



US010518910B1

(12) **United States Patent**
Romano et al.

(10) **Patent No.:** **US 10,518,910 B1**
(45) **Date of Patent:** **Dec. 31, 2019**

(54) **AGILE ATTITUDE CONTROL SYSTEM FOR SMALL SPACECRAFT**

(75) Inventors: **Marcello Romano**, Monterey, CA (US);
Paul Oppenheimer, Pacific Grove, CA (US)

(73) Assignee: **United States of America, as represented by the Secretary of the Navy**, Arlington, VA (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 2914 days.

(21) Appl. No.: **12/460,923**

(22) Filed: **Feb. 26, 2010**

Related U.S. Application Data

(60) Provisional application No. 61/156,250, filed on Feb. 27, 2009, provisional application No. 61/221,236, filed on Jun. 29, 2009.

(51) **Int. Cl.**
B64G 1/28 (2006.01)
G01C 19/04 (2006.01)

(52) **U.S. Cl.**
CPC **B64G 1/286** (2013.01); **G01C 19/04** (2013.01)

(58) **Field of Classification Search**
USPC 244/158.6, 164, 165
See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,825,716 A * 5/1989 Roberts et al. 74/5.34
2009/0039202 A1* 2/2009 Ogo et al. 244/165

OTHER PUBLICATIONS

Omagari, Kuniyuki, "Research of Control Momentum Gyros for Micro-Satellites and 3-DOF Attitude Dynamics Simulator Experiments", Sep. 5, 2005, Proc. of The 8th International Symposium on Artificial Intelligence, Robotics and Automation in Space.*
Berner, Reimer. "Control Moment Gyro Actuator for Small Satellite Applications" Apr. 2005. Department of Electrical and Electronic Engineering, University of Stellenbosch.*
Miniature Reaction and Momentum Wheels for Nanosatellites, IntelliTech Microsystems, Inc. Retrieved from the Internet: <URL: <http://www.imicro/biz/space/html>>. (3 pages).

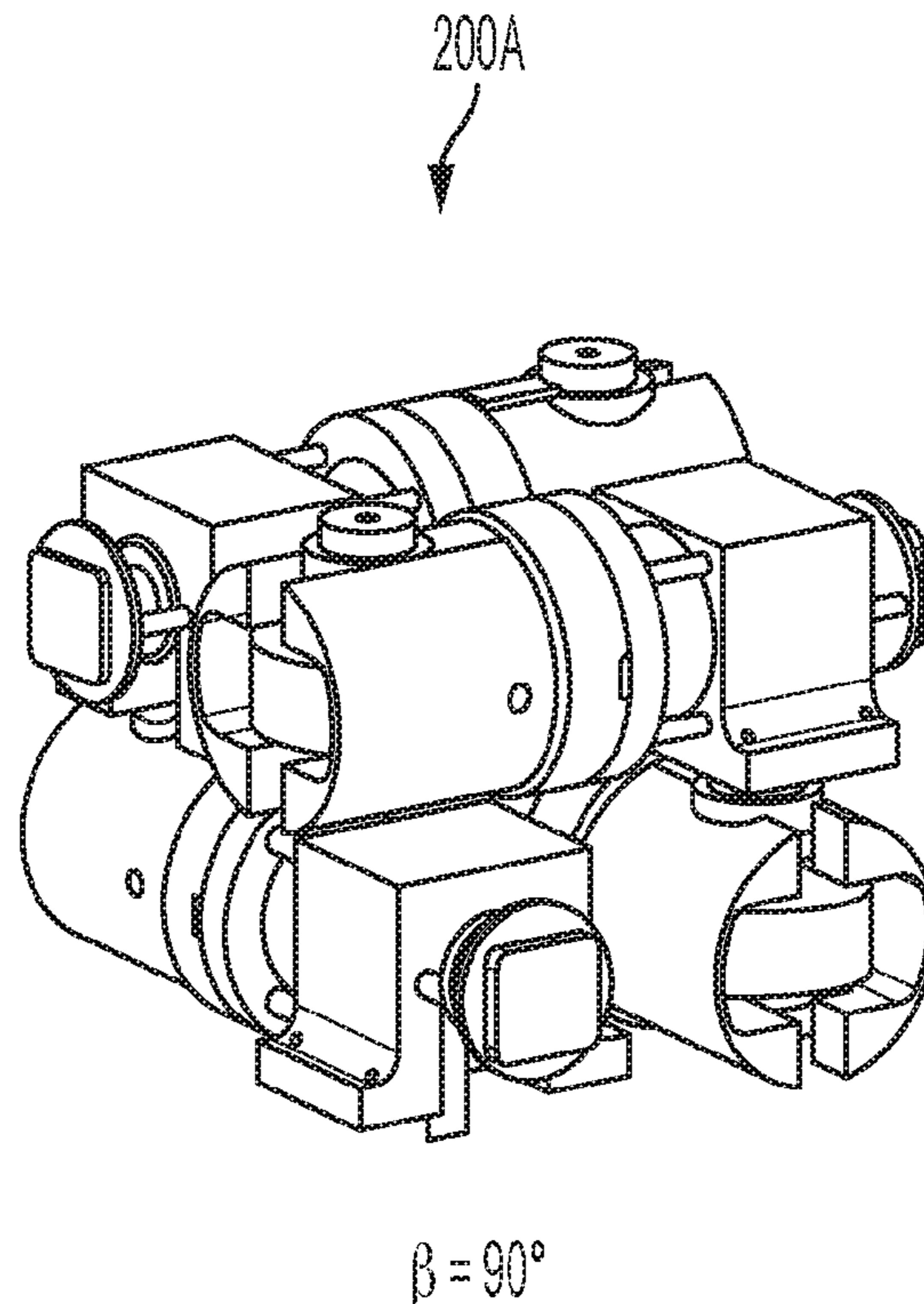
* cited by examiner

Primary Examiner — Joseph W Sanderson
(74) *Attorney, Agent, or Firm* — Naval Postgraduate School; Lisa A. Norris

(57) **ABSTRACT**

An agile attitude control system (AACS) that is a three axis attitude control device for small spacecraft based on miniature single gimbal control moment gyroscopes (SGCMGs) actuators. The AACS enables agile attitude slewing and accurate pointing/tracking for spacecraft made of multiple CubeSat units, or, more generally, for nanosatellites.

