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**Niwa et al.**

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(54) **MAGNETIC STORAGE APPARATUS INCLUDING A MAGNETIC RECORDING MEDIUM HAVING A BARRIER LAYER BETWEEN TWO HEAT SINK LAYERS**

(58) **Field of Classification Search**  
CPC ..... G11B 5/667; G11B 5/706; G11B 5/7325  
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(57) **ABSTRACT**

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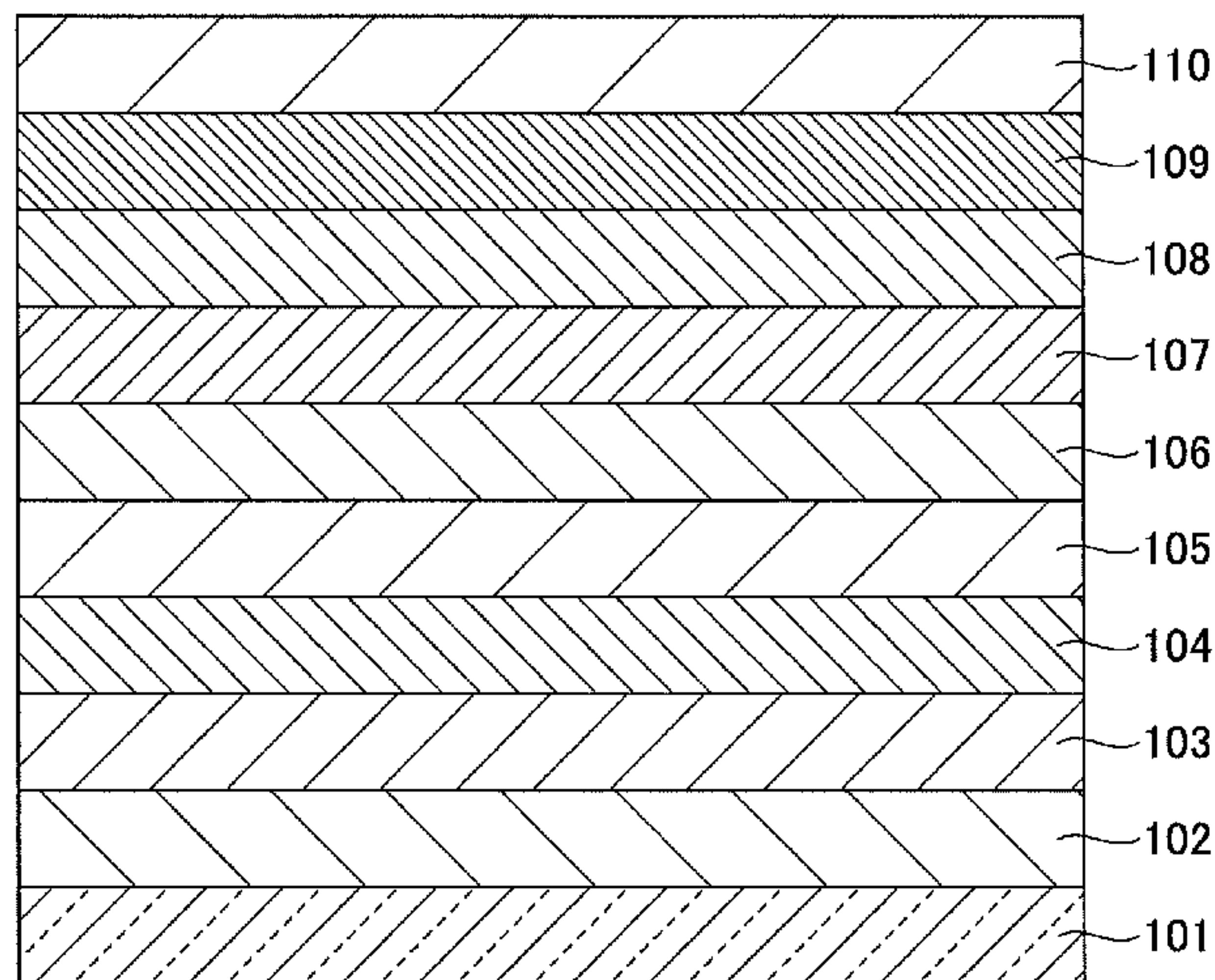
A magnetic recording medium includes a substrate, a first heat sink layer, a barrier layer, a second heat sink layer, and a magnetic layer that are successively stacked. The magnetic layer is made of a material including a first main component that is an alloy having a L1<sub>0</sub> crystal structure and a content of 50 at % or higher, or content of 50 mol % or higher. The barrier layer is made of a material including a second main component that is one of an oxide, a nitride, and a carbide having a content of 50 at % or higher, or content of 50 mol % or higher.

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401



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*G11B 5/00* (2006.01)
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- (58) **Field of Classification Search**  
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 See application file for complete search history.

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FIG. 1

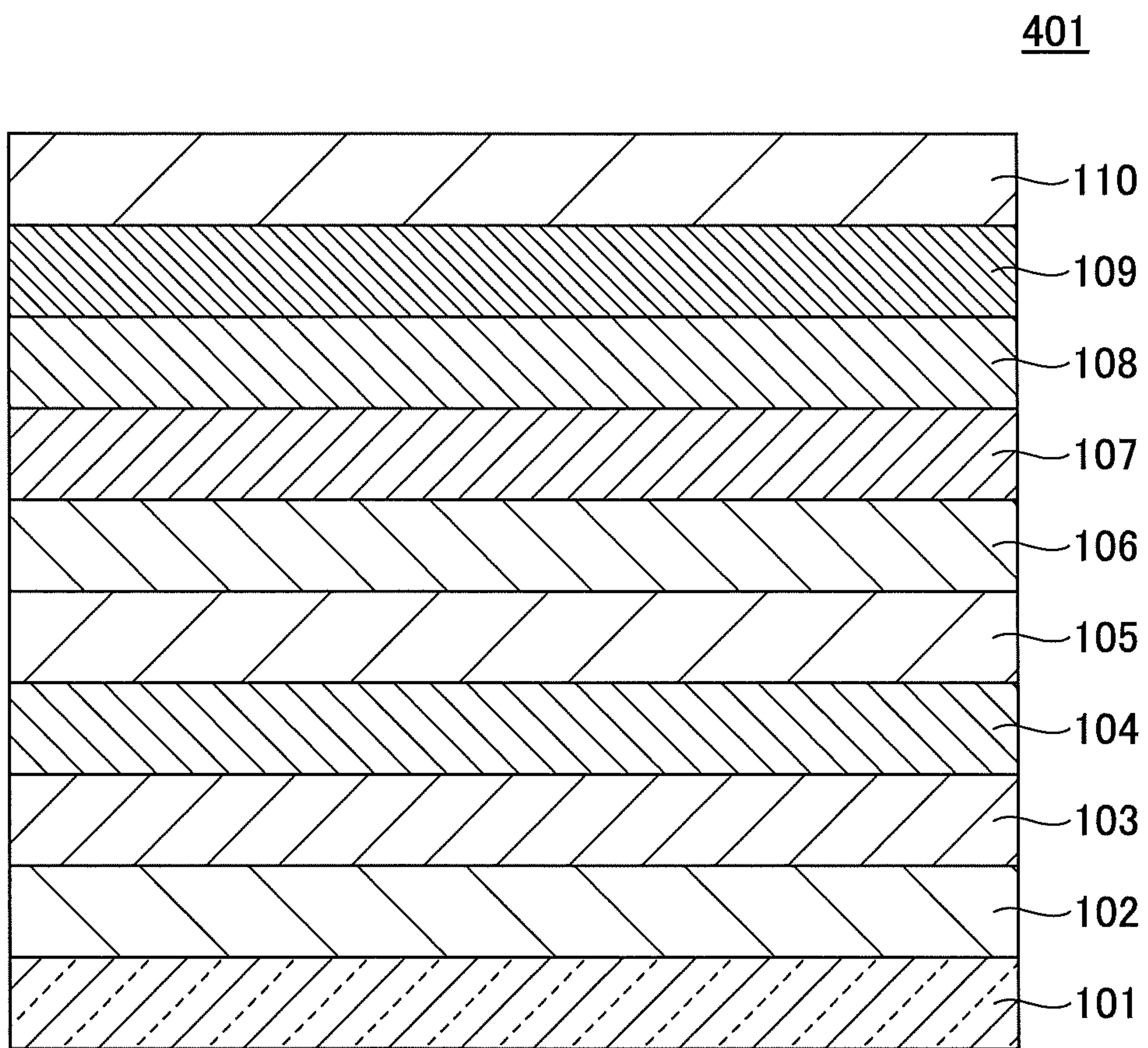




FIG.2

MATERIAL	THERMAL CONDUCTIVITY [W/m·K]	THICKNESS OF 1ST HEAT SINK LAYER [nm]
Ag	425	10
Au	316	20
Al	238	20
Cu	397	15
Rh	148	25
Mo	137	25
W	174	25

