effector in contact with tissue at an angle to the shaft when the tissue being treated is not readily accessible using an electrosurgical device having a straight, non-bending shaft.

Electrical energy applied by electrosurgical devices can be transmitted to the instrument by a generator in commu- 15 nication with the hand piece. The electrical energy may be in the form of radio frequency ("RF") energy. RF energy is a form of electrical energy that may be in the frequency range of 200 kilohertz (kHz) to 1 megahertz (MHz). In application, an electrosurgical instrument can transmit low 20 frequency RF energy through tissue, which causes ionic agitation, or friction, in effect resistive heating, thereby increasing the temperature of the tissue. Because a sharp boundary is created between the affected tissue and the surrounding tissue, surgeons can operate with a high level of 25 precision and control, without sacrificing un-targeted adjacent tissue. The low operating temperatures of RF energy is useful for removing, shrinking, or sculpting soft tissue while simultaneously sealing blood vessels. RF energy works particularly well on connective tissue, which is primarily 30 comprised of collagen and shrinks when contacted by heat.

The RF energy may be in a frequency range described in EN 60601-2-2:2009+A11:2011, Definition 201.3.218— HIGH FREQUENCY. For example, the frequency in less than 5 MHz. However, in bipolar RF applications, the frequency can be almost anything. Frequencies above 200 kHz can be typically used for monopolar applications in order to avoid the unwanted stimulation of nerves and muscles that would result from the use of low frequency 40 current. Lower frequencies may be used for bipolar applications if the risk analysis shows the possibility of neuromuscular stimulation has been mitigated to an acceptable level. Normally, frequencies above 5 MHz are not used in order to minimize the problems associated with high fre- 45 quency leakage currents. Higher frequencies may, however, be used in the case of bipolar applications. It is generally recognized that 10 mA is the lower threshold of thermal effects on tissue.

FIGS. 1 and 2 depict a motor-driven surgical system 10 50 that may be used to perform a variety of different surgical procedures. In the illustrated arrangement, the surgical system 10 comprises an interchangeable surgical tool assembly 1000 that is operably coupled to a handle assembly 500. In another surgical system aspect, the interchangeable surgical 55 tool assembly 1000 may also be effectively employed with a tool drive assembly of a robotically controlled or automated surgical system. For example, the surgical tool assembly 1000 disclosed herein may be employed with various robotic systems, instruments, components and methods such 60 as, but not limited to, those disclosed in U.S. Pat. No. 9,072,535, entitled SURGICAL STAPLING INSTRU-MENTS WITH ROTATABLE STAPLE DEPLOYMENT ARRANGEMENTS, which is hereby incorporated by reference herein in its entirety.

In the illustrated aspect, the handle assembly 500 may comprise a handle housing 502 that includes a pistol grip

portion that can be gripped and manipulated by the clinician. As will be briefly discussed below, the handle assembly **500** operably supports a plurality of drive systems that are configured to generate and apply various control motions to corresponding portions of the interchangeable surgical tool assembly 1000. As shown in FIG. 2, the handle assembly 500 may further include a handle frame 506 that operably supports the plurality of drive systems. For example, the handle frame 506 can operably support a "first" or closure drive system, generally designated as 510, which may be employed to apply closing and opening motions to the interchangeable surgical tool assembly 1000. In at least one form, the closure drive system 510 may include an actuator in the form of a closure trigger 512 that is pivotally supported by the handle frame 506. Such arrangement enables the closure trigger 512 to be manipulated by a clinician such that when the clinician grips the pistol grip portion of the handle assembly 500, the closure trigger 512 may be easily pivoted from a starting or "unactuated" position to an "actuated" position and more particularly to a fully compressed or fully actuated position. In use, to actuate the closure drive system 510, the clinician depresses the closure trigger 512 towards the pistol grip portion. As described in further detail in U.S. patent application Ser. No. 14/226,142, entitled SURGICAL INSTRUMENT COMPRISING A SENSOR SYSTEM, now U.S. Patent Application Publication No. 2015/0272575, which is hereby incorporated by reference in its entirety herein, when the clinician fully depresses the closure trigger 512 to attain the full closure stroke, the closure drive system **510** is configured to lock the closure trigger 512 into the fully depressed or fully actuated position. When the clinician desires to unlock the closure trigger 512 to permit it to be biased to the unactuated position, the clinician simply activates a closure release monopolar RF applications may be typically restricted to 35 button assembly 518 which enables the closure trigger to return to unactuated position. The closure release button assembly 518 may also be configured to interact with various sensors that communicate with a microcontroller in the handle assembly 500 for tracking the position of the closure trigger **512**. Further details concerning the configuration and operation of the closure release button assembly 518 may be found in U.S. Patent Application Publication No. 2015/0272575.

In at least one form, the handle assembly 500 and the handle frame 506 may operably support another drive system referred to herein as a firing drive system 530 that is configured to apply firing motions to corresponding portions of the interchangeable surgical tool assembly that is attached thereto. As was described in detail in U.S. Patent Application Publication No. 2015/0272575, the firing drive system **530** may employ an electric motor 505 that is located in the pistol grip portion of the handle assembly 500. In various forms, the motor **505** may be a DC brushed driving motor having a maximum rotation of, approximately, 25,000 RPM, for example. In other arrangements, the motor 505 may include a brushless motor, a cordless motor, a synchronous motor, a stepper motor, or any other suitable electric motor. The motor 505 may be powered by a power source 522 that in one form may comprise a removable power pack. The power pack may support a plurality of Lithium Ion ("LI") or other suitable batteries therein. A number of batteries connected in series or parallel may be used as the power source **522** for the surgical system 10. In addition, the power source 522 may be replaceable and/or rechargeable.

The electric motor 505 is configured to axially drive a longitudinally movable drive member **540** (FIG. **3**) in a distal and proximal directions depending upon the polarity

of the motor. For example, when the motor **505** is driven in one rotary direction, the longitudinally movable drive member will be axially driven in a distal direction "DD". When the motor 505 is driven in the opposite rotary direction, the longitudinally movable drive member **540** will be axially 5 driven in a proximal direction "PD". The handle assembly 500 can include a switch 513 which can be configured to reverse the polarity applied to the electric motor 505 by the power source **522** or otherwise control the motor **505**. The handle assembly 500 can also include a sensor or sensors 1 (not shown) that is configured to detect the position of the drive member and/or the direction in which the drive member is being moved. Actuation of the motor 505 can be controlled by a firing trigger (not shown) that is adjacent to the closure trigger **512** and pivotally supported on the handle 15 assembly **500**. The firing trigger may be pivoted between an unactuated position and an actuated position. The firing trigger may be biased into the unactuated position by a spring or other biasing arrangement such that when the clinician releases the firing trigger, it may be pivoted or 20 otherwise returned to the unactuated position by the spring or biasing arrangement. In at least one form, the firing trigger can be positioned "outboard" of the closure trigger **512**. As discussed in U.S. Patent Application Publication No. 2015/0272575, the handle assembly **500** may be equipped 25 with a firing trigger safety button (not shown) to prevent inadvertent actuation of the firing trigger. When the closure trigger **512** is in the unactuated position, the safety button is contained in the handle assembly 500 where the clinician cannot readily access it and move it between a safety 30 position preventing actuation of the firing trigger and a firing position wherein the firing trigger may be fired. As the clinician depresses the closure trigger, the safety button and the firing trigger pivot down wherein they can then be manipulated by the clinician.

In at least one form, the longitudinally movable drive member 540 may have a rack of teeth 542 formed thereon for meshing engagement with a corresponding drive gear arrangement (not shown) that interfaces with the motor. See FIG. 3. Further details regarding those features may be 40 found in U.S. Patent Application Publication No. 2015/ 0272575. In at least one arrangement, however, the longitudinally movable drive member is insulated to protect it from inadvertent RF energy. At least one form also includes a manually-actuatable "bailout" assembly that is configured 45 to enable the clinician to manually retract the longitudinally movable drive member should the motor 505 become disabled. The bailout assembly may include a lever or bailout handle assembly that is stored within the handle assembly **500** under a releasable door **550**. See FIG. **2**. The lever may be configured to be manually pivoted into ratcheting engagement with the teeth in the drive member. Thus, the clinician can manually retract the drive member 540 by using the bailout handle assembly to ratchet the drive member in the proximal direction "PD". U.S. Pat. No. 8,608,045, entitled 55 POWERED SURGICAL CUTTING AND STAPLING APPARATUS WITH MANUALLY RETRACTABLE FIR-ING SYSTEM, the entire disclosure of which is hereby incorporated by reference herein, discloses bailout arrangements and other components, arrangements and systems that 60 may also be employed with any one of the various interchangeable surgical tool assemblies disclosed herein.

In the illustrated aspect, the interchangeable surgical tool assembly 1000 includes a surgical end effector 1500 that comprises a first jaw 1600 and a second jaw 1800. In one 65 arrangement, the first jaw comprises an elongate channel 1602 that is configured to operably support a conventional

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(mechanical) surgical staple/fastener cartridge 1400 (FIG. 4) or a radio frequency (RF) cartridge 1700 (FIGS. 1 and 2) therein. The second jaw 1800 comprises an anvil 1810 that is pivotally supported relative to the elongate channel 1602. The anvil 1810 may be selectively moved toward and away from a surgical cartridge supported in the elongate channel 1602 between open and closed positions by actuating the closure drive system 510. In the illustrated arrangement, the anvil 1810 is pivotally supported on a proximal end portion of the elongate channel 1602 for selective pivotal travel about a pivot axis that is transverse to the shaft axis SA. Actuation of the closure drive system 510 may result in the distal axial movement of a proximal closure member or proximal closure tube 1910 that is attached to an articulation connector 1920.

Turning to FIG. 4, the articulation connector 1920 includes upper and lower tangs 1922, 1924 protrude distally from a distal end of the articulation connector 1920 to be movably coupled to an end effector closure sleeve or distal closure tube segment 1930. See FIG. 3. The distal closure tube segment 1930 includes an upper tang 1932 and a lower tang (not shown) that protrude proximally from a proximal end thereof. An upper double pivot link 1940 includes proximal and distal pins 1941, 1942 that engage corresponding holes in the upper tangs 1922, 1932 of the articulation connector 1920 and distal closure tube segment 1930, respectively. Similarly, a lower double pivot link 1944 includes proximal and distal pins 1945, 1946 that engage corresponding holes in the lower tangs 1924 of the articulation connector 1920 and distal closure tube segment 1930, respectively.

Still referring to FIG. 4, in the illustrated example, the distal closure tube segment 1930 includes positive jaw opening features or tabs 1936, 1938 that correspond with corresponding portions of the anvil 1810 to apply opening motions to the anvil 1810 as the distal closure tube segment 1930 is retracted in the proximal direction PD to a starting position. Further details regarding the opening and closing of the anvil 1810 may be found in U.S. patent application Ser. No. 15/635,621, entitled SURGICAL INSTRUMENT WITH POSITIVE JAW OPENING FEATURES, filed on Jun. 28, 2017, the entire disclosure of which is hereby incorporated by reference herein.

