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RISER TENSIONING SYSTEM

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E21B 19/00 (2006.01)

U.S. Cl. (52)

CPC *E21B 19/006* (2013.01)

Field of Classification Search

CPC E21B 19/006; E21B 19/004; E21B 19/02 See application file for complete search history.

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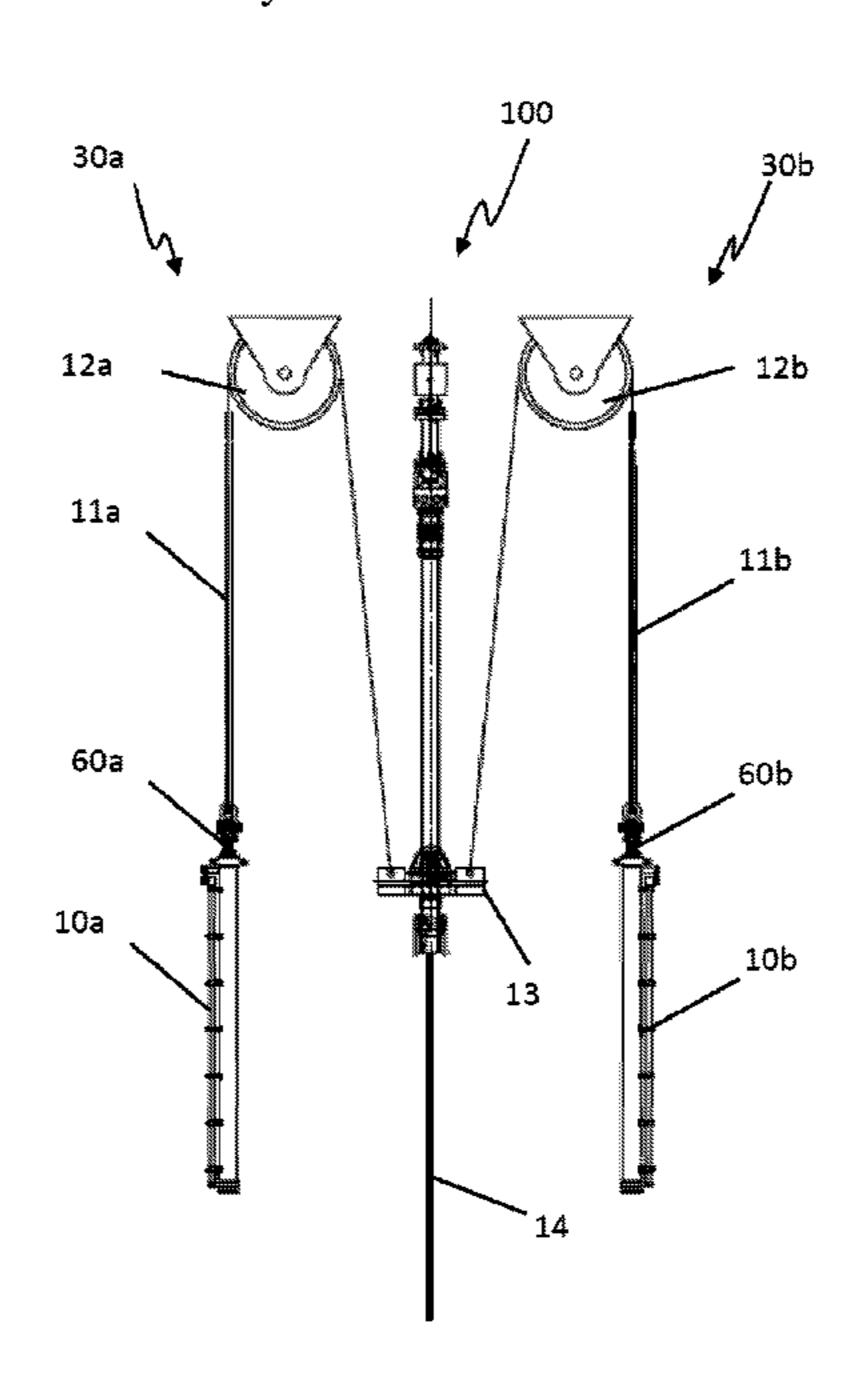
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(57)**ABSTRACT**

A riser tensioning system for providing a tensioning to a riser connected to a floating installation via a tension ring. The riser tensioning system includes at least one riser tensioner assembly. Each of the at least one riser tensioner assembly includes a riser tensioning cylinder comprising a cylinder rod, at least one sheave, and a wireline with a first end and a second end. The first end is fixed to the tension ring, and the second end is fixed to the cylinder rod. The wireline extends between the tension ring and the cylinder piston via the at least one sheave.

20 Claims, 11 Drawing Sheets



US 10,385,630 B2

Page 2

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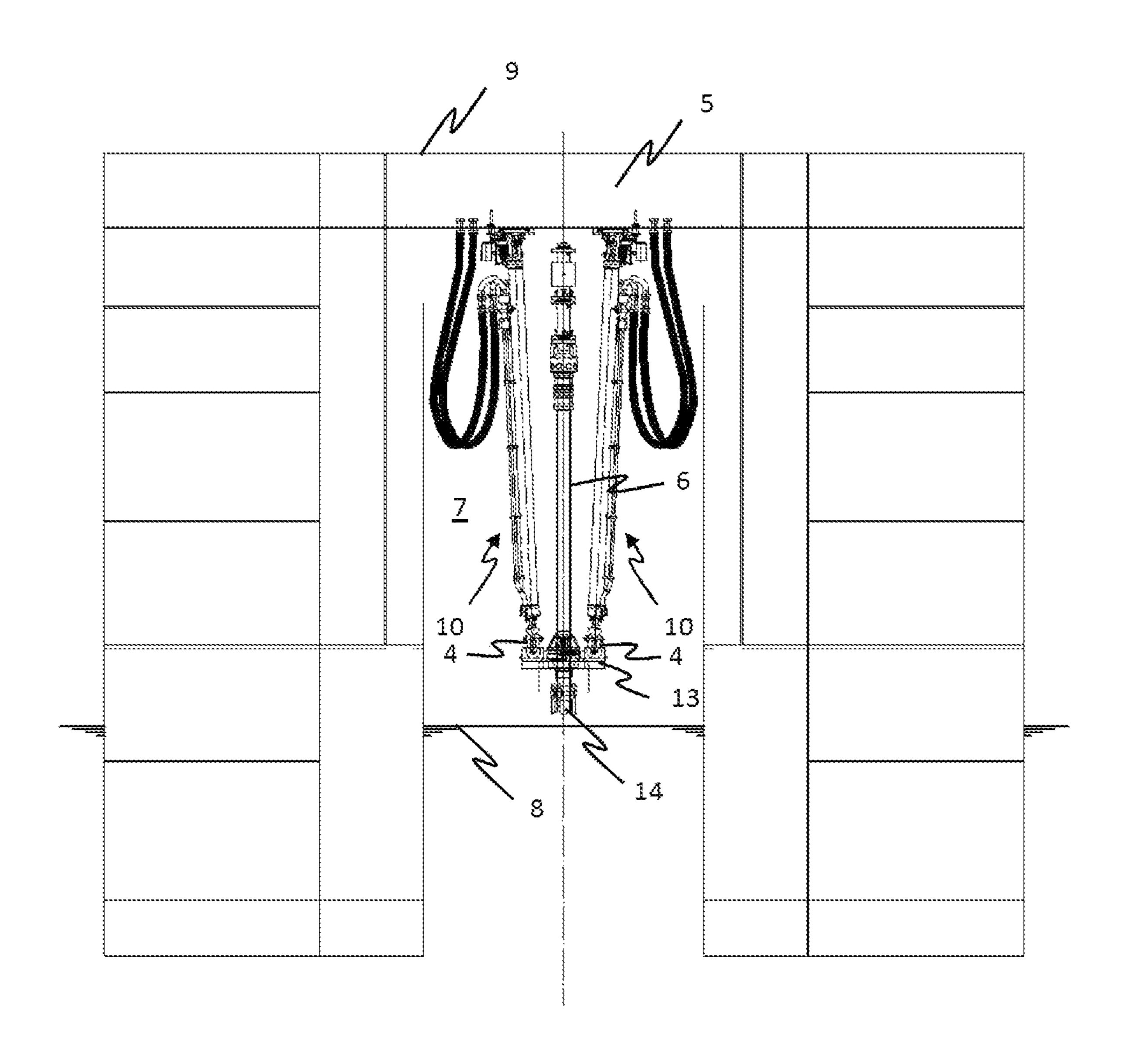


Fig. 1
(Prior Art)

