



US010385898B2

(12) **United States Patent**  
**Pourtier**

(10) **Patent No.:** **US 10,385,898 B2**  
(45) **Date of Patent:** **Aug. 20, 2019**

(54) **EXPANDING WALL ANCHOR AND USE FOR FIXING A COMPONENT TO A SUPPORT MATERIAL**

USPC ..... 411/60.1  
See application file for complete search history.

(71) Applicant: **ILLINOIS TOOL WORKS INC.**,  
Glenview, IL (US)

(56) **References Cited**

(72) Inventor: **Fabrice Pourtier**, Portes-les-Valence  
(FR)

U.S. PATENT DOCUMENTS

(73) Assignee: **Illinois Tool Works Inc.**, Glenview, IL  
(US)

3,709,089 A \* 1/1973 Seetaram ..... F16B 13/065  
411/61  
3,922,947 A \* 12/1975 Leonardo ..... F16B 13/065  
411/60.3  
4,314,784 A \* 2/1982 Tausig ..... F16B 13/065  
411/361  
4,474,516 A \* 10/1984 Schiefer ..... F16B 13/065  
411/44

(\* ) Notice: Subject to any disclaimer, the term of this  
patent is extended or adjusted under 35  
U.S.C. 154(b) by 44 days.

(Continued)

(21) Appl. No.: **15/036,088**

FOREIGN PATENT DOCUMENTS

(22) PCT Filed: **Aug. 21, 2014**

WO 2012120488 A1 9/2012

(86) PCT No.: **PCT/US2014/052199**

OTHER PUBLICATIONS

§ 371 (c)(1),

(2) Date: **May 12, 2016**

ISR and WO for PCT/US2014/052199 dated Oct. 22, 2014.

(87) PCT Pub. No.: **WO2015/073085**

*Primary Examiner* — Gary W Estremsky

(74) *Attorney, Agent, or Firm* — Neal, Gerber &  
Eisenberg LLP

PCT Pub. Date: **May 21, 2015**

(65) **Prior Publication Data**

US 2016/0273570 A1 Sep. 22, 2016

(57) **ABSTRACT**

(30) **Foreign Application Priority Data**

Nov. 13, 2013 (FR) ..... 13 61072

Expanding wall anchor, comprising (i) a threaded longitudinal body formed as a single piece with an expansion cone at one of its ends, this cone being connected to the rest of the body by a cylindrical portion of diameter  $d_1$  smaller than the nominal diameter  $D$  of the body, and (ii) an expanding sleeve of thickness  $e$  mounted around the said cylindrical portion of the body and through which the expansion cone is intended to be moved in order to deform the sleeve and anchor the wall anchor in a hole in a support material, characterized in that the ratio  $d_1/D$  is greater than or equal to 60% and the ratio  $e/d_1$  is greater than or equal to 22%.

(51) **Int. Cl.**

**F16B 13/06** (2006.01)

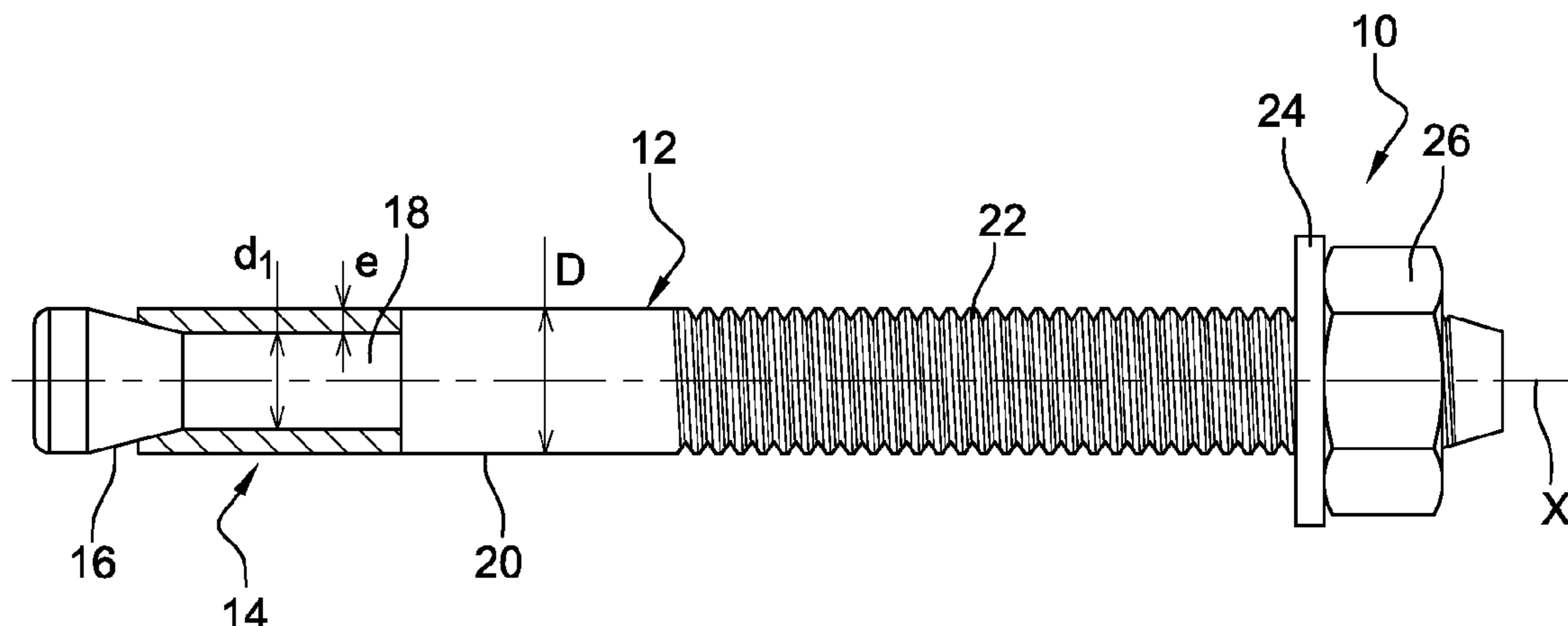
(52) **U.S. Cl.**

CPC ..... **F16B 13/065** (2013.01)

