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# (54) METHODS AND SYSTEMS FOR UTILIZING MILLIMETER-WAVE RADIO COMPONENTS IN SYNTHESIZING MICROWAVE SIGNALS

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H04B 15/00 (2006.01)

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H04B 1/40 (2015.01)

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(58) Field of Classification Search

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See application file for complete search history.

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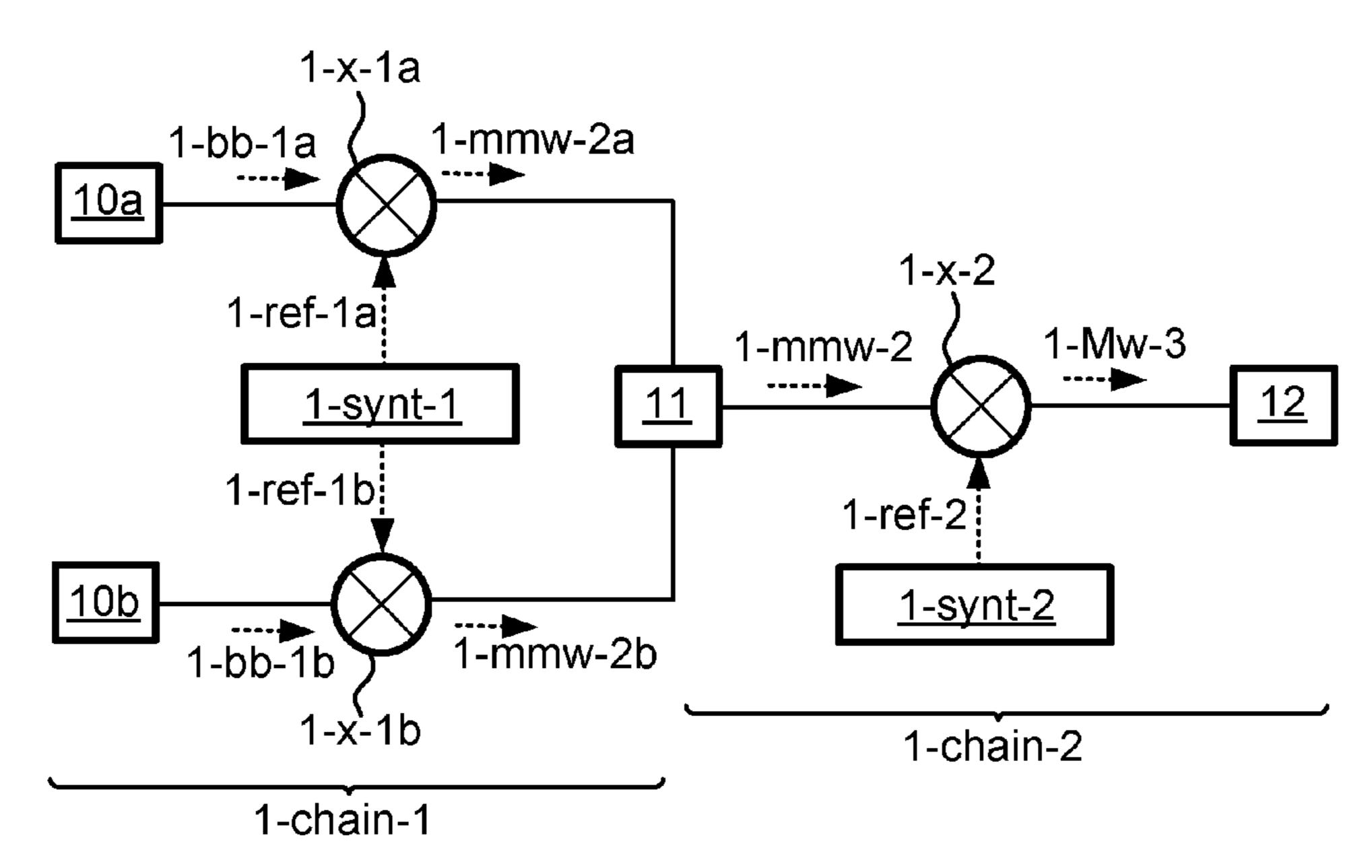
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### (57) ABSTRACT

Systems and methods for utilizing millimeter-wave radio components in synthesizing microwave signals. A first upconversion frequency generated using millimeter-wave radio components is used to up-convert a baseband signal into a first millimeter-wave signal, which is then down-converted into a microwave signal using a second and lower down-conversion frequency generated using additional millimeter-wave radio components. Using millimeter-wave conversion frequencies allows for tight integration of multiple transmission and reception chains while facilitating good coexistence of different microwave channels, and further allows for a wide span of frequencies over which microwave transmissions can be made.

### 21 Claims, 3 Drawing Sheets



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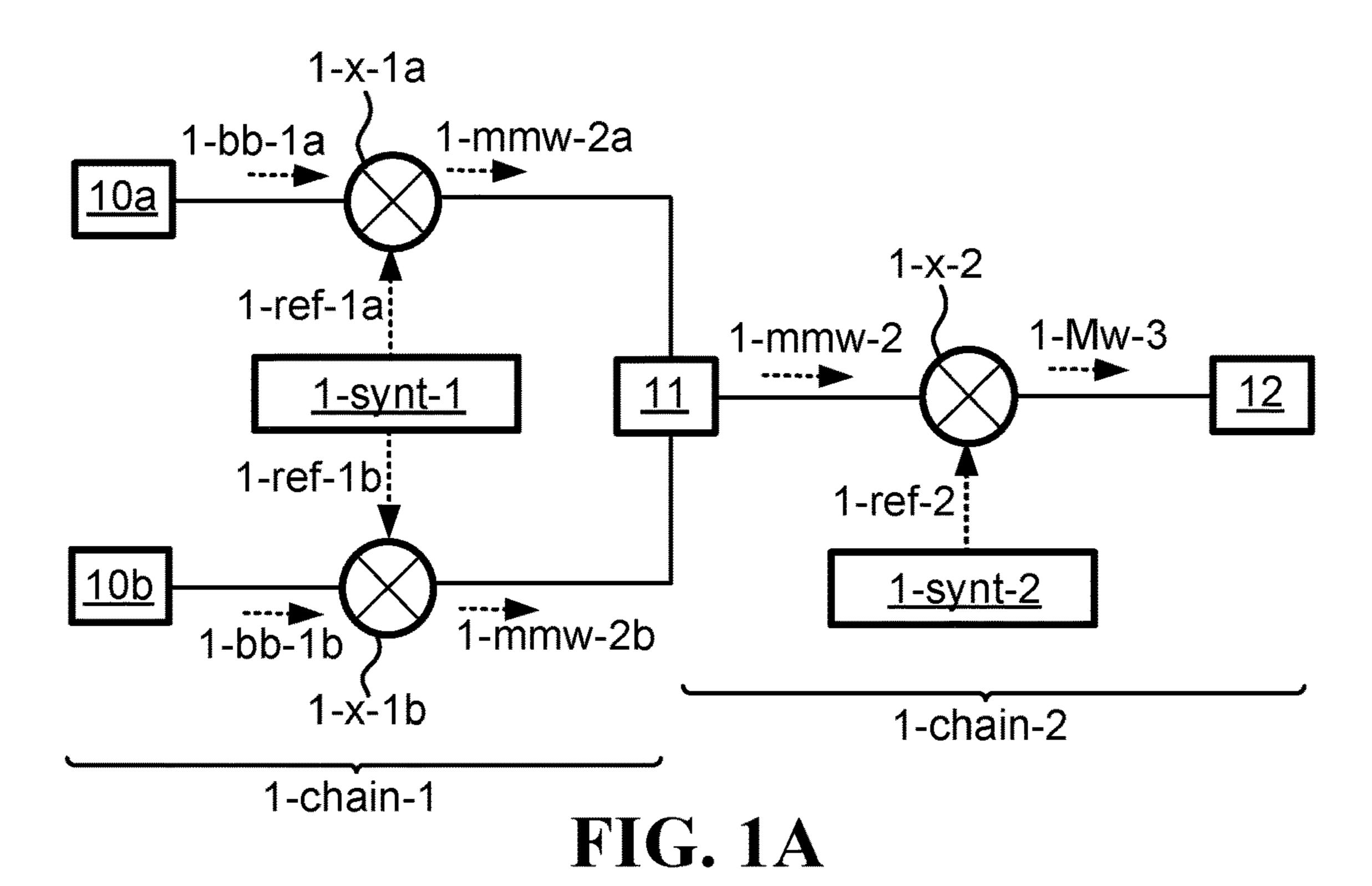
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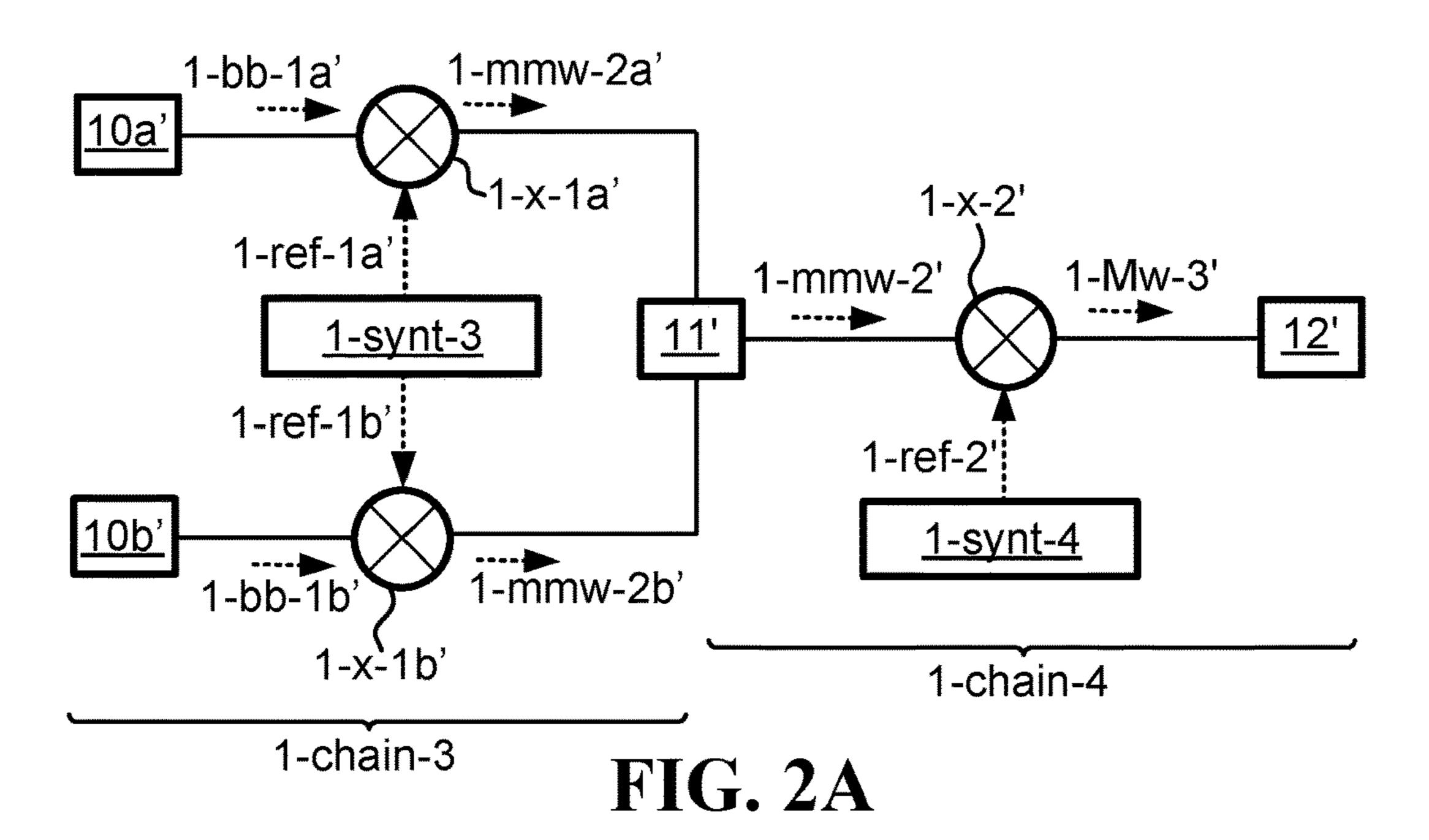
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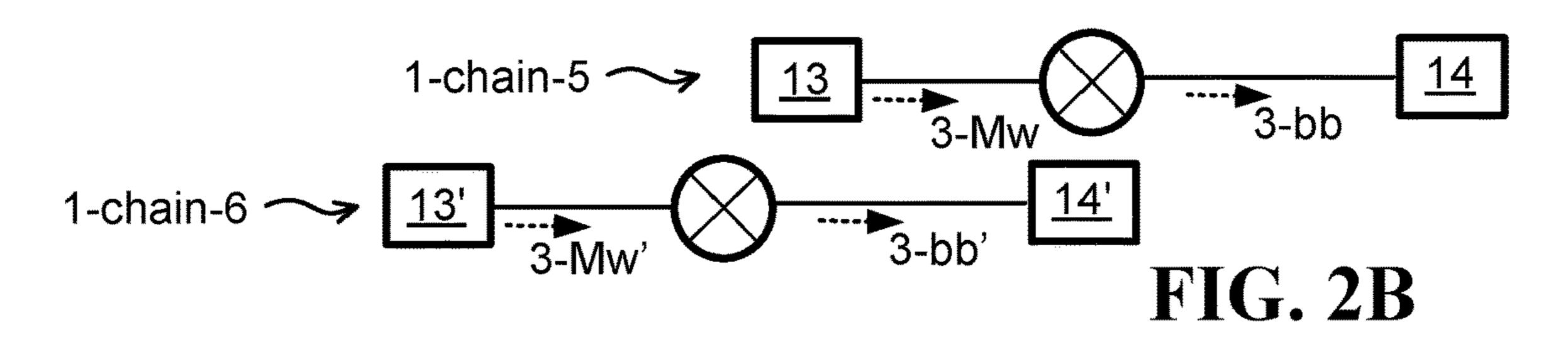
2-span'
2-span'
2-differential
2-differential
1-ref-2
1-mmw-2
Prequency