15 Claims, 6 Drawing Sheets



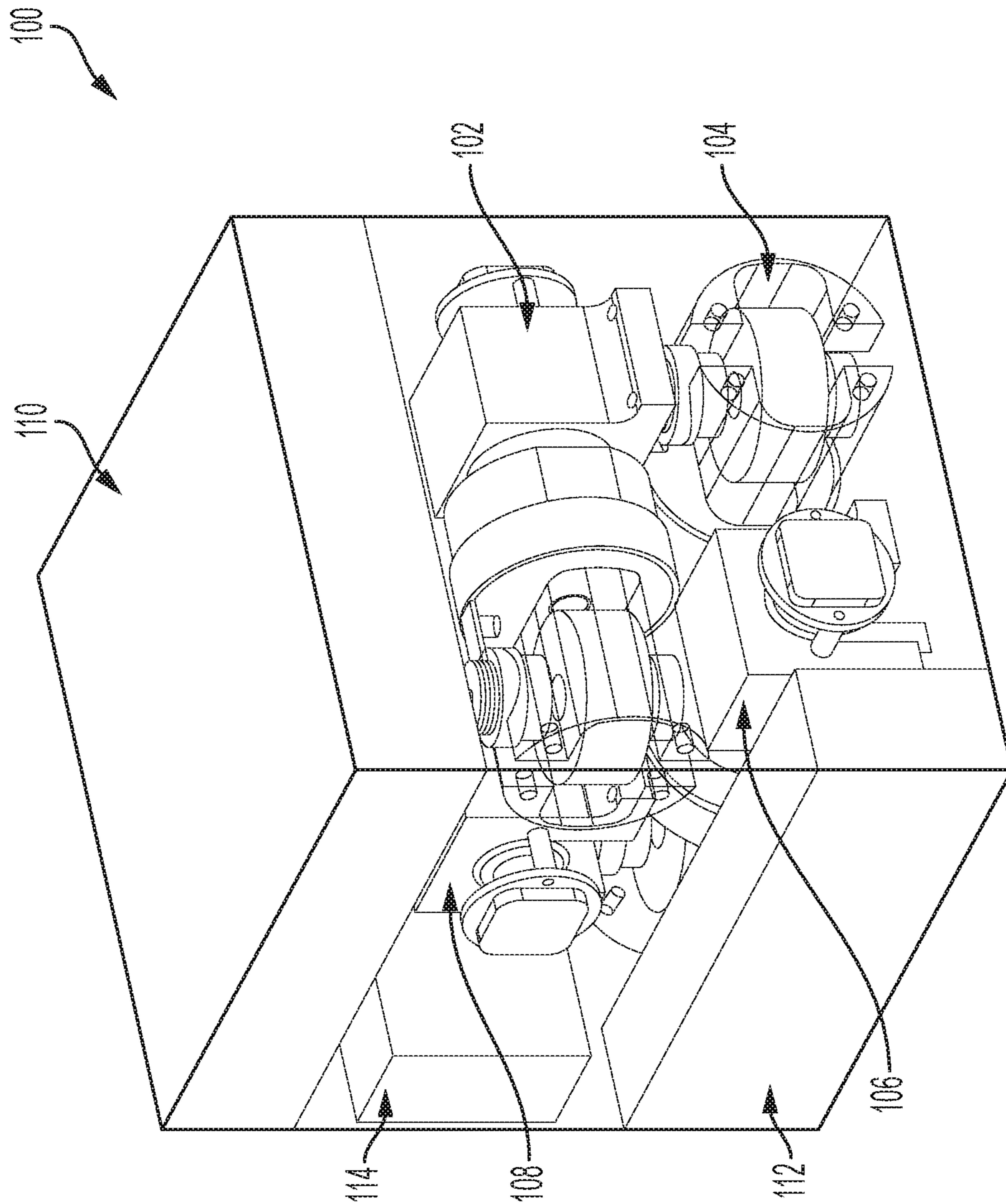
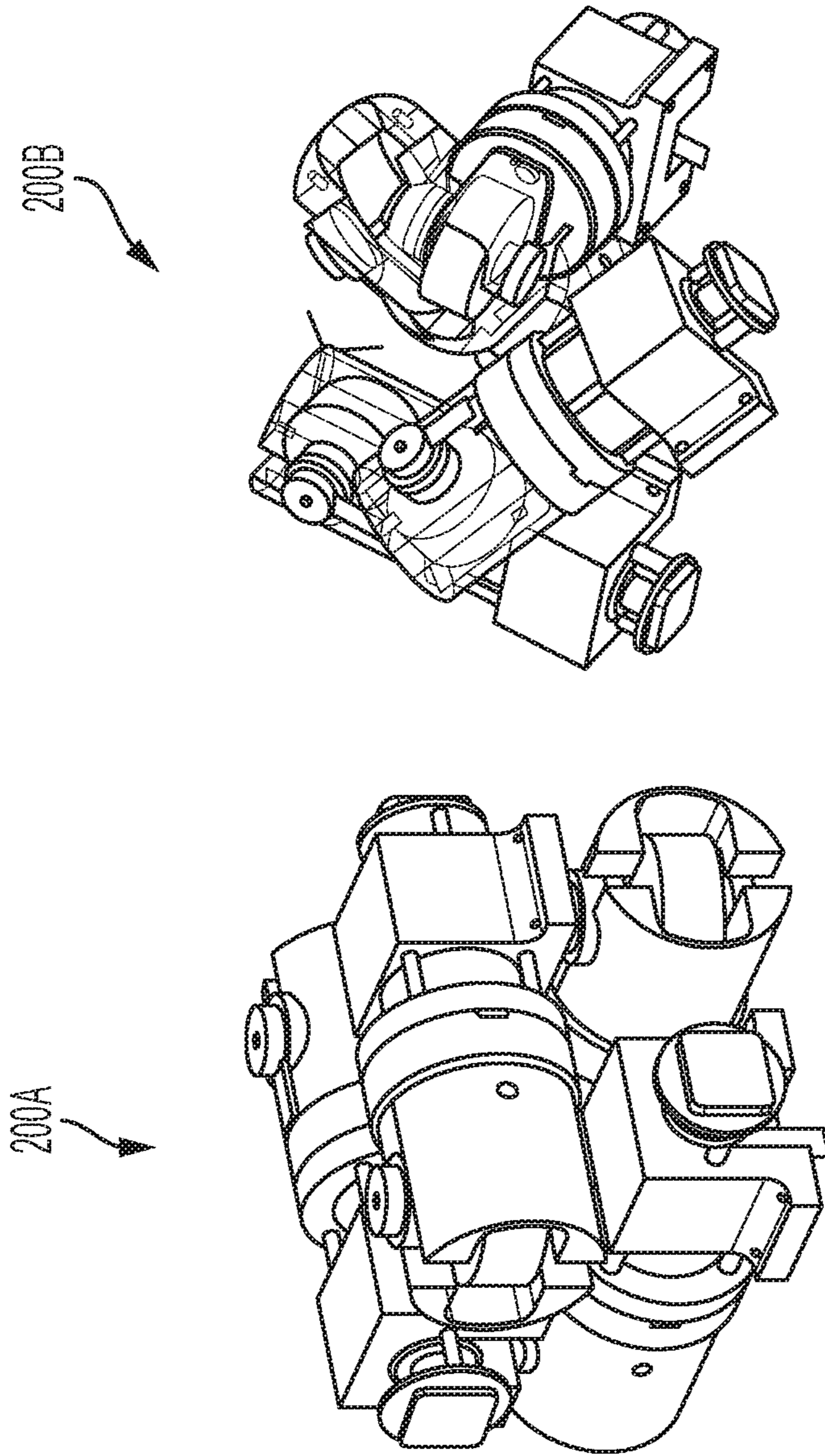