As shown in FIG. 5, in at least one arrangement, the interchangeable surgical tool assembly 1000 includes a tool frame assembly 1200 that comprises a tool chassis 1210 that operably supports a nozzle assembly 1240 thereon. As further discussed in detail in U.S. Patent Application Ser. No. 15/635,631, entitled SURGICAL INSTRUMENT WITH AXIALLY MOVABLE CLOSURE MEMBER, filed on Jun. 28, 2017, now U.S. Pat. No. 10,639,037, and which is hereby incorporated by reference in its entirety herein, the tool chassis 1210 and nozzle arrangement 1240 facilitate rotation of the surgical end effector 1500 about a shaft axis SA relative to the tool chassis **1210**. Such rotational travel is represented by arrow R in FIG. 1. As also shown in FIGS. 4 and 5, the interchangeable surgical tool assembly 1000 includes a spine assembly 1250 that operably supports the proximal closure tube 1910 and is coupled to the surgical end effector 1500. In various circumstances, for ease of assembly, the spine assembly 1250 may be fabricated from an upper spine segment 1251 and a lower spine segment 1252 that are interconnected together by snap features, adhesive, welding, etc. In assembled form, the spine assembly 1250 includes a proximal end 1253 that is rotatably supported in the tool chassis 1210. In one arrangement, for example, the proximal end 1253 of the spine assembly 1250

is attached to a spine bearing (not shown) that is configured to be supported within the tool chassis 1210. Such arrangement facilitates rotatable attachment of the spine assembly 1250 to the tool chassis such that the spine assembly 1250 may be selectively rotated about a shaft axis SA relative to 5 the tool chassis 1210.

As shown in FIG. 4, the upper spine segment 1251 terminates in an upper lug mount feature 1260 and the lower spine segment 1252 terminates in a lower lug mount feature **1270**. The upper lug mount feature **1260** is formed with a lug slot 1262 therein that is adapted to mountingly support an upper mounting link 1264 therein. Similarly, the lower lug mount feature 1270 is formed with a lug slot 1272 therein that is adapted to mountingly support a lower mounting link 1274 therein. The upper mounting link 1264 includes a pivot 15 socket 1266 therein that is offset from the shaft axis SA. The pivot socket 1266 is adapted to rotatably receive therein a pivot pin 1634 that is formed on a channel cap or anvil retainer 1630 that is attached to a proximal end portion 1610 of the elongate channel **1602**. The lower mounting link **1274** 20 includes lower pivot pin 1276 that adapted to be received within a pivot hole **1611** formed in the proximal end portion 1610 of the elongate channel 1602. The lower pivot pin 1276 as well as the pivot hole 1611 is offset from the shaft axis SA. The lower pivot pin 1276 is vertically aligned with the 25 pivot socket 1266 to define the articulation axis AA about which the surgical end effector 1500 may articulate relative to the shaft axis SA. See FIG. 1. Although the articulation axis AA is transverse to the shaft axis SA, in at least one arrangement, the articulation axis AA is laterally offset 30 therefrom and does not intersect the shaft axis SA.

Turning to FIG. 5, a proximal end 1912 of the proximal closure tube 1910 is rotatably coupled to a closure shuttle 1914 by a connector 1916 that is seated in an annular groove **1915** in the proximal closure tube segment **1910**. The 35 closure shuttle **1914** is supported for axial travel within the tool chassis 1210 and has a pair of hooks 1917 thereon configured to engage the closure drive system **510** when the tool chassis 1210 is coupled to the handle frame 506 (FIG. 9). The tool chassis 1210 further supports a latch assembly 40 **1280** for releasably latching the tool chassis **1210** to the handle frame **506**. Further details regarding the tool chassis 1210 and latch assembly 1280 may be found in U.S. patent application Ser. No. 15/635,631, entitled SURGICAL INSTRUMENT WITH AXIALLY MOVABLE CLOSURE 45 MEMBER, filed on Jun. 28, 2017, the entire disclosure of which is hereby incorporated by reference herein.

The firing drive system 530 in the handle assembly 500 is configured to be operably coupled to a firing system 1300 that is operably supported in the interchangeable surgical 50 tool assembly 1000. The firing system 1300 may include an intermediate firing shaft portion 1310 that is configured to be axially moved in the distal and proximal directions in response to corresponding firing motions applied thereto by the firing drive system **530**. See FIG. **4**. As shown in FIG. **5**, 55 a proximal end 1312 of the intermediate firing shaft portion 1310 has a firing shaft attachment lug 1314 formed thereon that is configured to be seated into an attachment cradle **544** (FIG. 3) that is on the distal end of the longitudinally movable drive member 540 of the firing drive system 530 60 within the handle assembly 500. Such arrangement facilitates the axial movement of the intermediate firing shaft portion 1310 upon actuation of the firing drive system 530. In the illustrated example, the intermediate firing shaft portion 1310 is configured for attachment to a distal cutting 65 portion or knife bar 1320. As shown in FIG. 4, the knife bar 1320 is connected to a firing member or knife member 1330.

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The knife member 1330 comprises a knife body 1332 that operably supports a tissue cutting blade 1334 thereon. The knife body 1332 may further include anvil engagement tabs or features 1336 and channel engagement features or a foot 1338. The anvil engagement features 1336 may serve to apply additional closure motions to the anvil 1810 as the knife member 1330 is advanced distally through the end effector 1500.

In the illustrated example, the surgical end effector 1500 is selectively articulatable about the articulation axis AA by an articulation system 1360. In one form, the articulation system 1360 includes proximal articulation driver 1370 that is pivotally coupled to an articulation link 1380. As can be most particularly seen in FIG. 4, an offset attachment lug 1373 is formed on a distal end 1372 of the proximal articulation driver 1370. A pivot hole 1374 is formed in the offset attachment lug 1373 and is configured to pivotally receive therein a proximal link pin 1382 formed on the proximal end 1381 of the articulation link 1380. A distal end 1383 of the articulation link 1380 includes a pivot hole 1384 that is configured to pivotally receive therein a channel pin 1618 formed on the proximal end portion 1610 of the elongate channel 1602. Thus, axial movement of proximal articulation driver 1370 will thereby apply articulation motions to the elongate channel 1602 to thereby cause the surgical end effector 1500 to articulate about the articulation axis AA relative to the spine assembly 1250. In various circumstances, the proximal articulation driver 1370 can be held in position by an articulation lock 1390 when the proximal articulation driver 1370 is not being moved in the proximal or distal directions. Further details regarding an example form of articulation lock 1390 may be found in U.S. patent application Ser. No. 15/635,837 entitled SURGICAL INSTRUMENT COMPRISING AN ARTICULATION SYSTEM LOCKABLE TO A FRAME, filed on Jun. 28, 2017, the entire disclosure of which is hereby incorporated by reference herein.

Further to the above, the interchangeable surgical tool assembly 1000 can include a shifter assembly 1100 which can be configured to selectively and releasably couple the proximal articulation driver 1310 to the firing system 1300. As illustrated in FIG. 5, for example, in one form, the shifter assembly 1100 includes a lock collar, or lock sleeve 1110, positioned around the intermediate firing shaft portion 1310 of the firing system 1300 wherein the lock sleeve 1110 can be rotated between an engaged position in which the lock sleeve 1110 operably couples the proximal articulation driver 1370 to the firing member assembly 1300 and a disengaged position in which the proximal articulation driver 1370 is not operably coupled to the firing member assembly 1300. When lock sleeve 1110 is in its engaged position, distal movement of the firing member assembly 1300 can move the proximal articulation driver 1370 distally and, correspondingly, proximal movement of the firing member assembly 1300 can move the proximal articulation driver 1370 proximally. When lock sleeve 1110 is in its disengaged position, movement of the firing member assembly 1300 is not transmitted to the proximal articulation driver 1370 and, as a result, the firing member assembly 1300 can move independently of the proximal articulation driver 1370. In various circumstances, the proximal articulation driver 1370 can be held in position by the articulation lock 1390 when the proximal articulation driver 1370 is not being moved in the proximal or distal directions by the firing member assembly 1300.

In the illustrated arrangement, the intermediate firing shaft portion 1310 of the firing member assembly 1300 is

formed with two opposed flat sides with a drive notch 1316 formed therein. See FIG. 5. As can also be seen in FIG. 5, the lock sleeve 1110 comprises a cylindrical, or an at least substantially cylindrical, body that includes a longitudinal aperture that is configured to receive the intermediate firing 5 shaft portion 1310 therethrough. The lock sleeve 1110 can comprise diametrically-opposed, inwardly-facing lock protrusions that, when the lock sleeve 1110 is in one position, are engagingly received within corresponding portions of the drive notch 1316 in the intermediate firing shaft portion 10 1310 and, when in another position, are not received within the drive notch 1316 to thereby permit relative axial motion between the lock sleeve 1110 and the intermediate firing shaft 1310. As can be further seen in FIG. 5, the lock sleeve 1110 further includes a lock member 1112 that is sized to be 15 movably received within a notch 1375 in a proximal end of the proximal articulation driver 1370. Such arrangement permits the lock sleeve 1110 to slightly rotate into and out of engagement with the intermediate firing shaft portion 1310 while remaining in position for engagement or in engage- 20 ment with the notch 1375 in the proximal articulation driver 1370. For example, when the lock sleeve 1110 is in its engaged position, the lock protrusions are positioned within the drive notch 1316 in the intermediate firing shaft portion 1310 such that a distal pushing force and/or a proximal 25 pulling force can be transmitted from the firing member assembly 1300 to the lock sleeve 1110. Such axial pushing or pulling motion is then transmitted from the lock sleeve 1110 to the proximal articulation driver 1370 to thereby articulate the surgical end effector **1500**. In effect, the firing 30 member assembly 1300, the lock sleeve 1110, and the proximal articulation driver 1370 will move together when the lock sleeve 1110 is in its engaged (articulation) position. On the other hand, when the lock sleeve 1110 is in its disengaged position, the lock protrusions are not received 35 within the drive notch 1316 in the intermediate firing shaft portion 1310 and, as a result, a distal pushing force and/or a proximal pulling force may not be transmitted from the firing member assembly 1300 to the lock sleeve 1110 (and the proximal articulation driver 1370).

In the illustrated example, relative movement of the lock sleeve 1110 between its engaged and disengaged positions may be controlled by the shifter assembly 1100 that interfaces with the proximal closure tube 1910. Still referring to FIG. 5, the shifter assembly 1100 further includes a shifter 45 key 1120 that is configured to be slidably received within a key groove formed in the outer perimeter of the lock sleeve 1110. Such arrangement enables the shifter key 1120 to move axially with respect to the lock sleeve 1110. As discussed in further detail in U.S. patent application Ser. No. 50 15/635,631, entitled SURGICAL INSTRUMENT WITH AXIALLY MOVABLE CLOSURE MEMBER, filed on Jun. 28, 2017, the entire disclosure of which is hereby incorporated by reference herein, a portion of the shifter key 1120 is configured to cammingly interact with a cam opening (not 55 shown) in the proximal closure tube portion 1910. Also in the illustrated example, the shifter assembly 1100 further includes a switch drum 1130 that is rotatably received on a proximal end portion of the proximal closure tube portion **1910**. A portion of the shifter key **1120** extends through an 60 axial slot segment in the switch drum 1130 and is movably received within an arcuate slot segment in the switch drum 1130. A switch drum torsion spring 1132 is mounted on the switch drum 1130 and engages a portion of the nozzle assembly 1240 to apply a torsional bias or rotation which 65 serves to rotate the switch drum 1130 until the portion of the shifter key 1120 reaches an end portion of the cam opening

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in the proximal closure tube portion 1910. When in this position, the switch drum 1130 may provide a torsional bias to the shifter key 1120 which thereby causes the lock sleeve 1110 to rotate into its engaged position with the intermediate firing shaft portion 1310. This position also corresponds to the unactuated configuration of the proximal closure tube 1910 (and distal closure tube segment 1930).