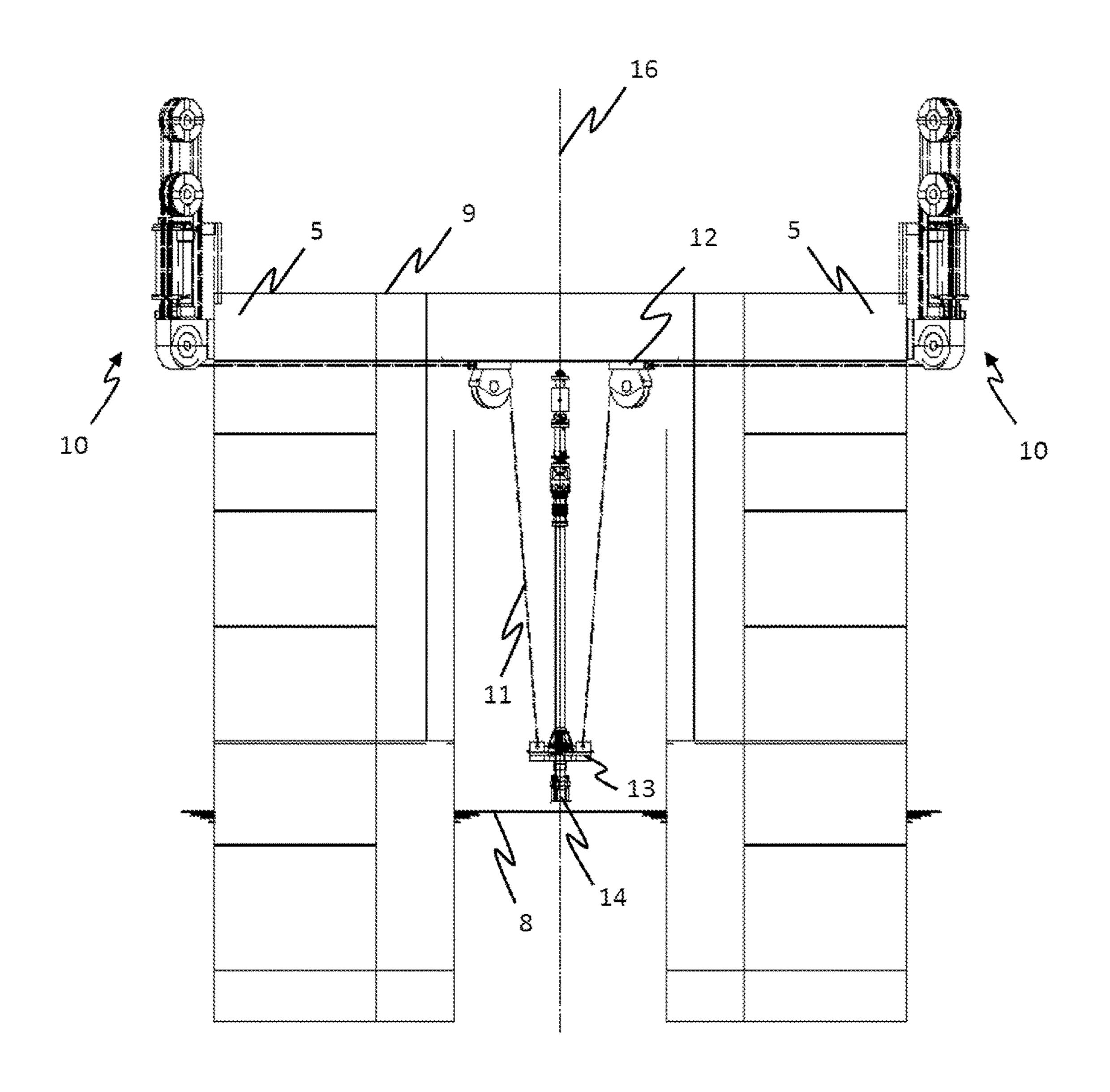


Fig. 2
(Prior Art)

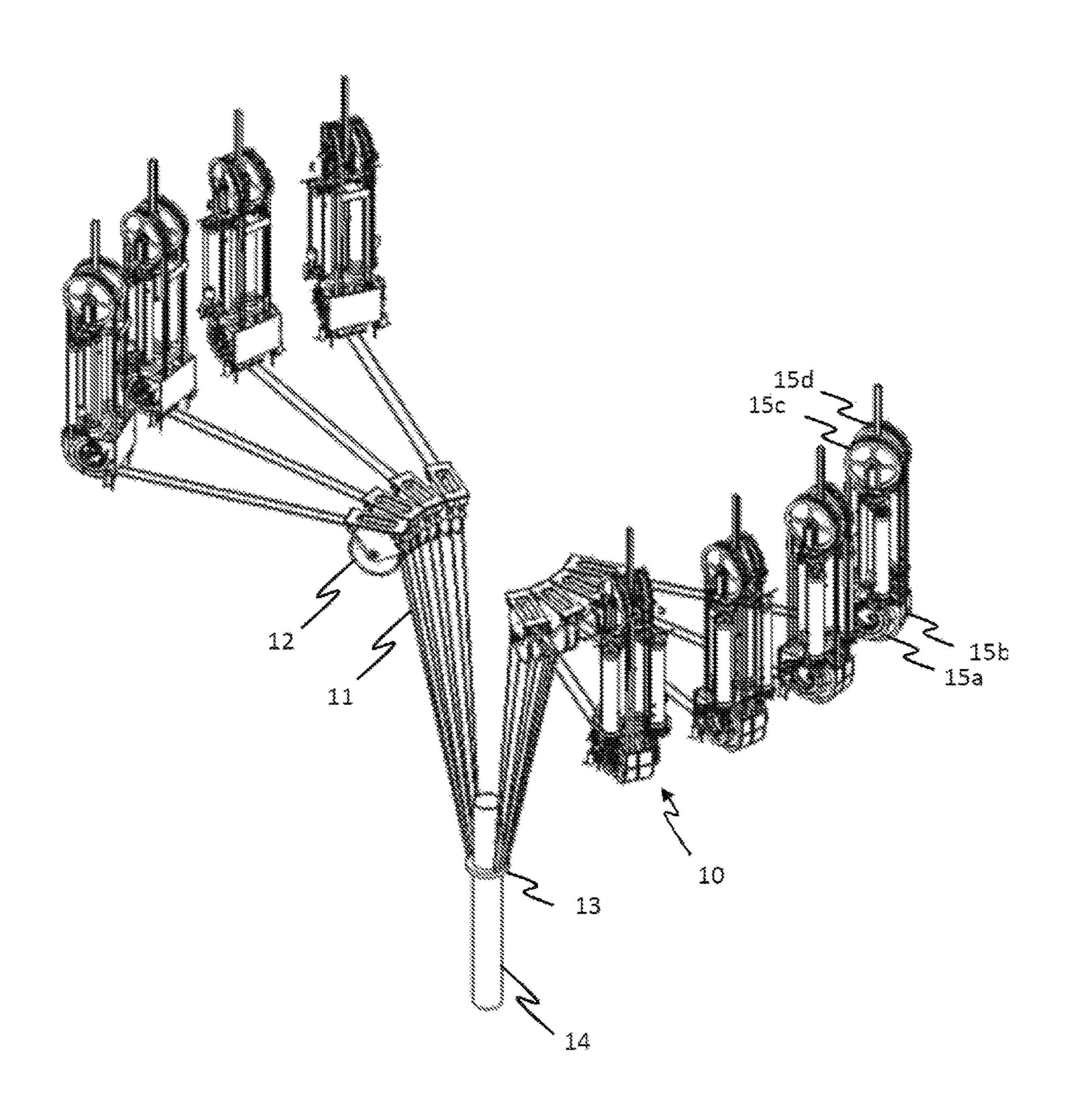


Fig. 3
(Prior Art)

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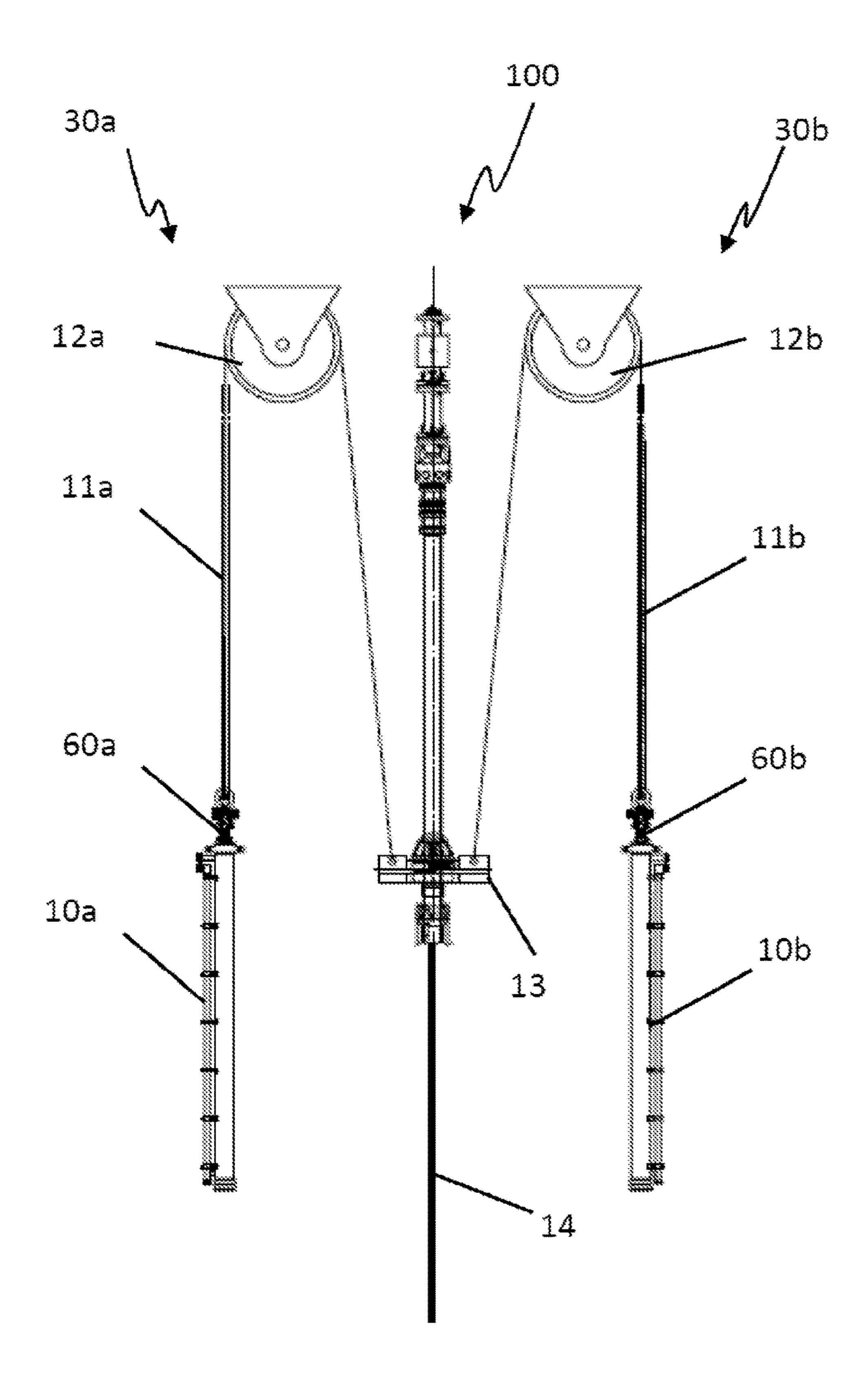