(58) **Field of Classification Search**

CPC ..... F16B 13/065

**19 Claims, 1 Drawing Sheet**



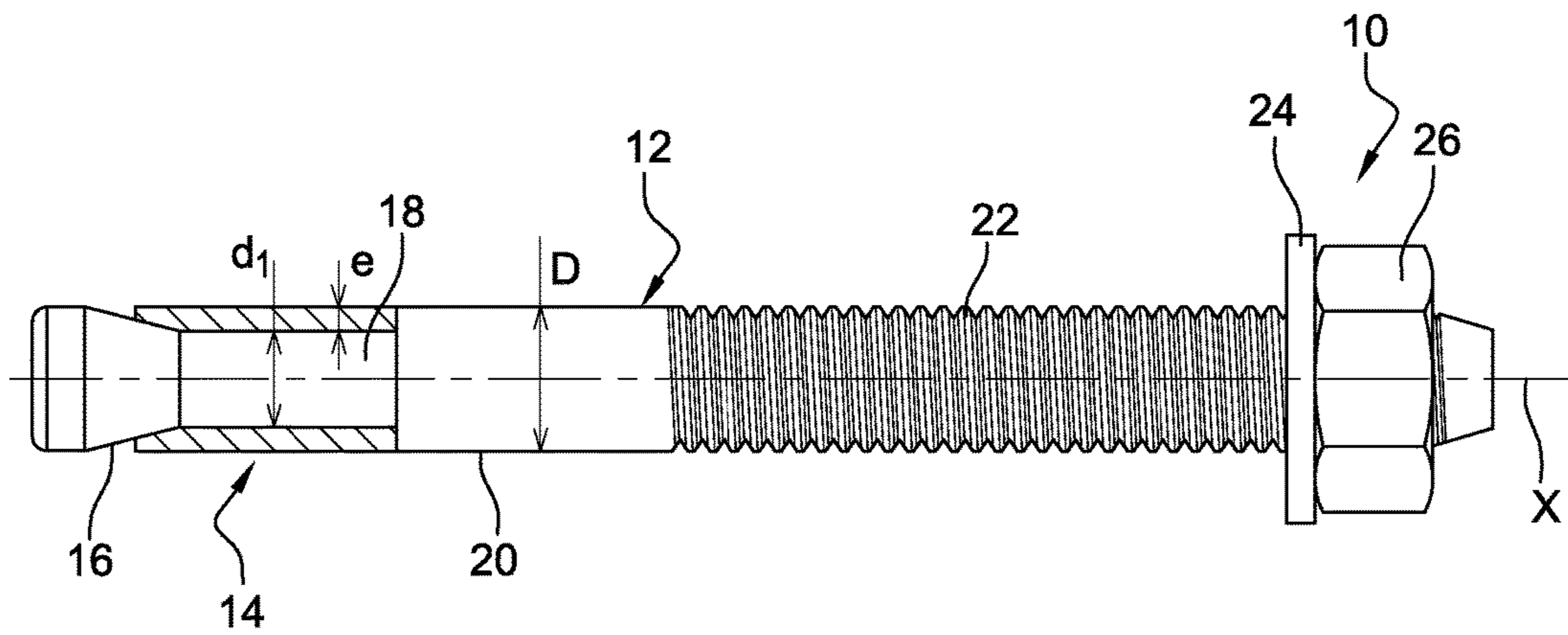
(56)