In one arrangement, for example, when the proximal closure tube 1910 is in an unactuated configuration (anvil 1810 is in an open position spaced away from the cartridge mounted in the elongate channel 1602) actuation of the intermediate firing shaft portion 1310 will result in the axial movement of the proximal articulation driver 1370 to facilitate articulation of the end effector **1500**. Once the user has articulated the surgical end effector 1500 to a desired orientation, the user may then actuate the proximal closure tube portion 1910. Actuation of the proximal closure tube portion **1910** will result in the distal travel of the distal closure tube segment 1930 to ultimately apply a closing motion to the anvil **1810**. This distal travel of the proximal closure tube portion 1910 will result in the cam opening therein cammingly interacting with a cam portion of the shifter key 1120 to thereby cause the shifter key 1120 to rotate the lock sleeve 1110 in an actuation direction. Such rotation of the lock sleeve 1110 will result in the disengagement of the lock protrusions from the drive notch 1316 in the intermediate firing shaft portion 1310. When in such configuration, the firing drive system 530 may be actuated to actuate the intermediate firing shaft portion 1310 without actuating the proximal articulation driver 1370. Further details concerning the operation of the switch drum 1130 and lock sleeve 1110, as well as alternative articulation and firing drive arrangements that may be employed with the various interchangeable surgical tool assemblies described herein, may be found in U.S. patent application Ser. No. 13/803,086, now U.S. Patent Application Publication No. 2014/0263541, and U.S. patent application Ser. No. 15/019,196, the entire disclosures of which are hereby incorporated by reference herein.

As also illustrated in FIGS. 5 and 15, the interchangeable surgical tool assembly 1000 can comprise a slip ring assembly 1150 which can be configured to conduct electrical power to and/or from the surgical end effector 1500 and/or communicate signals to and/or from the surgical end effector 1500, back to an onboard circuit board 1152, while facilitating rotational travel of the shaft and end effector 1500 about the shaft axis SA relative to the tool chassis 1210 by rotating the nozzle assembly 1240. As shown in FIG. 15, in at least one arrangement, the onboard circuit board 1152 includes an onboard connector 1154 that is configured to interface with a housing connector **562** (FIG. **9**) communicating with a microprocessor **560** (FIG. **9**) that is supported in the handle assembly **500** (FIG. **9**) or robotic system controller, for example. The slip ring assembly 1150 is configured to interface with a proximal connector 1153 that interfaces with the onboard circuit board 1152. Further details concerning the slip ring assembly 1150 and associated connectors may be found in U.S. patent application Ser. No. 13/803,086, now U.S. Patent Application Publication No. 2014/0263541, and U.S. patent application Ser. No. 15/019,196 which have each been herein incorporated by reference in their respective entirety as well as in U.S. patent application Ser. No. 13/800,067, entitled STAPLE CAR-TRIDGE TISSUE THICKNESS SENSOR SYSTEM, now U.S. Patent Application Publication No. 2014/0263552, which is hereby incorporated by reference herein in its entirety.

An example version of the interchangeable surgical tool assembly 1000 disclosed herein may be employed in connection with a standard (mechanical) surgical fastener cartridge 1400 or a cartridge 1700 that is configured to facilitate cutting of tissue with the knife member and seal the cut 5 tissue using radio frequency (RF) energy. Turning again to FIG. 4, a conventional or standard mechanical-type cartridge 1400 is depicted. Such cartridge arrangements are known and may comprise a cartridge body 1402 that is sized and shaped to be removably received and supported in the 10 elongate channel 1602. For example, the cartridge body **1402** may be configured to be removably retained in snap engagement with the elongate channel 1602. The cartridge body 1402 includes an elongate slot 1404 to accommodate axial travel of the knife member 1330 therethrough. The 15 cartridge body 1402 operably supports therein a plurality of staple drivers (not shown) that are aligned in rows on each side of the centrally disposed elongate slot **1404**. The drivers are associated with corresponding staple/fastener pockets **1412** that open through the upper deck surface **1410** of the 20 cartridge body **1402**. Each of the staple drivers supports one or more surgical staple or fastener (not shown) thereon. A sled assembly 1420 is supported within a proximal end of the cartridge body 1402 and is located proximal to the drivers and fasteners in a starting position when the cartridge 25 **1400** is new and unfired. The sled assembly **1420** includes a plurality of sloped or wedge-shaped cams 1422 wherein each cam 1422 corresponds to a particular line of fasteners or drivers located on a side of the slot 1404. The sled assembly **1420** is configured to be contacted and driven by 30 the knife member 1330 as the knife member is driven distally through the tissue that is clamped between the anvil and the cartridge deck surface 1410. As the drivers are driven upward toward the cartridge deck surface 1410, the fastener(s) supported thereon are driven out of their staple 35 pockets 1412 and through the tissue that is clamped between anvil and the cartridge.

Still referring to FIG. 4, the anvil 1810 in at least one form includes an anvil mounting portion 1820 that has a pair of anvil trunnions 1822 protruding laterally therefrom to be 40 pivotally received in corresponding trunnion cradles formed in the upstanding walls 1622 of the proximal end portion 1610 of the elongate channel 1602. The anvil trunnions 1822 are pivotally retained in their corresponding trunnion cradle by the channel cap or anvil retainer **1630**. The anvil mount- 45 ing portion 1820 is movably or pivotably supported on the elongate channel 1602 for selective pivotal travel relative thereto about a fixed anvil pivot axis that is transverse to the shaft axis SA. As shown in FIGS. 6 and 7, in at least one form, the anvil **1810** includes an anvil body portion **1812** 50 that is fabricated from an electrically conductive metal material for example and has a staple forming undersurface **1813** that has a series of fastener forming pockets **1814** formed therein on each side of a centrally disposed anvil slot **1815** that is configured to slidably accommodate the knife 55 member 1330 therein. The anvil slot 1815 opens into an upper opening 1816 that extends longitudinally through the anvil body 1812 to accommodate the anvil engagement features 1336 on the knife member 1330 during firing. When a conventional mechanical surgical staple/fastener cartridge 60 1400 is installed in the elongate channel 1602, the staples/ fasteners are driven through the tissue T and into forming contact with the corresponding fastener forming pockets **1814**. The anvil body **1812** may have an opening in the upper portion thereof to facilitate ease of installation for 65 example. An anvil cap 1818 may be inserted therein and welded to the anvil body 1812 to enclose the opening and

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improve the overall stiffness of the anvil body 1812. As shown in FIG. 7, to facilitate use of the end effector 1500 in connection with RF cartridges 1700, the tissue facing segments 1817 of the fastener forming undersurface 1813 may have electrically insulative material 1819 thereon.

In the illustrated arrangement, the interchangeable surgical tool assembly 1000 is configured with a firing member lockout system, generally designated as 1640. See FIG. 8. As shown in FIG. 8, the elongate channel 1602 includes a bottom surface or bottom portion 1620 that has two upstanding side walls 1622 protruding therefrom. A centrally disposed longitudinal channel slot 1624 is formed through the bottom portion 1620 to facilitate the axial travel of the knife member 1330 therethrough. The channel slot 1624 opens into a longitudinal passage 1626 that accommodates the channel engagement feature or foot 1338 on the knife member 1330. The passage 1626 serves to define two inwardly extending ledge portions 1628 that serve to engage corresponding portions of the channel engagement feature or foot 1338. The firing member lockout system 1640 includes proximal openings 1642 located on each side of the channel slot 1624 that are each configured to receive corresponding portions of the channel engagement feature or foot 1338 when the knife member 1330 is in a starting position. A knife lockout spring 1650 is supported in the proximal end 1610 of the elongate channel 1602 and serves to bias the knife member 1330 downward. As shown in FIG. 8, the knife lockout spring 1650 includes two distally ending spring arms 1652 that are configured to engage corresponding central channel engagement features 1337 on the knife body 1332. The spring arms 1652 are configured to bias the central channel engagement features 1337 downward. Thus, when in the starting (unfired position), the knife member 1330 is biased downward such that the channel engagement features or foot 1338 is received within the corresponding proximal openings 1642 in the elongate 1602 channel. When in that locked position, if one were to attempt to distally advance the knife 1330, the central channel engagement features 1137 and/or foot 1338 would engage upstanding ledges 1654 on the elongate channel 1602 (FIGS. 8 and 11) and the knife 1330 could not be fired.

Still referring to FIG. 8, the firing member lockout system 1640 also includes an unlocking assembly 1660 formed or supported on a distal end of the firing member body 1332. The unlocking assembly **1660** includes a distally extending ledge 1662 that is configured to engage an unlocking feature 1426 formed on the sled assembly 1420 when the sled assembly 1420 is in its starting position in an unfired surgical staple cartridge 1400. Thus, when an unfired surgical staple cartridge 1400 is properly installed in the elongate channel 1602, the ledge 1662 on the unlocking assembly 1660 contacts the unlocking feature 1426 on the sled assembly 1420 which serves to bias the knife member 1330 upward such that the central channel engagement features 1137 and/or foot 1338 clear the upstanding ledges **1654** in the channel bottom **1620** to facilitate axial passage of the knife member 1330 through the elongate channel 1602. If a partially fired cartridge 1400 is unwittingly installed in the elongate channel, the sled assembly 1420 will not be in the starting position and the knife member 1330 will remain in the locked position.

Attachment of the interchangeable surgical tool assembly 1000 to the handle assembly 500 will now be described with reference to FIGS. 3 and 9. To commence the coupling process, the clinician may position the tool chassis 1210 of the interchangeable surgical tool assembly 1000 above or adjacent to the distal end of the handle frame 506 such that

tapered attachment portions 1212 formed on the tool chassis **1210** are aligned with dovetail slots **507** in the handle frame **506**. The clinician may then move the surgical tool assembly 1000 along an installation axis IA that is perpendicular to the shaft axis SA to seat the tapered attachment portions 1212 in 5 "operable engagement" with the corresponding dovetail receiving slots 507 in the distal end of the handle frame 506. In doing so, the firing shaft attachment lug 1314 on the intermediate firing shaft portion 1310 will also be seated in the cradle **544** in the longitudinally movable drive member 10 540 within the handle assembly 500 and the portions of a pin 516 on a closure link 514 will be seated in the corresponding hooks 1917 in the closure shuttle 1914. As used herein, the term "operable engagement" in the context of two components means that the two components are sufficiently 15 engaged with each other so that upon application of an actuation motion thereto, the components may carry out their intended action, function and/or procedure. Also during this process, the onboard connector 1154 on the surgical tool assembly 1000 is coupled to the housing connector 562 that 20 communicates with the microprocessor **560** that is supported in the handle assembly 500 or robotic system controller, for example.

During a typical surgical procedure, the clinician may introduce the surgical end effector 1500 into the surgical site 25 through a trocar or other opening in the patient to access the target tissue. When doing so, the clinician typically axially aligns the surgical end effector 1500 along the shaft axis SA (unarticulated state). Once the surgical end effector 1500 has passed through the trocar port, for example, the clinician 30 may need to articulate the end effector 1500 to advantageously position it adjacent the target tissue. This is prior to closing the anvil **1810** onto the target tissue, so the closure drive system 510 would remain unactuated. When in this in the application of articulation motions to the proximal articulation driver 1370. Once the end effector 1500 has attained the desired articulated position, the firing drive system 530 is deactivated and the articulation lock 1390 may retain the surgical end effector 1500 in the articulated 40 position. The clinician may then actuate the closure drive system 510 to close the anvil 1810 onto the target tissue. Such actuation of the closure drive system **510** may also result in the shifter assembly 1100 delinking the proximal articulation driver 1370 from the intermediate firing shaft 45 portion 1310. Thus, once the target tissue has been captured in the surgical end effector 1500, the clinician may once again actuate the firing drive system 530 to axially advance the firing member 1330 through the surgical staple/fastener cartridge 1400 or RF cartridge 1700 to cut the clamped 50 tissue and fire the staples/fasteners into the cut tissue T. Other closure and firing drive arrangements, actuator arrangements (both handheld, manual and automated or robotic) may also be employed to control the axial movement of the closure system components, the articulation 55 system components and/or the firing system components of the surgical tool assembly 1000 without departing from the scope of the present disclosure.