FIG. 1



$\beta = 57.4^\circ$

FIG. 2B

$\beta = 90^\circ$

FIG. 2A

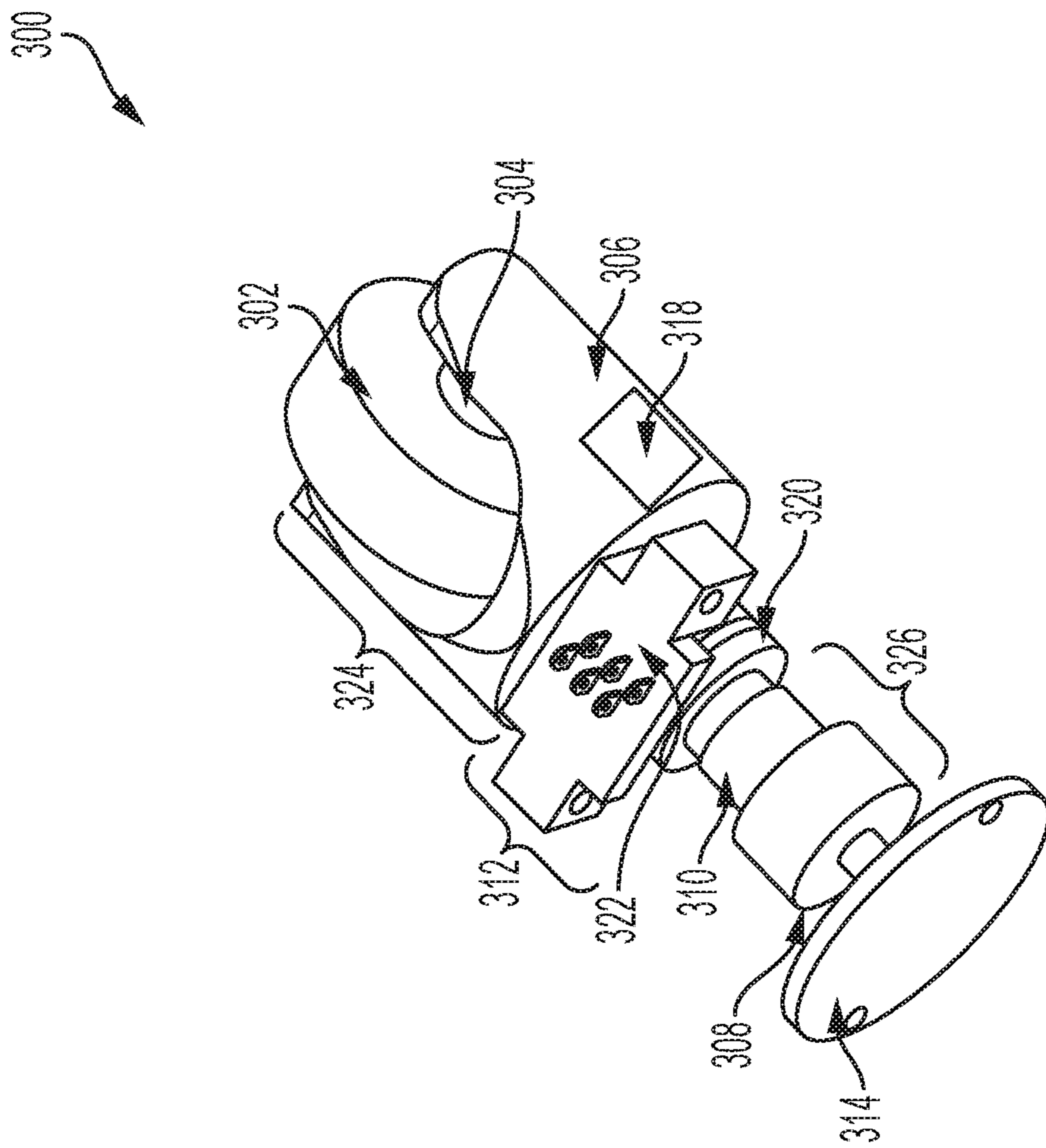