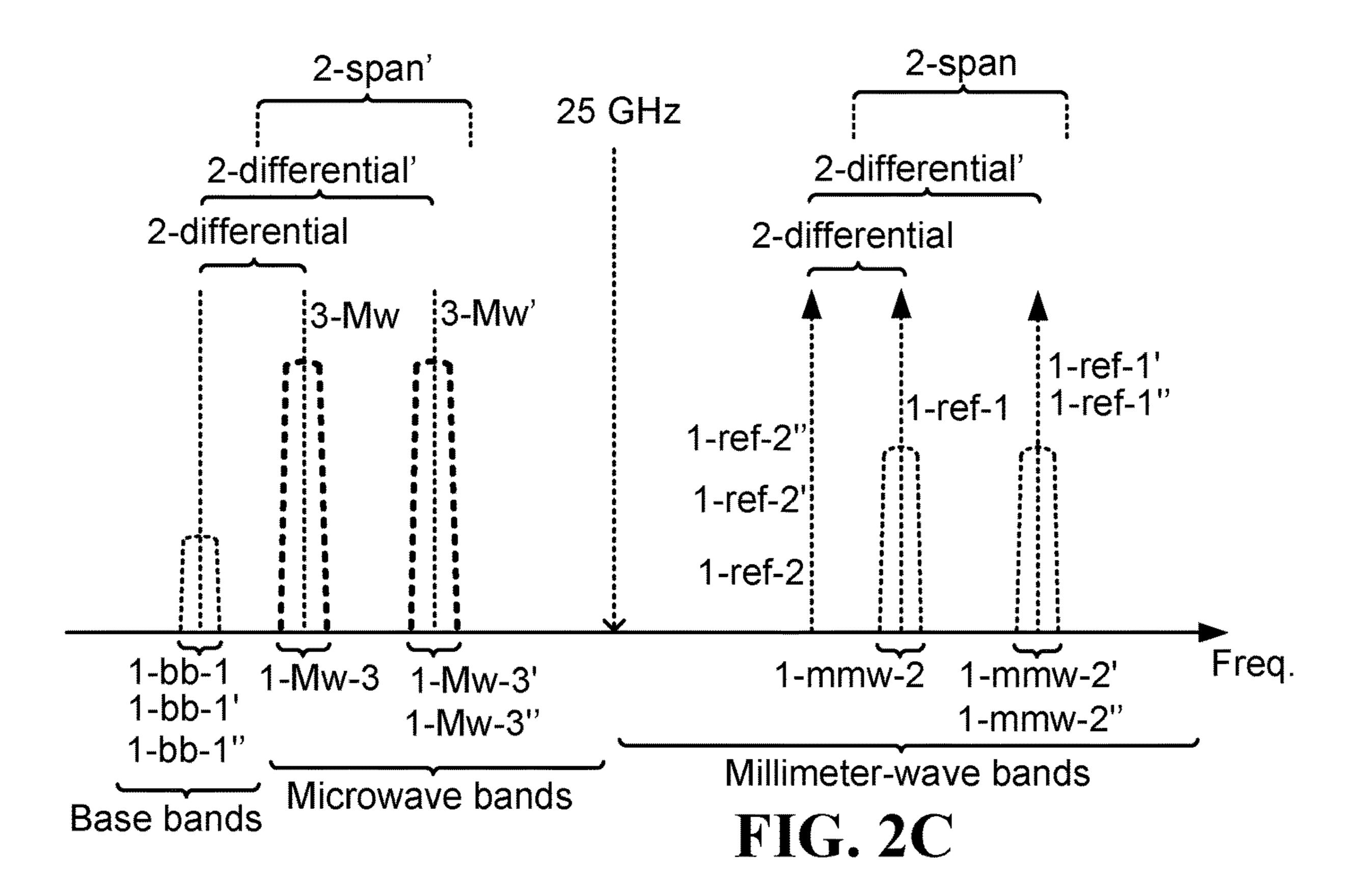
Millimeter-wave bands

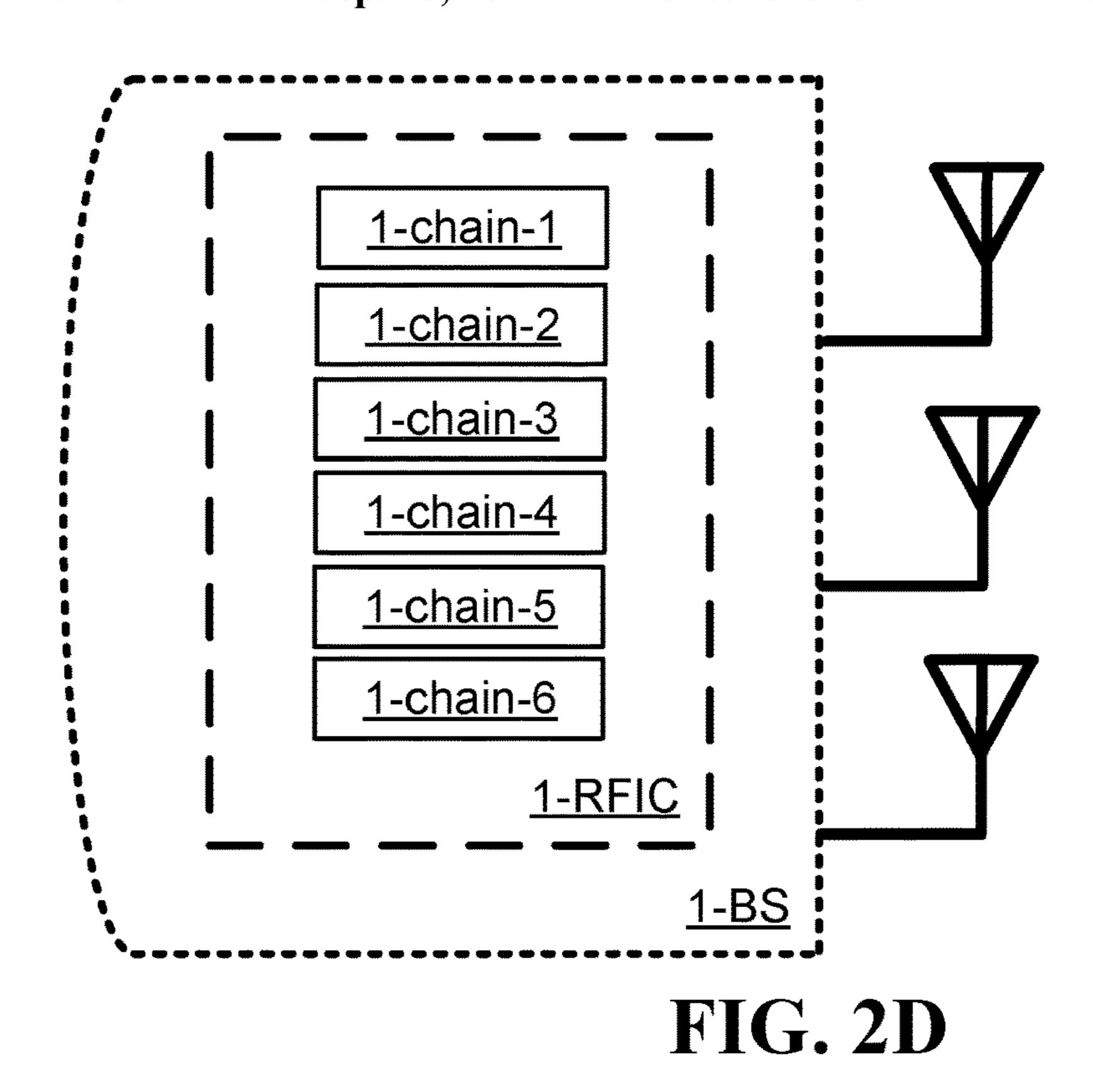
FIG. 1B



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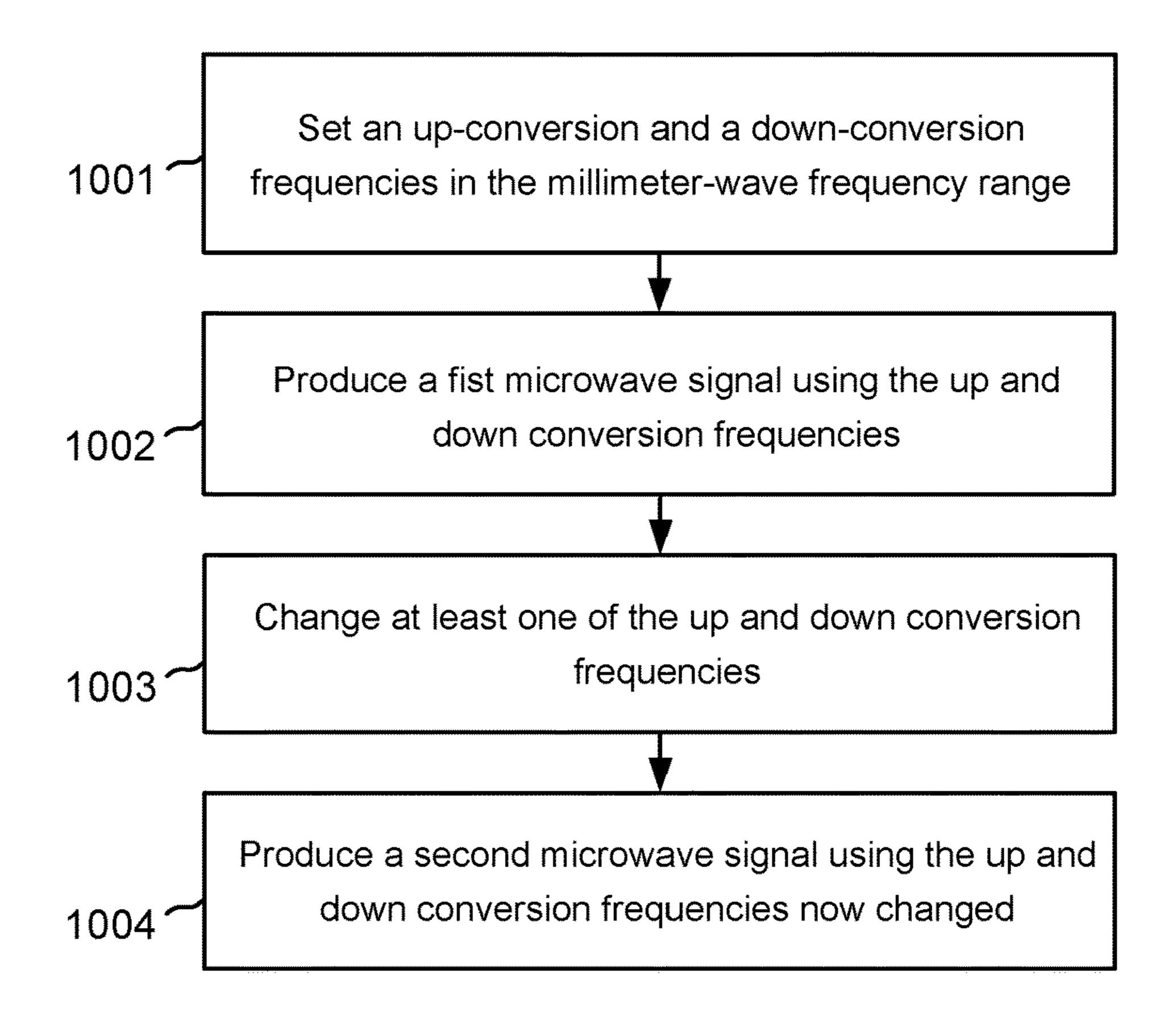


FIG. 3

# METHODS AND SYSTEMS FOR UTILIZING MILLIMETER-WAVE RADIO COMPONENTS IN SYNTHESIZING MICROWAVE SIGNALS

### BACKGROUND

In wireless communication systems, such as microwave systems, a transmission signal is generated by up-converting a base-band signal into a microwave signal, in which such up conversion is done using a single or multiple up-conversion frequencies in the microwave range. Using up-conversion frequencies in the microwave range may interfere with the operation of other nearby or co-located microwave channels, and may further or otherwise restrict the span of frequencies over which transmission of microwave signals 15 can be made.

#### **SUMMARY**

One embodiment is a system operative to use millimeter- 20 wave radio components to generate microwave signals over a wide frequency range. The system includes: a first millimeter-wave chain operative to up-convert signals from a baseband frequency into a millimeter-wave frequency; a second millimeter-wave chain operative to down-convert 25 signals from a millimeter-wave frequency into a microwave frequency; and at least a first programmable millimeterwave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is settable over a span of at least 1 GHz (one gigahertz). In one embodiment 30 the system is configured to: use the at least first programmable millimeter-wave oscillator to set a specific exact frequency differential between an up-conversion frequency associated with the first millimeter-wave chain and a downconversion frequency associated with the second millimeterwave chain, in which said specific exact frequency differential is therefore settable over a span of at least 1 GHz (one gigahertz); receive a first signal in a baseband frequency; use the first millimeter-wave chain, in conjunction with said up-conversion frequency, to up-convert the first signal from 40 said baseband frequency into a millimeter-wave frequency, thereby producing a millimeter-wave version of the first signal; and use the second millimeter-wave chain, in conjunction with said down-conversion frequency, to downconvert the millimeter-wave version of the first signal into a 45 microwave version of the first signal having a characteristic frequency that is therefore settable over a span of at least 1 GHz (one gigahertz).