As indicated above, the surgical tool assembly 1000 is mechanical surgical staple/fastener cartridges 1400 as well as with RF cartridges 1700. In at least one form, the RF cartridge 1700 may facilitate mechanical cutting of tissue that is clamped between the anvil **1810** and the RF cartridge 1700 with the knife member 1330 while coagulating elec- 65 trical current is delivered to the tissue in the current path. Alternative arrangements for mechanically cutting and

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coagulating tissue using electrical current are disclosed in, for example, U.S. Pat. Nos. 5,403,312; 7,780,663 and U.S. patent application Ser. No. 15/142,609, entitled ELECTRO-SURGICAL INSTRUMENT WITH ELECTRICALLY CONDUCTIVE GAP SETTING AND TISSUE ENGAG-ING MEMBERS, the entire disclosures of each said references being incorporated by reference herein. Such instruments, may, for example, improve hemostasis, reduce surgical complexity as well as operating room time.

As shown in FIGS. 10-12, in at least one arrangement, the RF surgical cartridge 1700 includes a cartridge body 1710 that is sized and shaped to be removably received and supported in the elongate channel 1602. For example, the cartridge body 1710 may be configured to be removably retained in snap engagement with the elongate channel 1602. In various arrangements, the cartridge body 1710 may be fabricated from a polymer material, such as, for example, an engineering thermoplastic such as the liquid crystal polymer (LCP) VECTRATM and the elongate channel **1602** may be fabricated from metal. In at least one aspect, the cartridge body 1710 includes a centrally disposed elongate slot 1712 that extends longitudinally through the cartridge body to accommodate longitudinal travel of the knife 1330 therethrough. As shown in FIGS. 10 and 11, a pair of lockout engagement tails 1714 extend proximally from the cartridge body 1710. Each lockout engagement tail 1714 has a lockout pad 1716 formed on the underside thereof that are sized to be received within a corresponding proximal opening portion 1642 in the channel bottom 1620. Thus, when the cartridge 1700 is properly installed in the elongate channel 1602, the lockout engagement tails 1714 cover the openings 1642 and ledges 1654 to retain the knife 1330 in an unlocked position ready for firing.

Turning now to FIGS. 10-13, in the illustrated example, position, actuation of the firing drive system 530 will result 35 the cartridge body 1710 is formed with a centrally disposed raised electrode pad 1720. As can be most particularly seen in FIG. 6, the elongate slot 1712 extends through the center of the electrode pad 1720 and serves to divide the pad 1720 into a left pad segment 1720L and a right pad segment 1720R. A right flexible circuit assembly 1730R is attached to the right pad segment 1720R and a left flexible circuit assembly 1730L is attached to the left pad segment 1720L. In at least one arrangement for example, the right flexible circuit 1730R comprises a plurality of electrical conductors 1732R that may include, for example, wider electrical conductors/conductors for RF purposes and thinner electrical conductors for conventional stapling purposes that are supported or attached or embedded into a right insulator sheath/member 1734R that is attached to the right pad 1720R. In addition, the right flexible circuit assembly 1730R includes a "phase one", proximal right electrode 1736R and a "phase two" distal right electrode 1738R. Likewise, the left flexible circuit assembly 1730L comprises a plurality of electrical conductors 1732L that may include, for example, wider electrical conductors/conductors for RF purposes and thinner electrical conductors for conventional stapling purposes that are supported or attached or embedded into a left insulator sheath/member 1734L that is attached to the left pad 1720L. In addition, the left flexible circuit assembly configured to be used in connection with conventional 60 1730L includes a "phase one", proximal left electrode 1736L and a "phase two" distal left electrode 1738L. The left and right electrical conductors 1732L, 1732R are attached to a distal micro-chip 1740 mounted to the distal end portion of the cartridge body 1710. In one arrangement, for example, each of the right and left flexible circuits 1730R, 1730L may have an overall width "CW" of approximately 0.025 inches and each of the electrodes 1736R,

1736L, 1738R, 1738R has a width "EW" of approximately 0.010 inches for example. See FIG. 13. However, other widths/sizes are contemplated and may be employed in alternative aspects.

In at least one arrangement, RF energy is supplied to the 5 surgical tool assembly 1000 by a conventional RF generator 400 through a supply lead 402. In at least one arrangement, the supply lead 402 includes a male plug assembly 406 that is configured to be plugged into corresponding female connectors 410 that are attached to a segmented RF circuit 10 1160 on the an onboard circuit board 1152. See FIG. 15. Such arrangement facilitates rotational travel of the shaft and end effector 1500 about the shaft axis SA relative to the tool chassis 1210 by rotating the nozzle assembly 1240 without winding up the supply lead 402 from the generator 15 400. An onboard on/off power switch 420 is supported on the latch assembly 1280 and tool chassis 1210 for turning the RF generator on and off. When the tool assembly 1000 is operably coupled to the handle assembly 500 or robotic system, the onboard segmented RF circuit 1160 communi- 20 cates with the microprocessor 560 through the connectors 1154 and 562. As shown in FIG. 1, the handle assembly 500 may also include a display screen 430 for viewing information about the progress of sealing, stapling, knife location, status of the cartridge, tissue, temperature, etc. As can also 25 be seen FIG. 15, the slip ring assembly 1150 interfaces with a distal connector 1162 that includes a flexible shaft circuit strip or assembly 1164 that may include a plurality of narrow electrical conductors 1166 for stapling related activities and wider electrical conductors 1168 used for RF purposes. As 30 shown in FIGS. 14 and 15, the flexible shaft circuit strip 1164 is centrally supported between the laminated plates or bars 1322 that form the knife bar 1320. Such arrangement facilitates sufficient flexing of the knife bar 1320 and flexible shaft circuit strip **1164** during articulation of the end effector 35 1500 while remaining sufficiently stiff so as to enable the knife member 1330 to be distally advanced through the clamped tissue.

Turning again to FIG. 10, in at least one illustrated arrangement, the elongate channel 1602 includes a channel 40 circuit 1670 supported in a recess 1621 that extends from the proximal end 1610 of the elongate channel 1602 to a distal location 1623 in the elongate channel bottom portion 1620. The channel circuit 1670 includes a proximal contact portion 1672 that contacts a distal contact portion 1169 of the 45 flexible shaft circuit strip 1164 for electrical contact therewith. A distal end 1674 of the channel circuit 1670 is received within a corresponding wall recess 1625 formed in one of the channel walls 1622 and is folded over and attached to an upper edge 1627 of the channel wall 1622. A 50 series of corresponding exposed contacts 1676 are provided in the distal end 1674 of the channel circuit 1670. As shown in FIG. 10. As can also be seen in FIG. 10, an end of a flexible cartridge circuit 1750 is attached to the distal micro-chip 1740 and is affixed to the distal end portion of the 55 cartridge body 1710. Another end 1754 is folded over the edge of the cartridge deck surface 1711 and includes exposed contacts 1756 configured to make electrical contact with the exposed contacts 1676 of the channel circuit 1670. Thus, when the RF cartridge 1700 is installed in the elongate 60 channel 1602, the electrodes as well as the distal micro-chip 1740 are powered and communicate with the onboard circuit board 1152 through contact between the flexible cartridge circuit 1750, the flexible channel circuit 1670, the flexible shaft circuit 1164 and the slip ring assembly 1150.

FIGS. 16A-16B is a block diagram of a control circuit 700 of the surgical instrument 10 of FIG. 1 spanning two

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drawing sheets according to one aspect of this disclosure. Referring primarily to FIGS. 16A-16B, a handle assembly 702 may include a motor 714 which can be controlled by a motor driver 715 and can be employed by the firing system of the surgical instrument 10. In various forms, the motor 714 may be a DC brushed driving motor having a maximum rotational speed of approximately 25,000 RPM. In other arrangements, the motor 714 may include a brushless motor, a cordless motor, a synchronous motor, a stepper motor, or any other suitable electric motor. The motor driver 715 may comprise an H-Bridge driver comprising field-effect transistors (FETs) 719, for example. The motor 714 can be powered by the power assembly 706 releasably mounted to the handle assembly 500 for supplying control power to the surgical instrument 10. The power assembly 706 may comprise a battery which may include a number of battery cells connected in series that can be used as the power source to power the surgical instrument 10. In certain circumstances, the battery cells of the power assembly 706 may be replaceable and/or rechargeable. In at least one example, the battery cells can be Lithium-Ion batteries which can be separably couplable to the power assembly 706.

The shaft assembly 704 may include a shaft assembly controller 722 which can communicate with a safety controller and power management controller 716 through an interface while the shaft assembly 704 and the power assembly 706 are coupled to the handle assembly 702. For example, the interface may comprise a first interface portion 725 which may include one or more electric connectors for coupling engagement with corresponding shaft assembly electric connectors and a second interface portion 727 which may include one or more electric connectors for coupling engagement with corresponding power assembly electric connectors to permit electrical communication between the shaft assembly controller 722 and the power management controller 716 while the shaft assembly 704 and the power assembly 706 are coupled to the handle assembly 702. One or more communication signals can be transmitted through the interface to communicate one or more of the power requirements of the attached interchangeable shaft assembly 704 to the power management controller 716. In response, the power management controller may modulate the power output of the battery of the power assembly 706, as described below in greater detail, in accordance with the power requirements of the attached shaft assembly 704. The connectors may comprise switches which can be activated after mechanical coupling engagement of the handle assembly 702 to the shaft assembly 704 and/or to the power assembly 706 to allow electrical communication between the shaft assembly controller 722 and the power management controller 716.

The interface can facilitate transmission of the one or more communication signals between the power management controller 716 and the shaft assembly controller 722 by routing such communication signals through a main controller 717 residing in the handle assembly 702, for example. In other circumstances, the interface can facilitate a direct line of communication between the power management controller 716 and the shaft assembly controller 722 through the handle assembly 702 while the shaft assembly 704 and the power assembly 706 are coupled to the handle assembly 702.

The main controller 717 may be any single core or multicore processor such as those known under the trade name ARM Cortex by Texas Instruments. In one aspect, the main controller 717 may be an LM4F230H5QR ARM Cortex-M4F Processor Core, available from Texas Instru-

ments, for example, comprising on-chip memory of 256 KB single-cycle flash memory, or other non-volatile memory, up to 40 MHz, a prefetch buffer to improve performance above 40 MHz, a 32 KB single-cycle serial random access memory (SRAM), internal read-only memory (ROM) loaded with 5 Stellaris Ware® software, 2 KB electrically erasable programmable read-only memory (EEPROM), one or more pulse width modulation (PWM) modules, one or more quadrature encoder inputs (QEI) analog, one or more 12-bit Analog-to-Digital Converters (ADC) with 12 analog input 10 channels, details of which are available for the product datasheet.

The safety controller may be a safety controller platform comprising two controller-based families such as TMS570 and RM4x known under the trade name Hercules ARM 15 Cortex R4, also by Texas Instruments. The safety controller may be configured specifically for IEC 61508 and ISO 26262 safety critical applications, among others, to provide advanced integrated safety features while delivering scalable performance, connectivity, and memory options.

The power assembly 706 may include a power management circuit which may comprise the power management controller 716, a power modulator 738, and a current sense circuit 736. The power management circuit can be configured to modulate power output of the battery based on the 25 power requirements of the shaft assembly 704 while the shaft assembly 704 and the power assembly 706 are coupled to the handle assembly **702**. The power management controller 716 can be programmed to control the power modulator **738** of the power output of the power assembly **706** and 30 the current sense circuit 736 can be employed to monitor power output of the power assembly 706 to provide feedback to the power management controller 716 about the power output of the battery so that the power management assembly 706 to maintain a desired output. The power management controller 716 and/or the shaft assembly controller 722 each may comprise one or more processors and/or memory units which may store a number of software modules.