FIG. 3

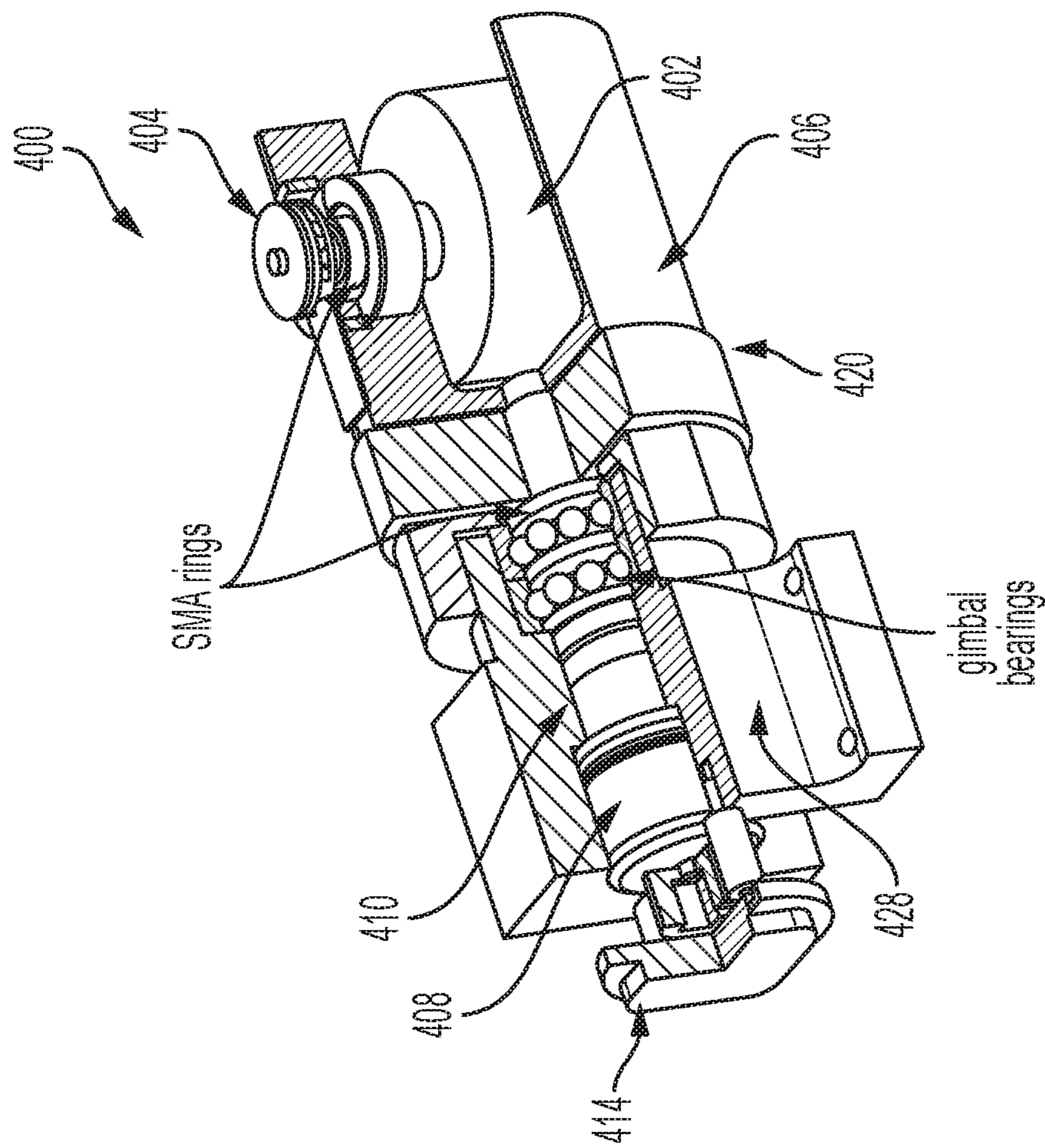
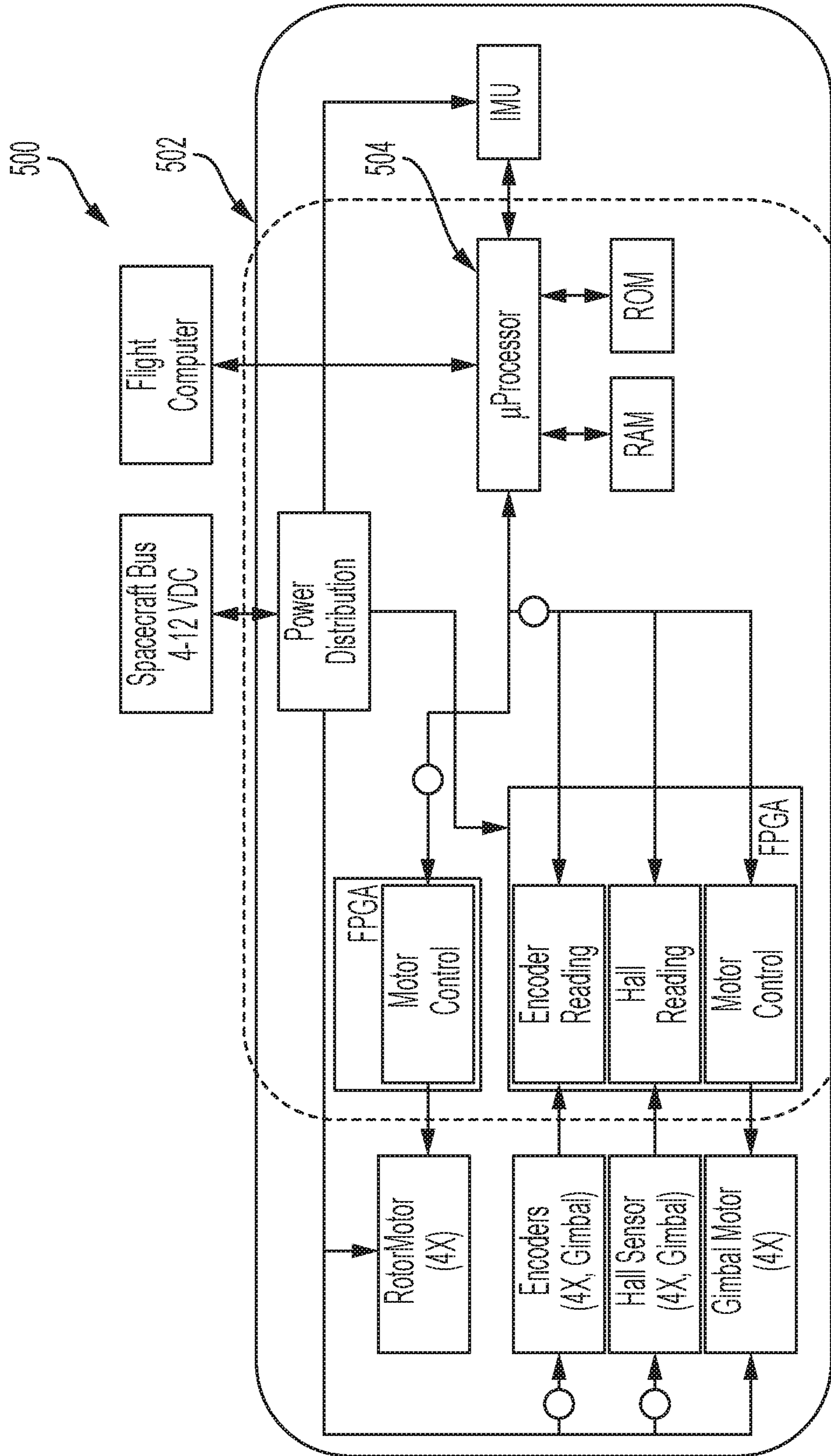