One embodiment is a method for using millimeter-wave radio components for generating microwave signals over a 50 wide frequency range. The method includes: setting a specific first up-conversion frequency and a specific first downconversion frequency using at least a first programmable millimeter-wave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is 55 settable over a span of at least 1 GHz (one gigahertz); up-converting a first signal from a baseband frequency into a millimeter-wave frequency using the specific first upconversion frequency, thereby producing a millimeter-wave version of the first signal, and then down-converting the 60 millimeter-wave version of the first signal using the specific first down-conversion frequency, thereby producing a microwave version of the first signal characterized by a particular first frequency that is equal to the difference between said specific first up-conversion frequency and said 65 specific first down-conversion frequency; setting at least one of: (i) a specific second up-conversion frequency and (ii) a

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specific second down-conversion frequency using at least the first programmable millimeter-wave oscillator; and upconverting a second signal from the baseband frequency into a millimeter-wave frequency using the specific second upconversion frequency, thereby producing a millimeter-wave version of the second signal, and then down-converting the millimeter-wave version of the second signal using the specific second down-conversion frequency, thereby producing a microwave version of the second signal characterized by a particular second frequency that is equal to the difference between said specific second up-conversion frequency and said specific second down-conversion frequency, in which the particular second frequency varies by at least 1 GHz (one gigahertz) from the particular first frequency as a result of said span.