The surgical instrument 10 (FIGS. 1-5) may comprise an output device 742 which may include devices for providing a sensory feedback to a user. Such devices may comprise, for example, visual feedback devices (e.g., an LCD display screen, LED indicators), audio feedback devices (e.g., a 45 speaker, a buzzer) or tactile feedback devices (e.g., haptic actuators). In certain circumstances, the output device 742 may comprise a display 743 which may be included in the handle assembly 702. The shaft assembly controller 722 and/or the power management controller 716 can provide 50 feedback to a user of the surgical instrument 10 through the output device **742**. The interface can be configured to connect the shaft assembly controller 722 and/or the power management controller 716 to the output device 742. The output device 742 can instead be integrated with the power 55 assembly 706. In such circumstances, communication between the output device 742 and the shaft assembly controller 722 may be accomplished through the interface while the shaft assembly 704 is coupled to the handle assembly 702.

The control circuit 700 comprises circuit segments configured to control operations of the powered surgical instrument 10. A safety controller segment (Segment 1) comprises a safety controller and the main controller 717 segment (Segment 2). The safety controller and/or the main controller 65 717 are configured to interact with one or more additional circuit segments such as an acceleration segment, a display

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segment, a shaft segment, an encoder segment, a motor segment, and a power segment. Each of the circuit segments may be coupled to the safety controller and/or the main controller 717. The main controller 717 is also coupled to a flash memory. The main controller 717 also comprises a serial communication interface. The main controller 717 comprises a plurality of inputs coupled to, for example, one or more circuit segments, a battery, and/or a plurality of switches. The segmented circuit may be implemented by any suitable circuit, such as, for example, a printed circuit board assembly (PCBA) within the powered surgical instrument 10. It should be understood that the term processor as used herein includes any microprocessor, processors, controller, controllers, or other basic computing device that incorporates the functions of a computer's central processing unit (CPU) on an integrated circuit or at most a few integrated circuits. The main controller 717 is a multipurpose, programmable device that accepts digital data as input, processes it according to instructions stored in its memory, and 20 provides results as output. It is an example of sequential digital logic, as it has internal memory. The control circuit 700 can be configured to implement one or more of the processes described herein.

The acceleration segment (Segment 3) comprises an accelerometer. The accelerometer is configured to detect movement or acceleration of the powered surgical instrument 10. Input from the accelerometer may be used to transition to and from a sleep mode, identify an orientation of the powered surgical instrument, and/or identify when the surgical instrument has been dropped. In some examples, the acceleration segment is coupled to the safety controller and/or the main controller 717.

back to the power management controller **716** about the power output of the battery so that the power management controller **716** may adjust the power output of the power assembly **706** to maintain a desired output. The power management controller **716** and/or the shaft assembly controller **722** each may comprise one or more processors and/or memory units which may store a number of software modules.

The surgical instrument **10** (FIGS. **1-5**) may comprise an output device **742** which may include devices for providing a sensory feedback to a user. Such devices may comprise, for

The shaft segment (Segment 5) comprises controls for an interchangeable shaft assembly 500 coupled to the surgical instrument 10 (FIGS. 1-5) and/or one or more controls for an end effector 1500 coupled to the interchangeable shaft assembly 500. The shaft segment comprises a shaft connector configured to couple the main controller 717 to a shaft PCBA. The shaft PCBA comprises a low-power microcontroller with a ferroelectric random access memory (FRAM), an articulation switch, a shaft release Hall effect switch, and a shaft PCBA EEPROM. The shaft PCBA EEPROM comprises one or more parameters, routines, and/or programs specific to the interchangeable shaft assembly 500 and/or the shaft PCBA. The shaft PCBA may be coupled to the interchangeable shaft assembly 500 and/or integral with the surgical instrument 10. In some examples, the shaft segment comprises a second shaft EEPROM. The second shaft 60 EEPROM comprises a plurality of algorithms, routines, parameters, and/or other data corresponding to one or more shaft assemblies 500 and/or end effectors 1500 that may be interfaced with the powered surgical instrument 10.

The position encoder segment (Segment 6) comprises one or more magnetic angle rotary position encoders. The one or more magnetic angle rotary position encoders are configured to identify the rotational position of the motor 714, an

interchangeable shaft assembly 500, and/or an end effector 1500 of the surgical instrument 10 (FIGS. 1-5). In some examples, the magnetic angle rotary position encoders may be coupled to the safety controller and/or the main controller 717.

The motor circuit segment (Segment 7) comprises a motor 714 configured to control movements of the powered surgical instrument 10 (FIGS. 1-5). The motor 714 is coupled to the main microcontroller processor 717 by an H-bridge driver comprising one or more H-bridge field-effect transistors (FETs) and a motor controller. The H-bridge driver is also coupled to the safety controller. A motor current sensor is coupled in series with the motor to measure the current draw of the motor. The motor current sensor is in signal communication with the main controller 717 and/or the 15 safety controller. In some examples, the motor 714 is coupled to a motor electromagnetic interference (EMI) filter.

The motor controller controls a first motor flag and a second motor flag to indicate the status and position of the motor 714 to the main controller 717. The main controller 20 717 provides a pulse-width modulation (PWM) high signal, a PWM low signal, a direction signal, a synchronize signal, and a motor reset signal to the motor controller through a buffer. The power segment is configured to provide a segment voltage to each of the circuit segments.

The power segment (Segment 8) comprises a battery coupled to the safety controller, the main controller 717, and additional circuit segments. The battery is coupled to the segmented circuit by a battery connector and a current sensor. The current sensor is configured to measure the total 30 current draw of the segmented circuit. In some examples, one or more voltage converters are configured to provide predetermined voltage values to one or more circuit segments. For example, in some examples, the segmented circuit may comprise 3.3V voltage converters and/or 5V 35 voltage converters. A boost converter is configured to provide a boost voltage up to a predetermined amount, such as, for example, up to 13V. The boost converter is configured to provide additional voltage and/or current during power intensive operations and prevent brownout or low-power 40 conditions.

A plurality of switches are coupled to the safety controller and/or the main controller 717. The switches may be configured to control operations of the surgical instrument 10 (FIGS. 1-5), of the segmented circuit, and/or indicate a 45 status of the surgical instrument 10. A bail-out door switch and Hall effect switch for bailout are configured to indicate the status of a bail-out door. A plurality of articulation switches, such as, for example, a left side articulation left switch, a left side articulation right switch, a left side 50 articulation center switch, a right side articulation left switch, a right side articulation right switch, and a right side articulation center switch are configured to control articulation of an interchangeable shaft assembly 500 (FIGS. 1 and 3) and/or the end effector 300 (FIGS. 1 and 4). A left side 55 reverse switch and a right side reverse switch are coupled to the main controller 717. The left side switches comprising the left side articulation left switch, the left side articulation right switch, the left side articulation center switch, and the left side reverse switch are coupled to the main controller 60 717 by a left flex connector. The right side switches comprising the right side articulation left switch, the right side articulation right switch, the right side articulation center switch, and the right side reverse switch are coupled to the main controller 717 by a right flex connector. A firing switch, 65 a clamp release switch, and a shaft engaged switch are coupled to the main controller 717.

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Any suitable mechanical, electromechanical, or solid state switches may be employed to implement the plurality of switches, in any combination. For example, the switches may be limit switches operated by the motion of components associated with the surgical instrument 10 (FIGS. 1-5) or the presence of an object. Such switches may be employed to control various functions associated with the surgical instrument 10. A limit switch is an electromechanical device that consists of an actuator mechanically linked to a set of contacts. When an object comes into contact with the actuator, the device operates the contacts to make or break an electrical connection. Limit switches are used in a variety of applications and environments because of their ruggedness, ease of installation, and reliability of operation. They can determine the presence or absence, passing, positioning, and end of travel of an object. In other implementations, the switches may be solid state switches that operate under the influence of a magnetic field such as Hall-effect devices, magneto-resistive (MR) devices, giant magneto-resistive (GMR) devices, magnetometers, among others. In other implementations, the switches may be solid state switches that operate under the influence of light, such as optical sensors, infrared sensors, ultraviolet sensors, among others. Still, the switches may be solid state devices such as 25 transistors (e.g., FET, Junction-FET, metal-oxide semiconductor-FET (MOSFET), bipolar, and the like). Other switches may include electrical conductorless switches, ultrasonic switches, accelerometers, inertial sensors, among others.

FIG. 17 is another block diagram of the control circuit 700 of the surgical instrument of FIG. 1 illustrating interfaces between the handle assembly 702 and the power assembly 706 and between the handle assembly 702 and the interchangeable shaft assembly 704 according to one aspect of this disclosure. The handle assembly 702 may comprise a main controller 717, a shaft assembly connector 726 and a power assembly connector 730. The power assembly 706 may include a power assembly connector 732, a power management circuit 734 that may comprise the power management controller 716, a power modulator 738, and a current sense circuit 736. The shaft assembly connectors 730, 732 form an interface 727. The power management circuit 734 can be configured to modulate power output of the battery 707 based on the power requirements of the interchangeable shaft assembly 704 while the interchangeable shaft assembly 704 and the power assembly 706 are coupled to the handle assembly 702. The power management controller 716 can be programmed to control the power modulator 738 of the power output of the power assembly 706 and the current sense circuit 736 can be employed to monitor power output of the power assembly 706 to provide feedback to the power management controller 716 about the power output of the battery 707 so that the power management controller 716 may adjust the power output of the power assembly 706 to maintain a desired output. The shaft assembly 704 comprises a shaft processor 719 coupled to a non-volatile memory 721 and shaft assembly connector 728 to electrically couple the shaft assembly 704 to the handle assembly 702. The shaft assembly connectors 726, 728 form interface 725. The main controller 717, the shaft processor 719, and/or the power management controller 716 can be configured to implement one or more of the processes described herein.

The surgical instrument 10 (FIGS. 1-5) may comprise an output device 742 to a sensory feedback to a user. Such devices may comprise visual feedback devices (e.g., an LCD display screen, LED indicators), audio feedback devices

(e.g., a speaker, a buzzer), or tactile feedback devices (e.g., haptic actuators). In certain circumstances, the output device 742 may comprise a display 743 that may be included in the handle assembly 702. The shaft assembly controller 722 and/or the power management controller 716 can provide 5 feedback to a user of the surgical instrument 10 through the output device **742**. The interface **727** can be configured to connect the shaft assembly controller 722 and/or the power management controller 716 to the output device 742. The output device 742 can be integrated with the power assembly 706. Communication between the output device 742 and the shaft assembly controller 722 may be accomplished through the interface 725 while the interchangeable shaft assembly 704 is coupled to the handle assembly 702. Having described a control circuit 700 (FIGS. 16A-16B and 6) for 15 controlling the operation of the surgical instrument 10 (FIGS. 1-5), the disclosure now turns to various configurations of the surgical instrument 10 (FIGS. 1-5) and control circuit 700.

FIG. 18 is a schematic diagram of a surgical instrument 20 600 configured to control various functions according to one aspect of this disclosure. In one aspect, the surgical instrument 600 is programmed to control distal translation of a displacement member such as the I-beam **614**. The surgical instrument 600 comprises an end effector 602 that may 25 comprise an anvil 616, an I-beam 614, and a removable staple cartridge 618 which may be interchanged with an RF cartridge 609 (shown in dashed line). The end effector 602, anvil 616, I-beam 614, staple cartridge 618, and RF cartridge 609 may be configured as described herein, for example, 30 with respect to FIGS. 1-15. For conciseness and clarity of disclosure, several aspects of the present disclosure may be described with reference to FIG. 18. It will be appreciated that the components shown schematically in FIG. 18 such as the control circuit 610, sensors 638, position sensor 634, end 35 effector 602, I-beam 614, staple cartridge 618, RF cartridge 609, anvil 616, are described in connection with FIGS. 1-17 of this disclosure.