References Cited

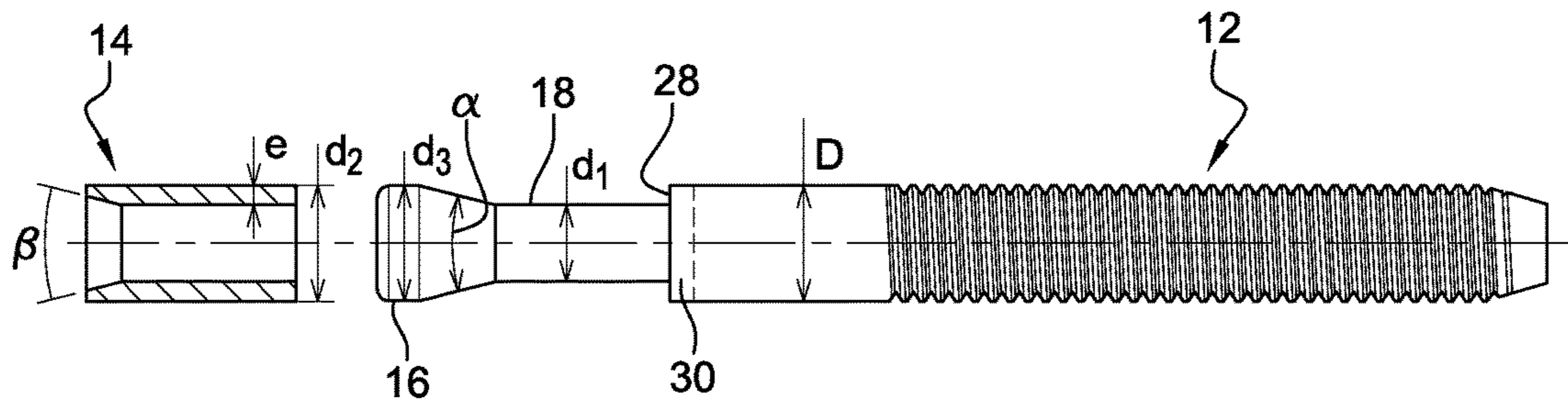
U.S. PATENT DOCUMENTS

4,519,735 A *	5/1985	Machtle .....	F16B 13/066	411/65	5,374,145 A *	12/1994	Mairesse .....	F01D 5/3023	29/525.11
4,688,977 A *	8/1987	Seetaram .....	F16B 13/066	411/45	5,419,664 A *	5/1995	Hengesbach .....	F16B 13/065	405/259.1
4,797,044 A *	1/1989	Velasco .....	F16B 13/065	411/45	5,569,091 A *	10/1996	Haage .....	F16B 13/065	411/40
4,869,632 A *	9/1989	Radtke .....	F01D 5/066	403/408.1	5,666,633 A *	9/1997	Arnold .....	B22F 3/225	419/10
4,929,134 A *	5/1990	Bergner .....	F16B 13/004	411/30	5,816,760 A *	10/1998	Mattner .....	F16B 13/004	411/30
4,968,200 A *	11/1990	Mark .....	F16B 13/065	411/55	6,027,292 A *	2/2000	Raber .....	F16B 13/065	411/60.1
4,971,494 A *	11/1990	Gauthier .....	F16B 13/065	411/55	6,524,046 B2 *	2/2003	Hsu .....	F16B 13/065	411/51
4,983,082 A *	1/1991	Mark .....	F16B 13/065	411/55	8,511,035 B2 *	8/2013	Zimmer .....	F16B 13/144	411/32
5,193,957 A *	3/1993	Fischer .....	F16B 13/065	411/55	8,678,730 B2 *	3/2014	Gaudron .....	F16B 13/065	411/37
5,211,512 A *	5/1993	Frischmann .....	F16B 13/065	405/259.4	2001/0010787 A1 *	8/2001	Hsu .....	F16B 13/065	411/61
5,284,409 A *	2/1994	Miyanaga .....	F16B 13/065	411/55	2010/0104393 A1	4/2010	Kobetsky et al.		
5,314,278 A *	5/1994	Weber .....	F16B 13/065	411/55	2013/0040743 A1 *	2/2013	Kind .....	B21H 1/18	470/2
					2014/0133933 A1 *	5/2014	Shimahara .....	B21H 3/022	411/44
					2014/0154025 A1	6/2014	Bergez et al.		