Fig. 4

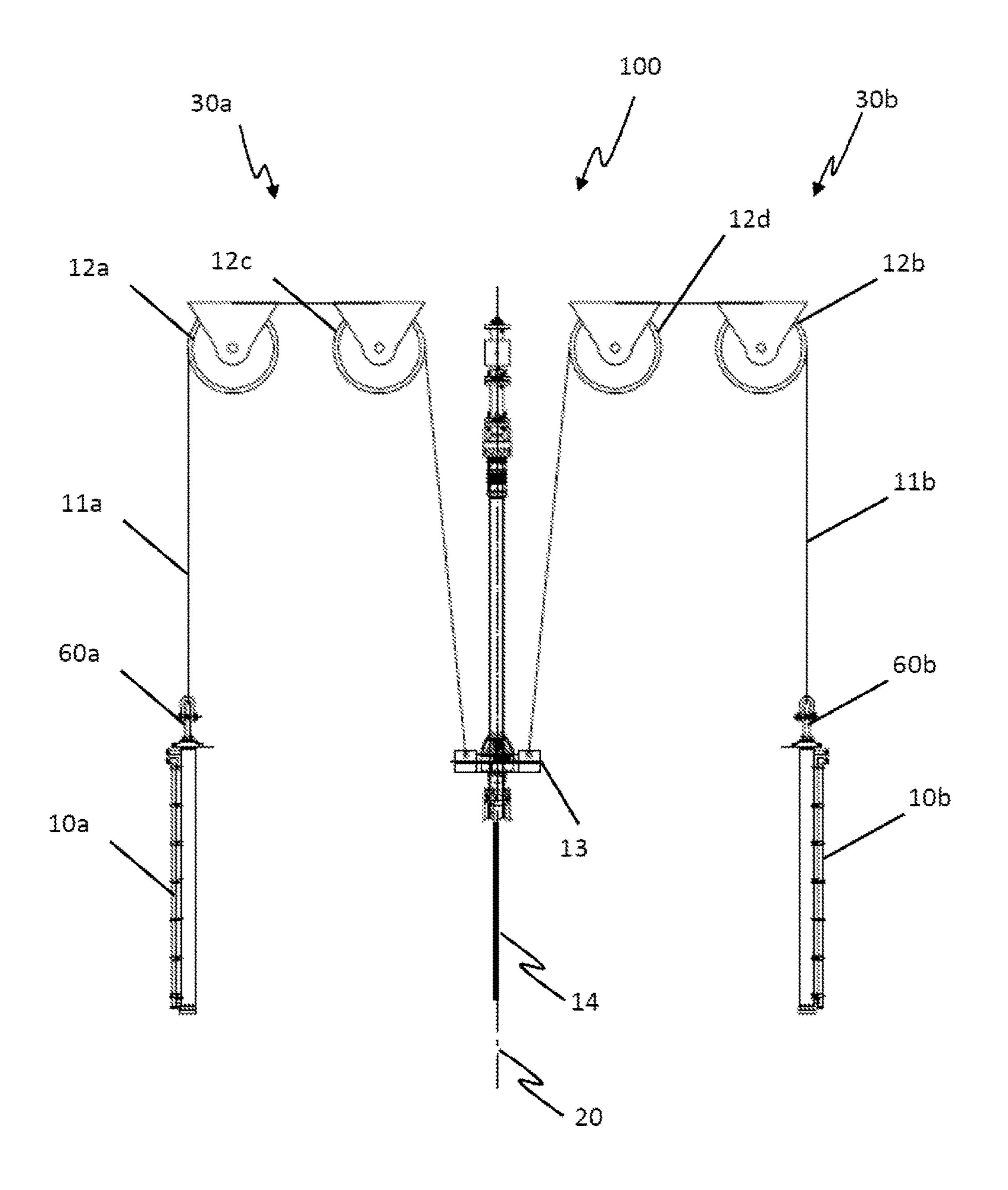


Fig. 5

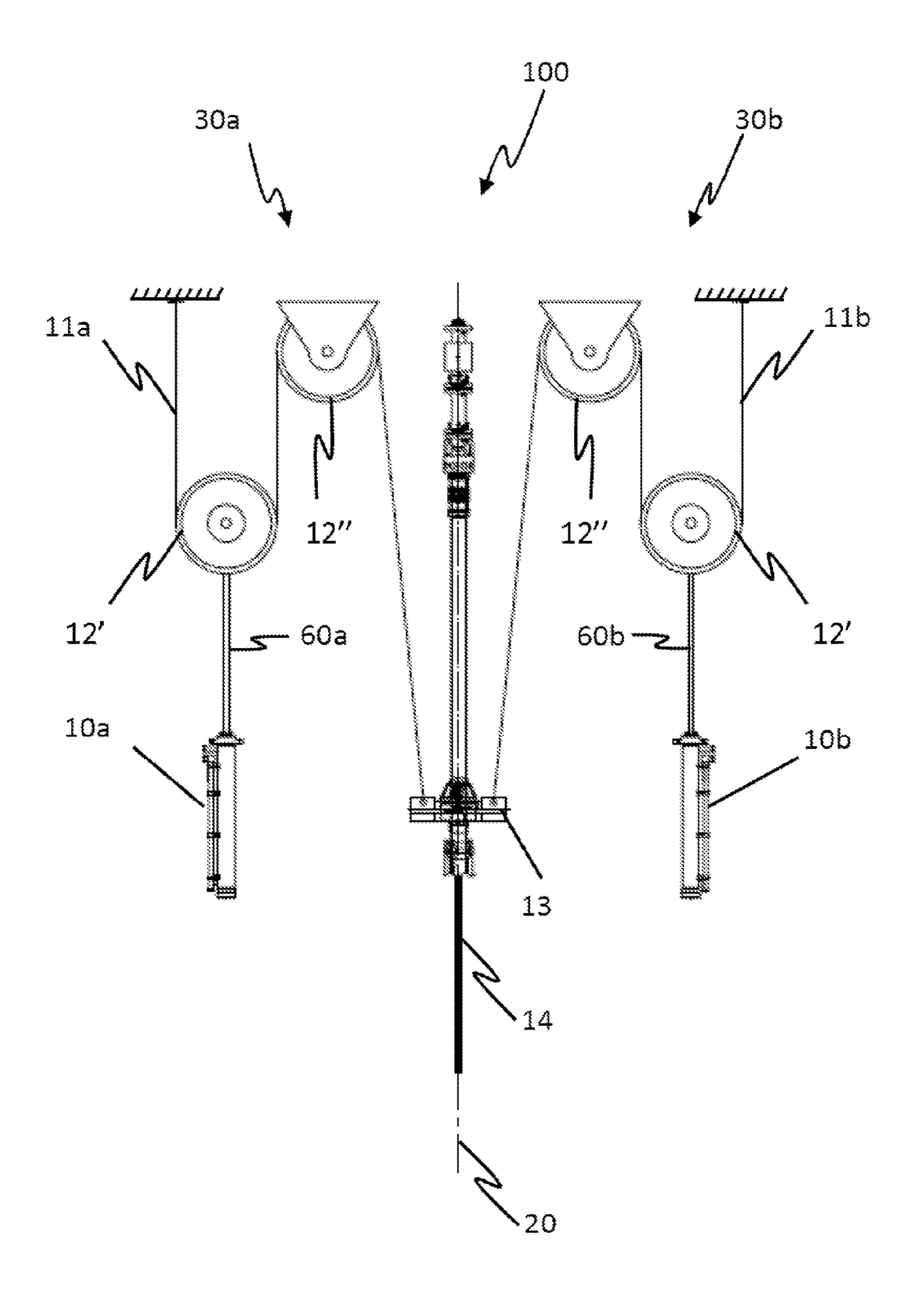


Fig. 6

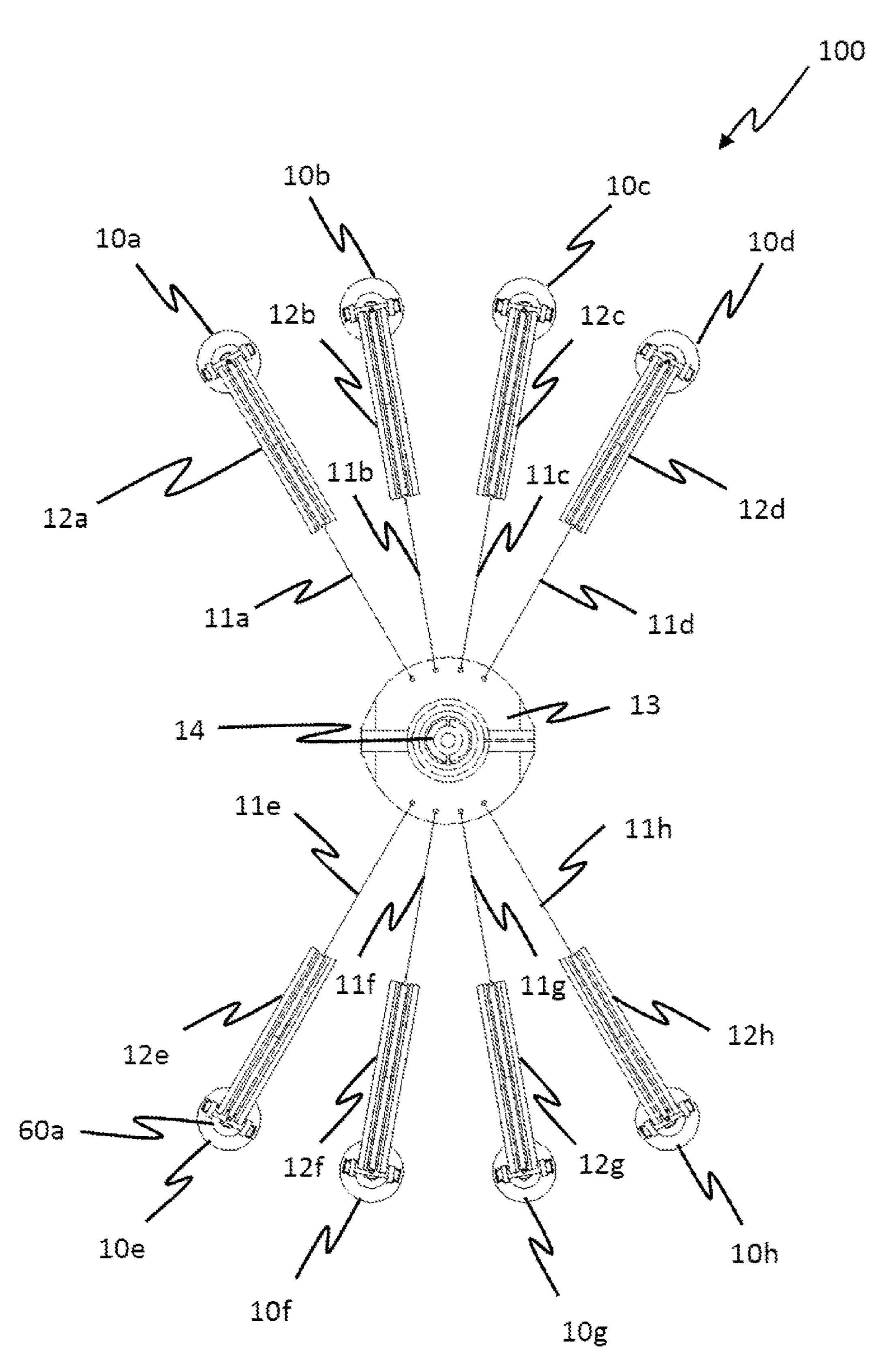


Fig. 7

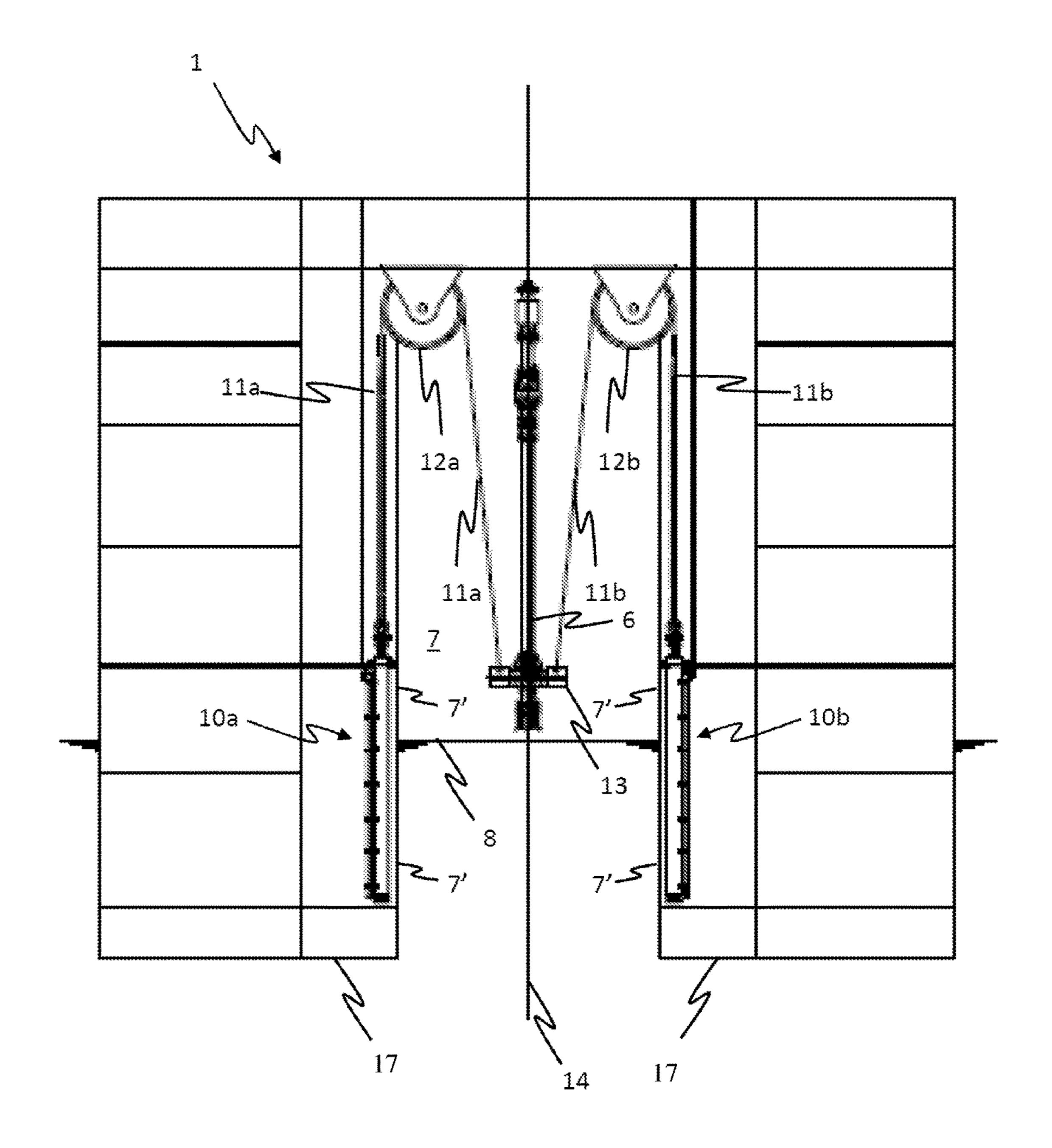


Fig. 8

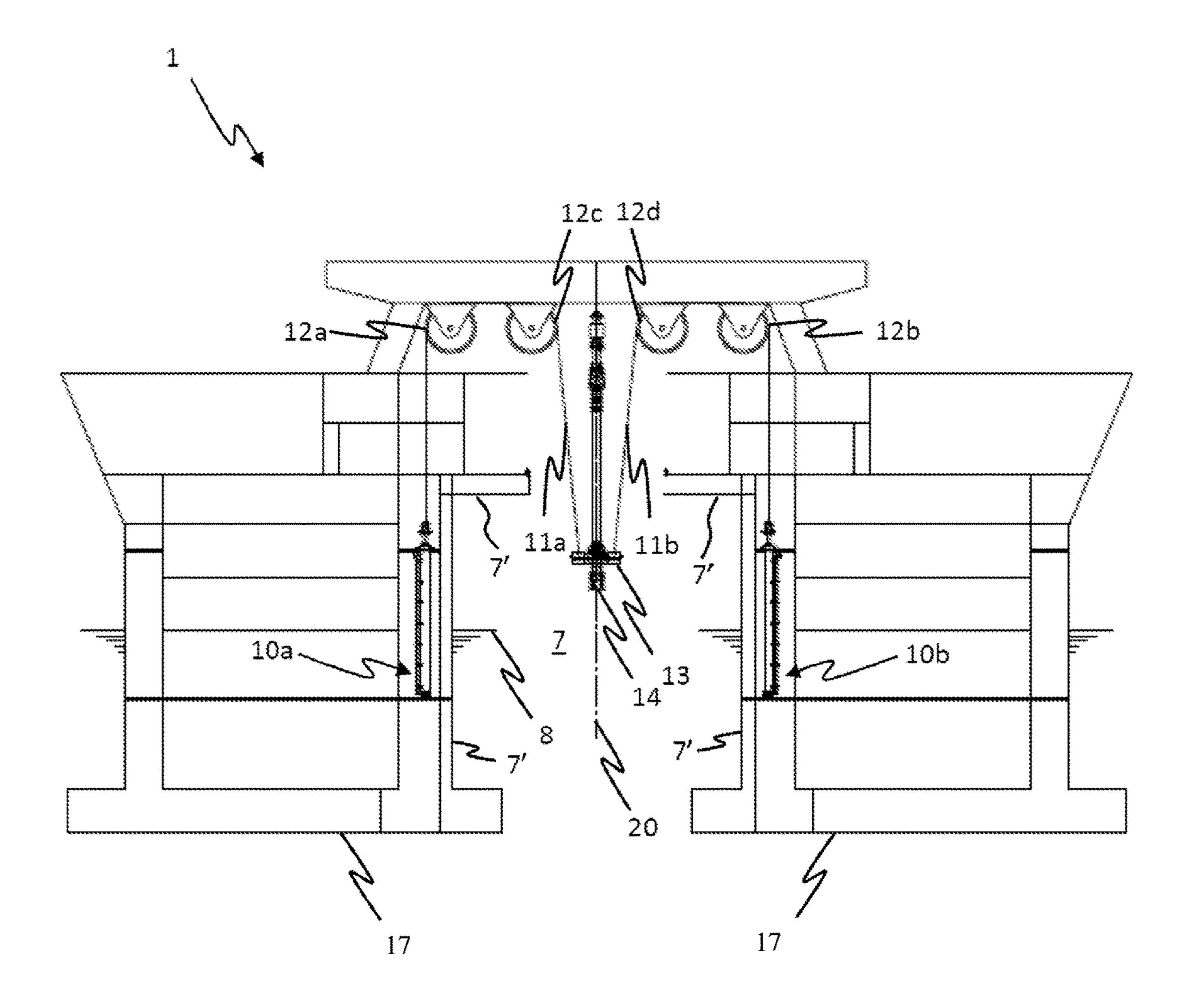


Fig. 9

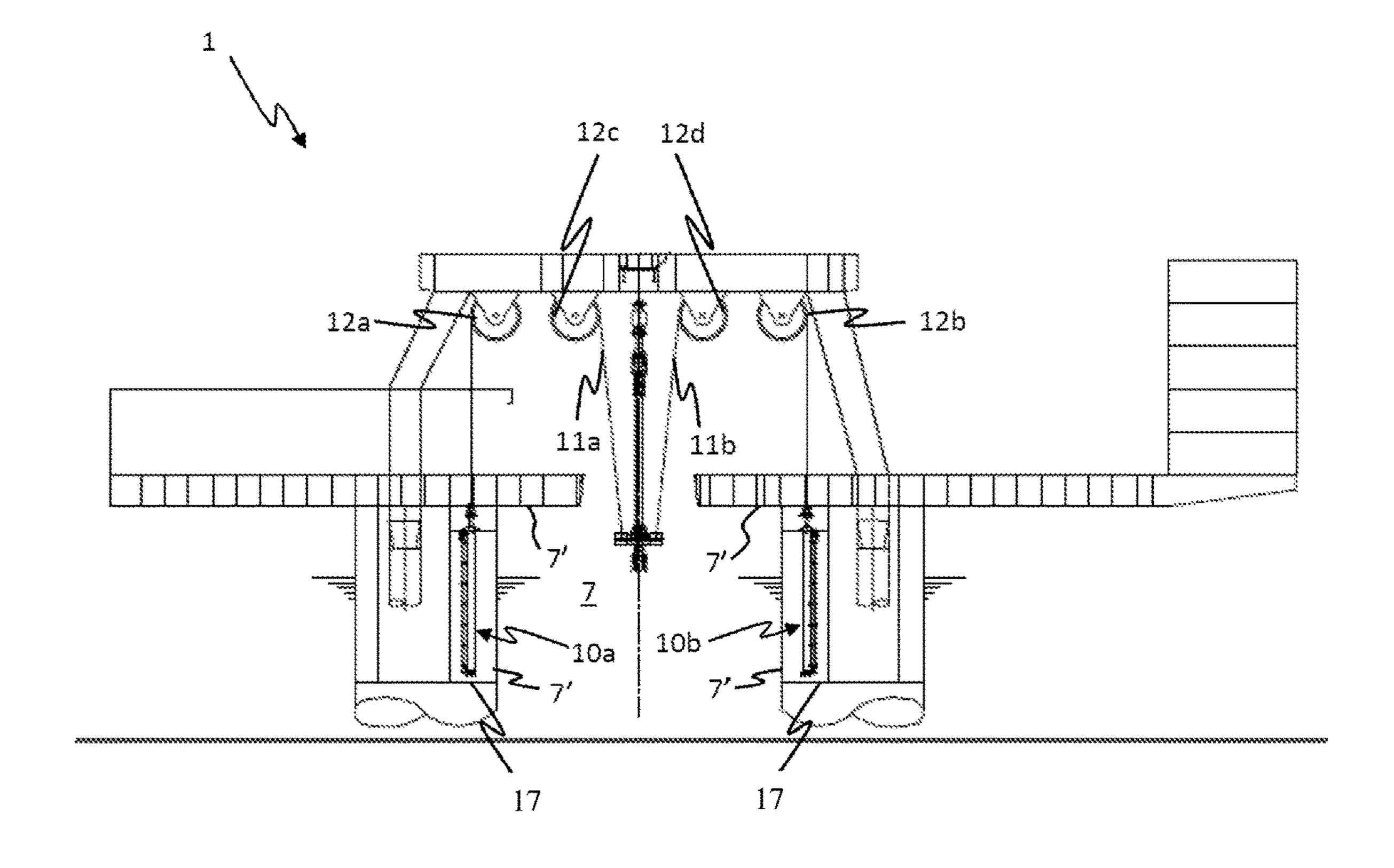


Fig. 10

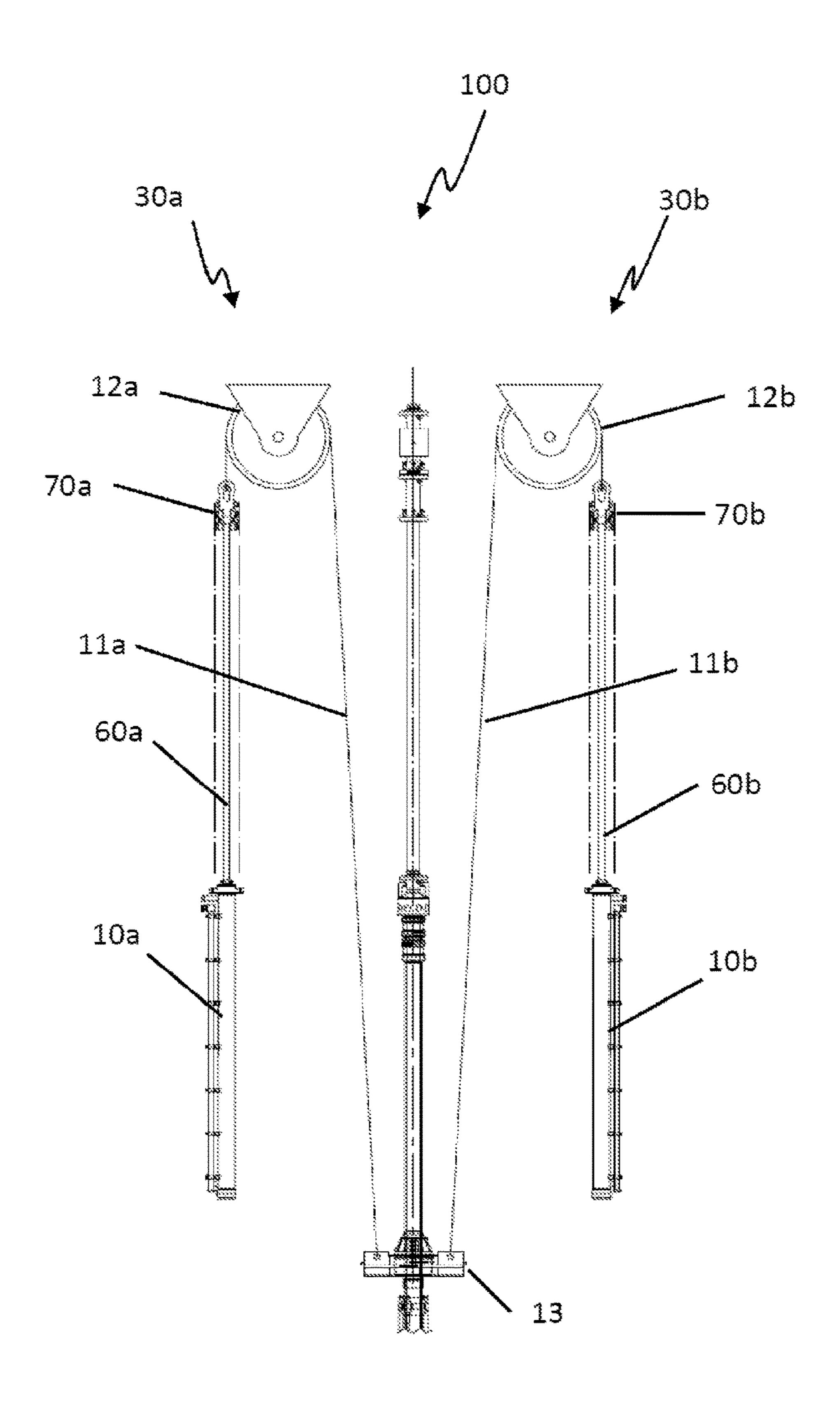


Fig. 11

RISER TENSIONING SYSTEM

CROSS REFERENCE TO PRIOR **APPLICATIONS**

This application is a U.S. National Phase application under 35 U.S.C. § 371 of International Application No. PCT/NO2016/050144, filed on Jun. 28, 2016 and which claims benefit to Norwegian Patent Application No. 20150914, filed on Jul. 13, 2015. The International Application was published in English on Jan. 19, 2017 as WO 2017/010889 A1 under PCT Article 21(2).

FIELD

The present invention relates generally to the field of floating offshore platforms or vessels for the exploitation of undersea deposits of petroleum and natural gas. The present invention relates more specifically to risers tensioners and to $_{20}$ a system for providing tension to risers which extend from a subsea wellhead or subsurface structure to a floating platform or vessel.

BACKGROUND

Offshore platforms for the exploitation of undersea petroleum and natural gas deposits typically support risers that extend to the platform from one or more wellheads or structures on the seabed. In deep water applications, floating 30 platforms (such as spars, tension leg platforms, extended draft platforms, and semi-submersible platforms) are typically used. These platforms are subject to motion due to wind, waves, and currents. The risers employed with such platforms must therefore be tensioned to permit the platform to move relative to the risers. Riser tension must also be maintained so that the riser does not buckle under its own weight. The tensioning mechanism must accordingly exert a substantially continuous tension force to the riser within a 40 well-defined range.

Hydro-pneumatic tensioner systems are one form of riser tensioning mechanism typically used to support risers known as "Top Tensioned Risers" on various platforms. A plurality of passive hydraulic cylinders with pneumatic 45 accumulators are thereby connected between the platform and the riser to provide and maintain the necessary riser tension. Platform responses to the above mentioned environmental conditions, mainly heave and horizontal motions, create changes in platform position relative to the riser, 50 causing the tensioning cylinders to stroke in and out. The spring effect resulting from the gas compression or expansion during a platform's vertical and horizontal movement relative to the seabed partially isolates the riser from the platform's motions.