Accordingly, the components represented schematically in FIG. 18 may be readily substituted with the physical and 40 functional equivalent components described in connection with FIGS. 1-17. For example, in one aspect, the control circuit 610 may be implemented as the control circuit 700 shown and described in connection with FIGS. 16-17. In one aspect, the sensors 638 may be implemented as a limit 45 switch, electromechanical device, solid state switches, Halleffect devices, magneto-resistive (MR) devices, giant magneto-resistive (GMR) devices, magnetometers, among others. In other implementations, the sensors **638** may be solid state switches that operate under the influence of light, such 50 as optical sensors, infrared sensors, ultraviolet sensors, among others. Still, the switches may be solid state devices such as transistors (e.g., FET, Junction-FET, metal-oxide semiconductor-FET (MOSFET), bipolar, and the like). In other implementations, the sensors 638 may include elec- 55 trical conductorless switches, ultrasonic switches, accelerometers, inertial sensors, among others. In one aspect, the position sensor 634 may be implemented as an absolute positioning system comprising a magnetic rotary absolute positioning system implemented as an AS5055EQFT single- 60 chip magnetic rotary position sensor available from Austria Microsystems, AG. The position sensor 634 may interface with the control circuit 700 to provide an absolute positioning system. The position may include multiple Hall-effect elements located above a magnet and coupled to a CORDIC 65 processor (for Coordinate Rotation Digital Computer), also known as the digit-by-digit method and Volder's algorithm,

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is provided to implement a simple and efficient algorithm to calculate hyperbolic and trigonometric functions that require only addition, subtraction, bitshift, and table lookup operations. In one aspect, the end effector 602 may be implemented as surgical end effector 1500 shown and described in connection with FIGS. 1, 2, and 4. In one aspect, the I-beam 614 may be implemented as the knife member 1330 comprising a knife body 1332 that operably supports a tissue cutting blade 1334 thereon and may further include anvil engagement tabs or features 1336 and channel engagement features or a foot 1338 as shown and described in connection with FIGS. 2-4, 8, 11 and 14. In one aspect, the staple cartridge 618 may be implemented as the standard (mechanical) surgical fastener cartridge 1400 shown and described in connection with FIG. 4. In one aspect, the RF cartridge 609 may be implemented as the radio frequency (RF) cartridge 1700 shown and described in connection with FIGS. 1, 2, 6, and 10-13. In one aspect, the anvil 616 may be implemented the anvil 1810 shown and described in connection with FIGS. 1, 2, 4, and 6. These and other sensors arrangements are described in commonly owned U.S. patent application Ser. No. 15/628,175, entitled TECH-NIQUES FOR ADAPTIVE CONTROL OF MOTOR VELOCITY OF A SURGICAL STAPLING AND CUT-TING INSTRUMENT, which is incorporated herein by reference in its entirety, now U.S. Pat. No. 10,881,399.

The position, movement, displacement, and/or translation of a liner displacement member, such as the I-beam 614, can be measured by an absolute positioning system, sensor arrangement, and position sensor represented as position sensor 634. Because the I-beam 614 is coupled to the longitudinally movable drive member 540, the position of the I-beam 614 can be determined by measuring the position of the longitudinally movable drive member 540 employing the position sensor 634. Accordingly, in the following description, the position, displacement, and/or translation of the I-beam 614 can be achieved by the position sensor 634 as described herein. A control circuit 610, such as the control circuit 700 described in FIGS. 16A and 16B, may be programmed to control the translation of the displacement member, such as the I-beam **614**, as described herein. The control circuit 610, in some examples, may comprise one or more microcontrollers, microprocessors, or other suitable processors for executing instructions that cause the processor or processors to control the displacement member, e.g., the I-beam 614, in the manner described. In one aspect, a timer/counter circuit 631 provides an output signal, such as elapsed time or a digital count, to the control circuit 610 to correlate the position of the I-beam **614** as determined by the position sensor 634 with the output of the timer/counter circuit 631 such that the control circuit 610 can determine the position of the I-beam **614** at a specific time (t) relative to a starting position. The timer/counter circuit **631** may be configured to measure elapsed time, count external evens, or time external events.

The control circuit **610** may generate a motor set point signal **622**. The motor set point signal **622** may be provided to a motor controller **608**. The motor controller **608** may comprise one or more circuits configured to provide a motor drive signal **624** to the motor **604** to drive the motor **604** as described herein. In some examples, the motor **604** may be a brushed DC electric motor, such as the motor **505** shown in FIG. **1**. For example, the velocity of the motor **604** may be proportional to the motor drive signal **624**. In some examples, the motor **604** may be a brushless direct current (DC) electric motor and the motor drive signal **624** may comprise a pulse-width-modulated (PWM) signal provided

to one or more stator windings of the motor 604. Also, in some examples, the motor controller 608 may be omitted and the control circuit 610 may generate the motor drive signal 624 directly.

The motor **604** may receive power from an energy source 5 612. The energy source 612 may be or include a battery, a super capacitor, or any other suitable energy source 612. The motor 604 may be mechanically coupled to the I-beam 614 via a transmission 606. The transmission 606 may include one or more gears or other linkage components to couple the 10 motor 604 to the I-beam 614. A position sensor 634 may sense a position of the I-beam **614**. The position sensor **634** may be or include any type of sensor that is capable of generating position data that indicates a position of the I-beam 614. In some examples, the position sensor 634 may 15 include an encoder configured to provide a series of pulses to the control circuit **610** as the I-beam **614** translates distally and proximally. The control circuit 610 may track the pulses to determine the position of the I-beam **614**. Other suitable position sensor may be used, including, for example, a 20 proximity sensor. Other types of position sensors may provide other signals indicating motion of the I-beam 614. Also, in some examples, the position sensor **634** may be omitted. Where the motor 604 is a stepper motor, the control circuit 610 may track the position of the I-beam 614 by aggregating 25 the number and direction of steps that the motor 604 has been instructed to execute. The position sensor **634** may be located in the end effector 602 or at any other portion of the instrument.

The control circuit **610** may be in communication with 30 one or more sensors **638**. The sensors **638** may be positioned on the end effector **602** and adapted to operate with the surgical instrument **600** to measure the various derived parameters such as gap distance versus time, tissue compression versus time, and anvil strain versus time. The 35 sensors **638** may comprise a magnetic sensor, a magnetic field sensor, a strain gauge, a pressure sensor, a force sensor, an inductive sensor such as an eddy current sensor, a resistive sensor, a capacitive sensor, an optical sensor, and/or any other suitable sensor for measuring one or more parameters of the end effector **602**. The sensors **638** may include one or more sensors.

The one or more sensors 638 may comprise a strain gauge, such as a micro-strain gauge, configured to measure the magnitude of the strain in the anvil 616 during a clamped 45 condition. The strain gauge provides an electrical signal whose amplitude varies with the magnitude of the strain. The sensors 638 may comprise a pressure sensor configured to detect a pressure generated by the presence of compressed tissue between the anvil 616 and the staple cartridge 618. 50 The sensors 638 may be configured to detect impedance of a tissue section located between the anvil 616 and the staple cartridge 618 that is indicative of the thickness and/or fullness of tissue located therebetween.

The sensors **638** may be configured to measure forces 55 exerted on the anvil **616** by the closure drive system. For example, one or more sensors **638** can be at an interaction point between the closure tube **1910** (FIGS. **1-4**) and the anvil **616** to detect the closure forces applied by the closure tube **1910** to the anvil **616**. The forces exerted on the anvil **60 616** can be representative of the tissue compression experienced by the tissue section captured between the anvil **616** and the staple cartridge **618**. The one or more sensors **638** can be positioned at various interaction points along the closure drive system to detect the closure forces applied to 65 the anvil **616** by the closure drive system. The one or more sensors **638** may be sampled in real time during a clamping

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operation by a processor as described in FIGS. 16A-16B. The control circuit 610 receives real-time sample measurements to provide analyze time based information and assess, in real time, closure forces applied to the anvil 616.

A current sensor 636 can be employed to measure the current drawn by the motor 604. The force required to advance the I-beam 614 corresponds to the current drawn by the motor 604. The force is converted to a digital signal and provided to the control circuit 610.

The RF energy source 400 is coupled to the end effector 602 and is applied to the RF cartridge 609 when the RF cartridge 609 is loaded in the end effector 602 in place of the staple cartridge 618. The control circuit 610 controls the delivery of the RF energy to the RF cartridge 609.

Electrosurgical instruments apply electrosurgical energy to seal tissue. However, at times tissue may be sealed with staples delivered by a staple cartridge and at other times the tissue may be sealed by the application of electrosurgical energy. This requires the user to inventory two separate instruments. Therefore, it would be desirable to provide an elongate shaft for use with a surgical stapler where an interchangeable RF cartridge is used in place of a staple cartridge. In situations where an interchangeable RF cartridge is used in place of a staple cartridge, the present disclosure provides various techniques for covering select surfaces with non-conductive coatings to determine the electrical path of radio frequency (RF) applied energy when the interchangeable RF cartridges is used in place of the staple cartridge.

FIG. 19 is a perspective view of a surgical system 4000. The surgical system 4000 is similar to the motor-driven surgical system 10 in that the surgical system 4000 is configured to be used in connection with the conventional surgical stapler/fastener cartridges 1400 and the radio-frequency cartridges 1700. However, the surgical system 4000 is different from the motor-driven surgical system 10 in that the surgical system 4000 is also configured to be used in connection with radio-frequency cartridges 4002 which are similar to but different from the radio-frequency cartridges 1700 and are described in more detail below. The surgical system 4000 is also different from the motor-driven surgical system 10 in that the surgical system 4000 includes a firing system 4004 (See FIG. 22) which is similar to but different from the firing system 1300 of the motor driven surgical system 10 and is described in more detail below.

As shown in FIG. 19, the surgical system 4000 includes a handle assembly 4006 and an interchangeable tool assembly 4008 coupleable to the handle assembly 4006. The handle assembly 4006 is similar or identical to the handle assembly 500 and the interchangeable tool assembly 4008 is similar or identical to the interchangeable tool assembly 1000. The interchangeable tool assembly 4008 includes an end effector 4010 which includes a first jaw 4012 and a second jaw 4014. The first jaw 4012 includes an elongate channel 4016 which is configured to removably support the radio-frequency cartridge 4002. According to various aspects, the elongate channel 4016 may also be configured to removably support the surgical stapler/fastener cartridge 1400 and the radio frequency cartridge 1700. The second jaw 4014 includes an anvil 4018. The end effector 4010 is similar or identical to the end effector 1500, the first jaw 4012 is similar or identical to the first jaw 1600, the second jaw 4014 is similar or identical to the second jaw 1800, the elongate channel 4016 is similar or identical to the elongate channel 1602 and the anvil 4018 is similar or identical to the anvil **1810**.

FIG. 20 is a partial cross-section of the end effector 4010 of the surgical system 4000 according to various aspects, showing the interface between the radio-frequency cartridge 4002 and the anvil 4018 when the end effector 4010 in a fully closed position. For purposes of clarity, the elongate 5 channel **4016** is not shown in FIG. **20**. The radio-frequency cartridge 4002 is similar to the radio frequency cartridge 1700 but is different in that the radio-frequency cartridge 4002 includes a cartridge deck surface 4020 which defines at least two protrusions 4022. Although only one of the 10 protrusions 4022 is shown in the cross-section of FIG. 20, it will be appreciated that a first one of the protrusions 4022 is positioned on one side of a centrally disposed elongate slot 4024 of the radio-frequency cartridge 4002 and a second one of the protrusions **4022** is positioned on the opposite side of 15 the centrally disposed elongate slot 4024 of the radiofrequency cartridge 4002 (See, e.g., FIG. 21).

The radio-frequency cartridge 4002 is also different from the radio frequency cartridge 1700 in that the radio-frequency cartridge 4002 includes insulative sheath members 20 4026 which respectively define protrusions 4028 which are associated with the protrusions 4022. Although only one of the insulative sheath members 4026 and one of the protrusions 4028 are shown in the cross-section of FIG. 20, it will be appreciated that a first one of the insulative sheath 25 members 4026 and a first one of the protrusions 4028 are positioned on one side of the centrally disposed elongate slot 4024 of the radio-frequency cartridge 4002, and a second one of the insulative sheath members 4026 and a second one of the protrusions 4028 are positioned on the opposite side 30 of the centrally disposed elongate slot 4024 of the radiofrequency cartridge 4002 (See, e.g., FIG. 21). The protrusions 4028 are positioned between the protrusions 4022 of the cartridge deck surface 4020 and the anvil 4018 of the interchangeable tool assembly 4008.