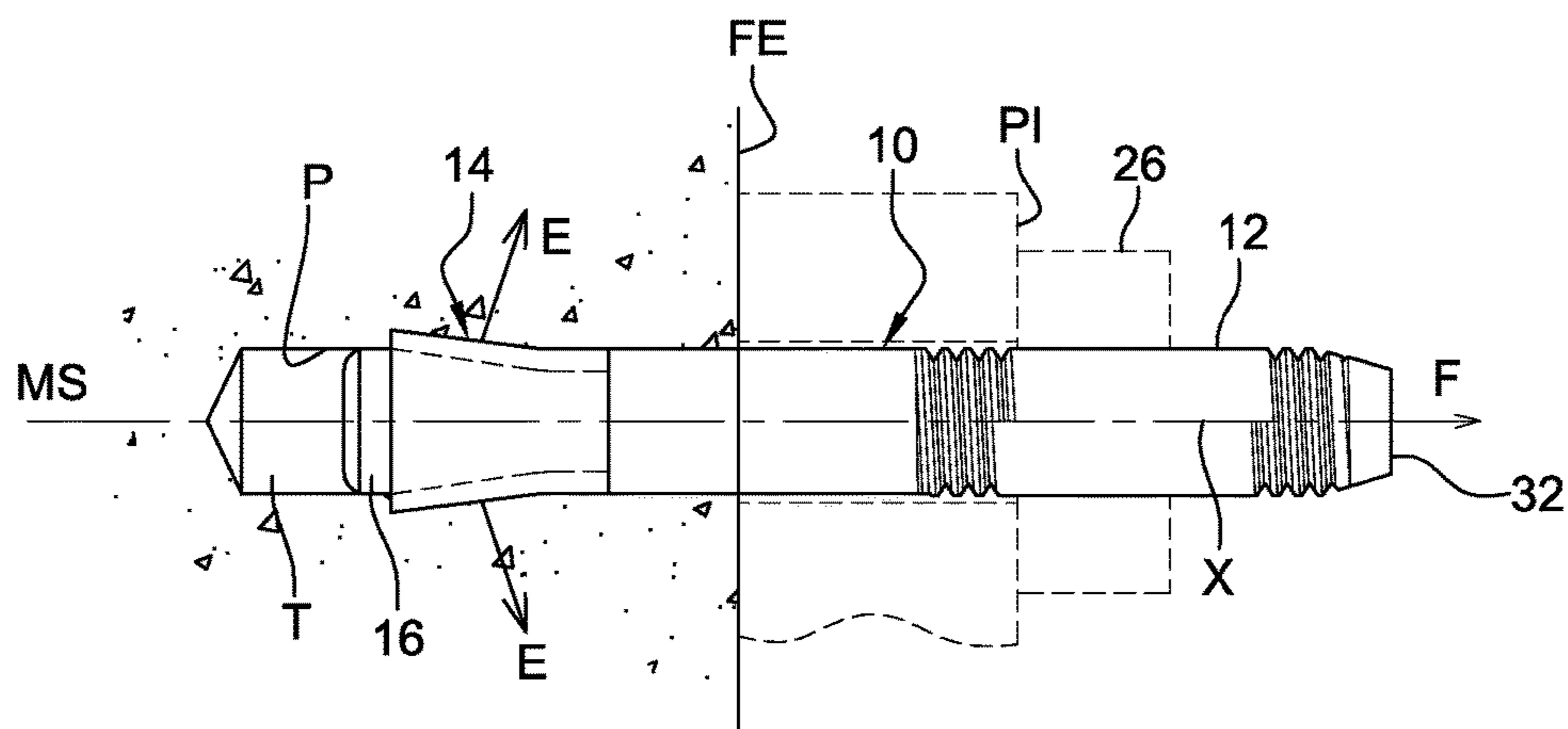
\* cited by examiner



**Fig. 1**



**Fig. 2**



**Fig. 3**

**EXPANDING WALL ANCHOR AND USE FOR  
FIXING A COMPONENT TO A SUPPORT  
MATERIAL**

RELATED APPLICATIONS

The present application is a National Phase of International Application Number PCT/US2014/052199, filed Aug. 21, 2014, and claims priority to French Application Number 1361072, filed Nov. 13, 2013.

TECHNICAL FIELD

The invention relates to an expanding wall anchor and its use for fixing a component to a support material, particularly a support material liable to be subjected to seismic loadings.

PRIOR ART

Typically, an expanding wall anchor comprises i) a threaded longitudinal body formed as a single piece with an expansion cone at one of its ends, this cone being connected to the rest of the body by a cylindrical portion of diameter smaller than the nominal diameter of the body, and ii) an expanding sleeve mounted around the said cylindrical portion of the body and through which the expansion cone is intended to be moved in order to deform the sleeve and anchor the wall anchor in a hole in a support material.

Documents US-A1-2010/0104393 and WO-A1-2012/120488 describe wall anchors of this type.

A wall anchor of this type is generally used in a concrete support after a receiving hole has been drilled therein with the nominal diameter of the body. The end part of the wall anchor comprising the expansion cone and bearing the expanding sleeve is forcibly engaged in this hole, for example by striking the wall anchor with a hammer. The component to be fixed is attached to the support material in such a way that the threaded part of the wall anchor passes through the component to be fixed, this threaded part accepting a nut that clamps the component against the support material. This clamping causes the body to undergo an axial translational movement with respect to the sleeve of the wall anchor, towards the outside end of the hole. The cone of the body therefore collaborates with the sleeve and forces it to expand, thus anchoring the sleeve in the support material and retaining the wall anchor with respect to the support material.

After the sleeve has been expanded, the tensile strength of this type of wall anchor is generally dependent on the cross section of the cylindrical portion of the body housing the sleeve, which is the smallest-diameter portion of the body of the wall anchor (as long as the sleeve holds fast in the support material and as long as the latter is able to withstand the stresses generated by the fixing).

However, regulations in this area are now evolving towards products that have been type tested for seismic loadings. This results in increasingly strict product testing conditions. In particular, the products have to undergo dynamic testing in cracked concrete the crack widths of which increase with each new seismic condition. The known products which were able to meet the earlier type testing certification conditions generally experience a drop in their performance, or even sometimes are no longer able to function at all under seismic loadings.

These changes to the type testing certification conditions, particularly the increase in the width of the cracks in the support material accepting this type of wall anchor during

the certification testing, mean that the sleeve has greater difficulty holding fast in the support material, or suitably holding the body of the wall anchor when the latter experiences seismic loadings.

5 The present invention proposes a simple, effective and economical solution to this problem.

SUMMARY OF THE INVENTION

10 The invention thus proposes an expanding wall anchor, comprising:

i) a threaded longitudinal body formed as a single piece with an expansion cone at one of its ends, this cone being connected to the rest of the body by a cylindrical portion of diameter  $d_1$  smaller than the nominal diameter  $D$  of the body, and

15 ii) an expanding sleeve of thickness  $e$  mounted around the said cylindrical portion of the body and through which the expansion cone is intended to be moved in order to deform the sleeve and anchor the wall anchor in a hole in a support material,

characterized in that the ratio  $d_1/D$  is greater than or equal to 60% and the ratio  $e/d_1$  is greater than or equal to 22%.

In the present application,  $d_1$  is the (outside) diameter of the cylindrical portion of the body of the wall anchor, around which the sleeve is mounted.  $D$  is the nominal diameter of the body of the wall anchor, namely the maximum (outside) diameter of the body.  $e$  is the thickness of the sleeve and more specifically the thickness of material of this sleeve (which is equal to the thickness of the metal sheet used to produce the sleeve when the sleeve is made from such sheet metal). It is conceivable for the thickness of the sleeve not to be perfectly constant, particularly when that end of the sleeve that is situated at the expansion cone end is thinner. It is also conceivable for this thickness  $e$  to vary because of the presence of anchoring lugs on the external surface of the sleeve or of local slits in the sleeve. The thickness  $e$  of the sleeve can therefore be considered to be measured here some distance from its ends and away from any zones of the sleeve that have lugs or slits. The sleeve may have an outside diameter  $d_2$  substantially equal to the nominal diameter  $D$ . As indicated in the foregoing, this diameter  $d_2$  is preferably measured some distance from the ends of the sleeve and away from such zones as have lugs or slits.