### BRIEF DESCRIPTION OF THE DRAWINGS

The embodiments are herein described by way of example only, with reference to the accompanying drawings. No attempt is made to show structural details of the embodiments in more detail than is necessary for a fundamental understanding of the embodiments. In the drawings:

FIG. 1A illustrates one embodiment of a first millimeterwave chain operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and a second millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency;

FIG. 1B illustrates one embodiment of a millimeter-wave signal having a certain characteristic frequency that is settable over a certain frequency span and a microwave signal derived from the millimeter-wave signal and thus having a certain characteristic frequency that is settable over a similar frequency span;

FIG. 2A illustrates one embodiment of a third millimeterwave chain operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and a fourth millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency;

FIG. 2B illustrates one embodiment of a fifth radiofrequency (RF) chain operative to receive a first microwave signal and a sixth RF chain operative to receive a second microwave signal;

FIG. 2C illustrates one embodiment of two millimeterwave signals having two different characteristic frequencies that are settable over a certain frequency span and two microwave signals derived respectively from the two millimeter-wave signal and thus having two respective characteristic frequencies that are settable over a similar frequency span;

FIG. 2D illustrates one embodiment of a radio frequency integrated circuit (RFIC) containing all of the RF chains and belonging to a wireless base-station or an access point; and

FIG. 3 illustrates one embodiment of a method for using millimeter-wave radio components for generating microwave signals over a wide frequency range.

### DETAILED DESCRIPTION

FIG. 1A illustrates one embodiment of a first millimeter-wave chain 1-chain-1 operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and a second millimeter-wave chain 1-chain-2 operative to down-convert signals from a millimeter-wave frequency into a microwave frequency. A baseband signal 1-bb-1, which may

contain I/Q components comprising an in-phase component 1-bb-1a (I) and a quadrature component 1-bb-1b (Q), is up-converted by the first millimeter-wave chain 1-chain-1 to a millimeter-wave frequency, thereby producing a millimeter-wave version 1-mmw-2 (1-mmw-2a, 1-mmw-2b) of the baseband signal 1-bb-1, in which a millimeter-wave frequency is any frequency above 25 GHz (twenty five gigahertz) and below 300 GHz (three hundred gigahertz). The millimeter-wave version 1-mmw-2 of the baseband signal 1-bb-1 is then down-converted by the second millimeter- 10 wave chain 1-chain-2 into a microwave frequency, thereby producing a microwave version 1-Mw-3 of the baseband signal 1-bb-1, in which a microwave frequency is any frequency above 300 MHz (three hundred megahertz) and below 25 GHz (twenty five gigahertz). The actual up- 15 conversion may be achieved using mixers 1-x-1a, 1-x-1b, in which the reference signals to the mixers 1-ref-1a, 1-ref-1b may be produced by a first synthesizer/millimeter-wave oscillator 1-synt-1. The actual down-conversion may be achieved using another mixer 1-x-2, in which the reference 20 signal 1-ref-2 to such a mixer 1-x-2 may be produced by a second synthesizer/millimeter-wave oscillator 1-synt-2. The microwave version 1-Mw-3 of the baseband signal 1-bb-1 may be then transmitted wirelessly via a microwave antenna. Elements 10a, 10b, 11, and 12 represent various 25 radio frequency components such as filters, amplifiers/ power amplifiers, power combiners, antennas, or any other component that is usually used in conjunction with radio frequency transmission chains.

FIG. 1B illustrates one embodiment of a millimeter-wave 30 signal 1-mmw-2 having a certain characteristic frequency that is settable over a certain frequency span 2-span and a microwave signal 1-Mw-3 derived from the millimeterwave signal 1-mmw-2 and thus having a certain character-2-span'. Millimeter-wave signal 1-mmw-2, which is a millimeter-wave version of baseband signal 1-bb-1, is produces by the first millimeter-wave chain 1-chain-1 using reference signals 1-ref-1a, 1-ref-1b (collectively referred to as 1-ref-1) from the local millimeter-wave oscillator 1-synt-1. In one 40 embodiment, millimeter-wave oscillator 1-synt-1 is a programmable oscillator, and therefore the reference signal 1-ref-1 can be set over a certain span of frequencies 2-span. Since millimeter-wave oscillator 1-synt-1 operates in the millimeter-wave frequency range, and since the span of 45 frequencies associated with a programmable oscillator usually increases with operating frequency, then millimeterwave oscillator 1-synt-1 is expected to have a relatively large frequency span over which reference signal 1-ref-1 can be set. For example, if millimeter-wave oscillator 1-synt-1 operates around a nominal frequency of 60 GHz (sixty gigahertz), then millimeter-wave oscillator 1-synt-1 can be expected to produce a reference signal 1-ref-1 over a span of frequencies 2-span that is at least 5% (five percent) of the nominal frequency, and therefore reference signal 1-ref-1 55 can be expected to be settable over a span of frequencies 2-span of at least 3 GHz (three gigahertz), e.g., from 58.5 GHz (fifty eight point five gigahertz) to 61.5 (sixty one point five gigahertz). Consequently, the resultant millimeter-wave signal 1-mmw-2 has a characteristic frequency that is settable over the same frequency span 2-span of 3 GHz (three gigahertz). Microwave signal 1-Mw-3, which is a microwave version of baseband signal 1-bb-1, is produces by the second millimeter-wave chain 1-chain-2 using reference signal 1-ref-2 from the local millimeter-wave oscillator 65 1-synt-2 and using the millimeter-wave signal 1-mmw-2 as an input. Since millimeter-wave signal 1-mmw-2 has a

characteristic frequency that is settable over the frequency span 2-span of 3 GHz (three gigahertz) as an example, then consequently, the resultant microwave signal 1-Mw-3 will have a characteristic frequency that is also settable over a similar frequency span 2-span' of 3 GHz (three gigahertz). The characteristic frequency (also referred to as nominal or center frequency) of microwave signal 1-Mw-3 depends on the two reference signals 1-ref-1, 1-ref-2, and more specifically on the difference 2-differential between the frequencies of 1-ref-1 and 1-ref-2. For example, if reference signals 1-ref-1, 1-ref-2 have the frequencies of 61.5 GHz (sixty one point five gigahertz) and 57.9 GHz (fifty seven point nine gigahertz) respectively, then the resultant characteristic frequency of microwave signal 1-Mw-3 will be 3.6 GHz (three point six gigahertz), which happens to be in a microwave band used for 5G cellular communication. Now, according to the example above, since reference signal 1-ref-1 is settable over a span 2-span of 3 GHz (three gigahertz), then the frequency of 1-ref-1 can also be set to 58.5 GHz (fifty eight point five gigahertz), and in that case the resultant characteristic frequency of microwave signal 1-Mw-3 will be 600 MHz (six hundred megahertz), which happens to be in a much lower microwave band used for LTE cellular communication. Similarly, the resultant characteristic frequency of microwave signal 1-Mw-3 can be set, according to this example, to any frequency between 600 MHz (six hundred megahertz) and 3.6 GHz (three point six gigahertz), which practically covers the entire span 2-span' of all frequencies used by cellular radio access networks (RANs). This result is quite unusual, and is made possible due to the translation of the large frequency span 2-span possible with millimeter-wave components 1-synt-1, 1-x-1, 1-synt-2, 1-x-2 into an unusually wide frequency span 2-span' over which a microwave signal 1-Mw-3 can be transmitted. It is istic frequency that is settable over a similar frequency span 35 noted that in the above example the reference frequency 1-ref-1 changes while the reference frequency 1-ref-2 remains constant, but a similar effect can be achieved by keeping reference frequency 1-ref-1 constant and changing reference frequency 1-ref-2, or by changing both reference frequencies 1-ref-1 and 1-ref-2, as long as the frequency differential 2-differential places the microwave signal 1-Mw-3 in the appropriate microwave band.

FIG. 2A illustrates one embodiment of a third millimeterwave chain 1-chain-3 operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and a fourth millimeter-wave chain 1-chain-4 operative to downconvert signals from a millimeter-wave frequency into a microwave frequency. A baseband signal 1-bb-1' (1-bb-1a', 1-bb-1b') is up-converted by the third millimeter-wave chain 1-chain-3 to a millimeter-wave frequency, thereby producing a millimeter-wave version 1-mmw-2' (1-mmw-2a', 1-mmw-2b') of the baseband signal 1-bb-1'. The millimeterwave version 1-mmw-2' of the baseband signal 1-bb-1' is then down-converted by the fourth millimeter-wave chain 1-chain-4 into a microwave frequency, thereby producing a microwave version 1-Mw-3' of the baseband signal 1-bb-1'. The actual up-conversion may be achieved using mixers 1-x-1a', 1-x-1b', in which the reference signals to the mixers 1-ref-1a', 1-ref-1b' (together 1-ref-1') may be produced by a third synthesizer/millimeter-wave oscillator 1-synt-3. The actual down-conversion may be achieved using another mixer 1-x-2', in which the reference signal 1-ref-2' to such a mixer 1-x-2' may be produced by a fourth synthesizer/ millimeter-wave oscillator 1-synt-4. The microwave version 1-Mw-3' of the baseband signal 1-bb-1' may be then transmitted wirelessly via a microwave antenna. Elements 10a', 10b', 11', and 12' represent various radio frequency compo-

nents such as filters, amplifiers/power amplifiers, power combiners, antennas, or any other component that is usually used in conjunction with radio frequency transmission chains.

FIG. 2B illustrates one embodiment of a fifth radio- 5 frequency (RF) chain 1-chain-5 operative to receive a first microwave signal 3-Mw and a sixth RF chain 1-chain-6 operative to receive a second microwave signal 3-Mw'. The fifth RF chain 1-chain-5 down-converts the first microwave signal 3-Mw into a corresponding baseband signal 3-bb, and 10 The sixth RF chain 1-chain-6 down-converts the second microwave signal 3-Mw' into a corresponding baseband signal 3-bb'. Elements 13, 13', 14, and 14' represent various radio frequency components such as low-noise amplifiers component that is usually used in conjunction with radio frequency reception chains.