FIG.3

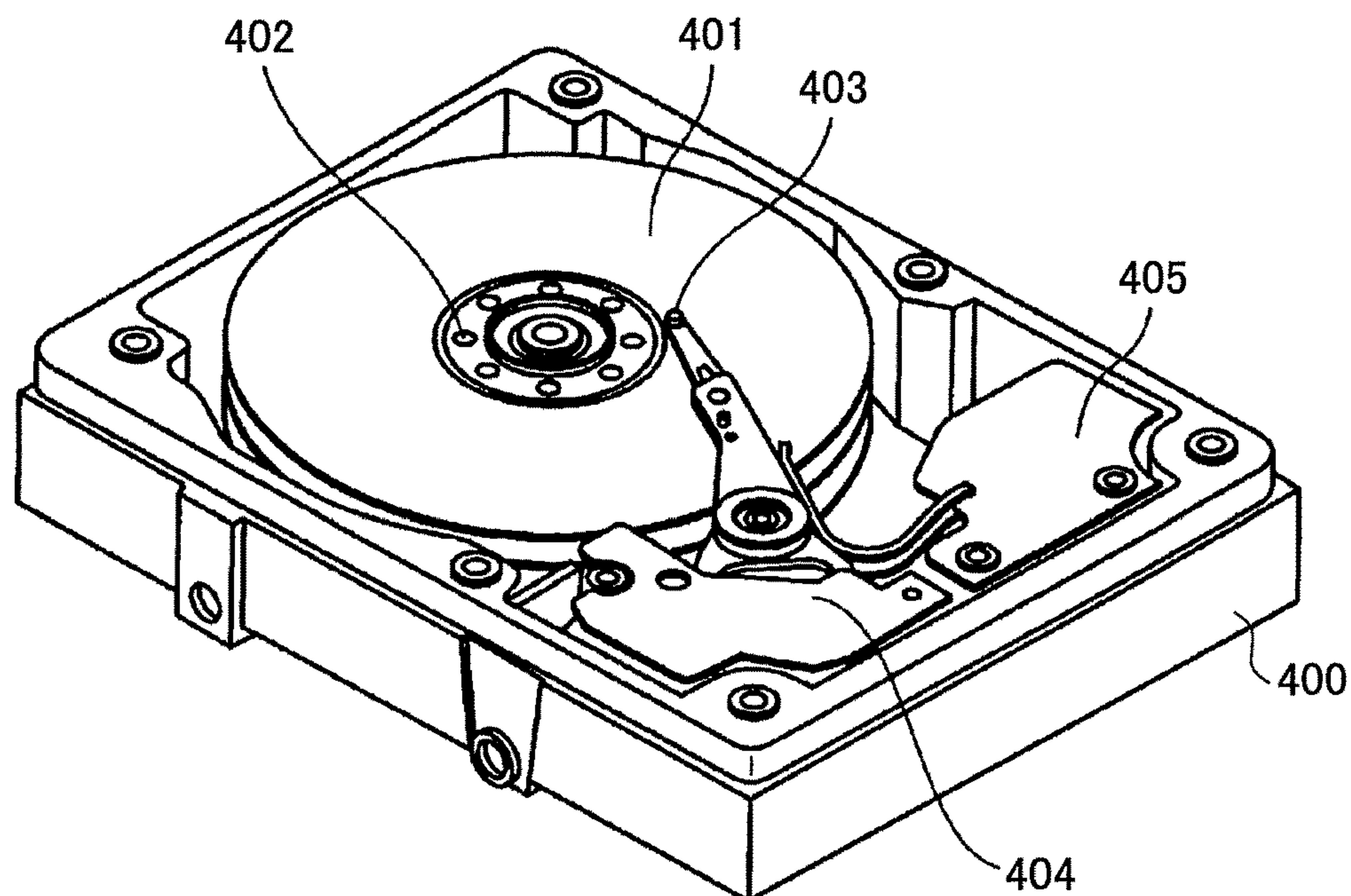


FIG. 4

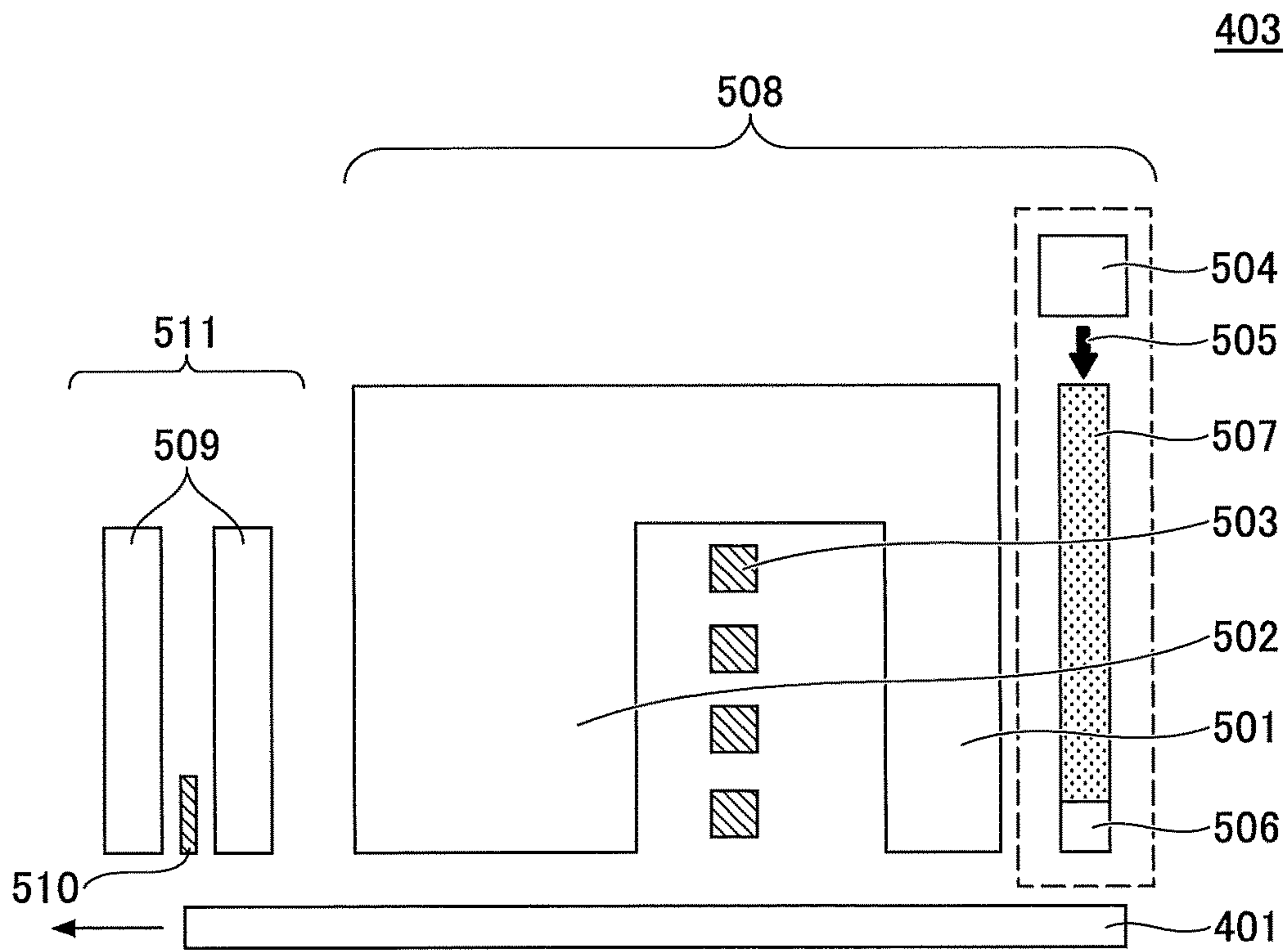


FIG.5

	1ST HEAT SINK LAYER		1ST BARRIER LAYER				2ND HEAT SINK LAYER		2ND BARRIER LAYER		$\Delta$ SNR [dB]	$\Delta$ LDI /LDI [%]	CT-TG [K/nm]
	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]	THERMAL CONDUCTIVITY [W/m·K]	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]				
EI1-1	W	30	MgO	2.5	50-75	W	5	MgO	4	$\pm 0$	-4.5	3.4	
EI1-2	W	30	MgO-46mol%TiO	2.5	-	W	5	MgO	4	$\pm 0$	-4.2	3.5	
EI1-3	W	30	TaN	2.5	8.3	W	5	MgO	4	$\pm 0$	-3.5	3.5	
EI1-4	W	30	ZrN	2.5	20.9	W	5	MgO	4	$\pm 0$	-4.8	3.6	
EI1-5	W	30	TiN	2.5	29.1	W	5	MgO	4	$\pm 0$	-4.3	3.5	
EI1-6	W	30	NbN	2.5	3.6	W	5	MgO	4	$\pm 0$	-3.5	3.3	
EI1-7	W	30	HfN	2.5	21.6	W	5	MgO	4	$\pm 0$	-3.9	3.4	
EI1-8	W	30	ZrC	2.5	20.6	W	5	MgO	4	$\pm 0$	-5.2	3.6	
EI1-9	W	30	TaC	2.5	22.2	W	5	MgO	4	$\pm 0$	-3.5	3.4	
EI1-10	W	30	TiC	2.5	17-21	W	5	MgO	4	$\pm 0$	-5.2	3.6	
EI1-11	W	30	NbC	2.5	14.2	W	5	MgO	4	$\pm 0$	-3.8	3.3	
EI1-12	W	30	MgO-38mol% TiO-10mol%TiN	2.5	-	W	5	MgO	4	$\pm 0$	-5.4	3.6	
EI1-13	W	30	MgO-38mol% TiO-10mol%TaN	2.5	-	W	5	MgO	4	$\pm 0$	-5.4	3.6	
CE1-1	W	35	-	-	-	-	-	MgO	4	ref1	ref2	2.7	
CE1-2	W	30	Cr	2.5	91.3	W	5	MgO	4	$\pm 0$	4.0	2.7	
CE1-3	W	30	Ta	2.5	57.6	W	5	MgO	4	-0.5	$\pm 0$	2.7	
CE1-4	W	30	V	2.5	31.6	W	5	MgO	4	-0.9	0.5	2.5	
CE1-5	W	30	Nb	2.5	54.1	W	5	MgO	4	$\pm 0$	$\pm 0$	2.7	
CE1-6	W	30	Hf	2.5	22.9	W	5	MgO	4	-1.5	0.5	2.5	