25 The applicant company has sought to optimize dimensional parameters of the wall anchor and has discovered that a ratio  $e/d_1$  (the ratio of the thickness of the sleeve to the diameter of the cylindrical portion of the body on which the sleeve is mounted) greater than or equal to 22% unexpectedly makes it possible to achieve very good results in terms of the mechanical and vibratory performance of the wall anchor under seismic loadings, even when anchored in a crack that is relatively wide. The ratio  $d_1/D$  is greater than or equal to 60%, i.e. the diameter  $d_1$  is greater than 0.6  $D$ , making it possible to give the wall anchor sufficient mechanical strength because, as explained in the foregoing, the tensile strength of the wall anchor is generally dependent on the cross section of this smallest-section portion of the body (it being possible for  $D$  to be comprised between 6 and 30 mm and, for example, measuring 8, 10, 12 or 16 mm). From a given value of  $d_1$ , it is therefore possible to deduce the value of the sleeve thickness  $e$  that will give the wall anchor the desired properties. For a wall anchor of given nominal diameter  $D$ , this wall anchor will have a sleeve the thickness  $e$  of which will be greater than the thicknesses of the sleeves of the wall anchors of the prior art (in which the  $e/d_1$  ratios are markedly below 22%). Increasing the thick-

3

ness  $e$  of the sleeve allows it to be made less sensitive to the increase in the width of the cracks and allows it to hold more fast under seismic loadings. In the aforementioned instance in which the sleeve is made from sheet metal, that amounts to using a thicker metal sheet from which to make the sleeve of the wall anchor according to the invention.

The ratio  $e/d_1$  may be greater than or equal to 23, 24 or 25%.

This ratio  $e/d_1$  is preferably less than 35%, or even 34, 33, 32, 31 or 30%. Specifically, in order to guarantee a sufficient resistive cross section with the steels commonly used by those skilled in the art to make the body of this type of wall anchor, the ratio  $e/d_1$  preferably has not to be too high, particularly in the case of small-diameter wall anchors which are more sensitive to body breakages.

The diameter  $d_1$  may be comprised between 3 and 15 mm, preferably between 4 and 13 mm, and more preferably between 5 and 12 mm. The thickness  $e$  may be comprised between 0.7 and 3.5 mm, preferably between 0.9 and 3 mm, and more preferably between 1 and 2.5 mm.

The expansion cone of the wall anchor may have an angle  $\alpha$  greater than or equal to 25, 26, and preferably 27°. This angle  $\alpha$  may be less than or equal to 35° and preferably less than or equal to 30°.

The sleeve may have an end, situated at the expansion cone end, that has a conicity obtained for example by an entry chamfer.

The applicant company has sought to improve the performance of its wall anchor still further in cracked concrete under seismic loading. It has thus had the idea of significantly increasing the angle  $\alpha$  of the expansion cone by comparison with the values commonly employed in the current state of the art. This angle  $\alpha$  is actually generally less than or equal to 20° for wall anchors intended for non-cracked concrete, and of the order of 20 to 22° for those intended to work in cracked concrete.

A large angle  $\alpha$  generates significant stress at the contact between the sleeve and the expansion cone of the body. This stress, if excessively high, has the effect of causing the sleeve to seize on the body, destroying the contact surface, which is detrimental to the overall operation of the wall anchor under such conditions. Sometimes the person skilled in the art uses an antifriction coating at this point of contact, in order to push back the limits of seizure described above. However, this coating has the disadvantage of reducing the holding performance of the wall anchor under the conditions described above. The applicant company, seeking to obtain superior performance despite the new seismic conditions, has raised the value of this angle  $\alpha$  to at least 27°, which goes against the technical preconceptions in this art. Astonishingly, recourse to these high angle  $\alpha$  values has made it possible to improve the operation and hold fast ability of the wall anchors. Increasing the value of the angle  $\alpha$  without seizure has in fact been made easier by the increase in the thickness  $e$  of the sleeve which allows this sleeve to withstand more severe operating conditions and makes it possible to push back the permissible limits at the sleeve/expansion cone contact region. The combination of these parameters has allowed the applicant company to produce wall anchors that function perfectly under seismic loading in cracked concrete while at the same time improving their ultimate strength, and as a result, their maximum safe working load.

The sleeve may have a length representing less than 25%, and for example less than 20%, of that of the body.

The cone may have a maximum diameter  $d_3$  substantially equal to the nominal diameter  $D$ .

4

The cylindrical portion of diameter  $d_1$  may be connected by a cylindrical portion of nominal diameter  $D$  to a threaded part of the body.

The present invention also relates to a use of a wall anchor as described hereinabove for fixing an object to a support material, particularly a support material liable to be subjected to seismic loadings.

#### BRIEF DESCRIPTION OF THE FIGURES

The invention will be better understood and further details, features and advantages of the present invention will become more clearly apparent from reading the following description, given by way of nonlimiting example with reference to the attached drawings, in which:

FIG. 1 is a schematic view of an expanding wall anchor according to the invention; and

FIG. 2 is another schematic view, in this instance an exploded view, of the wall anchor of FIG. 1; and

FIG. 3 is a schematic view in cross section of a support material in a hole of which an expanding wall anchor according to the invention is anchored.

#### DETAILED DESCRIPTION

The wall anchor **10** of FIG. 1, intended for fixing a component to a support material, comprises a longitudinal body **12** of axis  $X$  and an expanding sleeve **14** mounted coaxially around the body.

The body **12** essentially comprises an expansion cone **16** of angle  $\alpha$  and of maximum diameter  $d_2$  (FIG. 2), a cylindrical portion **18** of diameter  $d_1$ , a cylindrical portion **20** of diameter  $D$ , and a threaded part **22** which is able to accept a washer **24** and a nut **26**.

The expansion cone **16** is situated at one end of the body **12** and is connected by the portion **18** of diameter  $d_1$  to the portion **20** of diameter  $D$ .  $d_1$  is less than  $D$  which is the nominal diameter of the body **12** and which is substantially equal to the receiving or anchor hole bored in the support material. Thus, the portion **18** defines an annular groove between the cone **16** and the rest of the body **12**.