Riser tensioners constituting such hydro-pneumatic tensioning systems comprise cylinders in which the cylinder rods are at least indirectly connected to the riser so that the pressure induced movements of the rod relative to its support results in the desired riser tensioning. Such hydro- 60 pneumatic tensioner systems are presently produced in a variety of dimensions and sizes. Examples of typical state of the art riser tensioner systems are disclosed in WO 2004/ 013452, U.S. Pat. Nos. 4,886,397, 3,902,319, GB 2.109.036, WO 2012/016765 and WO 2014/090682.

Known riser tensioning systems include so-called "Direct Acting Tensioner" (DAT) systems and so-called "Wireline

Riser Tensioner" (WLT) systems. An example of such systems is described in WO 2012/016765 (for example, FIGS. 4 and 5).

The location of the DAT systems within a moon pool area of a floating platform or vessel results in the risk of exposure to seawater which introduces challenges related to the corrosive environment and heavy accelerations of cylinder and rod. DAT systems may also show poor performance due to internal load deviations within the system. There may, for example, be flow resistance in the pipework/hoses between the tensioning cylinders and accumulator(s).

The alternative WLT system is large and may require a fairly complex arrangement if the system is to be applied to drilling vessels with a setback/fingerboard (for storing drill pipes, drill collars, etc.) that is situated lower than the drill floor. Such a low setback arrangement is demanding, and most users choose DAT systems in these situations. In addition to the complex arrangement in drilling vessels with low setback, the WLT systems suffer from high load variations due to friction over the plurality of sheaves. The repeated bending of the wire over a number of sheaves increases wire wear. A cut and slip configuration or complete replacement of the wire may therefore be required. The WLT systems are often heavy compared to other riser tensioning ²⁵ systems, typically around 500 MT depending on capacity.

SUMMARY

An aspect of the present invention is to provide a riser tensioning system that at least mitigates the above disadvantages. An aspect of the present invention is more specifically to reduce the risk of seawater exposure while avoiding a complex arrangement when installing the system, thereby also making such a system suitable for use on a drilling vessel with a low setback.