FIG.6

	1ST HEAT SINK LAYER		1ST BARRIER LAYER		2ND HEAT SINK LAYER		2ND BARRIER LAYER		SNR [dB]	LDI [mA]	MWW [nm]	CT-TG [K/nm]
	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]				
EI2-1	W	25	ZrN	2.5	W-10at%Ta	5	MgO	4	12.5	46.0	60.5	3.1
EI2-2	W	30	ZrN	2.5	W-10at%Ta	5	MgO	4	12.7	47.5	66.0	3.4
EI2-3	W	35	ZrN	2.5	W-10at%Ta	5	MgO	4	12.9	49.0	72.5	3.7
EI2-4	W	40	ZrN	2.5	W-10at%Ta	5	MgO	4	13.2	50.5	78.3	3.9
CE2-1	W	25	-	-	W-10at%Ta	5	MgO	4	12.5	49.0	61.6	2.3
CE2-2	W	30	-	-	W-10at%Ta	5	MgO	4	12.7	50.5	66.4	2.6
CE2-3	W	35	-	-	W-10at%Ta	5	MgO	4	12.9	52.0	72.1	2.9

FIG.7

	1ST HEAT SINK LAYER		1ST BARRIER LAYER		2ND HEAT SINK LAYER		2ND BARRIER LAYER		$\Delta$ SNR [dB]	$\Delta$ LDI /LDI [%]
	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]	MATERIAL	THICKNESS [nm]		
EI3-1	W-5mol%SiO <sub>2</sub>	25	NbC	1	W-5mol%SiO <sub>2</sub>	5	MgO	5	$\pm$ 0	-4.5
EI3-2	W-5mol%SiO <sub>2</sub>	25	NbC	2.5	W-5mol%SiO <sub>2</sub>	5	MgO	5	$\pm$ 0	-5.1
EI3-3	W-5mol%SiO <sub>2</sub>	25	NbC	5	W-5mol%SiO <sub>2</sub>	5	MgO	5	$\pm$ 0	-5.0
EI3-4	W-5mol%SiO <sub>2</sub>	25	NbC	10	W-5mol%SiO <sub>2</sub>	5	MgO	5	$\pm$ 0	-5.0
EI3-5	W-5mol%SiO <sub>2</sub>	25	NbC	20	W-5mol%SiO <sub>2</sub>	5	MgO	5	$\pm$ 0	-2.2
CE3-1	W-5mol%SiO <sub>2</sub>	25	-	-	W-5mol%SiO <sub>2</sub>	5	MgO	5	ref3	ref4



**MAGNETIC STORAGE APPARATUS  
INCLUDING A MAGNETIC RECORDING  
MEDIUM HAVING A BARRIER LAYER  
BETWEEN TWO HEAT SINK LAYERS**

CROSS-REFERENCE TO RELATED  
APPLICATIONS

This application is based upon and claims priority to Japanese Patent Application No. 2017-030003 filed on Feb. 21, 2017, the entire contents of which are incorporated herein by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to a magnetic recording medium, and a magnetic storage apparatus including the magnetic recording medium.

2. Description of the Related Art

In order to further increase recording capacity (or storage capacity) of magnetic storage apparatuses such as HDDs (Hard Disk Drives), developments are made to increase recording density (or storage capacity) of magnetic recording media that are used in the HDDs. However, it is becoming more difficult to simultaneously reduce the size of magnetic grains forming a magnetic layer, improve thermal stability, and improve recording characteristics. This difficulty is also referred to as trilemma. On the other hand, active research and development in heat assisted magnetic recording methods show next-generation recording methods capable of overcoming the trilemma.

The heat assisted magnetic recording method uses a magnetic head having a laser light generator that generates laser light to irradiate near-field light on the magnetic recording medium. As a result, a surface of the magnetic recording medium is locally heated to assist recording, to record information on the magnetic recording medium in a state in which a coercivity of the magnetic recording medium is locally reduced. Because the heat assisted magnetic recording method heats the magnetic recording medium by the near-field light, measures are taken to control heating temperature and spreading of heat.

Examples of the measures taken to control heat include providing a heat sink layer made of high thermal conductivity material for the purposes of increasing thermal gradient and heat dissipation, providing a heat barrier layer under the magnetic layer for the purposes of effectively heating the magnetic layer, and providing a reflection control layer for the purposes of reducing reflection from the magnetic recording medium.

Various research, developments, and reports are made on the measures to control heat of the magnetic recording media used by the heat assisted magnetic recording method.

For example, U.S. Patent Publication No. US 2007/0026263 A1 proposes a magnetic recording medium having the heat sink layer including CuZr or AgPd, provided between a substrate and a magnetic recording layer.

In addition, Japanese Laid-Open Patent Publication No. 2006-196151 proposes a heat assisted magnetic recording medium having a temperature control layer formed by a thin film including regions of low thermal conductivity material at least partially through a thickness of the film, and regions of high thermal conductivity material separating the regions

of low thermal conductivity material. The high thermal conductivity material is Cu, Au, Ag, or the like, for example. On the other hand, the low thermal conductivity material is SiO<sub>2</sub>, ZrO<sub>2</sub>, or the like, for example.

For example, Japanese Laid-Open Patent Publication No. 2016-522957 proposes a stack including a heat sink layer, and a MgO—Ti(ON) layer. The heat sink layer is arranged between the substrate and the magnetic recording layer. The Mg—Ti(ON) layer is arranged between the heat sink layer and the magnetic recording layer.

On the other hand, Japanese Laid-Open Patent Publication No. 2015-26411 proposes a magnetic recording medium including a barrier layer having a NaCl type crystal structure. The barrier layer is provided between a crystalline underlayer including Mo as a main component, and a magnetic layer. The crystalline underlayer includes one or more elements selected from Si and C in a range of 1 mol % to 20 mol %, or an oxide in a range of 1 vol % to 50 vol %.

Further, Japanese Laid-Open Patent Publication No. 2015-122137 proposes a magnetic recording medium including the magnetic recording layer above a plasmon underlayer that includes an Au alloy. The Au alloy includes one or more alloy constituent elements substantially not mixed to Au.

The magnetic recording medium may be designed to increase the thickness of the heat sink layer made of the high thermal conductivity material, that is, to increase a laser diode current LDI applied to a laser diode of the magnetic head. In this case, there are tendencies for the thermal gradient to become sharp and SNR (Signal-to-Noise Ratio) to become high.

However, when the laser diode current LDI is increased, load on elements forming the magnetic head increases, to more easily deteriorate the magnetic head. The HDD not only requires high recording density, but also high reliability. For this reason, magnetic heads that easily deteriorate are undesirable for the HDD.

Accordingly, in the HDD using the heat assisted magnetic recording method, reducing the laser diode current LDI is highly desired from viewpoints of reducing the load on the magnetic head and extending serviceable life of the magnetic head.

However, reducing (or improving) the laser diode current LDI and increasing (or improving) the SNR are in a tradeoff relationship. Consequently, simply reducing the laser diode current LDI decreases (or deteriorates) the SNR. In other words, it is conventionally difficult to reduce the laser diode current LDI without decreasing (or deteriorating) the SNR.

SUMMARY OF THE INVENTION

Embodiments of the present invention can provide a magnetic recording medium and a magnetic storage apparatus, capable of reducing the laser diode current LDI applied to the laser diode of the magnetic head without deteriorating the SNR.

According to one aspect of the present invention, a magnetic recording medium includes a substrate, a first heat sink layer provided on the substrate, a first barrier layer provided on the first heat sink layer, a second heat sink layer provided on the first barrier layer, and a magnetic layer provided on the second heat sink layer, wherein the magnetic layer is made of a material including a first main component that is an alloy having a L1<sub>0</sub> crystal structure and a content of 50 at % or higher, or content of 50 mol % or higher, and wherein the first barrier layer is made of a material including



a second main component that is one of an oxide, a nitride, and a carbide having a content of 50 at % or higher, or content of 50 mol % or higher.

The second main component may have a NaCl type crystal structure, and may be selected from a group of materials consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, ZrN, VN, CrN, TiC, TaC, NbC, HfC, and ZrC.

Each of the first heat sink layer and the second heat sink layer may be made of a material including a third main component that is selected from a group materials consisting of Ag, Au, Al, Cu, Rh, Mo, and W, and having a content of 50 at % or higher, or content of 50 mol % or higher.