The portion **20** extends between the portion **18** and the threaded part **22** which generally has a length greater than the combined lengths of the cone **16** and of the portions **18**, **20**, along the axis  $X$ .

The body **12**, comprising the cone **16**, the portions **18**, **20** and the threaded part **22**, is formed as a single piece, generally of a hard and strong metal alloy (such as a steel). In theory, it is of solid cross section over its entire length.

The region of connection between the cylindrical portions **18**, **20** may comprise an external radial shoulder **28** (FIG. 2) which is notably intended to act as an axial end stop for the sleeve **14** when the wall anchor **10** is being inserted into the support material. If this shoulder **28** is formed of an annular collar **30**, this collar may be considered to define the nominal diameter  $D$  of the body **12**.

The expanding sleeve **14** is mounted around the portion **18**, i.e. in the aforementioned groove of the body **12**. The sleeve **14** has a thickness  $e$  and an outside diameter  $d_2$ .

The sleeve **14** is preferably mounted with clearance, particularly radial clearance, on this portion so that it can move along it. The radial clearance on the radius is preferably comprised between 0.05 and 0.3 mm.

This sleeve **14** is obtained in the usual way from a flat sheet material blank (generally sheet metal blank), which is cut, bent, struck and/or rolled so that once mounted on the portion **18** of the body **12** it has the desired skirt shape with

## 5

a longitudinal slit. The sleeve **14** may comprise projecting external lugs that anchor into the support material, the radially external ends of these lugs potentially being on a circumference centred on the axis X and the diameter of which is slightly greater than the nominal diameter D of the body.

The sleeve **14** is mounted around the portion **18** of the body by crimping such that the longitudinal edges of the sleeve face and are close to one another, with a relatively narrow slit separating them. Once crimped, the sleeve **14** is preferably able to move, within the extent of the functional clearance, axially and rotationally with respect to the body **12**.

This expanding sleeve **14** is intended to have the expansion cone **16** of the body **12** pass partially through it so that once it has deformed it anchors in the wall of a receiving or anchor hole in a support material.

As FIGS. 1 and 2 show, the sleeve **14** may at its end situated at the same end as the cone **16** have an entry chamfer which gives this end a certain conicity, so that once it has been mounted around the portion **18** of the body, the sleeve **14** has a frustoconical shape that more or less complements that of the expansion cone **16** of the body.

According to the invention, the wall anchor **10** is dimensioned such that the ratio  $d1/D$  is greater than or equal to 60% and that the ratio  $e/d1$  is greater than or equal to 22%. Moreover, the aforementioned angle  $\alpha$  of the cone **16** of the wall anchor is preferably comprised between 27 and 30°, and preferably measures approximately 27°.

As far as the  $d1/D$  ratio is concerned, the minimum value of 60% amounts to expressing the depth of the annular groove defined by the portion **18** of the body. In order not to weaken the body, this groove has not to be too deep, as too deep a groove results in a small-section portion **16** which therefore has low mechanical strength. The following table sets out the minimum value of  $d1$  for various values of the nominal diameter of the body of the wall anchor.

Nominal diameter D (in mm)	Minimum value of $d1$ (in mm - for a $d1/D$ ratio $\geq 0.6$ )
6	3.6
8	4.8
10	6
12	7.2
16	9.6

The ratio  $e/d1$  has a minimum value for guaranteeing the wall anchor good mechanical properties and, in particular, good ability to hold fast under seismic loadings.

The following table gives, by way of example, minimum values for the thickness  $e$  of the sleeve, which have been deduced from the  $d1$  values from the previous table.

Nominal diameter D (in mm)	Minimum value of $d1$ (in mm)	Minimum value of $e$ (in mm - for an $e/d1$ ratio $\geq 0.22$ )
6	3.6	0.792
8	4.8	1.056
10	6	1.32
12	7.2	1.584
16	9.6	2.112

Of course, the values of  $d1$  and of  $e$  of the wall anchor according to the invention are dependent on the nominal diameter D of the wall anchor and on the aforementioned

## 6

ratios  $d1/D$  and  $e/d1$ . The next table gives other examples of values of the thickness  $e$  for the same ratio  $d1/D$  ( $\geq 0.6$ ) and for a  $e/d1$  ratio greater than or equal to 25%.

Nominal diameter (in mm)	Minimum value of $d1$ (in mm)	Minimum value of $e$ (in mm - for an $e/d1$ ratio $\geq 0.25$ )
6	3.6	0.9
8	4.8	1.2
10	6	1.5
12	7.2	1.8
16	9.6	2.4

Fitting the expanding wall anchor according to the invention into a support material does not present any difficulties and can be done usually in the following way, with reference to FIG. 3.

Beforehand, a blind anchor or receiving hole T of diameter D is bored in the support material MS which is generally a hard material (concrete).

The depth of the hole is at least equal to the combined lengths of the cone **16**, of the portion **18** and of at least part of the portion **20** (or of the collar **30**).

The wall anchor **10** is introduced, expansion cone **16** end first, into the hole T using a tool, such as a hammer, acting on the transverse face **32** of the body **12**, at the opposite end from the cone **16**. As the cone **16** is driven into the hole T the sleeve **14**, driven axially by the shoulder **28** or the collar **30** of the body, is introduced at the same time.

The wall anchor **10** is therefore introduced into the hole T, with the expansion cone **16** ready to deform the sleeve **14** to anchor it completely in the wall P of the hole.

To achieve that, axial tension is applied in the direction of the arrow F to the body, towards the outside end of the hole T, which tension is obtained by the clamping nut **26**, depicted in chain line in FIG. 3, screwed onto the threaded part **22** of the body and used to attach a component PI, likewise depicted in chain line and mounted around the body **12** so that it sits against the face FE of the support material MS.