A further aspect of the present invention is to provide a riser tensioning system having a low weight compared to the weight of a typical WLT system, for example, a weight comparable to the weight of a typical DAT system.

A further aspect of the present invention is to provide a riser tensioning system that does not require a wire rope cut and slip configuration.

In an embodiment, the present invention provides a riser tensioning system for providing a tensioning to a riser connected to a floating installation via a tension ring. The riser tensioning system includes at least one riser tensioner assembly. Each of the at least one riser tensioner assembly comprises a riser tensioning cylinder comprising a cylinder rod, at least one sheave, and a wireline comprising a first end and a second end. The first end is fixed to the tension ring, and the second end is fixed to the cylinder rod. The wireline is configured to extend between the tension ring and the cylinder piston via the at least one sheave.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention is described in greater detail below on the basis of embodiments and of the drawings in which:

FIG. 1 shows a cross sectional view of a prior art Direct Acting Tensioner (DAT) system arranged within a moon pool of a drillship;

FIG. 2 shows a cross sectional view of a prior art Wireline Riser Tensioner (WLT) system arranged on a drillship;

FIG. 3 shows a perspective view of a prior art Wire Riser 65 Tensioner (WLT) system;

FIG. 4 shows a cross sectional view of a riser tensioner system in accordance with the present invention;

FIG. 5 shows a cross sectional view of a further riser tensioner system in accordance with the present invention;

FIG. 6 shows a cross sectional view of a riser tensioner system in accordance with a further aspect of the present invention;

FIG. 7 shows a top view of an arrangement of riser tensioner systems according to the present invention;

FIG. **8** shows a cross sectional view of a riser tensioner system in accordance with the present invention arranged within a drillship hull;

FIG. 9 shows a cross sectional view of the riser tensioner system of FIG. 5 where the riser tensioner cylinders are arranged within a typical buoy hull;

FIG. 10 shows a cross sectional view of the riser tensioner system of FIG. 5 where the riser tensioner cylinders are arranged within a typical semi-submersible hull; and