The radio-frequency cartridge 4002 is also different from the radio frequency cartridge 1700 in that the radio-frequency cartridge 4002 further includes flexible circuit assemblies 4030 which respectively define protrusions 4032 which are associated with the protrusions 4022 and the 40 protrusions 4028. Although only one of the flexible circuit assemblies 4030 and one of the protrusions 4032 are shown in the cross-section of FIG. 20, it will be appreciated that a first one of the flexible circuit assemblies 4030 and a first one of the protrusions 4032 are positioned on one side of the 45 centrally disposed elongate slot **4024** of the radio-frequency cartridge 4002, and a second one of the flexible circuit assemblies 4030 and a second one of the protrusions 4032 are positioned on the opposite side of the centrally disposed elongate slot 4024 of the radio-frequency cartridge 4002 50 (See, e.g., FIG. 21). The protrusions 4032 are positioned between the protrusions 4028 and the anvil 4020 of the interchangeable tool assembly 4004. Other than the protrusions 4022, 4028, 4032, the cartridge deck surface 4020 is similar to the cartridge deck surface 1711, the insulative 55 sheath members 4026 are similar to the insulator/sheath members 1734, and the flexible circuit assemblies 4030 are similar to the flexible circuit assemblies 1730.

When tissue T (FIG. 6) is positioned between the radio-frequency cartridge 4002 and the anvil 4018, and the anvil 4018 is moved towards the radio-frequency cartridge 4002 to clamp the tissue positioned between the radio-frequency cartridge 4002 and the anvil 4018, the minimum gap or distance d₁ between the anvil 4018 and the radio-frequency staple cartridge 4002 proximate the distal end of the end 65 effector 4010 is realized when the insulation material 1819 positioned on the tissue facing segments 1817 of the fastener

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forming undersurface **1813** of the anvil **4018** is brought into physical contact with the protrusions **4032**. Once this physical contact between the insulation material **1819** and the protrusions **4032** is established, the protrusions **4032** physically prevent (1) the anvil **4018** from being brought closer to the radio-frequency cartridge **4002** and (2) the tissue from being further compressed. The establishment of this minimum gap or distance d₁ also operates to help prevent the formation of an electrical short circuit between the radio-frequency cartridge **4002** and the anvil **4018**.

An example of an RF cartridge that routes RF energy through tissue from an electrode to an inner surface of a staple pocket is shown in FIGS. 6 and 7. Accordingly, turning briefly to FIGS. 6 and 7, there is shown a partial cross-sectional view of the end effector 1500 depicted in FIGS. 1-5 supporting an RF cartridge 1700 (FIGS. 10-12), 4002 (FIGS. 19 and 21) therein and with tissue T clamped between the cartridge 1400 (FIG. 4) and the anvil 1810 and a partial cross-sectional view of the anvil 1810. In the example illustrated in FIGS. 6 and 7, the anvil 1810 comprises non-conductive masking except in pockets 1814 such that all of the surfaces not for staple formation are masked off and coated with a non-conductive electrically insulative material 1819 creating a varying return path surface containing dimples and extension minimizing the charring and tissue sticking experienced by flat opposed electrodes. As shown in FIG. 6, in at least one form, the anvil 1810 includes an anvil body portion 1812 that is fabricated from an electrically conductive metal material for example and has a staple forming undersurface 1813 that has a series of fastener forming pockets **1814** formed therein on each side of a centrally disposed anvil slot 1815 that is configured to slidably accommodate the knife member 1330 (FIGS. 2-4, 22) therein. The anvil slot 1815 opens into an upper opening 35 **1816** that extends longitudinally through the anvil body to accommodate the anvil engagement features 1336 (FIG. 4) on the knife member 1330 during firing. When a conventional mechanical surgical staple/fastener cartridge 1400 (FIG. 4) is installed in the elongate channel 1602 (FIG. 4), the staples/fasteners are driven into forming contact with the corresponding fastener forming pockets **1814**. The anvil body **1812** may have an opening in the upper portion thereof to facilitate ease of installation for example. An anvil cap **1818** may be inserted therein and welded to the anvil body **1812** to enclose the opening and improve the overall stiffness of the anvil body 1812. As shown in FIG. 7, to facilitate use of the end effector 1500 (FIGS. 1 and 2) in connection with RF cartridges 1700, 4002 the tissue facing segments 1817 of the fastener forming undersurface 1813 may have electrically insulative material 1819 thereon. Accordingly, the features described in reference to FIGS. 6 and 7 can be applied to the end effector 4010 (FIGS. 19 and 21) and the RF cartridge 4002 (FIGS. 19-21).

FIG. 21 is a partial perspective view of the radio-frequency cartridge 4002 supported by the elongate channel 4016 according to various aspects. As described above, the radio-frequency cartridge 4002 includes flexible circuit assemblies 4030 and protrusions 4032 on each side of the centrally disposed elongate slot 4024. For purposes of clarity, the insulative sheath members 4026 are not shown in FIG. 21. Additionally, it will be appreciated that the protrusions 4022, 4028 are hidden from view in FIG. 21.

FIG. 22 is an exploded perspective assembly view of portions of the handle assembly 4006 and the interchangeable tool assembly 4008 according to various aspects. The handle assembly 4006 is similar or identical to the handle assembly 500. The interchangeable tool assembly 4008 is

similar to the interchangeable tool assembly 1000, but is different in that the portion of the firing system 4004 associated with the interchangeable tool assembly 4008 is different from the portion of the firing system 1300 associated with the interchangeable tool system 1000. The portion 5 of the firing system 4004 associated with the handle assembly 4006 is similar or identical to the portion of the firing system 1300 associated with the handle assembly 500. The portion of the firing system 4004 associated with the handle assembly 4006 includes a firing drive system 4034 which 10 includes a longitudinal drive member 4036. The longitudinal drive member 4036 has a rack of teeth 4038 formed thereon and has an attachment cradle 4040 on its distal end. The firing drive system 4034, the longitudinal drive member 4036, the rack of teeth 4038 and the attachment cradle 4040 15 are similar or identical to the firing drive system 530, the longitudinal drive member 540, the rack of teeth 542 and the attachment cradle **544** of the firing system **1300**.

The portion of the firing system 4004 associated with the interchangeable tool assembly 4008 includes a nozzle 20 assembly 4042, an intermediate firing shaft portion 4044, a firing shaft attachment lug 4046, a knife bar 4043, a firing member/knife member 4050 and a proximal closure tube 4054 which are similar or identical to the nozzle assembly **1240**, the intermediate firing shaft portion **1310**, the firing 25 shaft attachment lug 1314, the knife bar 1320, the firing member/knife member 1330 and the proximal closure tube **1910**. However, the portion of the firing system **4004** associated with the interchangeable tool assembly 4008 is different from the portion of the firing system 1300 associated with the interchangeable tool assembly 1000 in that the portion of the firing system 4004 associated with the interchangeable tool assembly 4008 further includes an electrically insulative material 4056 (an electrically non-conductive material) which operates to prevent radio-frequency 35 energy from inadvertently passing from the portion of the firing system 4004 associated with the interchangeable tool assembly 4008 to the handle assembly 4006. In situations where radio-frequency energy is applied to the surgical instrument 4000, the firing member/knife member 4050 may 40 conduct radio-frequency energy. Without the electrically insulative material 4056, the firing member/knife member 4050 may inadvertently conduct radio-frequency energy through the knife bar 4043, through the intermediate firing shaft portion 4044 and/or through the firing shaft attachment 45 lug 4046 to the portion of the firing system 4004 associated with the handle assembly 4006.

According to various aspects, the electrically insulative material 4056 is a coating which covers the firing shaft attachment lug 4046. When the firing shaft attachment lug 50 4046 is seated into the attachment cradle 4040 within the handle assembly 4006, electrically insulative material 4056 operates to electrically isolate the longitudinal drive member 4036 of the firing drive system 4034 and the handle assembly 4006 from the interchangeable tool assembly 4008. In 55 other words, the longitudinal drive member 4036 and the handle assembly 4006 are protected from receiving inadvertent radio-frequency energy from the interchangeable tool assembly 4008. According to other aspects, the electrically insulative material 4056 may also cover other portions 60 of the firing system 4004 to electrically isolate the longitudinal drive member 4036 and the handle assembly 4006 from the interchangeable tool assembly 4008. For example, the electrically insulative material 4056 may also cover other portions of a proximal end **4058** of intermediate firing 65 shaft portion 4044. Thus, by selectively covering various portions of the firing system 4004 associated with the

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interchangeable tool assembly 4008 with the electrically insulative material 4056, the conductive path of radio-frequency energy can be designed to electrically isolate the handle assembly 4006 from the interchangeable tool assembly 4008 for instances where the radio-frequency cartridge 1700 or the radio-frequency cartridge 4002 is being utilized with the surgical system 4000.

Aspects of the surgical instrument may be practiced without the specific details disclosed herein. Some aspects have been shown as block diagrams rather than detail. Parts of this disclosure may be presented in terms of instructions that operate on data stored in a computer memory. Generally, aspects described herein which can be implemented, individually and/or collectively, by a wide range of hardware, software, firmware, or any combination thereof can be viewed as being composed of various types of "electrical circuitry." Consequently, "electrical circuitry" includes electrical circuitry having at least one discrete electrical circuit, electrical circuitry having at least one integrated circuit, electrical circuitry having at least one application specific integrated circuit, electrical circuitry forming a general purpose computing device configured by a computer program (e.g., a general purpose computer or processor configured by a computer program, which at least partially carries out processes and/or devices described herein), electrical circuitry forming a memory device (e.g., forms of random access memory), and/or electrical circuitry forming a communications device (e.g., a modem, communications switch, or optical-electrical equipment). These aspects may be implemented in analog or digital form, or combinations thereof.

The foregoing description has set forth aspects of devices and/or processes via the use of block diagrams, flowcharts, and/or examples, which may contain one or more functions and/or operation. Each function and/or operation within such block diagrams, flowcharts, or examples can be implemented, individually and/or collectively, by a wide range of hardware, software, firmware, or virtually any combination thereof. In one aspect, several portions of the subject matter described herein may be implemented via Application Specific Integrated Circuits (ASICs), Field Programmable Gate Arrays (FPGAs), digital signal processors (DSPs), Programmable Logic Devices (PLDs), circuits, registers and/or software components, e.g., programs, subroutines, logic and/or combinations of hardware and software components, logic gates, or other integrated formats. Some aspects disclosed herein, in whole or in part, can be equivalently implemented in integrated circuits, as one or more computer programs running on one or more computers (e.g., as one or more programs running on one or more computer systems), as one or more programs running on one or more processors (e.g., as one or more programs running on one or more microprocessors), as firmware, or as virtually any combination thereof, and that designing the circuitry and/or writing the code for the software and or firmware would be well within the skill of one of skill in the art in light of this disclosure.

The mechanisms of the disclosed subject matter are capable of being distributed as a program product in a variety of forms, and that an illustrative aspect of the subject matter described herein applies regardless of the particular type of signal bearing medium used to actually carry out the distribution. Examples of a signal bearing medium include the following: a recordable type medium such as a floppy disk, a hard disk drive, a Compact Disc (CD), a Digital Video Disk (DVD), a digital tape, a computer memory, etc.; and a transmission type medium such as a digital and/or an analog communication medium (e.g., a fiber optic cable, a

waveguide, a electrical conductord communications link, a electrical conductorless communication link (e.g., transmitter, receiver, transmission logic, reception logic, etc.).