As the nut **26** is tightened, the expansion cone **16** is pulled and enters the sleeve **14**, which sleeve, because of its frustoconical shape which is the reverse of that of the cone, experiences an expansion right from the start of the tensile force applied by the retreating cone **16** and engages in the wall P of the hole. Thus, the sleeve **14** is immediately immobilized axially in position, preventing it from riding up in the hole.

As the expansion cone **16** gradually penetrates the sleeve **14**, as a result of the tightening of the nut **26**, to reach the final position illustrated in FIG. 3, for which the cone is appreciably engaged in the sleeve, the sleeve **14** undergoes an expansion such that it is forced to penetrate (arrows E) the wall P of the hole T so that the sleeve **14** is perfectly anchored in the support material MS.

The wall anchor **10** is then operational, fully immobilized by the tightening of the nut **26** that attaches the component PI to the support material MS.

## EXAMPLE

The description that follows contains a comparative example to illustrate the foregoing.

We have compared a product according to the invention (product A) that meets all of the requirements stipulated for cracked concrete and seismic loadings against a product of

the prior art that meets only the requirements stipulated for cracked concrete without seismic loadings (product B) and against a third product designed exclusively for non-cracked concrete (product C). The three wall anchors compared have the same nominal diameter, in this instance 12 mm (M12), and were set at identical anchoring depths into concretes of identical strengths. The various components of these wall anchors are made of comparable steels commonly used by those skilled in the art. The only appreciable differences are their ratio  $e/d1$  and their angle  $\alpha$  as defined above. The reference wall anchor is the wall anchor according to the invention (product A) which works under all the conditions and for which we consider the ultimate strength (RLU) (or “design resistance”) to be 100%.

The table below summarizes the results and parameters of our example.

Product	$e/d1$	$\alpha$	RLU	Does it work in cracked concrete	Does it work in concrete with seismic loading
A	25.6%	27	100%	YES	YES
B	17.4%	20	100%	NO	NO
B	17.4%	20	75%	YES	NO
C	17.4%	16	100%	NO	NO
C	17.4%	16	56%	YES	NO

Product A has an  $e/d1$  ratio greater than 22%, in this instance of 25.6%, an angle  $\alpha$  equal to  $27^\circ$  and works in all conditions. This is our reference.

Product B designed for cracked concrete but not for seismic loadings has an  $e/d1$  ratio of less than 22%, in this instance of 17.4%, and an angle  $\alpha$  less than  $27^\circ$ , in this instance of  $20^\circ$ . Its performance in cracked concrete is only 75% of the RLU of product A. If product B is loaded to achieve 100% of the RLU of product A, it no longer works in cracked concrete. This product B is not designed for seismic loading.

Product C designed solely for non-cracked concrete has an  $e/d1$  ratio of less than 22%, in this instance of 17.4%, and an angle  $\alpha$  less than  $27^\circ$ , in this instance of  $16^\circ$ . We reduced its RLU progressively in an attempt to make it work in cracked concrete but under lighter load. At the end of this exercise, the RLU of product C that allowed it to function in cracked concrete was only 56% of the RLU of product A.

This example clearly demonstrates the benefit of the invention and the significance of the claimed parameters in the performance of products in relation to the prior art.

The invention claimed is:

**1.** An expanding wall anchor, comprising:

- i) a longitudinal body formed as a single piece and including an expansion cone, a cylindrical portion, and a threaded portion, wherein the expansion cone forms a first end of the longitudinal body, the threaded portion forms a second opposing end of the longitudinal body, and the expansion cone is connected to the threaded body via the cylindrical portion, and
- ii) an expanding sleeve of thickness ( $e$ ) mounted around the cylindrical portion of the body and through which the expansion cone is configured to move to deform the expanding sleeve and to anchor the expanding wall anchor in a hole in a support material, wherein the cylindrical portion has a diameter ( $d1$ ), the longitudinal body has a nominal diameter ( $D$ ), and the diameter of the cylindrical portion ( $d1$ ) is smaller than the nominal diameter of the longitudinal body ( $D$ ),

the expanding sleeve has a maximum outside diameter ( $d2$ ) that is substantially equal to the nominal diameter of the longitudinal body ( $D$ ),

a first ratio ( $d1/D$ ) of the diameter of the cylindrical portion ( $d1$ ) to the nominal diameter of the longitudinal body ( $D$ ) is greater than or equal to 60%,

and a second ratio ( $e/d1$ ) of the thickness of the expanding sleeve ( $e$ ) to the diameter of the cylindrical portion ( $d1$ ) is greater than or equal to 22%.

**2.** The expanding wall anchor of claim 1, wherein the second ratio ( $e/d1$ ) of the thickness of the expanding sleeve ( $e$ ) to the diameter of the cylindrical portion ( $d1$ ) is less than 35%.

**3.** The expanding wall anchor of claim 1, wherein the expansion cone has an angle ( $\alpha$ ) greater than or equal to 25 degrees.

**4.** The expanding wall anchor of claim 1, wherein the expansion cone has an angle ( $\alpha$ ) greater than or equal to 26 degrees.

**5.** The expanding wall anchor of claim 1, wherein the expansion cone has an angle ( $\alpha$ ) less than or equal to 35 degrees.

**6.** The expanding wall anchor of claim 1, wherein the expansion cone has an angle ( $\alpha$ ) less than or equal to 30 degrees.

**7.** The expanding wall anchor of claim 1, wherein the nominal diameter of the longitudinal body ( $D$ ) is between 6 mm and 30 mm.

**8.** The expanding wall anchor of claim 1, wherein the diameter of the cylindrical portion ( $d1$ ) is between 3 mm and 15 mm.