According to another aspect of the present invention, a magnetic storage apparatus includes a magnetic recording medium, a magnetic head configured to write information to and read information from the magnetic recording medium, and a casing configured to accommodate the magnetic recording medium and the magnetic head, wherein the magnetic head includes a laser light generator configured to generate laser light, a waveguide configured to guide the laser light to a tip end of the magnetic head, and a near-field light generator configured to generate near-field light that heats the magnetic recording medium, wherein the magnetic recording medium includes a substrate, a first heat sink layer, a first barrier layer, a second heat sink layer, and a magnetic layer that are successively stacked, wherein the magnetic layer is made of a material including a first main component that is an alloy having a  $L1_0$  crystal structure and a content of 50 at % or higher, or content of 50 mol % or higher, and wherein the first barrier layer is made of a material including a second main component that is one of an oxide, a nitride, and a carbide having a content of 50 at % or higher, or content of 50 mol % or higher.

Other objects and further features of the present invention will be apparent from the following detailed description when read in conjunction with the accompanying drawings.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross sectional view illustrating an example of a magnetic recording medium in one embodiment of the present invention;

FIG. 2 is a table illustrating materials, thermal conductivities, and thicknesses of a first heat sink layer;

FIG. 3 is a perspective view illustrating an example of a magnetic storage apparatus in one embodiment of the present invention;

FIG. 4 is a cross sectional view schematically illustrating a structure of a magnetic head illustrated in FIG. 3;

FIG. 5 is a table illustrating configuration and properties of magnetic recording media in a first embodiment and a first comparison example;

FIG. 6 is a table illustrating configuration and properties of magnetic recording media in a second embodiment and a second comparison example; and

FIG. 7 is a table illustrating configuration and properties of magnetic recording media in a third embodiment and a third comparison example.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Embodiments and exemplary implementations of a magnetic recording medium and a magnetic storage apparatus according to the present invention will be described, by referring to the drawings. In each of the embodiments, the configuration, arrangement or position, material, and

amount (at % or mol %) of element used in the magnetic recording medium or the magnetic storage apparatus may be appropriately modified, unless indicated otherwise.

[Magnetic Recording Medium]

FIG. 1 is a cross sectional view illustrating an example of a magnetic recording medium 401 in one embodiment of the present invention. In this example, the magnetic recording medium 401 is a heat assisted magnetic recording medium. The heat assisted magnetic recording medium is sometimes also referred to as a thermally assisted magnetic recording medium.

The magnetic recording medium 401 includes a substrate 101, an adhesion layer 102, an orientation control layer 103, a first heat sink layer 104, a first barrier layer 105, a second heat sink layer 106, a second barrier layer 107, a magnetic layer 108, a protection layer 109, and a lubricant layer 110 that are stacked in this order. The first barrier layer 105 is made of a material including a main component that is one of an oxide, a nitride, and a carbide. The magnetic layer 108 is made of a material including a main component that is an alloy having a  $L1_0$  crystal structure.

The constitution of "a main component" of a material will be described later in the specification.

The stacked configuration of the magnetic recording medium 401 enable reduction in a laser diode current LDI applied to a laser diode of a magnetic head, that is, reduce a laser diode power of the magnetic head, without deteriorating the SNR. As a result, it is possible to extend the serviceable life of the magnetic head, and provide the magnetic recording medium 401 having a high recording density.

The effect of reducing the laser diode current LDI applied to the laser diode of the magnetic head without deteriorating the SNR is obtained because the first barrier layer 105, made of the material including the main component that is one of the oxide, the nitride, and the carbide, is sandwiched between the first heat sink layer 104 and the second heat sink layer 106 respectively having thermal conductivities higher than a thermal conductivity of the first barrier layer 105. It may be regarded that the sandwiched configuration, in which the first barrier layer 105 is sandwiched between the first and second heat sink layers 104 and 106, enables efficient use of heat of laser light irradiated from the magnetic head. Preferably, the first barrier layer 105 that is thin, is sandwiched between the first and second heat sink layers 104 and 106 that are thick. As a result, it is possible to form an interface having a large thermal conductivity difference between the first barrier layer 105 and each of the first and second heat sink layers 104 and 106, without deteriorating the effects of the first and second heat sink layers 104 and 106. The interface causes a larger thermal gradient (or heat gradient) to be generated within the first and second heat sink layers 104 and 106. It may be regarded that the larger thermal gradient increases heat transfer in a direction perpendicular to a recording surface of the magnetic recording medium 401. For example, the recording surface of the magnetic recording medium 401 may be formed by an exposed surface (that is, an upper surface in FIG. 1) of the lubricant layer 110.

The material forming the first heat sink layer 104 may be the same as, or may be different from, a material forming the second heat sink layer 106. The materials that are the same may have the same composition with identical constituent-element-contents, or may have the same composition with mutually different constituent-element-contents. The "constituent-element-content" of the material refers to a content (or amount) of the constituent element within the material.



The first and second heat sink layers **104** and **106** are provided to diffuse the heat, accumulated in the magnetic layer **108**, in the direction perpendicular to the recording surface of the magnetic recording medium **401**, in order to reduce spreading of the heat in a direction parallel to the recording surface of the magnetic recording medium **401**. In addition, the first and second heat sink layers **104** and **106** are provided to reduce spreading of the heat in the direction parallel to the recording surface of the magnetic recording medium **401**, in order to reduce a transition width of heat and to quickly dissipate the heat accumulated in the magnetic layer **108** after recording. For this reason, the first and second heat sink layers **104** and **106**, are preferably made of a high thermal conductivity material having a high thermal conductivity.

The first and second heat sink layers **104** and **106** are preferably made of a material including a main component that is selected from a group consisting of Ag, Au, Al, Cu, Rh, Mo, and W.

Next, a more detailed description will be given of the main component of each of the first and second heat sink layers **104** and **106**.

First, the present inventors used W having a thermal conductivity of 174 W/m·K for the first and second heat sink layers **104** and **106**, and designed the magnetic recording medium **401** capable of reducing the laser diode current LDI applied to the laser diode of the magnetic head without deteriorating the SNR. The SNR is measured by a known or conventional method of recording a signal on the magnetic recording medium **401** by the magnetic head, reproducing the recorded signal from the magnetic recording medium **401** by the magnetic head, and computing a ratio of a signal component of the reproduced signal to a noise component included in the reproduced signal.

More particularly, a stacked structure (design reference) is obtained by successively stacking the first heat sink layer **104** made of W and having a thickness of 25 nm, the first barrier layer **105** made of MgO and having a thickness of 2.5 nm, the second heat sink layer **106** made of W and having a thickness of 5 nm, the second barrier layer **107** made of MgO and having a thickness of 4 nm, and the magnetic layer **108** made of a material including a main component that is an alloy having a  $L1_0$  crystal structure.

The thermal gradients of the first and second heat sink layers **104** and **106** are computed from the reference stacked structure of the magnetic recording medium **401**. In addition, materials usable for the first and second heat sink layers **104** and **106** are studied from materials having a FCC (Face Centered Cubic) crystal structure or a BCC (Body Centered Cubic) crystal structure suited for controlling the orientation of the magnetic layer **108** made of the material including the main component that is the alloy having the  $L1_0$  crystal structure, and thermal conductivities of such materials having the FCC or BCC crystal structure. As a result, Ag, Au, Al, Cu, Rh, and Mo are selected as the materials suitable for the first and second heat sink layers **104** and **106**.

FIG. 2 is a table illustrating the materials, the thermal conductivities, and the thicknesses of the first heat sink layer **104**. FIG. 2 illustrates the thermal conductivities of Ag, Au, Al, Cu, Rh, and Mo, and the thicknesses of the first heat sink layer **104** that is designed to approximate the thermal gradient of the magnetic recording medium **401** having the reference stacked structure.

The thermal conductivities of Ag, Au, Al, Cu, Rh, and Mo illustrated in FIG. 2 have values referenced from "Metal

Data Book", pp. 12-13, Revised 4th Edition, series by The Japan Institute of Metals and Materials, Maruzen Co., Ltd. (pub.), 2004.

More preferably, the first and second heat sink layers **104** and **106** are made of a material including a main component that is (100)-face oriented crystalline Mo or W having the BCC crystal structure. In this case, it is possible to improve (100) orientation of the magnetic layer **108**, because the first and second heat sink layers **104** and **106** can be formed without greatly deteriorating the orientation between the first and second barrier layers **105** and **107**. In addition, although the magnetic recording medium **401** at the time of manufacture is heated to a high temperature, W and Mo are metals having a high melting point, and W and Mo are not greatly affected by heat.

In this specification and the claims, "a main component" of a material refers to a component having a content (or amount) of 50 at % or higher, or a content (or amount) of 50 mol % or higher, in the material. In other words, the amount of the main component present in the material is 50 at % or higher, or 50 mol % or higher. Preferably, the "main component" of the material refers to the component having a content (or amount) of 60 at % or higher, or a content (or amount) of 60 mol % or higher, in the material. In a case in which the material includes no constituent element having the content of 50 at % or higher, or the content of 50 mol % or higher, the main component may be one of the constituent elements of the material having a highest content (amount).