FIG. 2C illustrates one embodiment of the two millimeterwave signals 1-mmw-2, 1-mmw-2' having two different characteristic frequencies that are settable over a certain 20 frequency span 2-span and the two microwave signals 1-Mw-3, 1-Mw-3' derived respectively from the two millimeter-wave signals 1-mmw-2, 1-mmw-2' and thus having two respective characteristic frequencies that are settable over a similar frequency span 2-span'. For example, if both 25 millimeter-wave oscillators 1-synt-1 and 1-synt-3 operate around the same nominal frequency of 60 GHz (sixty gigahertz), then millimeter-wave oscillators 1-synt-1, 1-synth-3 can be expected to produce reference signals 1-ref-1, 1-ref-1' over a span of frequencies 2-span that is at 30 least 3 GHz (three gigahertz), e.g., from 58.5 GHz (fifty eight point five gigahertz) to 61.5 (sixty one point five gigahertz). Consequently, the resultant millimeter-wave signals 1-mmw-2, 1-mmw-2' have characteristic frequencies that are settable over the same frequency span 2-span of 3 35 from a baseband frequency into a millimeter-wave fre-GHz (three gigahertz). Microwave signals 1-Mw-3, 1-Mw-3', which are microwave versions of baseband signals 1-bb-1, 1-bb-1' respectively, are produces by the second and fourth millimeter-wave chains 1-chain-2, 1-chain-4 respectively using the reference signals 1-ref-2, 1-ref-2' from the 40 local millimeter-wave oscillators 1-synt-2, 1-synt-4 respectively and using the millimeter-wave signals 1-mmw-2, 1-mmw-2' as inputs respectively. Since both millimeterwave signals 1-mmw-2 and 1-mmw-2' have characteristic frequencies that are settable over the frequency span 2-span 45 of 3 GHz (three gigahertz) as an example, then consequently, the resultant microwave signals 1-Mw-3, 1-Mw-3' will have characteristic frequencies that are also settable over a similar frequency span 2-span' of 3 GHz (three gigahertz). If, as an example, reference signals 1-ref-1', 1-ref-2' have the fre- 50 quencies of 61.5 GHz (sixty one point five gigahertz) and 57.9 GHz (fifty seven point nine gigahertz) respectively, then the resultant characteristic frequency of microwave signal 1-Mw-3' will be 3.6 GHz (three point six gigahertz), which is equal the difference 2-differential' between these 55 frequencies. If, as an example, reference signals 1-ref-1, 1-ref-2 have the frequencies of 58.5 GHz (fifty eight point five gigahertz) and 57.9 GHz (fifty seven point nine gigahertz) respectively, then the resultant characteristic frequency of microwave signal 1-Mw-3 will be 600 MHz (six 60 hundred megahertz), which is equal to the difference 2-differential between these frequencies. In the above example, both of the signals 1-Mw-3' at 3.6 GHz and 1-Mw-3 at 600 MHz may exist concurrently, thereby facilitating parallel wireless/cellular transmissions at both a first 600 MHz band 65 and a second 3.6 GHz band, or at any other two different bands located inside the span of frequencies 2-span'.

According to one example, the reception path of the first 600 MHz band may be facilitated by the RF chain 1-chain-5, which may also operate in the first 600 MHz band, and the reception path of the second 3.6 GHz band may be facilitated by the RF chain 1-chain-6, which may also operate in the second 3.6 GHz band. Now, if all of the RF chains 1-chain-1, 1-chain-2, 1-chain-3, 1-chain-4, 1-chain-5, 1-chain-6 are co-located, perhaps in a single base-station or in a single radio frequency integrated circuit (RFIC), then it could be expected that impairments such as an unwanted non-linearity and other parasitic effects associated with synthesizing the microwave signal 1-Mw-3 at (for example) 600 MHz would create unwanted harmonics at (for example) 3.6 GHz, and therefore interfere with the reception (LNAs) and other amplifiers, filters, antennas, or any other 15 path 1-chain-6 in the second 3.6 GHz band, but this is avoided altogether by synthesizing the microwave signal 1-Mw-3 using millimeter-wave components 1-synt-1, 1-synt-2, 1-x-1, 1-x-2 and millimeter-wave frequencies.

> FIG. 2D illustrates one embodiment of a radio frequency integrated circuit 1-RFIC containing all of the RF chains 1-chain-1, 1-chain-2, 1-chain-3, 1-chain-4, 1-chain-5, 1-chain-6 and belonging to a wireless base-station, a remote radio head (RRH), or an access point 1-BS. Interferences between different microwave bands/channels are fundamentally avoided as a direct result of synthesizing the microwave signals 1-Mw-3, 1-Mw-3' using millimeter-wave components 1-synt-1, 1-synt-2, 1-x-1, 1-x-2, 1-synt-3, 1-synt-4, 1-x-1', 1-x-2' and employing millimeter-wave frequencies 1-ref-1, 1-ref-2, 1-ref-1', 1-ref-2' that are way above the frequencies of the microwave bands/channels.

> One embodiment is a system operative to use millimeterwave radio components to generate microwave signals over a wide frequency range. The system includes: a first millimeter-wave chain 1-chain-1 operative to up-convert signals quency; a second millimeter-wave chain 1-chain-2 operative to down-convert signals from a millimeter-wave frequency into a microwave frequency; and at least a first programmable millimeter-wave oscillator 1-synt-1 having an oscillation frequency 1-ref-1a, 1-ref-1b, 1-ref-1 that is above 25 GHz (twenty five gigahertz) and that is settable over a span 2-span of at least 1 GHz (one gigahertz).

> In one embodiment, the system is configured to: use the at least first programmable millimeter-wave oscillator 1-synt-1 to set a specific exact frequency differential 2-differential between an up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1 associated with the first millimeter-wave chain 1-chain-1 and a down-conversion frequency 1-ref-2 associated with the second millimeter-wave chain 1-chain-2, in which said specific exact frequency differential 2-differential is therefore settable over a span 2-span of at least 1 GHz (one gigahertz); receive a first signal 1-bb-1a, 1-bb-1b, 1-bb-1 in a baseband frequency; use the first millimeterwave chain 1-chain-1, in conjunction with said up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1, to up-convert the first signal 1-bb-1a, 1-bb-1b, 1-bb-1 from said baseband frequency into a millimeter-wave frequency, thereby producing a millimeter-wave version 1-mmw-2 of the first signal 1-bb-1a, 1-bb-1b, 1-bb-1; and use the second millimeter-wave chain 1-chain-2, in conjunction with said downconversion frequency 1-ref-2, to down-convert the millimeter-wave version 1-mmw-2 of the first signal into a microwave version 1-Mw-3 of the first signal having a characteristic frequency that is therefore settable over a span 2-span' of at least 1 GHz (one gigahertz).

> In one embodiment, the first programmable millimeterwave oscillator 1-synt-1 has an oscillation frequency that is

settable over a frequency span 2-span of at least 1.1 GHz (one point one gigahertz); the specific exact frequency differential 2-differential between the up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1 and the down-conversion frequency 1-ref-2 is settable over at least the range 2-span of 5 frequencies between 800 MHz (eight hundred megahertz) and 1.9 GHz (one point nine gigahertz); and the characteristic frequency of the microwave version 1-Mw-3 of the first signal is settable over at least the range of frequencies 2-span' between 800 MHz (eight hundred megahertz) and 10 1.9 GHz (one point nine gigahertz), in which said range of frequencies constitutes at least 57.8% (fifty seven point eight percent) of the characteristic frequency, and in which such a high range of frequencies is possible as a direct result of using the first millimeter-wave chain 1-chain-1 operative to 15 up-convert signals from a baseband frequency into a millimeter-wave frequency and the second millimeter-wave chain 1-chain-2 operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

In one embodiment, the first programmable millimeter- 20 wave oscillator 1-synt-1 has an oscillation frequency that is settable over a frequency span 2-span of at least 2.9 GHz (two point nine gigahertz); the specific exact frequency differential 2-differential between the up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1 and the down-conversion 25 frequency 1-ref-2 is settable over at least the range of frequencies 2-span between 800 MHz (eight hundred megahertz) and 3.7 GHz (three point seven gigahertz); and the characteristic frequency of the microwave version 1-Mw-3 of the first signal is settable over at least the range of 30 frequencies 2-span' between 800 MHz (eight hundred megahertz) and 3.7 GHz (three point seven gigahertz), in which said range of frequencies constitutes at least 78.3% (seventy eight point three percent) of the characteristic frequency, and in which such a very high range of frequencies is possible as 35 a direct result of using the first millimeter-wave chain 1-chain-1 operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and the second millimeter-wave chain 1-chain-2 operative to down-convert signals from a millimeter-wave frequency into a microwave 40 frequency.

In one embodiment, the first programmable millimeterwave oscillator 1-synt-1 has an oscillation frequency that is settable over a frequency span 2-span of at least 1.4 GHz (one point four gigahertz); the specific exact frequency 45 differential 2-differential between the up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1 and the down-conversion frequency 1-ref-2 is settable over at least the range of frequencies 2-span between 2.3 GHz (two point three gigahertz) and 3.7 GHz (three point seven gigahertz); and the 50 characteristic frequency of the microwave version 1-Mw-3 of the first signal is settable over at least the range of frequencies 2-span' between 2.3 GHz (two point three gigahertz) and 3.7 GHz (three point seven gigahertz), in which said range of frequencies constitutes at least 37.8% (thirty 55 seven point eight percent) of the characteristic frequency, and in which such a high range of frequencies is possible as a direct result of using the first millimeter-wave chain 1-chain-1 operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and the second 60 millimeter-wave chain 1-chain-2 operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

In one embodiment, the first programmable millimeterwave oscillator 1-synt-1 has an oscillation frequency that is 65 settable over a frequency span 2-span of at least 5 GHz (five gigahertz); the specific exact frequency differential 2-differ8

ential between the up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1 and the down-conversion frequency 1-ref-2 is settable over at least the range of frequencies 2-span between 800 MHz (eight hundred megahertz) and 5.8 GHz (five point eight gigahertz); and the characteristic frequency of the microwave version 1-Mw-3 of the first signal is settable over at least the range of frequencies 2-span' between 800 MHz (eight hundred megahertz) and 5.8 GHz (five point eight gigahertz), in which said range of frequencies constitutes at least 86.2% (eighty six point two percent) of the characteristic frequency, and in which such an ultra high range of frequencies is possible as a direct result of using the first millimeter-wave chain 1-chain-1 operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and the second millimeter-wave chain 1-chain-2 operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