FIG. 4



○ = Single Switch Controlled by MicroP

FIG. 5

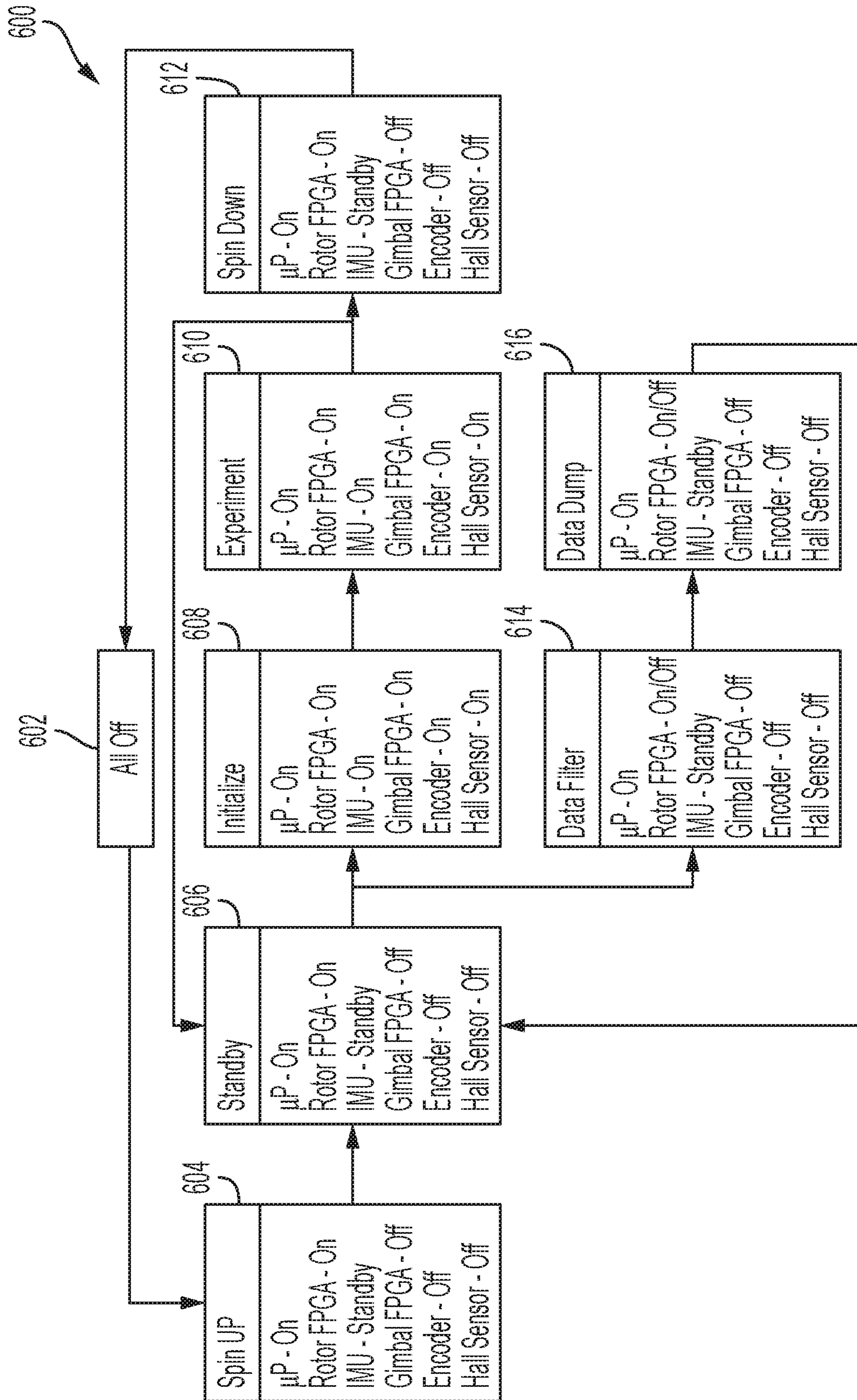


FIG. 6

1

AGILE ATTITUDE CONTROL SYSTEM FOR SMALL SPACECRAFT

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the benefit of U.S. Provisional Application No. 61/156,250, filed Feb. 27, 2009, and of U.S. Provisional Application No. 61/221,236, filed Jun. 29, 2009, each of which are hereby incorporated in their entirety by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates generally to attitude control systems. More particularly, the present invention relates to attitude control systems for small spacecraft.

2. Description of the Related Art

Existing attitude control systems for small spacecraft, such as nanosatellites, have limited generated torque and angular momentum storage capabilities. In particular, only one attitude control system is commercially available for the three axis attitude control system of small spacecraft, such as CubeSats. That system is a three-axis reaction wheel system and has limited generated torque and angular momentum storage capabilities.

SUMMARY OF THE INVENTION

Embodiments in accordance with the agile attitude control system (AACS) described herein provide agile and accurate attitude control for very small spacecraft, such as the class of nanosatellites. Embodiments in accordance with the agile attitude control system (AACS) described herein include miniature single gimbal control moment gyroscopes (SGCMGs) that provide higher torque/power ratios and higher torque/volume ratios than conventional reaction wheel systems currently used in small space systems.

In accordance with one embodiment, an agile attitude control system includes: a plurality of miniature single gimbal control moment gyroscopes (SGCMGs); and one or more electronic components coupled with the plurality of miniature SGCMGs. In one embodiment, the agile attitude control system is entirely contained within the volume of 1 liter or less and has a total mass of 1 kilogram or less. In one embodiment, the plurality of miniature SGCMGs are arranged in a "Box 90" configuration with $\beta=90^\circ$. In another embodiment, the plurality of miniature SGCMGs arranged in a pyramidal configuration with base angle $\beta=57.4^\circ$.

In accordance with another embodiment, a miniature single gimbal control moment gyroscope (SGCMG) includes: a single flywheel rotor assembly; a slip ring assembly coupled with the rotor assembly; a gimbal assembly coupled with the slip ring assembly; and a magnetic encoder coupled with the gimbal assembly. In one embodiment, the miniature SGCMG further includes a hall sensor.

Embodiments in accordance with the invention are best understood by reference to the following detailed description when read in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a generalized perspective volume allocation block drawing of an agile attitude control system (AACS) in accordance with one embodiment.

2

FIG. 2A illustrates an example of miniature SGCMGs arranged in a "Box 90" configuration with $\beta=90^\circ$ in accordance with one embodiment.

FIG. 2B illustrates an example of miniature SGCMGs arranged in a pyramidal configuration with base angle $\beta=57.4^\circ$ in accordance with another embodiment.

FIG. 3 illustrates a perspective drawing of a miniature single gimbal control moment gyroscope (SGCMG) in accordance with one embodiment.

FIG. 4 illustrates a cutaway perspective drawing of a miniature SGCMG and includes a gimbal housing in accordance with one embodiment.

FIG. 5 illustrates a high level architecture of an agile attitude control system (AACS) in accordance with one embodiment.

FIG. 6 illustrates a process diagram of operational flow of an AACS implemented as a standalone system in accordance with one embodiment.

Embodiments in accordance with the invention are further described herein with reference to the drawings.

DETAILED DESCRIPTION OF THE INVENTION

Embodiments in accordance with the agile attitude control system (AACS) described herein provide agile and accurate attitude control for very small spacecraft, such as the class of nanosatellites. Herein the phrase small spacecraft refers to the class of nanosatellites generally termed by those of skill in the art of space systems to indicate spacecraft with mass of the order of 1 kg (kilogram) to 10 kg. Nanosatellites include, in particular, the CubeSat spacecraft class.

Embodiments in accordance with the agile attitude control system described herein provide substantially improved performance over prior art systems with regard to the term of maximum output torque and, especially, maximum angular momentum storage. The higher angular momentum capability enables a much higher slewing rate to be achieved and allows disturbance torques to be rejected more effectively. Additionally, due at least in part to the physics of control moment gyroscopes, embodiments in accordance with the invention require less power to operate.