The first and second heat sink layers **104** and **106** may include at least one kind of oxide selected from a group consisting of  $B_2O_3$ ,  $GeO_2$ , MgO,  $SiO_2$ , TiO, and  $TiO_2$ , within a content range that does not greatly reduce the thermal conductivity. In this case, it is possible to diffuse the heat, accumulated in the magnetic layer **108**, in the direction perpendicular to the recording surface of the magnetic recording medium **401**, and increase the effect of reducing the spreading of the heat in the direction parallel to the recording surface of the magnetic recording medium **401**.

Next, the thicknesses of the first and second heat sink layers **104** and **106** will be described.

The first barrier layer **105** prevents diffusion of the heat supplied from the magnetic head. Hence, in order to efficiently utilize the effects of the first barrier layer **105** at the magnetic layer **108**, the first barrier layer **105** is preferably arranged close to the magnetic layer **108**. For this reason, the second heat sink layer **106** is preferably made thinner than the first heat sink layer **104**.

The thickness of the second heat sink layer **106** is preferably 0.5 nm or greater and 25 nm or less, and more preferably 1 nm or greater and 10 nm or less.

The thermal conductivities of the first and second heat sink layers **104** and **106** are preferably high. For this reason, the main component of the material forming the first and second heat sink layers **104** and **106** has a thermal conductivity of 100 W/m·K or higher, and more preferably 120 W/m·K or higher. In this case, it is possible to increase the thermal conductivity in the direction perpendicular to the recording surface of the magnetic recording medium **401**, at the first and second heat sink layers **104** and **106**. As a result, the thermal gradient in the direction perpendicular to the recording surface of the magnetic recording medium **401** becomes sharp, and the SNR of the magnetic recording medium **401** increases (or improves).

The main component of the material forming the first barrier layer **105** preferably has a NaCl type crystal structure. Examples of oxides having the NaCl type crystal structure include MgO, TiO, NiO, or the like. Examples of



nitrides having the NaCl type crystal structure include TiN, TaN, NbN, HfN, ZrN, VN, CrN, or the like. Examples of carbides having the NaCl type crystal structure include TiC, TaC, NbC, HfC, ZrC, or the like. Hence, the main component of the material forming the first barrier layer **105**,  
5 having the NaCl type crystal structure, may be selected from a group consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, ZrN, VN, CrN, TiC, TaC, NbC, HfC, and ZrC.

In the main component of the material forming the first barrier layer **105**, a ratio of the number of one of oxygen atoms, nitrogen atoms, and carbon atoms to the number of metal atoms is preferably 1:1. Of course, one of the oxides, nitrides, and carbides not having the ratio 1:1 with respect to the number of metal atoms may coexist in the material forming the first barrier layer **105**.  
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The thickness of the first barrier layer **105** is preferably 1 nm or greater and 10 nm or less, and more preferably 2.5 nm or greater and 10 nm or less. The effect of the first barrier layer **105** preventing the diffusion of heat increases when the thickness of the first barrier layer **105** is 1 nm or greater. On the other hand, the effect of the first and second heat sink layers **104** and **106** dissipating the heat increases when the thickness of the first barrier layer **105** is 10 nm or less.  
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The first barrier layer **105** may have a multi-layer structure that includes a plurality of stacked layers forming the first barrier layer **105**. Materials forming the plurality of stacked layers of the first barrier layer **105** having the multi-layer structure may be appropriately selected by taking into consideration crystal structures, lattice mismatches (or lattice misfits), or the like of the materials.  
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In one embodiment, the first barrier layer **105** is sandwiched between the first and second heat sink layers **104**, and in such a sandwiched configuration, it is preferable to take into consideration lattice matching of the layers in the sandwiched configuration. In other words, by forming the first barrier layer **105** by the material in which the main component has the NaCl type crystal structure, it is possible to maintain satisfactory orientation in the sandwiched configuration, and obtain satisfactory orientation of the magnetic layer **108**.  
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The first barrier layer **105** may be formed by DC sputtering or RF sputtering, using a sputtering target that is made of a composition of the main component in the material forming the first barrier layer **105**. In addition, the first barrier layer **105** may be formed by reactive sputtering that introduces oxygen, nitrogen, or hydrocarbon into a metal sputtering target. As long as the first barrier layer **105** finally has the desired composition and thickness, the effect of preventing diffusion of heat is obtainable regardless of the method used to form or deposit the first barrier layer **105**.  
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The thermal conductivity of the first barrier layer **105** is required to be lower than the thermal conductivities of the first and second heat sink layers **104** and **106**. For this reason, the thermal conductivity of the main component in the material forming the first barrier layer **105** is preferably 80 W/m·K or lower, and more preferably 30 W/m·K or lower.  
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In one embodiment, the first heat sink layer **104** and the first barrier layer **105** are in contact with each other, and the first barrier layer **105** and the second heat sink layer **106** are in contact with each other. According to this configuration, it is possible to further improve the effect of reducing the laser diode current LDI applied to the laser diode of the magnetic head and the effect of increasing (or improving) the SNR.  
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In one embodiment, the orientation control layer **103** is provided between the substrate **101** and the first heat sink

layer **104**. The orientation control layer **103** may be made of a Cr layer having the BCC crystal structure, or an alloy layer having the BCC crystal structure and including Cr as a main component thereof, or an alloy layer having a B2 crystal structure.  
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Examples of the alloy forming the alloy layer having the BCC crystal structure and including Cr as the main component thereof, include CrMn, CrMo, CrW, CrV, CrTi, CrRu, or the like. In this case, the crystal grain size, dispersion, or the like may be improved by adding B, Si, C, or the like to the alloy having the BCC crystal structure and including Cr as the main component thereof. On the other hand, examples of the alloy forming the alloy layer having a B2 crystal structure include RuAl, NiAl, or the like.  
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In one embodiment, the second barrier layer **107** is provided between the second heat sink layer **106** and the magnetic layer **108**. A main component of the material forming the second barrier layer **107**, having the NaCl type crystal structure, is preferably selected from a group consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, and TiC.  
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The second barrier layer **107** functions as a thermal barrier so that it is possible to efficiently utilize the magnetic layer **108** without diffusing heat supplied from the magnetic head. The second barrier layer **107** is required to have a thermal conductivity lower than the thermal conductivity of the magnetic layer **108**, in order to reduce the diffusion of heat by an interface formed between the second barrier layer **107** and the magnetic layer **108**.  
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The second barrier layer **107** also has a function to control the orientation of the magnetic layer **108** having the L1<sub>0</sub> crystal structure. For this reason, the main component of the material forming the second barrier layer **107** preferably has the NaCl type crystal structure and a relatively small lattice mismatch (or misfit) with the lattice constant of the magnetic layer **108** having the L1<sub>0</sub> crystal structure. From this viewpoint, the main component of the material forming the second barrier layer **107** is more preferably MgO or TiN.  
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The main component of the alloy forming the magnetic layer **108** has the L1<sub>0</sub> crystal structure.  
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Generally, in order to achieve a high recording density, the magnetic layer is preferably formed by magnetic grains having a grain diameter on the order of several nm and isolated by a grain boundary segregation material. However, the magnetic recording medium becomes thermally unstable as a volume of the magnetic grains decreases. Hence, in one embodiment, the main component of the alloy forming the magnetic layer **108** has the L1<sub>0</sub> crystal structure and high magnetic anisotropy energy.  
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In the magnetic layer **108**, the magnetic grains are preferably magnetically isolated. The grain boundary segregation material may be added to the alloy having the L1<sub>0</sub> crystal structure, such as FePt alloys, CoPt alloys, or the like, in order to control the magnetic grain size and the exchange coupling between the magnetic grains. Hence, the magnetic layer **108** becomes a granular structure which can reduce the exchange coupling between the magnetic grains and reduce the magnetic grain size. As a result, it is possible to further increase (or improve) the SNR of the magnetic recording medium **401**.  
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Examples of the grain boundary segregation material include at least one kind of compound selected from a group consisting of SiO<sub>2</sub>, TiO<sub>2</sub>, Cr<sub>2</sub>O<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub>, B<sub>2</sub>O<sub>3</sub>, Ta<sub>2</sub>O<sub>5</sub>, ZrO<sub>2</sub>, Y<sub>2</sub>O<sub>3</sub>, CeO<sub>2</sub>, Fe<sub>3</sub>O<sub>4</sub>, GeO<sub>2</sub>, TiO, ZnO, BN, and C.  
45

The protection layer **109** and the lubricant layer **110** are provided on the surface portion of the magnetic recording medium **401**. Hydrogen, nitrogen, or the like may be added  
50



to a material forming the protection layer **109**. The lubricant layer **110** may be formed by a liquid lubricant layer made of perfluoropolyether.

In one embodiment, a soft magnetic underlayer may be additionally provided in order to improve recording (or write) characteristics of the magnetic recording medium **401**. The soft magnetic underlayer may be made of a noncrystalline (or amorphous) alloy, a microcrystalline alloy, a polycrystal alloy, or the like. The soft magnetic underlayer may have a stacked structure in which layers are antiferromagnetically coupled via an Ru layer.

The soft magnetic underlayer may be made of a material selected from a group consisting of CoFeB, CoFeZr, CoFeTa, CoFeTaZr, CoFeTaB, CoFeNi, CoNiTa, CoNiZr, CoZrB, CoTaZr, CoNbZr, FeAlSi, and FeTaC.

[Magnetic Storage Apparatus]

FIG. **3** is a perspective view illustrating an example of a magnetic storage apparatus in one embodiment of the present invention.