In one embodiment, the system further includes: a third millimeter-wave chain 1-chain-3 operative to up-convert signals from a baseband frequency into a millimeter-wave frequency; a fourth millimeter-wave chain 1-chain-4 operative to down-convert signals from a millimeter-wave frequency into a microwave frequency; and at least one other programmable millimeter-wave oscillator 1-synt-3 having an oscillation frequency 1-ref-1a', 1-ref-1b', 1-ref-1' that is above 25 GHz (twenty five gigahertz) and that is settable over a frequency span 2-span of at least 1 GHz (one gigahertz). In one embodiment the system is further configured to: use the at least one other programmable millimeterwave oscillator 1-synt-3 to set another specific exact frequency differential 2-differential between another up-conversion frequency 1-ref-1a', 1-ref-1 b', 1-ref-1' associated with the third millimeter-wave chain 1-chain-3 and another down-conversion frequency 1-ref-2' associated with the fourth millimeter-wave chain 1-chain-4, in which said another specific exact frequency differential 2-differential' is therefore settable over a span 2-span of at least 1 GHz (one gigahertz); receive a second signal 1-bb-1a', 1-bb-1b', 1-bb-1' in a baseband frequency; use the third millimeter-wave chain 1-chain-3, in conjunction with said another up-conversion frequency 1-ref-1a', 1-ref-1 b', 1-ref-1', to up-convert the second signal 1-bb-1a', 1-bb-1 b', 1-bb-1' from said baseband frequency into a millimeter-wave frequency, thereby producing a millimeter-wave version 1-mmw-2' of the second signal 1-bb-1a', 1-bb-1b', 1-bb-1'; and use the fourth millimeter-wave chain 1-chain-4, in conjunction with said another down-conversion frequency 1-ref-2', to downconvert the millimeter-wave version 1-mmw-2' of the second signal into a microwave version 1-Mw-3' of the second signal having a characteristic frequency that is therefore settable over a span 2-span' of at least 1 GHz (one gigahertz). In one embodiment, the system further includes: a first circuitry 1-chain-5 operative to receive a first incoming signal 3-Mw having a characteristic frequency associated with the characteristic frequency of the microwave versions 1-Mw-3 of the first signal, and a second circuitry 1-chain-6 operative to receive a second incoming signal 3-Mw' having a characteristic frequency associated with the characteristic frequency of the microwave versions 1-Mw-3' of the second signal; the microwave version of the second signal 1-Mw-3' has a higher characteristic frequency than the microwave version of the first signal 1-Mw-3; and the first programmable millimeter-wave oscillator 1-synt-1 does not interfere with said reception of the second incoming signal 3-Mw' as a direct result of the first programmable millimeter-wave oscillator 1-synt-1 having an oscillation frequency 1-ref-1a, 1-ref-1b, 1-ref-1 that is above 25 GHz (twenty five giga-

hertz) and that is therefore way above the characteristic frequency of the second incoming signal 3-Mw'. In one embodiment, the microwave version 1-Mw-3 of the first signal and the first incoming signal 3-Mw are both associated with a first wireless communication channel, in which the microwave version 1-Mw-3 of the first signal is used as a transmission signal in conjunction with said first wireless communication channel; and the microwave version 1-Mw-3' of the second signal and the second incoming signal 3-Mw' are both associated with a second wireless communication channel, in which the microwave version of the second signal 1-Mw-3' is used as a transmission signal in conjunction with said second wireless communication channel, and in which the second wireless communication channel is associated with a frequency that is higher than the frequency associated with the first wireless communication channel.

In one embodiment, the first wireless communication channel is associated with frequencies selected from a group 20 consisting of: (i) frequencies in the 500 MHz (five hundred megahertz) band (i.e., frequencies between 500 MHz and 600 MHz), (ii) frequencies in the 600 MHz (six hundred megahertz) band, (iii) frequencies in the 700 MHz (seven hundred megahertz) band, (iv) frequencies in the 800 MHz 25 (eight hundred megahertz) band, and (v) frequencies in the 900 MHz (nine hundred megahertz) band; and the second wireless communication channel is associated with frequencies selected from a group consisting of: (i) frequencies in the 1.7 GHz (one point seven gigahertz) band, (ii) frequen- 30 cies in the 1.8 GHz (one point eight gigahertz) band, (iii) frequencies in the 1.9 GHz (one point nine gigahertz) band, (iv) frequencies in the 2.1 GHz (two point one gigahertz) band, (v) frequencies in the 2.3 GHz (two point three gigahertz) band, (vi) frequencies in the 2.4 GHz (two point 35 four gigahertz) band, (vii) frequencies in the 2.5 GHz (two point five gigahertz) band, and (viii) frequencies in the 3.6 GHz (three point six gigahertz) band; wherein the second wireless communication channel successfully coexists with the first wireless communication channel as a direct result of 40 the first programmable millimeter-wave oscillator 1-synth-1 having an oscillation frequency 1-ref-1a, 1-ref-1b, 1-ref-1 that is above 25 GHz (twenty five gigahertz) and that is therefore way above the frequencies of the second incoming signal 3-Mw' of the second wireless communication chan- 45 nel.

In one embodiment, the first wireless communication channel is associated with frequencies in the 2.4 GHz (two point four gigahertz) band (i.e., frequencies between 2.4 GHz and 2.5 GHz); and the second wireless communication 50 channel is associated with frequencies in the 5 GHz (five gigahertz) band (i.e., frequencies between 5 GHz and 5.8 GHz); wherein the second wireless communication channel successfully coexists with the first wireless communication channel as a direct result of the first programmable millimeter-wave oscillator 1-synth-1 having an oscillation frequency 1-ref-1a, 1-ref-1b, 1-ref-1 that is above 25 GHz (twenty five gigahertz) and that is therefore way above the frequencies of the second incoming signal 3-Mw' of the second wireless communication channel.

In one embodiment, at least most parts of the millimeter-wave chains 1-chain-1, 1-chain-2, 1-chain-3, 1-chain-4 and the programmable millimeter-wave oscillators 1-synt-1, 1-synt-3 are implemented on a single radio frequency integrated circuit (RFIC) 1-RFIC.

In one embodiment, the first and second wireless communication channels are associated with a radio access 10

network (RAN) component 1-BS such as a cellular base station or a wireless access point such as a WiFi access point.

In one embodiment, the at least first programmable millimeter-wave oscillator 1-synt-1 comprises: (i) the first programmable millimeter-wave oscillator 1-synt-1 and (ii) a second programmable millimeter-wave oscillator 1-synt-2, in which the up-conversion frequency 1-ref-1a, 1-ref-1b, 1-ref-1 is generated by the first programmable millimeter-wave oscillator 1-synt-1 and the down-conversion frequency 1-ref-2 is generated by the second programmable millimeter-wave oscillator 1-synt-2, thereby facilitating said setting of the exact frequency differential 2-differential.

FIG. 3 illustrates one embodiment of a method for using millimeter-wave radio components for generating micro-15 wave signals over a wide frequency range. The method includes: In step 1001, setting a specific first up-conversion frequency 1-ref-1 and a specific first down-conversion frequency 1-ref-2 using at least a first programmable millimeter-wave oscillator 1-synt-1 having an oscillation frequency 1-ref-1 that is above 25 GHz (twenty five gigahertz) and that is settable over a span 2-span of at least 1 GHz (one gigahertz). In step 1002, up-converting a first signal 1-bb-1 from a baseband frequency into a millimeter-wave frequency using the specific first up-conversion frequency 1-ref-1, thereby producing a millimeter-wave version 1-mmw-2 of the first signal 1-bb-1, and then down-converting the millimeter-wave version 1-mmw-2 of the first signal using the specific first down-conversion frequency 1-ref-2, thereby producing a microwave version 1-Mw-3 of the first signal characterized by a particular first frequency that is equal to the difference 2-differential between said specific first up-conversion frequency 1-ref-1 and said specific first down-conversion frequency 1-ref-2. In step 1003, setting at least one of: (i) a specific second up-conversion frequency 1-ref-1" (FIG. 2C) and (ii) a specific second down-conversion frequency 1-ref-2" (FIG. 2C) using at least the first programmable millimeter-wave oscillator 1-synt-1. In step 1004, up-converting a second signal 1-bb-1" (FIG. 2C) from the baseband frequency into a millimeter-wave frequency using the specific second up-conversion frequency 1-ref-1", thereby producing a millimeter-wave version 1-mmw-2" (FIG. 2C) of the second signal 1-bb-1", and then downconverting the millimeter-wave version 1-mmw-2" of the second signal using the specific second down-conversion frequency 1-ref-2", thereby producing a microwave version 1-Mw-3" (FIG. 2C) of the second signal characterized by a particular second frequency that is equal to the difference 2-differential' (FIG. 2C) between said specific second upconversion frequency 1-ref-1" and said specific second down-conversion frequency 1-ref-2", in which the particular second frequency varies by at least 1 GHz (one gigahertz) from the particular first frequency as a result of said span 2-span, 2-span'.

In one embodiment, the method further comprises: receiving a first request to transmit via a first microwave band, in which said setting of the specific first up-conversion frequency 1-ref-1 and the specific first down-conversion frequency 1-ref-2 is a result of said first request; and transmitting wirelessly the microwave version 1-Mw-3 of the first signal as a further result of said first request. In one embodiment, the method further comprises: receiving a second request to transmit via a second microwave band, in which said setting of the specific second up-conversion frequency 1-ref-1" and the specific second down-conversion frequency 1-ref-2" is a result of said second request; and transmitting wirelessly the microwave version 1-Mw-3" of the second signal as a further result of said second request.