**9.** The expanding wall anchor of claim 1, wherein the thickness of the expanding sleeve ( $e$ ) is between 0.7 mm and 3.5 mm.

**10.** The expanding wall anchor of claim 1, wherein the expanding sleeve has a length representing less than 25% of a length of the longitudinal body.

**11.** The expanding wall anchor of claim 10, wherein the expanding sleeve has a length representing less than 20% of a length of the longitudinal body.

**12.** The expanding wall anchor of claim 1, wherein the expansion cone has a maximum diameter ( $d3$ ) substantially equal to the nominal diameter of the longitudinal body ( $D$ ).

**13.** The expanding wall anchor of claim 1, wherein the cylindrical portion of diameter ( $d1$ ) is connected by a cylindrical portion of nominal diameter ( $D$ ) to a threaded part of the longitudinal body.

**14.** The expanding wall anchor of claim 1, wherein the expanding wall anchor is configured for fixing an object to the support material.

**15.** The expanding wall anchor of claim 1, wherein the expanding wall anchor is configured for fixing an object to the support material, and wherein the support material is liable to be subjected to seismic loadings.

**16.** The expanding wall anchor of claim 1, wherein the expanding wall anchor is configured to hold fast under seismic loading in cracked concrete.

**17.** The expanding wall anchor of claim 1, wherein: the first ratio ( $d1/D$ ) of the diameter of the cylindrical portion ( $d1$ ) to the nominal diameter of the longitudinal body ( $D$ ) is greater than or equal to 60%,

the second ratio ( $e/d1$ ) of the thickness of the expanding sleeve ( $e$ ) to the diameter of the cylindrical portion ( $d1$ ) is greater than or equal to 22%,

the second ratio ( $e/d1$ ) of the thickness of the expanding sleeve ( $e$ ) to the diameter of the cylindrical portion ( $d1$ ) is less than 35%,

9

the expansion cone has an angle (a) that is greater than or equal to 27 degrees, and the angle of the expansion cone (a) is less than or equal to 30 degrees, the expanding sleeve has an outside diameter (d2) substantially equal to the nominal diameter of the longitudinal body (D),  
 the nominal diameter of the longitudinal body (D) is between 8 mm and 16 mm,  
 the diameter of the cylindrical portion (d1) is between 3 mm and 15 mm,  
 the thickness of the expanding sleeve (e) is between 0.7 mm and 3.5 mm, and  
 the expanding sleeve has a length representing less than 20% of a length of the longitudinal body.

**18.** An expanding wall anchor, comprising:  
 a longitudinal body which is a single piece and comprises:  
 an expansion cone forming a first end of the longitudinal body,  
 a first cylindrical portion having a first end and an opposing second end, wherein the first end of the first cylindrical portion is connected to an end of the expansion cone,  
 a second cylindrical portion having a first end and an opposing second end, wherein the first end of the second cylindrical portion is connected to the second end of the first cylindrical portion, and  
 a threaded portion forming a second end of the longitudinal body, wherein an end of the threaded portion is connected to the second end of the second cylindrical portion; and  
 an expanding sleeve of thickness (e) which is mounted around the first cylindrical portion of the longitudinal body and into which the expansion cone is configured to move to deform the expanding sleeve and to anchor the expanding wall anchor in a hole in a support material,

wherein:

the expansion cone, the first cylindrical portion, the second cylindrical portion, and the threaded portion are formed from a single piece,  
 the first cylindrical portion has a diameter (d1), the second cylindrical portion has a diameter (D), and the diameter of the first cylindrical portion (d1) is less than the diameter of the second cylindrical portion (D),  
 the expanding sleeve has a maximum outside diameter (d2) that is substantially equal to the diameter of the second cylindrical portion (D),  
 a first ratio (d1/D) of the diameter of the first cylindrical portion (d1) to the diameter of the second cylindrical portion (D) is greater than or equal to 60%,

10

a second ratio (e/d1) of the thickness of the expanding sleeve (e) to the diameter of the first cylindrical portion (d1) is greater than or equal to 22%, and the expansion cone has an angle (a) greater than or equal to 27 degrees.

**19.** An expanding wall anchor, comprising:  
 a longitudinal body which is a single piece and comprises:  
 an expansion cone forming a first end of the longitudinal body,  
 a first cylindrical portion having a first end and an opposing second end, wherein the first end of the first cylindrical portion is connected to an end of the expansion cone,  
 a second cylindrical portion having a first end and an opposing second end, wherein the first end of the second cylindrical portion is connected to the second end of the first cylindrical portion, and  
 a threaded portion forming a second end of the longitudinal body, wherein an end of the threaded portion is connected to the second end of the second cylindrical portion; and  
 an expanding sleeve of thickness (e) which is mounted around the first cylindrical portion of the longitudinal body and into which the expansion cone is configured to move to deform the expanding sleeve and to anchor the expanding wall anchor in a hole in a support material,

wherein:

the expansion cone, the first cylindrical portion, the second cylindrical portion, and the threaded portion are formed from a single piece,  
 the first cylindrical portion has a diameter (d1), the second cylindrical portion has a diameter (D), and the diameter of the first cylindrical portion (d1) is less than the diameter of the second cylindrical portion (D),  
 the expanding sleeve has a maximum outside diameter (d2) that is substantially equal to the diameter of the second cylindrical portion (D),  
 a first ratio (d1/D) of the diameter of the first cylindrical portion (d1) to the diameter of the second cylindrical portion (D) is greater than or equal to 60%,  
 a second ratio (e/d1) of the thickness of the expanding sleeve (e) to the diameter of the first cylindrical portion (d1) is greater than or equal to 22%, and  
 the threaded portion has a length greater than a combined length of the cone, the first cylindrical portion, and the second cylindrical portion.

\* \* \* \* \*