A magnetic storage apparatus illustrated in FIG. **3** includes a plurality of magnetic recording media **401**, a driving mechanism **402** that drives the magnetic recording media **401** in a recording direction, a plurality of magnetic heads **403**, a head moving mechanism **404** that moves the magnetic heads **403**, and a signal processor **405** that are accommodated within a casing **400**. In this example, the magnetic storage apparatus employs the heat assisted recording method. In addition, the plurality of magnetic recording media **401** are heat assisted magnetic disks.

Hence, the driving mechanism **402** rotates the plurality of magnetic recording media **401**, that is, the heat assisted magnetic disks, in the recording direction. Each magnetic head **403** includes a recording (or write) part that records (or writes) signals to a corresponding one of the plurality of magnetic recording media **401**, and a reproducing (or read) part that reproduces (or reads) signals from the corresponding one of the plurality of magnetic recording media **401**. The head moving mechanism **404** moves the magnetic heads **403** relative to the plurality of magnetic recording media **401**. The signal processor **405** processes signals that are input to the magnetic heads **403** to be recorded on the plurality of magnetic recording media **401**, and processes signals that are reproduced from the plurality of magnetic recording media **401** by the magnetic heads **403** and output from the magnetic heads **403**.

FIG. **4** is a cross sectional view schematically illustrating a structure of the magnetic head illustrated in FIG. **3**. As illustrated in FIG. **4**, the magnetic head **403** includes a recording head **508** and a reproducing head **511**.

The recording head **508** includes a main magnetic pole **501**, an auxiliary magnetic pole **502**, a coil **503** that generates a magnetic field, a laser diode **504** that generates laser light **505**, a near-field light generator (or near-field light generating element) **506** that generates near-field light for heating the magnetic recording medium **401**, and a waveguide **507**. The waveguide **507** guides the laser light **505** generated from the laser diode **504** to the near-field light generator **506** that is provided at a tip end of the magnetic head **403**.

The reproducing head **511** includes a reproducing element **511**, such as a TMR (Tunneling Magneto-Resistive) element or the like, that is sandwiched between a pair of shields **509**.

The magnetic storage apparatus illustrated in FIG. **3** includes the magnetic recording media **401** that enable the laser diode current LDI and the SNR to be satisfactorily balanced. For this reason, it is possible to extend the serviceable life of the magnetic heads **403**, and provide the

magnetic storage apparatus having the magnetic recording media **401** with a high recording density.

[Exemplary Implementations]

Next, exemplary implementations according to the present invention, together with comparison examples, will be described. However, the present invention is not limited to these exemplary implementations, and various variations, modifications, and substitutions may be made without departing from the scope of the present invention.

#### First Embodiment

(Exemplary Implementation EI1-1)

In a first embodiment, the heat assisted magnetic recording medium **401** illustrated in FIG. **1** in accordance with an exemplary implementation EI1-1 was manufactured by the following method.

First, an adhesion layer **102** made of Cr-50 at % Ti (Cr-content of 50 at % and Ti-content of 50 at %) and having a thickness of 50 nm is deposited on a glass substrate **101** having an outer diameter of 2.5 inches, and thereafter heated to 320° C. Next, an orientation control layer **103** made of Cr and having a thickness of 20 nm, a first heat sink layer **104** made of W and having a thickness of 30 nm, a first barrier layer **105** made of MgO having the NaCl type crystal structure and a thickness of 2.5 nm, and a second heat sink layer **106** made of W and having a thickness of 5 nm are successively deposited on the adhesion layer **102**. Further, a second barrier layer **107** made of MgO and having a thickness of 4 nm is deposited on the second heat sink layer **106**, and thereafter heated to 620° C. Next, a magnetic layer **108** made of (Fe-50 at % Pt)-10 mol % SiO<sub>2</sub>-8 mol % BN (alloy-content of 82 mol % of alloy including Fe-content of 50 at % and Pt-content of 50 at %, SiO<sub>2</sub>-content of 10 mol %, and BN-content of 8 mol %) and having a thickness of 8 nm is deposited on the second barrier layer **107**. In addition, a protection layer **109** made of DLC (Diamond-Like Carbon) and having a thickness of 4.0 nm is deposited on the magnetic layer **108**. A liquid lubricant layer **110** made of perfluoropolyether and having a thickness of 1.5 nm is coated on the protection layer **109**.

An XRD (X-Ray Diffraction) spectrum of the heat assisted magnetic recording medium **401** in accordance with the exemplary implementation EI1, manufactured by the above described processes, was measured. A mixture of peaks of L1<sub>0</sub>-FePt(001) and L1<sub>0</sub>-FePt(002), with FCC-FePt (200) was confirmed. In addition, it was confirmed that the Cr orientation control layer **103** displays a (100) orientation, and that a combined peak of the first and second heat sink layers **104** and **106** also displays a (100) orientation.

(Exemplary Implementations EI1-2 to EI1-13)

In the first embodiment, the heat assisted magnetic recording media **401** illustrated in FIG. **1** in accordance with exemplary implementations EI1-2 to EI1-13 were manufactured by the method described above used to manufacture the heat assisted magnetic recording medium **401** in accordance with the exemplary implementation EI1-1, except that materials illustrated in FIG. **5** were used for the first barrier layer **105** of the exemplary implementations EI1-2 to EI1-13. FIG. **5** is a table illustrating configuration and properties of magnetic recording media in the first embodiment and a first comparison example. The first comparison example includes comparison examples CE1-1 to CE1-6 illustrated in FIG. **5**. Hence, FIG. **5** illustrates the material and the thickness of each of the first and second sink layers **104** and **106**, and the first and second barrier layers **105** and **107**, the thermal conductivity of the first barrier layer **105**, a ΔSNR



value, a  $\Delta$ LDI/LDI value, and a CT-TG value of each of the exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-1 to CE1-6. The  $\Delta$ SNR value, the  $\Delta$ LDI/LDI value, and the CT-TG value will be described later.

The materials forming the first barrier layer **105** of the exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-1 to CE1-6 are as follows.

Exemplary Implementation EI1-1: MgO

Exemplary Implementation EI1-2: MgO-46 mol % TiO (MgO-content of 54 mol % and a TiO-content of 46 mol %)

Exemplary Implementation EI1-3: TaN

Exemplary Implementation EI1-4: ZrN

Exemplary Implementation EI1-5: TiN

Exemplary Implementation EI1-6: NbN

Exemplary Implementation EI1-7: HfN

Exemplary Implementation EI1-8: ZrC

Exemplary Implementation EI1-9: TaC

Exemplary Implementation EI1-10: TiC

Exemplary Implementation EI1-11: NbC

Exemplary Implementation EI1-12: MgO-38 mol % TiO-10 mol % TiN (MgO-content of 52 mol %, TiO-content of 38 mol %, and TiN-content of 10 mol %)

Exemplary Implementation EI1-13: MgO-38 mol % TiO-10 mol % TaN (MgO-content of 52 mol %, TiO-content of 38 mol %, and TaN-content of 10 mol %)

Hence, the material forming the first barrier layer **105** is an oxide in the exemplary implementations EI1-1, EI1-2, EI1-12, and EI1-13, a nitride in the exemplary implementations EI1-3 to EI1-7, EI1-12, and EI1-13, and a carbide in the exemplary implementations EI1-8 to EI1-11, and each of these materials has the NaCl type crystal structure. For this reason, the first barrier layer **105** can be epitaxially grown on the first heat sink layer **104** made of W having the BCC crystal structure. In addition, the second heat sink layer **106** made of W can be epitaxially grown on the first barrier layer **105**.

(Comparison Examples CE1-1 to CE1-6)

In the first comparison example, the heat assisted magnetic recording media **401** in accordance with the comparison examples CE1-1 to CE1-6 were manufactured by the method described above used to manufacture the heat assisted magnetic recording medium **401** in accordance with the exemplary implementation EI1-1, except that materials illustrated in FIG. **5** were used for the first barrier layer **105** of the comparison examples CE1-1 to CE1-6.

No first barrier layer **105** is provided in the comparison example CE1-1. The first barrier layer **105** is made of a metal material illustrated in FIG. **5** in each of the comparison examples CE1-2 to CE1-6.

As illustrated in FIG. **5**, a sum of the thicknesses of the first and second heat sink layers **104** and **106** is 35 nm in the heat assisted magnetic recording media **401** in accordance with each of the exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-1 to CE1-6, so that the effects of the first and second heat sink layers **104** and **106** become approximately the same.

Next, the SNR, the laser diode current LDI, and the CT-TG (Cross-Track Thermal-Gradient) were evaluated for each of the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-1 to CE1-6. The CT-TG is the thermal gradient in a cross-track direction on each heat assisted magnetic recording medium **401**.

The SNR, that is an electromagnetic conversion characteristic, was measured by a spin stand tester using a magnetic head having a laser spot heating mechanism. The laser

diode current LDI applied to the laser diode of the magnetic head is adjusted, so that a recording track width (or MWW: Magnetic Write Width), defined as a half-value width of the reproduced signal waveform, becomes 70 nm.

In addition, the same spin stand tester to compute the CT-TG when a Curie temperature  $T_c$  is 700 K.