FIG. 11 shows a cross sectional view of a further riser tensioner system in accordance with the present invention.

DETAILED DESCRIPTION

In an embodiment, the present invention provides a riser tensioning system for providing tensioning to a riser connected to a floating installation via a tension ring, the system 25 comprising at least one riser tensioner assembly, each riser tensioner assembly comprising: a riser tensioning cylinder, the riser tensioning cylinder having a cylinder rod; at least one sheave; a wireline having a first end and a second end, the first end being fixed to the tension ring and the second 30 end being fixed to the cylinder rod; whereby the wireline extends between the tension ring and the cylinder rod via the at least one sheave.

Providing a riser tensioning system with a wireline having its end fixed to the cylinder piston and extending to a tension 35 ring via at least one sheave may eliminate the need to provide sheaves fixed to the riser tensioning cylinders, thus making these more flexible in their placement. Having the ends of the wireline fixed (i.e., fixedly connected) to the tension ring and the cylinder rod also allows for an approximately 1:1 transmission ratio between the cylinder rod and the tension ring, thereby avoiding frictional losses associated with systems having further sheaves for gearing.

The at least one sheave may be pivotable around an axis parallel to the riser during use.

The ratio between the diameter (d) of the wireline and the diameter (D) of at least one of the at least one sheave may be at least 30. This avoids the need to perform cut-and-slip or replacement of the wireline.

The riser tensioning system may comprise 4, 6, 8 or 10 50 riser tensioner assemblies. The cylinder rod may work in tension.

In an embodiment, the present invention provides a riser tensioning system for providing tensioning to a riser connected to a floating installation via a tension ring, the system comprising at least one riser tensioner assembly, each riser tensioner assembly comprising: a riser tensioning cylinder, the riser tensioning cylinder having a cylinder rod; at least one first sheave fixed to the cylinder rod; at least one second sheave; a wireline having a first end and a second end, the first end being fixed to the tension ring and the second end being fixed to the floating installation; whereby the wireline extends between the tension ring and the cylinder piston via the at least one first sheave and the at least one second sheave.