More particularly, embodiments in accordance with the agile attitude control subsystem (AACS) described herein include miniature single gimbal control moment gyroscopes (SGCMGs). The miniature SGCMGs provide higher torque/power ratios and higher torque/volume ratio than conventional reaction wheel systems currently used in small space systems.

Generally viewed, the agile attitude control system (AACS) described herein is a three axis attitude control device for small spacecraft based on miniature single gimbal control moment gyroscopes (SGCMGs) actuators. The AACS enables agile attitude slewing and accurate pointing/tracking for spacecraft made of multiple (2-5+) CubeSat units, or, more generally, for nanosatellites. These attitude control capabilities are highly desirable for several critical space missions, such as Earth imaging, optical communications, and other DOD and civilian applications.

FIG. 1 is a generalized perspective volume allocation block drawing of an agile attitude control system (AACS) 100 in accordance with one embodiment. Referring now to FIG. 1, agile attitude control system (AACS) 100 includes a plurality of miniature single gimbal control moment gyroscopes (SGCMGs) 102, 104, 106, 108; and one or more electronic components 110, 112, 114 communicatively coupled with the plurality of miniature SGCMGs 102, 104,

106, 108. One or more electronic components **110, 112, 114** include: a control electronic component; an amplifier electronic component; and a power conversion electronic component.

In one embodiment, AACS **100** is entirely contained within the volume of 1 liter or less and has a total mass of 1 kilogram or less. In a further embodiment, AACS **100** is entirely contained in a cube shape of 10 cm (centimeters) per side and within a volume at or less than 1 liter and has a total mass at or less than 1 kilogram.

In an illustrative embodiment, electronic components **112, 114** are 9.4 cm×3.0 cm×1.7 cm in size and electronic component **110** is 9.4 cm×9.4 cm×2.5 cm in size. In one embodiment, the electronics are designed as printed circuit boards (PCBs). Electronic component **110** is the control electronic component, electronic component **112** is the amplifier electronic component, and electronic component **114** is the power conversion electronic component.

AACS **100** includes a structural interface (not shown) for fixing the plurality of miniature SGCMGs **102, 104, 106, 108** and the one or more electronic components **110, 112, 114** in specified positions. AACS **100** further includes a structural interface (not shown) that further provides electrical, data, and mechanical interconnections between AACS **100** and one or more external systems, such as a nanosatellite, CubeSat, or other small spacecraft (not shown). The structural interface surrounds miniature SGCMGs **102, 104, 106, 108** and electronic components **110, 112, 114** and is openly structured to facilitate integration with the external structure to allow access for wirings and for hosting elements external to AACS **100**. The structural interface fixes the plurality of miniature SGCMGs **102, 104, 106, 108** in a specified orientation. The structural interface is any structure that keeps the elements in FIG. **1** suitably connected in the configuration shown in FIGS. **1, 2A** and **2B**, such as for example, an openly structured box, cube or box-like structure.

In one embodiment, AACS **100** includes four miniature single gimbal control moment gyroscopes (SGCMGs): miniature SGCMG **102**, a first miniature SGCMG, miniature SGCMG **104**, a second miniature SGCMG, miniature SGCMG **106**, a third miniature SGCMG, and miniature SGCMG **108**, a fourth miniature SGCMG.

In one embodiment, miniature SGCMGs **102, 104, 106, 108** are arranged in a box formation with base angle $\beta=90^\circ$ as illustrated in FIG. **1**. This formation is sometimes termed a “Box 90” configuration by those of skill in the art. FIG. **2A** illustrates an example of miniature SGCMGs **102, 104, 106, 108** arranged in a “Box 90” configuration **200A** with $\beta=90^\circ$.

In another embodiment, miniature SGCMGs **102, 104, 106, 108** are arranged in a pyramidal configuration with base angle $\beta=57.4^\circ$, and the angular momentum envelope results in a sphere with radius of at or about 7 mN-m-s. A cube with sides of length 31 mN-m-s would fit inside that sphere, resulting in the ability to provide 15.4 mN-m-s about all three axes simultaneously. FIG. **2B** illustrates an example of miniature SGCMGs **102, 104, 106, 108** arranged in a pyramidal configuration **200B** with base angle $\beta=57.4^\circ$.

In an illustrative embodiment, each miniature SGCMG **102, 104, 106, 108** has dimensions 32 mm (millimeters) in diameter by 76 mm long. Each miniature SGCMG has 8.4 mN-m-s (millinewton meter per second) of angular momentum. The maximum output torque is at least 10 mN-m. The overall power consumption is between the range at or about 0.4 W to 1.5 W.

In one embodiment, at least three miniature magnetotorquers (not shown) are used together with miniature SGC-

MGs **102, 104, 106, 108** for angular momentum dumping. The miniature magnetotorquers are mounted internally to AACS **100**, while in alternate embodiments, the miniature magnetotorquers are mounted in another location on or in the external structure, e.g. the small spacecraft.

FIG. **3** illustrates a perspective drawing of a miniature SGCMG **102** in accordance with one embodiment. FIG. **4** illustrates a cutaway perspective drawing of the miniature SGCMG of FIG. **3** and includes a gimbal housing in accordance with one embodiment. Referring now to FIGS. **3** and **4**, each miniature SGCMG **102, 104, 106, 108**, represented here by miniature SGCMG **102** for ease of description, includes a rotor assembly **324** including a single flywheel rotor **302** coupled with a rotor motor **304** and encased in a rotor housing **306**. A slip ring assembly **312** couples rotor assembly **324** to a gimbal assembly **326** including a gimbal motor **308** with harmonic drive gear **310** encased in a gimbal housing **328**. A magnetic encoder **314** is coupled to gimbal assembly **326**. In one embodiment, a hall sensor **318** is coupled to rotor assembly **324**. In another embodiment, hall sensor **318** is coupled to rotor housing **306**.

In operation, magnetic encoder **314** reads the angular position of gimbal motor **308**. In one embodiment, gimbal housing **328** mounts to a stationary surface tied to a primary external structure. In another embodiment, gimbal housing **328** is mounted on a structural interface of AACS **100**.

Gimbal motor **308** rotates rotor assembly **324** through the harmonic gear driven shaft of harmonic gear **310**. Slip ring assembly **312** passes motor winding connections through the rotary joint allowing continuous 360° operation. In an illustrative embodiment, rotor **302** is mounted with a compliant preloaded set of duplex pair angular contact bearings internal to rotor housing **306**. In one embodiment, both the gimbal bearings and rotor bearings are mounted with the aid of shape-memory alloy (SMA) retaining rings.

Rotor **302** is actuated by rotor motor **304**, which in an illustrative embodiment, is a brushless DC motor. Slip ring assembly **312** includes space rated slip rings **320** connected to a slip ring brush block **322** and is used for electrical connection of rotor motor **304**.