The SNR is evaluated using the SNR of the heat assisted magnetic recording medium **401** in accordance with the comparison example CE1-1 having no first barrier layer **105**, as a SNR reference value ref1. The  $\Delta$ SNR value of each of exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-2 to CE1-6 is a difference of the SNR of each of the exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-2 to CE1-6 from the SNR reference value ref1 of the comparison example CE1-1.

The laser diode current LDI is evaluated using the laser diode current LDI applied to the laser diode **504** of the magnetic head **403** for the comparison example CE1-1 having no first barrier layer **105**, as a LDI reference value ref2. The LLDI/LDI value for each of the exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-2 to CE1-6 is a ratio a difference of the laser diode current LDI for each of exemplary implementations EI1-1 to EI1-13 and the comparison examples CE1-2 to CE1-6 from the LDI reference value ref2 for the comparison example CE1-1, with respect to the LDI reference value ref2 for the comparison example CE1-1.

The thermal conductivities of the materials forming the first barrier layer **105** have values illustrated in FIG. **5**. The thermal conductivities of the oxides, the nitrides, and the carbides illustrated in FIG. **5** and forming the first barrier layer **105** have values referenced from Werner Martienssen et al. (Eds.), "Springer Handbook of Condensed Matter and Materials Data", pp. 440, 460, 462, 464, 468, and 470, ISBN: 9783540443766, Springer (pub.), 2005. On the other hand, the thermal conductivities of the metals illustrated in FIG. **5** and forming the first barrier layer **105** have values referenced from "Metal Data Book", pp. 12-13, Revised 4th Edition, series by The Japan Institute of Metals and Materials, Maruzen Co., Ltd. (pub.), 2004.

In the case of the exemplary implementations EI1-1 to EI1-13 in which the first barrier layer **105** is made of the oxide, the nitride, or the carbide, the  $\Delta$ SNR values of the heat assisted magnetic recording media **401** were within error ranges. The SNR values for the exemplary implementations EI1-1 to EI1-13 were substantially the same as the SNR reference value ref1 of the comparison example CE1-1 in which no first barrier layer **105** is provided.

In contrast, in the case of the exemplary implementations EI1-1 to EI1-13, the laser diode current LDI decreased by approximately 3.5% to 5.4% with respect to the reference LDI ref2 for the comparison example CE1-1 in which no first barrier layer **105** is provided.

Accordingly, it was confirmed that, in the case of the exemplary implementations EI1-1 to EI1-13 having the first barrier layer **105** made of the oxide, the nitride, or the carbide, the laser diode current LDI can be reduced without deteriorating (or decreasing) the SNR.

Among the exemplary implementations EI1-1 to EI1-13, it was confirmed that the reduction in the laser diode current LDI is slightly larger when the first barrier layer **105** is made of the nitride or carbide of Zr or Ti, or includes MgO, as compared to when the first barrier layer **105** is made of the nitride or carbide of Ta, Nb, or Hf.

In contrast, it was confirmed that no reduction occurs in the laser diode current LDI for the comparison examples CE1-1 to CE1-6 in which the first barrier layer **105** is made



of a metal material. In addition, no improvement of the SNR was confirmed for these comparison examples CE1-1 to CE1-6. Accordingly, it was confirmed from these results that there is no improvement in the balance between the SNR and the laser diode current LDI when the metal material is used for the first barrier layer **105**, but rather, that the balance between the SNR and the laser diode current LDI deteriorates.

It was also confirmed from FIG. 5 that the CT-TG of the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI1-1 to EI1-13 increases by approximately 30% when compared to the CT-TG of the heat assisted magnetic recording media **401** in accordance with the comparison examples CE1-1 to CE1-6. In other words, it was confirmed that the thermal gradient improves for the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI1-1 to EI1-13 improves when compared to the thermal gradient of the heat assisted magnetic recording media **401** in accordance with the comparison examples CE1-1 to CE1-6.

The thermal conductivities of the materials forming the first barrier layer **105** of the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI1-1 to EI1-13 differ depending on the materials. However, the thermal conductivity of each of the materials forming the first barrier layer **105** of the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI1-1 to EI1-13 is considerably lower than the thermal conductivity of 174 W/m·K of W forming the first and second heat sink layers **104** and **106**.

#### Second Embodiment

(Exemplary Implementation EI2-1)

In a second embodiment, the heat assisted magnetic recording medium **401** illustrated in FIG. 1 in accordance with an exemplary implementation EI2-1 was manufactured by the following method.

First, an adhesion layer **102** made of Cr-50 at % Ti and having a thickness of 50 nm is deposited on a glass substrate **101** having an outer diameter of 2.5 inches, and thereafter heated to 320° C. Next, an orientation control layer **103** made of Cr and having a thickness of 20 nm, a first heat sink layer **104** made of W and having a thickness of 25 nm, a first barrier layer **105** made of ZrN having a thickness of 2.5 nm, and a second heat sink layer **106** made of W-10 at % Ta and having a thickness of 5 nm are successively deposited on the adhesion layer **102**. Further, a second barrier layer **107** made of MgO having the NaCl crystal structure and a thickness of 4 nm is deposited on the second heat sink layer **106**, and thereafter heated to 650° C. Next, a first magnetic layer made of (Fe-50 at % Pt)-35 mol % C and having a thickness of 4 nm is deposited on the second barrier layer **107**, and a second magnetic layer made of (Fe-50 at % Pt)-12 mol % SiO<sub>2</sub> and a thickness of 4 nm is deposited on the first magnetic layer. The first and second magnetic layers are successively stacked to form a magnetic layer **108**. In addition, a protection layer **109** made of DLC and having a thickness of 4 nm is deposited on the magnetic layer **108**. A liquid lubricant layer **110** made of perfluoropolyether and having a thickness of 1.5 nm is coated on the protection layer **109**.

(Exemplary Implementations EI2-2 to EI2-4)

In the second embodiment, the heat assisted magnetic recording media **401** illustrated in FIG. 1 in accordance with exemplary implementations EI2-2, EI2-3, and EI2-4 were manufactured by the method described above used to manu-

facture the heat assisted magnetic recording medium **401** in accordance with the exemplary implementation EI2-1, except that the thickness of the first heat sink layer **104** is 30 nm, 35 nm, and 40 nm, respectively, as illustrated in FIG. 6. FIG. 6 is a table illustrating configuration and properties of magnetic recording media in the second embodiment and a second comparison example. The second comparison example includes comparison examples CE2-1 to CE2-3 illustrated in FIG. 6. Hence, FIG. 6 illustrates the material and the thickness of each of the first and second sink layers **104** and **106**, and the first and second barrier layers **105** and **107**, the SNR value, the laser diode current LDI, the MWW value, and the CT-TG value of each of the exemplary implementations EI2-1 to EI2-4 and the comparison examples CE2-1 to CE2-3. The MWW value is defined as the half-value width of the reproduced signal waveform, used when confirming the SNR and the laser diode current LDI.

(Comparison Examples CE2-1 to CE2-3)

In the second comparison example, the heat assisted magnetic recording media **401** in accordance with the comparison examples CE2-1 to CE2-3 were manufactured by the method described above used to manufacture the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI2-1 to EI2-3, except that no first barrier layer **105** is provided in the comparison examples CE2-1 to CE2-3.

The heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI2-1 to EI2-3 in which the material forming the first barrier layer **105** is a nitride, and the heat assisted magnetic recording media **401** in accordance with the comparison examples CE2-1 to CE2-3 having no first barrier layer **105**, were compared for cases in which the thicknesses of the first heat sink layer **104** are the same, respectively. From results of this comparison, it was confirmed that the SNRs are substantially the same for the exemplary implementations EI2-1 to EI2-3 and the comparison examples CE2-1 to CE2-3, respectively. On the other hand, under the condition in which the thicknesses of the first heat sink layer **104** are the same, it was confirmed that the laser diode currents LDI for the exemplary implementations EI2-1 to EI2-3 are reduced by approximately 3 mA with respect to the laser diode currents LDI for the comparison examples CE2-1 to CE2-3, respectively. Accordingly, from these results, it was confirmed that the exemplary implementations EI2-1 to EI2-3 and also EI2-4 can reduce the laser diode current LDI without deteriorating the SNR, when compared to the comparison examples CE2-1 to CE2-3.

#### Third Embodiment

(Exemplary Implementation EI3-1)

In a third embodiment, the heat assisted magnetic recording medium **401** illustrated in FIG. 1 in accordance with an exemplary implementation EI3-1 was manufactured by the following method.

First, an adhesion layer **102** made of Cr-50 at % Ti and having a thickness of 50 nm is deposited on a glass substrate **101** having an outer diameter of 2.5 inches, and thereafter heated to 300° C. Next, an orientation control layer **103** made of Cr-10 at % Ti and having a thickness of 30 nm, a first heat sink layer **104** made of W-5 mol % SiO<sub>2</sub> (W-content of 95 mol % and SiO<sub>2</sub>-content of 5 mol %) and having a thickness of 25 nm, a first barrier layer **105** made of NbC having a thickness of 1 nm, and a second heat sink layer **106** made of W-5 mol % SiO<sub>2</sub> and having a thickness of 5 nm are



successively deposited on the adhesion layer **102**. Further, a second barrier layer **107** made of MgO having the NaCl crystal structure and a thickness of 5 nm is deposited on the second heat sink layer **106**, and thereafter heated to 600° C. Next, a magnetic layer **108** made of (Fe-46 at % Pt)-15 mol % SiO<sub>2</sub> and having a thickness of 8 nm is deposited on the second barrier layer **107**. In addition, a protection layer **109** made of DLC and having a thickness of 4 nm is deposited on the magnetic layer **108**. A liquid lubricant layer **110** made of perfluoropolyether and having a thickness of 1.5 nm is coated on the protection layer **109**.