The at least one second sheave may be pivotable around an axis parallel to the riser during use. 4

The ratio between the diameter (d) of the wireline and the diameter (D) of at least one of the at least one first or second sheave may be at least 30.

The riser tensioning system may comprise 4, 6, 8 or 10 riser tensioner assemblies. The cylinder rod may work in tension.

In an embodiment, the present invention provides a floating installation comprising a riser tensioning system.

The floating installation may comprise a physical boundary that at least partly covers the riser tensioning cylinder of the at least one riser tensioner assembly, the physical boundary being configured to at least partly block any direct exposure of ambient water onto the riser tensioning cylinder during use.

The floating installation may further comprise a moon pool, wherein the riser tensioning cylinder of the at least one riser tensioner assembly is placed outside the moon pool.

The physical boundary may comprise the walls of the moon pool.

The riser tensioning cylinder of the at least one riser tensioner assembly may be placed below a drill floor and a deck of the floating installation.

The riser tensioning cylinder of the at least one riser tensioner assembly may be placed in a base structure of the floating installation, the base structure extending at least partly around the moon pool and below a waterline, wherein the riser tensioning cylinder is positioned in the base structure at least partly below the waterline.

A system according to the present invention is applicable for drillships, semi-submersibles, and buoys with both low setback arrangements and setback on drill floor.

The present invention is described further below under reference to the drawings. Numerous specific details are thereby introduced to provide a thorough understanding of embodiments of the system. One skilled in the relevant art, however, will recognize that these embodiments can be practiced without one or more of the specific details, or with other components, systems, etc. In other instances, well-known structures or operations are not shown, or are not described in detail, to avoid obscuring aspects of the disclosed embodiments.

FIG. 1 shows a typical prior art DAT system arranged on an offshore installation, where the DAT system consists of a plurality of direct acting tensioning cylinders 10, pulling on a marine riser 14. The tensioning cylinders 10 are connected to a tension ring 13 via tension ring shackles 4. Supported by the structure underneath drill floor area 5 and connected to a telescopic joint 6 load ring, it generates a nearly constant pull on the riser 14.

In these systems, the tensioning cylinders 10 are located in a moon pool area 7 provided in the offshore installation, directly above the water line 8. The main components are the tensioning cylinders 10 which generate a pulling force on the riser 14. This pulling force is generated by a pneumatic pressure in a closed volume. The system is completely passive and needs very little attention during a drilling operation if well maintained. Each tensioning cylinder 10 normally has a positioning system to determine position, speed and direction of the rod movement. A cylinder rod side of the cylinder is connected to a high pressure accumulator (not shown) via a shut off valve, and a cylinder piston side of the cylinder is connected to a low pressure vessel (not shown) for nitrogen preservation. A hose and a gooseneck connects the tensioning cylinders 10 to shut off skids placed 65 in moon pool area 7. DAT systems normally have a low weight compared to WLT-systems, which systems will be described below.

FIGS. 2 and 3 show typical prior art WLT systems arranged on an offshore installation. In such a system, the wireline riser tensioner cylinders 10 are located in the drill floor area 5. The wireline riser tensioner cylinders 10 are typically placed symmetrically around a well center axis 16 on drill floor level.

The WLT system is designed to keep close to constant tension in the marine riser 14 via a plurality of wirelines 11. It maintains the tension in each wireline 11, which is connected to a tension ring 13 on the marine riser 14. The 10 wireline 11 from the tension ring 13 runs over pivot hinged idler sheaves 12 and then around the sheave assemblies 15a-d on each end of the tensioning cylinders 10. The wireline 11 may then run, for example, three turns around a snubber drum (not shown) with the end of wireline 11 being 15 anchored to a clamp (not shown).

The WLT system is generally more protected from seawater exposure compared to the DAT system since the riser tensioning cylinders 10 are not located in the moon pool area.

FIG. 4 shows a first embodiment of a riser tensioning system 100 for a floating installation according to the present invention, where the riser tensioning system 100, for the sake of simplicity, is shown with two individually operated riser tensioning assemblies 30a and 30b. Each of 25 the riser tensioning assemblies 30a and 30b comprises a respective individually operated riser tensioning cylinder 10a, 10b, sheaves 12a, 12b and wirelines 11a, 11b.

The wireline 11a is connected at one end to a cylinder rod 60a of the tensioning cylinder 10a, runs over a sheave 12a 30 and, at its other end, is connected to a tension ring 13 which supports a marine riser 14.

Similarly, the wireline 11b is connected at one end to a cylinder rod 60b of the tensioning cylinder 10b, runs over a sheave 12b and, at its other end, is connected to the tension 35 ring 13 which supports the marine riser 14. The marine riser 14 extends downwards towards a sea floor along a riser axis 20 (see FIG. 5.).

Each of the sheaves 12a and 12b may be pivotable around a vertical axis. In use, the sheaves 12a and 12b may be fixed 40 at a suitable point in the structure of the floating installation; the sheaves 12a and 12b can, for example, be fixed above or in the vicinity of a moon pool 7 (see FIGS. 8-10).

FIG. 5 shows a second embodiment of the riser tensioning system 100 according to the present invention where a 45 wireline 11a extends between a cylinder rod 60a of the tensioning cylinder 10a and the tension ring 13, while a wireline 11b extends between a cylinder rod 60b of the tensioning cylinder 10b and the tension ring 13. In this embodiment, each of the wirelines 11a, 11b runs over a 50 respective first sheave 12a or 12b, and a respective second sheave 12c or 12d. The sheaves 12c and 12d may be pivotable around a vertical axis and can, in use, be fixed above or in the vicinity of a moon pool 7 (see FIGS. 8-10).

FIG. 5 shows the riser tensioning system 100, for the sake 55 of simplicity, with only two individually operated riser tensioning assemblies. It should be understood, however, that the riser tensioning system 100 according to the present invention can comprise more than two riser tensioning assemblies, as will be explained according to FIG. 7.

FIG. 6 shows another embodiment according to an aspect of the present invention. In this embodiment, there is provided a riser tensioning system 100 for providing tensioning to a marine riser 14 connected to a floating installation 1 (see FIGS. 8-10) via a tension ring 13. The cylinder rods 60a and 65 60b are, at their ends, connected to sheaves 12'. The wirelines 11a and 11b extend from a fixation point in the

6

structure of the installation 1 (for example, a deck) and are in their other ends connected to the tension ring 13. The wirelines 11a and 11b extend, respectively, via the sheaves 12' connected to the cylinder rods 60a and 60b, via a second sheave 12" connected to the structure of the installation 1 and to the tension ring 13. The cylinder rods 60a and 60b operate in tension, and, via the sheaves 12', provide tension to the wirelines 11a and 11b. In this embodiment, a transmission ratio of 1:2 between the cylinder rod and wireline motion can be obtained, thus permitting a shorter design stroke length of the tensioning cylinders 10a and 10b than the distance travelled by the tension ring 13.

FIG. 7 shows, from above, the embodiment of the riser tensioning system 100 according to FIG. 4, where it can be seen that the embodiment of the riser tensioning system 100 comprises eight individual riser tensioning assemblies, each comprising tensioning cylinders 10a-10h, the tensioning cylinders 10a-10h being arranged in two groups, each group comprising four tensioning cylinders 10a-10d, 10e-10h, where the groups of tensioning cylinders are placed opposite each other around a tension ring 13 for a marine riser 14.

Each of the tensioning cylinders 10a-10h are connected to a respective wireline 11a-11h, each wireline 11a-11h extending between a cylinder rod (see, for example, FIG. 4) of the tensioning cylinder 10a-10h and the tension ring 13, and being run over respective sheaves 12a-12h.

FIG. 8 shows the riser tensioning system 100 according to FIG. 4 arranged in an offshore installation 1, where the tensioning cylinders 10a-10h (only two tensioning cylinders 10a, 10b are shown for the sake of simplicity) are arranged around a moon pool 7 with a marine riser 14 therein.

A physical boundary in the form of walls 7' at least partly covers the tensioning cylinders 10a-10h and, optionally, the sheaves 12a-12h, so that the tensioning cylinders 10a-10h and the sheaves 12a-12h are not directly exposed to seawater, or at least partly protected from exposure to seawater.

In an embodiment, the walls 7' can, for example, form part of the structure of the moon pool 7. The tensioning cylinders 10a-10h are advantageously placed outside the moon pool 7. In an embodiment, the tensioning cylinders 10a-10h can, for example, be placed outside a moon pool 7 and below a drill floor 5 and a deck 9 of the offshore installation 1.

The offshore installation 1 may also comprise a base structure 17, where the base structure 17 extends at least partly around the moon pool area 7 and below the waterline 8 when the offshore installation 1 is in operation. In an embodiment, the tensioning cylinders 10a-10h can, for example, be positioned in the base structure 17 at least partly below the waterline 8.