Gimbal motor **308** is connected to slip ring assembly **312**. In an illustrative embodiment, gimbal motor **308** is a brushless DC motor and is integrated with harmonic drive gear **310**. Magnetic encoder **314** is connected to gimbal motor **308**. Magnetic encoder **314** is used to accurately measure the angular position of gimbal assembly **326** with respect to the external structure, e.g., a spacecraft. In one embodiment magnetic encoder **314** is a non-contact magnetic encoder.

In an illustrative embodiment, gimbal motor **308** is a Maxon ECF **14** brushless DC motor, part number 339251 with Braycote grease and a power rating of 1.5 W (available from Maxon Motor, Switzerland). In operation the gimbal rate of gimbal motor **308** is controllable to within $\pm 0.5^\circ/\text{sec}$ on the slow speed side. In one embodiment, the gimbal rate commands are bidirectional and from 0 to $\pm 20^\circ/\text{sec}$ (0.35 rad/sec).

In an illustrative embodiment, rotor motor **304** is a Maxon EC10F motor, part number 30199 with Braycote grease and power rating of 0.2 W (available from Maxon Motor, Switzerland). In operation rotor motor **304** has a nominal spin rate of 12,000 rpm and peak of 15,000 rpm. Rotor motor **304** speed is controllable to within ± 150 rpm of the desired value during all modes of operation. Rotor motor **304** spins in the clockwise direction, looking at rotor motor **304** from rotor **302**.

In an illustrative embodiment, slip ring assembly **312** is a Sibley Company 5 power ring assembly rated at 0.75 amps @ 12V with a 6 RPM max but not continuous from -20° C. to $+50^{\circ}$ C. and is bi-directional (available from The Sibley Company, Connecticut). Slip ring assembly **312** further has ID minimum=0.250" and OD maximum=1.25".

In an illustrative embodiment, magnetic encoder **314** is a magnetic encoder from Renishaw with option **1B** for increased temperature operation (available from Renishaw Inc., Illinois). In an illustrative embodiment, magnetic encoder **314** is a RMB201C series 13 bit incremental encoder for 8192 counts per revolutions. With a gear reduction of 160:1 from the harmonic gear, the motor output has 1,310,720 cts/rev or a count every 0.00027 deg (0.99 arc sec). The magnet rotates clockwise.

In an illustrative embodiment, harmonic gear **310** is a MicroMotion harmonic gear, part number MHD-10 (available from MicroMotion-gmbh, Germany) and is installed directly on gimbal motor **308**.

In an illustrative embodiment, hall sensor **318** is an Optek OMH3040B hall sensor (available from OPTEK Technology, Texas) used on the slow speed side of rotor assembly **324** as an index for the position measurements.

In an illustrative embodiment, miniature SGCMGs **102**, **104**, **106**, **108** are packaged in AACS **100** together with driver electronics for rotor motor **304** and gimbal motor **308** based on printed circuit board (PCB) technology. In this embodiment, a printed circuit board including non-volatile memory is included in AACS **100**, for example, in electronic components **110**, **112**, and/or **114**. The printed circuit board is based on FPGA, ASICS or other microprocessor technology.

Although not shown in FIGS. **1-4** it can be understood by those of skill in the art that mechanical, electronic and data connections are included and can be implemented in various configurations.

FIG. **5** illustrates a high level architecture **500** of an agile attitude control system (AACS) **100** system in accordance with one embodiment. Referring to FIG. **5**, AACS **100** system is a self-contained suite including one or more micro-processors which can perform attitude determination with embedded inertial measurement unit (IMU) and/or external sensors. The one or more microprocessors then commands the gimbal and motor rates.

In this embodiment, a printed circuit board **502** includes a microprocessor **504** which runs, i.e., executes, software including: (1) an attitude control algorithm; (2) a gimbal steering law algorithm; (3) an internal singularity avoidance algorithm; and (4) one or more momentum dumping algorithms.

Microprocessor **504** performs steering laws, singularity avoidance, communication to flight computer, communication to field programmable gate array(s) (FPGAs), fault detection mode selection, data storage, attitude determination and control. Microprocessor **504** runs preplanned experimental maneuvers or accepts external torque commands in the spacecraft coordinate system. Microprocessor **504** shuts down components not in use for specific modes via digitally activated switches.

Microprocessor **504** includes functions that perform attitude determination with an embedded IMU and/or with external sensors. Microprocessor **504** then controls the gimbal and motor rates via field programmable gate array(s) (FPGAs). In one embodiment, the FPGA(s) are used as motion controllers with the ability to incorporate magnetic encoder **314** and hall sensor **318** feedback. The FPGA(s) are responsible for determining the gimbal speed and positions

(slow speed side) and to report back to microprocessor **504**. In one embodiment, separate FPGAs are used to control the motor rotors **304** and gimbal motors **308**. In a further embodiment, a separate FPGA controls all four rotor motors **304** at a constant rate.

It can be understood by those of skill in the art that the above detailed architecture **500** is but one example and that a variety of other architectures are also possible.

FIG. **6** illustrates a process diagram of operational flow of an AACS **100** as a standalone system in accordance with one embodiment. Referring now to FIG. **6**, AACS **100** can be operated as a standalone system in either a ground test bed or flight experiment. After spacecraft checkout, AACS **100** is powered up and rotor motors, i.e., rotor motors **304**, are spun up to a constant speed. Rotor motors **304** remain at that constant speed unless an internal fault is detected or commanded by the external system, e.g., the spacecraft, to spin down due to a higher level fault. AACS **100** is at its quiescent power profile for this period. The spacecraft is uncontrolled by AACS **100** in this regime.

For pre-planned maneuvers, the program moves through a series of modes described below for a total experiment time of less than 5 minutes. The AACs system can reach its peak power at this time. The AACS system can be commanded indefinitely in direct torque control or 3-axis stabilization modes (optional). The flight computer can then choose when to remove the saved/processed IMU (inertial measurement unit) data for dumping to the ground.

The data filtering or dumping modes can be run while the system is in standby. After a nominal experiment, the system returns to the standby mode. Multiple types of experiments can be run.

Referring to FIGS. **5** and **6**, in All Off mode **602** all power is turned off to all systems and microprocessor **604** is set to a sleep mode. In Spin Up mode **604** the rotor FPGA controller is turned on. The rotor motors **304** are brought up to the set constant speed. In Standby mode **606** microprocessor **604** and rotor FPGAs are on commanding a constant rotor speed. All other systems are off.