The foregoing description of these aspects has been presented for purposes of illustration and description. It is not intended to be exhaustive or limiting to the precise form disclosed. Modifications or variations are possible in light of the above teachings. These aspects were chosen and described in order to illustrate principles and practical application to thereby enable one of ordinary skill in the art to utilize the aspects and with modifications as are suited to the particular use contemplated. It is intended that the claims submitted herewith define the overall scope.

Various aspects of the subject matter described herein are set out in the following numbered examples:

Example 1. An interchangeable tool assembly, comprising: a first jaw configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period; a second jaw coupled to the first jaw, wherein a surface of the second jaw defines a plurality of staple forming pockets configured to form staples driven from the staple cartridge; and an electrically insulative material covering segments of the surface of the second jaw other than the staple forming pockets, wherein the staple forming pockets define at least one return path for radio-frequency energy delivered by the radio-frequency cartridge.

Example 2. The interchangeable tool assembly of Example 1, wherein the interchangeable tool assembly is configured to be releasably coupleable to a handle assembly, and wherein at least one component positioned within the interchangeable tool assembly comprises electrical insulation to electrically insulate the handle assembly from inadvertent radio-frequency energy from the interchangeable tool assembly.

Example 3. The interchangeable tool assembly of one or more of Example 1 through Example 2, wherein the interchangeable tool assembly is configured to be releasably 40 coupleable to a handle assembly, and wherein at least one component positioned within the interchangeable tool assembly comprises electrical insulation to electrically insulate the handle assembly from inadvertent radio-frequency energy from the interchangeable tool assembly.

Example 4. The interchangeable tool assembly of one or more of Example 1 through Example 3, wherein the plurality of staple forming pockets comprise: a first plurality of staple forming pockets positioned to a first side of a centrally disposed anvil slot; and a second plurality of staple forming pockets positioned to a second side of the centrally disposed anvil slot.

Example 5. The interchangeable tool assembly of one or more of Example 1 through Example 4, wherein the plurality of staple forming pockets provide for a plurality of different 55 return paths for radio-frequency energy delivered by the radio-frequency cartridge.

Example 6. The interchangeable tool assembly of one or more of Example 1 through Example 5, wherein the segments of the surface of the second jaw face the first jaw.

Example 7. The interchangeable tool assembly of one or more of Example 1 through Example 6, further comprising a firing system positioned within the interchangeable tool assembly, wherein the firing system is configured to couple to a handle assembly, wherein the firing system is electrically insulated to electrically insulate the handle assembly from inadvertent radio-frequency energy.

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Example 8. The interchangeable tool assembly of one or more of Example 1 through Example 7, further comprising a staple cartridge.

Example 9. The interchangeable tool assembly of one or more of Example 1 through Example 8, wherein the surgical system further comprises the radio-frequency cartridge.

Example 10. The interchangeable tool assembly of Example 9, wherein the radio-frequency cartridge comprises at least two protrusions which collectively provide for a minimum gap distance between the first and second jaws.

Example 11. A surgical tool assembly, comprising: an elongate channel configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period; and an anvil coupled to the elongate channel, wherein the anvil comprises: a surface which faces the elongate channel and defines a plurality of staple forming pockets configured to form staples driven from the staple cartridge; and an electrically insulative material which covers segments of the surface of the second jaw, wherein the plurality of staple forming pockets provide for a plurality of different return paths for radio-frequency energy delivered by the radio-frequency cartridge.

Example 12. The surgical tool assembly of Example 11, wherein the elongate channel and the anvil collectively form an end effector.

Example 13. The surgical tool assembly of one or more of Example 11 through Example 12, wherein the plurality of staple forming pockets comprise: a first plurality of staple forming pockets positioned to a first side of a centrally disposed anvil slot; and a second plurality of staple forming pockets positioned to a second side of the centrally disposed anvil slot.

Example 14. The surgical tool assembly of one or more of Example 11 through Example 13, wherein the segments of the surface of the second jaw are other than the staple forming pockets.

Example 15. The surgical tool assembly of one or more of Example 11 through Example 14, wherein the surgical tool assembly further comprises the staple cartridge.

Example 16. The surgical tool assembly of one or more of Example 11 through Example 15, wherein the surgical tool assembly further comprises the radio-frequency cartridge.

Example 17. The surgical tool assembly of Example 16, wherein the radio-frequency cartridge comprises at least two protrusions which collectively provide for a minimum gap distance between the elongate channel and the anvil.

Example 18. An interchangeable tool assembly, comprising: an end effector configured to releasably couple to a shaft assembly, wherein the end effector comprises: an elongate channel configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period; and an anvil coupled to the elongate channel, wherein the anvil comprises an electrically insulative material and defines a plurality of different return paths for radio frequency energy delivered by the radio-frequency cartridge.

Example 19. The interchangeable tool assembly of Example 18, wherein the electrically insulative material faces the elongate channel.

Example 20. The interchangeable tool assembly of one or more of Example 18 through Example 19, further comprising the radio-frequency cartridge.

The invention claimed is:

1. An interchangeable tool assembly configured to be releasably coupleable to a handle assembly comprising a drive system, the interchangeable tool assembly comprising:

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- a first jaw configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period, wherein the first jaw defines an elongate channel defining a recess and configured to accommodate the staple cartridge and the radio-frequency cartridge, wherein the elongate channel comprises a flexible channel circuit positioned within the recess and configured to power the radio-frequency cartridge when the radio-frequency cartridge is installed in the elongate channel, wherein the flexible to channel circuit comprises an exposed contact that extends out of the recess and is folded over and directly attached to an upper edge of the elongate channel;
- a second jaw coupled to the first jaw, wherein the second jaw comprises an outer tissue contacting surface and a plurality of staple forming pockets configured to form staples driven from the staple cartridge, wherein each staple forming pocket of the plurality of staple forming pockets comprises an inner staple forming surface;
- a first electrically insulative material covering segments 20 of the outer tissue contacting surface of the second jaw outside the staple forming pockets, wherein the inner staple forming surface of at least one of the staple forming pockets is electrically conductive and defines a return path for radio-frequency energy delivered by 25 the radio-frequency cartridge;
- a shaft member configured to be moved axially within the interchangeable tool assembly, the shaft member comprising an attachment portion, the attachment portion configured to engage the drive system of the handle 30 assembly; and
- a second electrically insulative material covering the attachment portion, the second electrically insulative material configured to electrically insulate the interchangeable tool assembly from the handle assembly.
- 2. The interchangeable tool assembly of claim 1, wherein the plurality of staple forming pockets comprise:
 - a first plurality of staple forming pockets positioned to a first side of a centrally disposed anvil slot; and
 - a second plurality of staple forming pockets positioned to 40 a second side of the centrally disposed anvil slot.
- 3. The interchangeable tool assembly of claim 1, wherein the segments of the outer tissue contacting surface of the second jaw face the first jaw.
- 4. The interchangeable tool assembly of claim 1, further 45 comprising the staple cartridge.
- 5. The interchangeable tool assembly of claim 1, further comprising the radio-frequency cartridge.
- 6. The interchangeable tool assembly of claim 5, wherein the radio-frequency cartridge comprises at least two protrusions which collectively provide for a minimum gap distance between the first and second jaws.
- 7. A surgical tool assembly configured to be releasably coupleable to a handle assembly comprising a drive system, the surgical tool assembly comprising:
 - an elongate channel configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period, wherein the elongate channel defines a recess, wherein a flexible channel circuit is positioned within the recess and 60 comprises an exposed contact that extends out of the recess and is folded over and directly attached to an upper edge of the elongate channel, and wherein the flexible channel circuit is configured to power the radio-frequency cartridge when the radio-frequency 65 cartridge is supported by the elongate channel and in electrical communication with the exposed contact;

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- an anvil coupled to the elongate channel, wherein the anvil comprises:
 - an outer tissue contacting surface which faces the elongate channel;
 - a plurality of staple forming pockets configured to form staples driven from the staple cartridge, wherein each staple forming pocket of the plurality of staple forming pockets comprises an inner staple forming surface; and
 - a first electrically insulative material which covers segments of the outer tissue contacting surface of the anvil outside the staple forming pockets, wherein the inner staple forming surfaces are electrically conductive and provide for a plurality of different return paths for radio-frequency energy delivered by the radio-frequency cartridge;
- a shaft member configured to be moved axially within the surgical tool assembly, the shaft member comprising an attachment portion, the attachment portion configured to engage the drive system of the handle assembly; and
- a second electrically insulative material covering the attachment portion, the second electrically insulative material configured to electrically insulate the surgical tool assembly from the handle assembly.
- 8. The surgical tool assembly of claim 7, wherein the elongate channel and the anvil collectively form an end effector.
- 9. The surgical tool assembly of claim 7, wherein the plurality of staple forming pockets comprise:
 - a first plurality of staple forming pockets positioned to a first side of a centrally disposed anvil slot; and
 - a second plurality of staple forming pockets positioned to a second side of the centrally disposed anvil slot.
- 10. The surgical tool assembly of claim 7, wherein the surgical tool assembly further comprises the staple cartridge.
 - 11. The surgical tool assembly of claim 7, wherein the surgical tool assembly further comprises the radio-frequency cartridge.
 - 12. The surgical tool assembly of claim 11, wherein the radio-frequency cartridge comprises at least two protrusions which collectively provide for a minimum gap distance between the elongate channel and the anvil.
 - 13. An interchangeable tool assembly configured to be releasably coupleable to a handle assembly comprising a drive system, the interchangeable tool assembly comprising: a circuit board;
 - an end effector configured to releasably couple to a shaft assembly, wherein the end effector comprises:
 - an elongate channel configured to support a staple cartridge during a first time period and a radio-frequency cartridge during a second time period, wherein the elongate channel comprises a flexible channel circuit configured to electrically couple the radio-frequency cartridge to the circuit board when the radio-frequency cartridge is supported by the elongate channel; and
 - an anvil coupled to the elongate channel, wherein the anvil comprises an outer surface that faces the elongate channel, an inner surface that does not face the elongate channel, and a first electrically insulative material that covers at least a portion of the outer surface of the anvil, wherein the inner surface is electrically conductive and defines a plurality of different return paths for radio-frequency energy delivered by the radio-frequency cartridge;
 - a shaft member configured to be moved axially within the interchangeable tool assembly to actuate the end effec-

tor, the shaft member comprising an attachment portion, the attachment portion configured to engage the

drive system of the handle assembly; and

a second electrically insulative material covering the attachment portion, the second electrically insulative 5 material configured to electrically insulate the interchangeable tool assembly from the handle assembly,

wherein the elongate channel defines a recess, wherein a majority of the flexible channel circuit is positioned within the recess, and wherein the flexible channel 10 circuit comprises an exposed contact that extends out of the recess and is folded over and directly attached to an upper edge of the elongate channel.

14. The interchangeable tool assembly of claim 13, fur- $_{15}$ ther comprising the radio-frequency cartridge.

15. The interchangeable tool assembly of claim 13, wherein the circuit board comprises a radio-frequency circuit, and wherein the flexible channel circuit is configured to electrically couple the radio-frequency cartridge to the **36**

radio-frequency circuit when the radio-frequency cartridge is supported by the elongate channel.

16. The interchangeable tool assembly of claim **13**, further comprising the radio-frequency cartridge, wherein the radio-frequency cartridge comprises a cartridge body comprising an electrode pad defining an elongate slot, wherein the elongate slot divides the electrode pad into a first pad segment and a second pad segment.

17. The interchangeable tool assembly of claim 16, wherein a first flexible circuit assembly is attached to the first pad segment, wherein a second flexible circuit assembly is attached to the second pad segment.

18. The interchangeable tool assembly of claim 17, wherein the first flexible circuit assembly comprises a first electrode and a second electrode configured for different phases of operation, and wherein the first flexible circuit assembly comprises a circuit width that is greater than an electrode width of the first electrode and the second electrode.