In one embodiment, the first microwave band is associated with frequencies selected from a group consisting of: (i) frequencies in the 500 MHz (five hundred megahertz) band, (ii) frequencies in the 600 MHz (six hundred megahertz) band, (iii) frequencies in the 700 MHz (seven hundred 5 megahertz) band, (iv) frequencies in the 800 MHz (eight hundred megahertz) band, and (v) frequencies in the 900 MHz (nine hundred megahertz) band; and the second microwave band is associated with frequencies selected from a group consisting of: (i) frequencies in the 1.7 GHz (one 10 point seven gigahertz) band, (ii) frequencies in the 1.8 GHz (one point eight gigahertz) band, (iii) frequencies in the 1.9 GHz (one point nine gigahertz) band, (iv) frequencies in the 2.1 GHz (two point one gigahertz) band, (v) frequencies in the 2.3 GHz (two point three gigahertz) band, (vi) frequen- 15 cies in the 2.4 GHz (two point four gigahertz) band, (vii) frequencies in the 2.5 GHz (two point five gigahertz) band, and (viii) frequencies in the 3.6 GHz (three point six gigahertz) band.

In one embodiment, the first microwave band is associ- 20 ated with frequencies in the 2.4 GHz (two point four gigahertz) band; and the second microwave band is associated with frequencies in the 5 GHz (five gigahertz) band.

In one embodiment, said setting of at least one of: (i) the specific second up-conversion frequency 1-ref-1" and (ii) 25 the specific second down-conversion frequency 1-ref-2" using at least the first programmable millimeter-wave oscillator 1-synt-1 comprises: setting the specific second upconversion frequency 1-ref-1" using the first programmable millimeter-wave oscillator 1-synt-1; in which: the specific 30 second down-conversion frequency 1-ref-2" is equal to the specific first down-conversion frequency 1-ref-2, and therefore the specific second down-conversion frequency 1-ref-2" does not require setting.

specific second up-conversion frequency 1-ref-1" and (ii) the specific second down-conversion frequency 1-ref-2" using at least the first programmable millimeter-wave oscillator 1-synt-1 comprises: setting the specific second downconversion frequency 1-ref-2" using the first programmable 40 millimeter-wave oscillator 1-synt-1; in which: the specific second up-conversion frequency 1-ref-1" is equal to the specific first up-conversion frequency 1-ref-1, and therefore the specific second up-conversion frequency 1-ref-1" does not require setting.

In one embodiment, said setting of at least one of: (i) the specific second up-conversion frequency 1-ref-1" and (ii) the specific second down-conversion frequency 1-ref-2" using at least the first programmable millimeter-wave oscillator 1-synt-1 comprises: setting the specific second up- 50 conversion frequency 1-ref-1" using the first programmable millimeter-wave oscillator 1-synt-1; and setting the specific second down-conversion frequency 1-ref-2" using a second programmable millimeter-wave oscillator 1-synt-2.

In this description, numerous specific details are set forth. 55 However, the embodiments/cases of the invention may be practiced without some of these specific details. In other instances, well-known hardware, materials, structures and techniques have not been shown in detail in order not to obscure the understanding of this description. In this 60 description, references to "one embodiment" and "one case" mean that the feature being referred to may be included in at least one embodiment/case of the invention. Moreover, separate references to "one embodiment", "some embodiments", "one case", or "some cases" in this description do 65 not necessarily refer to the same embodiment/case. Illustrated embodiments/cases are not mutually exclusive, unless

so stated and except as will be readily apparent to those of ordinary skill in the art. Thus, the invention may include any variety of combinations and/or integrations of the features of the embodiments/cases described herein. Also herein, flow diagrams illustrate non-limiting embodiment/case examples of the methods, and block diagrams illustrate non-limiting embodiment/case examples of the devices. Some operations in the flow diagrams may be described with reference to the embodiments/cases illustrated by the block diagrams. However, the methods of the flow diagrams could be performed by embodiments/cases of the invention other than those discussed with reference to the block diagrams, and embodiments/cases discussed with reference to the block diagrams could perform operations different from those discussed with reference to the flow diagrams. Moreover, although the flow diagrams may depict serial operations, certain embodiments/cases could perform certain operations in parallel and/or in different orders from those depicted. Moreover, the use of repeated reference numerals and/or letters in the text and/or drawings is for the purpose of simplicity and clarity and does not in itself dictate a relationship between the various embodiments/cases and/or configurations discussed. Furthermore, methods and mechanisms of the embodiments/ cases will sometimes be described in singular form for clarity. However, some embodiments/cases may include multiple iterations of a method or multiple instantiations of a mechanism unless noted otherwise. For example, when a controller or an interface are disclosed in an embodiment/ case, the scope of the embodiment/case is intended to also cover the use of multiple controllers or interfaces.

Certain features of the embodiments/cases, which may have been, for clarity, described in the context of separate embodiments/cases, may also be provided in various combinations in a single embodiment/case. Conversely, various In one embodiment, said setting of at least one of: (i) the 35 features of the embodiments/cases, which may have been, for brevity, described in the context of a single embodiment/ case, may also be provided separately or in any suitable sub-combination. The embodiments/cases are not limited in their applications to the details of the order or sequence of steps of operation of methods, or to details of implementation of devices, set in the description, drawings, or examples. In addition, individual blocks illustrated in the figures may be functional in nature and do not necessarily correspond to discrete hardware elements. While the meth-45 ods disclosed herein have been described and shown with reference to particular steps performed in a particular order, it is understood that these steps may be combined, subdivided, or reordered to form an equivalent method without departing from the teachings of the embodiments/cases. Accordingly, unless specifically indicated herein, the order and grouping of the steps is not a limitation of the embodiments/cases. Embodiments/cases described in conjunction with specific examples are presented by way of example, and not limitation. Moreover, it is evident that many alternatives, modifications and variations will be apparent to those skilled in the art. Accordingly, it is intended to embrace all such alternatives, modifications and variations that fall within the spirit and scope of the appended claims and their equivalents.

What is claimed is:

- 1. A system operative to use millimeter-wave radio components to generate microwave signals over a wide frequency range, comprising:
  - a first millimeter-wave chain operative to up-convert signals from a baseband frequency into a millimeterwave frequency;

- a second millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency; and
- at least a first programmable millimeter-wave oscillator having an oscillation frequency that is above 25 GHz 5 (twenty five gigahertz) and that is settable over a span of at least 1 GHz (one gigahertz);

wherein the system is configured to:

lator to set a specific exact frequency differential 10 between an up-conversion frequency associated with the first millimeter-wave chain and a down-conversion frequency associated with the second millimeter-wave chain, in which said specific exact frequency differential is therefore settable over a span of at least 1 GHz 15 (one gigahertz);

receive a first signal in a baseband frequency;

use the first millimeter-wave chain, in conjunction with said up-conversion frequency, to up-convert the first signal from said baseband frequency into a millimeter- 20 wave frequency, thereby producing a millimeter-wave version of the first signal; and

use the second millimeter-wave chain, in conjunction with said down-conversion frequency, to down-convert the millimeter-wave version of the first signal into a 25 microwave version of the first signal having a characteristic frequency that is therefore settable over a span of at least 1 GHz (one gigahertz).

2. The system of claim 1, wherein:

the first programmable millimeter-wave oscillator has an oscillation frequency that is settable over a frequency span of at least 1.1 GHz (one point one gigahertz);

the specific exact frequency differential between the upconversion frequency and the down-conversion frequency is settable over at least the range of frequencies 35 between 800 MHz (eight hundred megahertz) and 1.9 GHz (one point nine gigahertz); and

the characteristic frequency of the microwave version of the first signal is settable over at least the range of frequencies between 800 MHz (eight hundred mega- 40 hertz) and 1.9 GHz (one point nine gigahertz), in which said range of frequencies constitutes at least 57.8% (fifty seven point eight percent) of the characteristic frequency, and in which such a high range of frequencies is possible as a direct result of using the first 45 millimeter-wave chain operative to up-convert signals from a baseband frequency into a millimeter-wave frequency and the second millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

3. The system of claim 1, wherein:

the first programmable millimeter-wave oscillator has an oscillation frequency that is settable over a frequency span of at least 2.9 GHz (two point nine gigahertz);

the specific exact frequency differential between the up- 55 conversion frequency and the down-conversion frequency is settable over at least the range of frequencies between 800 MHz (eight hundred megahertz) and 3.7 GHz (three point seven gigahertz); and

the characteristic frequency of the microwave version of 60 the first signal is settable over at least the range of frequencies between 800 MHz (eight hundred megahertz) and 3.7 GHz (three point seven gigahertz), in which said range of frequencies constitutes at least 78.3% (seventy eight point three percent) of the characteristic frequency, and in which such a very high range of frequencies is possible as a direct result of

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using the first millimeter-wave chain operative to upconvert signals from a baseband frequency into a millimeter-wave frequency and the second millimeterwave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

4. The system of claim 1, wherein:

the first programmable millimeter-wave oscillator has an oscillation frequency that is settable over a frequency span of at least 1.4 GHz (one point four gigahertz);

the specific exact frequency differential between the upconversion frequency and the down-conversion frequency is settable over at least the range of frequencies between 2.3 GHz (two point three gigahertz) and 3.7 GHz (three point seven gigahertz); and

the characteristic frequency of the microwave version of the first signal is settable over at least the range of frequencies between 2.3 GHz (two point three gigahertz) and 3.7 GHz (three point seven gigahertz), in which said range of frequencies constitutes at least 37.8% (thirty seven point eight percent) of the characteristic frequency, and in which such a high range of frequencies is possible as a direct result of using the first millimeter-wave chain operative to up-convert signals from a baseband frequency into a millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

5. The system of claim 1, wherein:

the first programmable millimeter-wave oscillator has an oscillation frequency that is settable over a frequency span of at least 5 GHz (five gigahertz);

the specific exact frequency differential between the upconversion frequency and the down-conversion frequency is settable over at least the range of frequencies between 800 MHz (eight hundred megahertz) and 5.8 GHz (five point eight gigahertz); and

the characteristic frequency of the microwave version of the first signal is settable over at least the range of frequencies between 800 MHz (eight hundred megahertz) and 5.8 GHz (five point eight gigahertz), in which said range of frequencies constitutes at least 86.2% (eighty six point two percent) of the characteristic frequency, and in which such an ultra high range of frequencies is possible as a direct result of using the first millimeter-wave chain operative to up-convert signals from a baseband frequency into a millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency.