Considerable design flexibility is achieved by providing a riser tensioning system according to the present invention, allowing freedom to position the tensioning cylinders 10a-10h below a drill floor 5 and/or a deck 9 of an offshore installation 1, while maintaining various advantages of a direct-acting tensioning or a WLT system. Examples are low complexity, flexibility low friction, high reliability, and low maintenance requirements.

The possibility of locating the tensioning cylinders outside the moon pool area 7 and/or inside the base structure 17 facilitates very short piping for hydraulic fluid, thus reducing load variations due to hydraulic flow resistance. This can be achieved by placing any required accumulators and related hydraulic/pneumatic equipment close to the tensioning cylinders 10*a*-10*h*.

According to the present invention, the tensioning cylinders can also be placed in areas with strict space restrictions, for example, in a base structure 17 alongside vertical walls

7', while any sheaves used can still be designed with a sufficient size to provide low wear on the wire rope. (This typically means a wire-to-sheave diameter ratio, D/d, of at least 30.) Arranging the tensioning cylinders 10a-10h in a position lower than the drill floor 5 and the deck 9 on a 5 floating installation 1 is advantageous in terms of vessel stability and center of gravity, and to free up space for other equipment on the drill floor 5, deck 9, and in the moon pool area 7, where strict space restrictions typically exist.

It should be understood that any of the embodiments of 10 the riser tensioning system 100 according to FIGS. 4 to 7 can be arranged in the offshore installation 1.

- FIG. 9 shows an offshore installation 1 in the form of a semi-submersible vessel where the riser tensioning system 100 according to FIG. 5 is arranged in the semi-submersible 15 vessel. The riser tensioning system 100 is arranged so that the walls 7' will protect the tensioning cylinders 10a-10h and the sheaves 12a-12h from seawater exposure, so that the riser tensioning system 100 is less affected by the harsh environment offshore.
- FIG. 10 shows a column formed offshore installation 1 where the riser tensioning system 100 is arranged in the columns of the offshore installation 1.

FIG. 11 shows an alternative embodiment of the riser tensioning system 100 as described in relation to FIG. 4. In 25 this embodiment, guide elements 70a and 70b are provided to guide the cylinder rods 60a and 60b, respectively. Each guide element 70a and 70b is adapted to guide the respective cylinder rod 60a or 60b linearly, i.e., along a linear path, in extension of the longitudinal direction of the respective 30 tensioning cylinder 10a or 10b. The guide elements 70a and 70b can, for example, support the cylinder rods 60a and 60balong their full stroke. The guide elements 70a and 70bprovide that the cylinder rods 60a and 60b are not exposed to excessive bending or transverse (side) forces, particularly 35 in their stroked-out positions, such as the situation shown in FIG. 11. This is particularly important for long-stroke cylinders which are typically used in many such installations described here (compare FIGS. 8-10).

The guide elements 70a and 70b may be in the form of 40 guides or tracks along which the cylinder rods 60a and 60b are led. The guide elements 70a and 70b are advantageously fixed on the wall 7', thereby allowing the cylinder rots 60a and 60b to extend parallel to the wall 7'.

A riser tensioning system according to any of the above 45 embodiments will typically consist of 4, 6, 8 or 10 riser tensioners cylinders 10a-10h. The number of riser tensioner cylinders depends on the application and the load requirements.

The cylinder rods **60***a*, **60***b* of the riser tensioning cylinders **10***a***-10***h* in the riser tensioning system **100** or installation **1** according to the present invention as described above advantageously operate in tension when providing a force for tensioning the wirelines **11***a***-11***h*. This provides the advantage that long-stroke cylinders can be used, without the risk of bending or side forces, as opposed to cylinders operating in compression.

In the preceding description, various aspects of the apparatus according to the present invention have been described with reference to the illustrative embodiments. For purposes of explanation, specific numbers, systems and configurations are set forth in order to provide a thorough understanding of the apparatus and its workings. This description is not, however, intended to be construed in a limiting sense. Various modifications and variations of the illustrative 65 embodiment, as well as other embodiments of the apparatus, which are apparent to persons skilled in the art to which the

8

disclosed subject matter pertains, are deemed to lie within the scope of the present invention. Reference should also be had to the appended claims.

What is claimed is:

- 1. A floating installation comprising:
- a riser tensioning system for providing a tensioning to a riser connected to the floating installation via a tension ring, the riser tensioning system comprising:
 - at least one riser tensioner assembly, each of the at least one riser tensioner assembly comprising,
 - a riser tensioning cylinder comprising a cylinder rod which is configured to work in tension,
 - at least one sheave, and
 - a wireline comprising a first end and a second end, the first end being fixed to the tension ring, and the second end being fixed to the cylinder rod, the wireline being configured to extend between the tension ring and the cylinder piston via the at least one sheave;

a moon pool; and

a base structure configured to extend at least partly around the moon pool and below a waterline,

wherein,

the riser tensioning cylinder of the at least one riser tensioner assembly is arranged in the base structure of the floating installation, and

the riser tensioning cylinder is positioned in the base structure at least partly below the waterline.

- 2. The floating installation as recited in claim 1, wherein the at least one sheave is, during a use, configured to be pivotable around an axis which is parallel to the riser.
 - 3. The floating installation as recited in claim 1, wherein, the wireline comprises a wireline diameter,
 - at least one of the at least one sheave comprises a sheave diameter, and
 - a ratio between the wireline diameter and the sheave diameter is at least 30.
- 4. The floating installation as recited in claim 1, wherein the at least one riser tensioner assembly comprises 4, 6, 8 or 10 riser tensioner assemblies.
- 5. The floating installation as recited in claim 1, further comprising:
 - a physical boundary that at least partly covers the riser tensioning cylinder of the at least one riser tensioner assembly, the physical boundary being configured to at least partly block any direct exposure of ambient water onto the riser tensioning cylinder during a use.
- 6. The floating installation as recited in claim 5, wherein the riser tensioning system further comprises:
 - at least one guide element configured to guide the cylinder rod in a linear direction.
- 7. The floating installation as recited in claim 6, wherein the at least one guide element is fixed to the physical boundary.
 - 8. The floating installation as recited in claim 5, wherein, the moon pool comprises walls, and
 - the physical boundary also comprises the walls of the moon pool.
- 9. The floating installation as recited in claim 1, further comprising:
 - a drill floor; and
 - a deck,
 - wherein,

the riser tensioning cylinder of the at least one riser tensioner assembly is arranged below the drill floor and the deck of the floating installation.

- 10. The floating installation as recited in claim 1, wherein the floating installation is a drilling vessel.
 - 11. A floating installation comprising:
 - a riser tensioning system for providing a tensioning to a riser connected to a floating installation via a tension 5 ring, the riser tensioning system comprising:
 - at least one riser tensioner assembly, each of the at least one riser tensioner assembly comprising,
 - a riser tensioning cylinder comprising a cylinder rod which is configured to work in tension,
 - at least one first sheave fixed to the cylinder rod,
 - at least one second sheave, and
 - a wireline comprising a first end and a second end, the first end being fixed to the tension ring, and the second end being fixed to the floating installation, 15 the wireline being configured to extend between the tension ring and the cylinder piston via at least one of the at least one first sheave and the at least one second sheave;
 - a moon pool;
 - a base structure configured to extend at least partly around the moon pool and below a waterline; and
 - a wall arranged in the base structure above the riser tensioning cylinder, the wall being configured to at least partly cover the riser tensioning cylinder so as to 25 protect the riser tensioning cylinder from exposure to seawater,

wherein,

- the riser tensioning cylinder of the at least one riser tensioner assembly is arranged in the base structure of 30 the floating installation, and
- the riser tensioning cylinder is positioned in the base structure at least partly below the waterline.
- 12. The floating installation as recited in claim 11, wherein the at least one second sheave, during a use, is 35 configured to be pivotable around an axis which is parallel to the riser.
- 13. The floating installation as recited in claim 11, wherein,

the wireline comprises a wireline diameter,

10

- at least one of the at least one first sheave and the at least one second sheave comprises a sheave diameter, and
- a ratio between the wireline diameter and the sheave diameter is at least 30.
- 14. The floating installation system as recited in claim 11, wherein the at least one riser tensioner assembly comprises 4, 6, 8 or 10 riser tensioner assemblies.
- 15. The floating installation as recited in claim 11, further comprising:
 - a physical boundary that at least partly covers the riser tensioning cylinder of the at least one riser tensioner assembly, the physical boundary being configured to at least partly block any direct exposure of ambient water onto the riser tensioning cylinder during a use.
- 16. The floating installation as recited in claim 15, wherein the riser tensioning system further comprises:
- at least one guide element configured to guide the cylinder rod in a linear direction.
- 17. The floating installation as recited in claim 16, wherein the at least one guide element is fixed to the physical boundary.
- 18. The floating installation as recited in claim 15, wherein,

the moon pool comprises walls, and

- the physical boundary also comprises the walls of the moon pool.
- 19. The floating installation as recited in claim 11, further comprising:
 - a drill floor; and
 - a deck,
 - wherein,
 - the riser tensioning cylinder of the at least one riser tensioner assembly is arranged below the drill floor and the deck of the floating installation.
- 20. The floating installation as recited in claim 11, wherein the floating installation is a drilling vessel.

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