In Initialization mode **608**, encoders, hall sensors, IMU and gimbal FPGAs are turned on. Gimbal motors **308** are rotated until the hall sensor position is detected from gimbal positions initialization and IMU data is recorded. In Experiment mode **610**, the pre-planned or torque commanded experiment is run based on the experiment sub-mode. All maneuvers end with the gimbal returning to an indexed, "home" position at the hall sensor. In Spin Down mode **612**, rotor motor angular speeds are brought down to zero speed. In Data Filter mode **614** IMU data is post processed to reduce its size before sending to the flight computer. In Data Dump mode **616**, filtered IMU data is given to the flight computer for down linking to the ground at a future time.

It can be understood by those of skill in the art that the above detailed process **600** is but one example and that a variety of other system processes are also possible.

Embodiments in accordance with the agile attitude control system described herein provide substantially improved performance over existing attitude control systems for small spacecraft with regard to the term of maximum output torque and, especially, maximum angular momentum storage. The higher angular momentum capability enables a much higher slewing rate to be achieved and allows disturbance torques to be rejected more effectively. Additionally, due at least in part to the physics of control moment gyroscopes, embodiments in accordance with the invention can require less power to operate.

This disclosure provides exemplary embodiments of the present invention. The scope of the present invention is not limited by these exemplary embodiments. Numerous variations, whether explicitly provided for by the specification or implied by the specification or not, may be implemented by one of skill in the art in view of this disclosure.

What is claimed is:

1. An agile attitude control system (AACS) comprising:
 - a plurality of miniature single gimbal control moment gyroscopes (SGCMGs), wherein each of said miniature SGCMGs further comprises:
 - a single flywheel rotor assembly, said single flywheel rotor assembly further comprising:
 - a rotor motor,
 - one or more rotor bearings, and
 - a rotor housing enclosing said rotor motor and said one or more rotor bearings;
 - a gimbal assembly, said gimbal assembly further comprising:
 - a gimbal motor,
 - a harmonic drive gear,
 - one or more gimbal bearings, and
 - a gimbal housing enclosing said gimbal motor and said one or more gimbal bearings;
 - a slip ring assembly coupled with said single flywheel rotor assembly and with said gimbal assembly, said slip ring assembly located between said single flywheel rotor assembly and said gimbal assembly;
 - a magnetic encoder coupled with said gimbal assembly; and
 - a hall sensor coupled with said single flywheel rotor assembly; and
 - one or more electronic components coupled with said plurality of miniature SGCMGs,
 - wherein said agile attitude control system is entirely contained within the volume of 1 liter or less and has a total mass of 1 kilogram or less.
2. The agile attitude control system (AACS) of claim 1 wherein said one or more electronic components comprise:
 - a control electronic component;
 - an amplifier electronic component; and
 - a power conversion electronic component.
3. The agile attitude control system of claim 1 wherein said plurality of miniature SGCMGs comprises:
 - a first miniature SGCMG;
 - a second miniature SGCMG;
 - a third miniature SGCMG; and
 - a fourth miniature SGMG.
4. The agile attitude control system of claim 3 wherein said plurality of miniature SGCMGs are arranged in a pyramidal configuration with base angle $\beta=57.4^\circ$.
5. The agile attitude control system of claim 3 wherein said plurality of miniature SGCMGs are arranged in a box 90 configuration with base angle $\beta=90^\circ$.
6. The agile attitude control system of claim 1 further comprising:
 - a structural interface, said structural interface fixing said plurality of miniature SGCMGs and said one or more electronic components in specified positions within a cube shape of about 10 cm per cube side.
7. A miniature single gimbal control moment gyroscope (SGCMG) comprising:
 - a single flywheel rotor assembly, said single flywheel rotor assembly further comprising:
 - a rotor motor,
 - one or more rotor bearings, and

- a rotor housing enclosing said rotor motor and said one or more rotor bearings;
 - a gimbal assembly, said gimbal assembly further comprising:
 - a gimbal motor,
 - a harmonic drive gear,
 - one or more gimbal bearings, and
 - a gimbal housing enclosing said gimbal motor and said one or more gimbal bearings;
 - a slip ring assembly coupled with said single flywheel rotor assembly and with said gimbal assembly, said slip ring assembly located between said single flywheel rotor assembly and said gimbal assembly;
 - a magnetic encoder coupled with said gimbal assembly; and
 - a hall sensor coupled with said single flywheel rotor assembly.
8. The miniature single gimbal control moment gyroscope (SGCMG) of claim 7 wherein said miniature SGCMG has dimensions 32 mm (millimeters) in diameter by 76 mm long.
 9. The miniature single gimbal control moment gyroscope (SGCMG) of claim 7 wherein said miniature SGCMG has 8.4 mN-m-s (millinewton meter per second) of angular momentum.
 10. The miniature single gimbal control moment gyroscope (SGCMG) of claim 7 wherein said miniature SGCMG is for use in attitude control of small spacecraft.
 11. An agile attitude control system (AACS) for three axis attitude control of small spacecraft comprising:
 - a plurality of miniature single gimbal control moment gyroscopes (SGCMGs), wherein each of said miniature SGCMGs further comprises:
 - a single flywheel rotor assembly, said single flywheel rotor assembly further comprising:
 - a rotor motor,
 - one or more rotor bearings, and
 - a rotor housing enclosing said rotor motor and said one or more rotor bearings;
 - a gimbal assembly, said gimbal assembly further comprising:
 - a gimbal motor,
 - a harmonic drive gear,
 - one or more gimbal bearings, and
 - a gimbal housing enclosing said gimbal motor and said one or more gimbal bearings;
 - a slip ring assembly gimbal coupled with said single flywheel rotor assembly and with said gimbal assembly, said slip ring assembly located between said single flywheel rotor assembly and said gimbal assembly; and
 - one or more electronic means coupled with said plurality of miniature SGCMGs, said one or more electronic means for controlling said plurality of miniature SGCMGs to provide three axis attitude control of external small spacecraft,
 - wherein said agile attitude control system is entirely contained within the volume of 1 liter or less and has a total mass of 1 kilogram or less.
 12. The agile attitude control system of claim 11 wherein said plurality of miniature SGCMGs comprises:
 - a first miniature SGCMG;
 - a second miniature SGCMG;
 - a third miniature SGCMG; and
 - a fourth miniature SGMG,
 and further wherein said plurality of miniature SGCMGs are arranged in a pyramidal configuration with base angle $\beta=57.4^\circ$.

13. The agile attitude control system of claim **11** wherein said plurality of miniature SGCMGs comprises:

a first miniature SGCMG;

a second miniature SGCMG;

a third miniature SGCMG; and

5

a fourth miniature SGMG,

and further wherein said plurality of miniature SGCMGs are arranged in a box 90 configuration with base angle $\beta=90^\circ$.

14. The agile attitude control system of claim **11** further comprising:

10

a structural interface, said structural interface fixing said plurality of miniature SGCMGs and said one or more electronic components in specified positions.

15. The agile attitude control system of claim **11** wherein said agile attitude control system is connectable to said external small spacecraft.

15

* * * * *