6. The system of claim 1, further comprising:

- a third millimeter-wave chain operative to up-convert signals from a baseband frequency into a millimeterwave frequency;
- a fourth millimeter-wave chain operative to down-convert signals from a millimeter-wave frequency into a microwave frequency; and
- at least one other programmable millimeter-wave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is settable over a frequency span of at least 1 GHz (one gigahertz);

wherein the system is further configured to:

use the at least one other programmable millimeter-wave oscillator to set another specific exact frequency differential between another up-conversion frequency associated with the third millimeter-wave chain and another down-conversion frequency associated with

the fourth millimeter-wave chain, in which said another specific exact frequency differential is therefore settable over a span of at least 1 GHz (one gigahertz);

receive a second signal in a baseband frequency;

use the third millimeter-wave chain, in conjunction with 5 said another up-conversion frequency, to up-convert the second signal from said baseband frequency into a millimeter-wave frequency, thereby producing a millimeter-wave version of the second signal; and

use the fourth millimeter-wave chain, in conjunction with said another down-conversion frequency, to down-convert the millimeter-wave version of the second signal into a microwave version of the second signal having a characteristic frequency that is therefore settable over a span of at least 1 GHz (one gigahertz).

7. The system of claim 6, wherein:

the system further comprises: a first circuitry operative to receive a first incoming signal having a characteristic frequency associated with the characteristic frequency of the microwave versions of the first signal, and a 20 second circuitry operative to receive a second incoming signal having a characteristic frequency associated with the characteristic frequency of the microwave versions of the second signal;

the microwave version of the second signal has a higher 25 characteristic frequency than the microwave version of the first signal; and

the first programmable millimeter-wave oscillator does not interfere with said reception of the second incoming signal as a direct result of the first programmable 30 millimeter-wave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is therefore way above the characteristic frequency of the second incoming signal.

8. The system of claim 7, wherein:

the microwave version of the first signal and the first incoming signal are both associated with a first wireless communication channel, in which the microwave version of the first signal is used as a transmission signal in conjunction with said first wireless communication 40 channel; and

the microwave version of the second signal and the second incoming signal are both associated with a second wireless communication channel, in which the microwave version of the second signal is used as a 45 transmission signal in conjunction with said second wireless communication channel, and in which the second wireless communication channel is associated with a frequency that is higher than the frequency associated with the first wireless communication channel.

9. The system of claim 8, wherein:

the first wireless communication channel is associated with frequencies selected from a group consisting of:
(i) frequencies in the 500 MHz (five hundred mega-55 hertz) band, (ii) frequencies in the 600 MHz (six hundred megahertz) band, (iii) frequencies in the 700 MHz (seven hundred megahertz) band, (iv) frequencies in the 800 MHz (eight hundred megahertz) band, and (v) frequencies in the 900 MHz (nine hundred mega-60 hertz) band; and

the second wireless communication channel is associated with frequencies selected from a group consisting of:
(i) frequencies in the 1.7 GHz (one point seven gigahertz) band, (ii) frequencies in the 1.8 GHz (one point 65 eight gigahertz) band, (iii) frequencies in the 1.9 GHz (one point nine gigahertz) band, (iv) frequencies in the

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2.1 GHz (two point one gigahertz) band, (v) frequencies in the 2.3 GHz (two point three gigahertz) band, (vi) frequencies in the 2.4 GHz (two point four gigahertz) band, (vii) frequencies in the 2.5 GHz (two point five gigahertz) band, and (viii) frequencies in the 3.6 GHz (three point six gigahertz) band;

wherein the second wireless communication channel successfully coexists with the first wireless communication channel as a direct result of the first programmable millimeter-wave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is therefore way above the frequencies of the second incoming signal of the second wireless communication channel.

10. The system of claim 8, wherein:

the first wireless communication channel is associated with frequencies in the 2.4 GHz (two point four gigahertz) band; and

the second wireless communication channel is associated with frequencies in the 5 GHz (five gigahertz) band;

wherein the second wireless communication channel successfully coexists with the first wireless communication channel as a direct result of the first programmable millimeter-wave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is therefore way above the frequencies of the second incoming signal of the second wireless communication channel.

11. The system of claim 8, wherein at least most parts of the millimeter-wave chains and the programmable millimeter-wave oscillators are implemented on a single radio frequency integrated circuit (RFIC).

12. The system of claim 8, wherein the first and second wireless communication channels are associated with a radio access network (RAN) component such as a cellular base station or a wireless access point such as a WiFi access point.

13. The system of claim 1, wherein the at least first programmable millimeter-wave oscillator comprises: (i) the first programmable millimeter-wave oscillator and (ii) a second programmable millimeter-wave oscillator, in which the up-conversion frequency is generated by the first programmable millimeter-wave oscillator and the down-conversion frequency is generated by the second programmable millimeter-wave oscillator, thereby facilitating said setting of the exact frequency differential.

14. A method for using millimeter-wave radio components for generating microwave signals over a wide frequency range, comprising:

setting a specific first up-conversion frequency and a specific first down-conversion frequency using at least a first programmable millimeter-wave oscillator having an oscillation frequency that is above 25 GHz (twenty five gigahertz) and that is settable over a span of at least 1 GHz (one gigahertz);

up-converting a first signal from a baseband frequency into a millimeter-wave frequency using the specific first up-conversion frequency, thereby producing a millimeter-wave version of the first signal, and then down-converting the millimeter-wave version of the first signal using the specific first down-conversion frequency, thereby producing a microwave version of the first signal characterized by a particular first frequency that is equal to the difference between said specific first up-conversion frequency and said specific first down-conversion frequency;

setting at least one of: (i) a specific second up-conversion frequency and (ii) a specific second down-conversion frequency using at least the first programmable millimeter-wave oscillator; and

up-converting a second signal from the baseband frequency into a millimeter-wave frequency using the specific second up-conversion frequency, thereby producing a millimeter-wave version of the second signal, and then down-converting the millimeter-wave version of the second signal using the specific second down-conversion frequency, thereby producing a microwave version of the second signal characterized by a particular second frequency that is equal to the difference between said specific second up-conversion frequency and said specific second down-conversion frequency, in which the particular second frequency varies by at least 1 GHz (one gigahertz) from the particular first frequency as a result of said span.

15. The method of claim 14, further comprising:

receiving a first request to transmit via a first microwave 20 band, in which said setting of the specific first upconversion frequency and the specific first down-conversion frequency is a result of said first request; and transmitting wirelessly the microwave version of the first signal as a further result of said first request.

16. The method of claim 15, further comprising:

receiving a second request to transmit via a second microwave band, in which said setting of the specific second up-conversion frequency and the specific second down-conversion frequency is a result of said 30 second request; and

transmitting wirelessly the microwave version of the second signal as a further result of said second request.

17. The method of claim 16, wherein:

the first microwave band is associated with frequencies 35 selected from a group consisting of: (i) frequencies in the 500 MHz (five hundred megahertz) band, (ii) frequencies in the 600 MHz (six hundred megahertz) band, (iii) frequencies in the 700 MHz (seven hundred megahertz) band, (iv) frequencies in the 800 MHz 40 (eight hundred megahertz) band, and (v) frequencies in the 900 MHz (nine hundred megahertz) band; and

the second microwave band is associated with frequencies selected from a group consisting of: (i) frequencies in the 1.7 GHz (one point seven gigahertz) band, (ii) 45 frequencies in the 1.8 GHz (one point eight gigahertz) band, (iii) frequencies in the 1.9 GHz (one point nine gigahertz) band, (iv) frequencies in the 2.1 GHz (two

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point one gigahertz) band, (v) frequencies in the 2.3 GHz (two point three gigahertz) band, (vi) frequencies in the 2.4 GHz (two point four gigahertz) band, (vii) frequencies in the 2.5 GHz (two point five gigahertz) band, and (viii) frequencies in the 3.6 GHz (three point six gigahertz) band.

18. The method of claim 16, wherein:

the first microwave band is associated with frequencies in the 2.4 GHz (two point four gigahertz) band; and

the second microwave band is associated with frequencies in the 5 GHz (five gigahertz) band.

19. The method of claim 14, wherein said setting of at least one of: (i) the specific second up-conversion frequency and (ii) the specific second down-conversion frequency using at least the first programmable millimeter-wave oscillator comprises:

setting the specific second up-conversion frequency using the first programmable millimeter-wave oscillator;

in which:

the specific second down-conversion frequency is equal to the specific first down-conversion frequency, and therefore the specific second down-conversion frequency does not require setting.

20. The method of claim 14, wherein said setting of at least one of: (i) the specific second up-conversion frequency and (ii) the specific second down-conversion frequency using at least the first programmable millimeter-wave oscillator comprises:

setting the specific second down-conversion frequency using the first programmable millimeter-wave oscillator;

in which:

the specific second up-conversion frequency is equal to the specific first up-conversion frequency, and therefore the specific second up-conversion frequency does not require setting.

21. The method of claim 14, wherein said setting of at least one of: (i) the specific second up-conversion frequency and (ii) the specific second down-conversion frequency using at least the first programmable millimeter-wave oscillator comprises:

setting the specific second up-conversion frequency using the first programmable millimeter-wave oscillator; and setting the specific second down-conversion frequency using a second programmable millimeter-wave oscillator.

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