(Exemplary Implementations EI3-2 to EI3-5)

In the third embodiment, the heat assisted magnetic recording media **401** illustrated in FIG. 1 in accordance with exemplary implementations EI3-2, EI3-3, EI3-4, and EI3-5 were manufactured by the method described above used to manufacture the heat assisted magnetic recording medium **401** in accordance with the exemplary implementation EI3-1, except that the thickness of the first barrier layer **105** is 2.5 nm, 5 nm, 10 nm, and 20 nm, respectively, as illustrated in FIG. 7. FIG. 7 is a table illustrating configuration and properties of magnetic recording media in the third embodiment and a third comparison example. The third comparison example includes a comparison example CE3-1 illustrated in FIG. 7. Hence, FIG. 7 illustrates the material and the thickness of each of the first and second sink layers **104** and **106**, and the first and second barrier layers **105** and **107**, the  $\Delta$ SNR value, and the  $\Delta$ LDI/LDI of each of the exemplary implementations EI3-1 to EI3-5 and the comparison example CE3-1. The recording track width (or MWW), defined as the half-value width of the reproduced signal waveform, was 70 nm when confirming the SNR and the laser diode current LDI.

(Comparison Example CE3-1)

In the third comparison example, the heat assisted magnetic recording medium **401** in accordance with the comparison example CE3-1 was manufactured by the method described above used to manufacture the heat assisted magnetic recording media **401** in accordance with the exemplary implementations EI3-1 to EI3-5, except that no first barrier layer **105** is provided in the comparison example CE3-1.

As illustrated in FIG. 7, a sum of the thicknesses of the first and second heat sink layers **104** and **106** is 30 nm in the heat assisted magnetic recording media **401** in accordance with each of the exemplary implementations EI3-1 to EI3-5 and the comparison example CE3-1, so that the effects of the first and second heat sink layers **104** and **106** become approximately the same.

The SNR is evaluated using the SNR of the heat assisted magnetic recording medium **401** in accordance with the comparison example CE3-1 having no first barrier layer **105**, as a SNR reference value ref3. The  $\Delta$ SNR value of each of exemplary implementations EI3-1 to EI3-5 is a difference of the SNR of each of the exemplary implementations EI3-1 to EI3-5 from the SNR reference value ref3 of the comparison example CE3-1.

The laser diode current LDI is evaluated using the laser diode current LDI applied to the laser diode **504** of the magnetic head **403** for the comparison example CE3-1 having no first barrier layer **105**, as a LDI reference value ref4. The  $\Delta$ LDI/LDI value for each of the exemplary implementations EI3-1 to EI3-5 is a ratio a difference of the laser diode current LDI for each of exemplary implementations EI3-1 to EI3-5 from the LDI reference value ref4 for the comparison example CE3-1, with respect to the LDI reference value ref4 for the comparison example CE3-1.

In the case of the exemplary implementations EI3-1 to EI3-5 in which the first barrier layer **105** is made of the carbide, the tSNR values of the heat assisted magnetic recording media **401** were within error ranges. The SNR values for the exemplary implementations EI3-1 to EI3-5 were substantially the same as the SNR reference value ref3 of the comparison example CE3-1 in which no first barrier layer **105** is provided.

In contrast, in the case of the exemplary implementations EI3-1 to EI3-5, the laser diode current LDI decreased by approximately 2.2% to 5.1% with respect to the reference LDI ref4 for the comparison example CE3-1 in which no first barrier layer **105** is provided.

Accordingly, it was confirmed that, in the case of the exemplary implementations EI3-1 to EI3-5 having the first barrier layer **105** made of the carbide, the laser diode current LDI can be reduced without deteriorating (or decreasing) the SNR.

Embodiments and exemplary implementations of the present invention can provide a magnetic recording medium and a magnetic storage apparatus, capable of reducing the laser diode current LDI applied to the laser diode of the magnetic head without deteriorating the SNR.

Although the embodiments and the exemplary implementations are numbered with, for example, "first," "second," "third," etc., the ordinal numbers do not imply priorities of the embodiments and the exemplary implementations.

Further, the present invention is not limited to these embodiments and exemplary implementations, but various variations and modifications may be made without departing from the scope of the present invention.

What is claimed is:

1. A magnetic recording medium comprising:

a substrate;

a first heat sink layer provided on the substrate;

a first barrier layer provided on the first heat sink layer;  
a second heat sink layer provided on the first barrier layer;  
and

a magnetic layer provided on the second heat sink layer, wherein the magnetic layer is made of a material including a first main component that is an alloy having a L1<sub>0</sub> crystal structure and a content of 50 at % or higher, or content of 50 mol % or higher, and

wherein the first barrier layer is made of a material including a second main component that is one of an oxide, a nitride, and a carbide having a content of 50 at % or higher, or content of 50 mol % or higher.

2. The magnetic recording medium as claimed in claim 1, wherein the second main component has a NaCl type crystal structure.

3. The magnetic recording medium as claimed in claim 2, wherein the second main component having the NaCl type crystal structure is selected from a group consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, ZrN, VN, CrN, TiC, TaC, NbC, HfC, and ZrC.

4. The magnetic recording medium as claimed in claim 1, wherein the first barrier layer has a thickness in a range of 1 nm to 10 nm.

5. The magnetic recording medium as claimed in claim 1, wherein the second main component has a thermal conductivity of 80 W/m·K or lower.

6. The magnetic recording medium as claimed in claim 1, wherein the second heat sink layer has a thickness less than a thickness of the first heat sink layer.

7. The magnetic recording medium as claimed in claim 1, wherein each of the first heat sink layer and the second heat sink layer is made of a material including a third main



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component that is selected from a group consisting of Ag, Au, Al, Cu, Rh, Mo, and W, and having a content of 50 at % or higher, or content of 50 mol % or higher.

8. The magnetic recording medium as claimed in claim 1, wherein each of the first heat sink layer and the second heat sink layer is made of a material including a third main component that has a thermal conductivity of 100 W/m·K or higher.

9. The magnetic recording medium as claimed in claim 1, further comprising:

a second barrier layer provided between the second heat sink layer and the magnetic layer,

wherein the second barrier layer is made of a material including a main component having a NaCl type crystal structure and selected from a group consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, and TiC, and having a content of 50 at % or higher, or content of 50 mol % or higher.

10. A magnetic storage apparatus comprising:

a magnetic recording medium;

a magnetic head configured to write information to and read information from the magnetic recording medium; and

a casing configured to accommodate the magnetic recording medium and the magnetic head,

wherein the magnetic head includes a laser light generator configured to generate laser light, a waveguide configured to guide the laser light to a tip end of the magnetic head, and a near-field light generator configured to generate near-field light that heats the magnetic recording medium,

wherein the magnetic recording medium includes a substrate, a first heat sink layer, a first barrier layer, a second heat sink layer, and a magnetic layer that are successively stacked,

wherein the magnetic layer is made of a material including a first main component that is an alloy having a L1<sub>0</sub> crystal structure and a content of 50 at % or higher, or content of 50 mol % or higher, and

wherein the first barrier layer is made of a material including a second main component that is one of an oxide, a nitride, and a carbide having a content of 50 at % or higher, or content of 50 mol % or higher.

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11. The magnetic storage apparatus as claimed in claim 10, wherein the second main component of the first barrier layer of the magnetic recording medium has a NaCl type crystal structure and is selected from a group consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, ZrN, VN, CrN, TiC, TaC, NbC, HfC, and ZrC.

12. The magnetic storage apparatus as claimed in claim 10, wherein the first barrier layer of the magnetic recording medium has a thickness in a range of 1 nm to 10 nm.

13. The magnetic storage apparatus as claimed in claim 10, wherein the second main component of the first barrier layer of the magnetic recording medium has a thermal conductivity of 80 W/m·K or lower.

14. The magnetic storage apparatus as claimed in claim 10, wherein the second heat sink layer of the magnetic recording medium has a thickness less than a thickness of the first heat sink layer.

15. The magnetic storage apparatus as claimed in claim 10, wherein each of the first heat sink layer and the second heat sink layer of the magnetic recording medium is made of a material including a third main component that is selected from a group consisting of Ag, Au, Al, Cu, Rh, Mo, and W, and having a content of 50 at % or higher, or content of 50 mol % or higher.

16. The magnetic storage apparatus as claimed in claim 10, wherein each of the first heat sink layer and the second heat sink layer of the magnetic recording medium is made of a material including a third main component that has a thermal conductivity of 100 W/m·K or higher.

17. The magnetic storage apparatus as claimed in claim 10, wherein the magnetic recording medium further includes:

a second barrier layer provided between the second heat sink layer and the magnetic layer,

wherein the second barrier layer is made of a material including a main component having a NaCl type crystal structure and selected from a group consisting of MgO, TiO, NiO, TiN, TaN, NbN, HfN, and TiC, and having a content of 50 at % or higher, or content of 50 mol % or higher.

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